



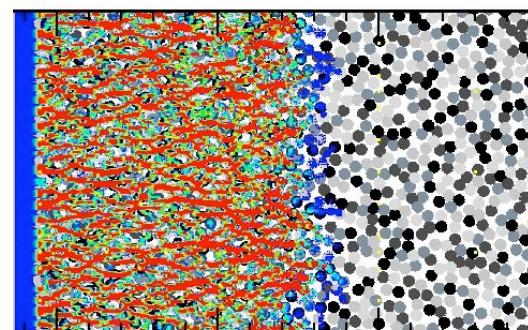
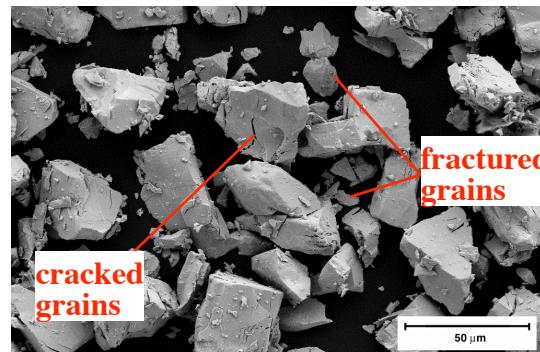
Dynamic Behavior of Granular Ceramics: Experiments and Simulations

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Aerospace Engineering Department
University of Illinois at Urbana-Champaign

October 11, 2010



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- **Introduction to Shock and High-Pressure Physics**
- **Introduction to Granular Materials**
- **Planar Impact Experiments**
- **Mesoscale Modeling**
- **Other Experimental Work**
- **Conclusions**

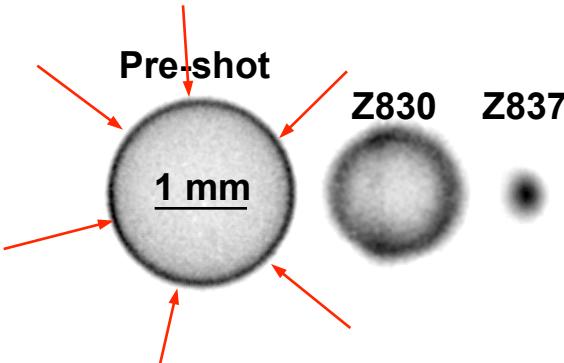


Why Do We Need To Know the Behavior of Materials Under Extreme Conditions?

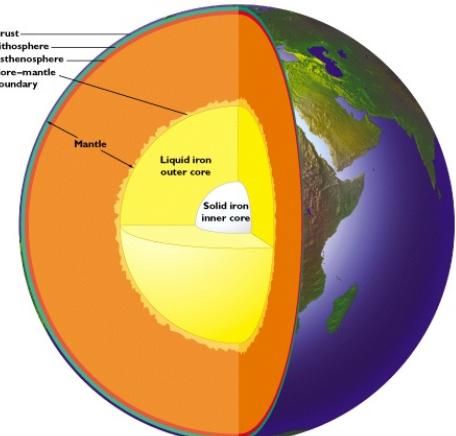
- weapons applications (warheads, armor, etc.)
- explosives behavior and applications



- inertial confinement fusion



- planetary science ($P \sim 360$ GPa, $T \sim 7000$ K)



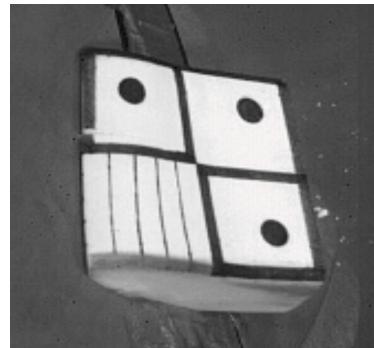


Applications of Shock and Impact Physics in Aerospace Engineering

Pluto New Horizons



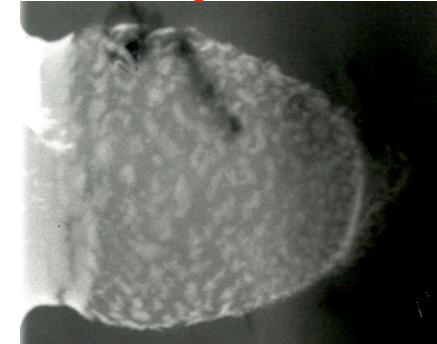
- internal blast
- runway debris & small arms fire
- military aviation and weapons design



SWRI foam impact expt.

- impact of asteroids or orbital debris ($V=8-15$ km/s)
- launch safety for radiological materials (RTG's) or reactors (Prometheus mission)
- launch debris (foam, ice, etc.)

hypervelocity impact



Solar Probe

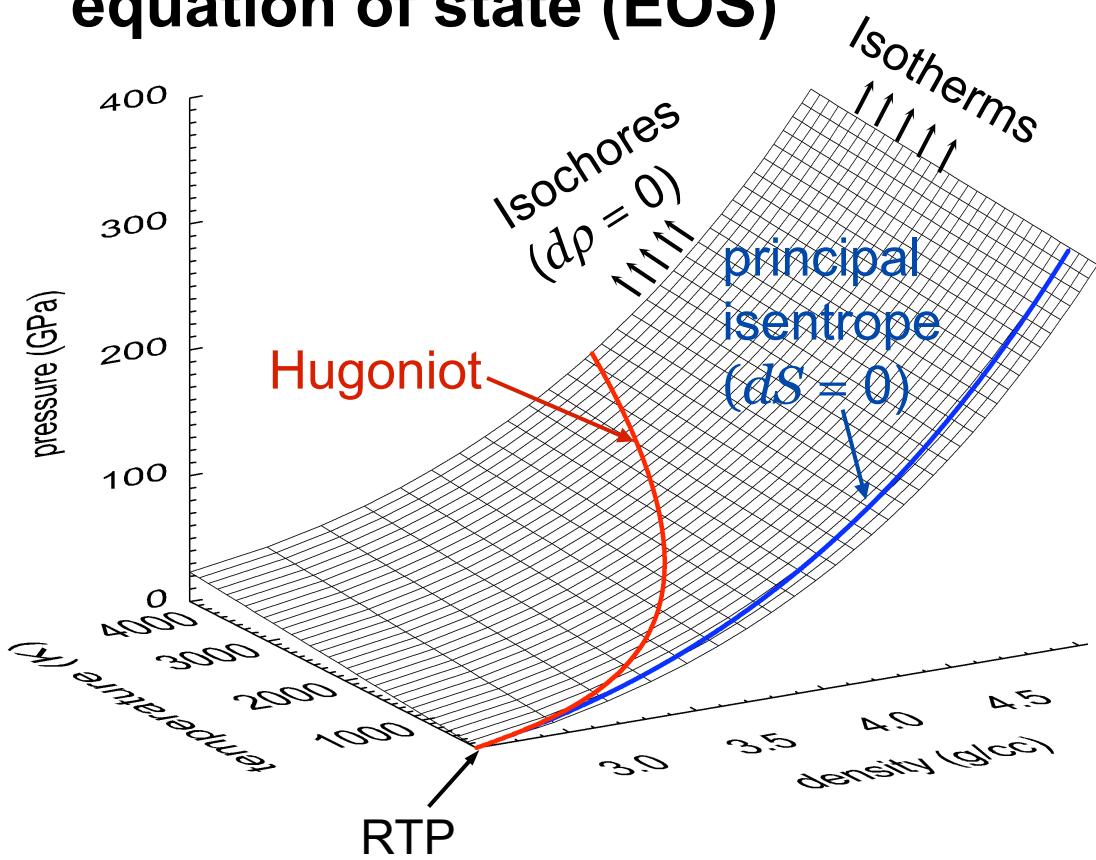
- $100 \mu\text{m}$ particles
- up to 300 km/s velocities
- $P_{\max} \sim 100 \text{ TPa}$, $T_{\max} \sim 10^6 \text{ K}$



Material Behavior: EOS & Constitutive Aspects

M. Knudson,
M. Desjarlais

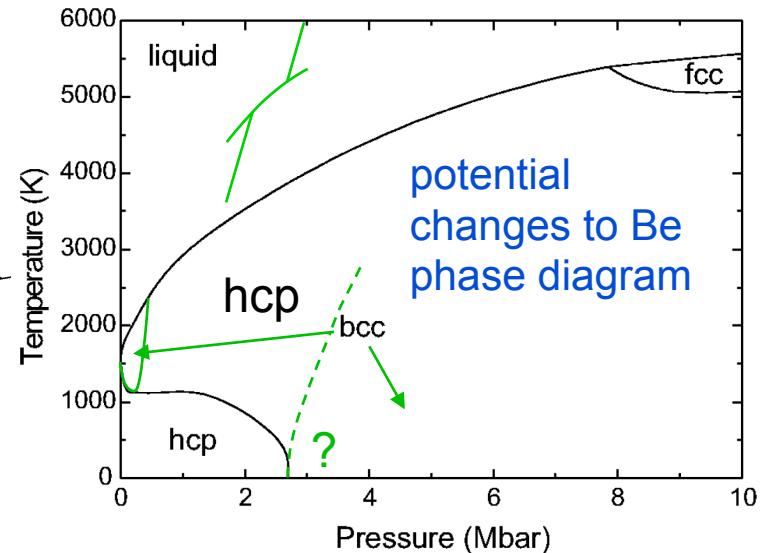
equation of state (EOS)



one thermodynamic state variable as a function of two others:

$$\text{pressure } P = P(r, T)$$

$$\text{Helmholtz energy } f = f(v, T)$$



Also: strength, damage, spall (tensile failure), compaction



What is a Shock Wave?

- A “discontinuous” wave that moves at a fixed velocity (if steady)
 - wave front moves at speed U_s (*shock velocity*)
 - shocked material moves at speed u_p (*particle or mass velocity*)
 - uniaxial strain condition ($\varepsilon_y = \varepsilon_z = \varepsilon_{xy} = \varepsilon_{yz} = \varepsilon_{xz} = 0$)

shocked material	unshocked material
σ_x, ρ, E	$\sigma_x = 0, \rho_o,$ $E_o, u_p = 0,$
$u_p \rightarrow$	$U_s \rightarrow$

$x \longrightarrow$
(fixed wrt unshocked material)

- States ahead and behind shock assumed to be in thermodynamic equilibrium
 - well defined temperature in each state
 - described by equilibrium thermodynamics
- Shock compression is adiabatic
 - very fast process (< 1 ns)
 - irreversible (i.e. NOT isentropic)
 - temperature *typically* increases



Conservation Equations and the Shock Hugoniot

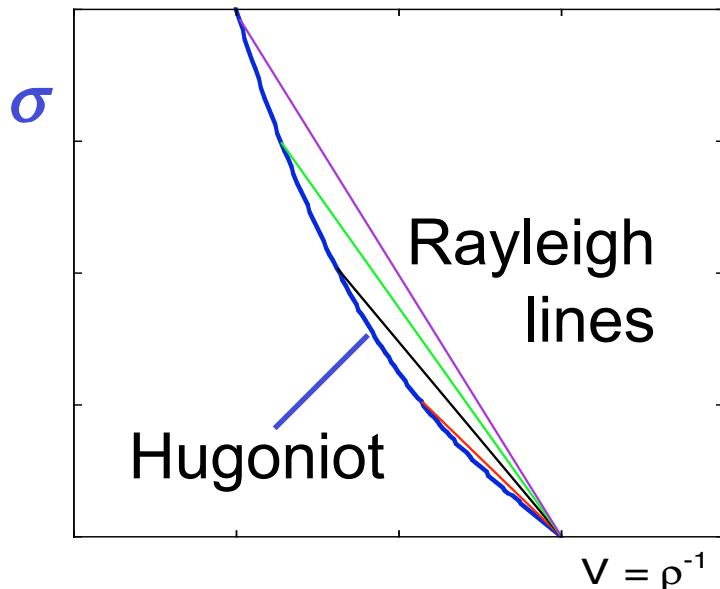
- Five variables: σ_x , u_p , U_s , ρ , and E
- Three conservation relationships (Rankine-Hugoniot jump conditions)
 - By measuring two variables (typically σ_x , u_p , or U_s), the other three can be determined

conservation of

mass: $\rho_0 U_s = \rho (U_s - u_p)$

momentum: $\sigma_x = \rho_0 U_s u_p$

energy: $E - E_0 = 0.5 \sigma_x (V_0 - V)$



material loads along the Rayleigh line, so the Hugoniot is a collection of end states, not a material response curve
the Hugoniot is not a complete equation of state (EOS)!



Gas Guns to Generate Shock Waves



Single Stage Gun 100mm



~1 km/s
~30 GPa

Propellant Gun 89mm



~2 km/s
~100 GPa

Two-Stage Gun 29mm



~8 km/s
~700 GPa

gas guns

- launch thin plates (mm's) at high velocities
- well-posed, repeatable initial conditions
- sample is in uniaxial strain
- used to study material behavior at high pressures and strain rates
- usable in laboratory setting

Three-Stage Gun 17mm



~16 km/s
~2 TPa

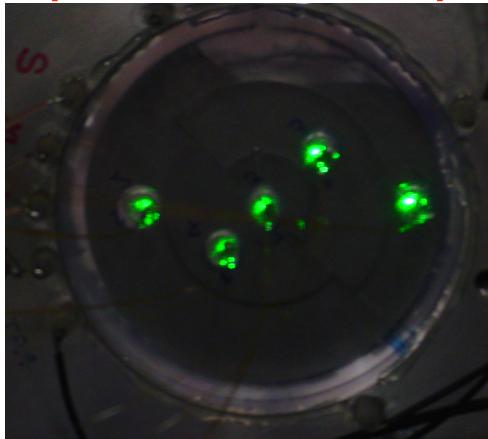
Chhabildas, L. C., Dunn, J. E., Reinhart, W. D., and Miller, J. M. (1993). "An impact technique to accelerate flier plates to velocities over 12 km/s," *Int. J. Impact Eng.* **14**, 121-132.

also: explosives, lasers, magnetic loading (Z)

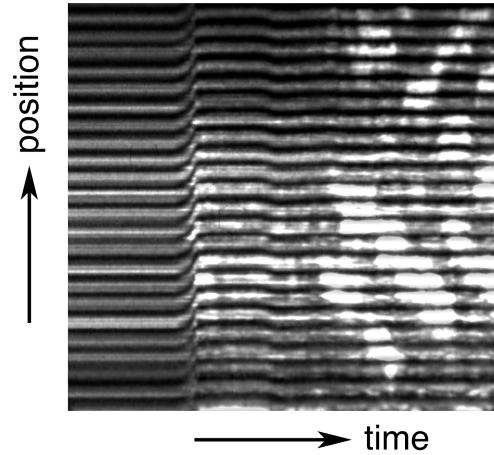


Diagnostics for Dynamic Experiments

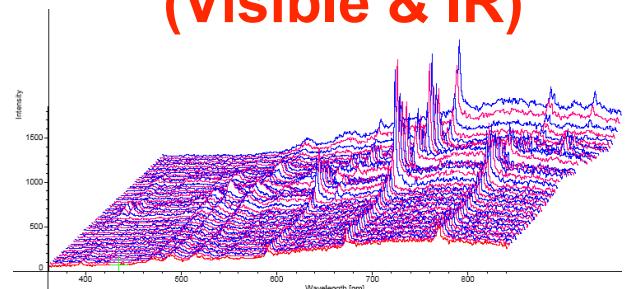
Velocity Interferometry (VISAR & PDV)



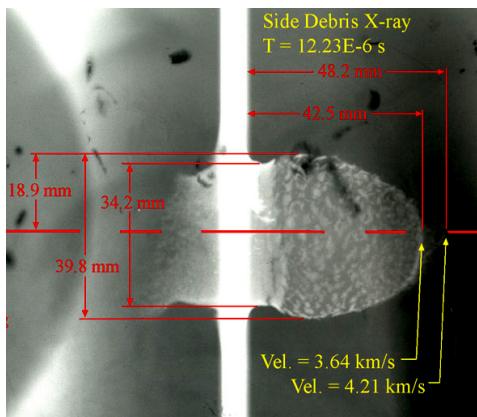
Line-VISAR



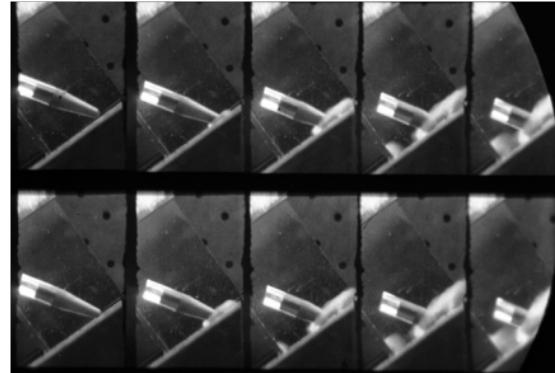
Time-Resolved Spectroscopy (Visible & IR)



Flash X-rays



High-Speed Photography



Pressure Gauges

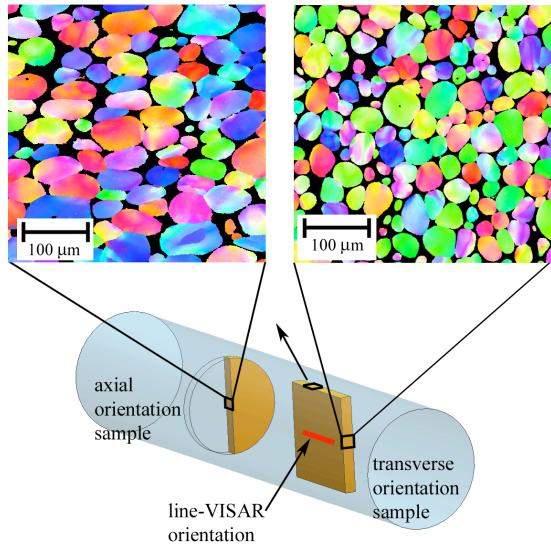


Advanced Diagnostics: pRad, synchrotron, etc.

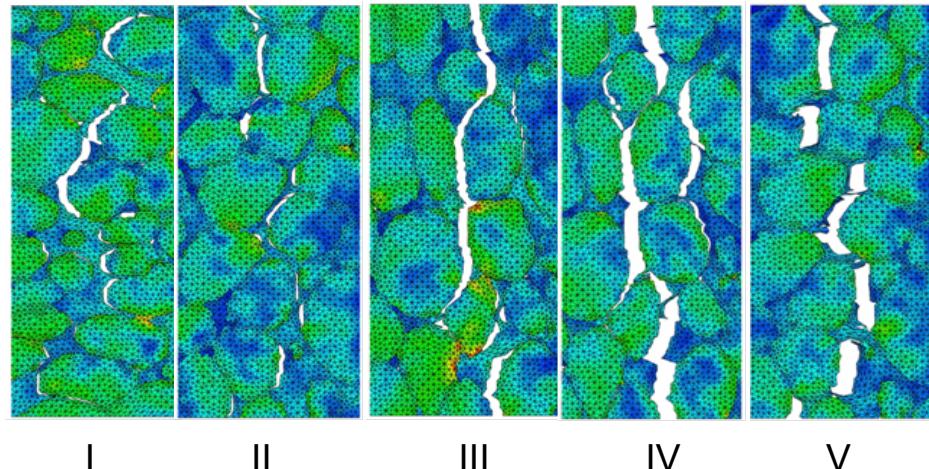
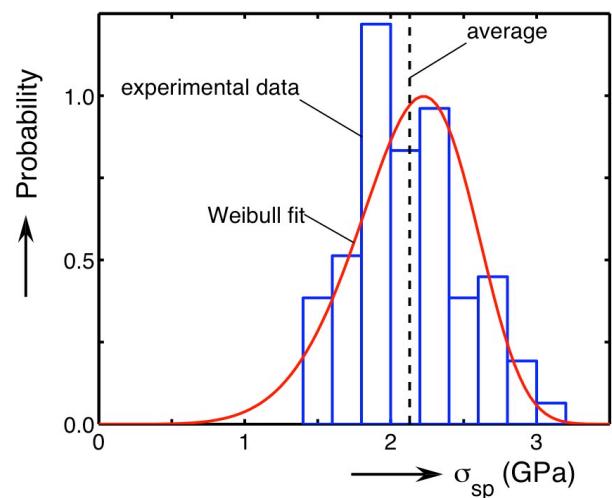
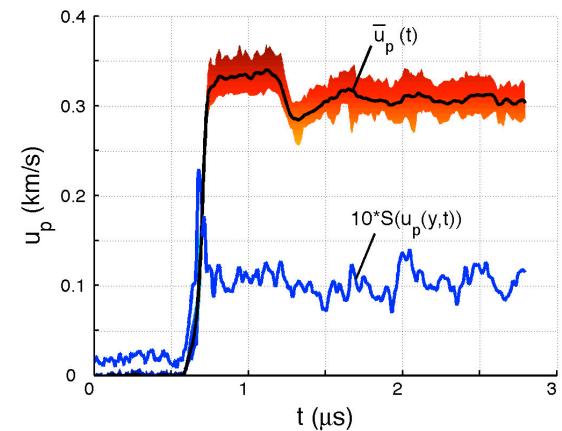
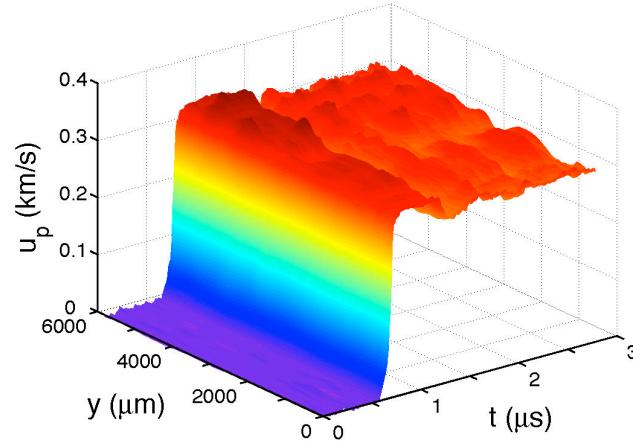


Heterogeneous and Statistical Aspects of Spall

J. Clayton,
T. Vogler



WHA - tungsten heavy alloy



Vogler, T. J., and Clayton, J. D. (2008). "Heterogeneous deformation and spall of an extruded tungsten alloy: plate impact experiments and crystal plasticity modeling," *J. Mech. Phys. Solids* 56, 297-335.

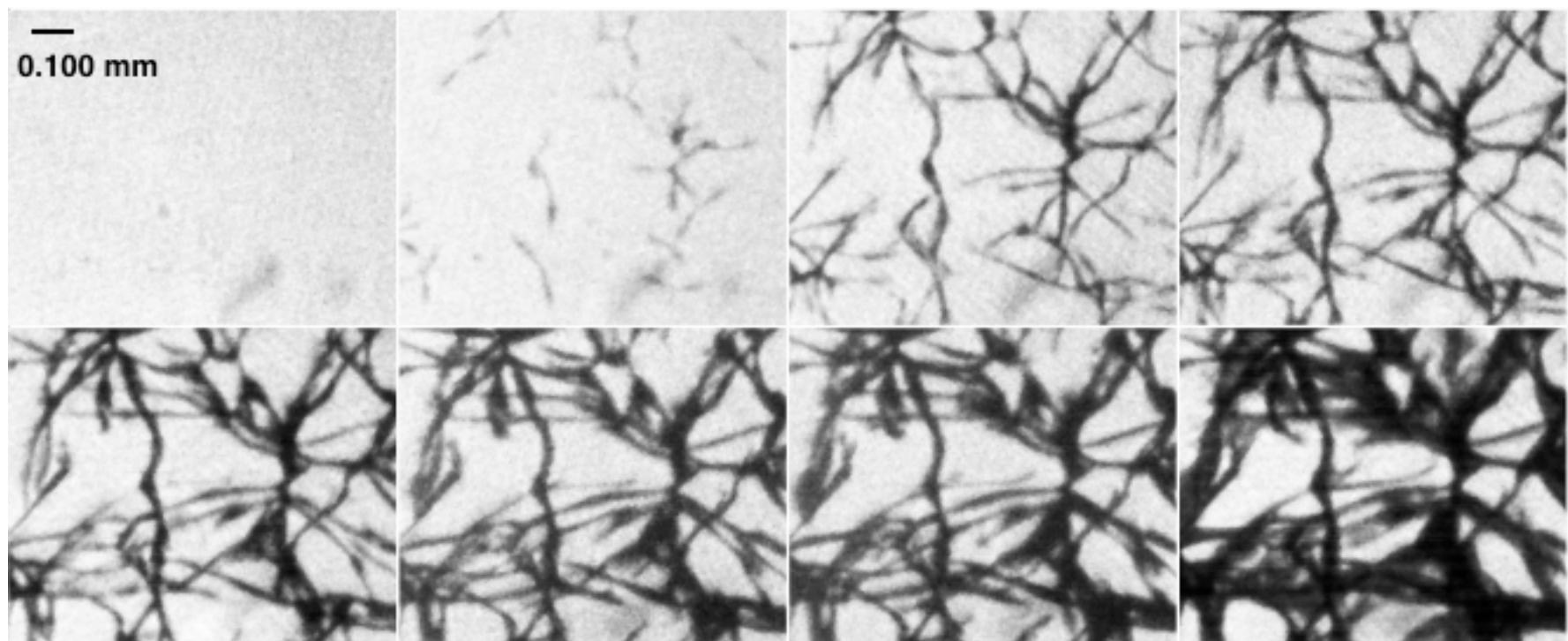


Nanosecond Freezing of Water

- 2.7 GPa (ice VII)
- 25 ns exposure

**$t(\text{ns})$ from
shock arrival =**

230	330	530	630
730	830	930	1530

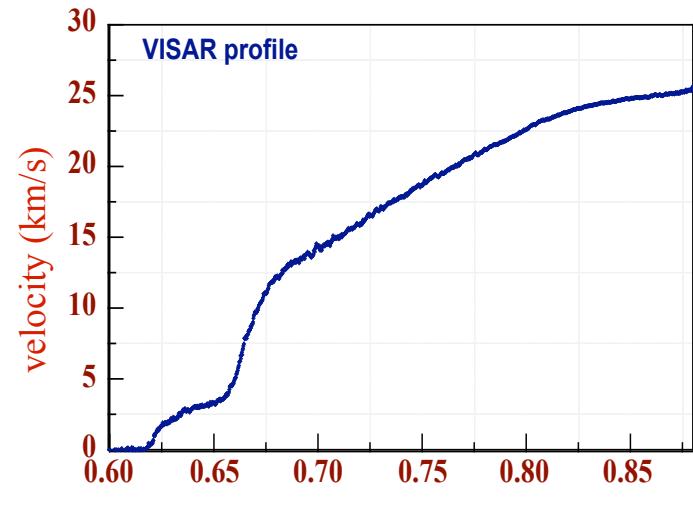
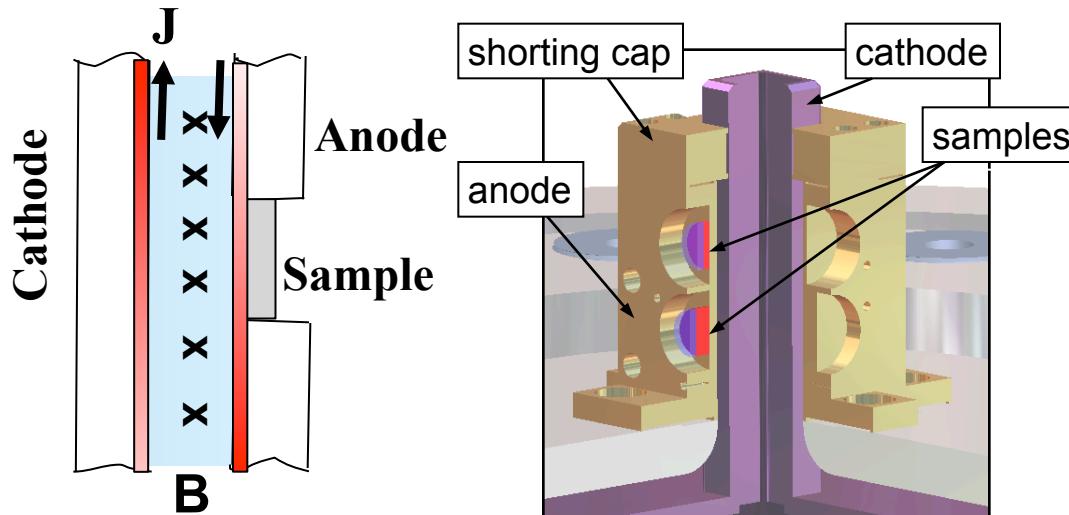
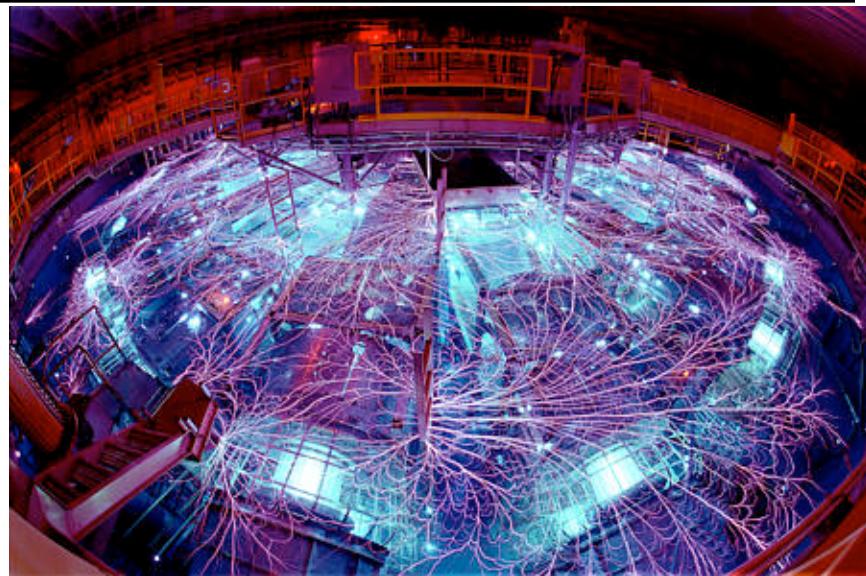


D.H. Dolan and Y.M. Gupta, J. Chem. Phys. **121**, 9050 (2004).



Z Pulsed Power Machine

- Designed for ICF applications
- Generates ~ 26 MA over 100's of ns
- Utilize current to generate magnetic forces
- Magnetic forces create smooth waves in materials
- Waves used for isentropic loading (to ~ 400 GPa) and to launch high-velocity flyer plates (to ~ 40 km/s)

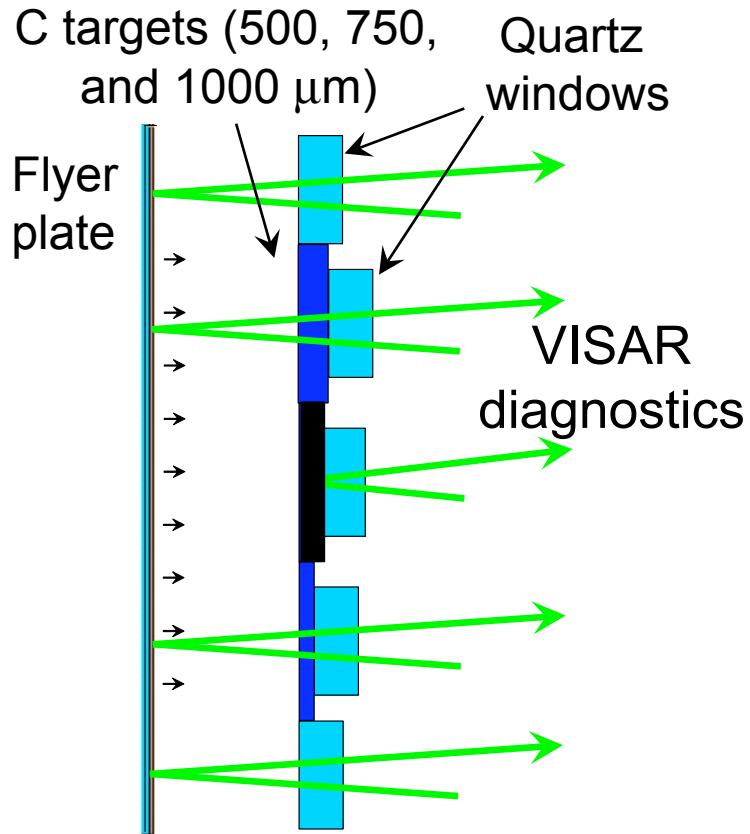


Davis, J.-P., Deeney, C., Knudson, M. D., Lemke, R. L., Pointon, T. D., and Bliss, D. E. (2005). "Magnetically driven isentropic compression to multimegabar pressures using shaped current pulses on the Z accelerator," *Physics of Plasmas* 12, 056310.

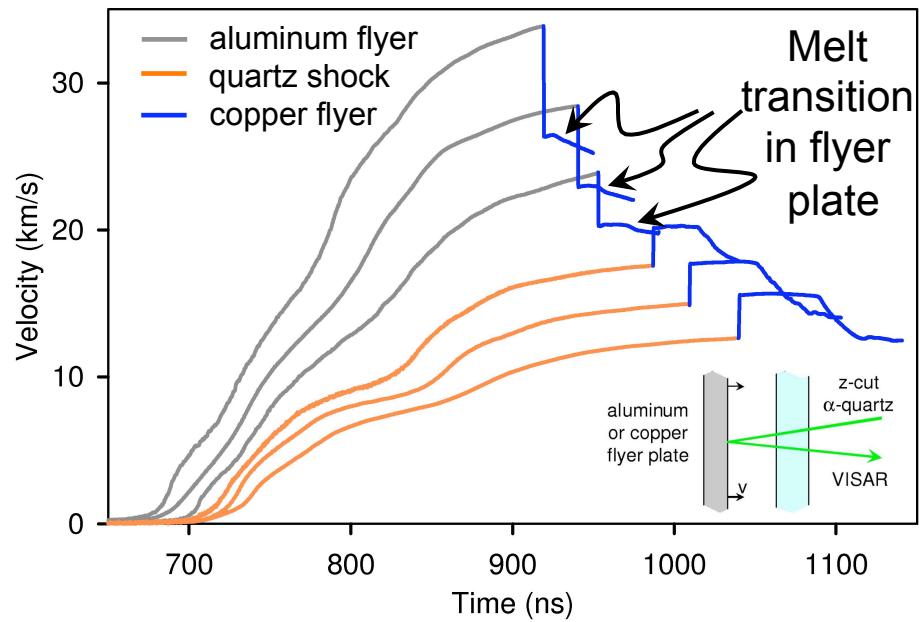


Quartz of Interest as Standard - Window in Z Shots

M. Knudson
M. Desjarlais



Knudson, M. D., M. P. Desjarlais and D. H. Dolan (2008). "Shock-wave exploration of the high-pressure phases of carbon." *Science 322: 1822-1825.*

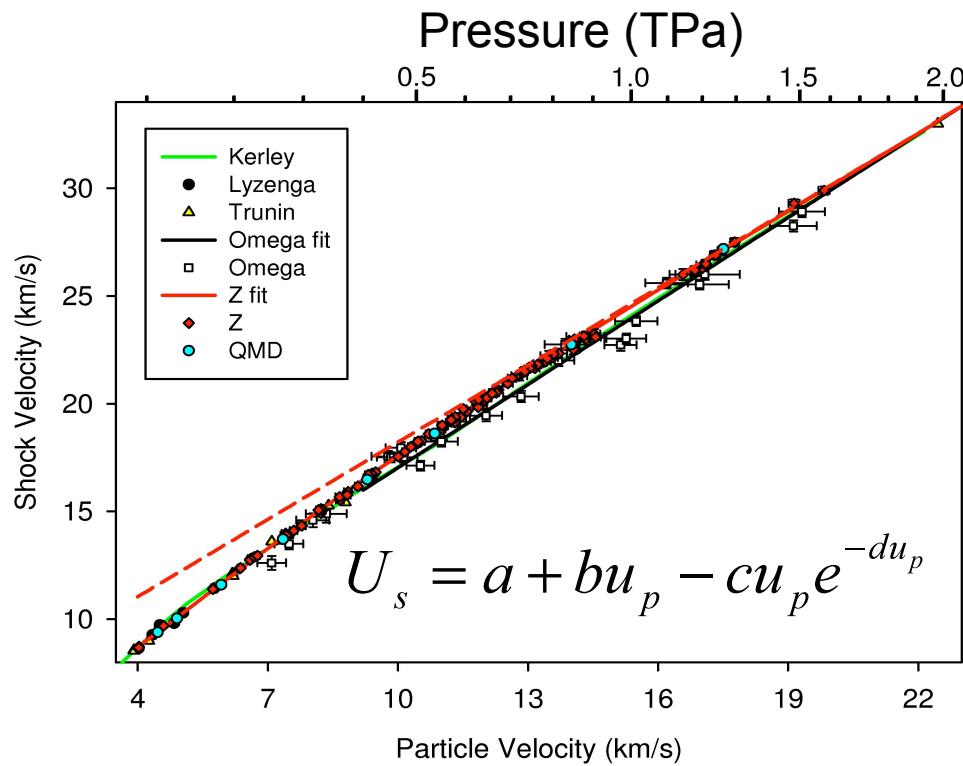


quartz data has large uncertainty and scatter, and $U_s - u_p$ exhibits significant curvature in the several 100 GPa regime; attributed to dissociation

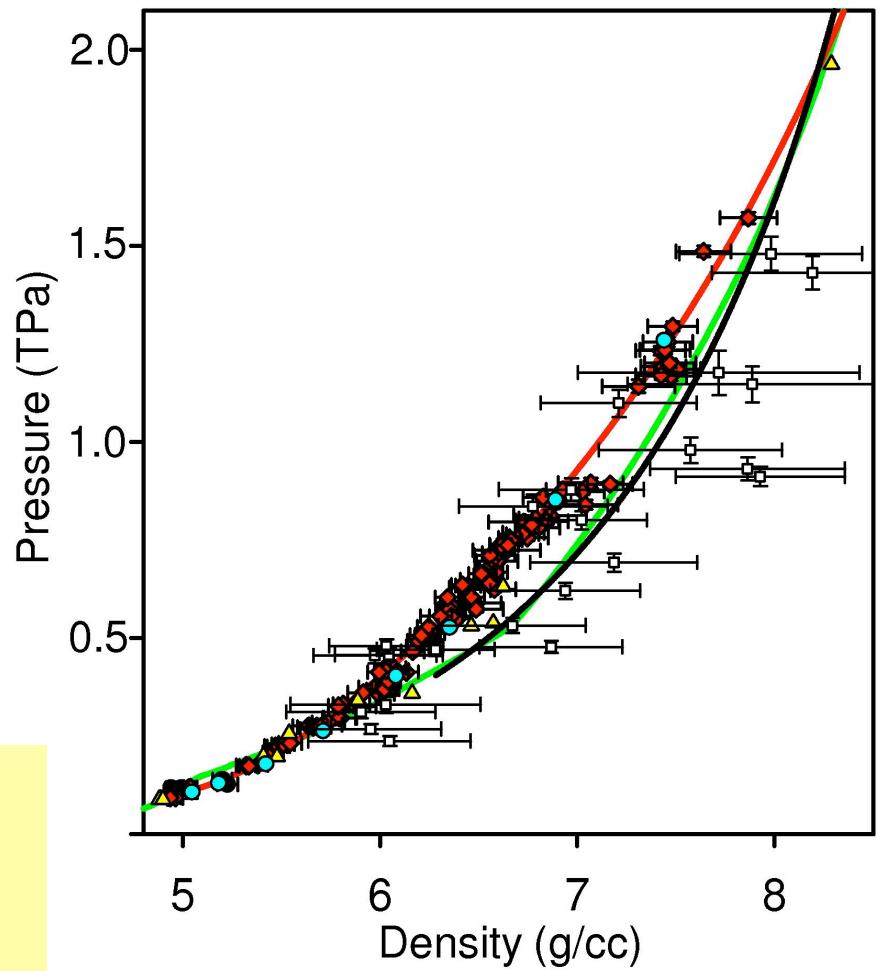


New Hugoniot Data for α -Quartz to 1.5 TPa

M. Knudson
M. Desjarlais



Data set includes ~ 150 points



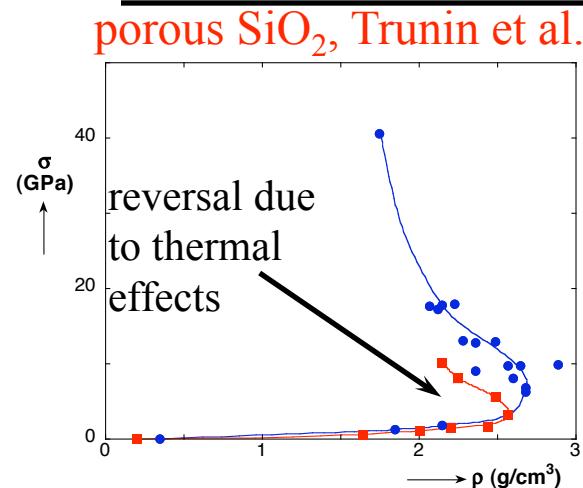
Knudson, M. D. and M. P. Desjarlais
(2009). "Shock compression of quartz to
1.6 TPa: redefining a pressure standard."
Physical Review Letters **103**: 225501.



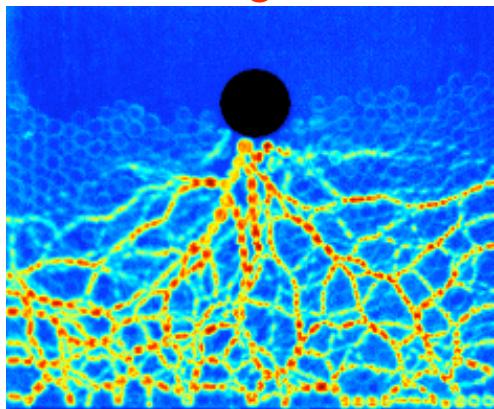
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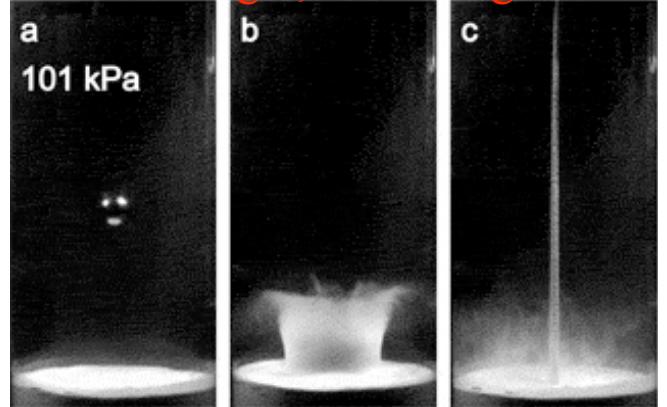
Background on Dynamic Behavior of Granular Materials



B. Behringer, Duke



H. Jaeger, U. Chicago



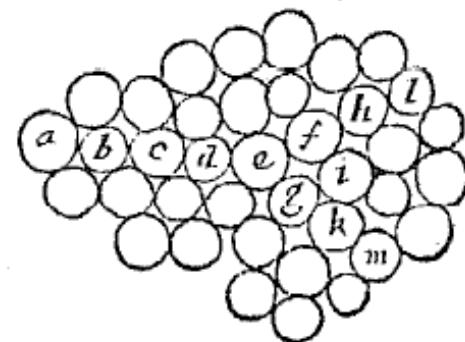
- granular materials display a rich variety of behaviors
- significant experimental and modeling challenges
- extensive quasi-static and low-velocity impact work
- determine thermal behavior through P-V work (Trunin, 2004)
- consolidation studied extensively to optimize loading, etc.
- partial compaction region seldom addressed
- applications: dynamic consolidation, planetary science, energy/blast absorption, ceramic armor



Very Early Thoughts on Particulate Materials

Newton's *Principia*, Book II, 1687:

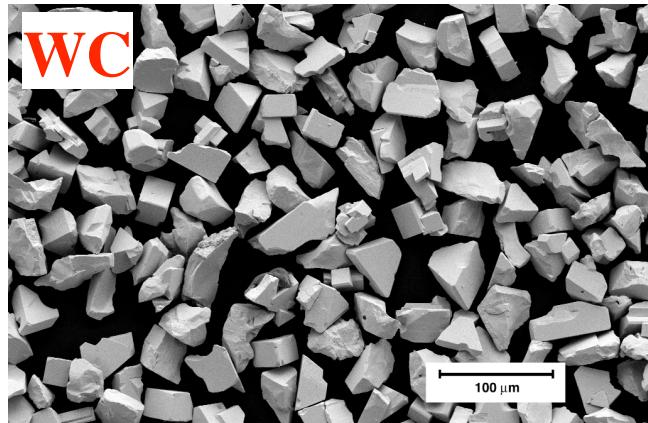
Si jaceant particulæ *a, b, c, d, e* in linea recta, potest quidem pressio directe propagari ab *a* ad *e*; at particulæ *e* urgebit particulæ oblique positas *f* & *g* oblique, & particulæ illæ *f* & *g* non sustinebunt pressionem illatam, nisi fulciantur a particulis ulterioribus *h* & *k*; quatenus autem fulciuntur, premunt particulæ fulcientes; & hæ non sustinebunt pressionem nisi fulciantur ab ulterioribus *l* & *m* easque premant, & sic deinceps in infinitum. Pressio igitur, quam primum propagatur ad particulæ quæ non in directum jacent, divaricare incipiet & oblique propagabitur in infinitum; & postquam incipit oblique propagari, si inciderit in particulæ ulteriores, quæ non in directum jacent, iterum divaricabit; idque toties, quoties in particulæ non accurate in directum jacentes inciderit. *Q. E. D.*





Investigation of Dynamic Behavior of Granular Ceramics

- investigate dynamic compaction behavior of ceramic powders (WC, sand, Al_2O_3 , etc.)
- develop insight into physics of dynamic behavior of these materials and the parameters that influence it
- explore a variety of techniques (quasi-static experiments, mesoscale simulations, etc.) to predict dynamic results
- determine suitability of current models within Sandia codes for simulating dynamic behavior of powders

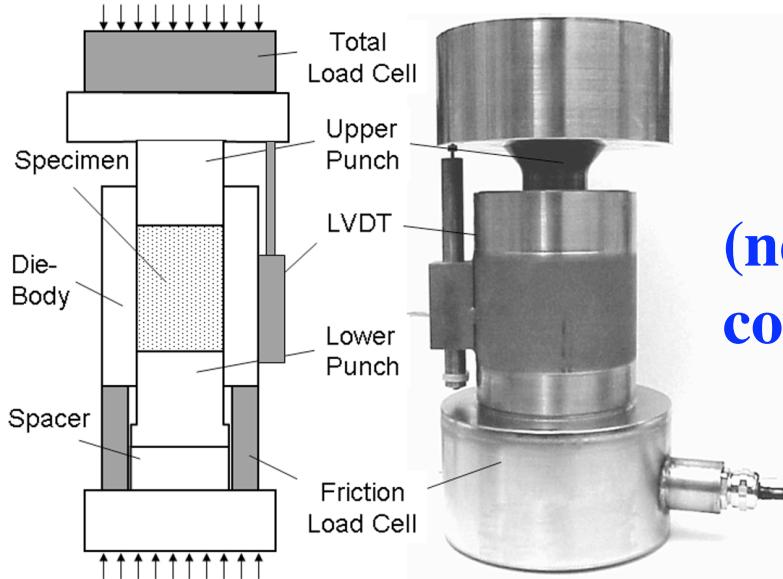




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Static Die Compaction Experiments



(nearly) uniaxial strain
compaction to ~ 1.6 GPa

Objectives

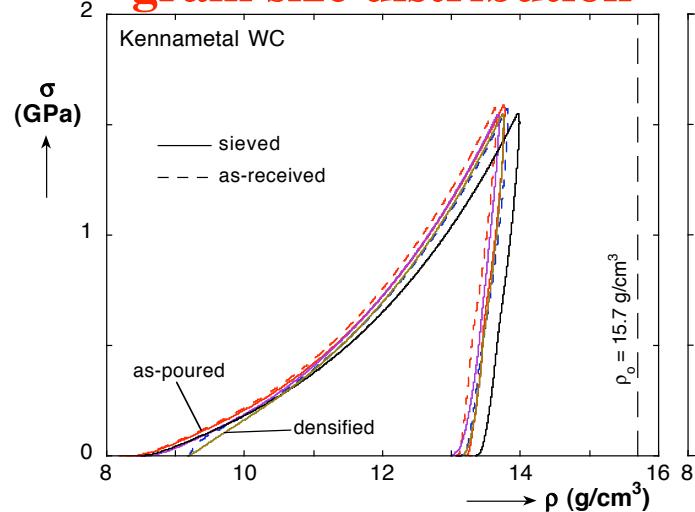
- Determine compaction curve functional form
- Examine effects of experimental parameters (grain size, grain size distribution, grain shape, initial density, loading path, etc.)
- Correlate with dynamic results



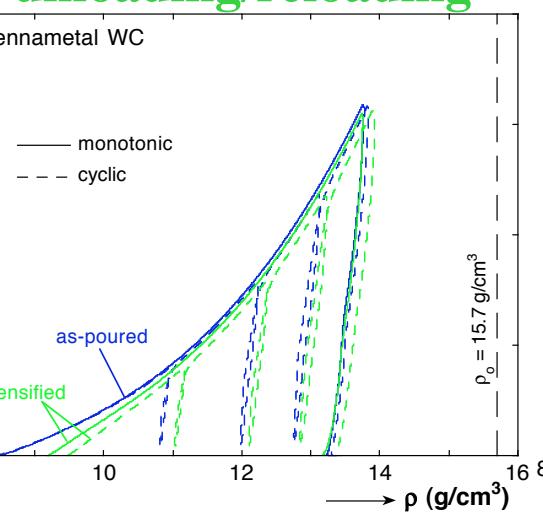
Static Compaction Results

evaluate effects of important variables on loading response

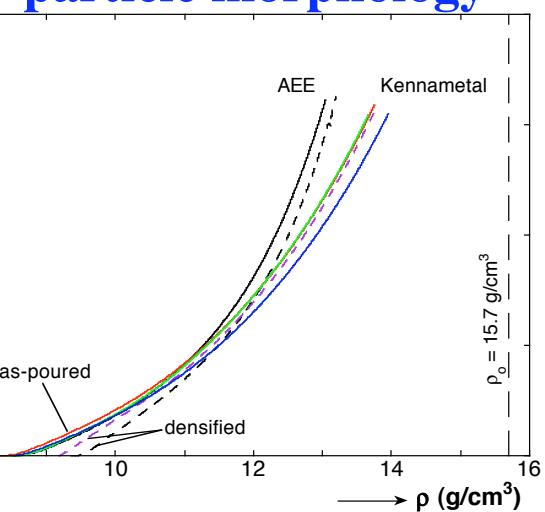
grain size distribution



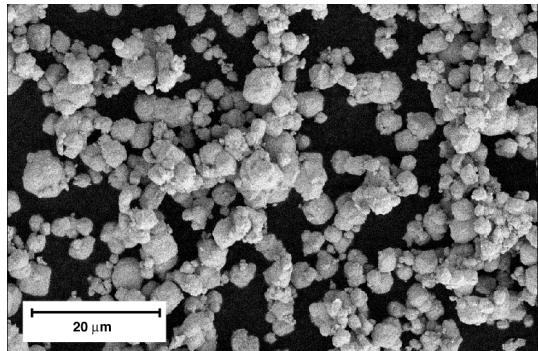
unloading/reloading



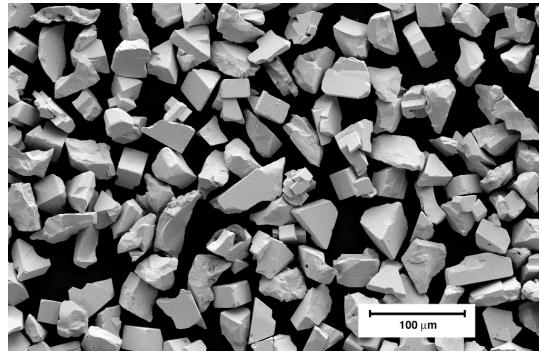
particle morphology



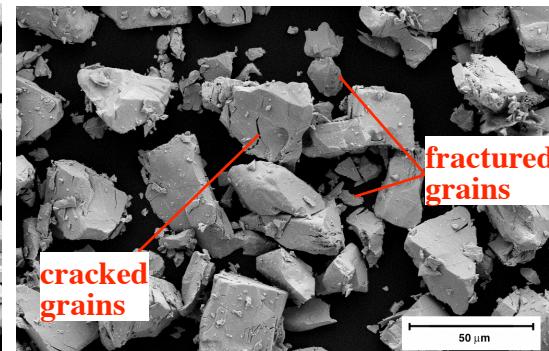
AEE WC



Kennametal WC

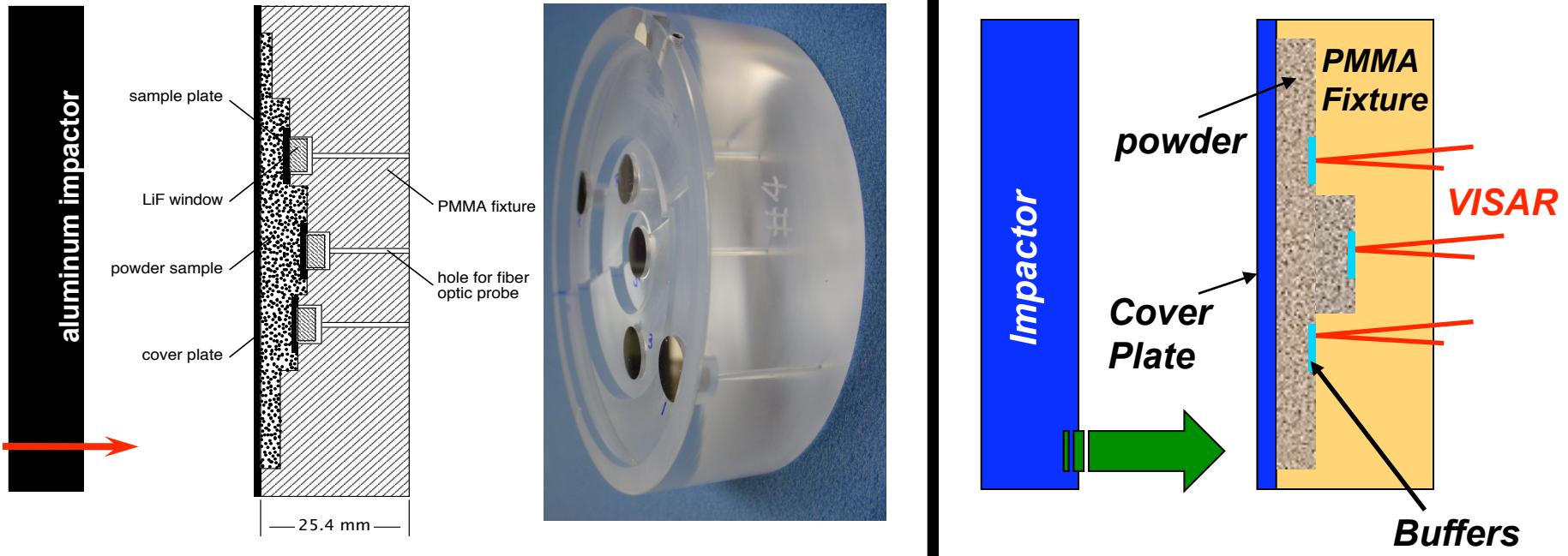


Post-Compaction





Planar Impact Experiments on Granular Materials



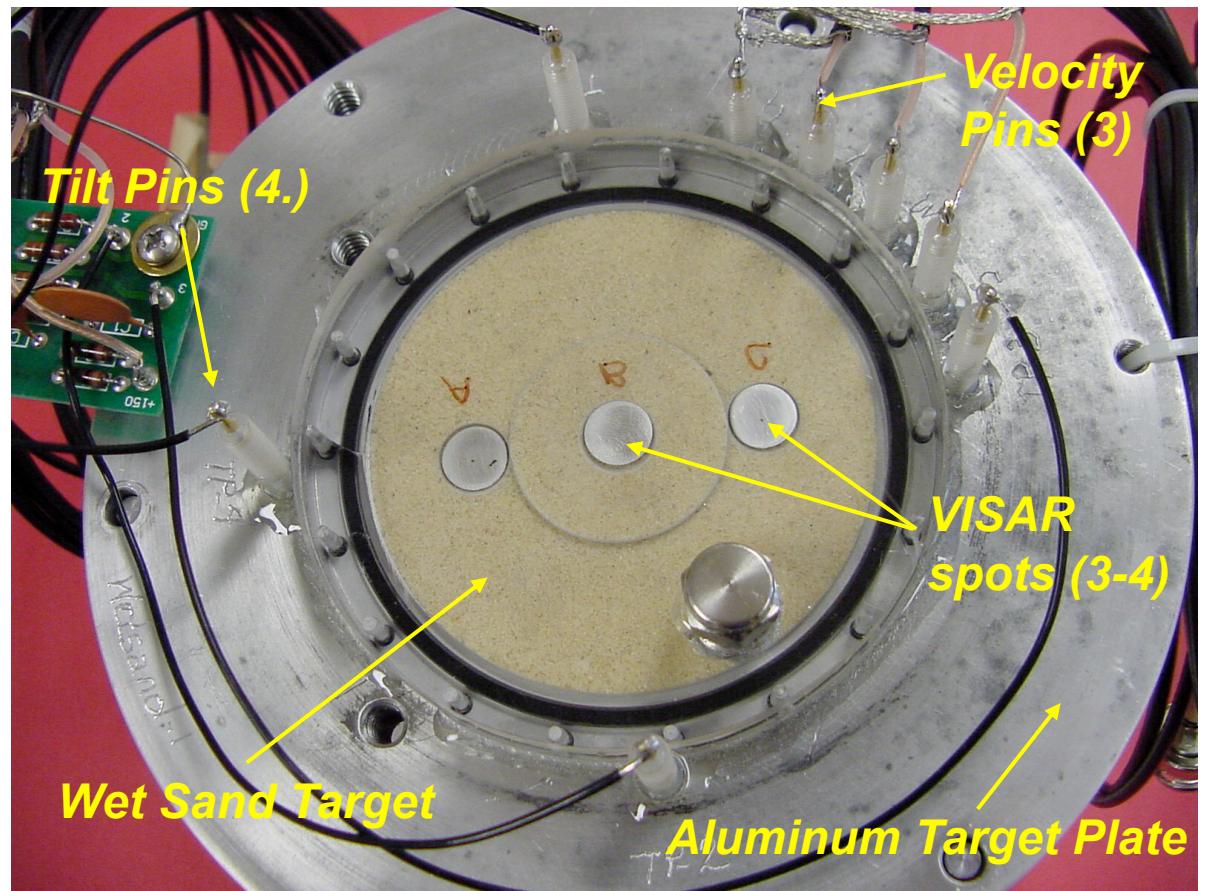
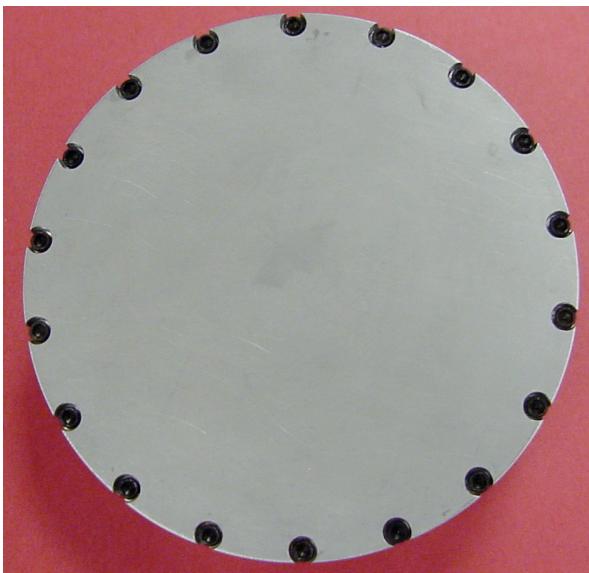
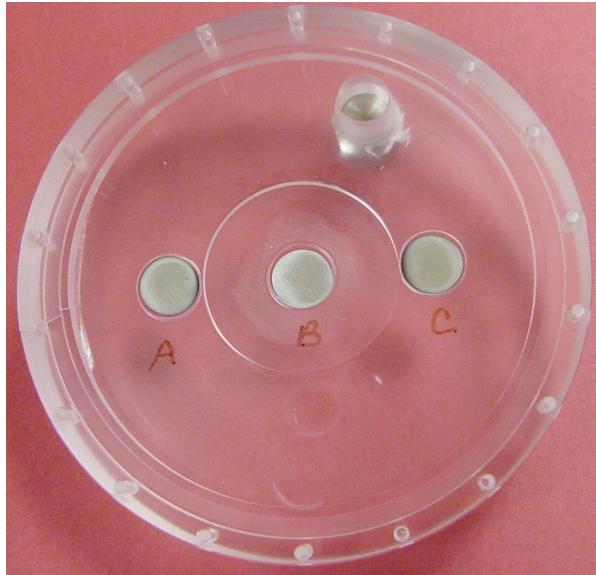
multiple sample thicknesses on the same experiment for accurate shock velocity and uniform powder density; sealed capsule allows fluid / powder mixtures

Vogler, T.J., Lee, M.Y., Grady, D.E., 2007. "Static and dynamic compaction of ceramic powders." *International Journal of Solids and Structures* **44**, 636-658.

Brown, J.L., Thornhill, T.F., Reinhart, W.D., Chhabildas, L.C., Vogler, T.J., 2007. "Shock response of dry sand." in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 1363-1366.



Wet Sand Targets



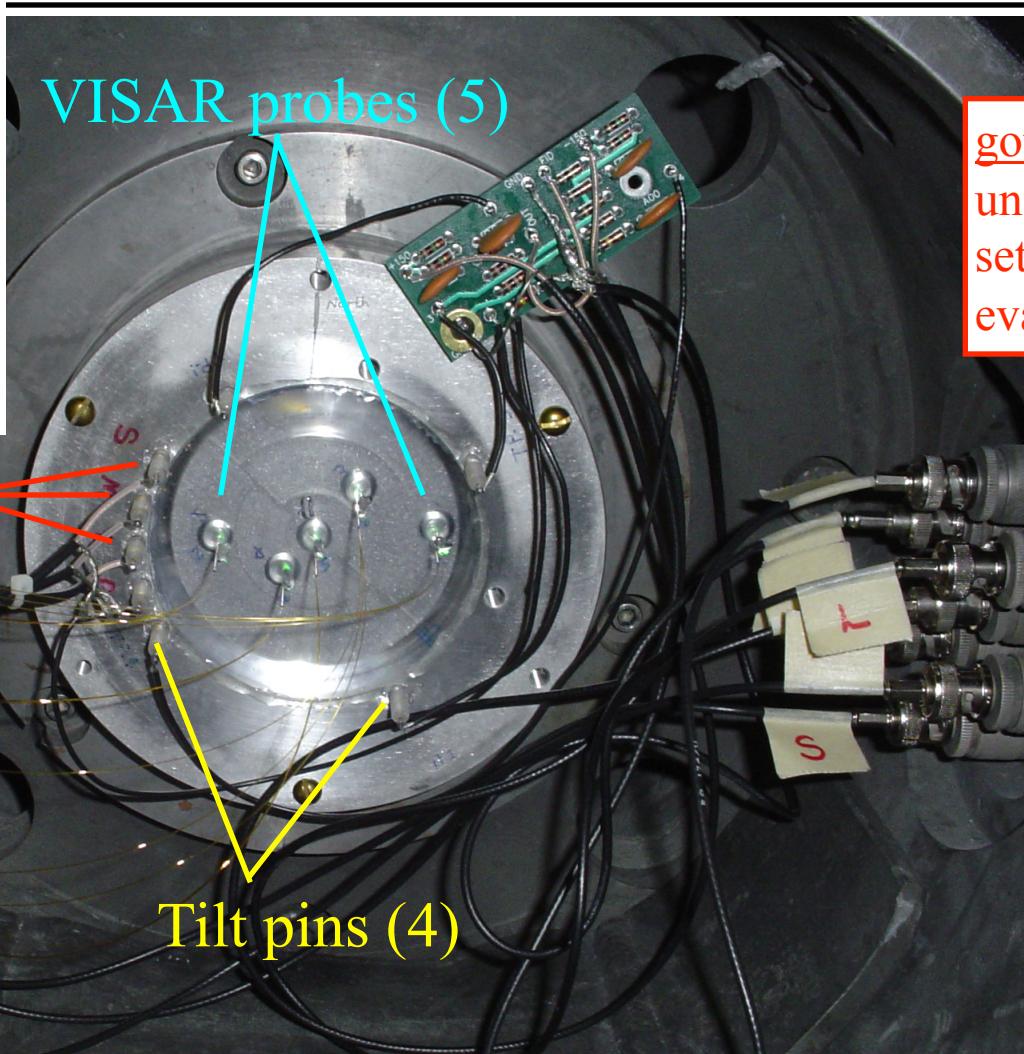


Target Mounted in Gas Gun

Single Stage Gun 100mm



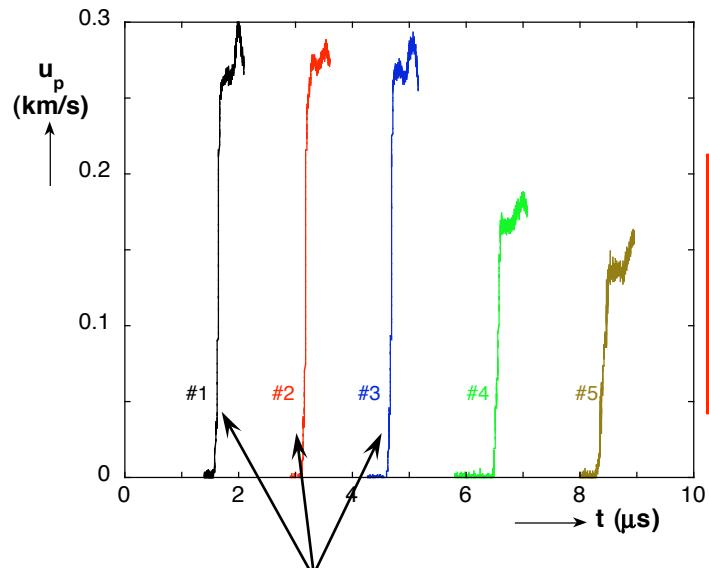
$\sim 1 \text{ km/s}$
 $\sim 30 \text{ GPa}$



gotcha's:
uniformity
settling
evacuation

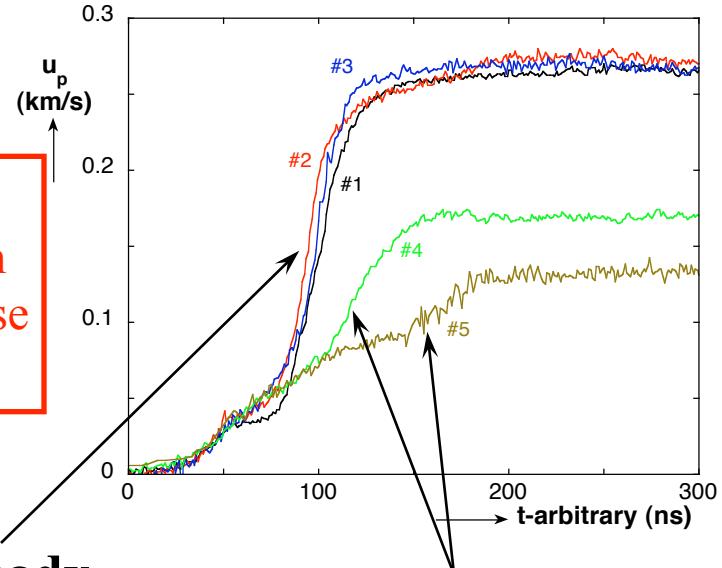


Measured Steady Waves



shock velocity calculated based on powder thicknesses and arrival times

gotcha's:
attenuation
edge release
steadiness



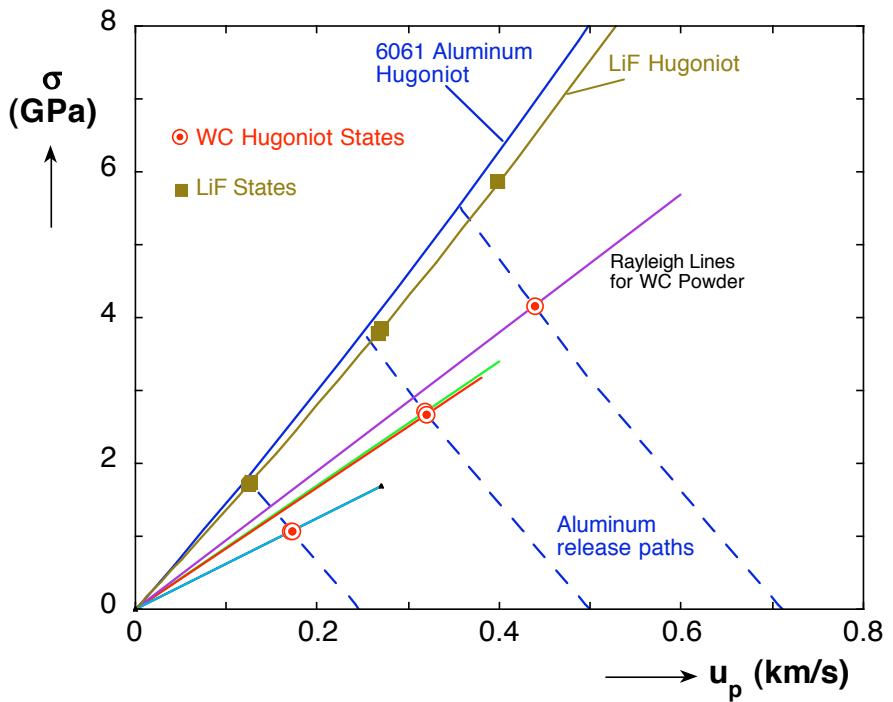
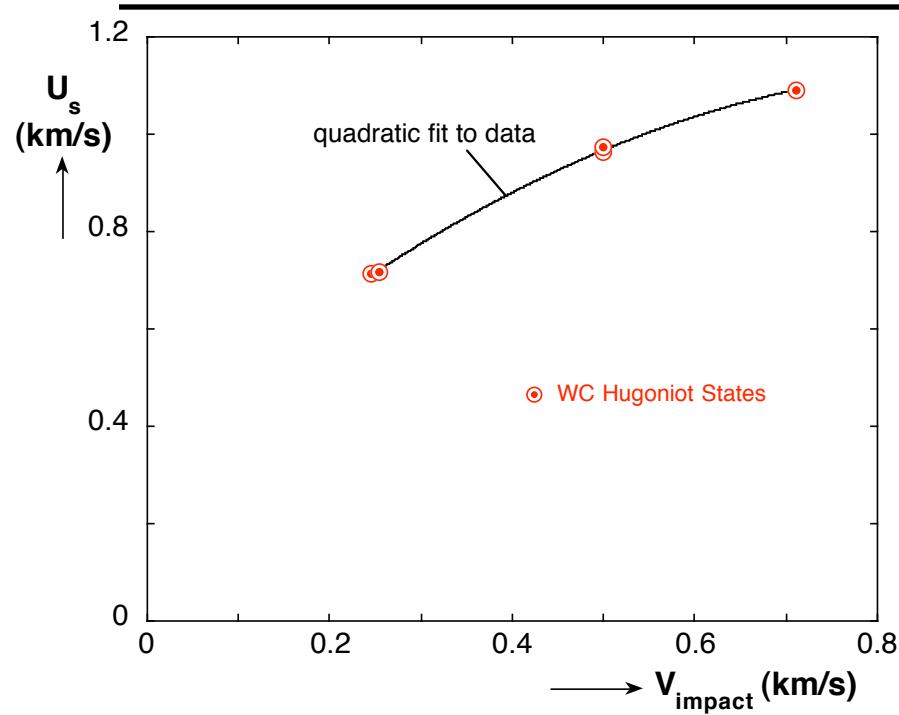
**steady,
structured
waves**

**attenuated
waves**

- seem to be first time-resolved measurements of steady waves in granular materials
- since waves are steady, Rankine-Hugoniot jump conditions can be used even though waves have finite rise times



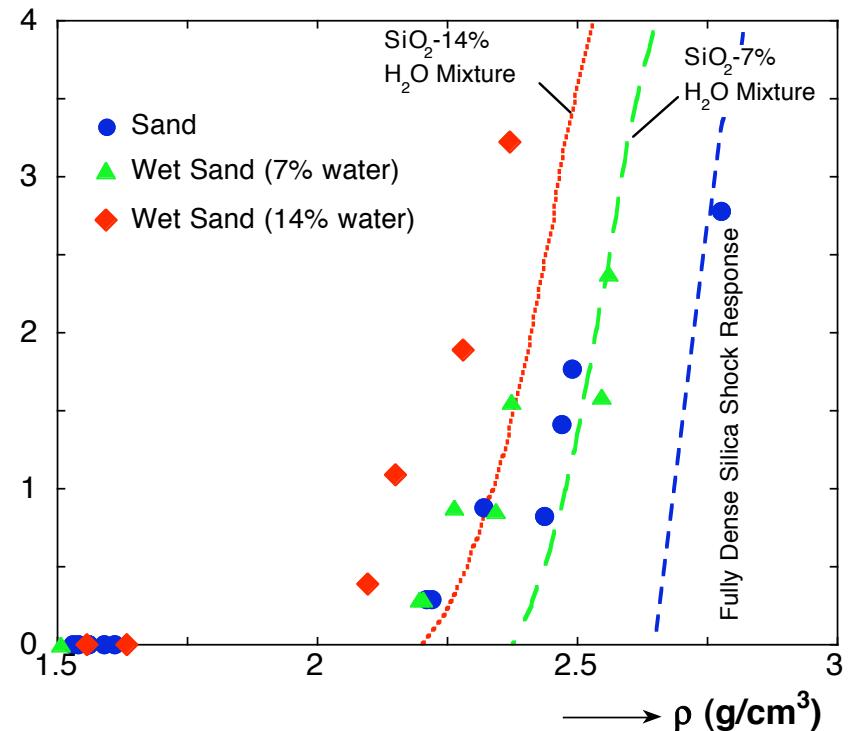
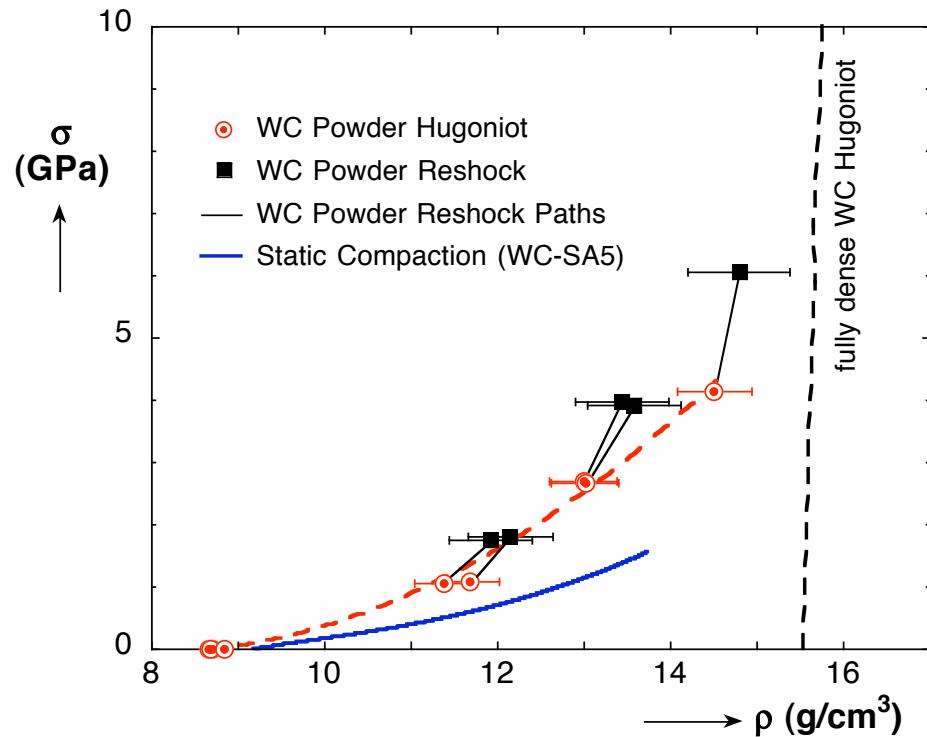
Shock Velocities and Hugoniot States



- impedance matching to aluminum impactor used to determine Hugoniot stress and particle velocity ($\sigma = \rho_{oo} U_s u_p$)
- density then calculated from $\rho = \rho_{oo} U_s / (U_s - u_p)$



Compaction Response for WC and Wet/Dry Sand

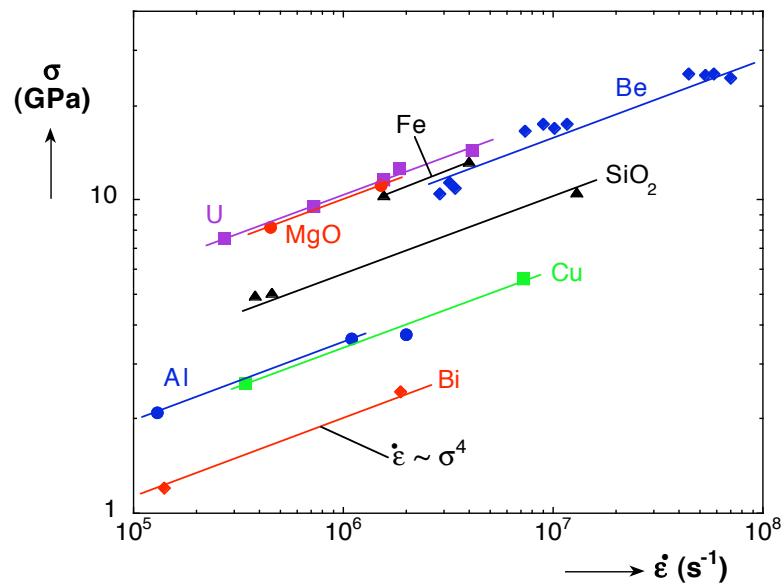


- first reshock state lies above Hugoniot suggesting elastic response of compacted material
- dynamic response is stiffer than static response for WC, about the same for sand

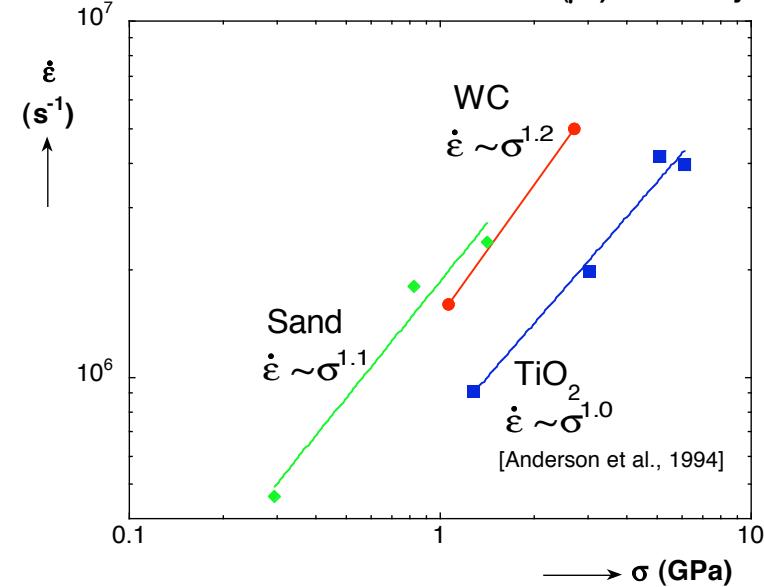
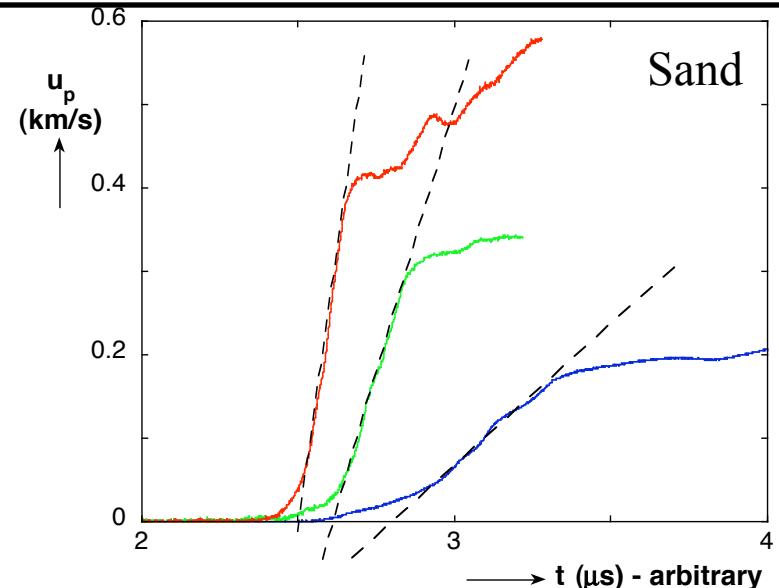


Scaling Between Rise Time of Wave and Stress

for many fully dense materials (Al, Be, Bi, Cu, Fe, MgO, SiO₂, U),
rise times of steady waves scale as
• $\dot{\varepsilon} \sim \sigma^4$ (Swegle & Grady, 1985)



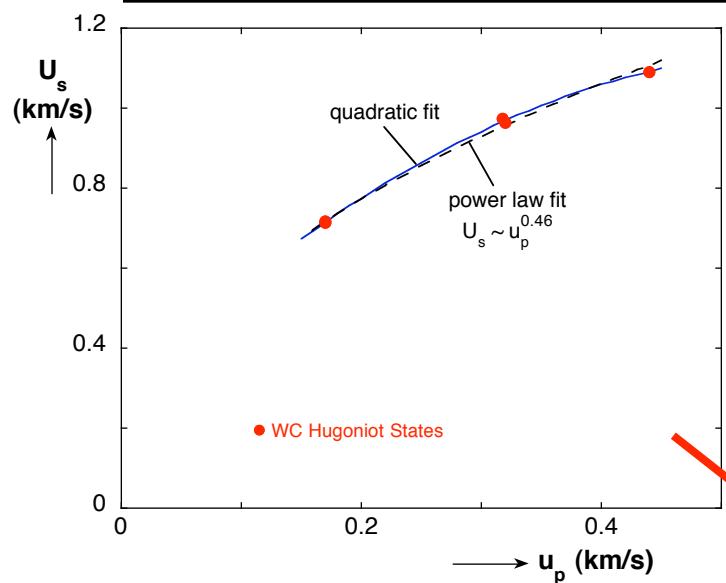
data on three granular ceramics
and sugar suggest a linear scaling
between stress and strain rate



[Anderson et al., 1994]



A Simple Scaling Argument for Granular Materials



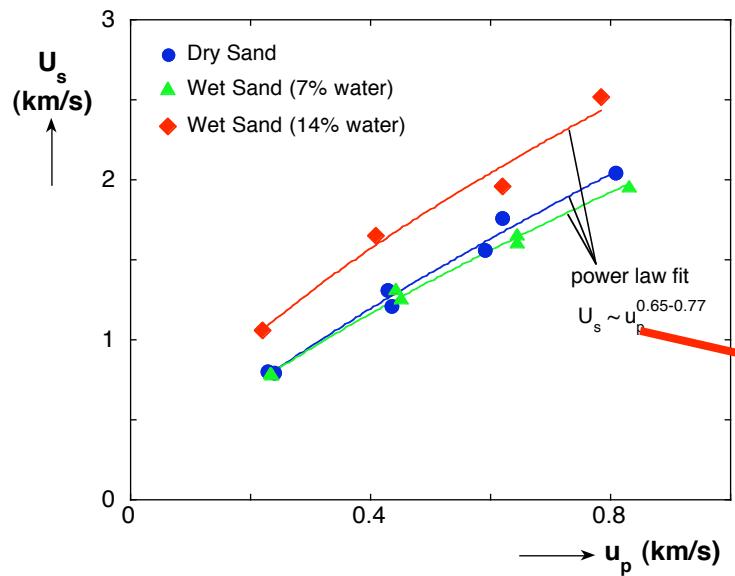
$$\sigma = \rho_{oo} U_s u_p$$

$$\varepsilon = \frac{u_p}{U_s}$$

$$\dot{\varepsilon} \propto \frac{\varepsilon}{\Delta t} \propto \frac{u_p}{d} \frac{U_s}{u_p}$$

$$\dot{\varepsilon} \propto \frac{u_p^2}{d U_s}$$

mass
traversing
pores controls
width of
shock front



$$\sigma \propto u_p^{3/2}$$

$$\text{if } U_s \propto u_p^{0.5}$$

$$\dot{\varepsilon} \propto u_p^{3/2}$$

$$\rightarrow \dot{\varepsilon} \propto \sigma$$

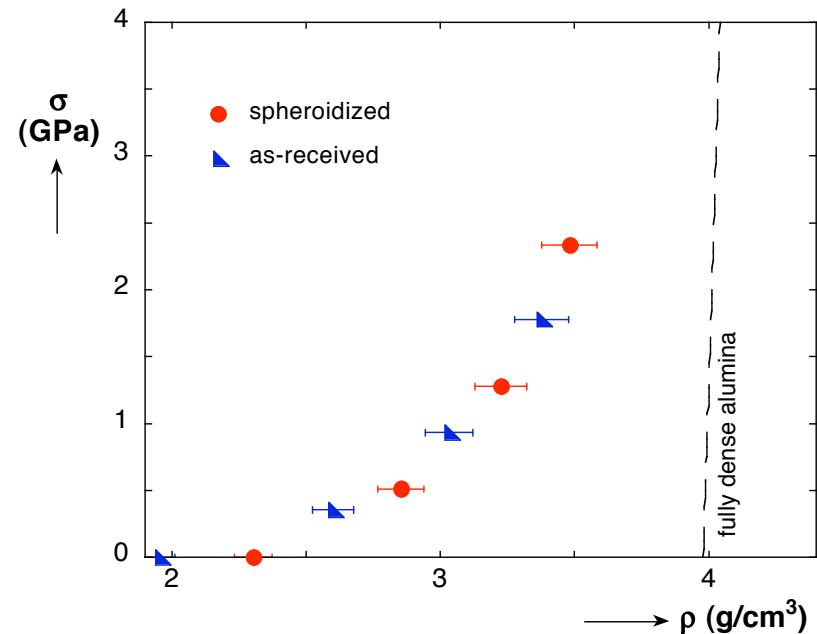
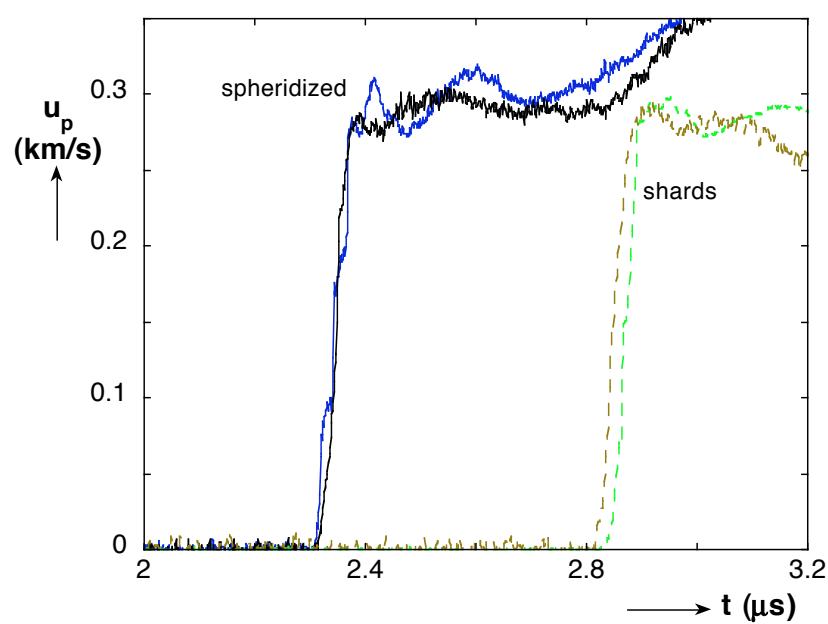
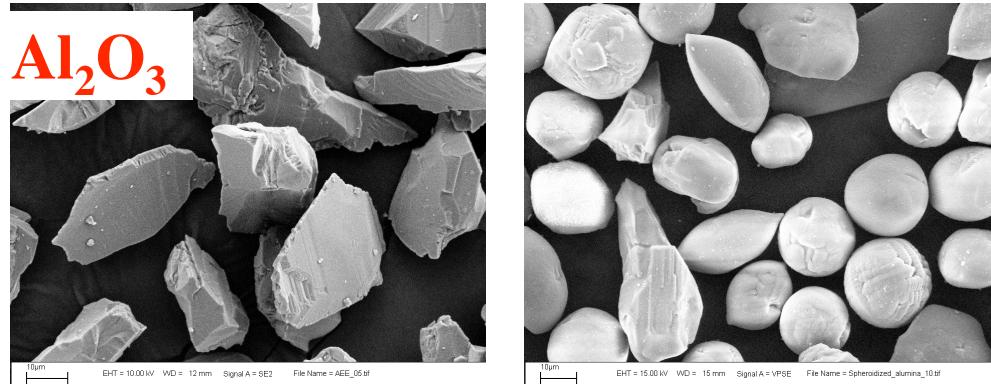
$$\text{if } U_s \propto u_p^{0.75}$$

$$\dot{\varepsilon} \propto \sigma^{0.7}$$



Effect of Particle Morphology

plasma processing
used to create
spheres, changing
particle morphology

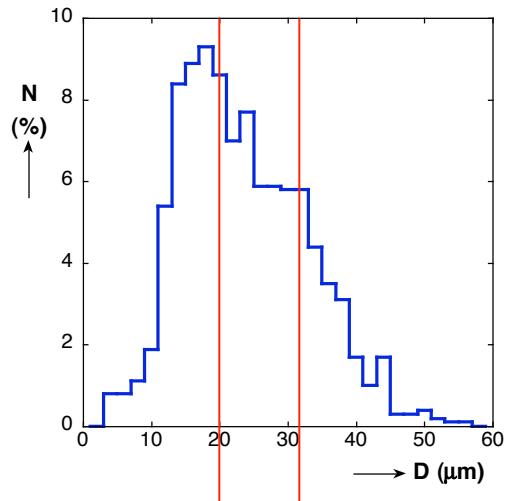


compaction results indistinguishable, but small differences in VISAR records

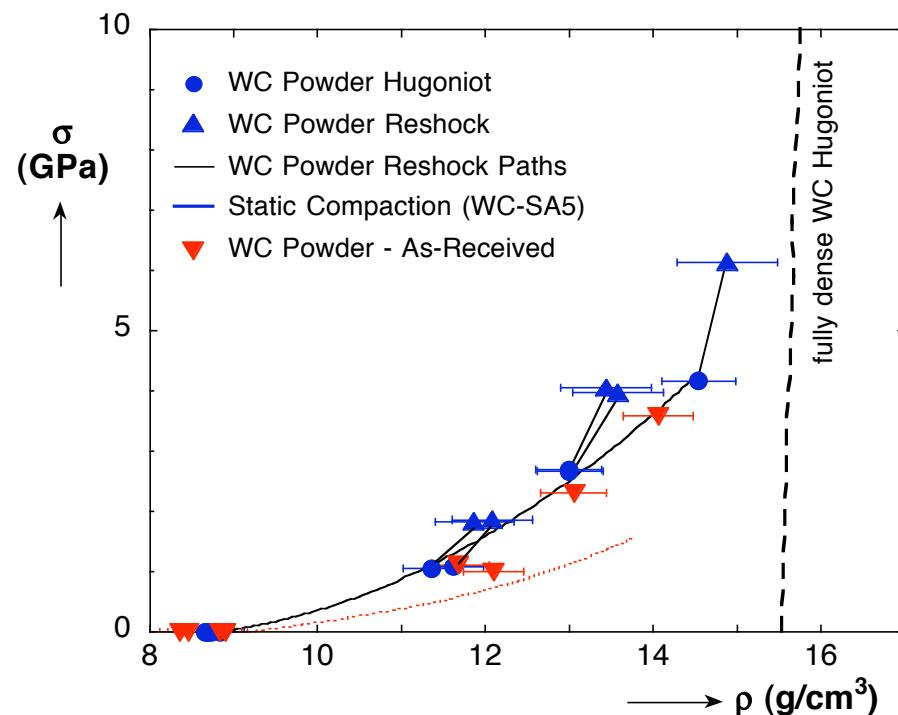


Particle Size Distribution

as-received particle size distribution



sieved to
20-32 μm



*results are insensitive to particle size distribution,
at least over the same order of magnitude*



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Mesoscale Modeling of Granular Materials: Past Work

- collapsing ring of material under external pressure (Carroll & Holt, 1972; Nesterenko, 2001; Tong & Ravichandran, 1997)
- Williamson (1990) considered a unit cell in a uniform distribution of particles under dynamic loading
- Benson and coworkers (1994-present) studied compaction of granular materials (primarily metals) using a 2-D Eulerian code for a moderate number of grains
- Baer (2002-present) simulated compaction of HMX and sugar (HMX simulant) using a 3-D Eulerian code for a moderate number of particles
 - *follow approach of Benson et al. for larger number of grains by exploiting parallel computing platforms*
 - *begin with 2-D and determine whether 3-D is necessary*



Mesoscale Modeling of Granular Materials



- particles idealized as circles (rods) for initial work
- constant velocity boundary condition applied
- run in CTH (explicit Eulerian finite difference code)
- Mie-Gruneisen EOS, elastic-perfectly plastic strength for WC

Borg, J.P., Vogler, T.J., (2008). "Mesoscale calculations of the dynamic behavior of a granular ceramic." *International Journal of Solids and Structures* 45, 1676-1696.

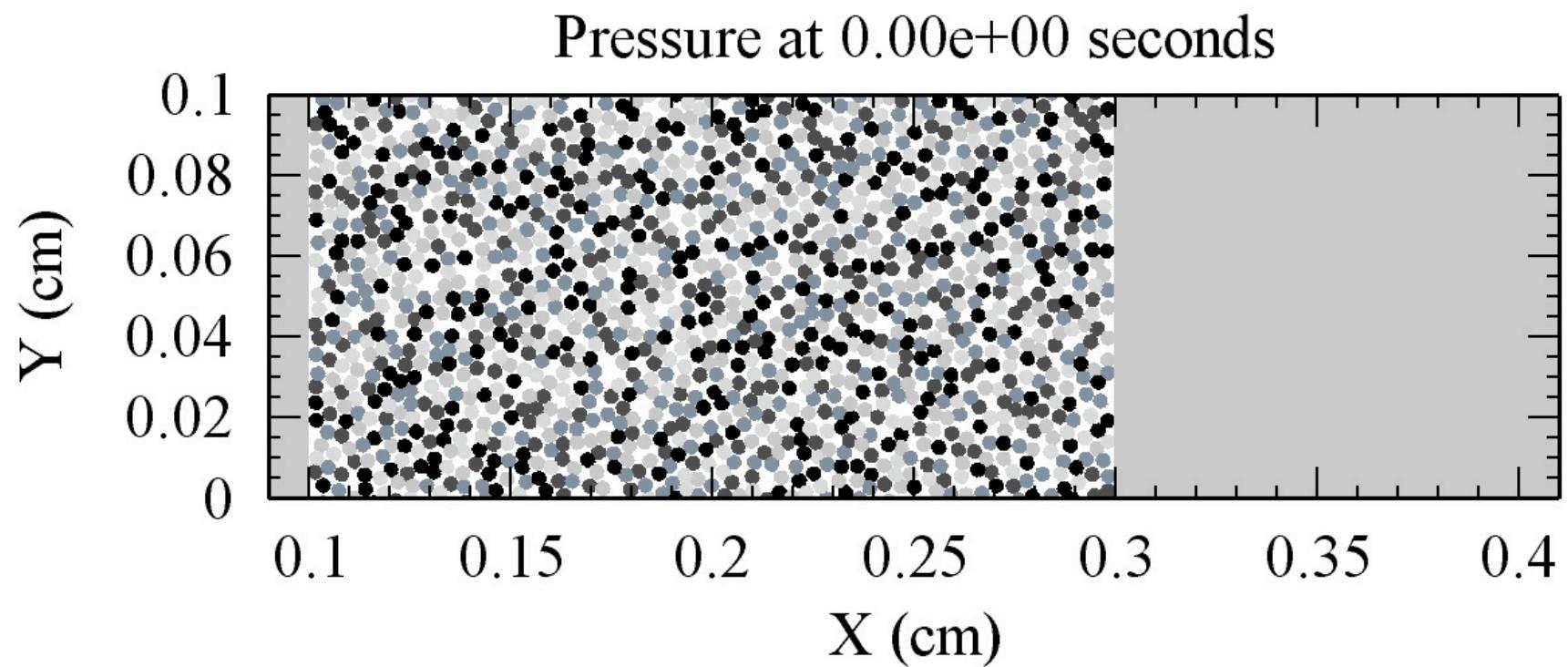
Borg, J.P., and Vogler, T.J. (2008). "Mesoscale simulations of a dart penetrating sand," *Int. J. Impact Eng.* (in press).

Borg, J.P., and Vogler, T.J. (2007). "Mesoscale calculations of shock loaded granular ceramics," in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 227-230.

get at underlying physics of granular materials

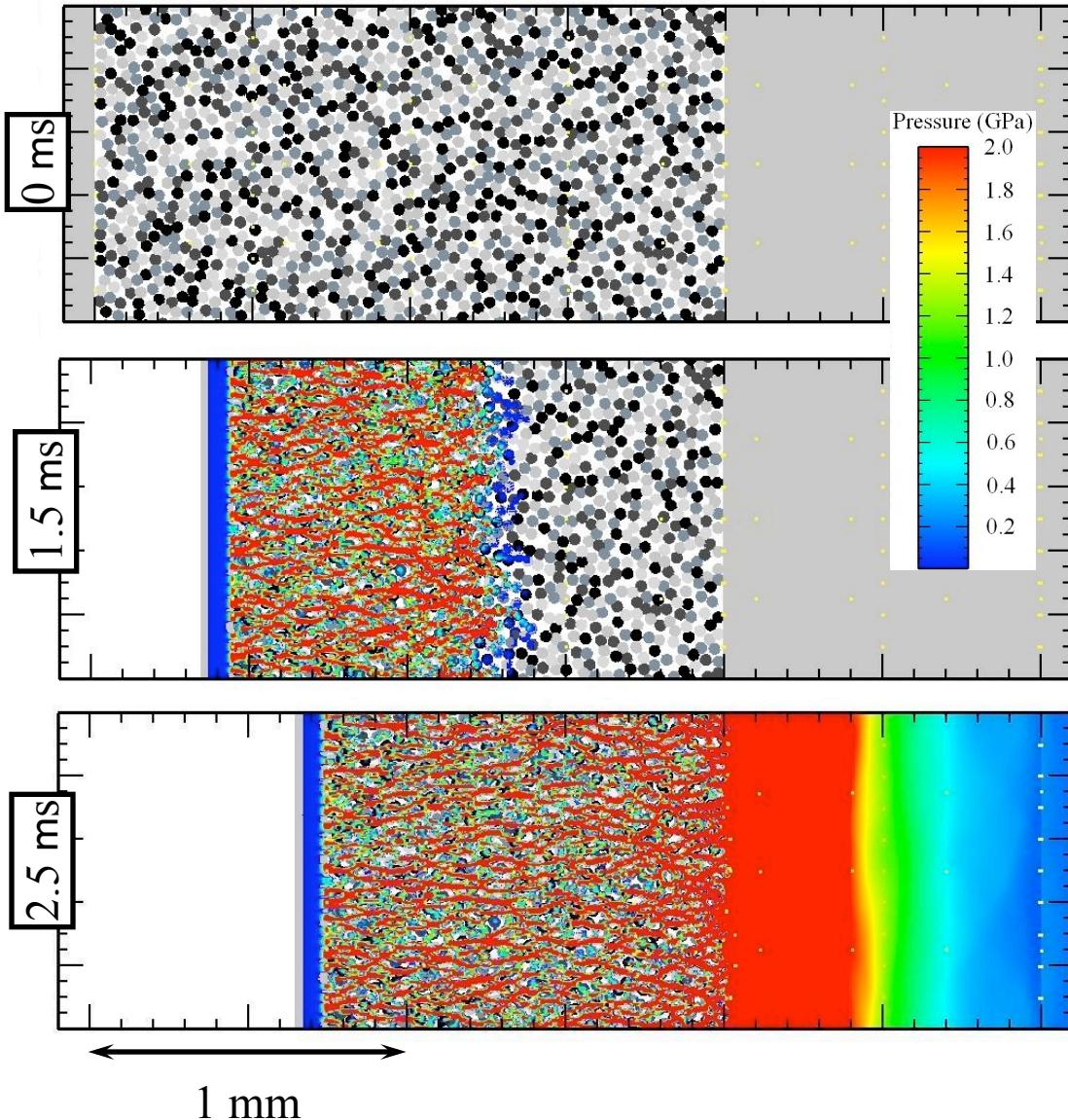


Computational Dynamic Compaction





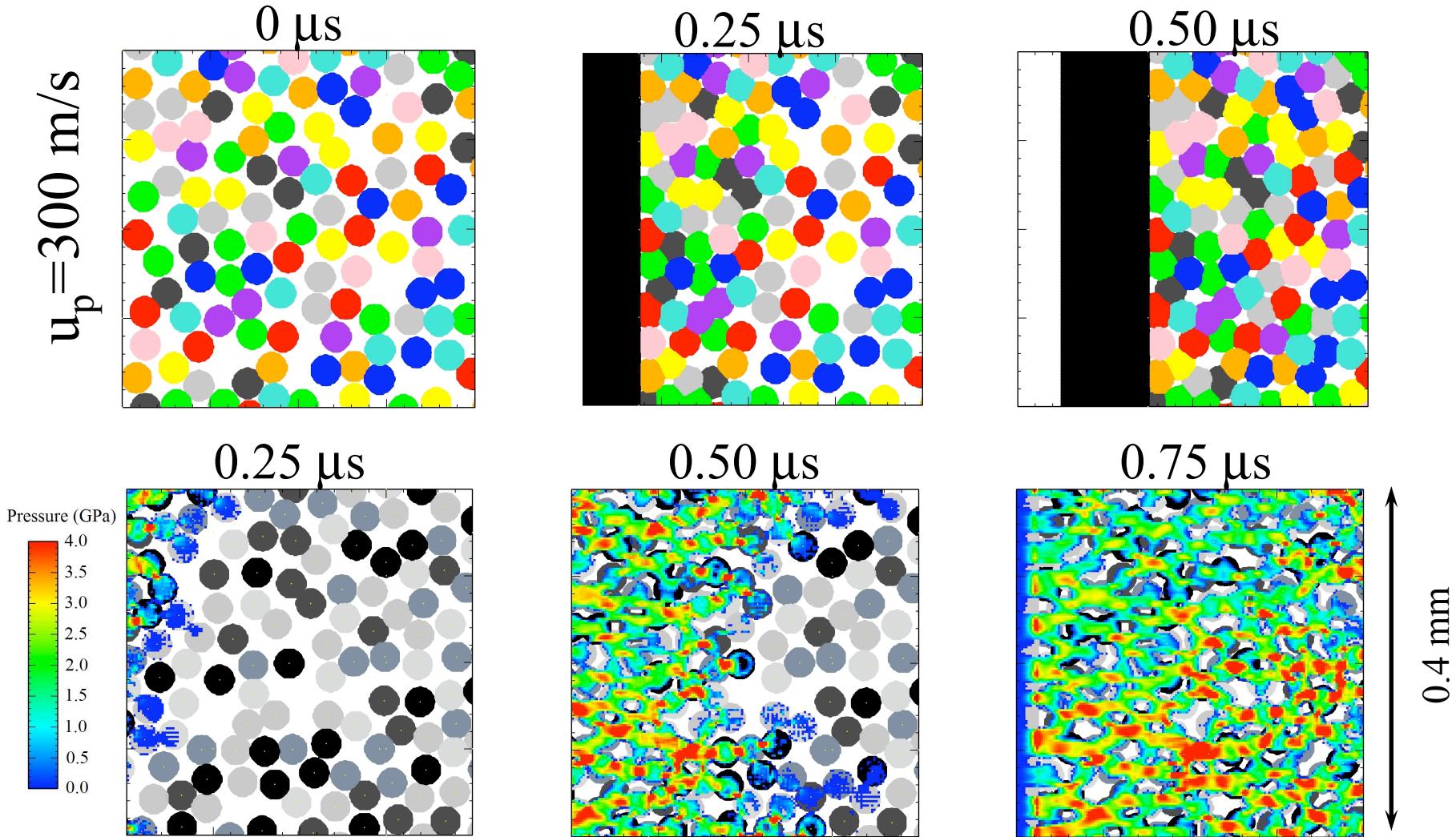
Computational Dynamic Compaction



- **driver plate velocity**
 $u_p = 300 \text{ m/s}$
- **shock thickness on the order of $\sim 2\text{-}5$ particles**
- **strong force chains observed**
- **wave smooths in aluminum buffer**



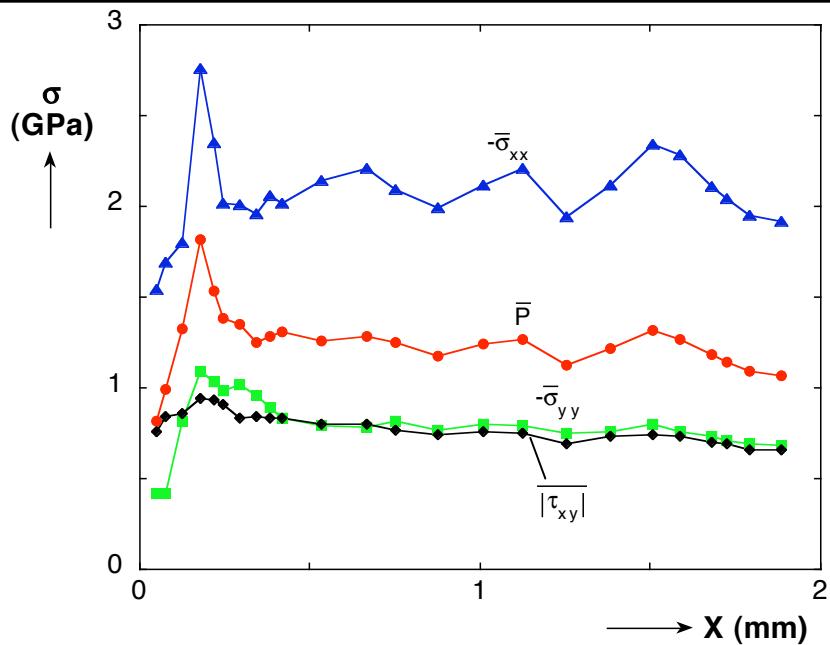
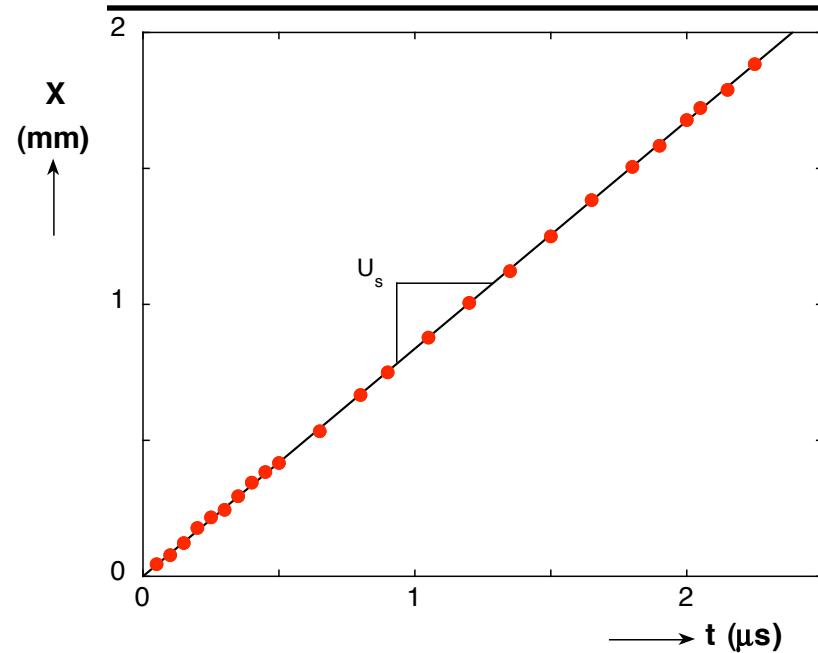
Close-Up of Compaction Process



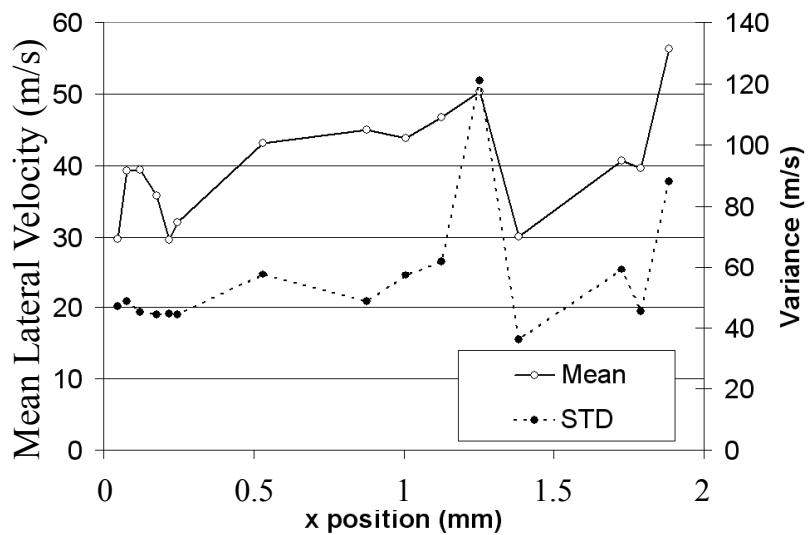
no jetting or vortices so deformation is “*quasi-static*”
(Benson et al., 1997)



Properties of Propagating Wave

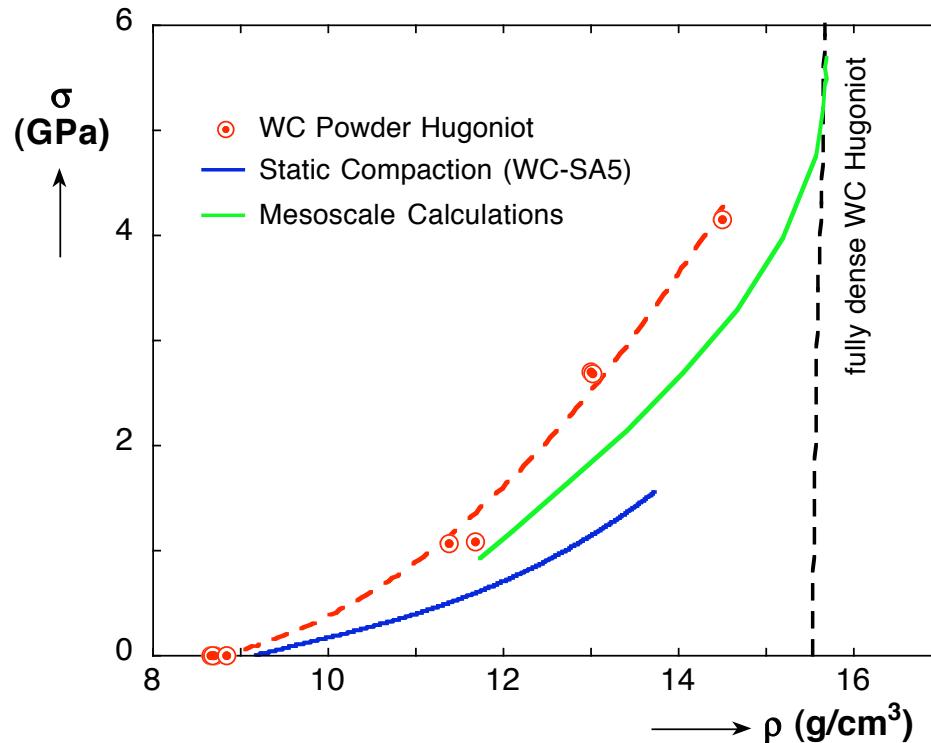


- arrival time of wave suggests steadiness at all times
- stresses in wave front indicate nearly 0.5 mm required to reach steady state
- lateral motion >10% of longitudinal velocity





Calculated Hugoniot from Literature Parameters



$$\sigma = \rho_o U_s u_p$$
$$\rho = \rho_o \frac{U_s}{U_s - u_p}$$

- simulations provide reasonable estimate for Hugoniot
- shortcomings of model:
 - missing physics of granular contact and fracture
 - wrong connectivity in 2-D
 - spherical particles unrealistic
 - inaccurate strength for small particles



Sensitivity to Simulation Parameters

Material Properties

- Particle size distribution (**negligible effect**)
- Dynamic yield strength (**strong effect**)
- Material EOS (**negligible effect**)
- Spall strength (**strong effect but threshold**)

Two-Dimensional Properties

- Material distribution (**strong effect**)
- Variations in boundary conditions (**small effect**)

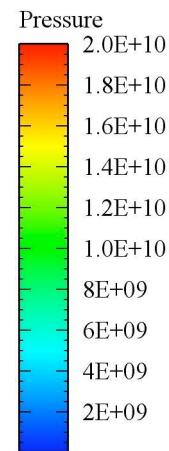
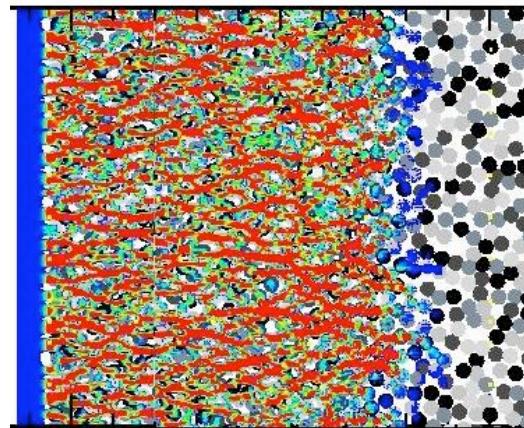
Hydrocode Behavior

- Mixed cell strength (**very strong effect**)

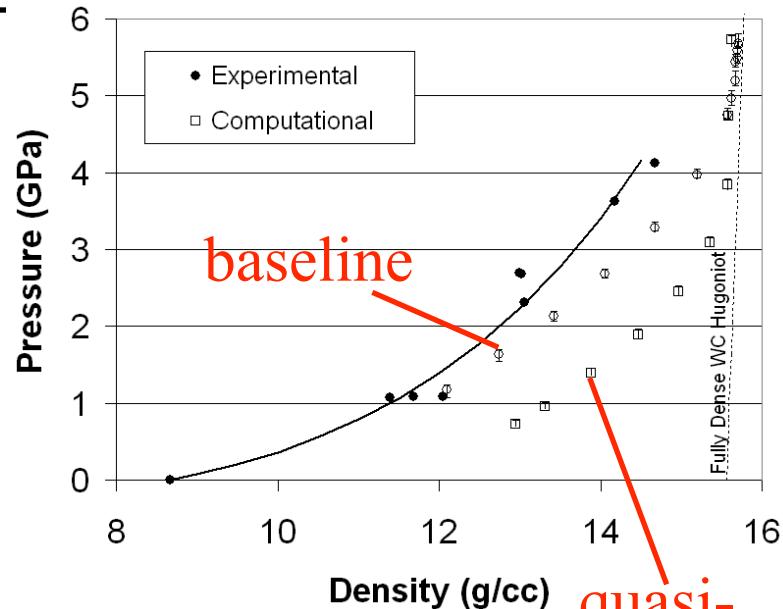
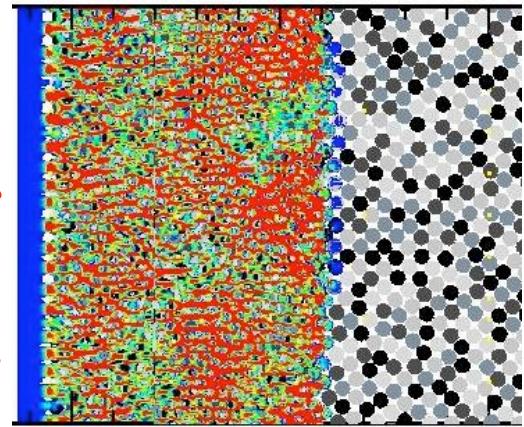


Effect of Order on Shock Structure

Baseline



Quasi-Crystalline



for the quasi-crystalline case:

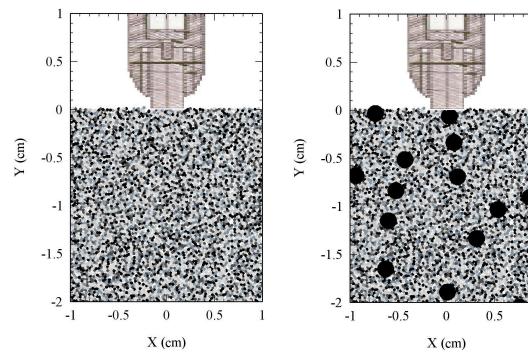
- wave much slower
- shock front less diffuse
- force chains less pronounced
- shock propagation must rely on momentum (i.e. particle motion) to transport shock information
- lateral motion minimized
- material becomes anisotropic (slow and fast directions)

quasi-crystalline



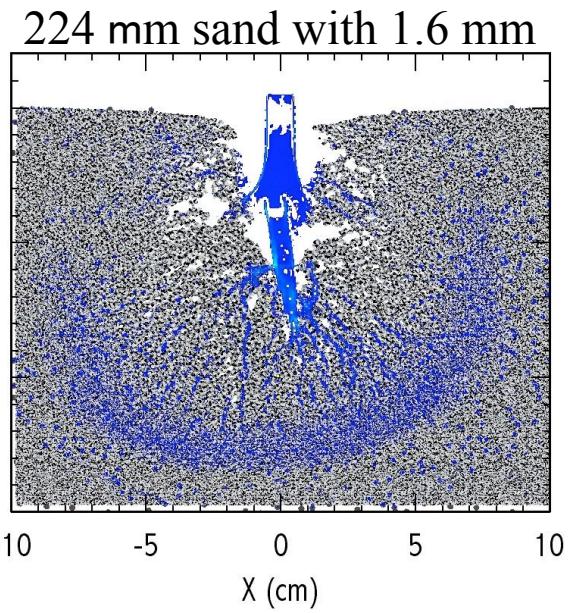
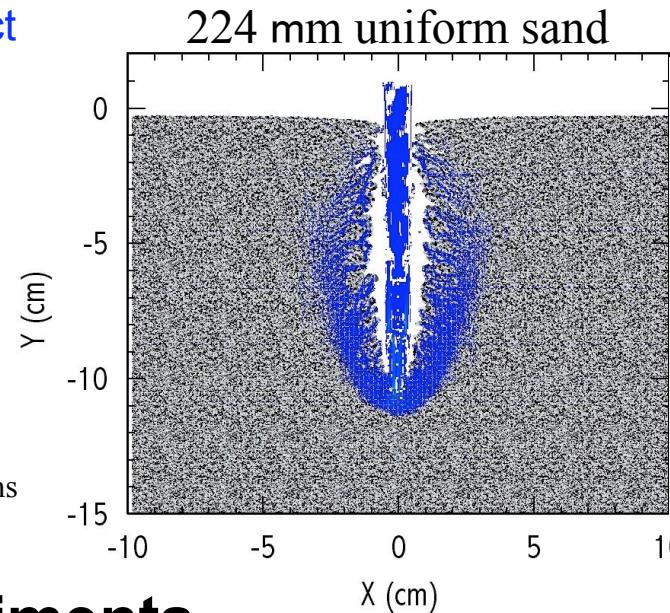
“System Level” Work providing insight into nonuniform targets

Borg and Vogler, Int. J. Impact
Engineering (in press)

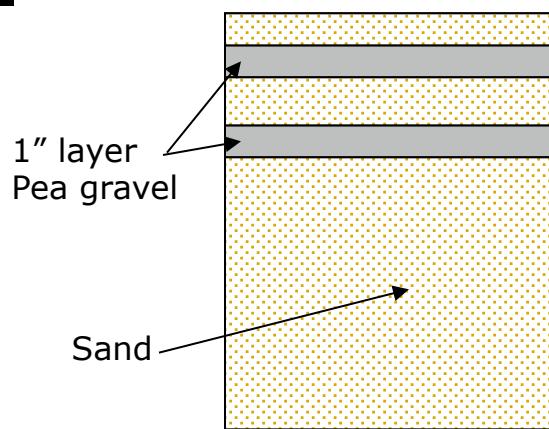
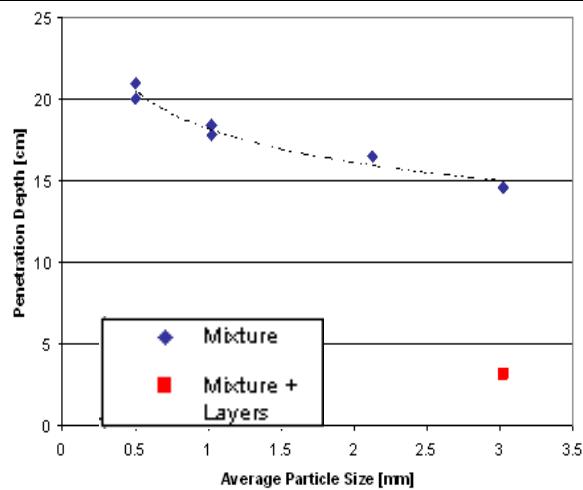


224 mm Sand

with 1.6 mm grains



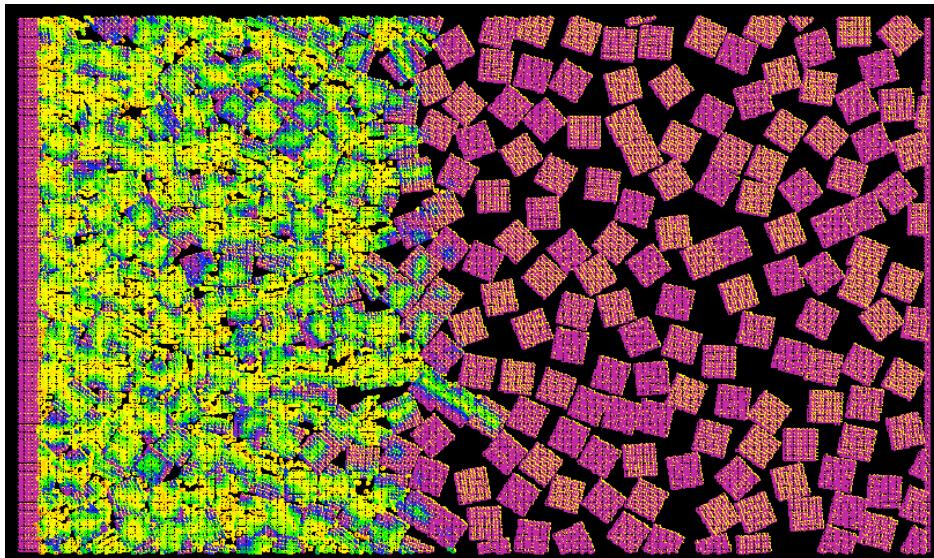
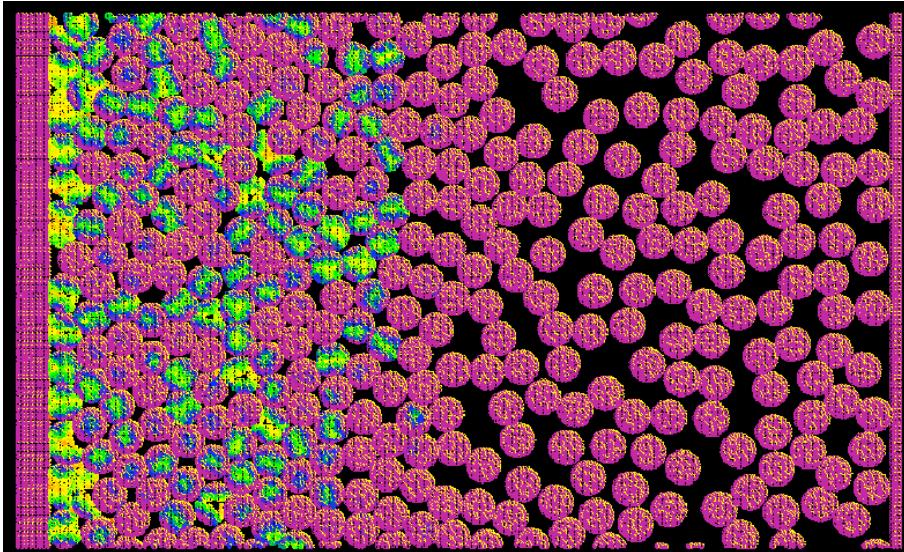
small-scale experiments



mesoscale simulations
in progress to
understand deflection
mechanism



Initial Mesoscale Calculations with Peridynamics



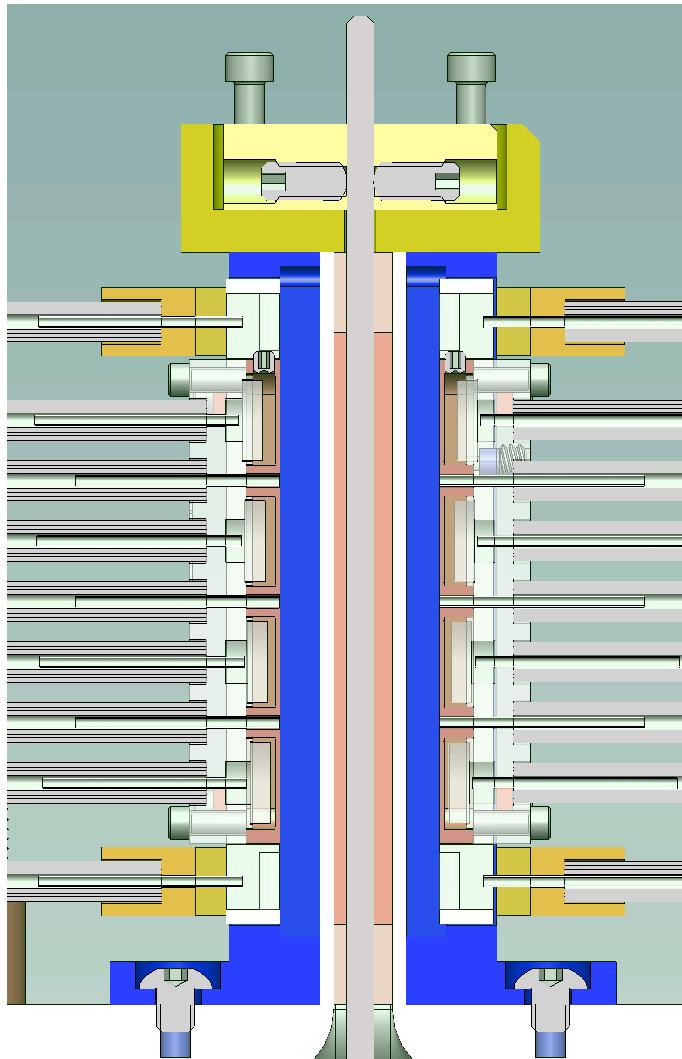
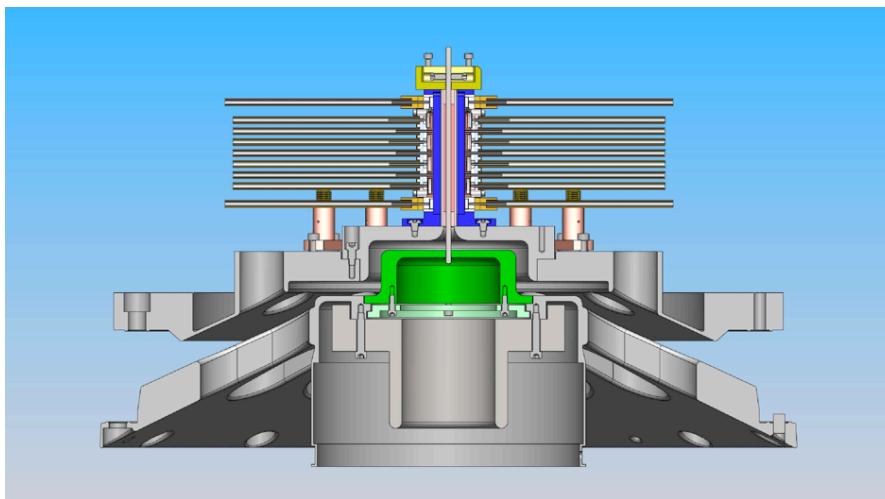
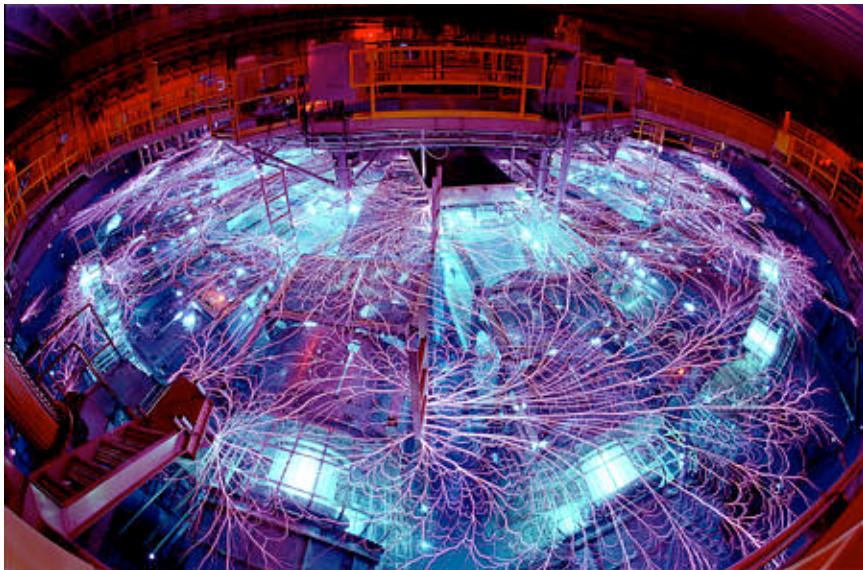
- non-local method based on reformulation of governing equations in integral form (Silling, Jmps 2000)
- model framework still under development
- includes fracture and contact missing from CTH
- response insensitive to particle shape despite large differences in particle fracture (dissipation due to fracture is small)



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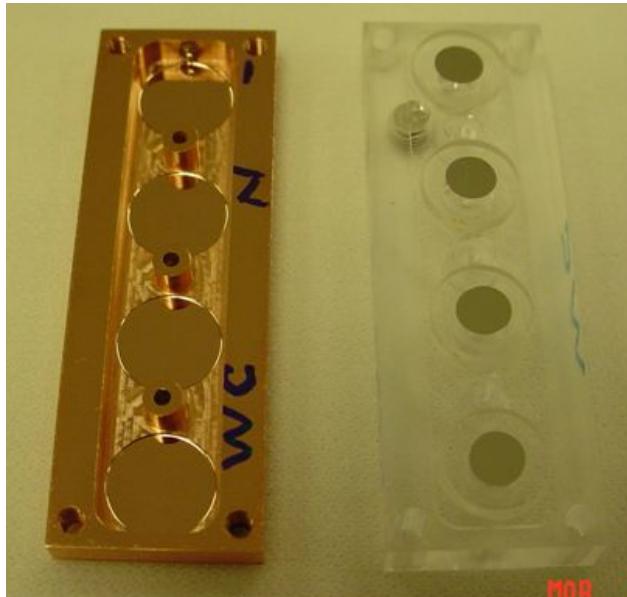


Ultra-High Pressure Z Experiments





Z Powder Capsule



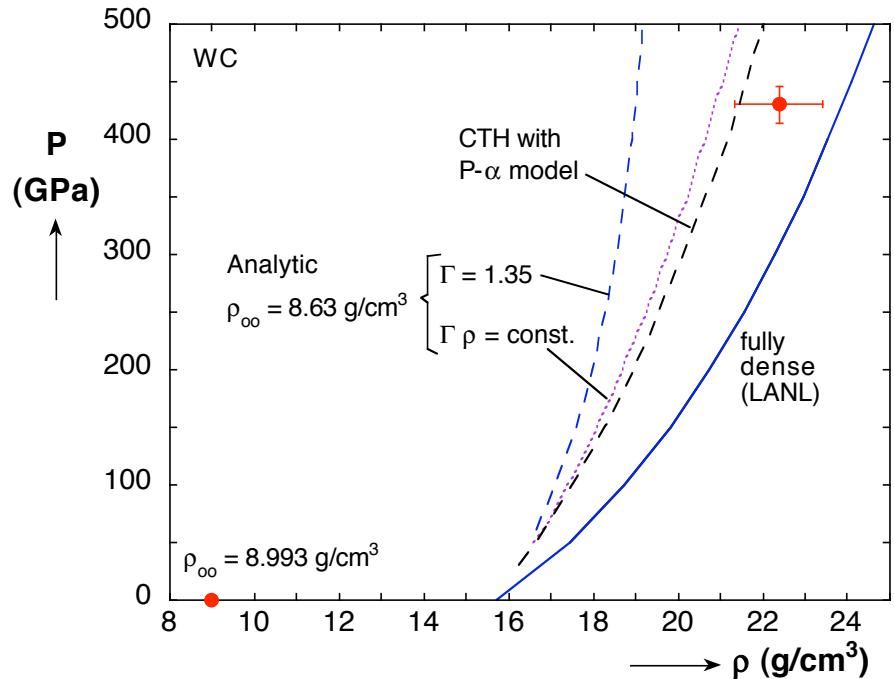
each target consists of:

- 300 μm Cu flyer on 700 μm Al
- 300 μm Cu driver
- four WC thicknesses of 400, 600, 800, and 1000 μm
- quartz windows.

VISAR measurements made at each sample/window interface and above, below, and between the samples



Z Experiment - Granular WC

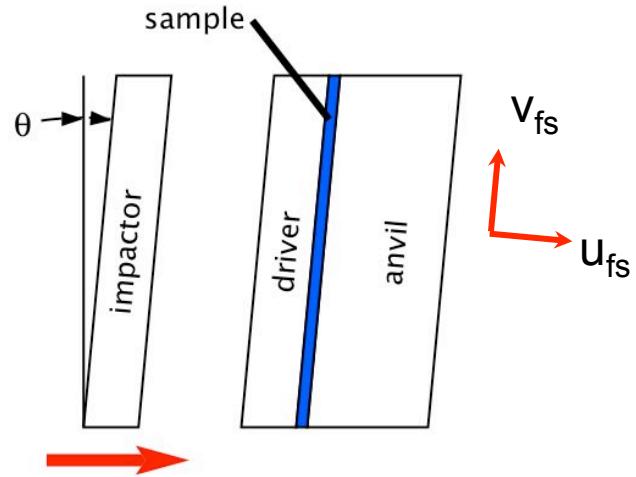
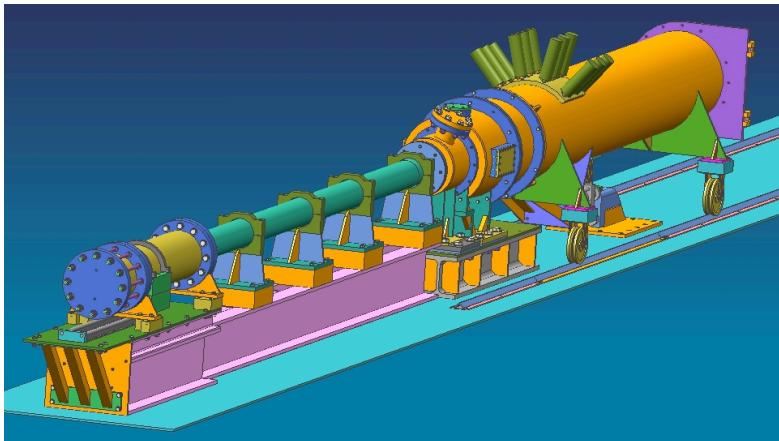


- Fully dense WC Hugoniot from LASL shock compendium
- Porous Hugoniot calculated analytically for $\Gamma=1.35$ and $\Gamma\rho=\text{constant}$ with initial density of 8.63 g/cc; melting neglected
- Calculations with CTH utilizing a Mie-Gruneisen EOS and the P - α model; melting neglected

- Data point shown is for Z-2096, impact of a copper flyer into the copper driver at 9.85 km/s. Initial sample density was 8.993 g/cc.
- Porous material melts at 45-50 GPa vs. 390-440 GPa
- Preliminary error bars based on uncertainty in shock velocity, EOS of copper, impact velocity, and initial density.



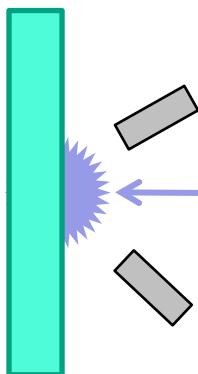
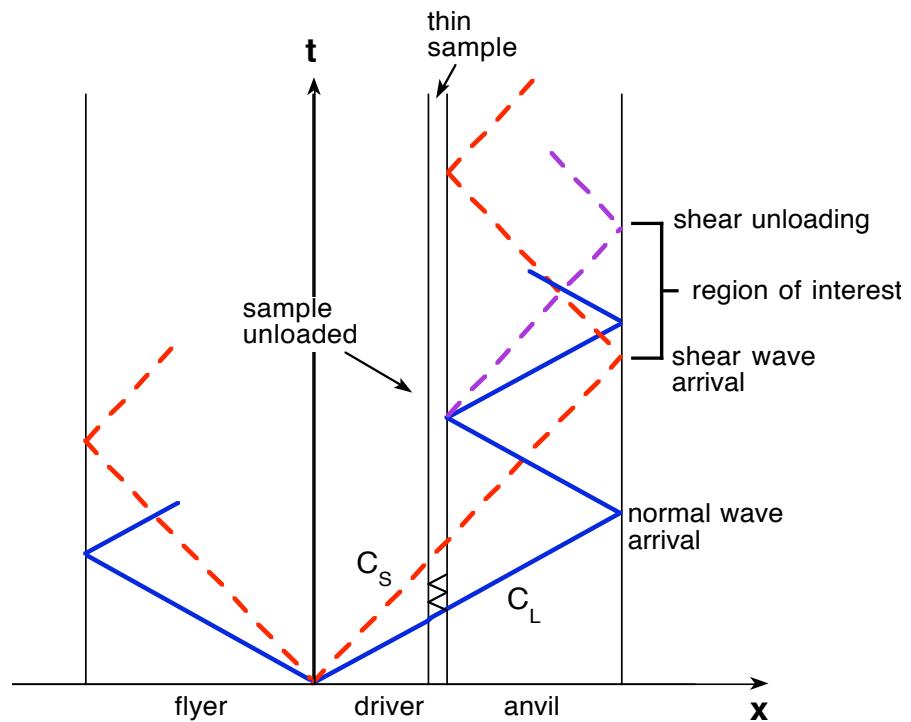
Pressure-Shear Loading of Granular Materials



- slotted barrel prevents rotation and ensures planar impact at angle θ
- elastic impactor, driver, and anvil simplify analysis (steel, WC, etc.)
- angle θ must be small enough to prevent slipping (less than $\sim 30^\circ$)
- variation of impact velocity, angle, and sample thickness allow control of pressure and strain rate
- capable of strain rates of 10^5 - 10^6 s⁻¹



Basics of Pressure-Shear Experiments



$$v_{12}^* = \frac{\cos(17) + 1}{2} v_x + \frac{\sin(17)}{2} v_y$$
$$v_{13}^* = \frac{\cos(25) + 1}{2} v_x - \frac{\sin(25)}{2} v_y$$

- normal stress (pressure) defined by flyer/driver/anvil material and impact velocity

$$\sigma = \frac{1}{2} \cos(\theta) V_{impact} \rho_o^{anvil} c_o^{anvil}$$

- shear stress given by:

$$\tau(t) = \frac{1}{2} \rho_o^{anvil} c_o^{anvil} v_{fs}(t)$$

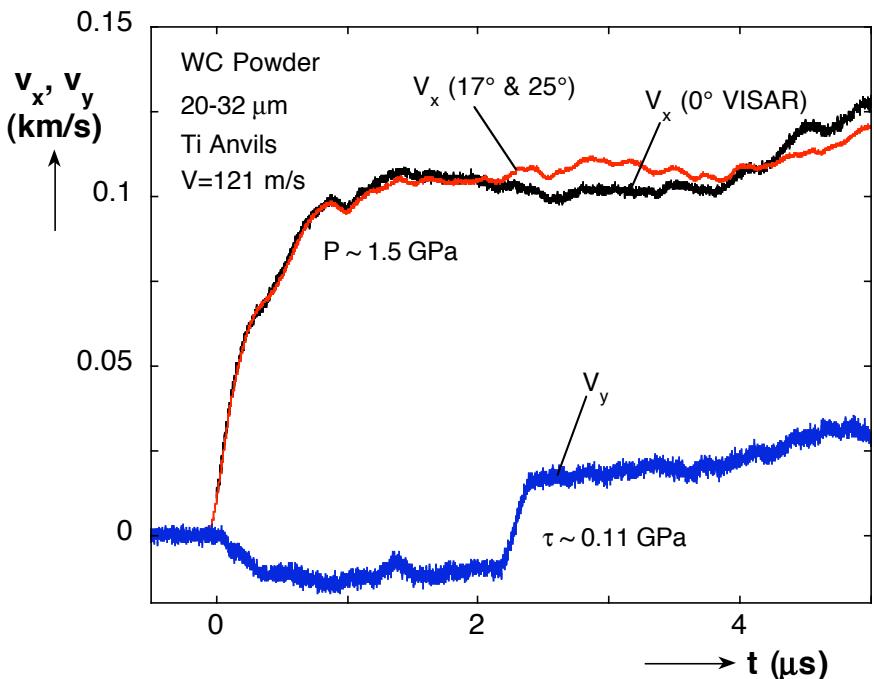
- strain rate given by:

$$\dot{\gamma} = \frac{V \sin \theta - v_{fs}}{h}$$



Experiment WC-1

- 250 μm sample thickness,
20-30 μm grains
- Ti-6-4 plates
- $V=121 \text{ m/s}$, $\theta=20^\circ$
- resolve velocities to normal (v_x) and transverse (v_y) components - check against 0° probe
- tilt causes initial transverse velocity
- nearly steady-state shearing observed after about 2.2 μs



$$\dot{\gamma} = \frac{V \sin \theta - v_y}{h} \approx 1 \times 10^5 \text{ s}^{-1}$$



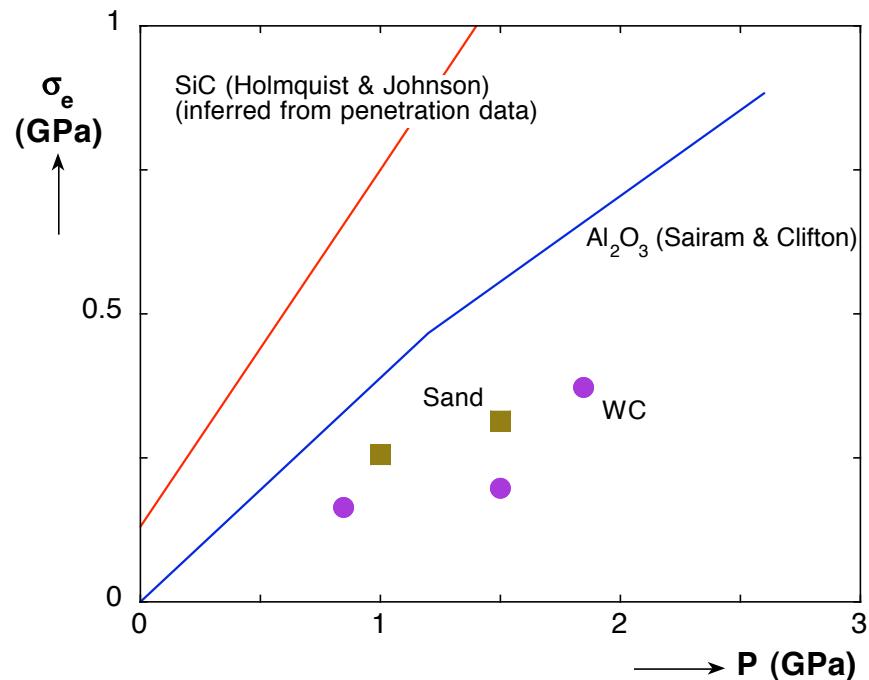
Ceramic Powder Strength

- Holmquist & Johnson inferred strength of granular SiC through high-velocity penetration experiments

- Sairam & Clifton performed pressure-shear experiments on Al_2O_3

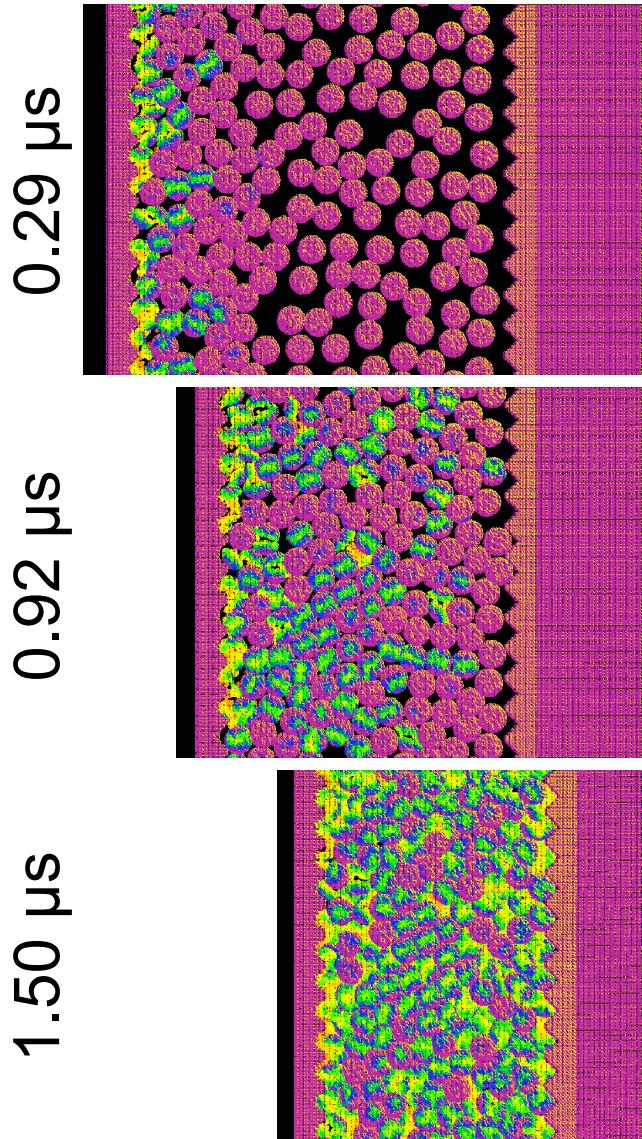
- current results appear plausible, but more work needed:

- ensure slippage not occurring (alternate anvil materials, surface finishes, angles, etc.)
- increase impact velocities/pressures
- examination of recovered plates / particles

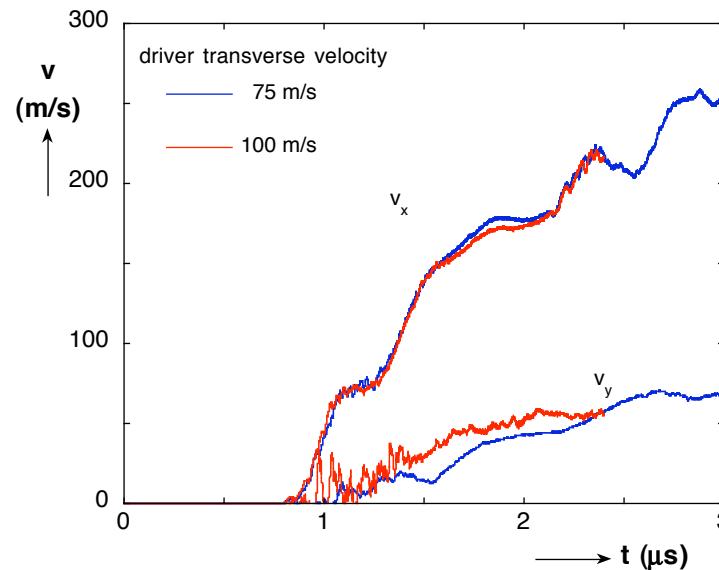




Mesoscale Simulations of Pressure-Shear Loading



CTH mesoscale simulations of pressure-shear loading are qualitatively wrong



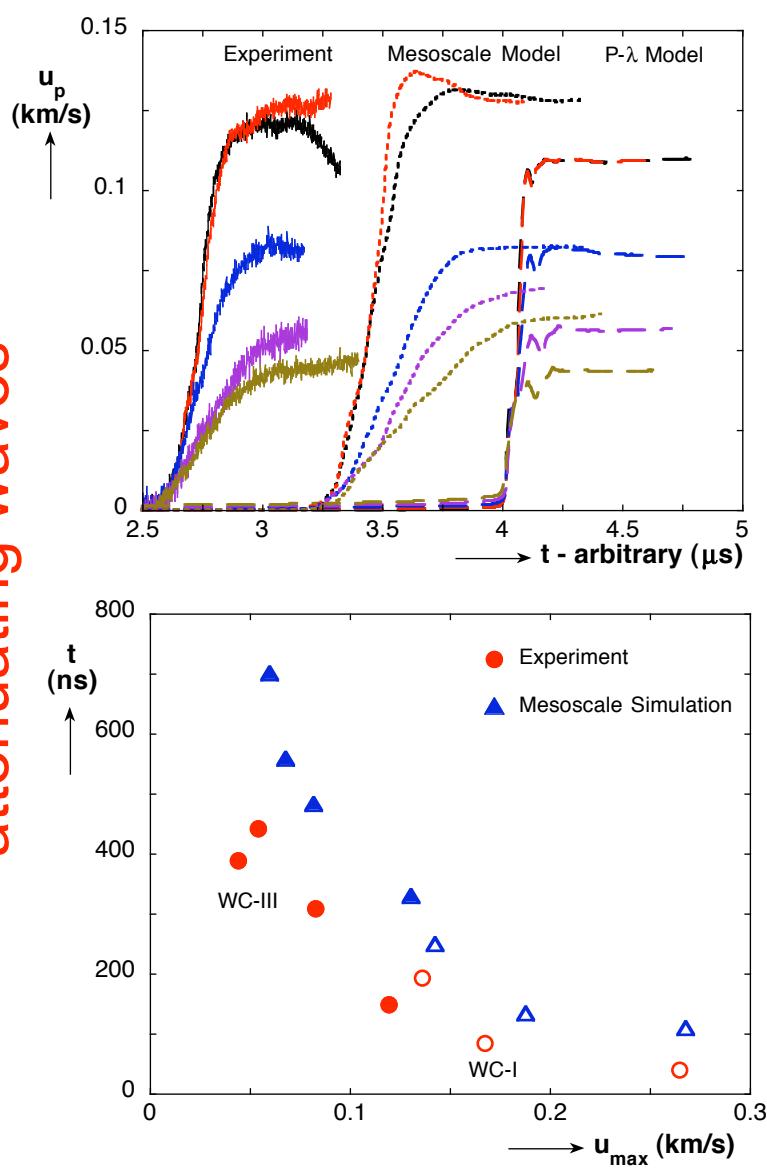
initial pressure-shear simulations with EMU promising, but additional work needed



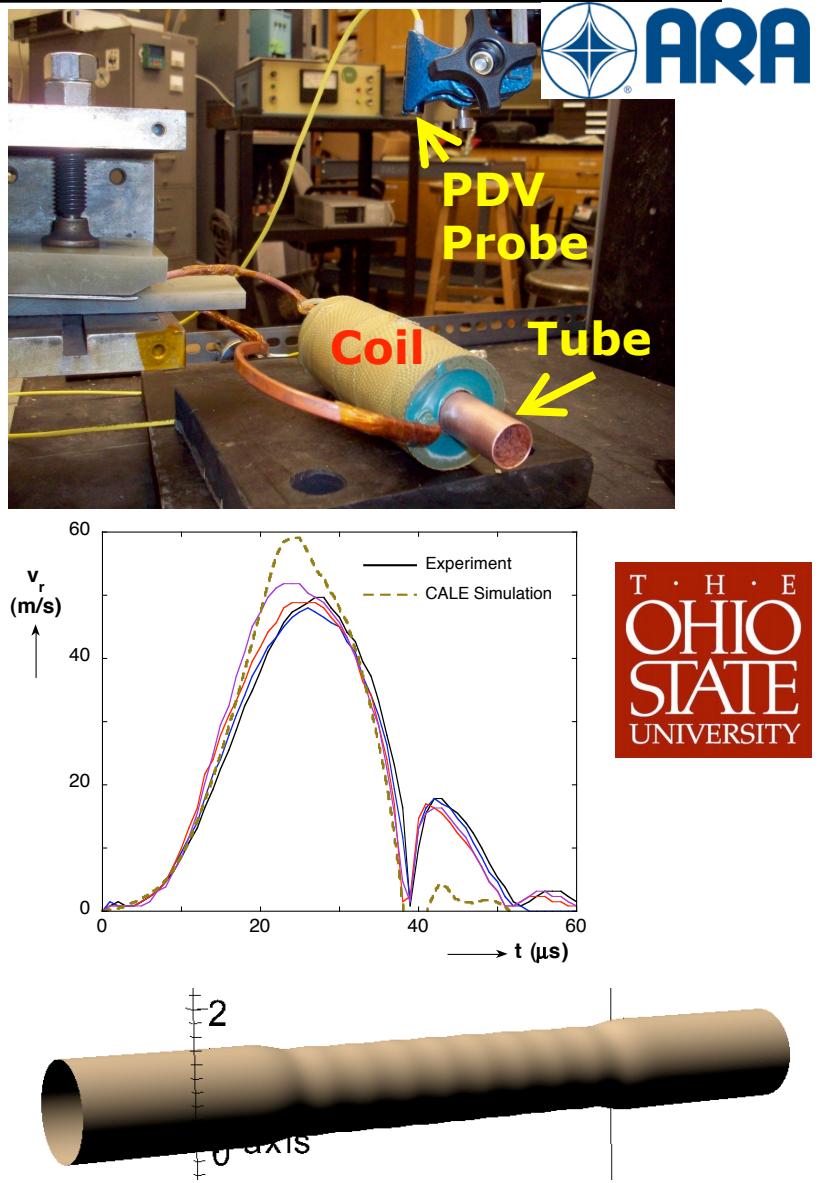
Dynamic Validation Experiments: necessary to build confidence in models

G. Daehn,
G. Fenton

attenuating waves



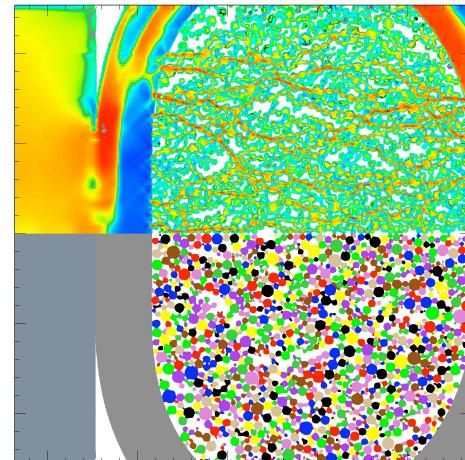
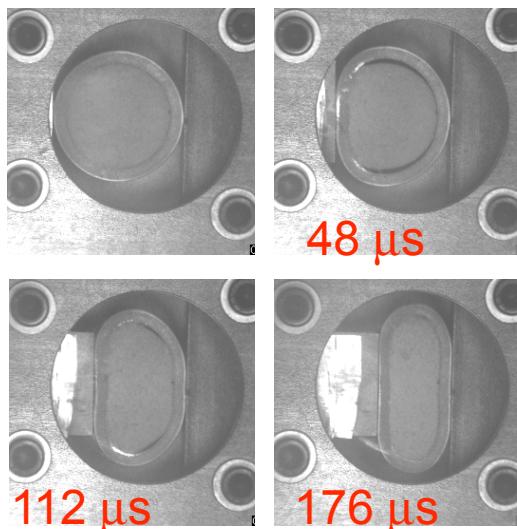
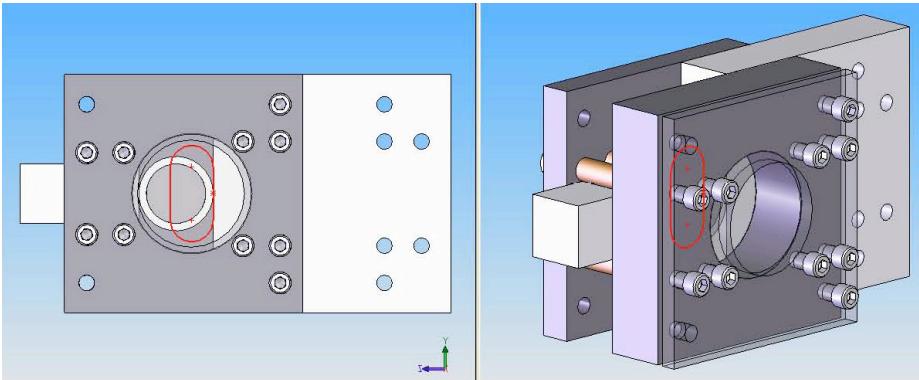
magnetically driven cylinders



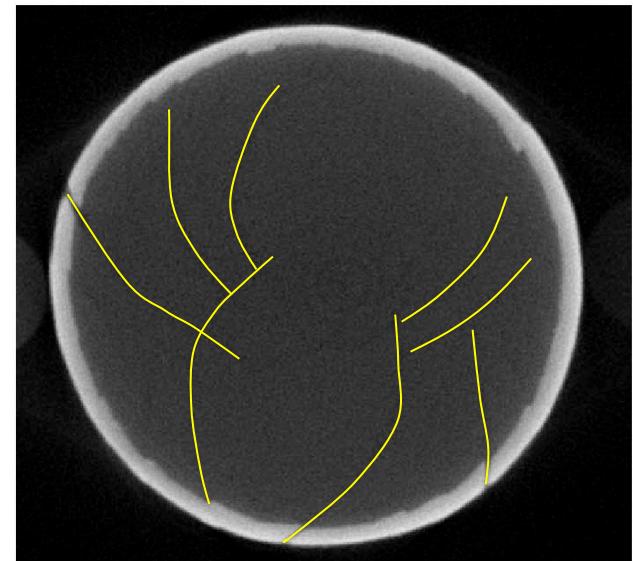


D. Sandoval

Validation Experiments for Granular Materials



K. Lappo



a good validation experiment is simple, instrumentable, in a relevant regime, well posed, repeatable, and sensitive to the relevant material behavior



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Conclusions

- **planar waves in granular ceramics:**
 - steady waves observed with very low wave speeds observed
 - waves have finite rise times; strain rate $\sim \sigma$
 - dynamic response significantly stiffer than static response for WC; about the same for sand
- **mesoscale simulations:**
 - nonuniform stress distribution (force chains)
 - significant lateral motion and distance to reach steady state
 - particle methods or other techniques needed for missing physics
 - may be suitable for some macroscopic simulations
- **high pressure experiments on Z:**
 - attain pressure levels that cannot readily be reached
 - probe thermal aspects of high pressure EOS
- **pressure-shear experiments:**
 - directly measure deviatoric response of granular materials
 - additional work needed to verify and understand results



Acknowledgements

J.P. Borg - mesoscale modeling

**W.D. Reinhart, T.F. Thornhill, J. Martinez, R. Palomino,
H. Anderson - STAR facility gas gun experiments**

**Z - the large crew for design, assembly and operations;
R. Lemke, M. Knudson for design & analysis**

D. Sandoval, K. Lappo - validation experiments

T. Buchheit - nanoindentation

**D.E. Grady, L.C. Chhabildas - decades of shock physics
experience**

*numerous technicians and support staff
are essential to facility operations*