

# Mixing-controlled Reactive Transport at the Pore Scale and Its impact on Flow Field and Upscaling of Reactive Transport



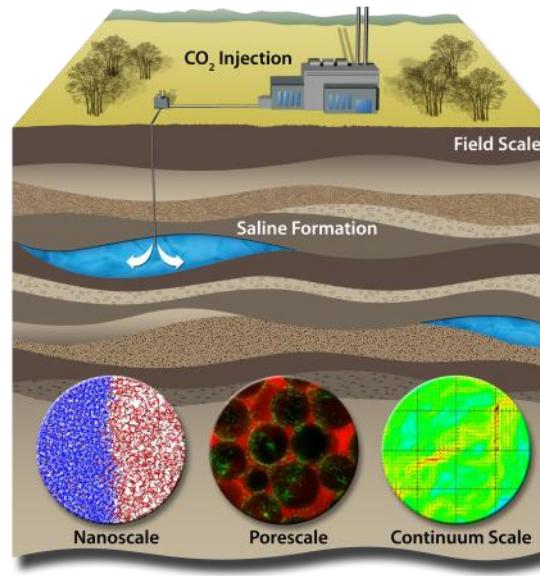
Hongkyu Yoon

September 4, 2013



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# Outline

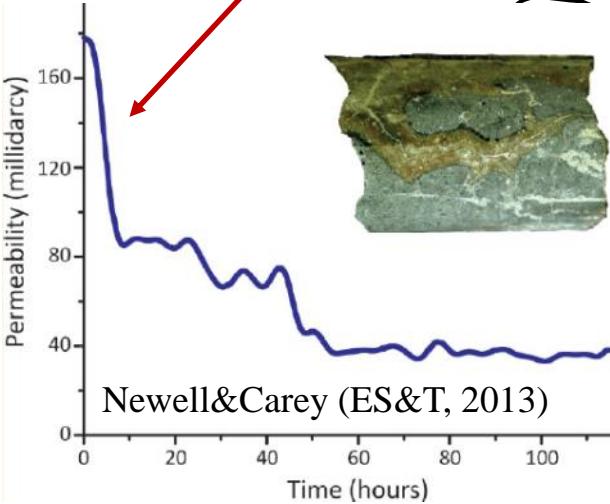
- **Motivations**
- Research Efforts
- Research Highlights
- Future Works

# Reactive Transport Processes during Geological Carbon Storage

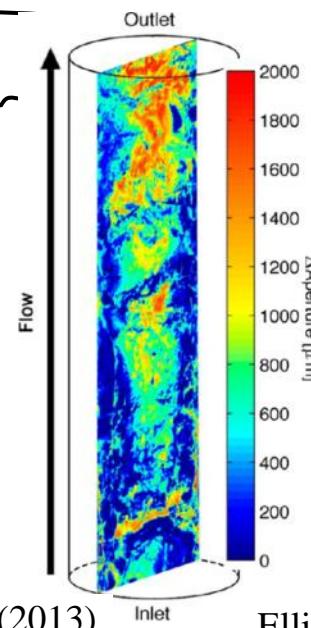
Injection well

Caprock  
Storage zone

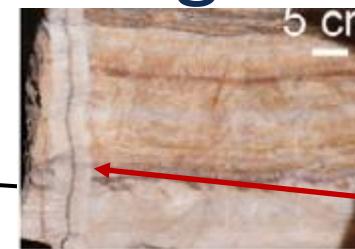
Permeability at the interface of cement and siltstone



Deng et al. (2013)

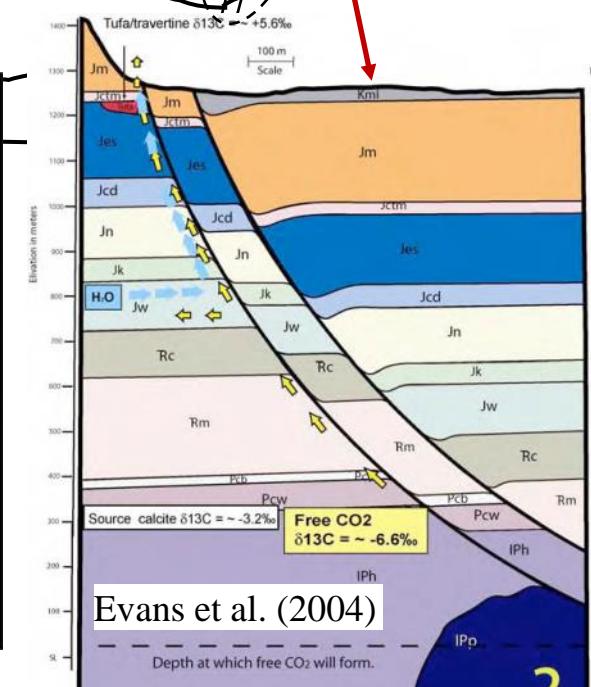


Ellis et al. (2013)



Gratier et al.,  
Geology, 2012;  
Crystal Geyser,  
Utah

fault

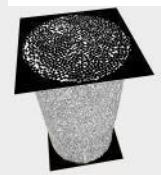


# Multi-Scale Problems

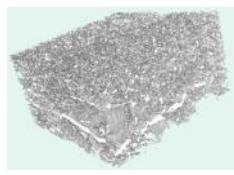
## Pore Scale



Core sample



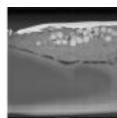
Micro-CT



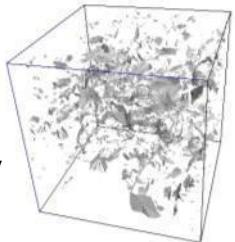
Statistical REV



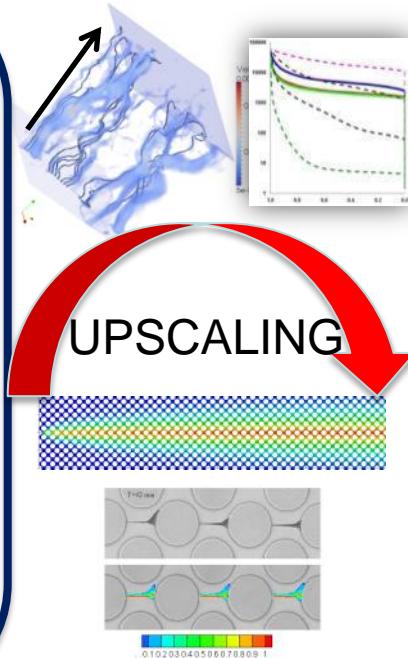
Confocal Microscopy



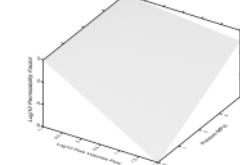
FIB-SEM



Pore throats



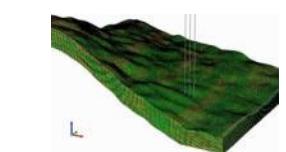
## Grid Block Scale



Reaction rate



Reactive flow



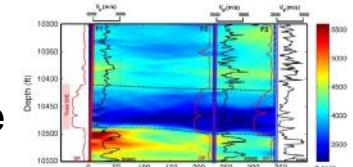
3D permeability field

Observed Data

Different types

Spatial scale

Temporal scale



Seismic data

## Predictive

Fundamental (first-principles)

Complex

Molecular Dynamics  
(molecular scale)

Solid/Fluid Dynamics  
(pore scale)

Darcy's Law  
(continuum scale)

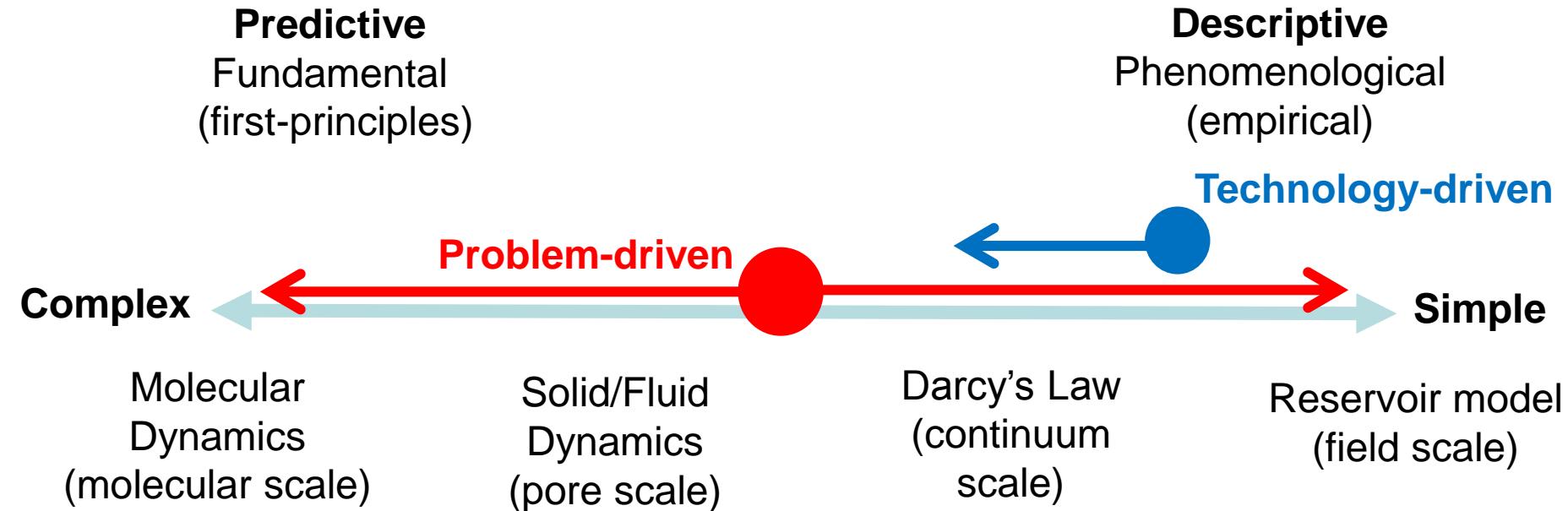
## Descriptive

Phenomenological (empirical)

Simple

Reservoir model  
(field scale)

# What is the approximate level of complexity?



Where do we want (or need) to be?  
Where can we be in practice?

# Research Direction

- Develop experimental and numerical tools to study a comprehensive understanding of multi-physics processes over a range of scales (nano to field scales)
- Apply recent advances in tool development to bridge the gap between two questions

## Example: Pore Scale Reactive Transport

- Developed a novel pore scale reactive transport model of coupled fluid flow, reactive transport, and precipitation and dissolution using pore scale experiments in a microfluidic pore-network (i.e., micromodel)

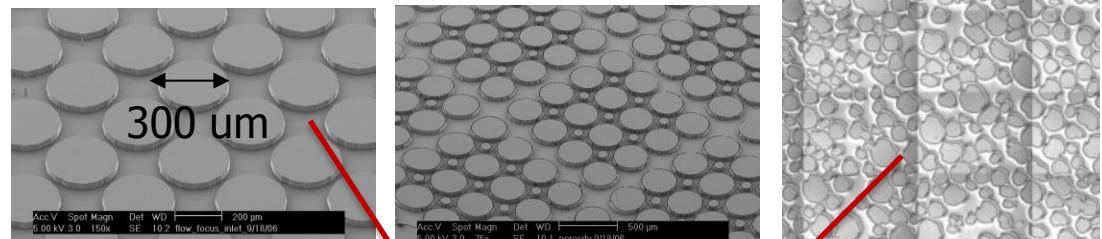
# Micromodel Experiment

## Micromodel Description

Depth: ~20 mm

Porosity: ~0.39

Flowrate: ~2 cm/min

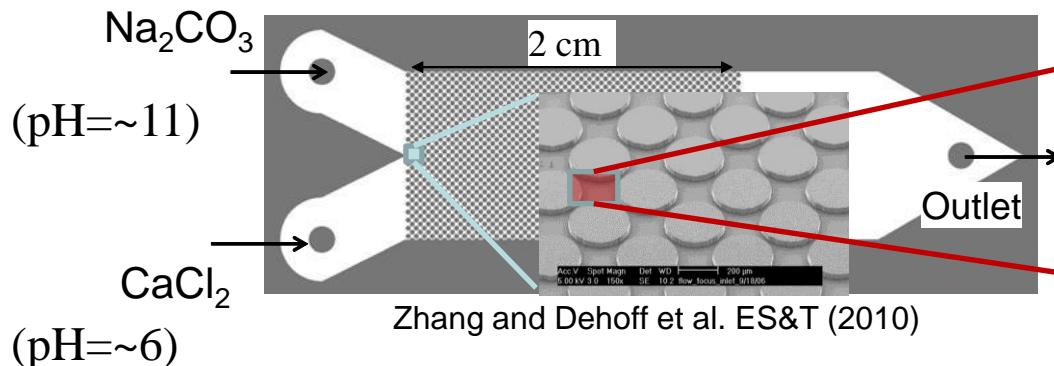


Base Case  
Small Cylinder

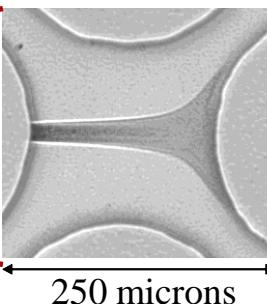
Aggregates

Irregular

Thermal oxidation:  
~ 100 micron thick oxide layer



Zhang and Dehoff et al. ES&T (2010)

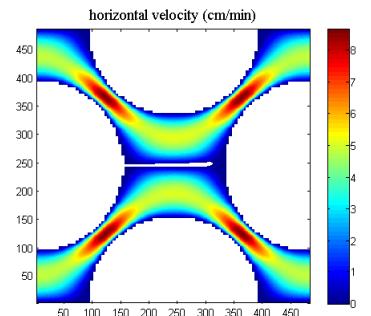


Microscopic image of  
calcium carbonate  
(CaCO<sub>3</sub>) precipitates

- Two solutions are mixing along the centerline and CaCO<sub>3</sub> precipitates
- Range of concentrations and solution chemistry vary
- Microscopic images are taken over time

# Pore Scale Model Framework

Lattice Boltzmann Method:  
Velocity field ( $u$ ) at pore scale



Velocity

Finite Volume Method: Reactive transport at pore scale

$\Delta t$

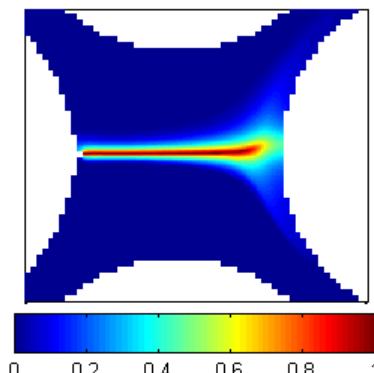
$\Psi_j = C_j + \sum_{i=1}^{N_{eq}} \nu_{ji} C_i$  Chemical equilibrium in bulk fluid (e.g.,  $\text{H}^+$ ,  $\text{HCO}_3^-$ , ...)  
Extended Debye-Hückel Equation for activity coefficients

$$D \frac{\partial \Psi_j}{\partial \mathbf{n}} = -I_m \quad \text{on reactive surface}$$

$$I_m = k_{cc} \left( [\Omega]^n - 1 \right)^n \quad \Omega = \frac{Q_{cc}}{K_{sp}} \text{ or } \ln \left( \frac{Q_{cc}}{K_{sp}} \right)$$

Update of  $\text{CaCO}_3$  volumetric content ( $V_m$ )

$$\frac{\partial V_m}{\partial t} = \overline{V_m} s_m k_{cc} \left( \left[ \frac{a_{\text{Ca}^{2+}} a_{\text{CO}_3^{2-}}}{K_{sp}} \right]^n - 1 \right)^m$$

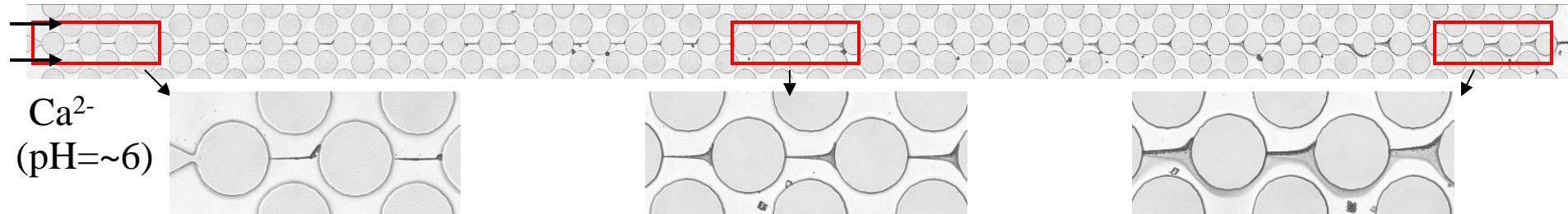


Mineral phase  
volumetric content

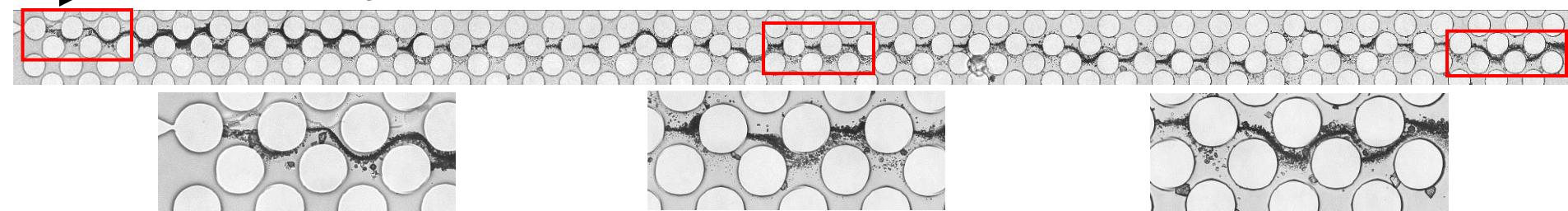
# Experimental Results

$\text{CO}_3^{2-}$ (pH=~11)  $[\text{Ca}^{2+}]_T = [\text{CO}_3^{2-}]_T = 25 \text{ mM}$  at ~2 hrs

Zhang et al., ES&T (2010)

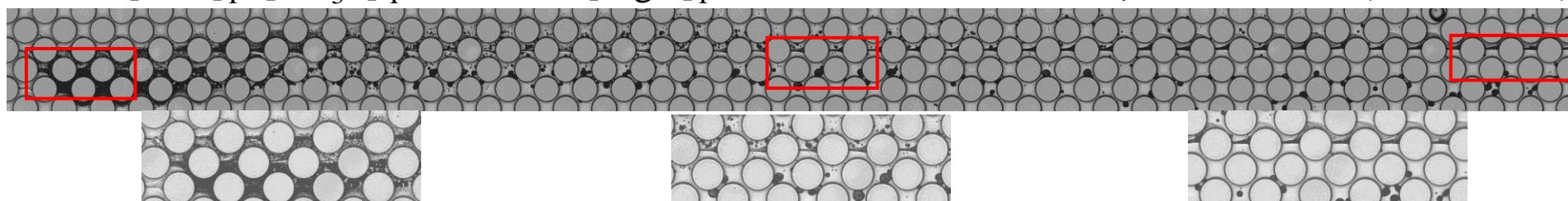


$[\text{Ca}^{2+}]_T = [\text{CO}_3^{2-}]_T = 6.5 \text{ mM}$  at ~24 hrs



$[\text{Ca}^{2+}]_T = [\text{CO}_3^{2-}]_T = 10 \text{ mM}$  &  $[\text{Mg}^{2+}]_T = 40 \text{ mM}$  at ~16 hrs

Boyd, Yoon et al., GCA (2013, submitted)

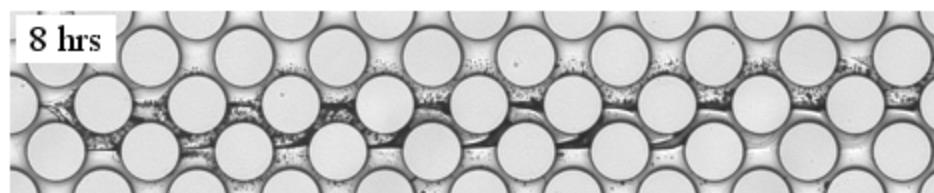
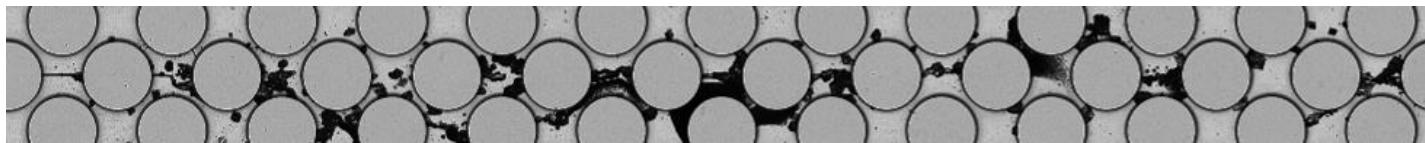


- Precipitation ~ along the centerline within 1-2 pore spaces in the transverse direction
- Width of the precipitate line ~ increase with distance from the inlet
- Rate of precipitation is concentration and species dependent

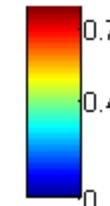
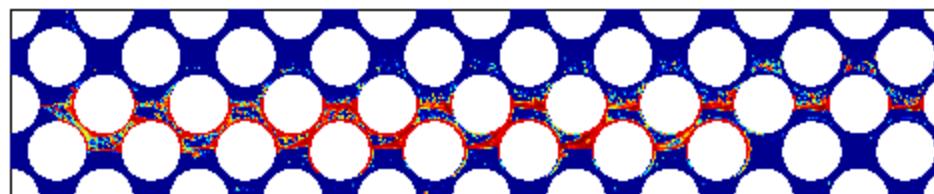
# Image Analysis

## Otsu thresholding

- Pixels segmented into foreground and background
- Uses threshold values that result in minimum interclass variance between foreground and background



Volumetric Fraction of Precipitate



# Results: Precipitation only at grain boundary

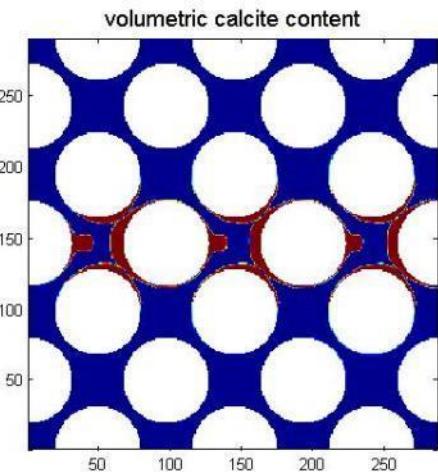
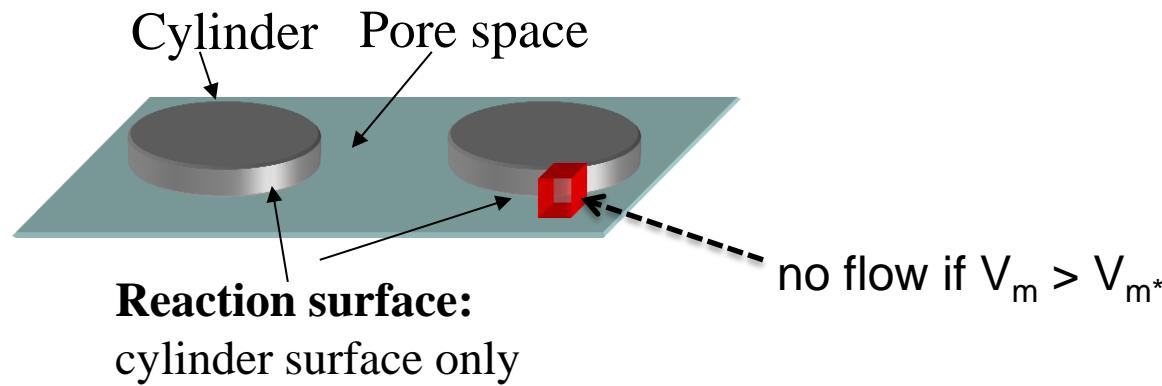
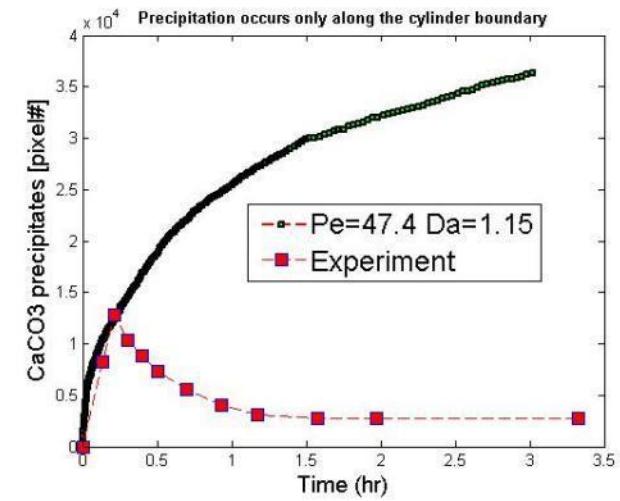


Image of precipitates  
at 180 min



25 mM  
Experiment



# Precipitation patterns

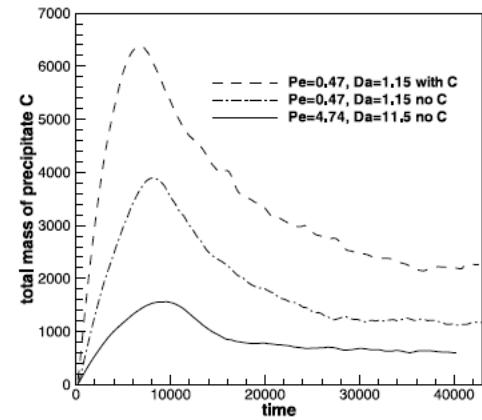
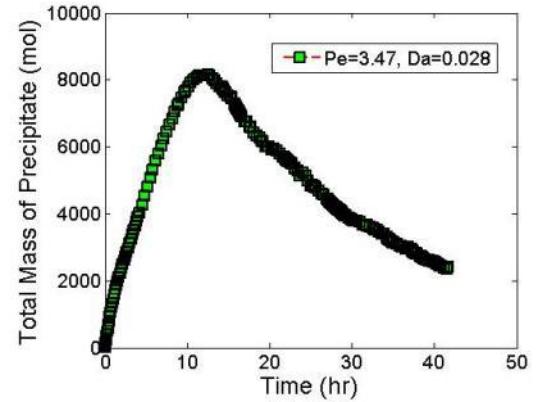
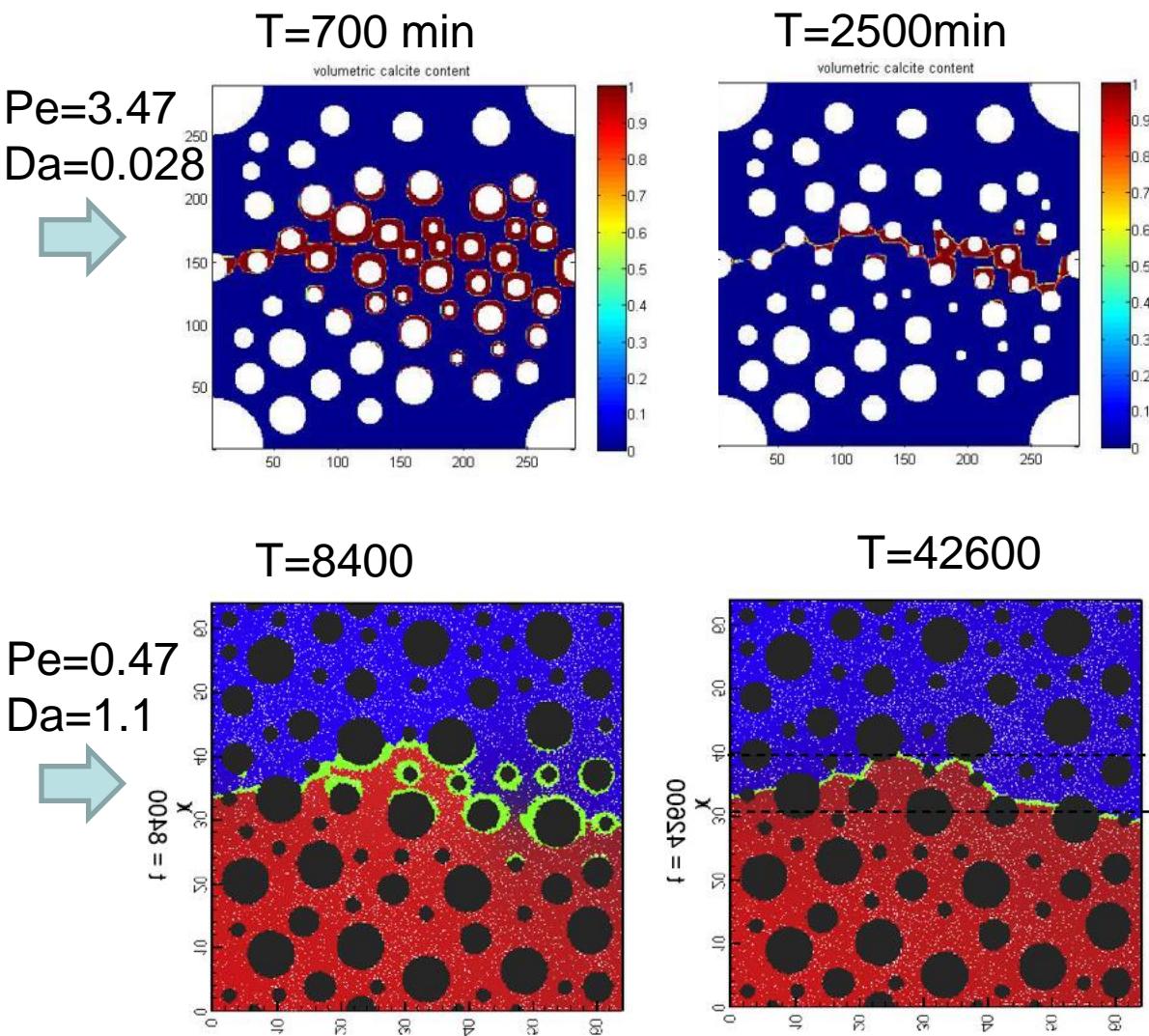
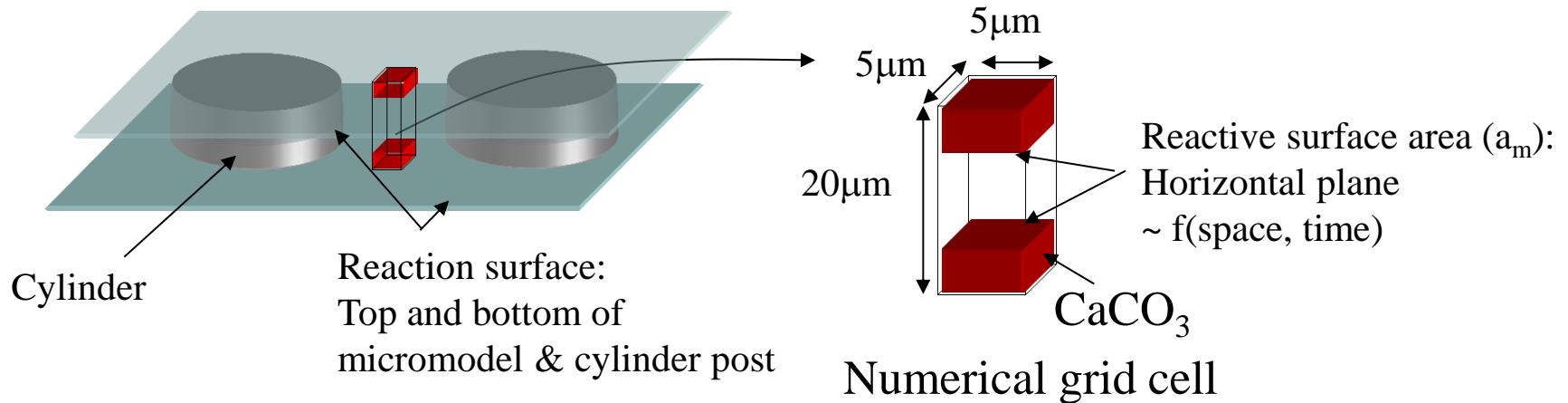


Figure 8. Time dependence of the total mass of precipitate  $C$  obtained from several simulations with and without the intermediate reaction product,  $C$ , for different  $Pe$  and  $Da$ .

# Reaction in a micromodel system

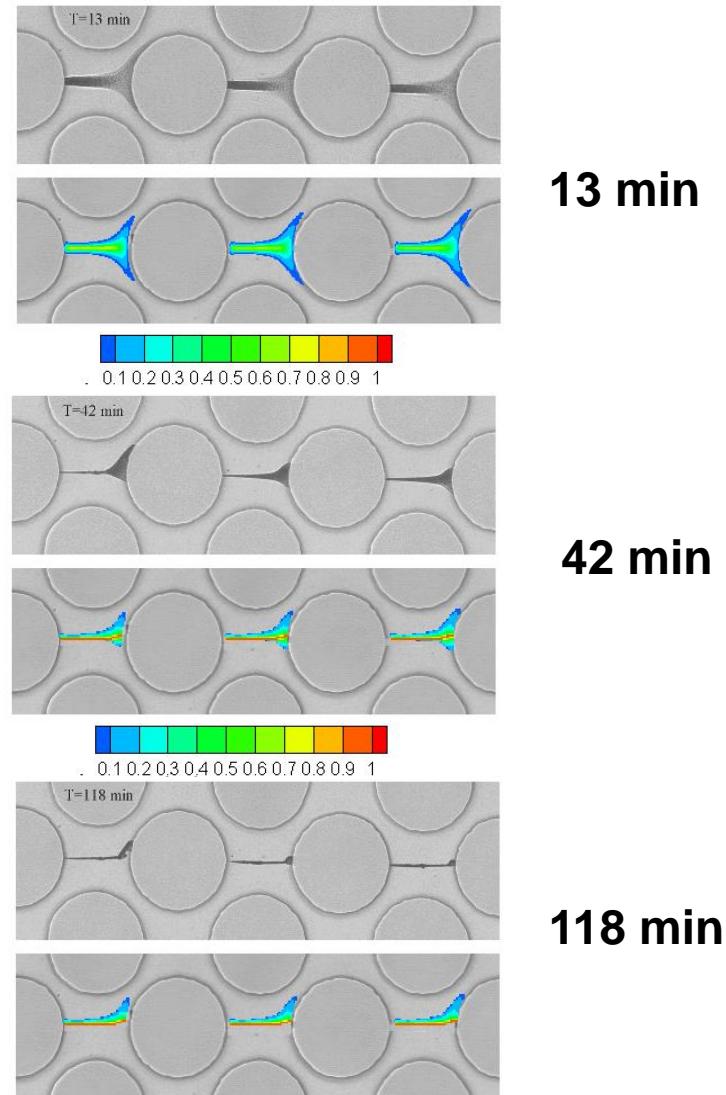
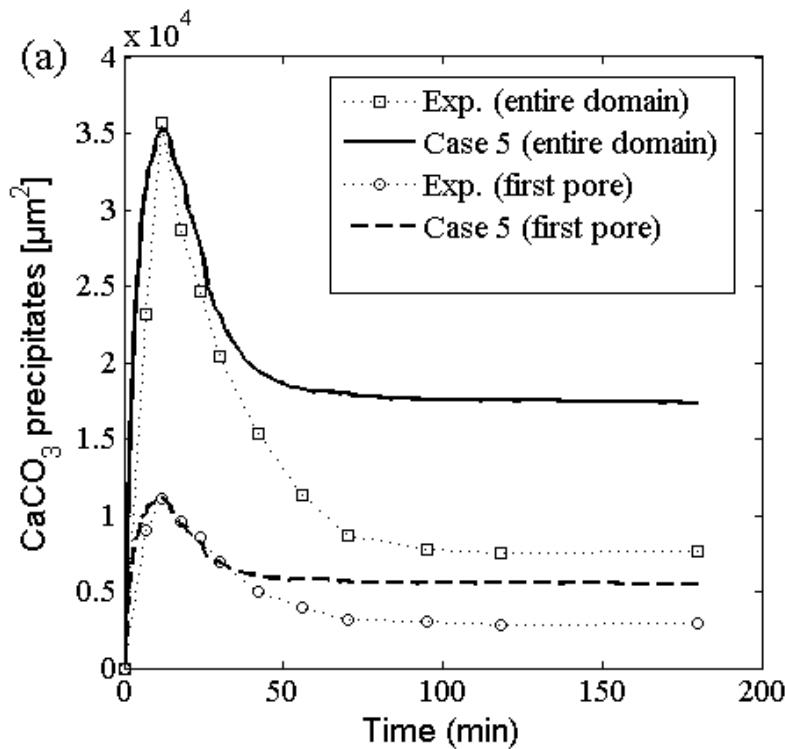
## 1. Quasi 3D grid cell for reactive surface



## 2. Effective diffusion coefficient = $D_m * \text{tortuosity} (\tau)$

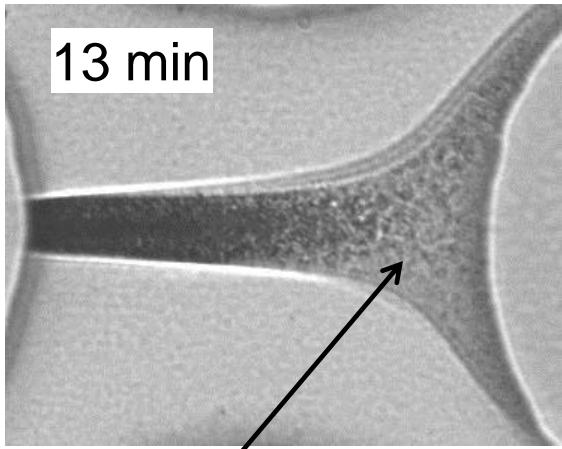
- $\tau(V_m) = (1 - V_m)^n$  where  $n \sim 0$  to 3
- Diffusion is allowed until the grid cell is fully occupied by  $\text{CaCO}_3$

# Simulation results: Increase surface area during dissolution by 300

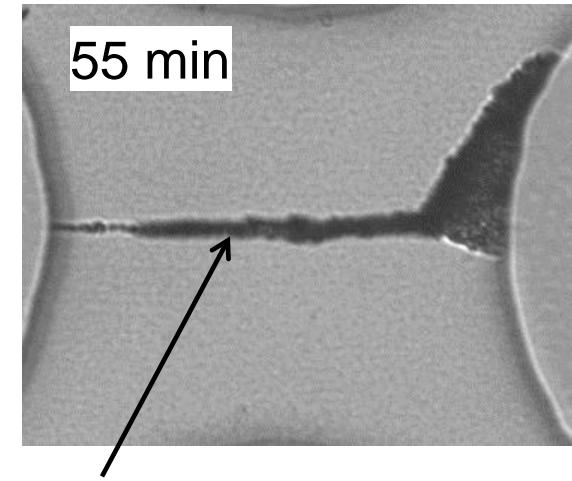
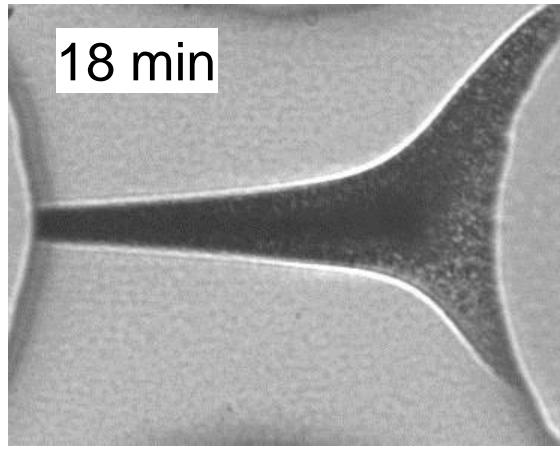


- Model results match thickness and area of precipitate until 30 min
- Model predicts dissolution below the centerline well, but not above the centerline

# Matching simulation to late-time dissolution

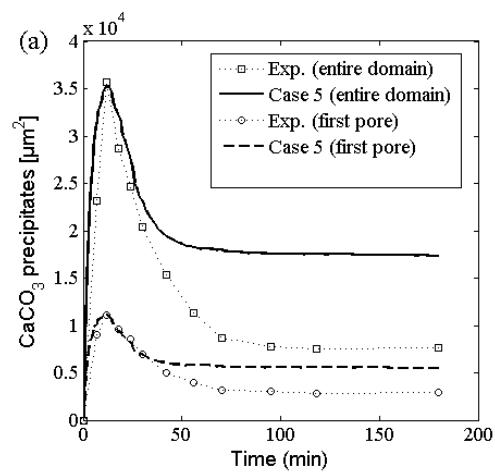


Amorphous Calcium Carbonate & Vaterite



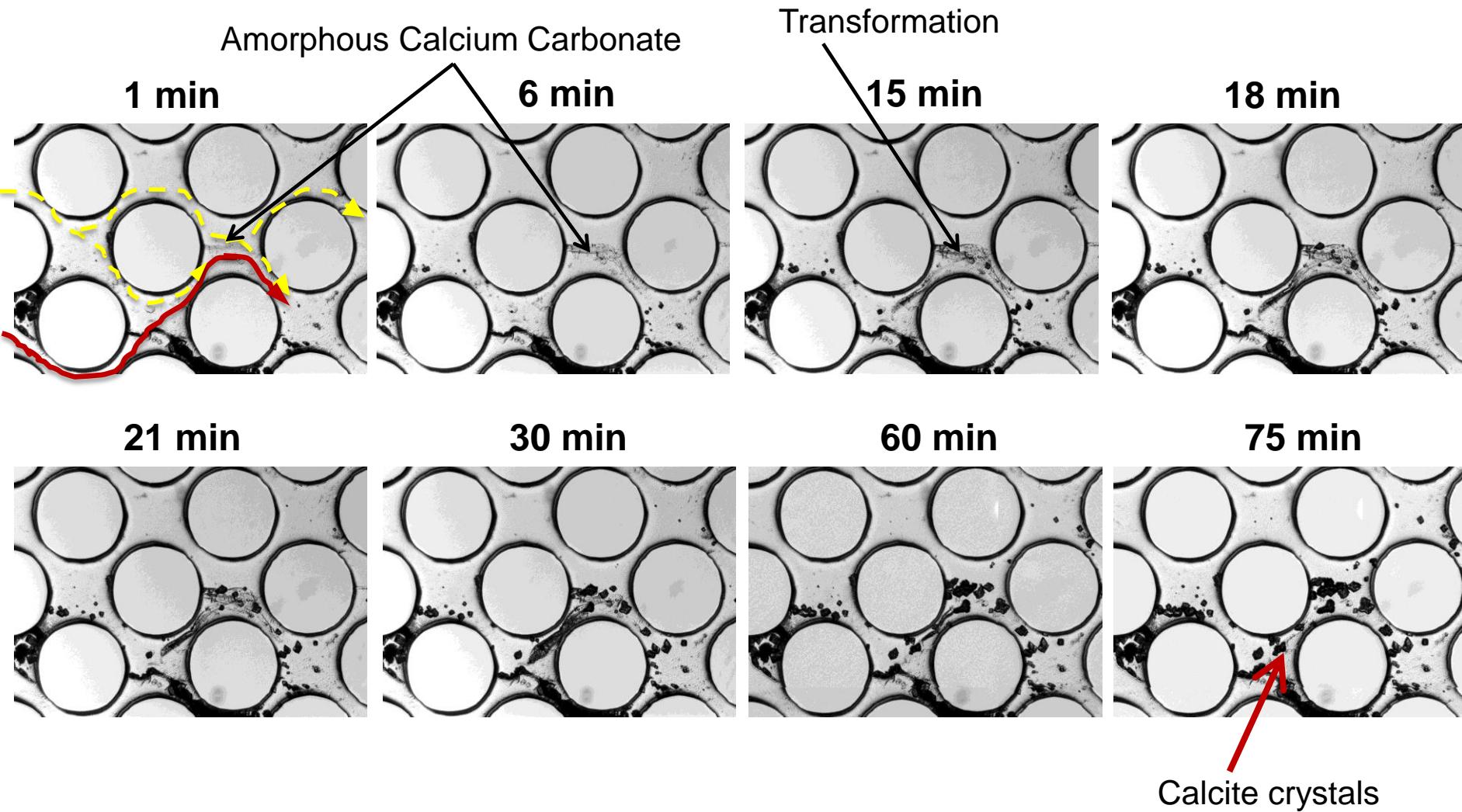
Predominantly Vaterite

- Increase in surface area over time
- Transformation to different forms of  $\text{CaCO}_3$
- Stability of nano-particles after pore blocking (or reduced mixing along the centerline)
- Effect of nano-crystal size on solubility  
(Emmanuel and Ague, Chem. Geo. 2011)



# Rapid precipitation and transformation

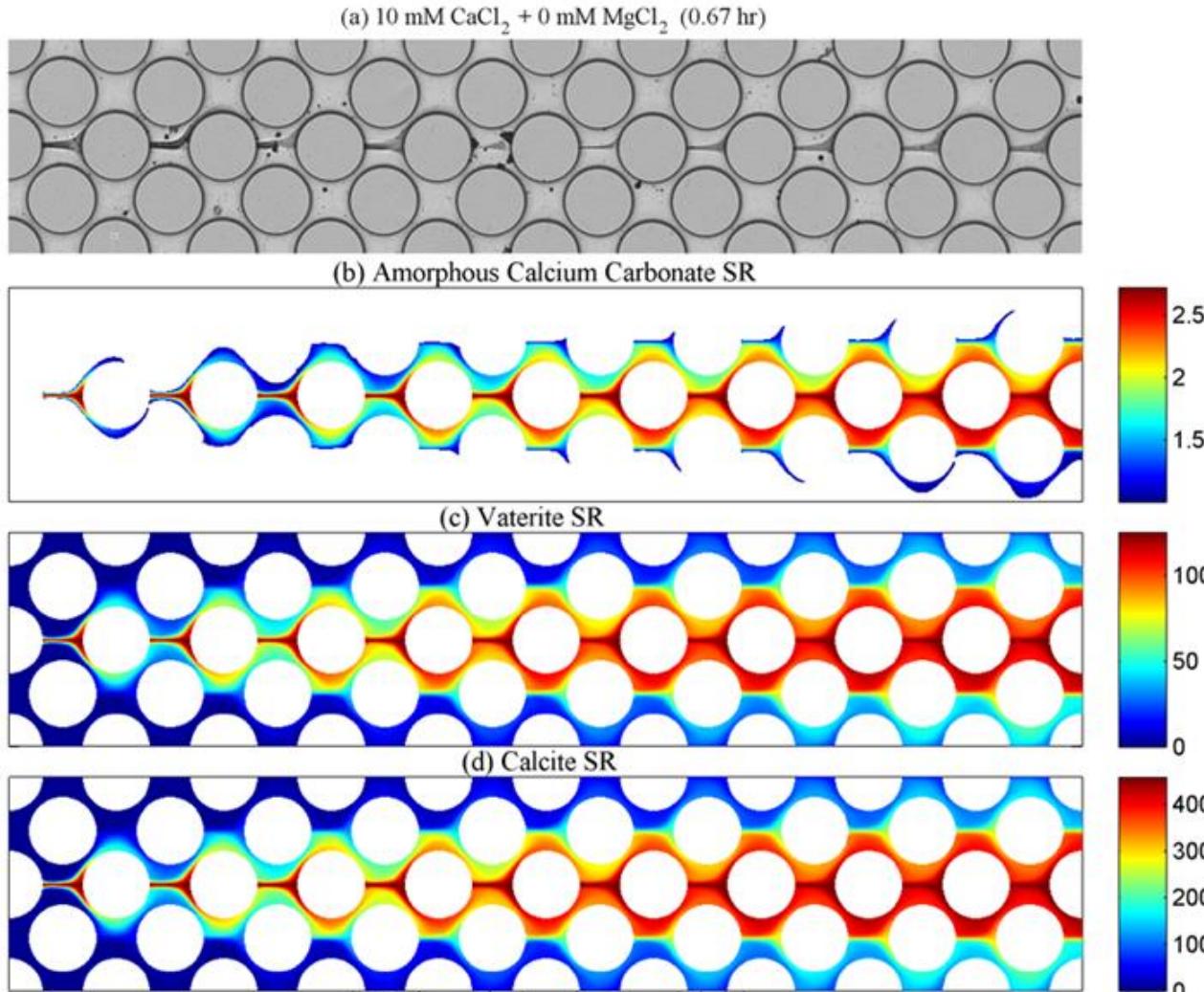
## 6.5 mM Case



# Calcium Carbonate: Polymorph

Saturation Ratio (SR) = Ion Activity product / K<sub>sp</sub>  
SR>1: thermodynamically favorable to form

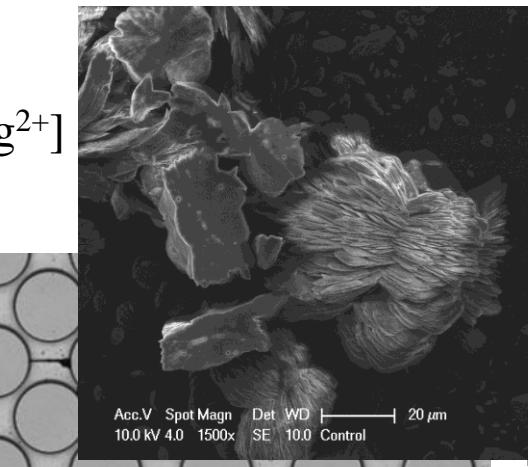
$$\begin{aligned} [\text{Ca}^{2+}]_T &= \\ [\text{CO}_3^{2-}]_T & \\ = 10 \text{ mM} & \end{aligned}$$



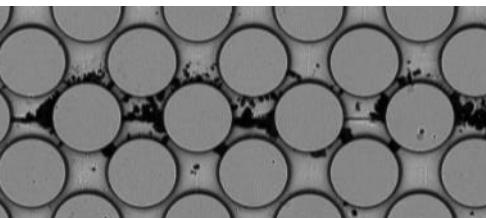
# Adding Magnesium

Adding  $[Mg^{2+}]$

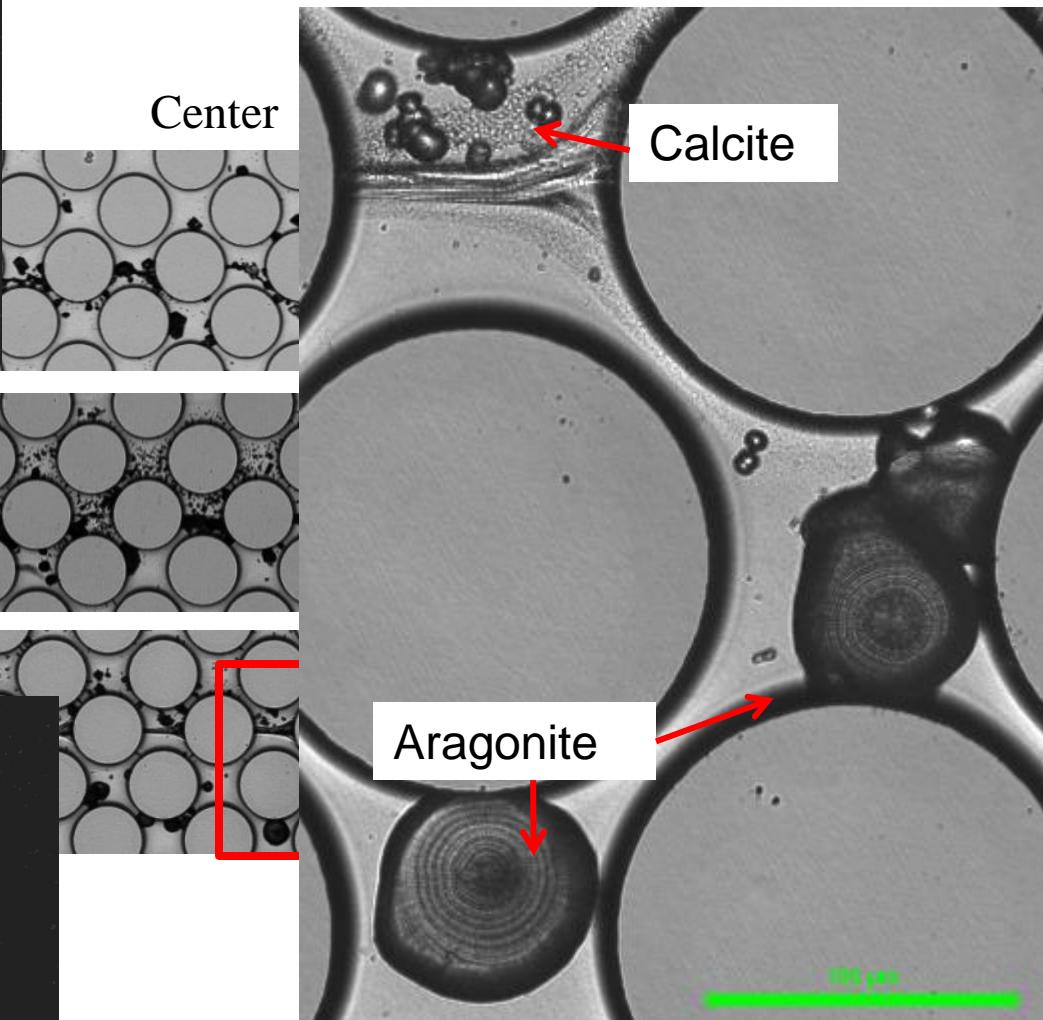
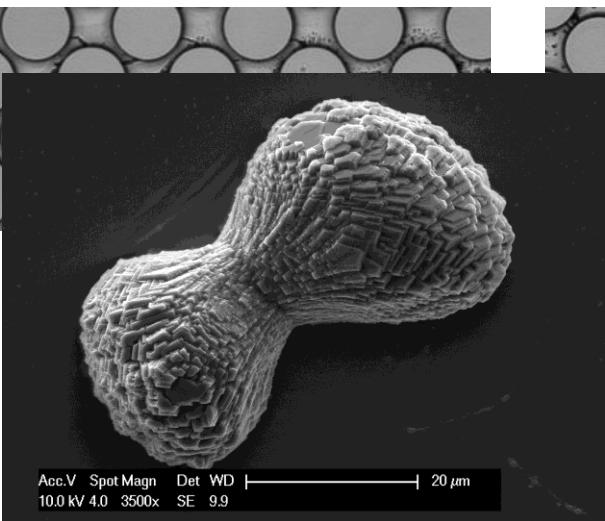
$[Mg^{2+}]$   
=0mM



$[Mg^{2+}]$   
=10mM



$[Mg^{2+}]$   
=40mM



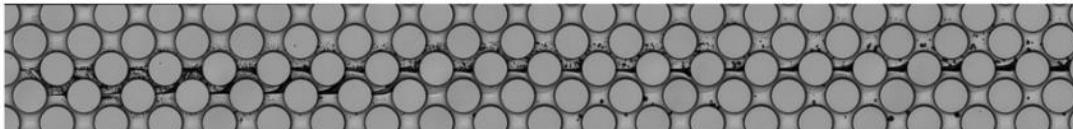
Aragonite

20 μm

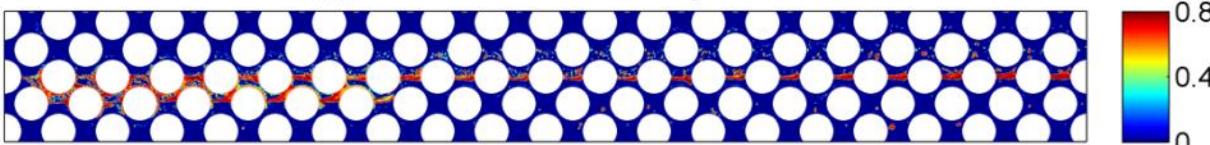
# Impact of precipitation on flow pattern and reaction kinetics

$$[\text{Ca}^{2+}]_T = [\text{CO}_3^{2-}]_T = 10 \text{ mM} \text{ & } [\text{Mg}^{2+}]_T = 40 \text{ mM}$$

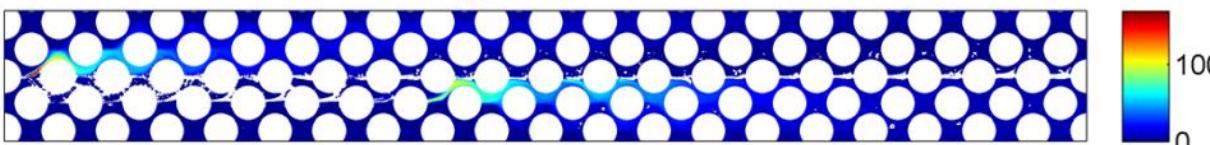
(a) Microscopy Image at 8hrs



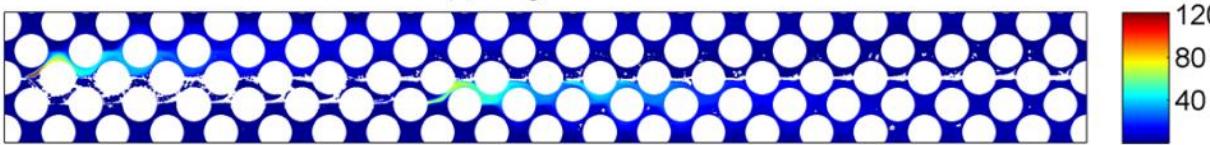
(b) Volumetric Fraction of Precipitate



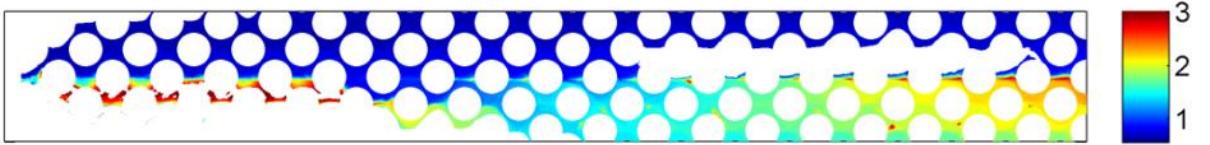
(c) Calcite SR



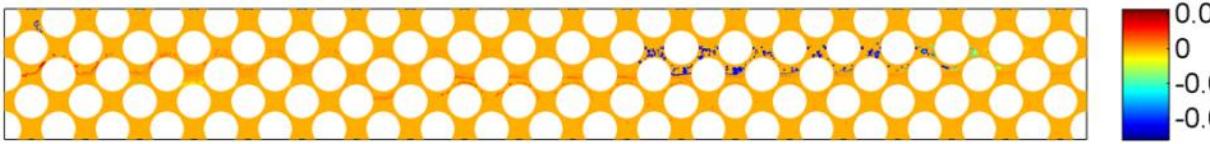
(d) Aragonite SR



(e)  $\log_{10}\{\text{Mg}^{2+}\}/\{\text{Ca}^{2+}\}$  Ratio

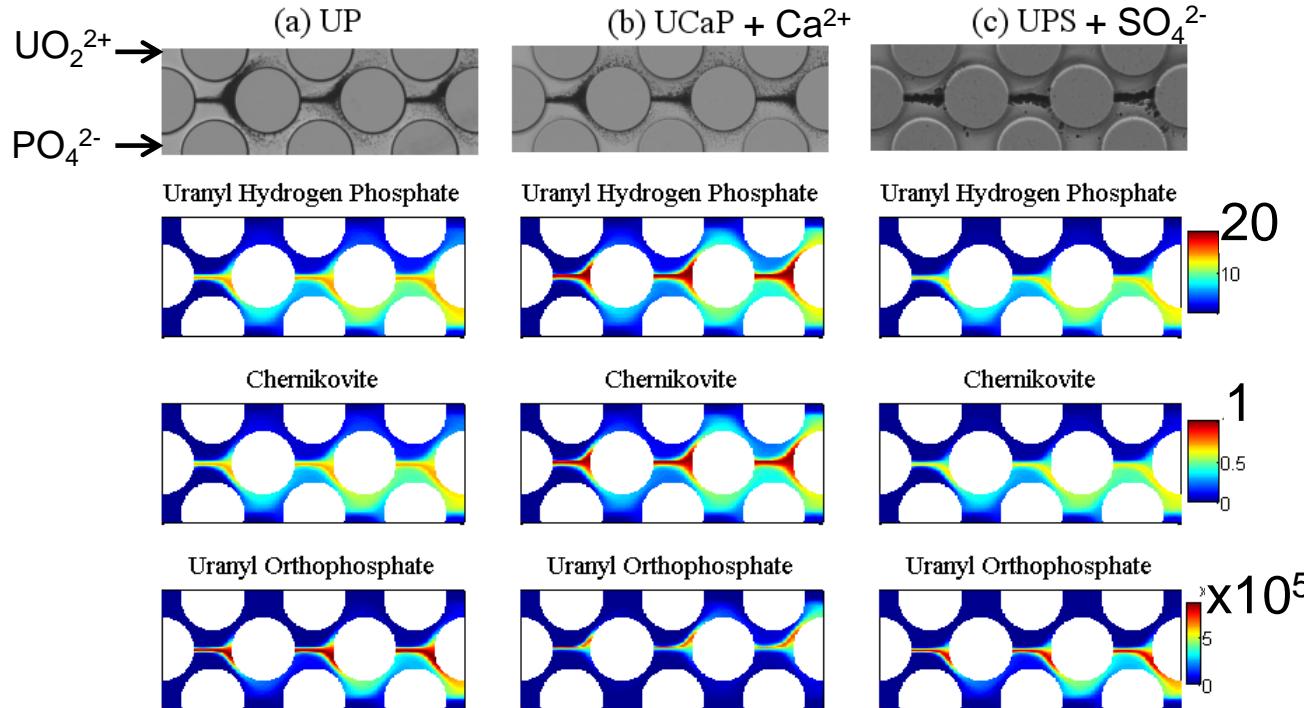


(f) Volumetric Reaction Rate (1/min)



# Impact of Solution Chemistry

Saturation Ratio (SR) = Ion Activity product / K<sub>sp</sub>  
SR>1: thermodynamically favorable to form



Due to a kinetically controlled reaction,  
only uranyl hydrogen phosphate (or chernikovite) is formed

# Summary and Implications

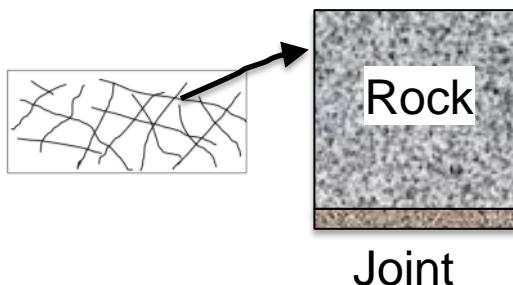
- Mineral precipitation rate along flow direction is concentration dependent and limited by transverse mixing
- $\text{CaCO}_3$  mineral phases are concentration dependent
- Overall, reaction kinetics, crystal growth and morphology are spatially and temporally affected by solution chemistry and hydrodynamics at pore scale
- Pore-scale model can be used to test if pore-scale processes observed in micromodels is predicted, and to develop an upscaled reaction model

# Upscaling and Ongoing effort

# Upscaling/Hybrid modeling

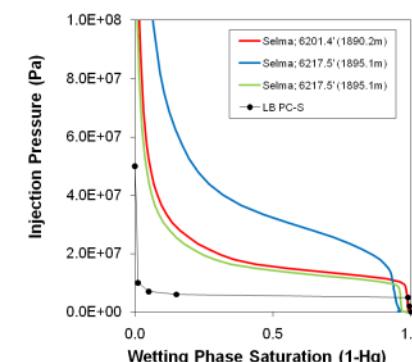
No general method/ framework for upscaling:

- Homogenization (multiple scale expansions)
- Volume averaging
- Pore network models (approx. physics)
- Mass balance principles based on pore scale models.
- Constitutive equation with closure based on detailed pore scale solutions (e.g., response function model )
- Hybrid pore-continuum approach



Geomodel (Kayanta):

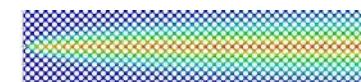
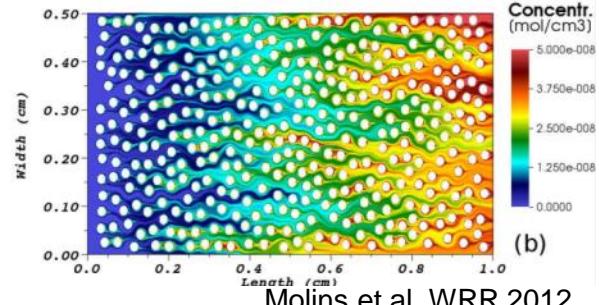
Equivalent continuum joint model



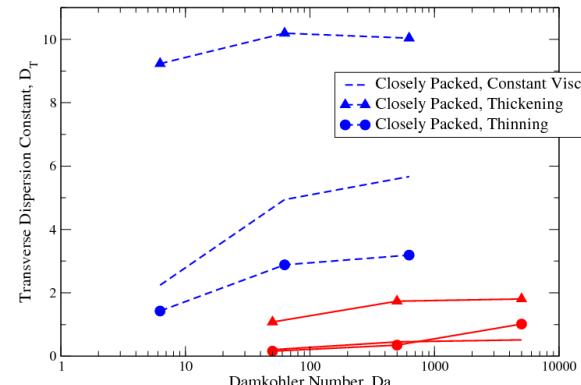
Pc-Sw Curve

Upscaled reaction rate

$$\dot{r}_{eff} = \frac{(\bar{C}_{in} - \bar{C}_{out})Q}{\nu A} \quad \bar{C}Q = \int \mathbf{u}c \bullet \mathbf{n} dS$$



$$D_{T,R} = \frac{1}{X^3} \frac{9\pi\nu}{16C_0^2\varphi^2} \left[ \int_0^X m(x) dx \right]^2$$

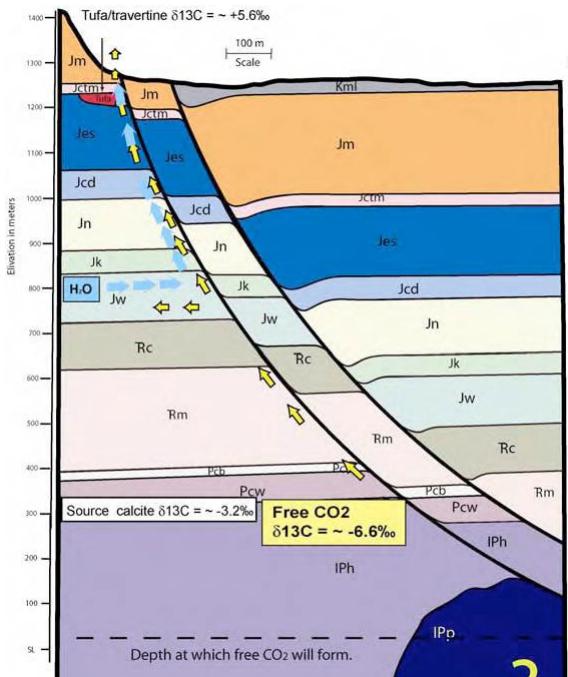


Upscaled dispersion

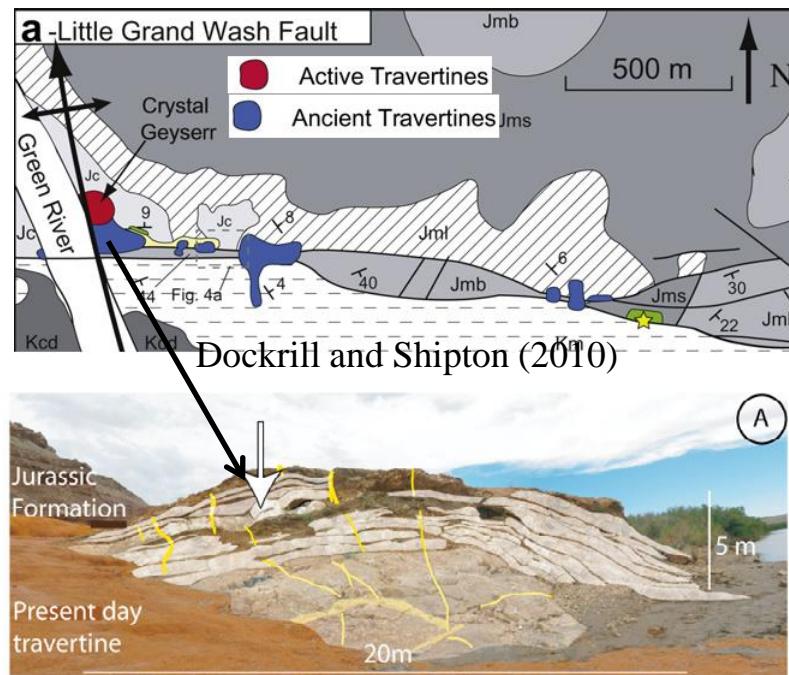
Davison, Yoon et al. (2012)

# Simulation of Little Grand Wash Fault

- Two hypotheses for CO<sub>2</sub> migration in the Crystal Geyser area:
  - CO<sub>2</sub> gas release from mantle along the fault
  - CO<sub>2</sub> dissolved in groundwater leaking up along the fault
- Develop scheme for selecting appropriate model for CO<sub>2</sub> leakage based on surface observation of travertine mounds



Evans et al. (2004)

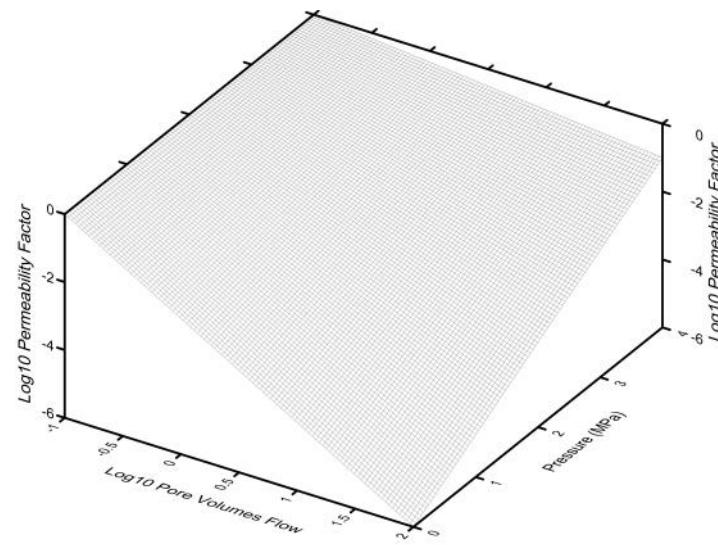


Burnside (2010)

# Crystal Geyser Site: Grand Wash

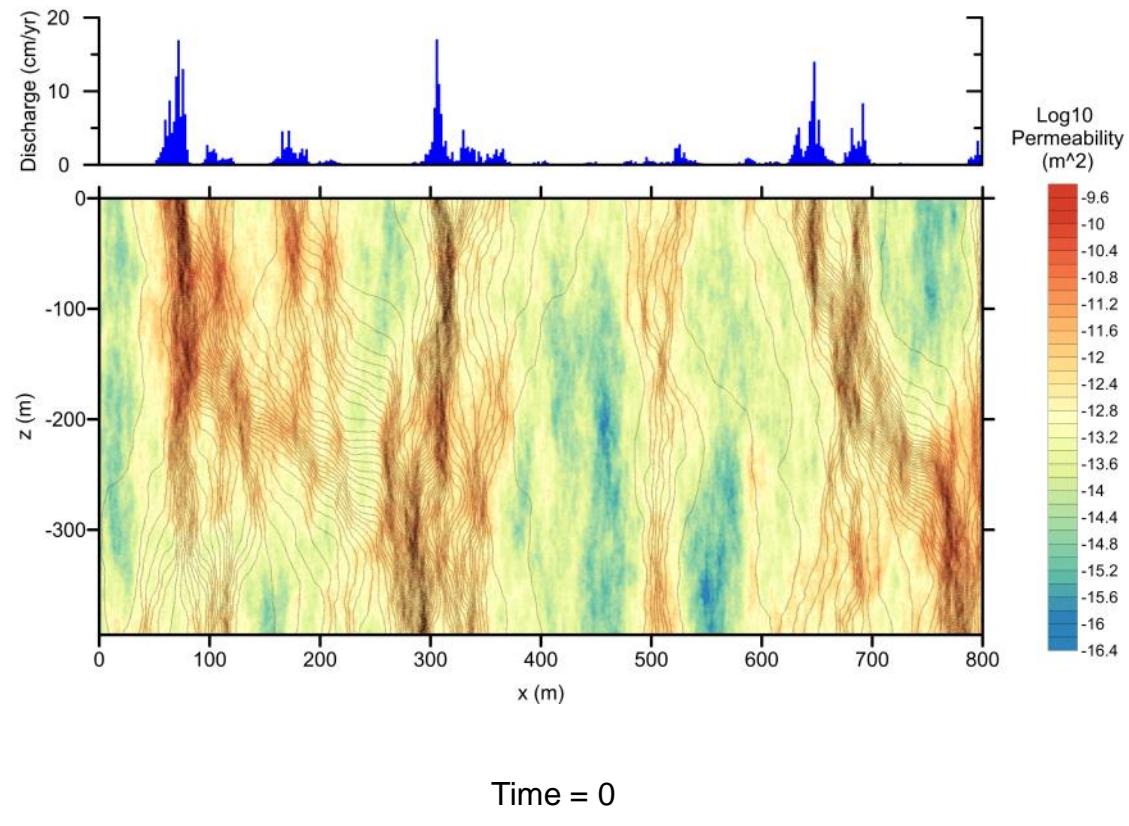
## Fault Modeling

- Simplified, two-dimensional response surface defined for preliminary modeling example
- Permeability reduction due to calcite precipitation is a function of cumulative pore volume throughput of groundwater and as a function of fluid pressure
- Fluid pressure is taken as a gross proxy for chemical conditions in which higher calcite solubility is associated with higher fluid pressure (greater depth)



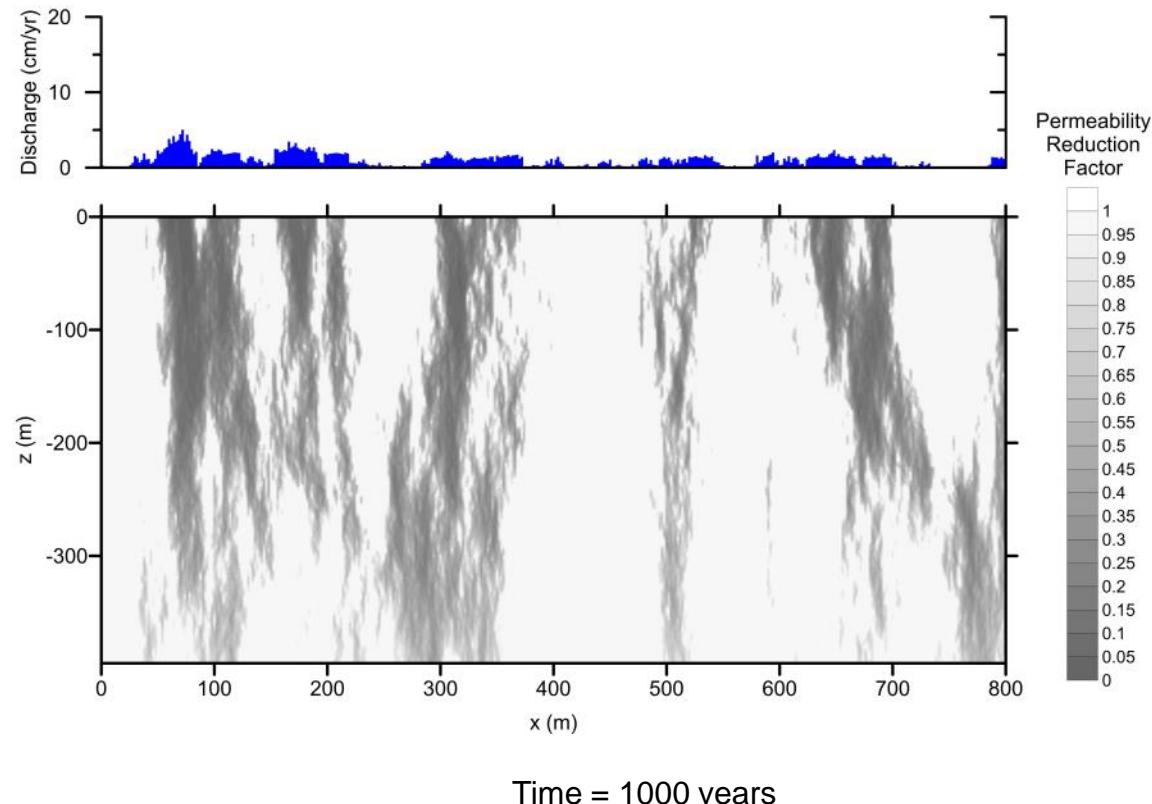
# Crystal Geyser Site: Grand Wash Fault Modeling

- Unconditional geostatistical simulation of initial permeability is semi-quantitatively consistent with geologic mapping of fault segments and alteration
- Initial simulated steady-state flow pattern is qualitatively similar to the spacing of springs and seeps along the Grand Wash fault with spacings of 100's of m between locations of groundwater discharge



# Crystal Geyser Site: Grand Wash Fault Modeling

- **Transient flow simulation includes explicit updating of the permeability field at each time step using the response surface shown previously**
- **Permeability is reduced by several orders of magnitude by calcite precipitation, primarily in the shallower high-flow channels**
- **Evolution of the flow field results in more dispersed groundwater discharge at the surface**



# Response Function based on Pore Scale Simulations

Influx conditions

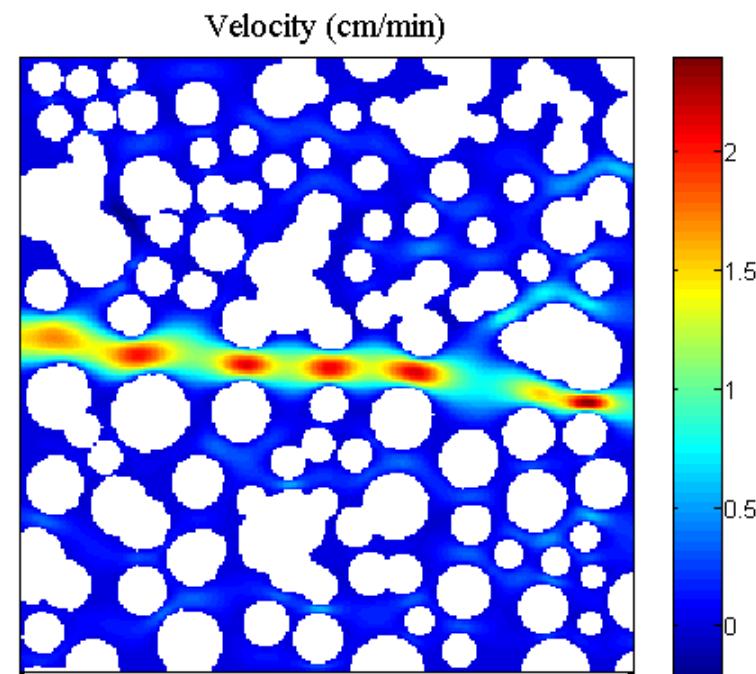
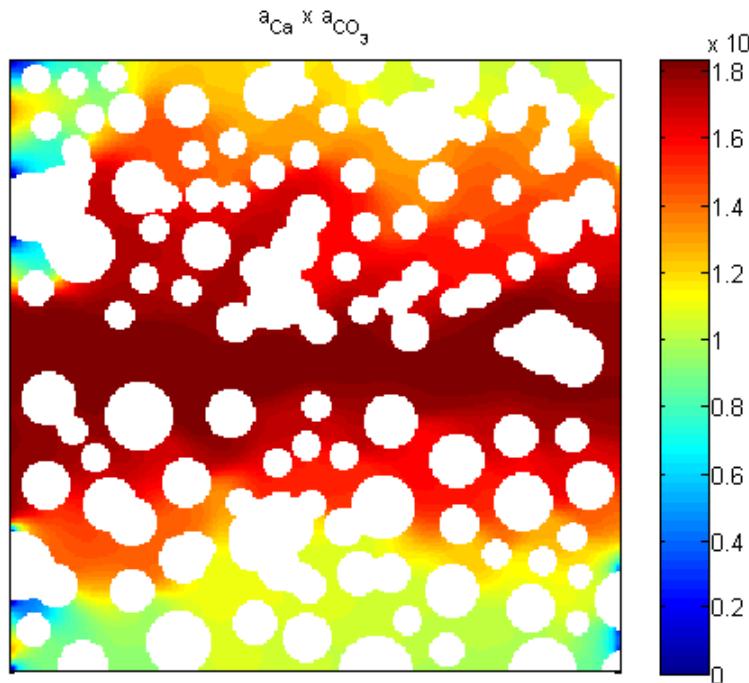
$[\text{Ca}^{2+}]_T = [\text{CO}_3^{2-}]_T = 20 \text{ mM}$

$\text{Pe} = 0.08, 0.8, 8$

$\text{Da} = 0.002, 0.02, 0.1$

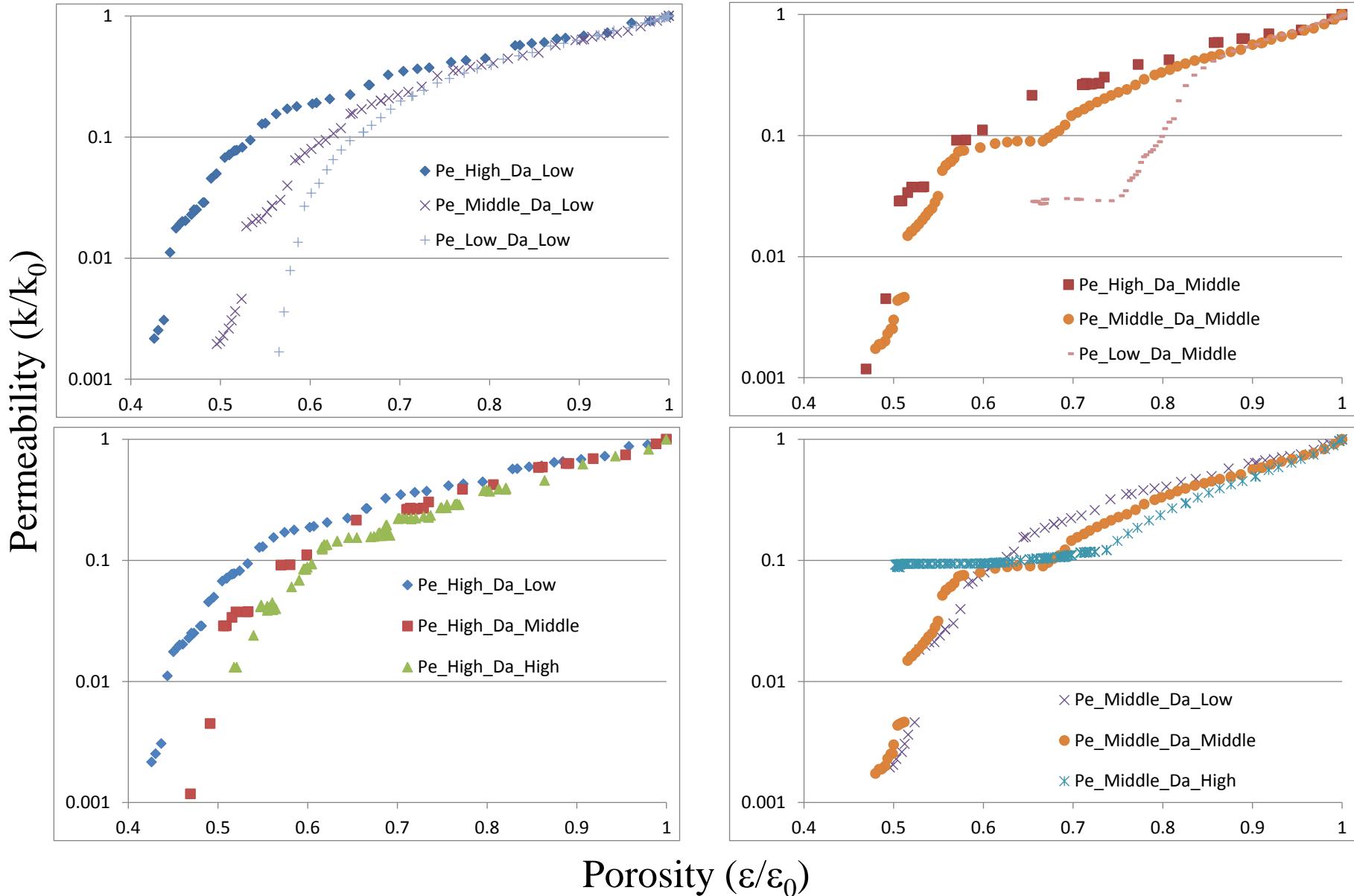
Speciation:  $\text{Ca}^{2+}, \text{H}^+, \text{CO}_3^{2-}, \text{HCO}_3^-$ ,  $\text{H}_2\text{CO}_3$

No speciation:  $\text{Ca}^{2+}, \text{CO}_3^{2-}$

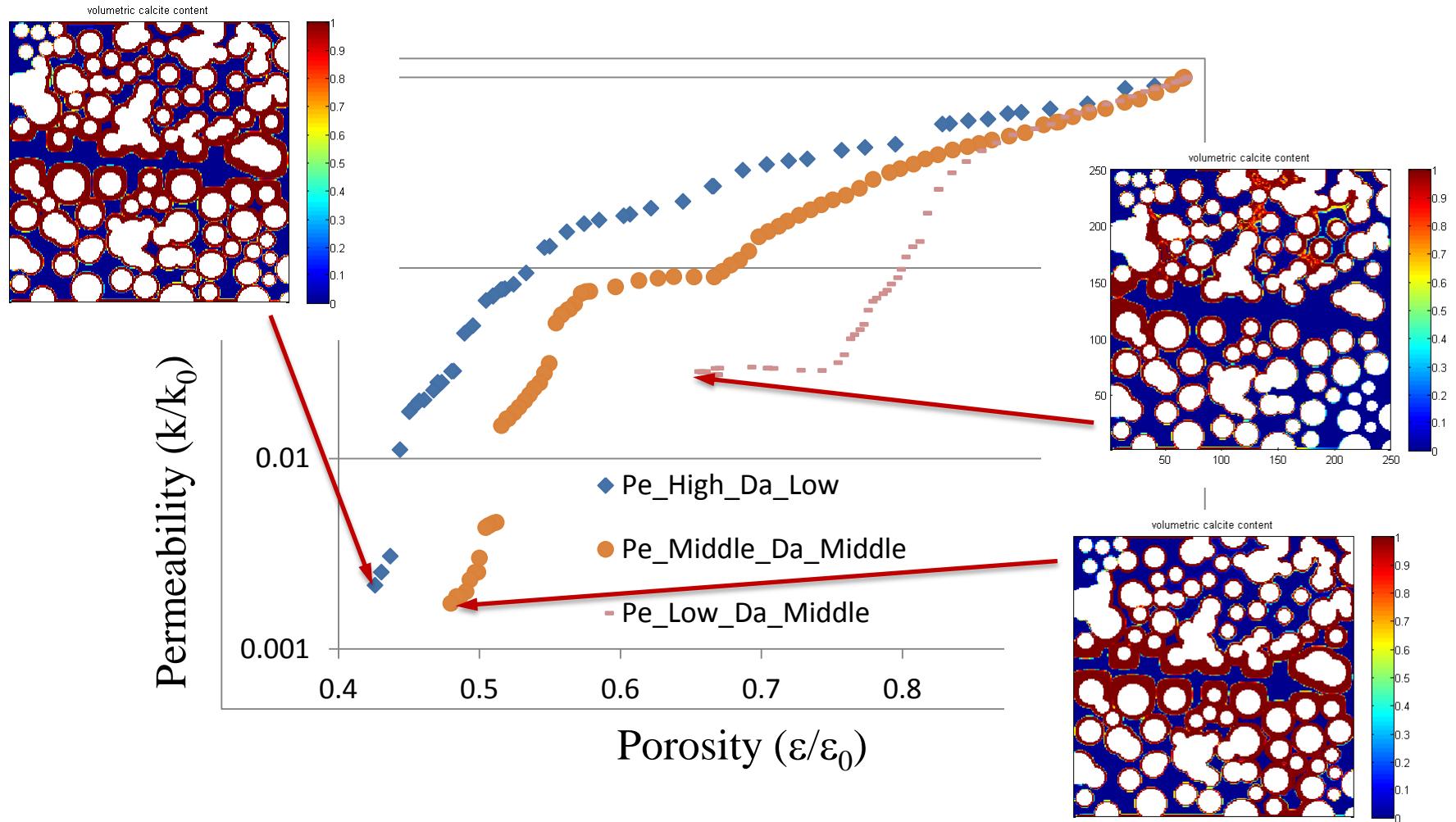


$$K_{\text{sp, calcite}} = 3.3 \times 10^{-9} \text{ M}^2$$

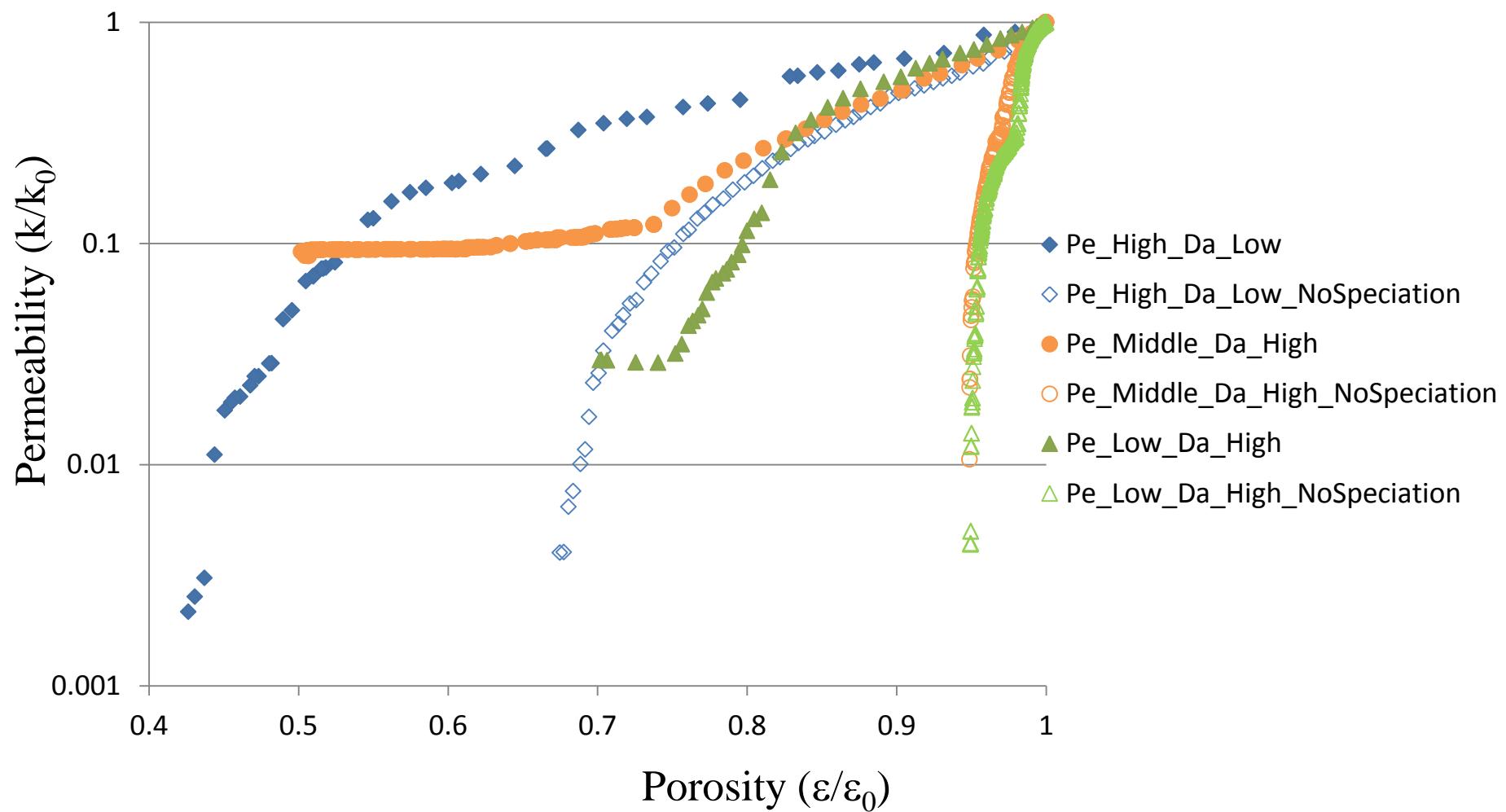
# Response Function based on Pore Scale Simulations



# Permeability-Porosity Relationships

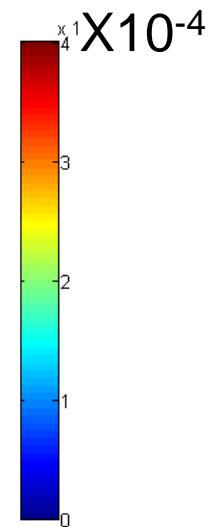
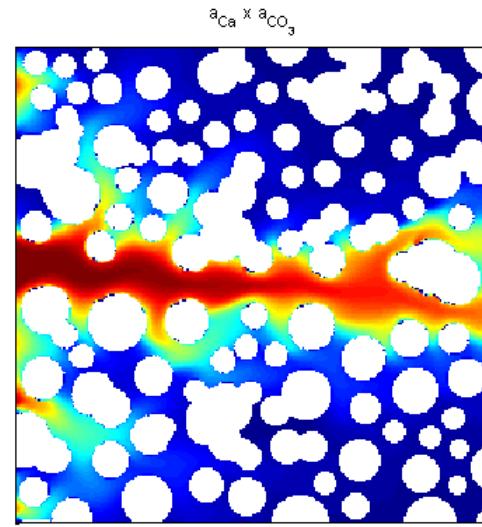
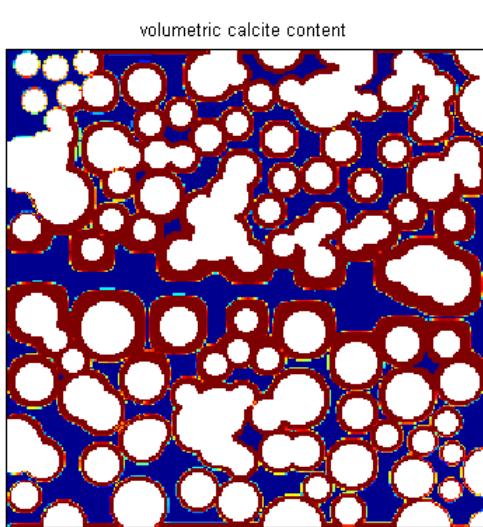


# Chemical Speciation

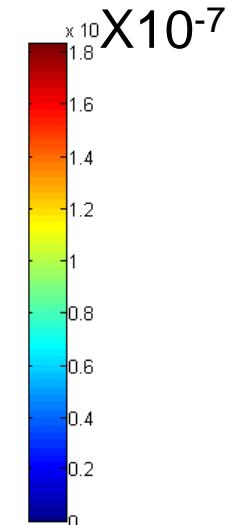
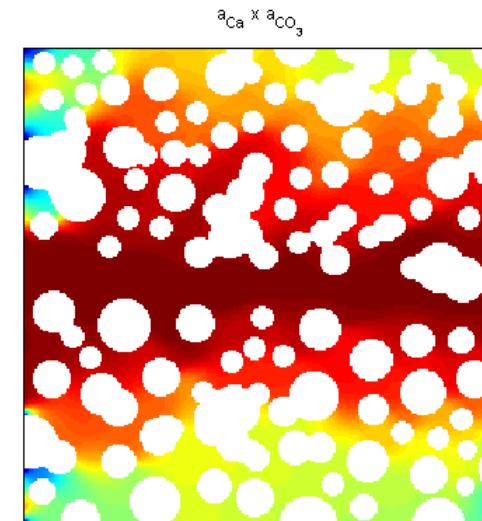
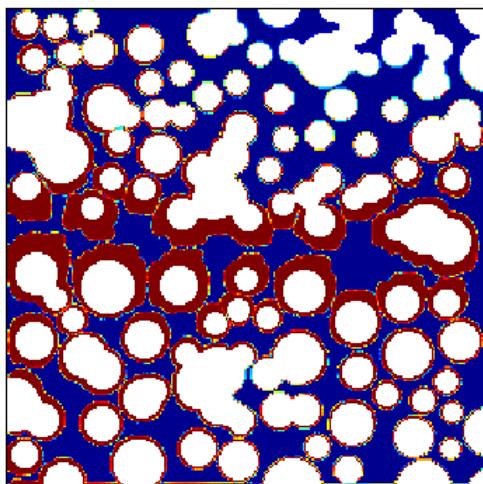


# High Pe & Low Da

Speciation

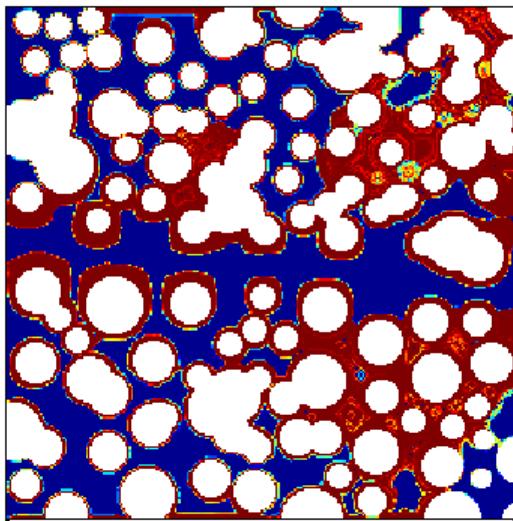


No speciation

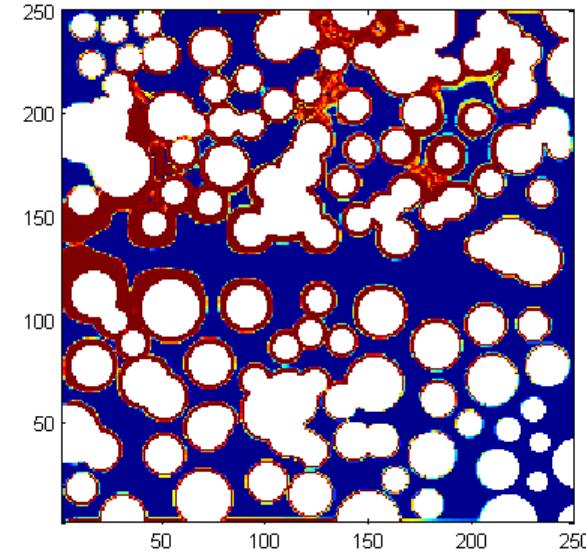


# Comparison

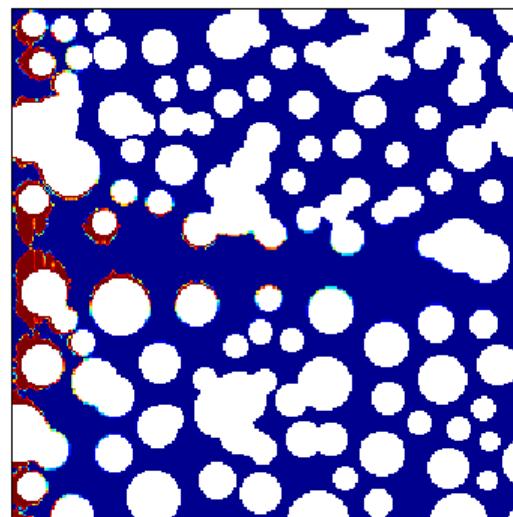
$Pe=0.8; Da=0.1$



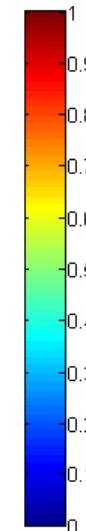
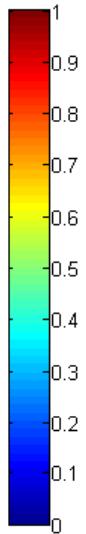
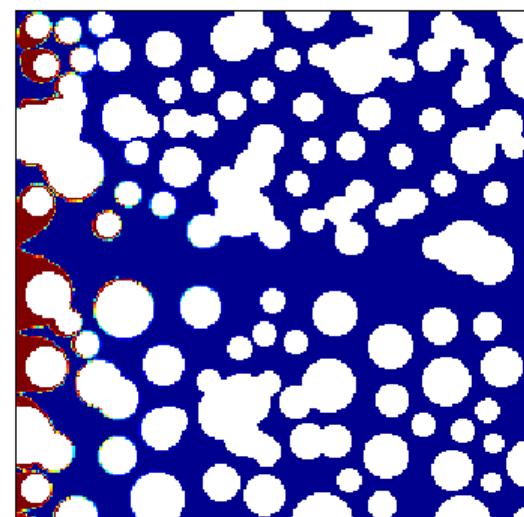
$Pe=0.08; Da=0.02$



Speciation



No speciation



# Summary and Implications

- Vigorously tested pore-scale model can be used to develop a response function (or dimension reduced model) for permeability and porosity ( $k$ - $\varepsilon$ ) relationships
- $k$ - $\varepsilon$  relationships will be affected by solution chemistry, chemical reaction, pore structure configurations in addition to Pe and Da numbers
- Adaptive strategy to couple continuum and pore-scale using a response function approach will be tested

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