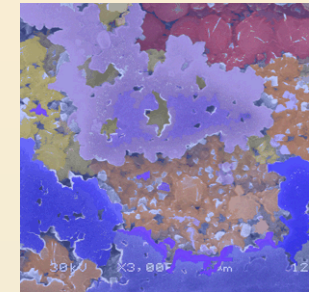
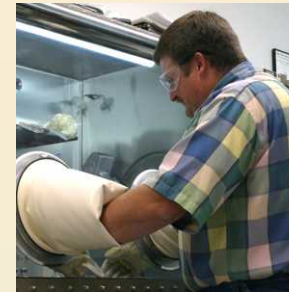
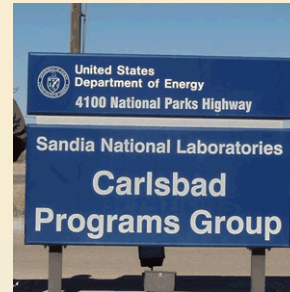
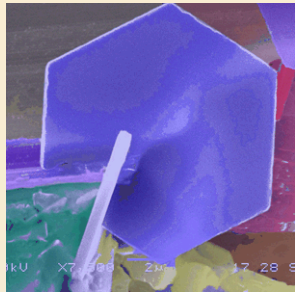


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# Anoxic Corrosion of Steel and Lead in Na-Cl $\pm$ Mg Dominated Brines and Effects on PA

*DOE/EPA Technical Exchange; November 14-15, 2012; Carlsbad, NM*

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# Purpose and Scope

- Determine Fe Corrosion Rates for use in PA H<sub>2</sub> Gas Generation Model
- Determine what corrosion products are likely to form
  - Kinetics of Fe and Pb corrosion
  - Potential for passivation of metal surfaces
- Determine the extent to which Fe and Pb consume CO<sub>2</sub>
  - Potential for Fe and Pb to support MgO as engineered barrier
- Work conducted under:
  - TP 06-02 *Iron and Lead Corrosion in WIPP-Relevant Conditions*
  - AP-159 *Determination of Gas Generation Rates from Iron/Lead Corrosion Experiments*

# Experimental Setup

- WIPP-relevant environmental conditions
  - Temperature: 26°C
  - Relative humidity: approx. 72%
  - Atmosphere:
    - N<sub>2</sub> and N<sub>2</sub> + CO<sub>2</sub> (350 ppm, 1500 ppm, or 3500 ppm)
    - Anoxic: < 5 ppm O<sub>2</sub>
  - Brine compositions:
    - ERDA-6 ± organics (NaCl-dominated brine)
    - GWB ± organics (NaCl-MgCl<sub>2</sub> dominated brine)
    - organics - EDTA, citrate, acetate, oxalate
- Materials:
  - Iron – ASTM A1008 low-carbon steel
  - Lead – QQ-L-171e Grade C chemical Pb
- Three sample positions: humid, partially submersed, fully submersed
- Four time segments (6, 12, 18 and 24 months)
- Experiments are being performed in a flow-through system designed to maintain above environmental conditions
- 864 total samples (432 steel, 432 lead)

# Sample Analysis

- Characterization of coupon surfaces
  - Before and after removal of corrosion products
  - SEM and digital photography
- Characterization of corrosion products
  - XRD
  - SEM with Energy Dispersive Spectroscopy (EDS)
- Weight loss after removal of corrosion products
- Determination of corrosion rates from weight loss data
- Determination of Updates to Corrosion Rate Parameters

# Typical Appearance of Steel Coupons

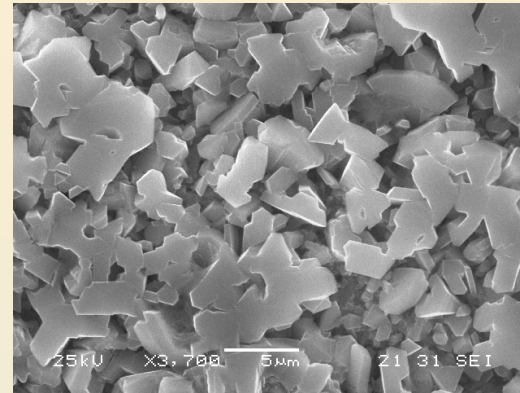
Coupon 021

24 month exposure, 0 ppm CO<sub>2</sub>, ERDA-6 no organics



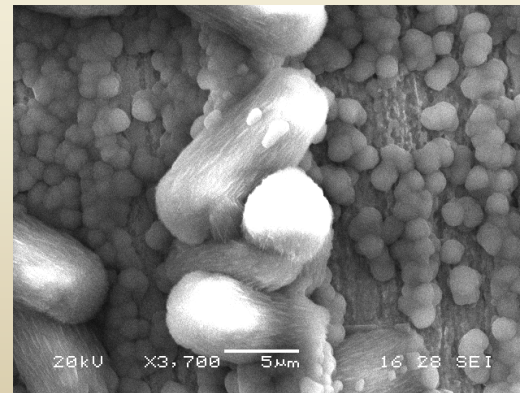
Coupon 104

6 month exposure, 0 ppm CO<sub>2</sub>, ERDA-6 no organics



Coupon 327

6 month exposure, 1500 ppm CO<sub>2</sub>, ERDA-6 w/ organics



# Possible Corrosion Products

	Steel		Lead	
Low CO <sub>2</sub> < ~1500 ppm	Amakinite Green Rust	(Fe,Mg)(OH) <sub>2</sub> Fe(III) <sub>2</sub> Fe(II) <sub>4</sub> (OH) <sub>12</sub> CO <sub>3</sub> ·2H <sub>2</sub> O	N/A	N/A
High CO <sub>2</sub> > ~1500 ppm	Siderite Ankerite	(Fe,Ca)CO <sub>3</sub> CaFe(CO <sub>3</sub> ) <sub>2</sub>	Cerussite Tarnowitzite	PbCO <sub>3</sub> (Ca,Pb)CO <sub>3</sub>

# Weight Loss Determination

- Coupon placed in cleaning solution for 2 minutes

Material	Chemical	Max. Time	Temp.
Iron (Fe)	500 mL conc. HCl 3.5 g hexamethylene tetramine Reagent water to make 1000 mL	10 min	20 to 25 °C
Lead (Pb)	250 g ammonium acetate Reagent water to make 1000 mL	5 min	60 to 70 °C

Source: ASTM G 1 – 03 *Standard Practice for Preparing, Cleaning and Evaluation Corrosion Test Specimens*. West Conshohocken, PA: American Society for Testing and Materials (ASTM) International.

- After 2 minutes, removed, scrubbed, rinsed in DI water followed by ethanol
- Coupon weighed
- Repeat process for 5 to 10 cycles

# Weight Loss Graphical Analysis

**AB – Removal of corrosion product and base metal**

**BC – Removal of base metal only**

**D – Projected final weight**

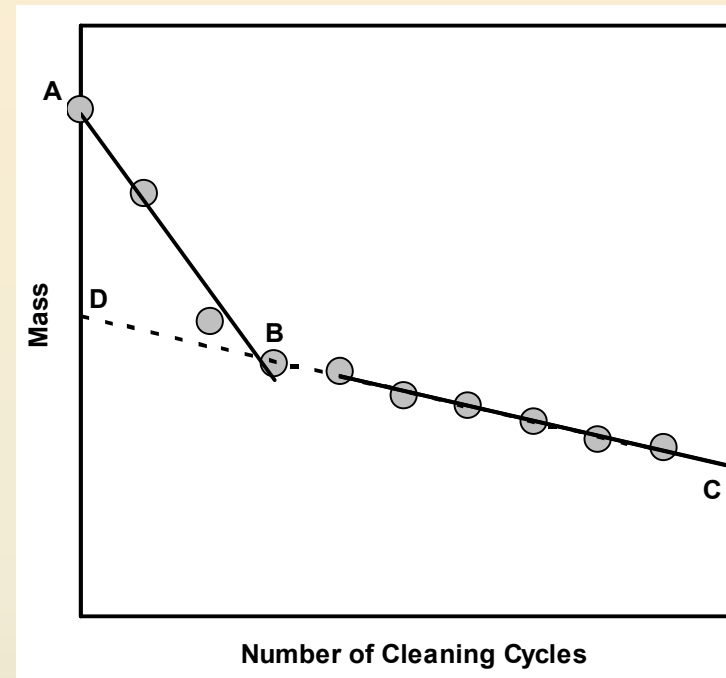
$$rate(\mu m / yr) = \frac{W \times 87.6}{SA \times t \times \rho} \times 1000$$

$W$  - mass loss (mg)

$SA$  - exposed surface area (cm<sup>2</sup>)

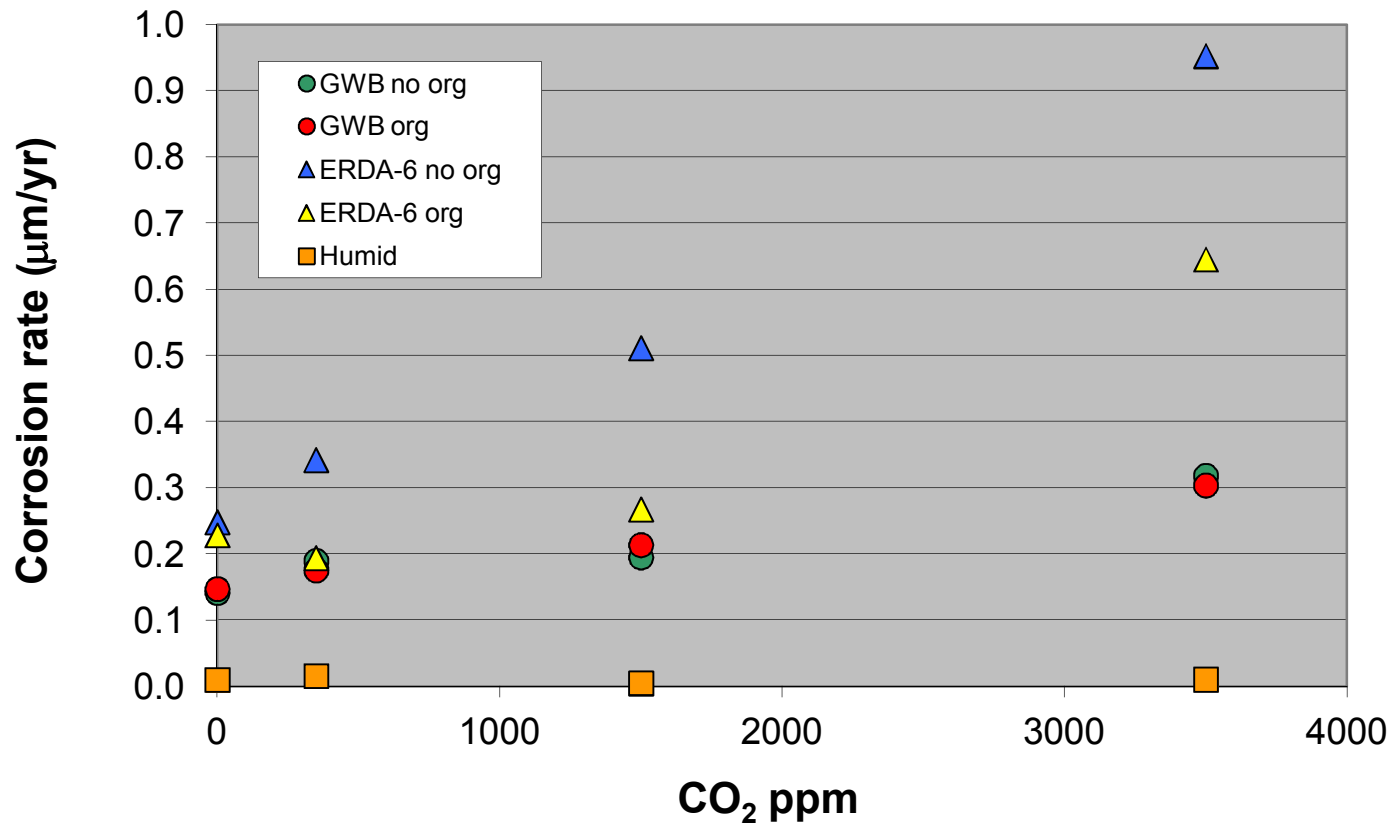
$t$  - exposure duration (hours)

$\rho$  - metal density (g/cm<sup>3</sup>)

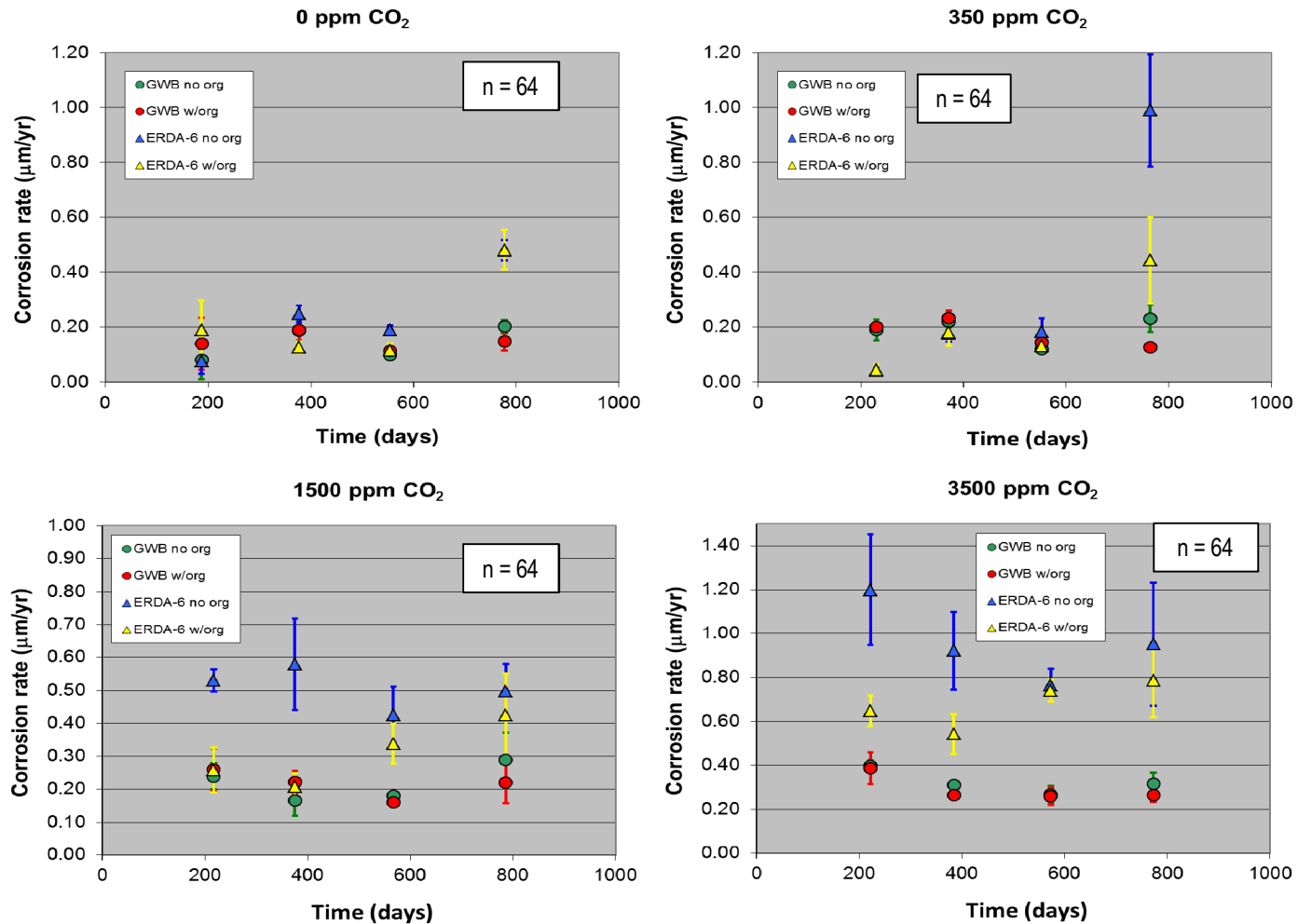




# Corrosion Rates for Fe Coupons (All results)



# Fe Corrosion Rates with Time



# Gas Generation in PA

$$q_{r gc} = \left( R_{ci} S_{b, eff} + R_{ch} S_g^* \right) D_s \rho_{Fe} X_c \left( H_2 | Fe \right) M_{H_2}$$

$q_{r gc}$  -  $H_2$  gas generation rate due to corrosion (kg/m<sup>3</sup>/s)

$D_s$  - surface area concentration of steel in the repository (m<sup>2</sup> / m<sup>3</sup> )

$M_{H_2}$  - molecular weight of  $H_2$  (kg/mol)

$R_{Ci}$  - inundated corrosion rate in the absence of  $CO_2$  (m/s) [CORRMCO2]

$R_{Ch}$  - corrosion rate under humid conditions (m/s) [HUMCORR]

$S_{b, eff}$  - effective brine saturation due to capillary action in the waste materials

$X_C(H_2|Fe)$  - stoichiometric coefficient for gas generation due to corrosion of steel (mol  $H_2$ /mol Fe) [STOIFX]

$\rho_{Fe}$  - molar density of steel (mol/m<sup>3</sup>)

# Current PA Parameters

- Current PA Corrosion Parameters

Parameter	Units	Description	Distribution Type	Distribution Parameters
CORRMCO2	m/s	Rate of anoxic steel corrosion under brine-inundated conditions with no CO <sub>2</sub> present	Uniform	Min = 0 Max = 3.17e-14
HUMCORR	m/s	Rate of anoxic steel corrosion under humid conditions	Constant	0
STOIFX	none	Stoichiometric coefficient for gas generation	Constant	1

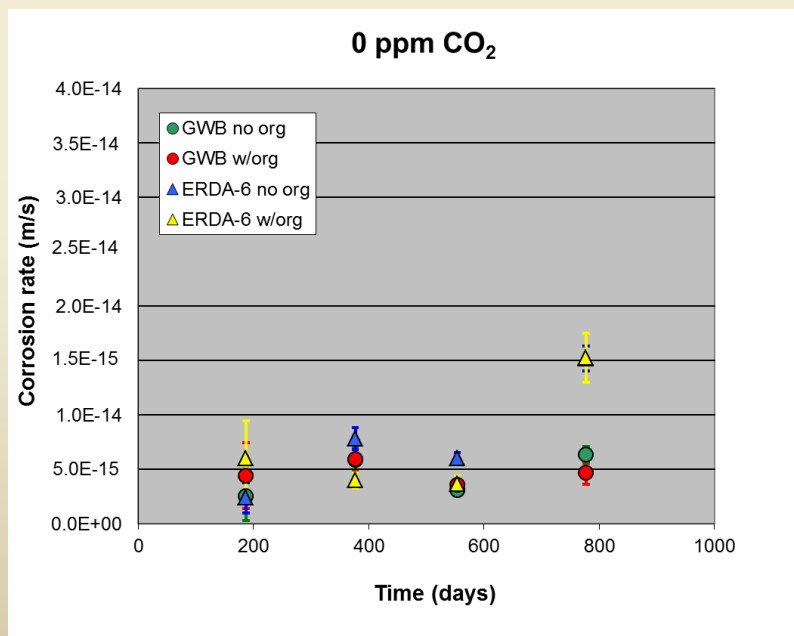
Source: WIPP PA Parameter Viewer

# Updated PA Parameters

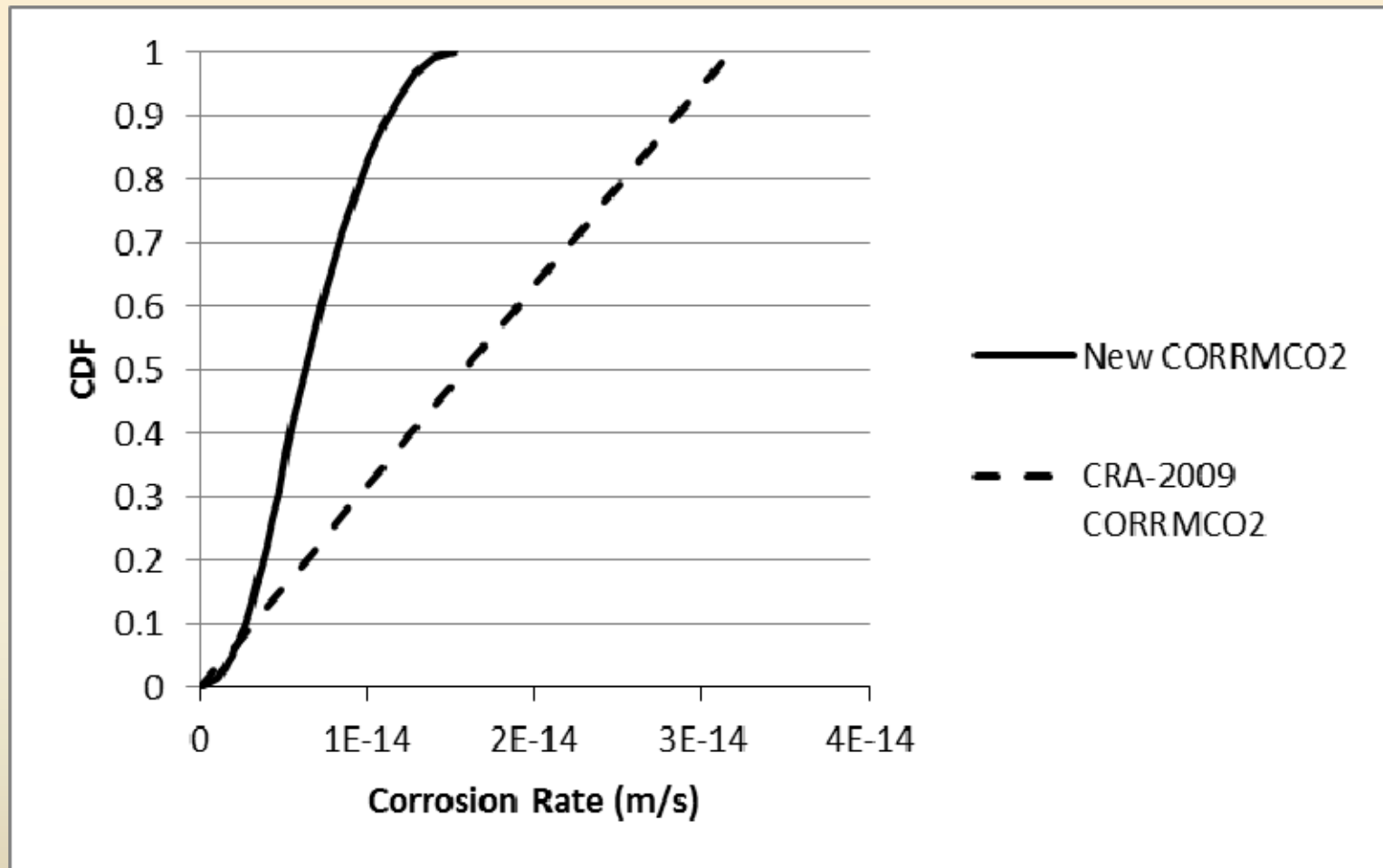
- Proposed PA Parameter Updates

Parameter	Units	Description	Distribution Type	Distribution Parameters
CORRMCO2	m/s	Rate of anoxic steel corrosion under brine-inundated conditions with no CO <sub>2</sub> present	Triangular	Min = 0 Max = 1.523e-14 Mode = 4.749e-15 Mean = 6.660e-15

- HUMCORR and STOIFX remain unchanged



# PA Parameters



# Summary

- Corrosion of Fe
  - ERDA-6 (NaCl-dominated) is more corrosive than GWB (NaCl-MgCl<sub>2</sub>)
  - The presence of organics is important only for ERDA-6 (suppresses corrosion)
  - Corrosion increases with CO<sub>2</sub>
- Steel subjected to humid conditions shows no evidence of corrosion
- No clear evidence of passivation for Fe at low CO<sub>2</sub> ppm
- Based on the new steel corrosion data it is suggested that the PA parameter CORRMCO<sub>2</sub> be changed from a uniform to a triangular distribution with new values.

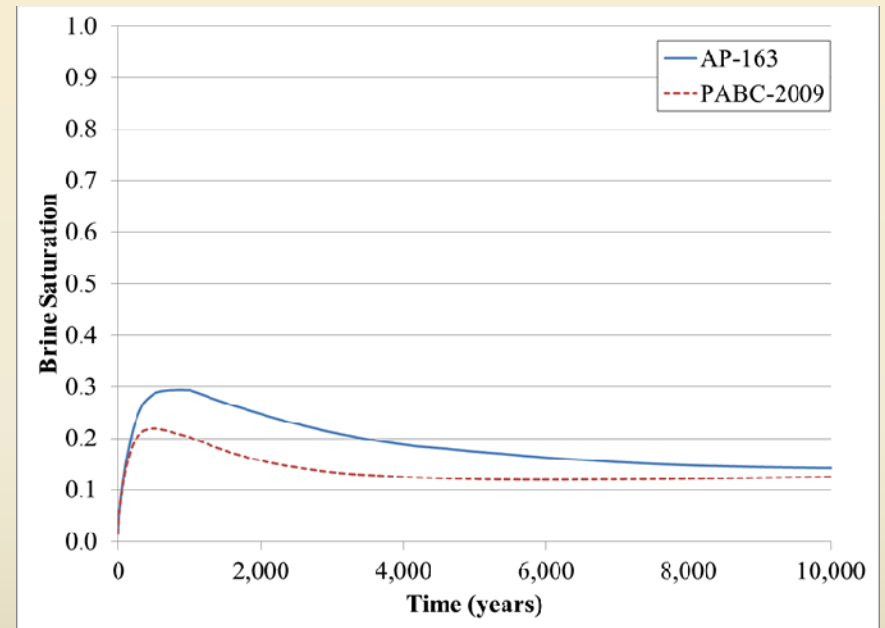
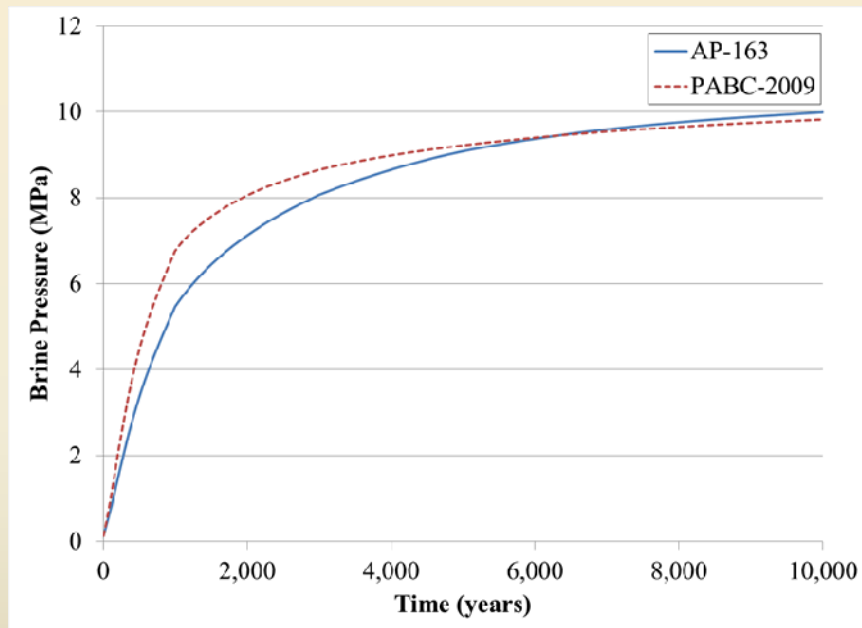
# Effects of New Parameter on PA



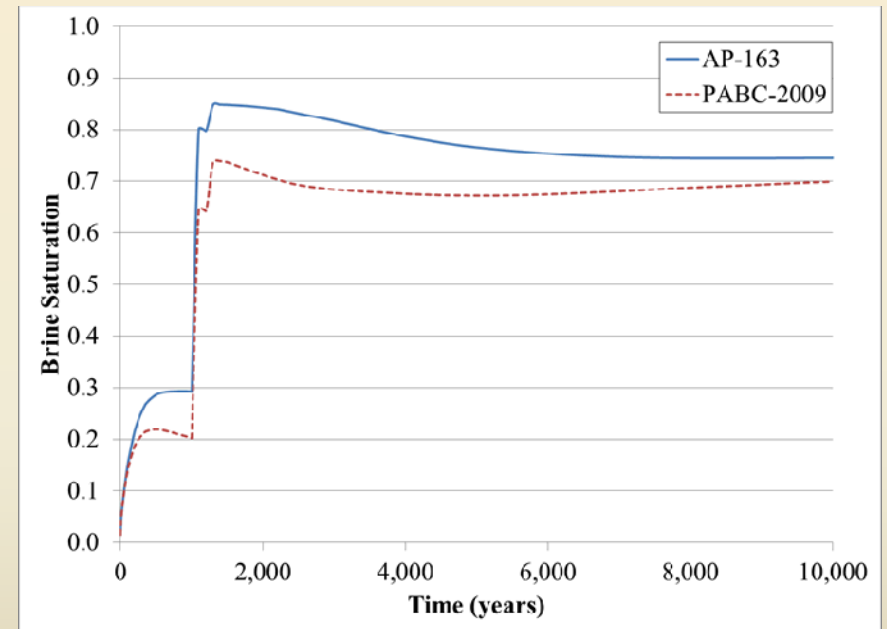
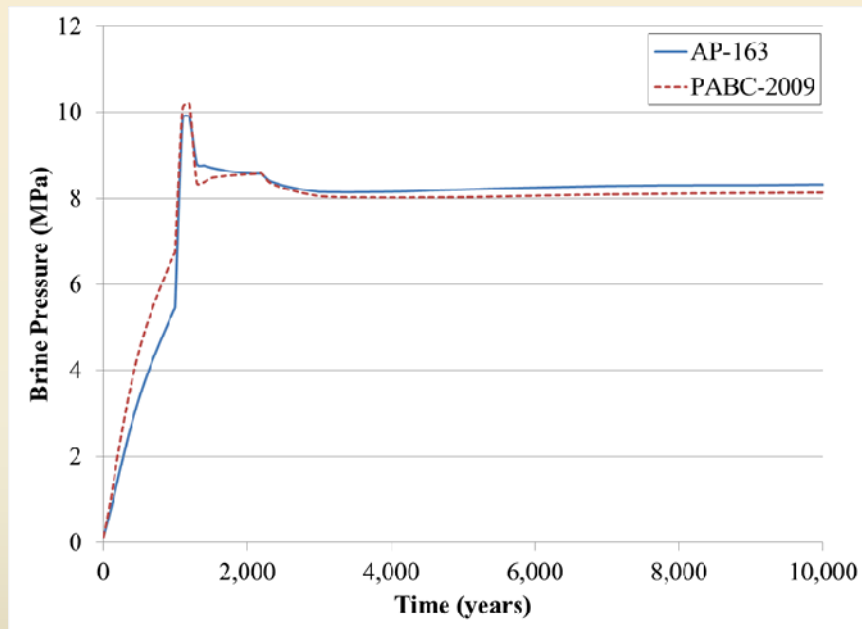
# Preliminary Results

- Increase in saturations
- Pressure
  - Initially lower, then increases at later times or after intrusion
- Less overall waste material degradation, especially at earlier times

# Undisturbed

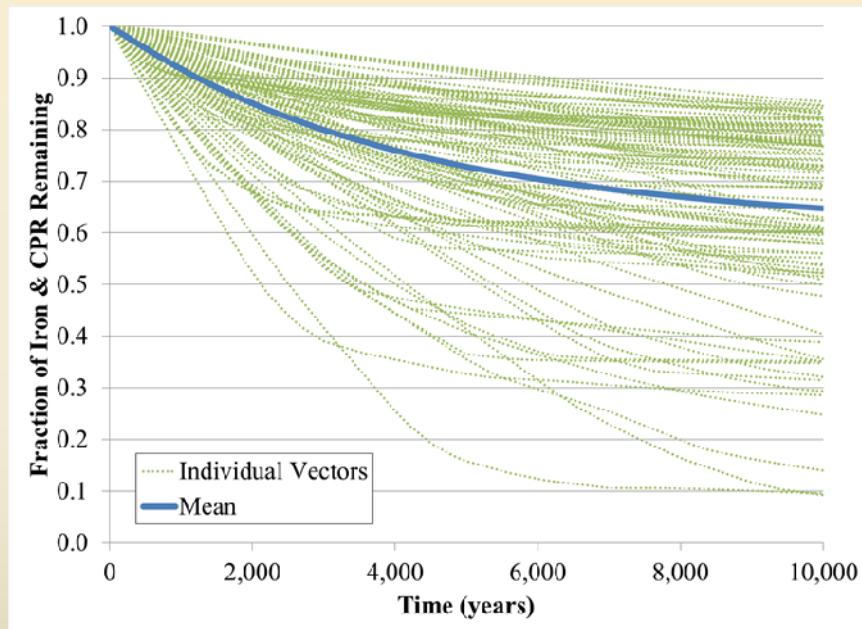


# E1 Intrusion

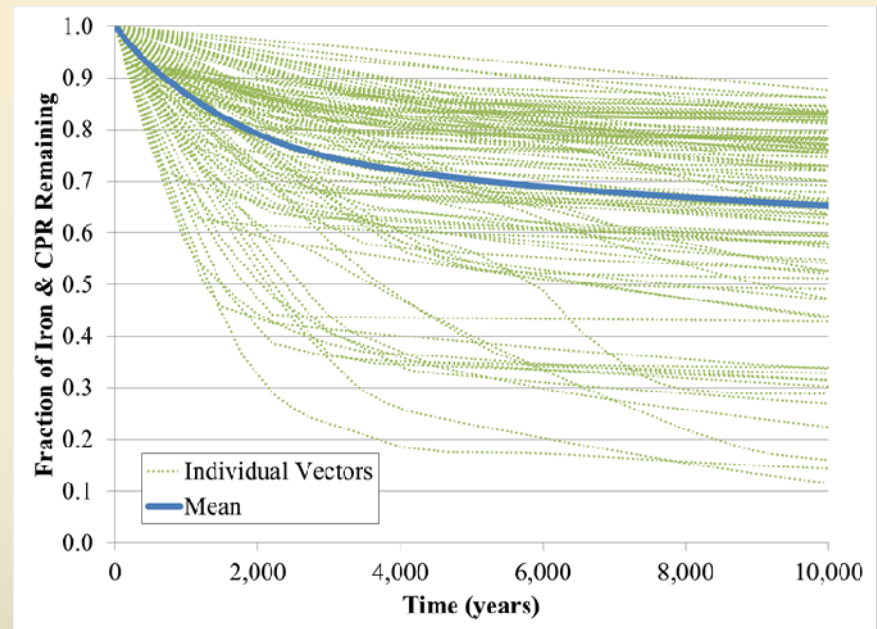


# Waste Material Degradation

## AP-163



## PABC-2009



# Supplemental Materials

# Coupon Compositions

## Steel

Element	Weight Percent
Al	0.026
C	0.050
Ca	0.001
Cr	0.040
Cu	0.110
Fe	balance
Mn	0.250
Mo	0.010
N	0.009
Nb	0.003
Ni	0.040
P	0.006
S	0.005
Si	0.010
Sn	0.007
Ti	0.002
V	0.002

Source: Material Test Report for AE960  
(ERMS 551552)

## Lead

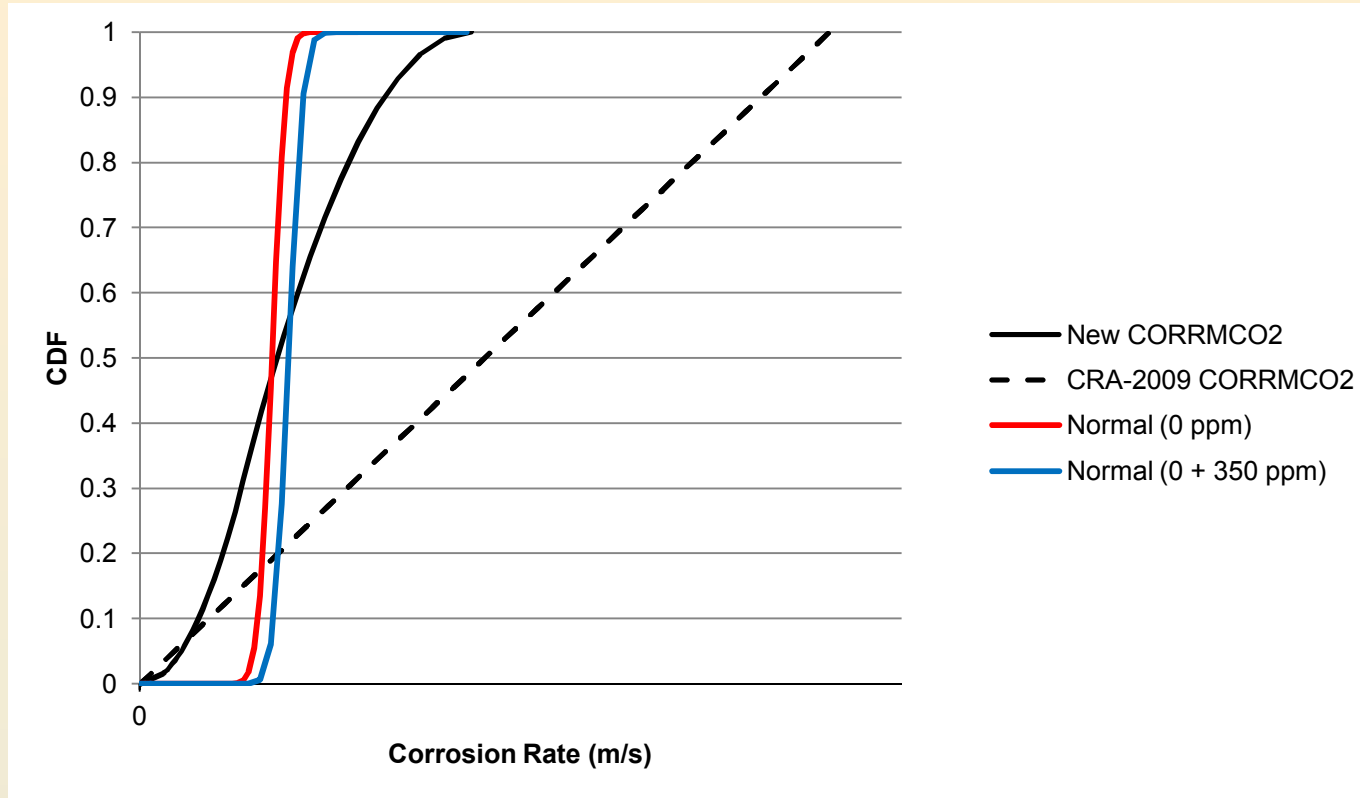
Element	Weight Percent
Ag	0.010
Bi	0.015
Cd	0.001
Cu	0.070
Fe	0.001
Ni	0.001
Pb	99.900
Sb+Sn+As	0.001
Zn	0.001

Source: Certificate of Compliance and Inspection  
Metal Coupon, Lot 32829 (ERMS 551551)

# Brine Compositions

Total Elemental Concentration	GWB Concentration (molal)	ERDA-6 Concentration (molal)	GWB Concentration (molal)	ERDA-6 Concentration (molal)
Na <sup>+</sup>	4.98	6.05	4.99	5.96
K <sup>+</sup>	0.559	0.109	0.563	0.109
Li <sup>+</sup>	$5.05 \times 10^{-3}$	---	$5.05 \times 10^{-3}$	---
Ca <sup>2+</sup>	$1.24 \times 10^{-2}$	$1.28 \times 10^{-2}$	$1.03 \times 10^{-2}$	$1.22 \times 10^{-2}$
Mg <sup>2+</sup>	0.635	0.121	0.663	0.179
Cl <sup>-</sup>	6.30	6.00	6.24	5.98
Br <sup>-</sup>	$3.18 \times 10^{-2}$	$1.24 \times 10^{-2}$	$3.19 \times 10^{-2}$	$1.24 \times 10^{-2}$
SO <sub>4</sub> <sup>2-</sup>	0.209	0.191	0.262	0.203
B <sub>4</sub> O <sub>7</sub> <sup>2-</sup>	$4.73 \times 10^{-2}$	$1.77 \times 10^{-2}$	$4.76 \times 10^{-2}$	$1.77 \times 10^{-2}$
EDTA	---	---	$8.85 \times 10^{-6}$	$9.99 \times 10^{-6}$
Oxalate	---	---	$3.38 \times 10^{-4}$	$3.35 \times 10^{-4}$
Citrate	---	---	$9.09 \times 10^{-4}$	$9.04 \times 10^{-4}$
Acetate	---	---	$1.19 \times 10^{-2}$	$1.19 \times 10^{-2}$

Source: WIPP-FePb-3 p. 51, 52 (ERMS 550783)



Mean =  $6.059\text{E-}15$  m/s  
Std. Error =  $5.059\text{e-}16$  m/s  
n=64

Mean =  $6.811\text{E-}15$  m/s  
Std. Error =  $7.292\text{e-}16$  m/s  
n=124