

Natural Frequencies and Mode Shapes of a Coupled Cantilever Array

Hartono Sumali, Matthew A. Spletzer
Sandia National Laboratories
July 2013

Introduction

This is a study material to discuss during the 2013 Summer School at the Instituto de Investigaciones en Matemáticas Aplicadas y en Sistemas, Universidad Nacional Autónoma de México (UNAM), Mexico City.

Single Cantilever

From Euler-Bernoulli theory (EB), the natural frequency of a prismatic cantilever beam is

$$\omega_m = u_m^2 \sqrt{\frac{EI / L^3}{\rho AL}} \quad (1)$$

For a cantilever beam with no tip mass, EB gives $u_1^2 = 1.8751^2 = 3.5160$ [Blevins, 1981]. For realizing the natural frequency with a lumped spring-mass system, assume a spring constant k equal to the static stiffness of the cantilever at the tip, compute the effective lumped mass according to

$$\omega_m^2 = \frac{k}{m} = \frac{3EI / L^3}{m} = u_m^4 \frac{EI / L^3}{\rho AL} \quad (2)$$

Therefore, the effective mass is

$$m = \frac{3}{u_m^4} \rho AL \quad (3)$$

Cantilever Array Model

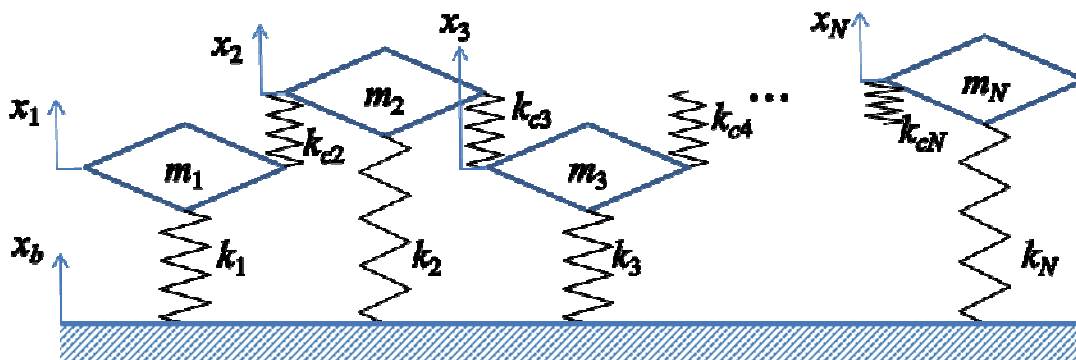


Figure 1: Lumped model of cantilever array

The bases of the cantilevers are excited by a common base displacement x_b . The stiffness of each cantilever i is k_i . The deflection of cantilever i pulls cantilevers $i-1$ and $i+1$ through a coupling stiffness k_{ci} and k_{ci+1} . Therefore, the model assumes equations of motion

$$\begin{aligned}
 m_1 \ddot{x}_1 &= k_1(x_b - x_1) + k_{c2}(x_2 - x_1) \\
 m_2 \ddot{x}_2 &= k_{c2}(x_1 - x_2) + k_2(x_b - x_2) + k_{c3}(x_3 - x_2) \\
 &\quad \dots \\
 m_i \ddot{x}_i &= k_{ci}(x_{i-1} - x_i) + k_i(x_b - x_i) + k_{ci+1}(x_{i+1} - x_i) \\
 &\quad \dots \\
 m_N \ddot{x}_N &= k_{cN}(x_{N-1} - x_N) + k_N(x_b - x_N).
 \end{aligned} \tag{4}$$

If all the cantilevers are identical, $k_i = k$, and so are the coupling between all two adjacent cantilevers, $k_{ci} = k_c$, then the equations of motion can be written as

$$\mathbf{M}\ddot{\mathbf{x}} + \mathbf{K}\mathbf{x} = \mathbf{K}_b x_b \tag{5}$$

where [Spletzer et al, 2008]

$$\begin{aligned}
 \mathbf{M} &= \text{diag}(m_1, m_2, \dots, m_N) \\
 \mathbf{x} &= (x_1, x_2, \dots, x_N)^T \\
 \mathbf{K}_b &= \text{diag}(k_1, k_2, \dots, k_N)
 \end{aligned} \tag{6}$$

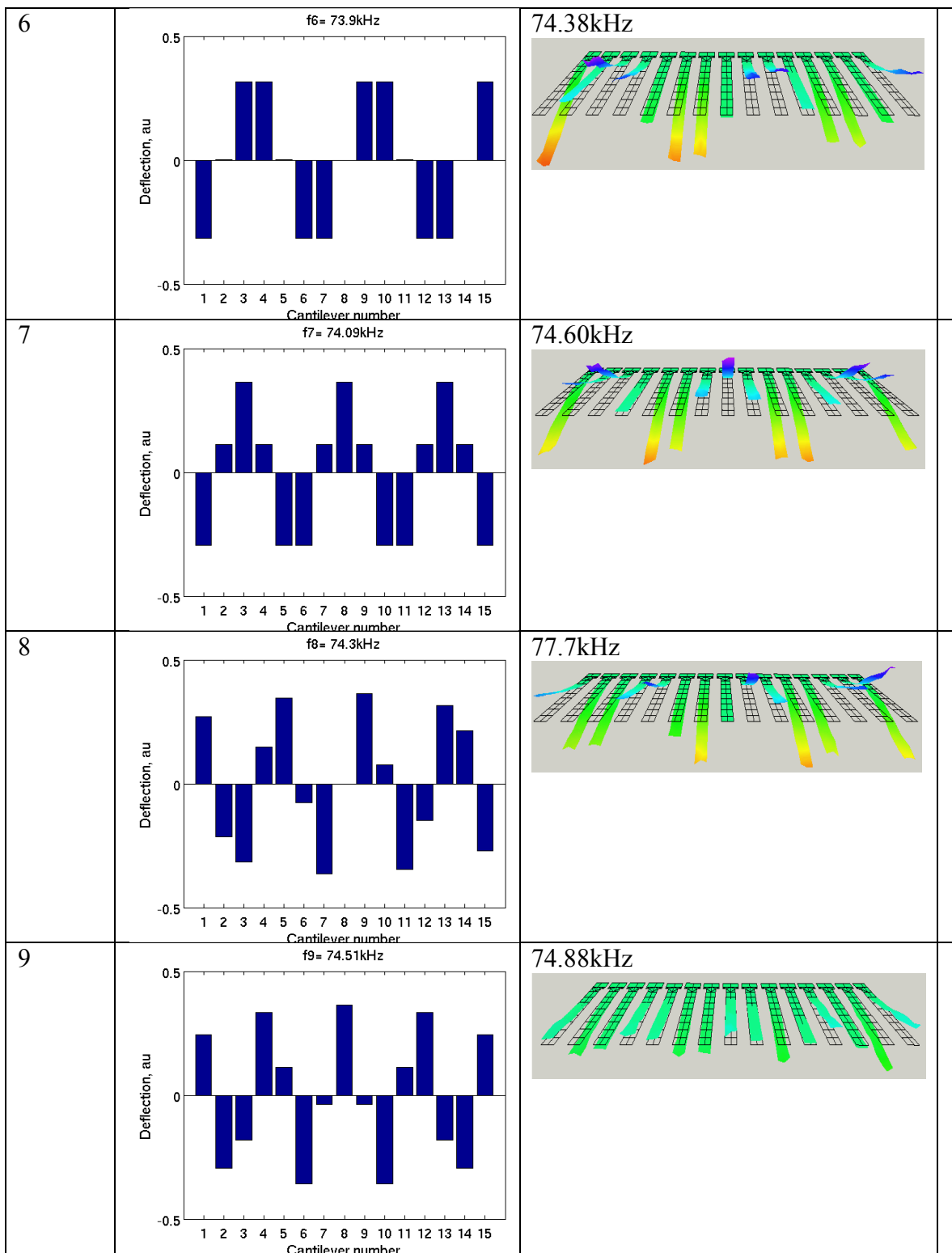
and

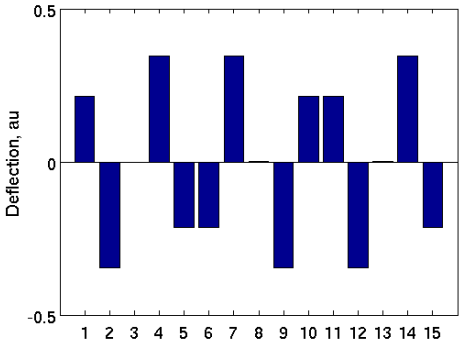
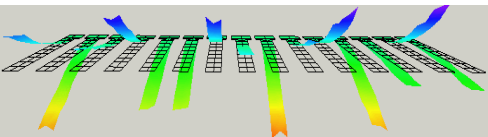
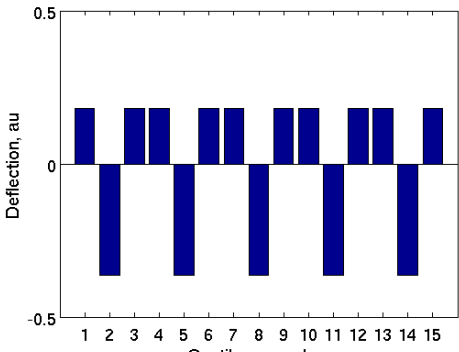
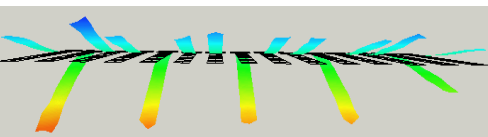
$$\mathbf{K} = \begin{bmatrix} k_1 + k_{c2} & -k_{c2} & \dots & 0 \\ -k_{c2} & k_2 + k_{c2} + k_{c3} & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & -k_{cN-1} & k_N + k_{cN} \end{bmatrix} \tag{7}$$

The natural frequency and mode shapes can be obtained by solving the eigenvalue problem of Eq. (5).

Mode Shapes

Mode number	Predicted	Measured
2	$f_2 = 73.41\text{kHz}$ Deflection, au Cantilever number	68.09kHz
3	$f_3 = 73.47\text{kHz}$ Deflection, au Cantilever number	71.80kHz
4	$f_4 = 73.58\text{kHz}$ Deflection, au Cantilever number	73.30kHz
5	$f_5 = 73.72\text{kHz}$ Deflection, au Cantilever number	73.99kHz



10	f10 = 74.72kHz  <table><caption>Approximate Deflection Data for f10 = 74.72kHz</caption><thead><tr><th>Cantilever number</th><th>Deflection, au</th></tr></thead><tbody><tr><td>1</td><td>0.25</td></tr><tr><td>2</td><td>-0.35</td></tr><tr><td>3</td><td>0.00</td></tr><tr><td>4</td><td>0.35</td></tr><tr><td>5</td><td>-0.25</td></tr><tr><td>6</td><td>-0.25</td></tr><tr><td>7</td><td>0.35</td></tr><tr><td>8</td><td>0.00</td></tr><tr><td>9</td><td>-0.35</td></tr><tr><td>10</td><td>0.25</td></tr><tr><td>11</td><td>0.25</td></tr><tr><td>12</td><td>-0.35</td></tr><tr><td>13</td><td>0.00</td></tr><tr><td>14</td><td>0.35</td></tr><tr><td>15</td><td>-0.25</td></tr></tbody></table>	Cantilever number	Deflection, au	1	0.25	2	-0.35	3	0.00	4	0.35	5	-0.25	6	-0.25	7	0.35	8	0.00	9	-0.35	10	0.25	11	0.25	12	-0.35	13	0.00	14	0.35	15	-0.25	74.97kHz 
Cantilever number	Deflection, au																																	
1	0.25																																	
2	-0.35																																	
3	0.00																																	
4	0.35																																	
5	-0.25																																	
6	-0.25																																	
7	0.35																																	
8	0.00																																	
9	-0.35																																	
10	0.25																																	
11	0.25																																	
12	-0.35																																	
13	0.00																																	
14	0.35																																	
15	-0.25																																	
11	f11 = 74.91kHz  <table><caption>Approximate Deflection Data for f11 = 74.91kHz</caption><thead><tr><th>Cantilever number</th><th>Deflection, au</th></tr></thead><tbody><tr><td>1</td><td>0.25</td></tr><tr><td>2</td><td>-0.35</td></tr><tr><td>3</td><td>0.25</td></tr><tr><td>4</td><td>0.25</td></tr><tr><td>5</td><td>-0.35</td></tr><tr><td>6</td><td>0.25</td></tr><tr><td>7</td><td>0.25</td></tr><tr><td>8</td><td>-0.35</td></tr><tr><td>9</td><td>0.25</td></tr><tr><td>10</td><td>0.25</td></tr><tr><td>11</td><td>-0.35</td></tr><tr><td>12</td><td>0.25</td></tr><tr><td>13</td><td>0.25</td></tr><tr><td>14</td><td>-0.35</td></tr><tr><td>15</td><td>0.25</td></tr></tbody></table>	Cantilever number	Deflection, au	1	0.25	2	-0.35	3	0.25	4	0.25	5	-0.35	6	0.25	7	0.25	8	-0.35	9	0.25	10	0.25	11	-0.35	12	0.25	13	0.25	14	-0.35	15	0.25	75.02kHz 
Cantilever number	Deflection, au																																	
1	0.25																																	
2	-0.35																																	
3	0.25																																	
4	0.25																																	
5	-0.35																																	
6	0.25																																	
7	0.25																																	
8	-0.35																																	
9	0.25																																	
10	0.25																																	
11	-0.35																																	
12	0.25																																	
13	0.25																																	
14	-0.35																																	
15	0.25																																	