

Wind Turbine Basics and Preliminary Design Analysis

Presented to Moffett Productions as a part of NMSBA

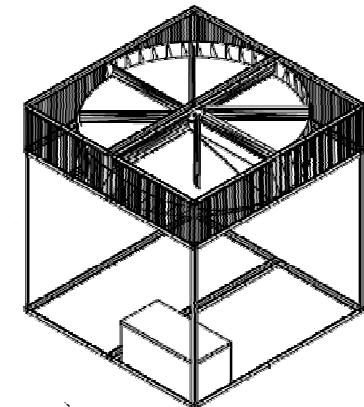


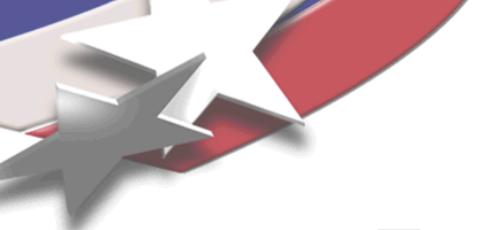
300W C type vertical axis wind turbine generator,
<http://www.alibaba.com/>

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Turbine Design Types Overview



<http://www.pollutionissues.com/Ec-Fi/Electric-Power.html>



http://www.eoearth.org/article/Darrieus,_Georges_Jeans_Mary

Horizontal Axis Wind Turbines (HAWT)

- Vast majority of grid connected commercial turbines
- Commercial wind turbines' power production is on the order of megawatts at ~\$.05/kWh
- Requires yawing mechanism to point into wind
- Driven by a lift system
- Vibration concerns due to flexible structure
- Light weight design enables access to high elevation greater wind speeds

Vertical Axis Wind Turbines (VAWT)

- Wind direction independent
- Less efficient design especially if drag type system
- Susceptible to damage from high wind conditions



Turbine Design Types Overview

Drag machine

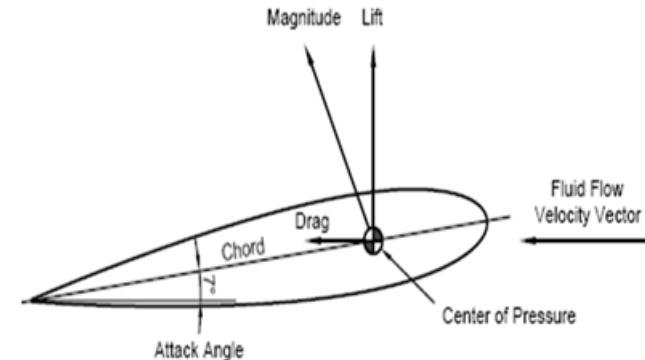
- Rotor surface cannot move faster than the wind speed resulting in reduced efficiency
- Relatively inexpensive and simple to design
- Useful for small power requirements
- Minimal current literature and research conducted due to limited number in operation



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Lift machine

- Efficiencies due to airfoil blades
- Rotor speed can be up to 10 times wind speed
- More complicated to analyze (typically need design software to analyze)
- Growing body of research and funding



<http://www.oea.com/energy/home>



Wind Power

$$P_w = \frac{1}{2} C_p \rho A v^3$$

P_w = power output from wind turbine (W)

ρ = density of air, 1.225 kg/m³ (15°C, sea level)

A = rotor swept area (m)

V = wind speed (m/s)

C_p = power coefficient

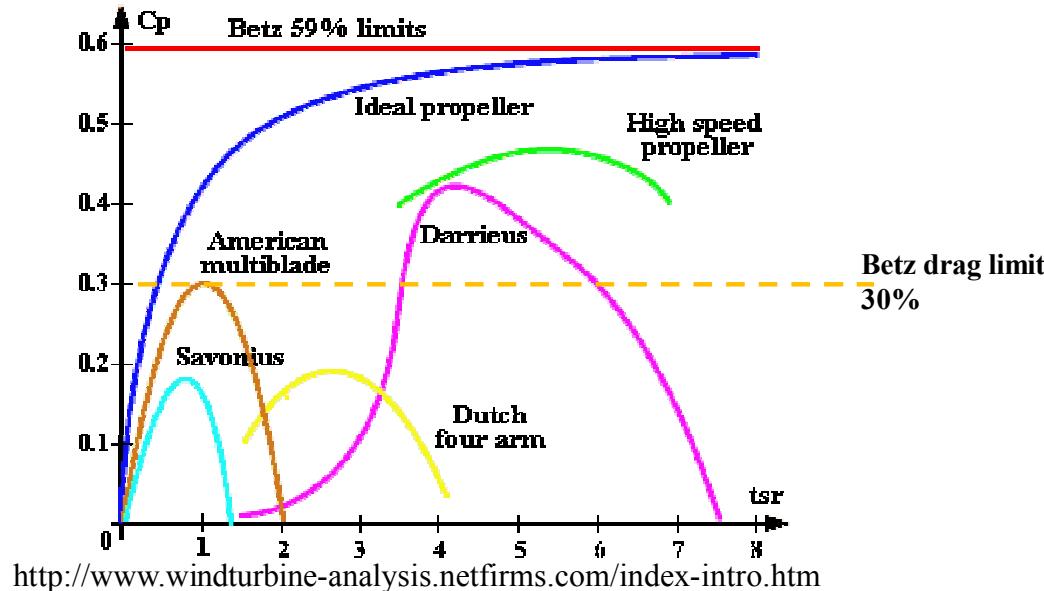
Betz limit law: using the law of conservation of mass and energy
no ideal wind-energy extraction machine can use more than
16/27 (59.3%) of the kinetic energy of the captured wind

$C_{p \max} = 0.59$ (lift)

$C_{p \max} = 0.3$ (drag)

Commercial modern HAWT designs between 70% to 80% of $C_{p \max}$

Power Coefficient (C_p)



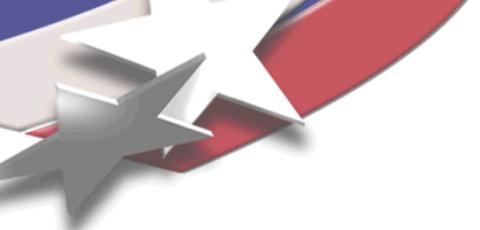
- Fraction of the power in the wind extracted by the rotor

$$c_p = \frac{\text{rotor power}}{\text{power in the wind}}$$

- Power coefficient varies with tip speed ratio (ratio of rotor tip speed to free wind speed)
- *Experimentally and analytically obtained value (Ideal HAWT with parallelepiped blades)*

$$c_p = \frac{I_{\text{shaft}} \omega^3}{\rho A v^3}$$

$$I_{\text{shaft}} = \frac{N_b \rho_b L_b W_b t_b L_b^2}{3}$$



Savonius Rotor

- Vertical axis drag turbine based on pressure difference between the retreating blade and the advancing blade due to differences in drag coefficients
- Wind tunnel performance study conducted by Sandia National Laboratories (May 1975) at Vought Systems Division Low Speed Wind Tunnel

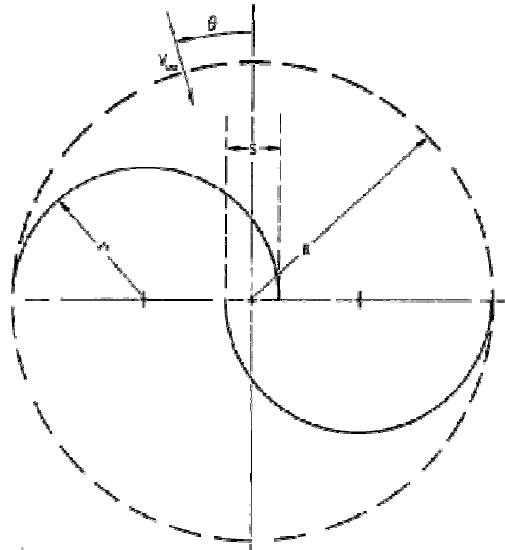
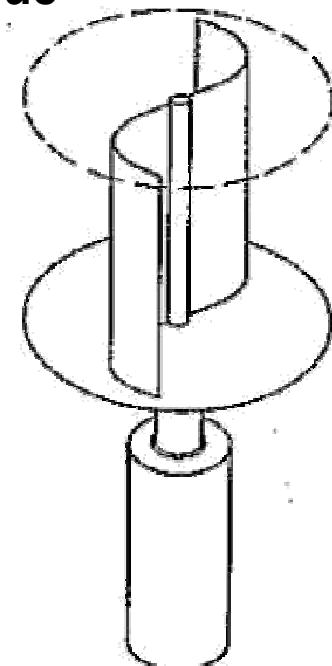


Figure 5. Schematic of the two-bucket Savonius rotor with 180° bucket

Sandia National Laboratories. [SAND76-0131 Wind Tunnel Performance Data for Two- and Three-Bucket Savonius Rotors](#) July, 1977.

Savonius-Rotor



<http://www.iwr.de/wind/tech/grund/typen.html>



SNL Savonius Rotor Experiment

- **Variables**

- **Number of buckets 2, 3**
- **Gap spacing (s/d) 0, 0.1, 0.15, 0.2**
- **Rotor height 1m, 1.5m**
- **Free stream velocity 7m/s 14 m/s**

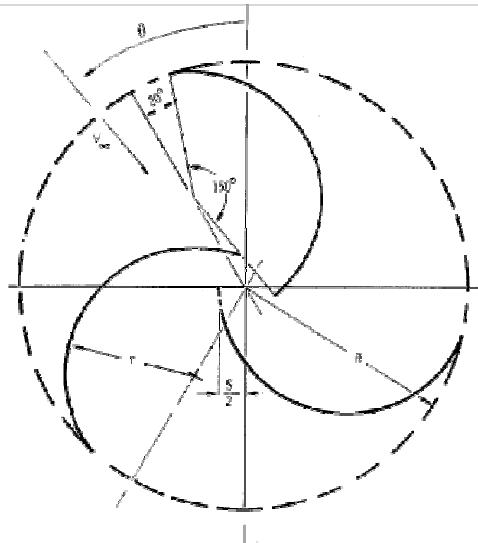
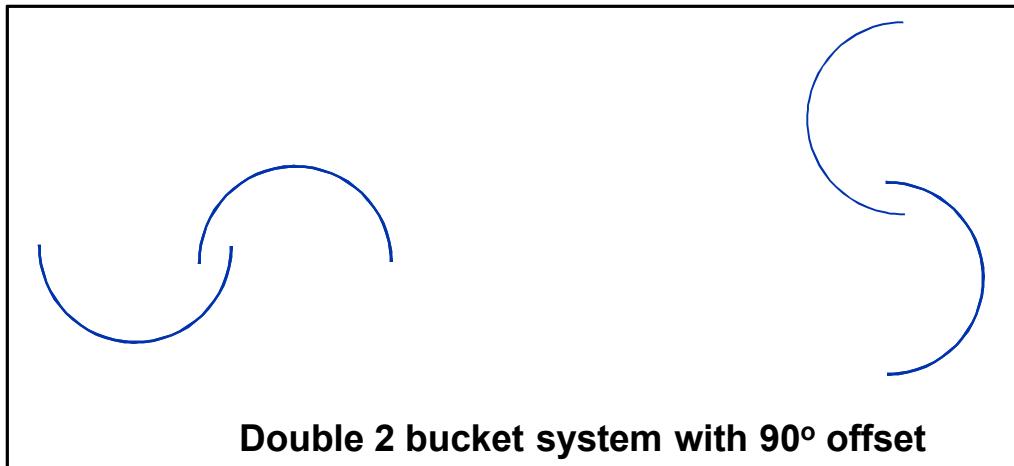


Figure 6. Schematic of the three-bucket Savonius rotor with 150° buckets.



SNL Savonius Rotor Experiment Results

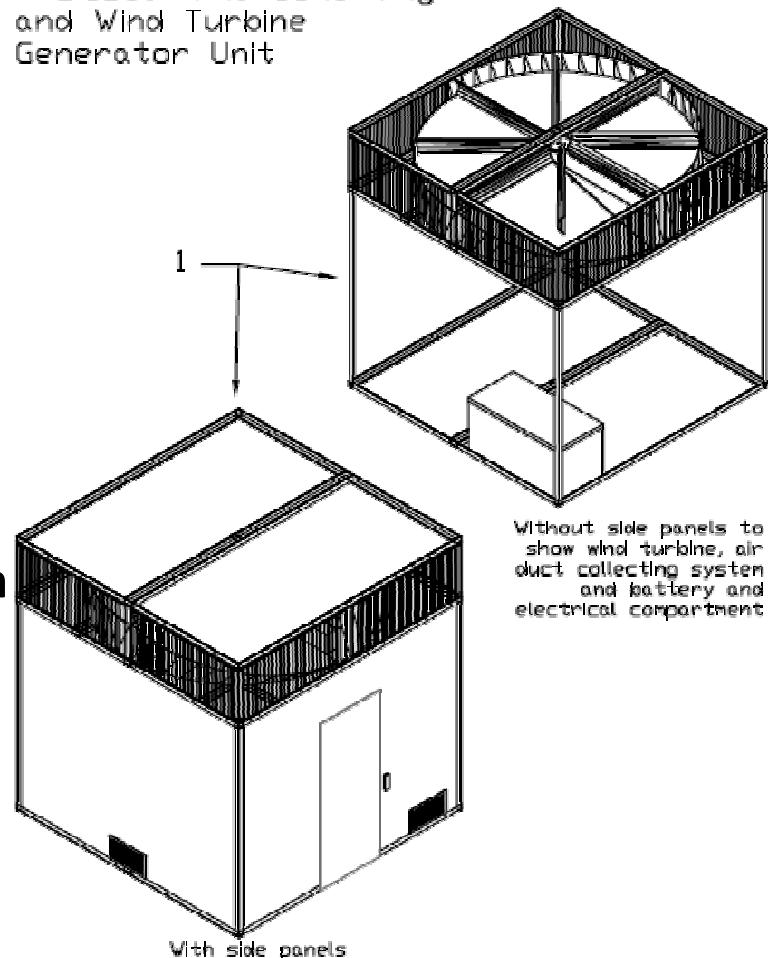
- Static torque coefficient for the 2 bucket system had *higher variability* and *greater minimum torque* values than the 3 bucket system. Double 2 bucket systems with 90 degree offset was optimal.
- Bucket overlap ratio between 0.1-0.15 was optimal
- Peak power coefficient (Cp) values ranged between 0.22-0.26 for the *two-bucket* configuration and were 0.15-0.17 for the *three bucket* configuration



Design Assumptions

- Inconspicuous design to avoid radar detection
- Portable – not grid-tied , battery charging
- Nominal dimension 9m x 9m x 9m
- Power 1.5kW – 3.0 kW
- Air Duct System
 - Removed for initial calculations
 - Potentially useful to protect turbine from high wind conditions
- Turret
 - Rotor shape makes design independent of wind direction

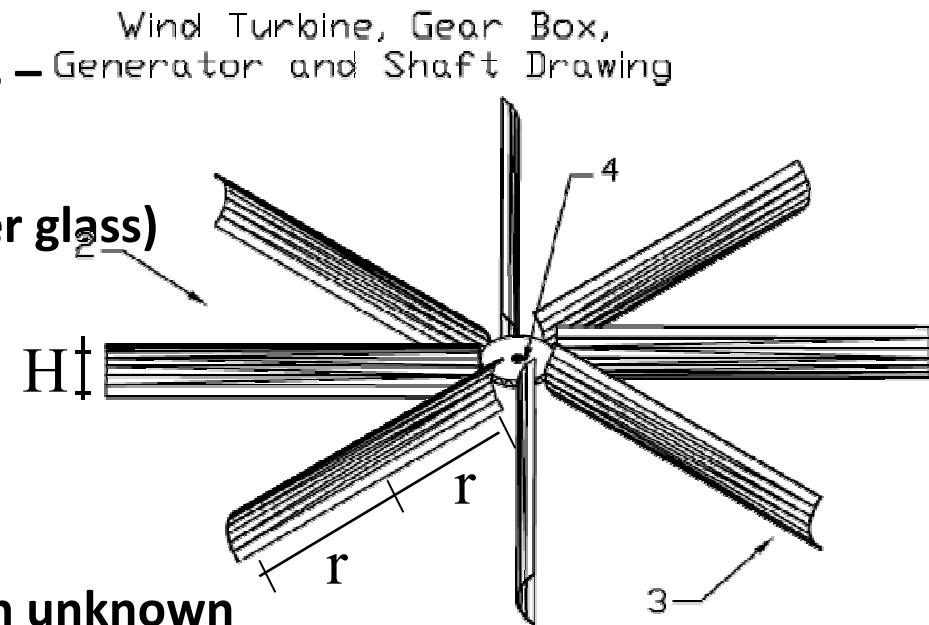
Enclosed Wind Collecting and Wind Turbine Generator Unit



Design Assumptions

- Rotor shape and dimension

- No deflection due to gravity loads – Generator and Shaft Drawing
blade supported on bottom
 - Material unspecified (assume fiber glass)
 - Diameter = 9 meters
 - Assume 3 blades
 - Cupped shape



- Wind Speed

- Portable design therefore location unknown
 - Height of turbine approx 9 m
 - Solve for minimal wind speed for feasibility study

- Similar performance to a Savonius



Solving for wind speed, v

$$v = \left(\frac{P_w}{\frac{1}{2} C_p \rho A} \right)^{1/3}$$

$P_w = 1.5 \text{ kW}$

$\rho = \text{density of air, } 1.225 \text{ kg/m}^3 \text{ (15°C, sea level)}$

$A = 4rH \text{ (m)} = 4 * 2.25\text{m} * 1.25\text{m} = 11.25 \text{ m}^2$

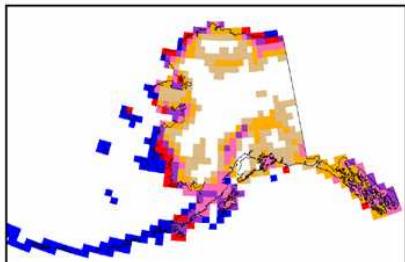
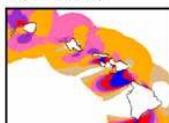
$C_p = \text{power coefficient} = .17$

$$V = 10.86 \text{ m/s}$$

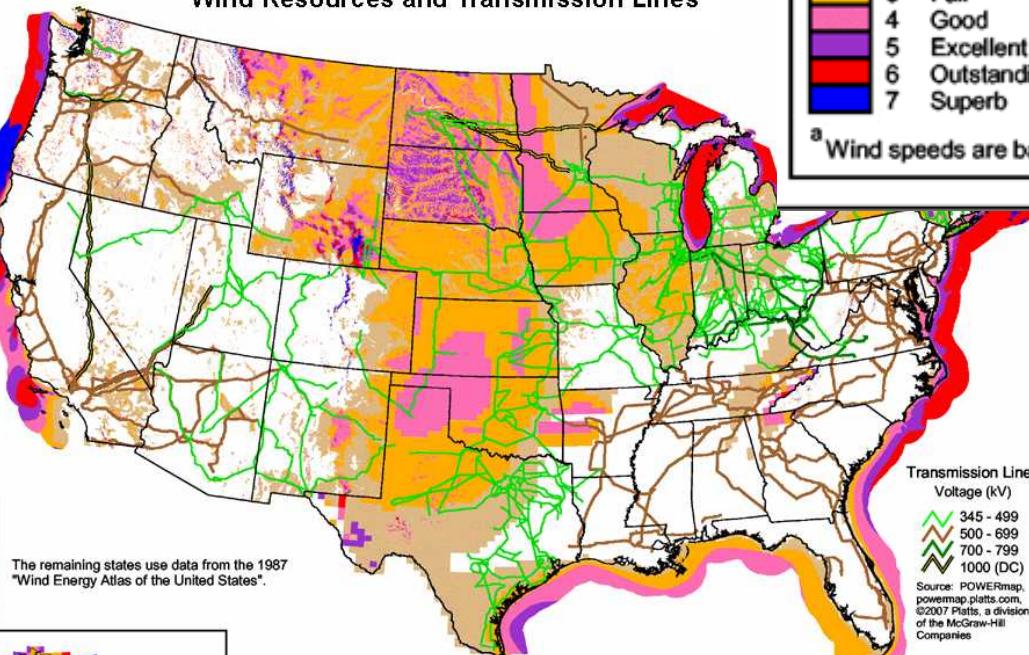
United States Wind Speed Data

- What does 10.9 m/s mean?

NREL Updated Maps:
 Arizona (2003)
 California (2002)
 Colorado (2004)
 Connecticut (2001)
 Delaware (2002)
 Hawaii (2004)
 Idaho (2002)
 Illinois (2001)
 Indiana (2004)
 Maine (2001)
 Maryland (2002)
 Massachusetts (2001)
 Michigan (2004)
 Missouri (2005)
 Montana (2002)
 Nebraska (2005)
 Nevada (2003)
 New Jersey (2002)
 New Hampshire (2001)
 New Mexico (2003)
 North Carolina (2002)
 North Dakota (2000)
 Ohio (2004)
 Oregon (2002)
 Pennsylvania (2002)
 Rhode Island (2001)
 South Dakota (2001)
 Texas mesas (2000)
 Utah (2003)
 Vermont (2001)
 Virginia (2002)
 Washington (2002)
 West Virginia (2002)
 Wyoming (2002)



Wind Resources and Transmission Lines



The remaining states use data from the 1987 "Wind Energy Atlas of the United States".

Wind Power Classification				
Wind Power Class	Resource Potential	Wind Power Density at 50 m W/m ²	Wind Speed at 50 m m/s	Wind Speed at 50 m mph
2	Marginal	200 - 300	5.6 - 6.4	12.5 - 14.3
3	Fair	300 - 400	6.4 - 7.0	14.3 - 15.7
4	Good	400 - 500	7.0 - 7.5	15.7 - 16.8
5	Excellent	500 - 600	7.5 - 8.0	16.8 - 17.9
6	Outstanding	600 - 800	8.0 - 8.8	17.9 - 19.7
7	Superb	800 - 1600	8.8 - 11.1	19.7 - 24.8

^a Wind speeds are based on a Weibull k value of 2.0

Effect of elevation on wind:

$$v_2 = v_1 \left(\frac{h_2}{h_1} \right)^n$$

Solving for v2...

$$h_1 = 9 \text{ m} \quad v_1 = 10.9 \text{ m/s}$$

$$h_2 = 50 \text{ m} \quad n = \text{ground surface friction coefficient choose 0.2}$$

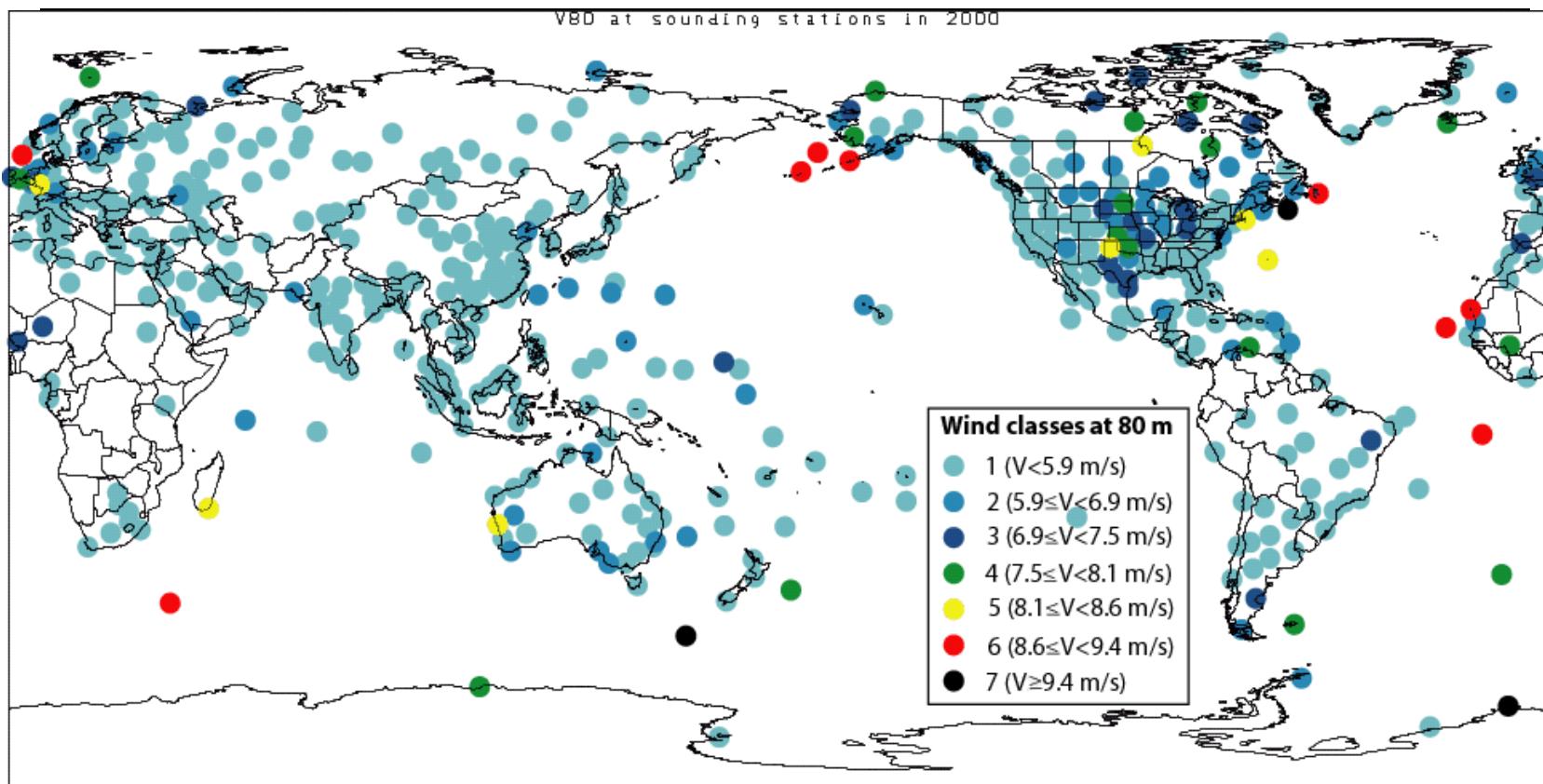
N=0.1, water or smooth ground

N=0.2, tall crops

N=0.3 city downtown

$$v_2 = 15.3 \text{ m/s}$$

Global Wind Speed Data



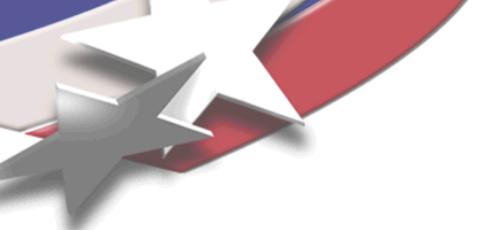
Map of wind speed extrapolated to 80 m an averaged over all days of the year 2000 at sounding locations with 20 or more valid readings for the year 2000 (Archer, 2005) .

$$v_2 = v_1 \left(\frac{h_2}{h_1} \right)^n$$

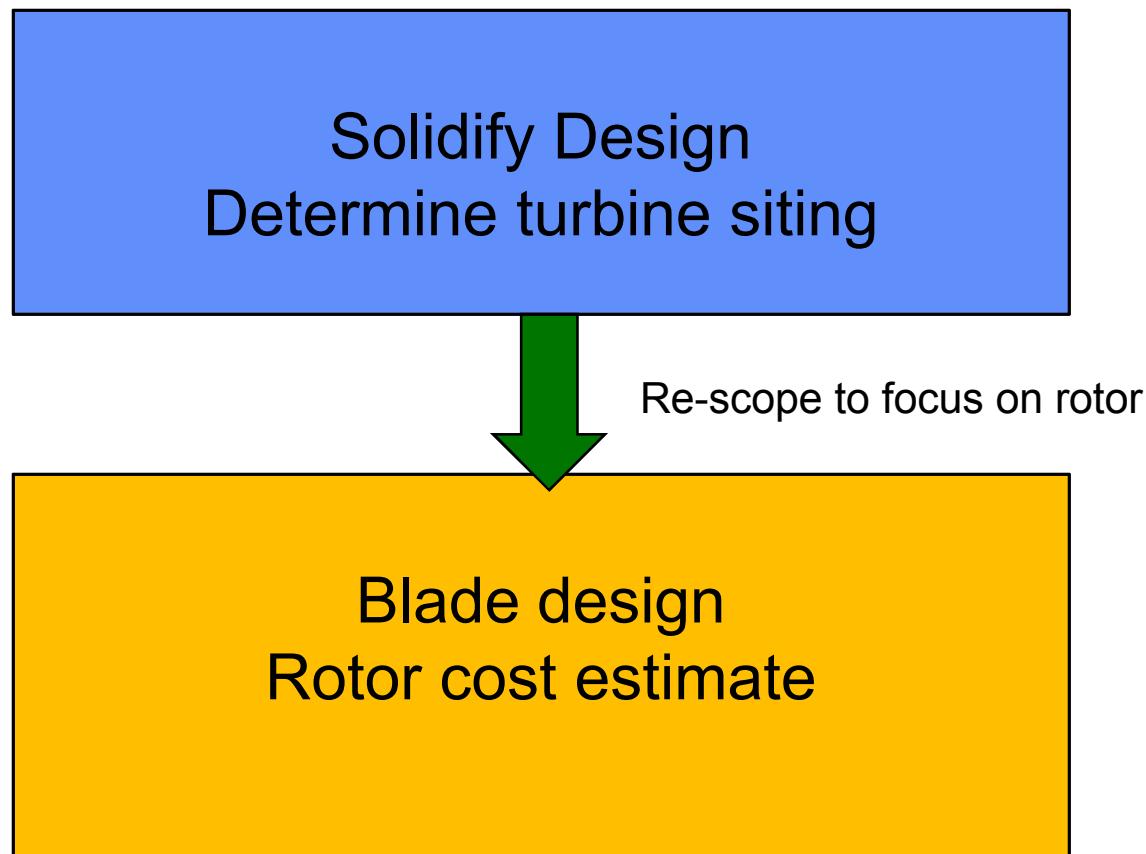
$h_1 = 9 \text{ m}$ $v_1 = 10.86 \text{ m/s}$
 $h_2 = 80 \text{ m}$ $n = 0.2$
 $v_2 = 16.8 \text{ m/s}$



Sandia
National
Laboratories



Next Steps





References

Archer, C.L. and Mark Z. Jacobson. “Evaluation of global wind power” *Journal of Geophysical Research – Atmospheres*, 2005.

Burton, Tony et al. Wind Energy Handbook Chichester: John Wiley & Sons Inc, 2001.

Manwell, J.F., J.G McGowan and A.L. Rogers. Wind Energy Explained Theory, Design and Application Chichester: John Wiley & Sons Inc, 2009.

Paraschivoiu, Ion. Wind turbine design: with emphasis on Darrieus concept Montreal: Polytechnic International Press, 2002.

Sandia National Laboratories. SAND76-0131 Wind Tunnel Performance Data for Two- and Three-Bucket Savonius Rotors July, 1977.



QUESTIONS/COMMENTS

<http://www.greenrightnow.com/kabc/2009/07/14/new-texas-water-tower-will-combine-wind-power/>



Design Worksheet