

Pressure Fluctuations Beneath Instability Wave Packets and Turbulent Spots in a Hypersonic Boundary Layer

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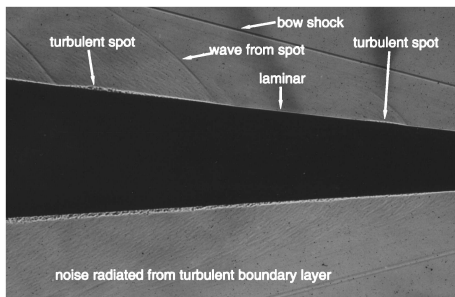


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Motivation

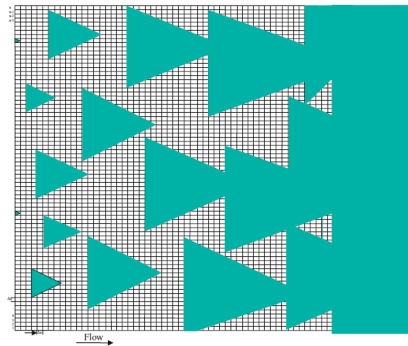
- **Pressure fluctuations peak during boundary-layer transition.**
 - Need to model fluctuations and spatial distribution for structural design of reentry vehicles.
 - Also important for vibration of internal components.
- **Seek to develop more accurate model using turbulent-spot approach.**
 - Current models based on incompressible flow data or from noisy tunnels.



Schlieren image of turbulent spots on a 5° sharp cone at Mach 4.3 in NOL Ballistics Range, from Reda.

Turbulent Spot Approach to Modeling Transitional Pressure Fluctuations

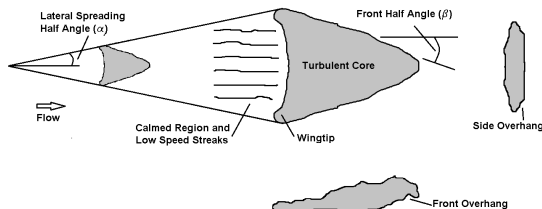
- Model already developed for pressure fluctuations on a flat plate in incompressible flow.
- Need accurate measurements of the growth and the internal structure of the spots as input to model.
- No previous measurements of internal pressure structure of spots in hypersonic flow.



Turbulent spot model simulation, from Vinod (2007).

Turbulent Spot Geometry

- **Spot growth is characterized by:**
 - Lateral spreading half angle.
 - Front half angle or leading and trailing edge velocities.
- **Spot model also relies on:**
 - Spatial distribution of pressure fluctuations.
 - How spots merge.



Schematic of a turbulent spot.

Instability Wave Packets

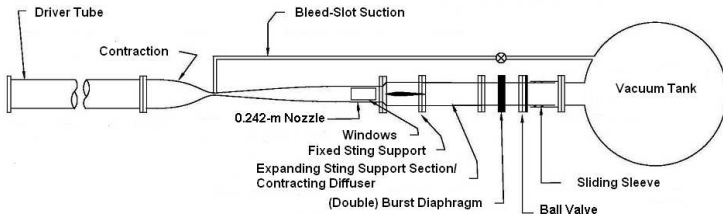
- **The second-mode instability is one of the dominant boundary-layer instabilities at hypersonic speeds.**
- **Acts like an acoustic wave trapped in the boundary layer.**
 - Reflects between model surface and sonic line in the boundary layer as it travels downstream.
 - Dominant instability is 2D.
- **Appears as rope waves in schlieren images.**

Boeing/AFOSR Mach-6 Quiet Tunnel (BAM6QT)

- **Ludwig tube design.**
- **Can be operated under noisy or quiet flow.**
- **For quiet flow:**
 - Contraction boundary layer removed using bleed slots.
 - Laminar boundary layer restarted at throat.
 - Long, highly-polished nozzle to reduce growth of instabilities.
 - Laminar flow is maintained downstream of nozzle exit.



BAM6QT nozzle and test section.



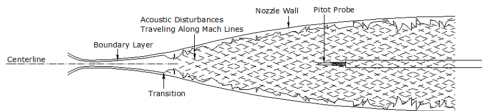
Conventional vs. Quiet Tunnels

- **Conventional Tunnels**

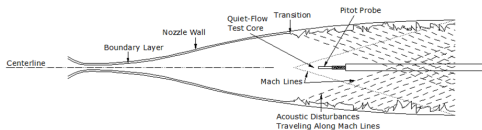
- High noise near 2–5% of the mean.
- Noise can cause much earlier transition than in flight.

- **Quiet Tunnel**

- Low noise around 0.05%.
- Comparable to flight.



Conventional Tunnel



Quiet Tunnel

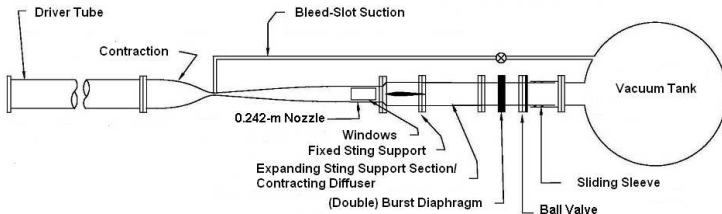
Schematic of difference between conventional and quiet tunnel, from Segura (2007).

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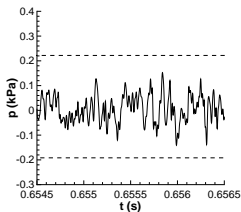


BAM6QT nozzle and test section.

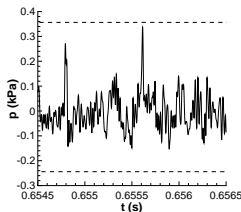


Previous Pressure Measurements on a 7° Sharp Cone

- **Pressure measurements did not clearly show spots even though statistical evidence pointed to their presence.**
 - Tunnel noise interferes with pressure fluctuation measurements.
 - Transition only occurs on model under noisy flow.
 - Tunnel noise is measured under laminar boundary layer.
 - Frequency response and spatial resolution limitations.
 - Thin boundary layer.



Laminar boundary layer

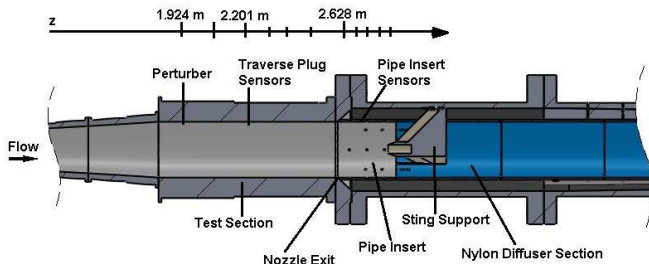


Transitional boundary layer

- **Wall measurements in a quiet tunnel avoid these problems.**
 - Thick, laminar boundary layer.

Experimental Setup

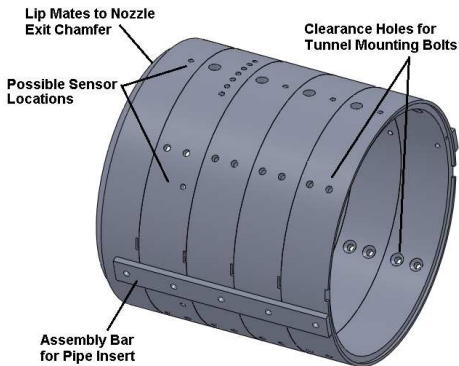
- **Perturber on top wall of tunnel, upstream of sensors.**
- **Row of Kulite pressure transducers on top wall of tunnel.**
 - 4 sensors in nozzle traverse plug.
 - 5 sensors downstream of nozzle exit in pipe insert.
- **Two spanwise rows of Kulite pressure transducers, one near perturber and one in pipe insert.**



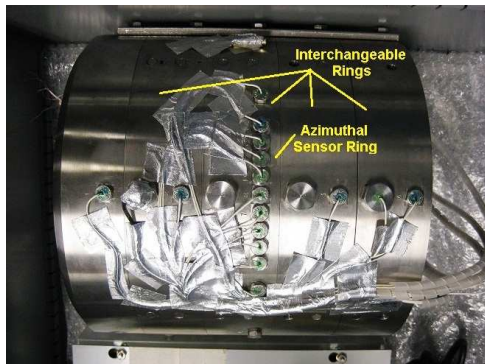
Setup schematic.

Experimental Setup

- **Pipe insert made of five rings.**
 - Can place spanwise sensor array at four downstream locations.
 - Five sensor locations on either side of tunnel centerline.
- **Location of ring changed during testing.**

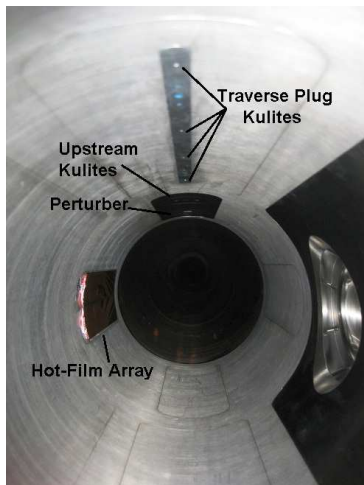


CAD model.

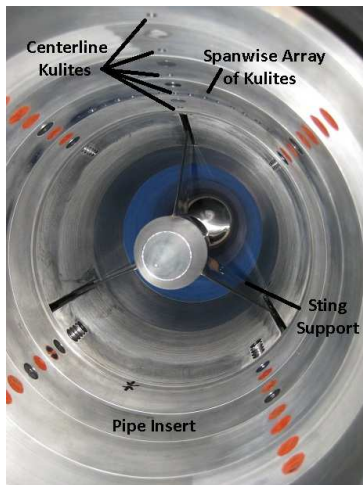


Multi-ring pipe insert.

Experimental Setup



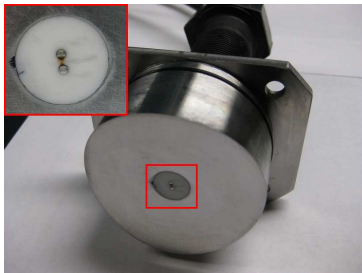
Looking upstream into nozzle.



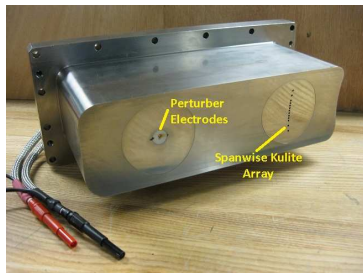
Looking downstream into pipe insert.

Flow Perturber

- **Two electrodes with gap perpendicular to flow.**
- **Ignition coil and timing circuit used to create perturbations.**
- **Perturbations created at 200 Hz.**
 - Avoids picking up electro-magnetic interference during measurements.
- **50 disturbances are used to compute ensemble-averaged time traces and an averaged power spectral density.**



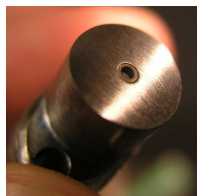
Perturber electrodes.



Perturber nozzle-wall insert.

Instrumentation: Kulite Pressure Transducers (XCQ-062-15A)

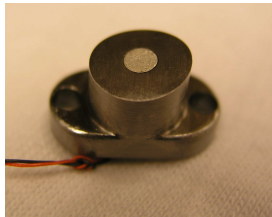
- Resonant frequency near 300 kHz.
- A-screen used for frequency measurements up to ~ 90 kHz.
- Higher frequency measurements will have some attenuation.



Kulite installed in insert.

Instrumentation: PCB132 Pressure Transducers

- Piezoelectric-type sensor.
- Resonant frequency above 1 MHz.
- Signal high-pass filtered at 11 kHz.
- Limited spatial resolution.
- Designed as time-of-arrival sensors.
- Have not yet been sufficiently dynamically calibrated.



PCB132 installed in insert.

Instrumentation: ALTP sensors

- High-frequency heat-transfer gage.
- Typical electronics provide AC signal between 17 Hz and 1 MHz and separate DC signal.

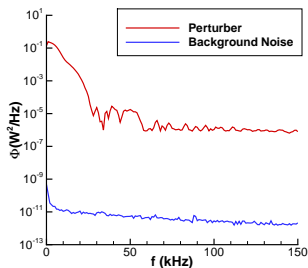
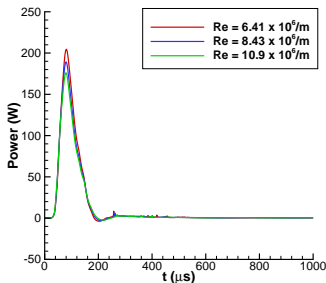
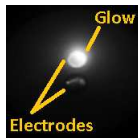


ALTP installed in insert.

Controlled Generation of Nozzle-Wall Disturbances

Electrical Perturbation Measurements

- Made voltage and current measurements of perturbation.
- Observe a lower-frequency pulse instead of a rapid spark.
 - Corresponds to a pulsed glow perturbation.
- Computed PSD of perturbation power.
 - Dominant frequencies below 30 kHz.
 - Still significant frequency content above 150 kHz.

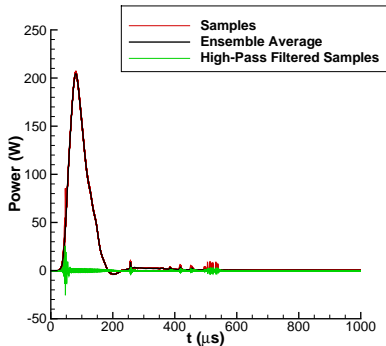


Ensemble-averaged time traces.

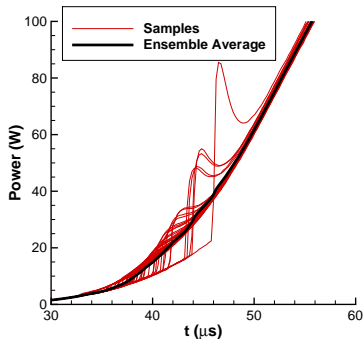
Power spectral density at
 $Re = 6.41 \times 10^6/m$.

Electrical Perturbation Measurements

- Higher frequency contribution was investigated.
- Individual samples show deviations from mean near $50\ \mu\text{s}$ and $250\text{--}500\ \mu\text{s}$.
- During initiation of glow pulse, high frequencies are generated.



Individual samples and ensemble average.

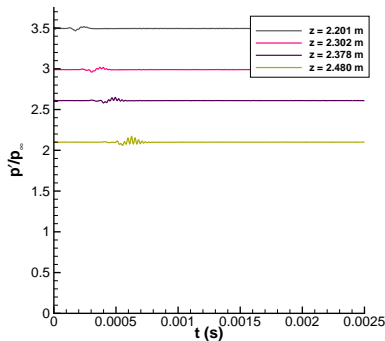


Close-up of high frequencies during glow initiation.

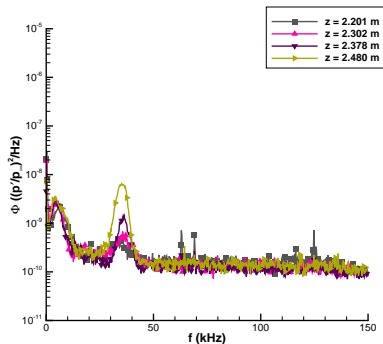
Centerline Measurements of Controlled Disturbances

Centerline Measurements at $Re = 6.33 \times 10^6/m$

- Perturbation initially generates a linear wave packet.
- Packet grows and becomes nonlinear by $z = 2.679$ m.
- Additional peaks appear in the spectra by $z = 2.730$ m.
- Start to get rise in broadband frequencies by $z = 2.831$ m.



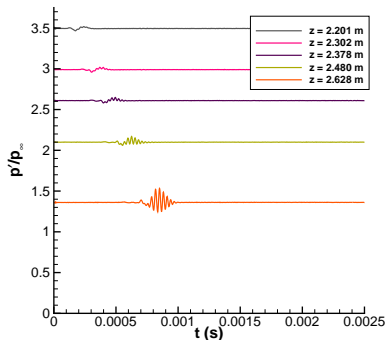
Time traces.



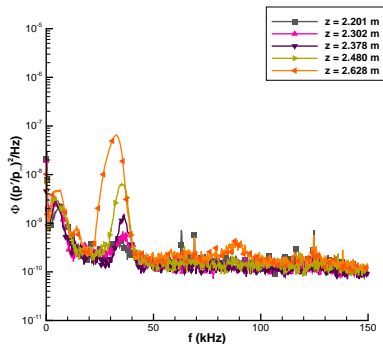
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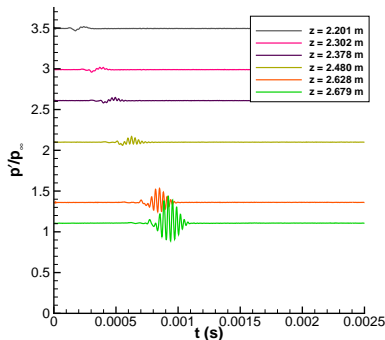
Time traces.



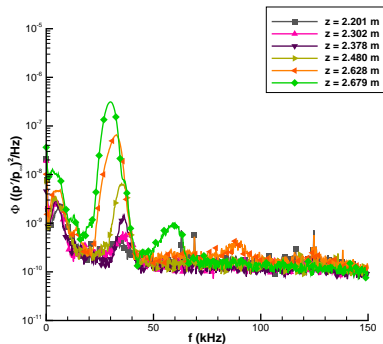
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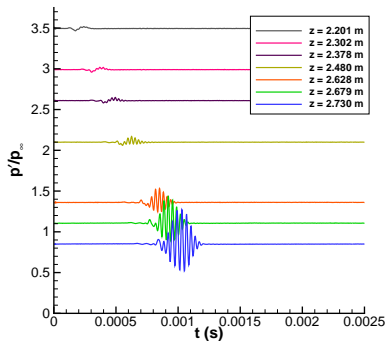
Time traces.



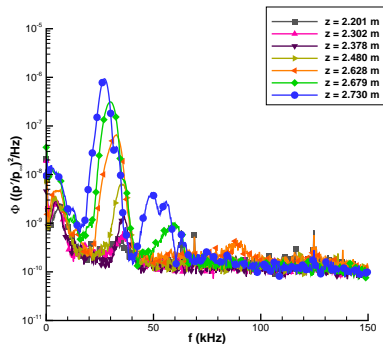
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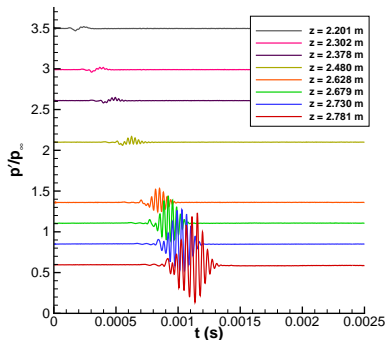
Time traces.



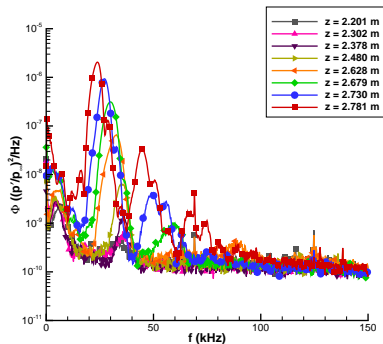
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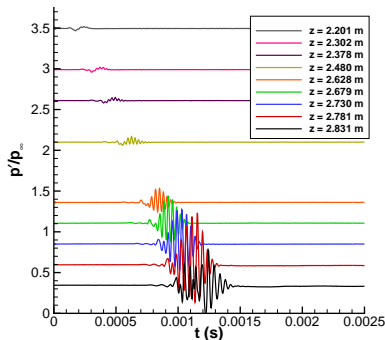
Time traces.



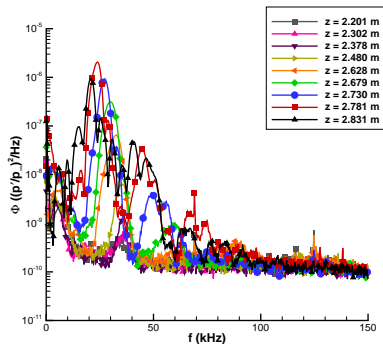
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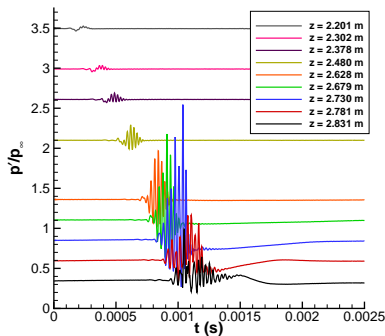
Time traces.



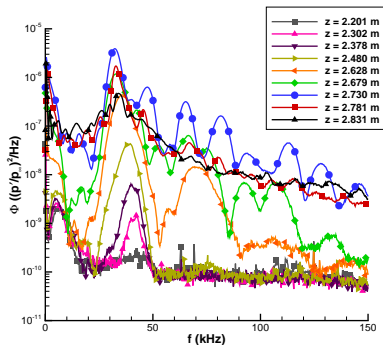
Power spectral density.

Centerline Measurements at $Re = 8.25 \times 10^6/m$

- Small second-mode waves grow and develop along nozzle length.
- Peak frequency is $\sim 30\text{--}40$ kHz.
- Large amplitude fluctuations visible before breakdown.
- Second-mode waves still visible on either side of turbulent fluctuations.



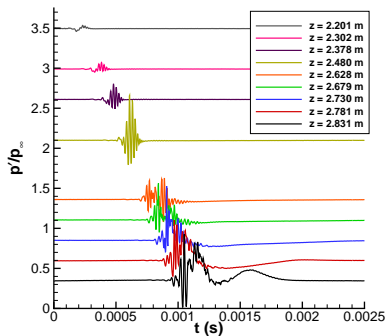
Time traces.



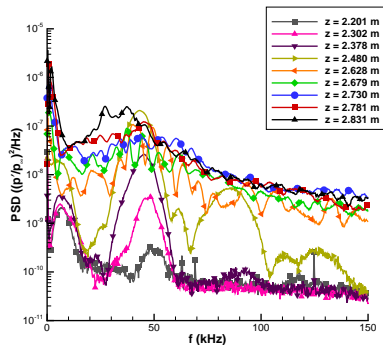
Power spectral density.

Centerline Measurements at $Re = 10.8 \times 10^6/m$

- Second-mode waves grow larger in amplitude further upstream.
- Peak frequency is $\sim 45\text{--}50$ kHz.
- Breakdown occurs before pipe insert sensors.
- Second-mode waves still visible on either side of turbulent fluctuations.



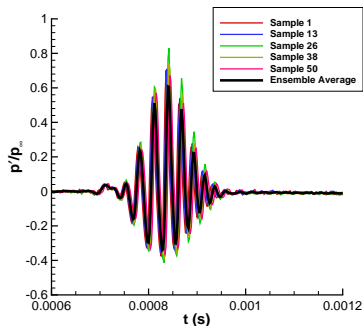
Time traces.



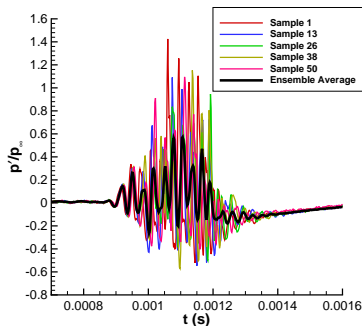
Power spectral density.

Deviation of Individual Samples from Ensemble Average at $Re = 8.25 \times 10^6/m$

- Samples show good repeatability through breakdown.
- Average traces do not represent samples once they breakdown.
- Power spectral density computed from traces shows average frequency content of disturbances.



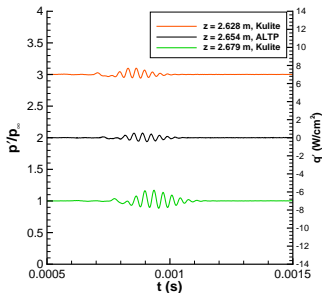
$z = 2.628$ m



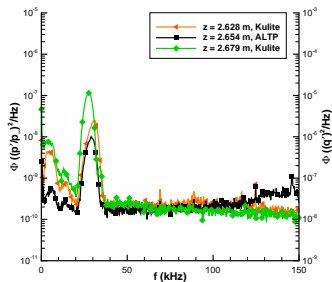
$z = 2.831$ m

Comparison of Kulite and ALTP Ensemble Averages at $Re = 5.76 \times 10^6/m$

- Can verify results by comparing to other sensors.
- Kulite data compared to nearby heat-transfer ALTP gages.
- Sensors show similar wave packet structures, but differences arise at higher Re .



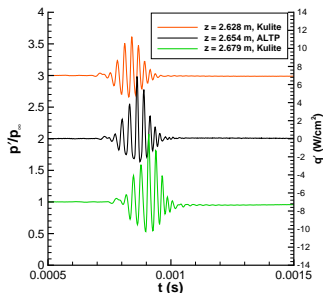
Time traces.



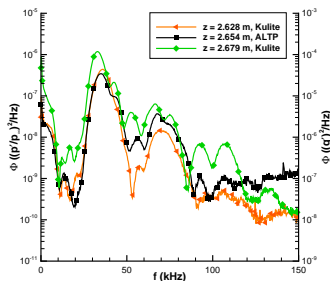
Power spectral density.

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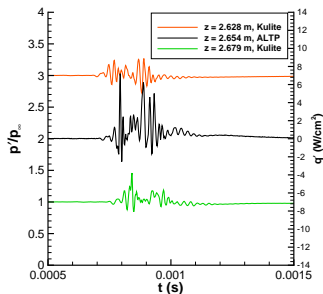
Time traces.



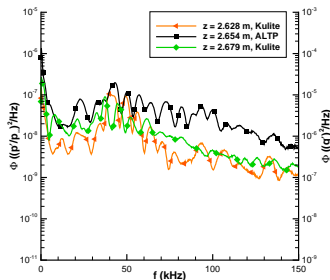
Power spectral density.

Comparison of Kulite and ALTP Ensemble Averages at $Re = 10.8 \times 10^6/m$

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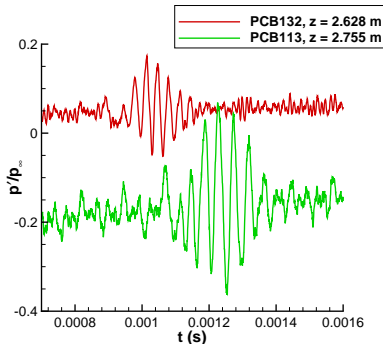
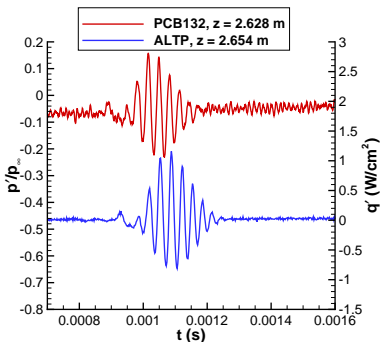
Time traces.



Power spectral density.

Verification with Other Sensors, $Re = 5.80 \times 10^6/m$

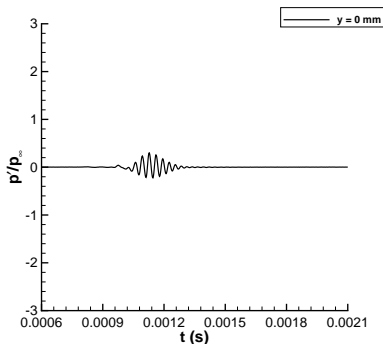
- Can also compare to other pressure sensors (PCB132 and PCB113).
- All sensors show wave packets, but there are differing electronic noise levels.
- ALTP has best signal-to-noise ratio, PCB113 has the worst.



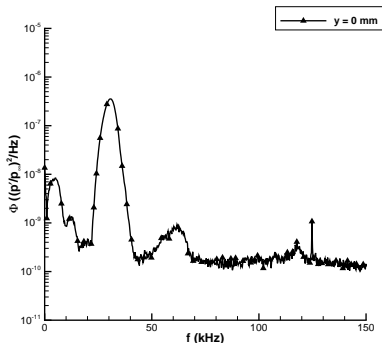
Spanwise Distribution of Pressure Fluctuations within Controlled Disturbances

Spanwise Measurements at $Re = 6.33 \times 10^6/m$, $z = 2.679$ m

- Spanwise Kulite array used to observe off-center disturbance structure.
- Largest waves occur near the centerline.
- Some asymmetry in these measurements.



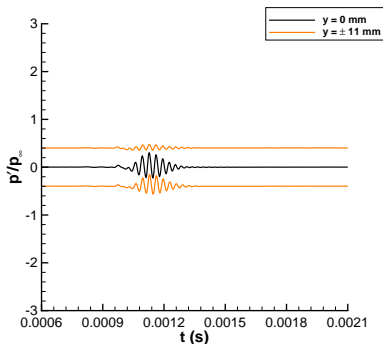
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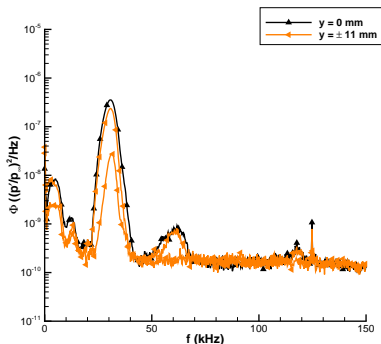
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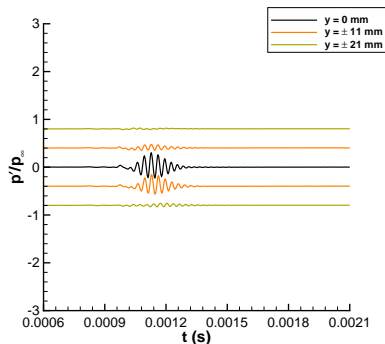
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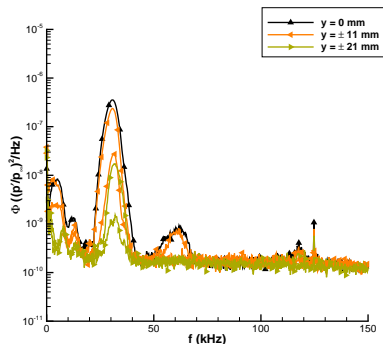
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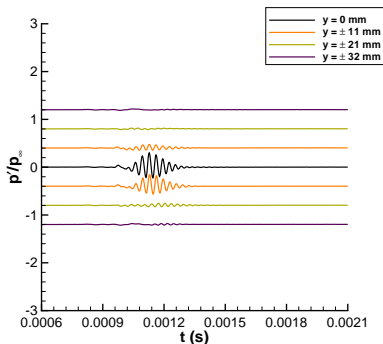
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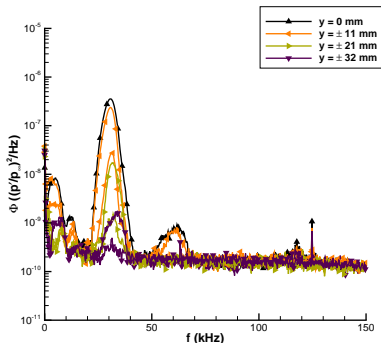
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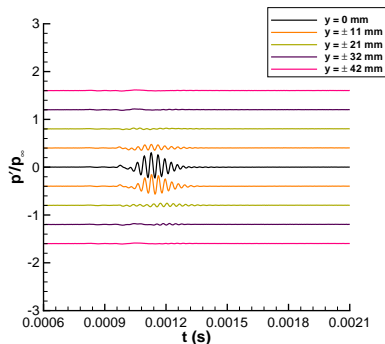
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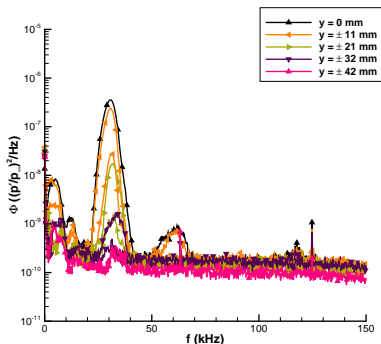
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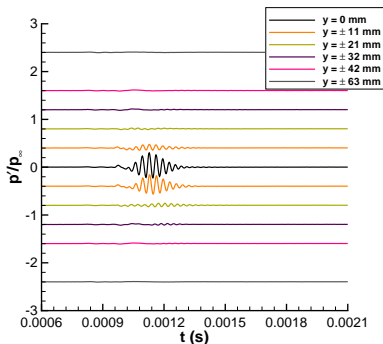
Time traces.



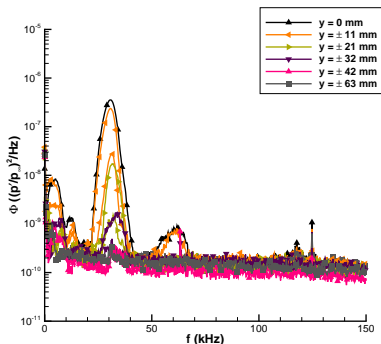
Power spectral density.

Spanwise Measurements at $Re = 6.33 \times 10^6/m$, $z = 2.679$ m

- Spanwise Kulite array used to observe off-center disturbance structure.
- Largest waves occur near the centerline.
- Some asymmetry in these measurements.



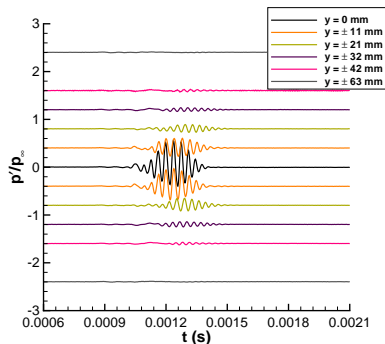
Time traces.



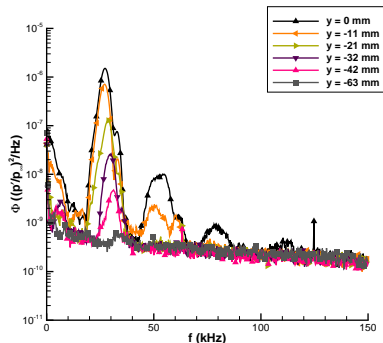
Power spectral density.

Spanwise Measurements at $Re = 6.33 \times 10^6/m$, $z = 2.730$ m

- Wave amplitudes grow further downstream.
- By $z = 2.831$ m, averaged wave amplitude decreases.
- Some waves may be breaking down, leading to smaller averaged amplitudes and more broadband frequencies in the PSD.



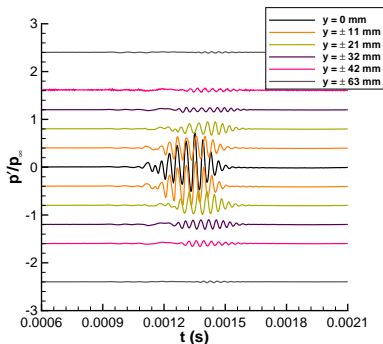
Time traces.



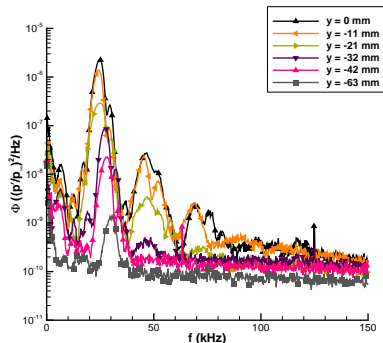
Power spectral density.

Spanwise Measurements at $Re = 6.33 \times 10^6/m$, $z = 2.781$ m

- Wave amplitudes grow further downstream.
- By $z = 2.831$ m, averaged wave amplitude decreases.
- Some waves may be breaking down, leading to smaller averaged amplitudes and more broadband frequencies in the PSD.



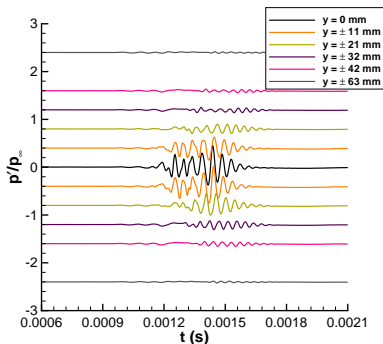
Time traces.



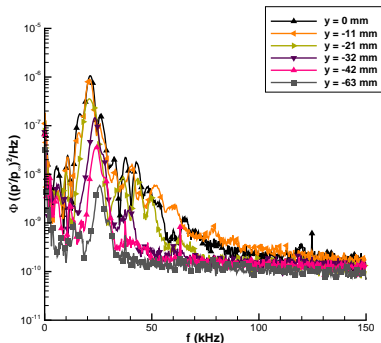
Power spectral density.

Spanwise Measurements at $Re = 6.33 \times 10^6/m$, $z = 2.831$ m

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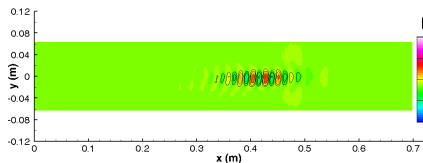


Time traces.

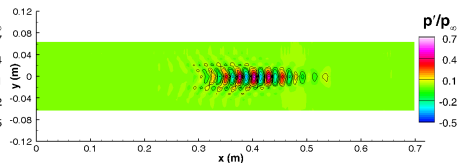


Power spectral density.

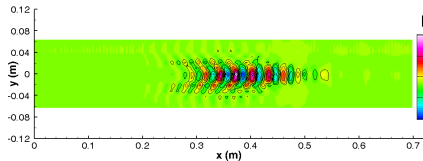
Contour Plots of Spanwise Measurements at $Re = 6.3 \times 10^6/m$



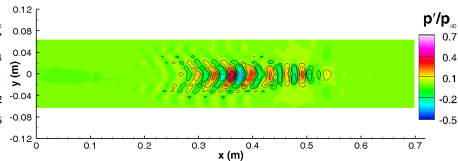
(a) $z = 2.679$ m



(b) $z = 2.730$ m

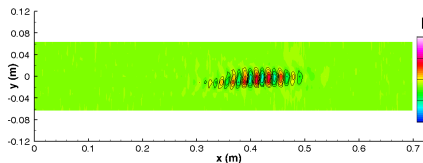


(c) $z = 2.781$ m

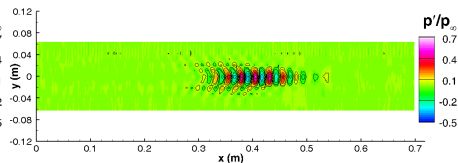


(d) $z = 2.831$ m

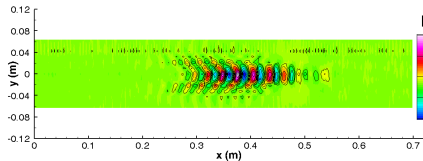
Contour Plots of Spanwise Measurements at $Re = 6.3 \times 10^6/m$



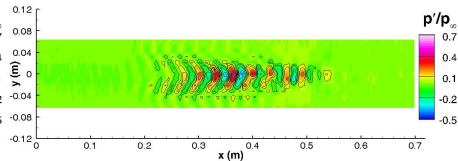
(e) $z = 2.679$ m



(f) $z = 2.730$ m



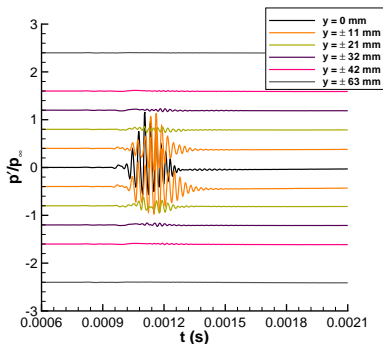
(g) $z = 2.781$ m



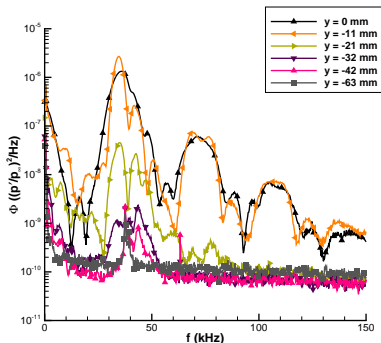
(h) $z = 2.831$ m

Spanwise Measurements at $Re = 8.3 \times 10^6/m$, $z = 2.679$ m

- Spanwise measurements agree with centerline results.
- Large second-mode waves near centerline.
- Waves decrease in amplitude further from centerline.
- Breakdown of the waves begins in the center of the disturbances.



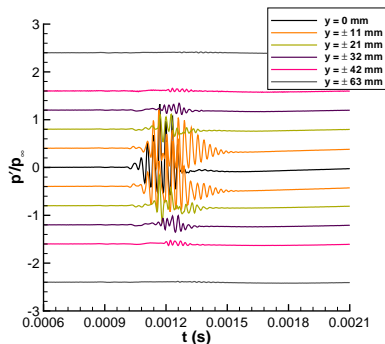
Time traces.



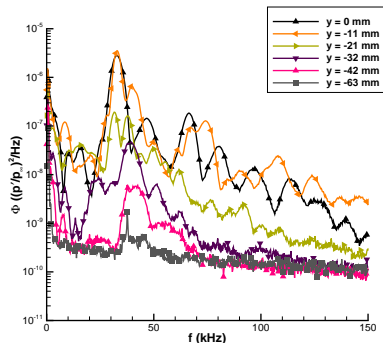
Power spectral density.

Spanwise Measurements at $Re = 8.3 \times 10^6/m$, $z = 2.730$ m

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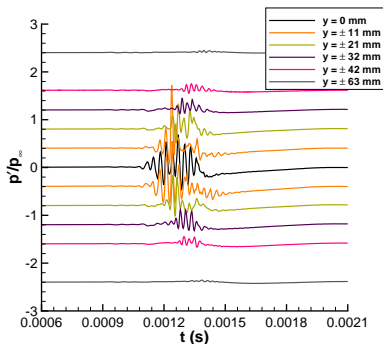
Time traces.



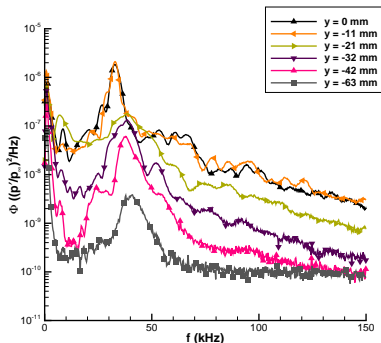
Power spectral density.

Spanwise Measurements at $Re = 8.3 \times 10^6/m$, $z = 2.781$ m

- Further downstream, waves break down on centerline.
- Broadband frequencies observed in spectra.
- Second-mode waves still observed at front, rear, and spanwise edges of spots.



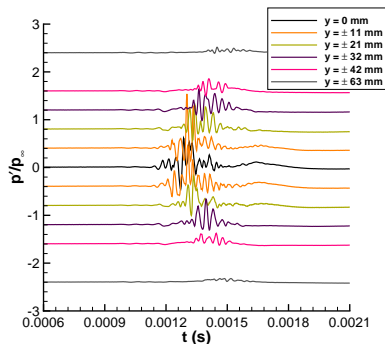
Time traces.



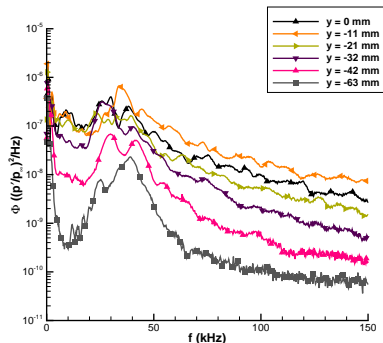
Power spectral density.

Spanwise Measurements at $Re = 8.3 \times 10^6/m$, $z = 2.831$ m

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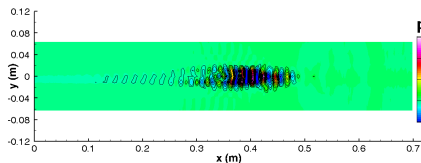


Time traces.

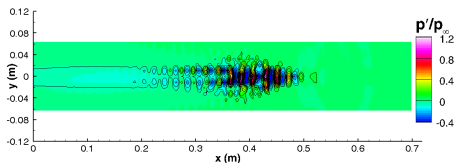


Power spectral density.

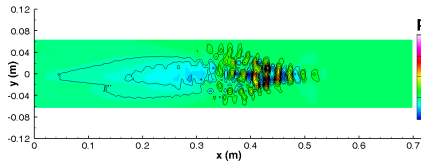
Contour Plots of Spanwise Measurements near $Re = 8.30 \times 10^6/m$



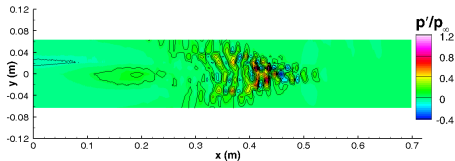
(a) $z = 2.679$ m



(b) $z = 2.730$ m

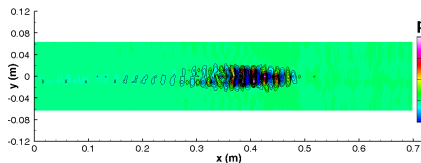


(c) $z = 2.781$ m

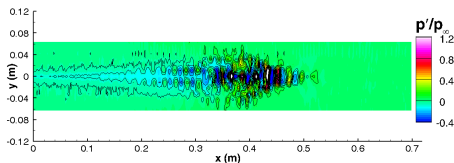


(d) $z = 2.831$ m

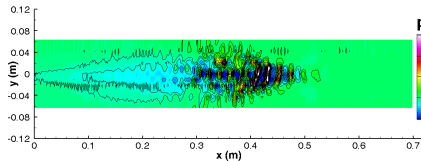
Contour Plots of Spanwise Measurements near $Re = 8.30 \times 10^6/m$



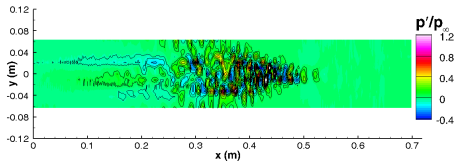
(e) $z = 2.679$ m



(f) $z = 2.730$ m



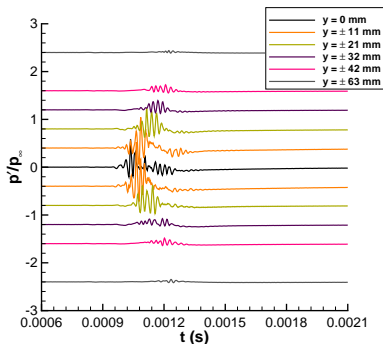
(g) $z = 2.781$ m



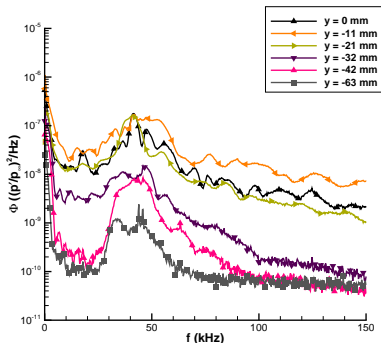
(h) $z = 2.831$ m

Spanwise Measurements at $Re = 10.8 \times 10^6/m$, $z = 2.679$ m

- Characteristic arrowhead shape of turbulent spots is seen.
- Turbulent fluctuations are observed near center.
- Second-mode waves persist at spanwise edges.
- Waves also observed in front and rear of spots.



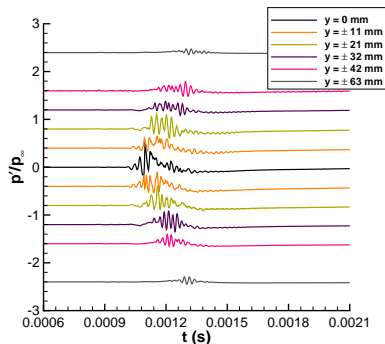
Time traces.



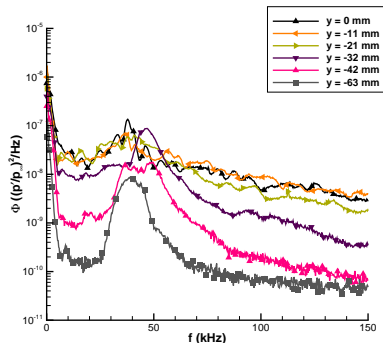
Power spectral density.

Spanwise Measurements at $Re = 10.8 \times 10^6/m$, $z = 2.730$ m

- Characteristic arrowhead shape of turbulent spots is seen.
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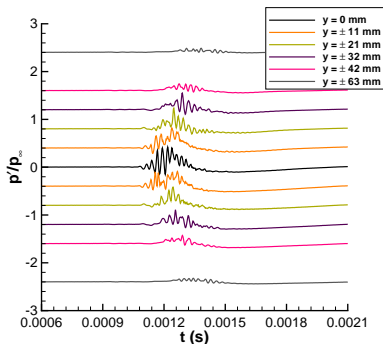
Time traces.



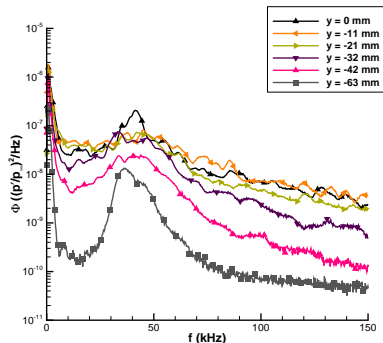
Power spectral density.

Spanwise Measurements at $Re = 10.8 \times 10^6/m$, $z = 2.781$ m

- Characteristic arrowhead shape of turbulent spots is seen.
- Turbulent fluctuations are observed near center.
- Second-mode waves persist at spanwise edges.
- Waves also observed in front and rear of spots.



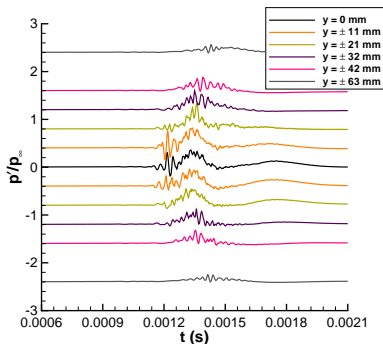
Time traces.



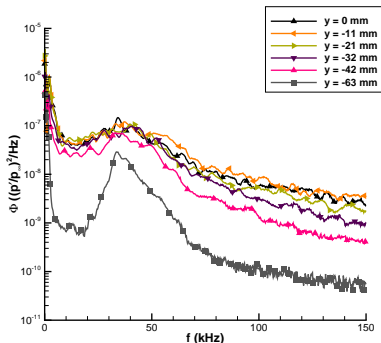
Power spectral density.

Spanwise Measurements at $Re = 10.8 \times 10^6/m$, $z = 2.831$ m

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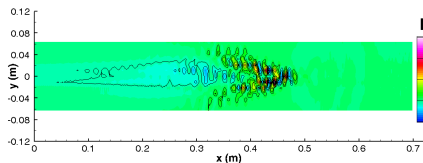


Time traces.

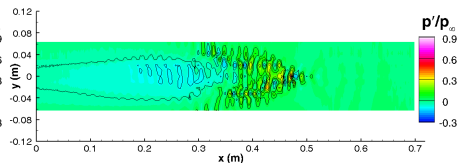


Power spectral density.

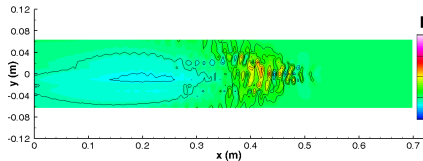
Contour Plots of Spanwise Measurements at $Re = 10.8 \times 10^6/m$



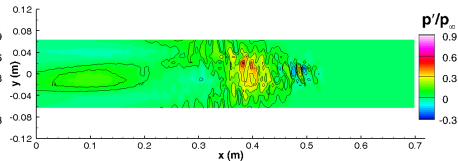
(a) $z = 2.679$ m



(b) $z = 2.730$ m

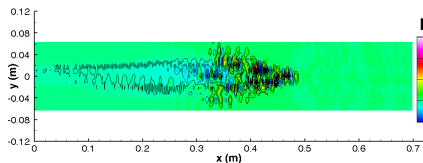


(c) $z = 2.781$ m

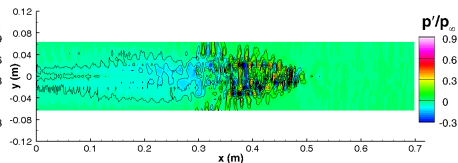


(d) $z = 2.831$ m

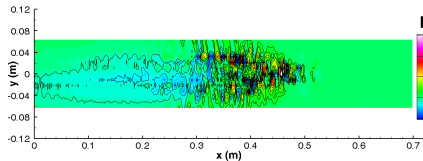
Contour Plots of Spanwise Measurements at $Re = 10.8 \times 10^6/m$



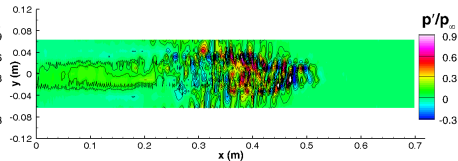
(e) $z = 2.679$ m



(f) $z = 2.730$ m



(g) $z = 2.781$ m

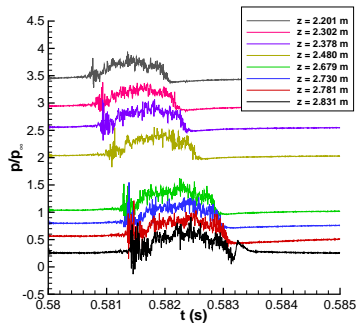


(h) $z = 2.831$ m

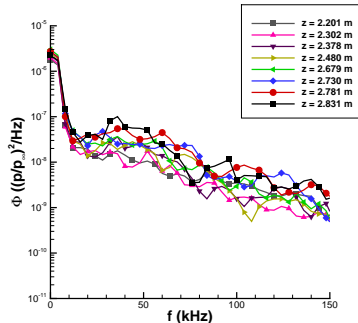
Natural Growth of Nozzle-Wall Disturbances

Large Turbulent Spot at $Re = 11.2 \times 10^6/m$

- Spots originate near throat and grow large along nozzle length.
- Cover majority of nozzle circumference.
- Occur more frequently at higher Re .
- Last sensor shows a second pressure peak behind the spot.



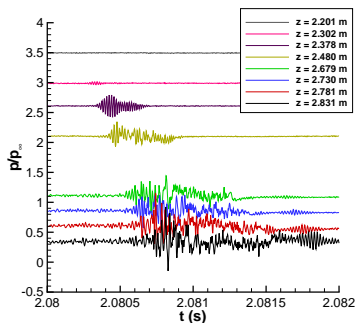
Time traces.



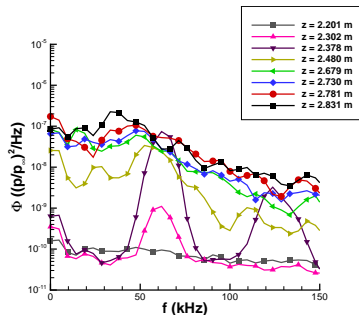
Power spectral density.

Natural Nozzle Wall Disturbances: Second-Mode Disturbances at $Re = 10.6 \times 10^6 / m$

- Small disturbances originate further downstream on nozzle wall.
- Wave packets agree with computed second-mode frequencies.
- Packets breakdown into turbulent spots.
- Occur more frequently at higher Re .

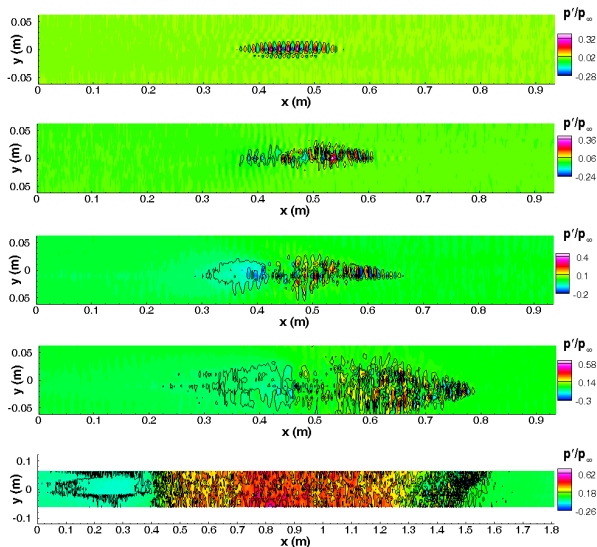


Time traces.



Power spectral density.

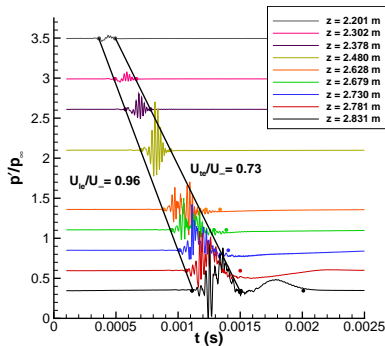
Spanwise Distribution of Pressure Fluctuations, Re near $10.8 \times 10^6/m$



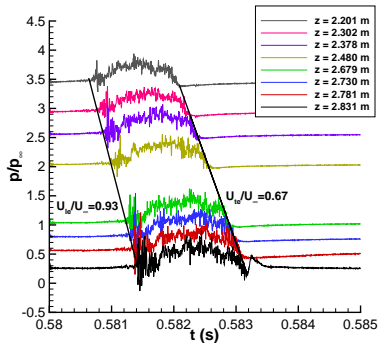
Turbulent-Spot Model Parameters

Convection Velocities Near $Re = 11.0 \times 10^6/m$

- Average leading edge convection velocity of $0.95 U_\infty$.
- Trailing edge convection velocity varies with Re between 0.64 – $0.75 U_\infty$.
- Computed velocities agree well with natural disturbances, DNS, and other experiments.



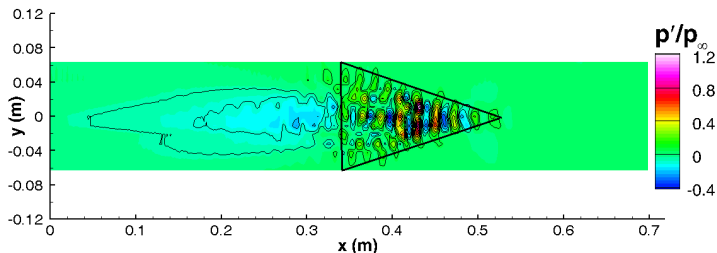
Controlled disturbances.



Naturally developing turbulent spots

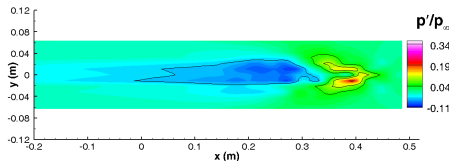
Lateral Spreading Angle of Disturbances, $Re = 8.30 \times 10^6 / m$

- **Triangular footprint was estimated for disturbances at four downstream locations.**
 - Lateral edges of disturbances as they change downstream are used to compute lateral spreading angle.
- **Found angle of ~ 15 degrees, much higher than expected.**
 - High-frequency pressure fluctuations have never been used to define the spot footprint before.
 - May provide a different spreading angle than other experimental or computational methods.

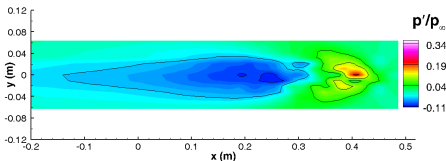


Low-Frequency Component of Disturbances

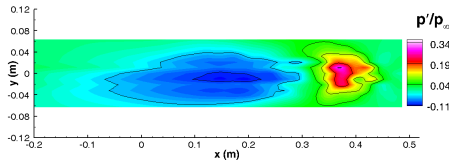
- Time traces near $Re = 10.8 \times 10^6 / m$ were low-pass filtered at 15 kHz to look at mean pressure change within disturbances.
- Higher mean pressure in core, $\sim 20\text{--}30\%$ above p_∞ .
- Low pressure calmed region behind spots, $\sim 10\%$ below p_∞ .



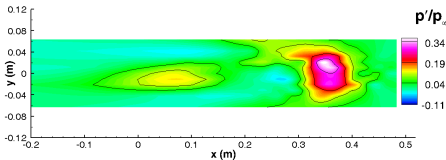
(a) $z = 2.679$ m



(b) $z = 2.730$ m



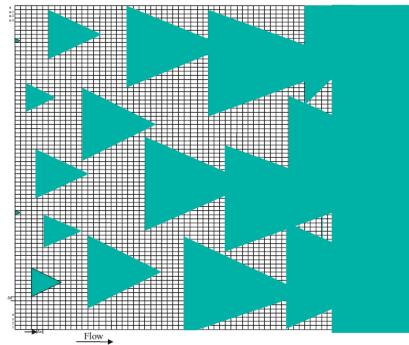
(c) $z = 2.781$ m



(d) $z = 2.831$ m

Turbulent Spot Model Parameters

- **Spot growth is characterized by:**
 - ✓ Lateral spreading half angle.
 - ✓ Leading and trailing edge convection velocities.
- **Spot model also relies on:**
 - ✓ Spatial distribution of pressure fluctuations.
 - ✗ How spots merge.

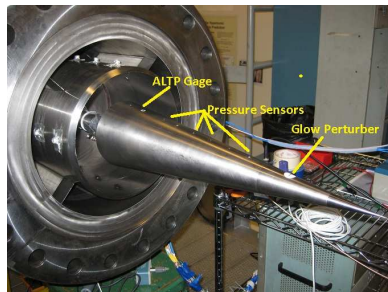


Turbulent spot model simulation, from Vinod (2007).

Controlled Perturbations on a Seven-Degree Cone

Controlled Perturbations on a Seven-Degree Cone: Experimental Setup

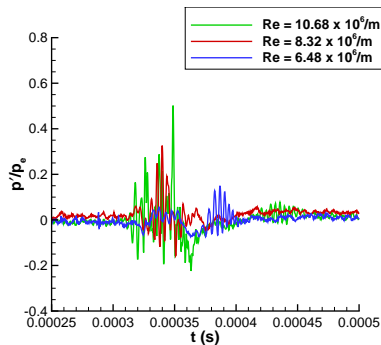
- Glow perturber was placed on cone.
- Followed by a line of 8 sensors along centerline.
- A mix of Kulite, PCB132, and ALTP sensors were used.
- Results shown here are from a PCB132 midway down cone.



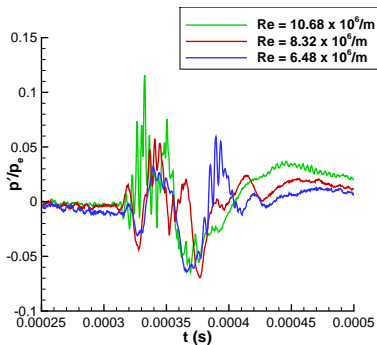
Cone installed in BAM6QT for
glow-perturber tests.

PCB132 Results at varying Re

- **Similar perturbations used to generate ensemble averages.**
 - Still scatter from sample to sample.
- **Can see second-mode wave packet at low Re .**
- **Becomes turbulent at high Re .**
- **Appears similar to transitional physics on nozzle wall.**



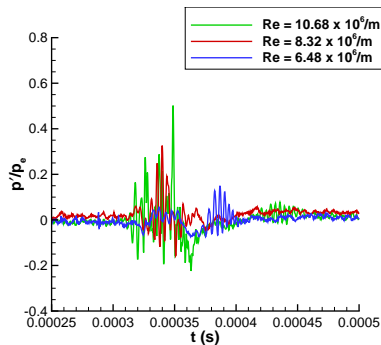
Time traces of individual samples.



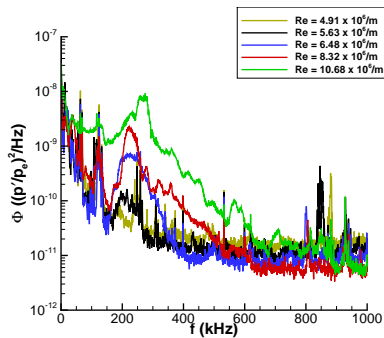
Ensemble-averaged time traces.

PCB132 Results at varying Re

- **Similar perturbations used to generate ensemble averages.**
 - Still scatter from sample to sample.
- **Can see second-mode wave packet at low Re .**
- **Becomes turbulent at high Re .**
- **Appears similar to transitional physics on nozzle wall.**



Time traces of individual samples.



Power spectral density.

- **Thick nozzle-wall boundary layer allows resolution of boundary-layer disturbances with pressure instrumentation.**
- **Wave packets:**
 - Smaller wave packets are ordered and concentrated near the centerline.
 - Larger wave packets become distorted.
 - Weaker second-mode disturbances extend in spanwise direction.
- **Turbulent spots:**
 - At higher Re , wave packets break down to turbulence in center of spots.
 - See characteristic arrowhead shape of turbulent spots.
 - At edges, front, and rear of spots, second-mode waves are still observed and dominate the spectra.

- **Natural disturbances:**

- Two disturbances primarily seen at higher Re .
 - Large turbulent spots growing from near throat.
 - Second-mode waves breaking down to turbulent spots further downstream in nozzle.
- Natural disturbances have similar characteristics to controlled disturbances.

- **Development of turbulent-spot model:**

- Experiments provide convection velocity, spreading angle, and pressure-fluctuation field of disturbances.
- Still need to address what happens as disturbances merge.

- **Extension to a seven-degree cone:**

- Wave packets and turbulent spots can be created and studied on cone with available pressure instrumentation.
- Growth and breakdown of waves appears similar to nozzle wall, but improved measurements needed.

Suggestions for Future Work

- **Increase measurement length to study more developed spots and spot merging.**
 - Can use a pipe-insert extension to double measurement length.
 - Can better study longitudinal spot merging.
 - Can place two perturbers 90 degrees apart to study lateral spot merging.
- **Improved cone measurements.**
 - Need centerline measurements with a line of PCB132 sensors.
 - Need spanwise measurements.
- **Comparisons to DNS computations.**
- **Iterations with model developers.**