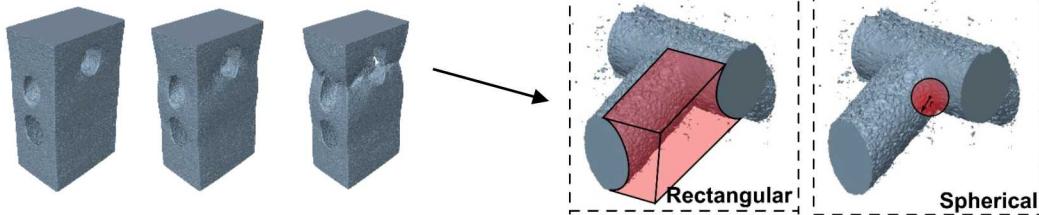
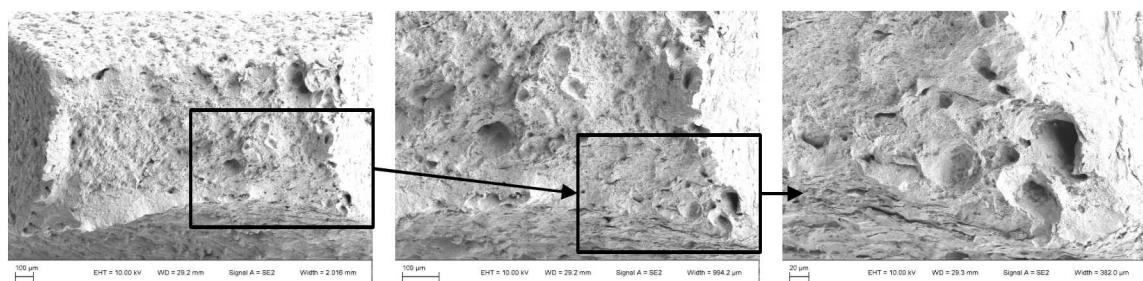


SAND2019-11592PE

Interfaces in Explosively Bonded Stainless Steel



PRESENTED BY

Thomas A. Ivanoff

SolAero Interview
September 24, 2019



Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia LLC, a wholly owned subsidiary of Honeywell International Inc. for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

Outline



About Me

- Education
- Postdoctoral work, technical abilities and projects

Explosive Bonding

Other project highlights (ability to adapt to different material systems)

- Carbon fiber reinforced composite
- Glass-to-metal seals
- Robo-Met.3D® serial sectioning system

Interests

Education



The University of Arkansas – 2008 to 2012

B.S. in Physics

B.S. in Mechanical Engineering

- Research: Tribological study of thin films patterned with Ag nano- rods
- Advisor: Min Zou

The University of Texas at Austin – 2012 to 2017

Advisor: Eric Taleff

M.S. in Mechanical Engineering – 2012 to 2014

- *Retrogression-Reaging and Hot Forming of AA7075*

Ph.D. in Mechanical Engineering – 2014 to 2017

- *Reconstruction of Solidification History from Cast Microstructure in Remelted Nickel Alloy 718*
- Additional projects: Hot forming Ti-6Al-4V

Postdoctoral Work

Sandia National Laboratories (Org. 1851) – January 2018 to Present

Mentor: Jonathan Madison

Manager: Cole Yarrington

Primary Research Focus

Develop and advance three-dimensional (3D) characterization techniques and quantitative assessment metrics. Identify potential applications to leverage 3D data for new insights into materials and support of Sandia's mission.

Technical Abilities

Material Mechanics

Mechanical behavior of materials

Materials processing and Solidification

3D characterization and analysis

Failure analysis

Fundamental R&D

Engineering support

Productivity/Deliverables

5 Journal Publications

- 4 more in progress

9 Technical Conference Presentations

1 Invited Webinar

3 Technical Posters

Personnel Development

Co-mentor: 1 technologist and 3 undergraduate interns

Workflow Optimizations

3D characterization codes

Advanced RoboMet.3D capabilities

Data management workflows

Postdoctoral Work

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Research Collaborations

The Third Sandia Fracture Challenge

Org. 1528

Micro-CT Processing

Org. 1556

Thermal Spray LDRD

Org. 1344

Defect Detection in AM Metals

Org. 1832, Org. 1444, Org. 5264

Org. 1463

Explosive Bonding

Org. 1831

Fiber Reinforced Composites

Org. 1815, Org. 1513

Engineering Support

Glass-to-metal Seals

Org. 2500

Transformers

Org. 2644

Micro-springs

Org. 2613

Inductors

Org. 2641

Ferro-electrics

Org. 2584

Springs

Org. 2641

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Org. 1344

Fiber Reinforced Composites
Org. 1815, Org. 1513

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Glass-to-metal Seals
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Org. 2584

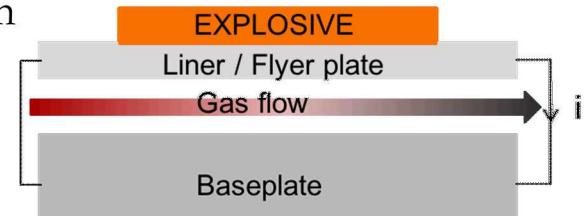
Micro-springs
Org. 2613

Springs
Org. 2641

5 Testing in Extreme Environments with the Z machine

This study explores the use of plastic explosives to close a 6 inch gas flow valve in the Z machine

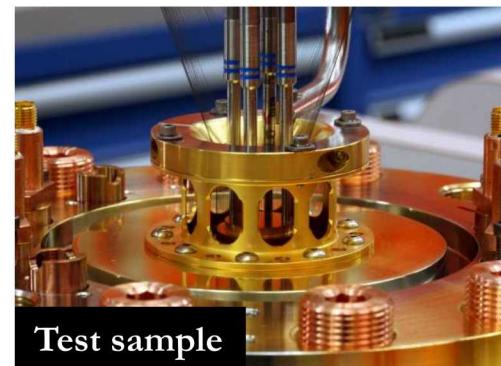
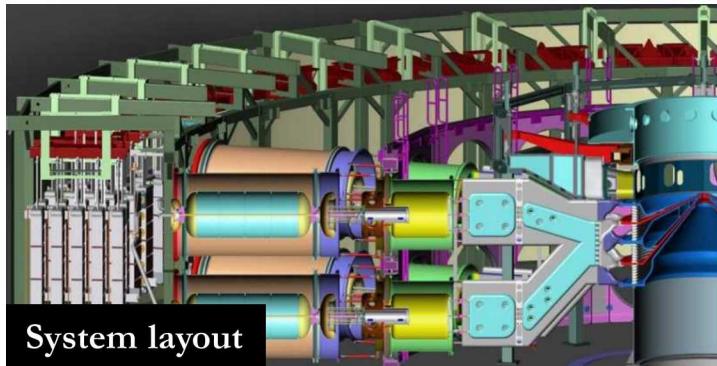
- Precise timing required
- Valve hermetically sealed within $\sim 100 \mu\text{s}$
- Cannot contaminate the test environment



Schematic of explosive closure valve

Z machine at Sandia National Laboratories

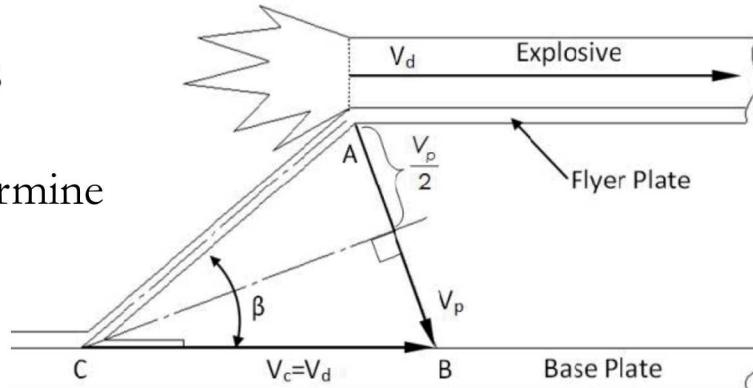
- World's most powerful and efficient laboratory radiation source
- Pulsed power system creates extreme environments for materials testing



Explosive Bonding Parameters

Two primary process parameters determine the quality of a bond

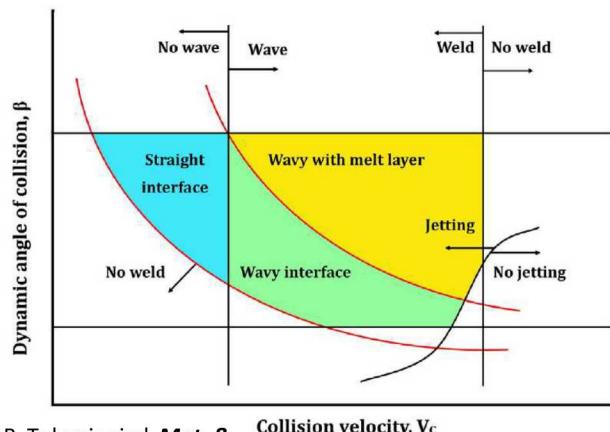
- Collision velocity (V_c)
- Collision angle (β)



J. Ribeiro et al. *J. Phys, Conf. Series*, vol. 500 (2014), pp. 052038.1-6

Ammonium nitrate and fuel oil (ANFO)

- Detonation velocities between 2-3 km/s



M. Athar & B. Tolaminejad, *Mat. & Design*, vol. 86 (2015), pp. 516-525

Z machine requires plastic explosives

- Detonation velocities between 6-7 km/s

Provides over ANFO:

- Cleanliness
- Faster closure speed
- Improved timing

Bonding between two plates. Note incomplete bonding and porosity.

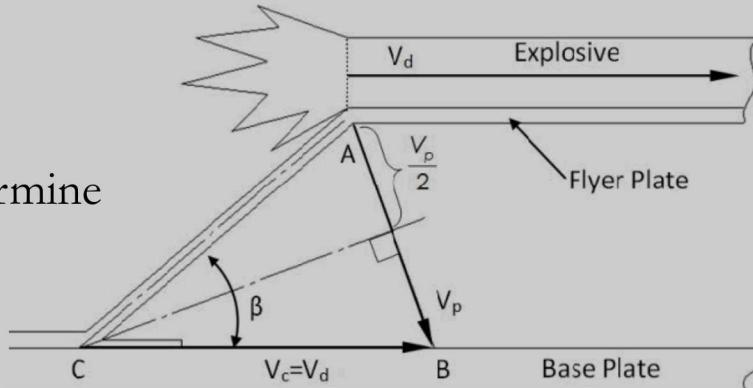


3 mm

Explosive Bonding Parameters

Two primary process parameters determine the quality of a bond

- Collision velocity (V_c)
- Collision angle (β)



J. Ribeiro et al. *J. Phys. Conf. Series*, vol. 500 (2014), pp. 052038.1-6

Ammonium nitrate and fuel oil (ANFO)

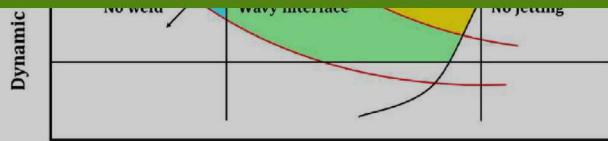
Z machine requires plastic explosives

Characterize bond interfaces in 304L stainless steel plates explosively bonded using plastic explosives using:

Metallography and fractography

Three-dimensional reconstructions from micro-computed tomography

Mechanical testing (lap-shear, microhardness)



M. Athar & B. Tolaminejad, *Mat. & Design*, vol. 86 (2015), pp. 516-525

Bonding between two plates. Note incomplete bonding and porosity.

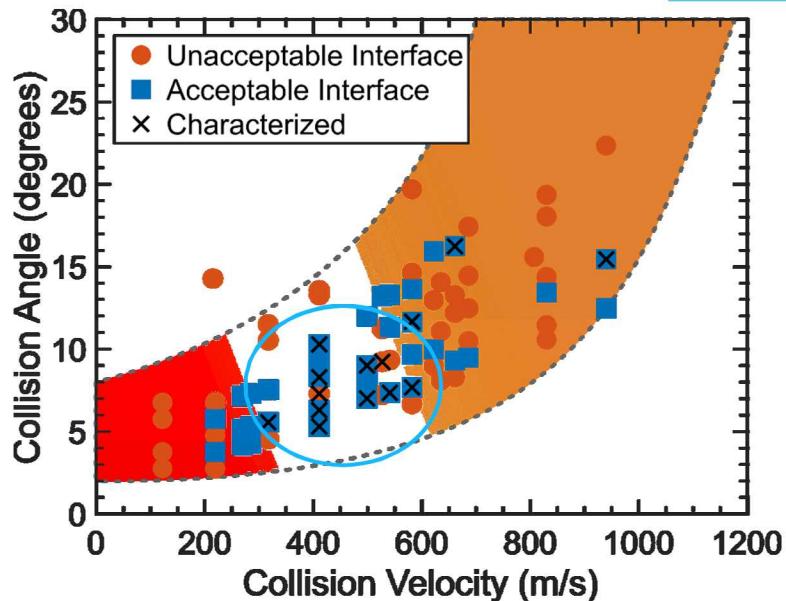


Experimental Setup

Varied Collision angle and velocity

- 15 “acceptable” process settings studied in detail

Each plate sectioned after bonding for micro-computed tomography (μ CT) and mechanical testing



Explosive bonding :

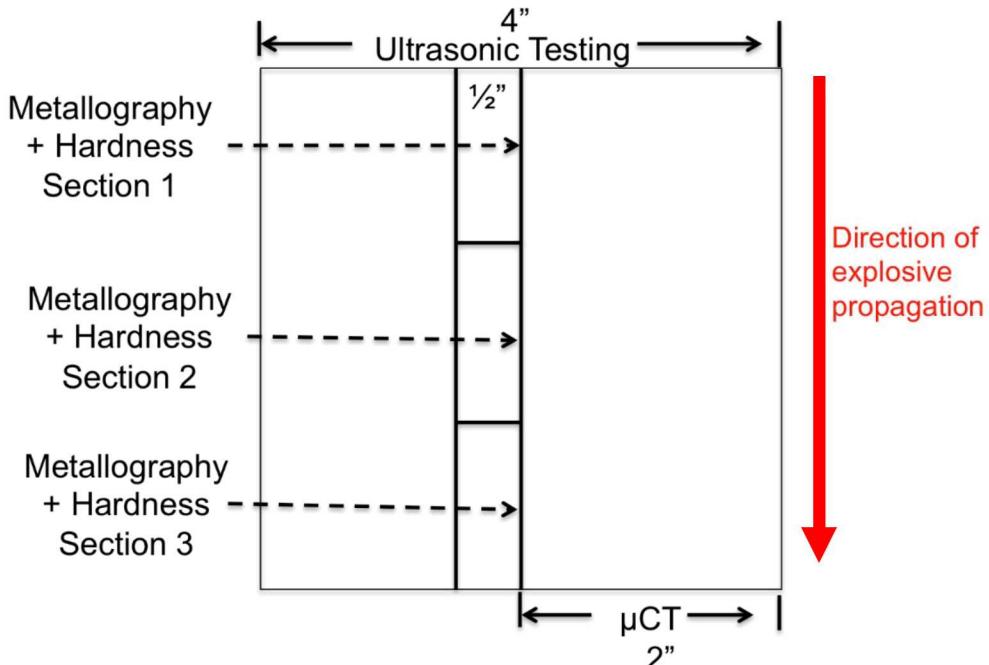
Wvenner Saul and Lloyd Payne

Experimental Setup

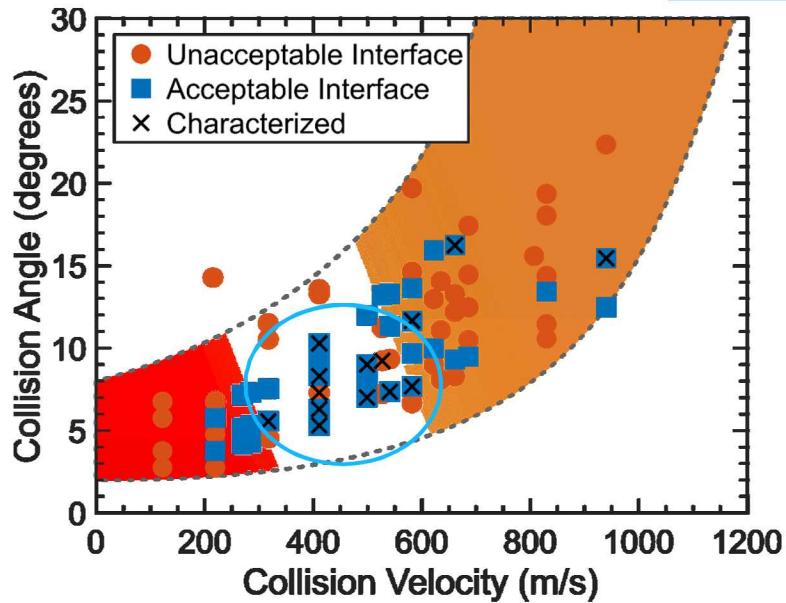
Varied Collision angle and velocity

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Each plate sectioned after bonding for micro-computed tomography (μ CT) and mechanical testing



Schematic of the bonded plates demonstrating how material was sectioned for different characterizations.

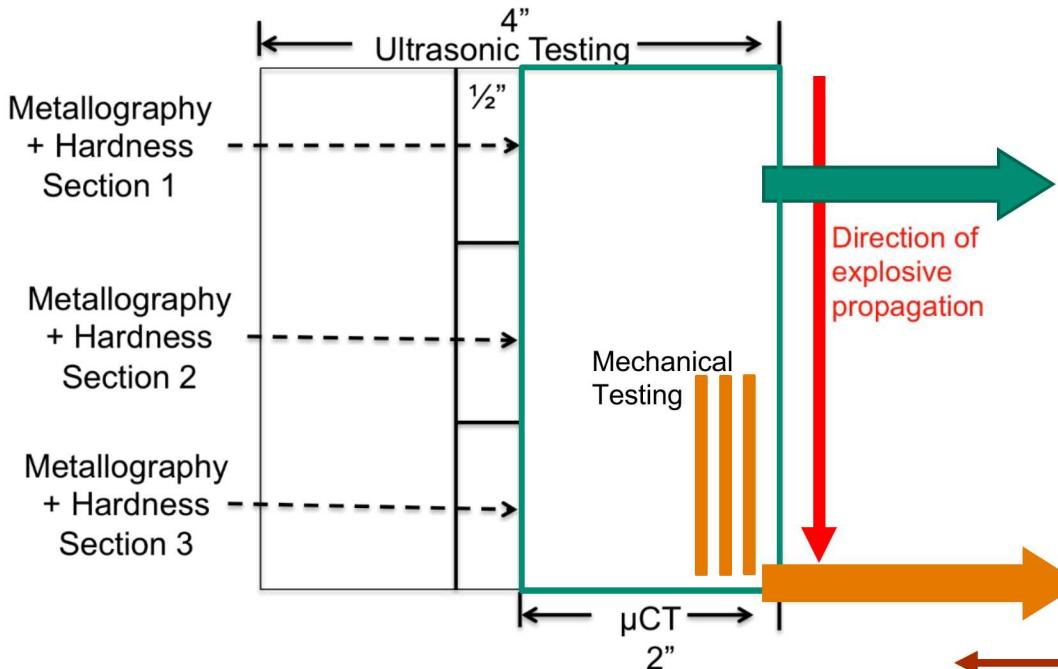


Experimental Setup

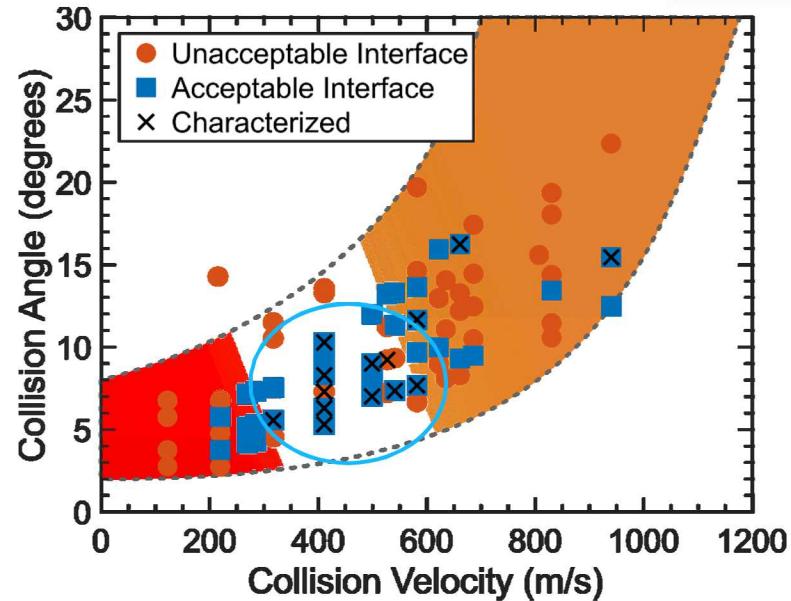
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Schematic of the bonded plates demonstrating how material was sectioned for different characterizations.



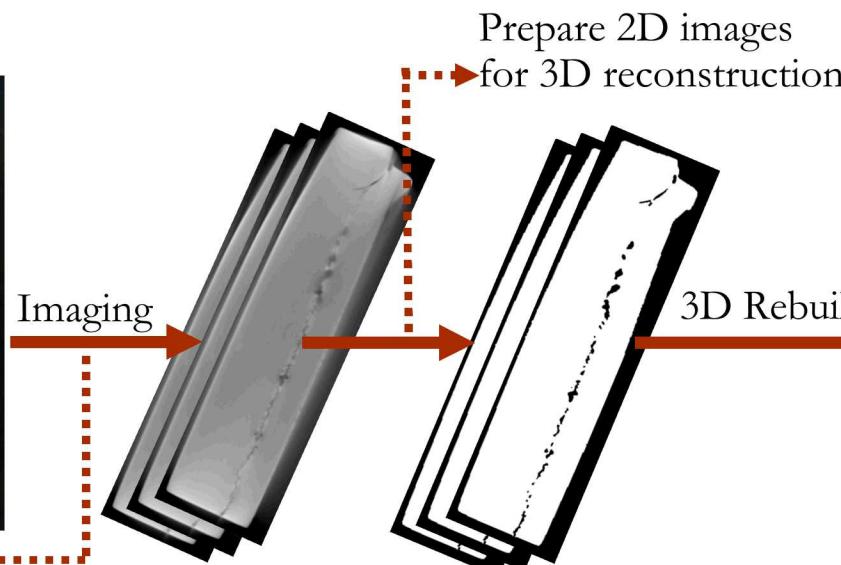
Bonded plates characterized using μ CT



Lap-shear test specimen
Loading direction

8 3D Reconstruction Method

Part to be reconstructed

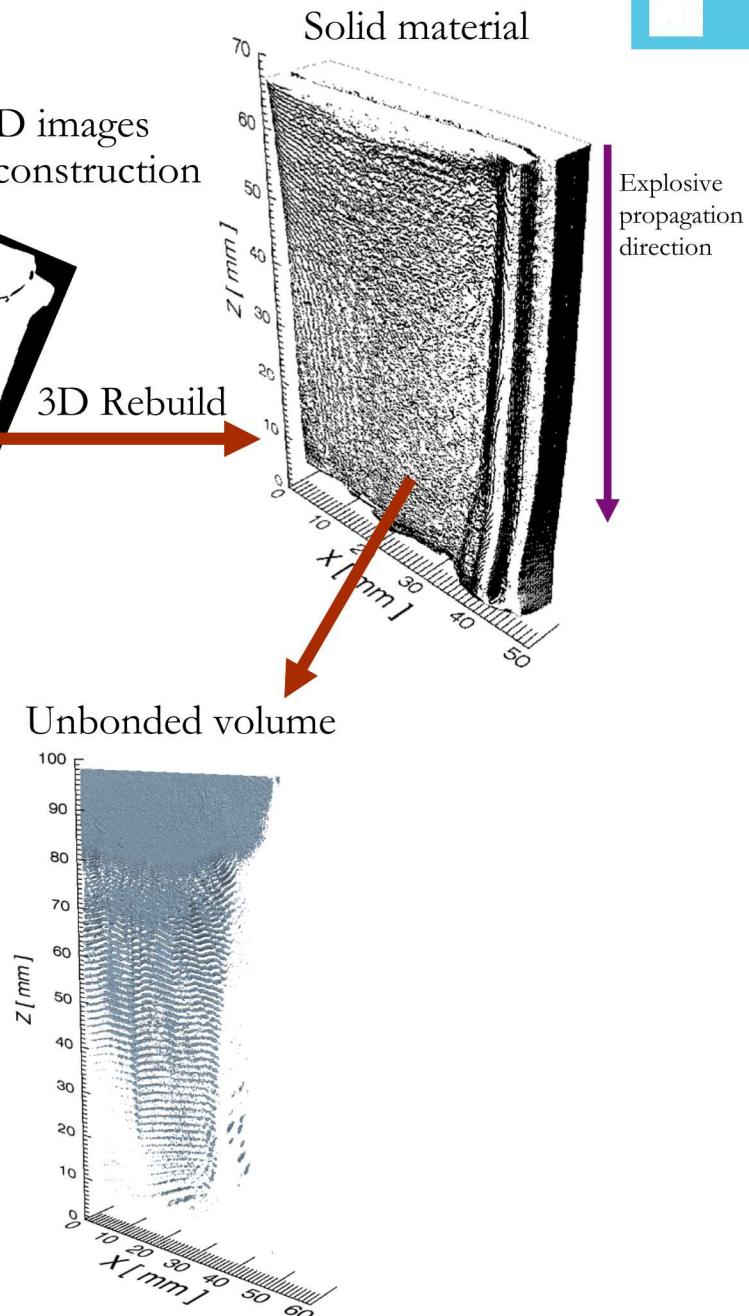


Non-destructive

- Micro-computed tomography



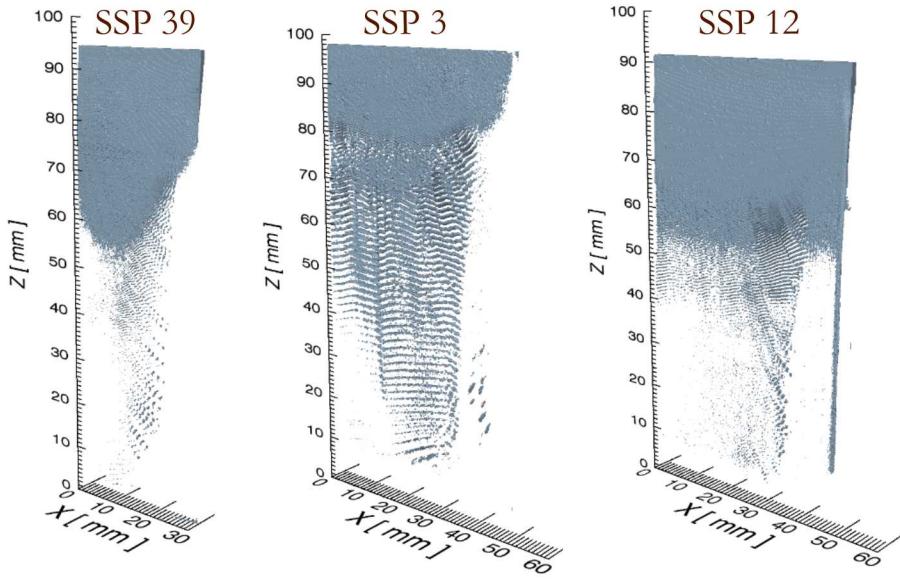
Nikon Avonix M2 225/450 kV
Helical Scanner



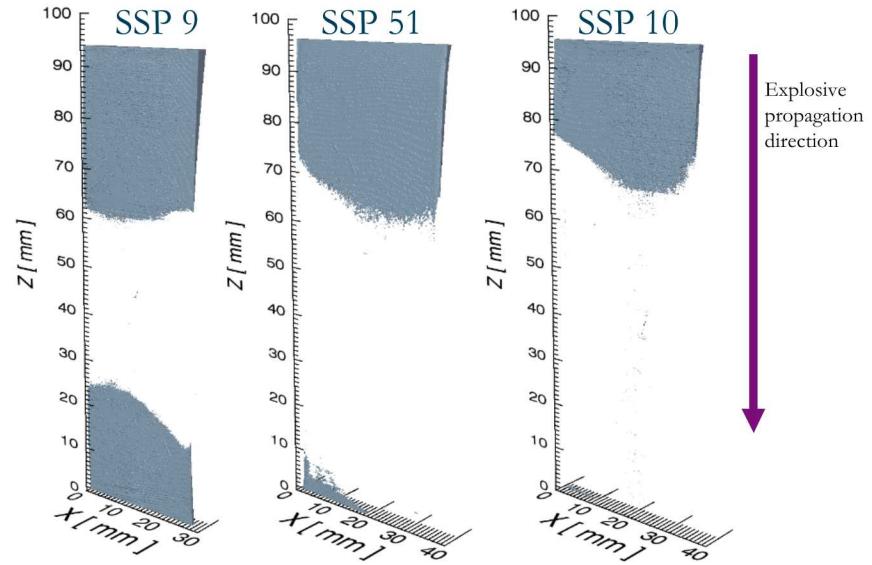
3D Reconstruction of Unbonded Volumes



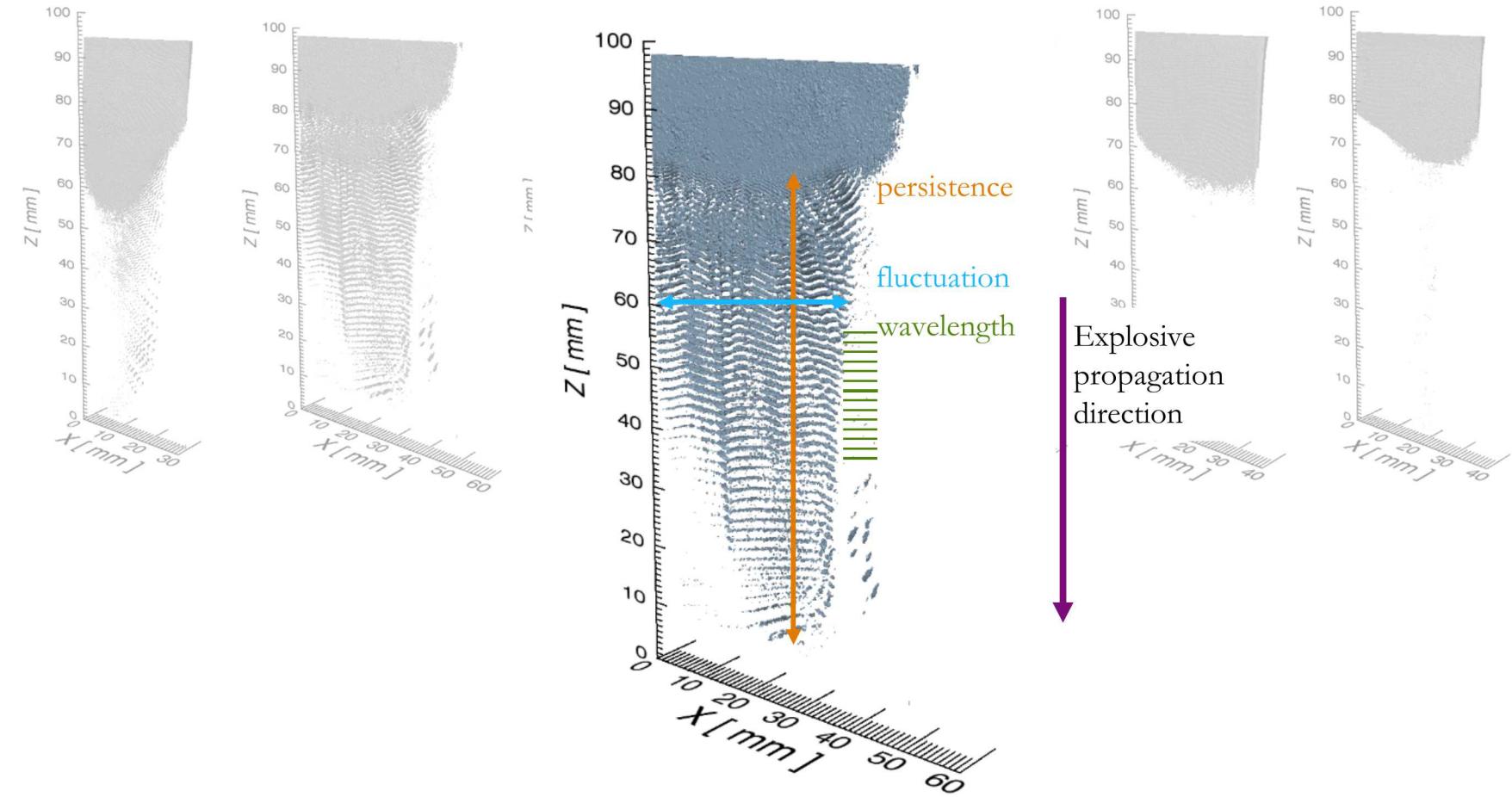
Porous bond interfaces



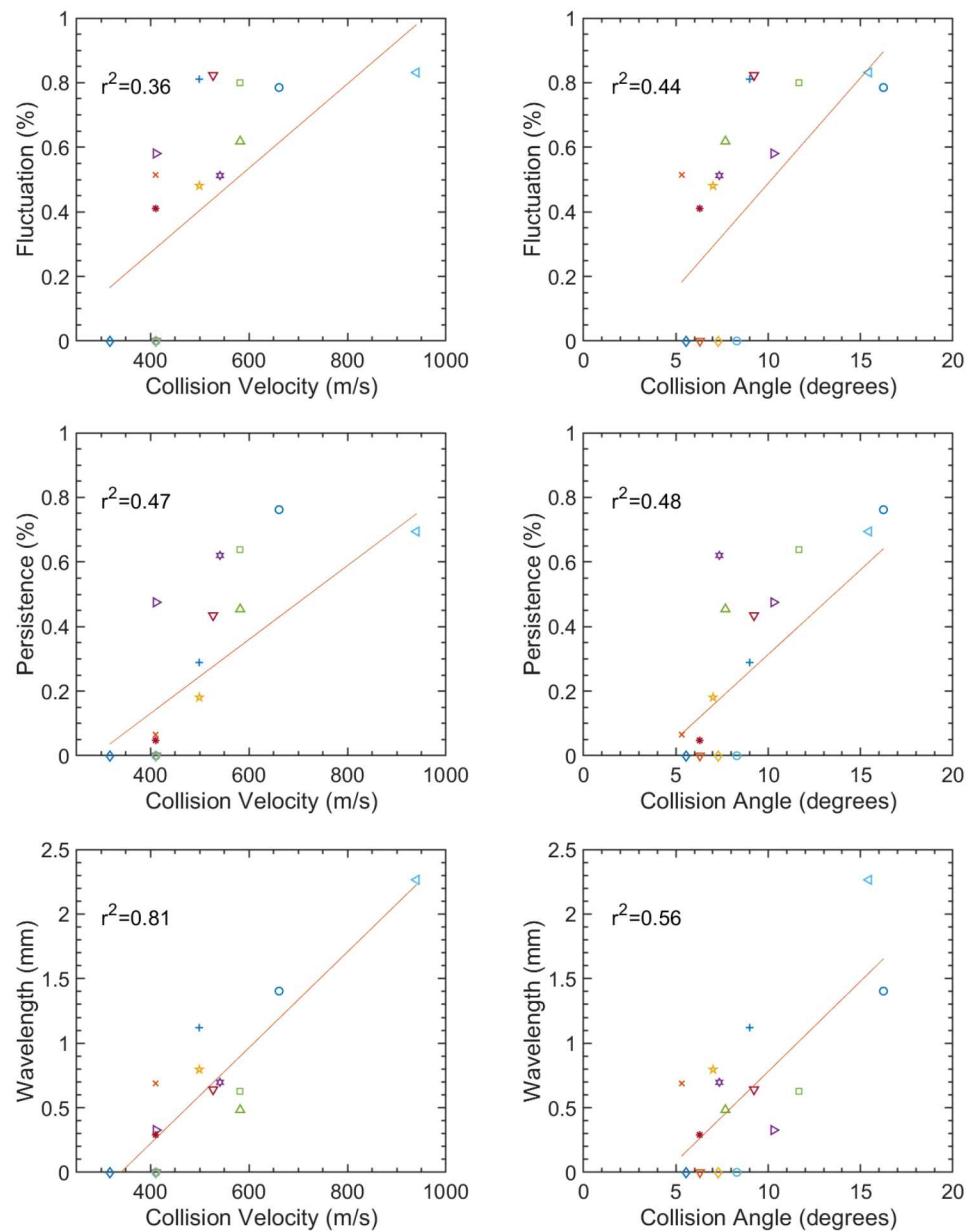
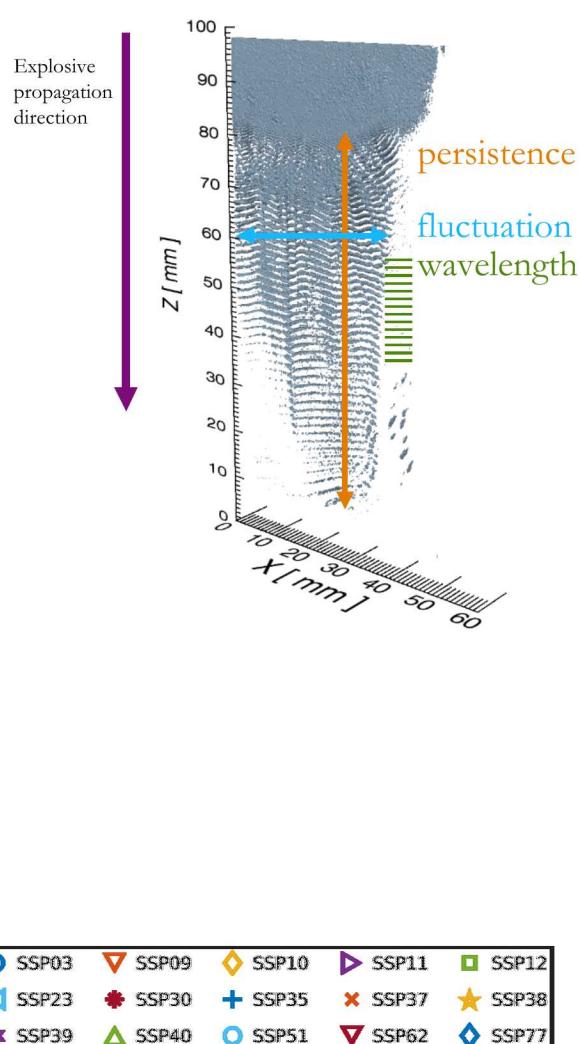
Solid bond interfaces



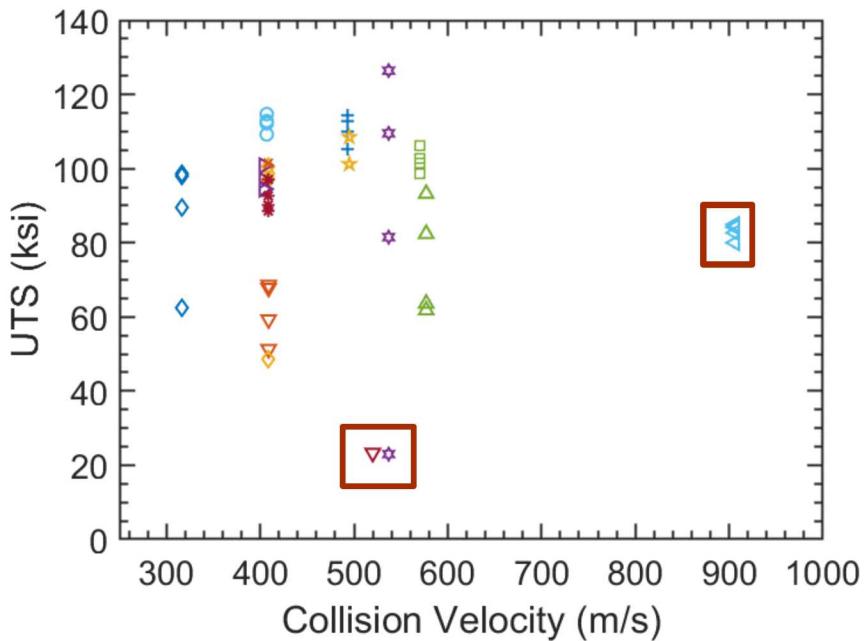
3D Reconstruction of Unbonded Volumes



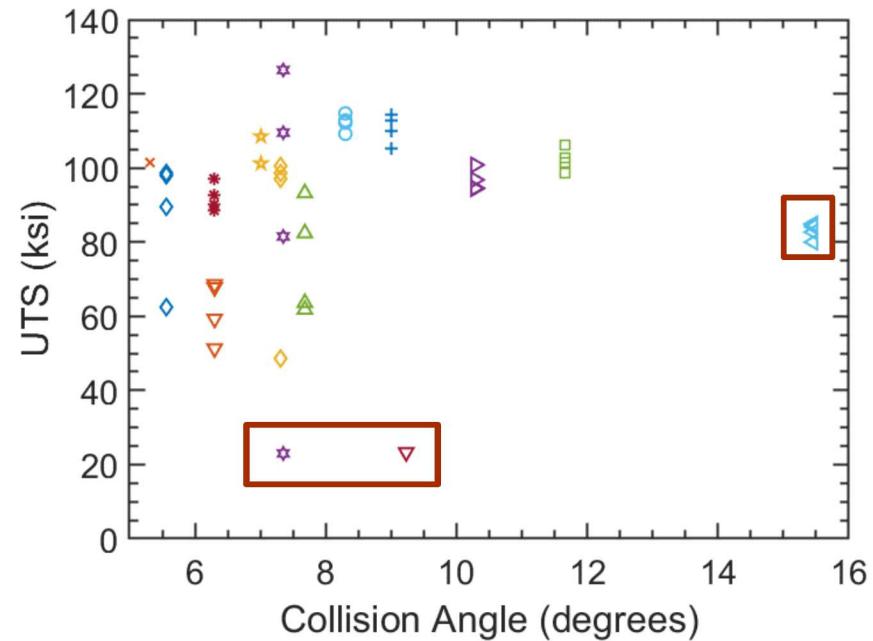
Process Parameter Relationship with Bond Character



UTS from Lap-shear Tensile Tests



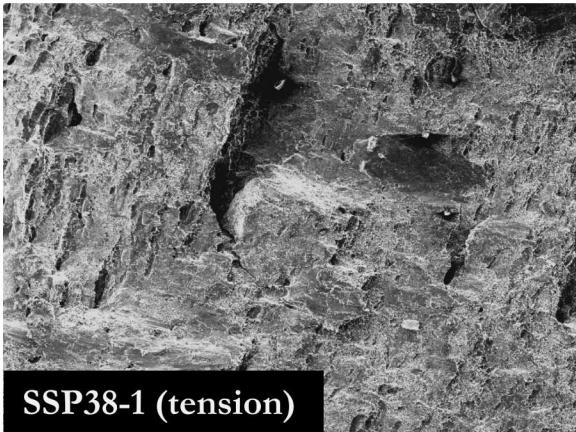
Trends are weak between UTS and collision velocity, collision angle



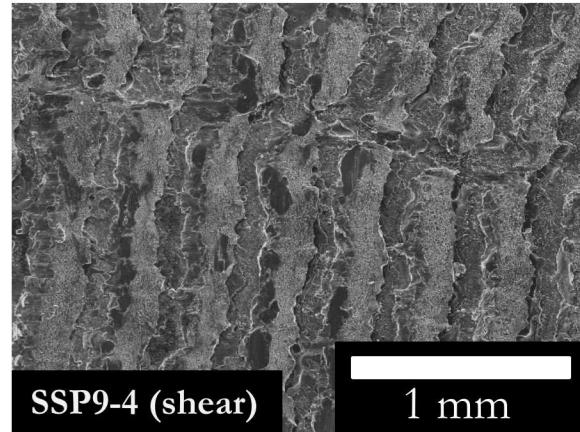
Outliers mask potential relationships

Fractography

Failure in parent material



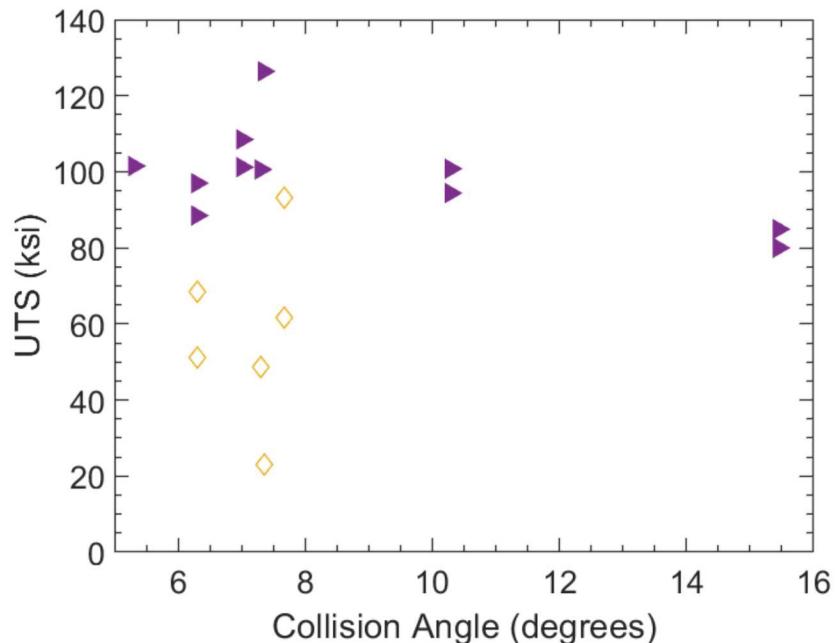
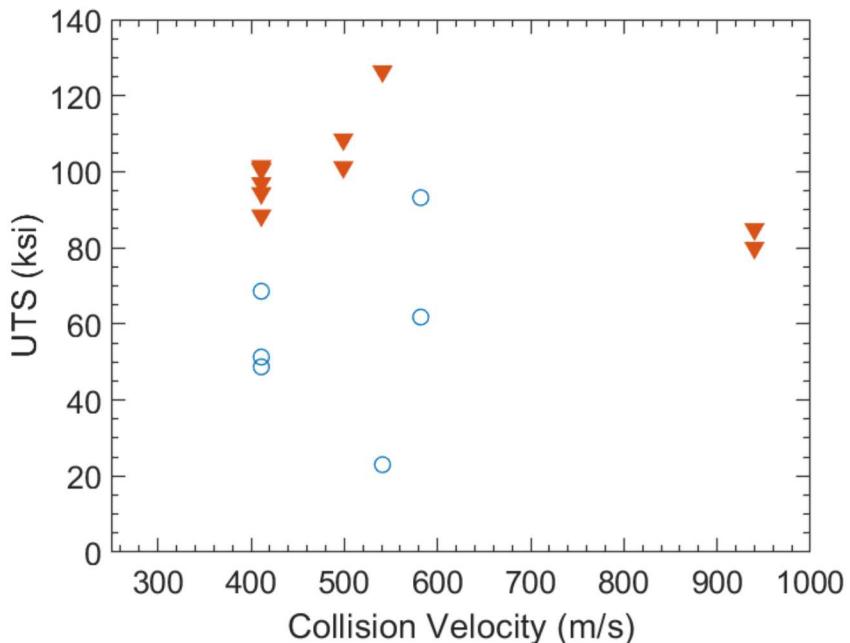
Failure along interface



1 mm

UTS from Lap-shear Tensile Tests

Filled symbols failed in **Parent Material**
Open symbols failed along **Interface**



1. Material that failed along interface exhibits no trends
2. UTS shows a relationship with collision velocity for parent material failures

Conclusions

Determined process parameters for bonding using plastic explosives that produce hermetically sealed interfaces in 304L stainless steel plate

- Processing window is narrower than that for ANFO

Overall, bonds demonstrate significant variability in porosity content and strength along the bond length and width

Utilizing multiple characterizations (global or local) can reveal trends and expertise in characterization and analysis can clarify interpretation of complex results

Microstructure of Fiber Reinforced Composite

CHALLENGE

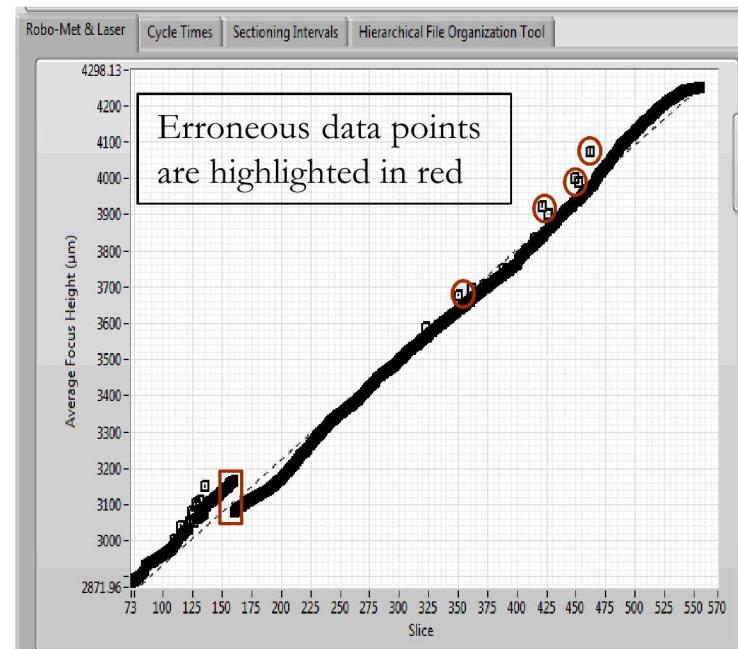
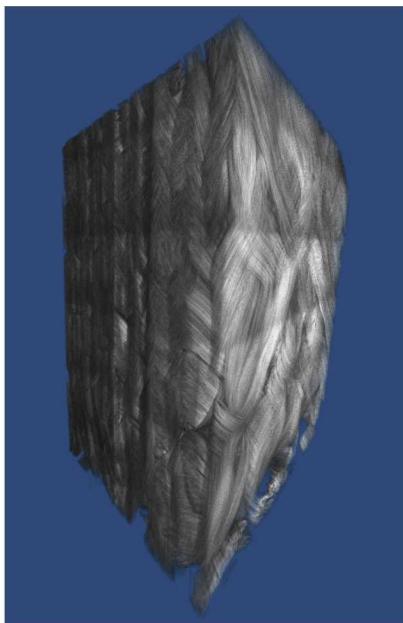
Characterize structure of a woven carbon fiber matrix. Identify **(1) long-range weave pattern** and porosity, **(2) distribution of fibers** within a single weave and **(3) individual fibers**.

FIBER DETAILS

Total volume examined is 10x9x6 mm. Individual fibers are ~ 5 μm in diameter.



Section of the fiber reinforced composite for serial sectioning.



Microstructure of Fiber Reinforced Composite



CHARACTERIZATION

Optical microscopy (5X), 4 x 6 montage, 931 slices (9000x9600 pixels)

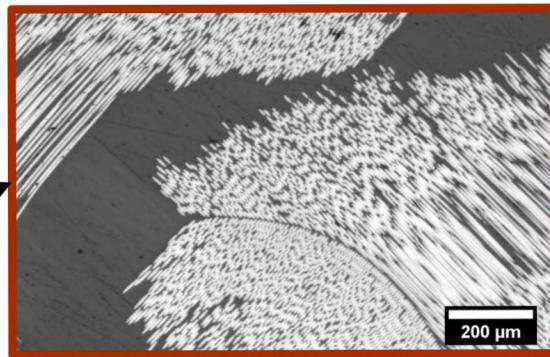
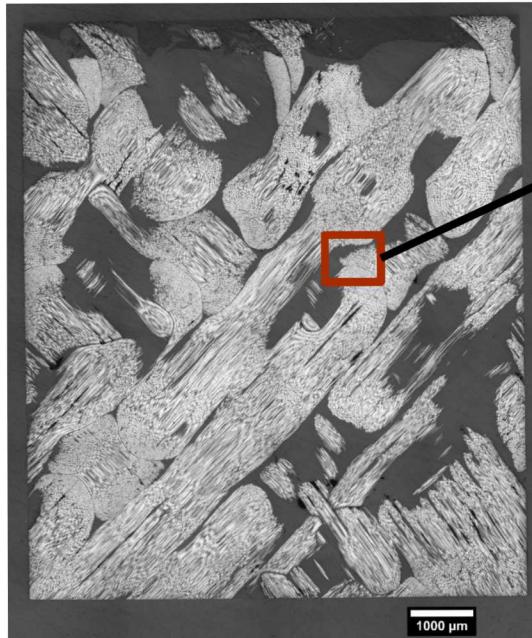
RECONSTRUCTION & ANALYSIS

Matlab and FIJI

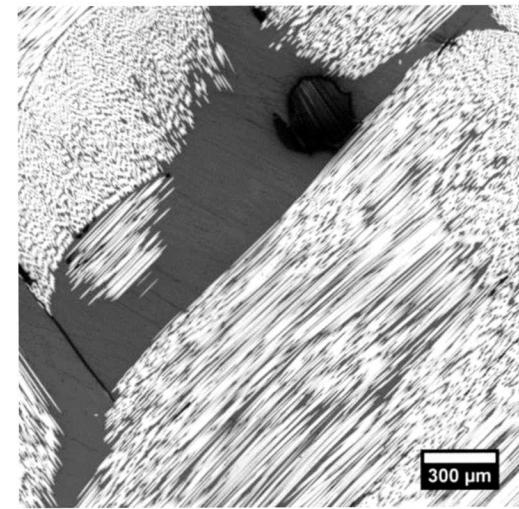
- *Image Processing*
- *Volumetric Analysis*

INSIGHTS

- Largest pores exists between the fiber weaves, but porosity still exists within individual weaves.
- Fiber distribution changes when weaves contact/impede each other



Fiber distributions change throughout weaves depending on interaction with other weaves



Cracks in Glass-to-metal Seals

CHALLENGE

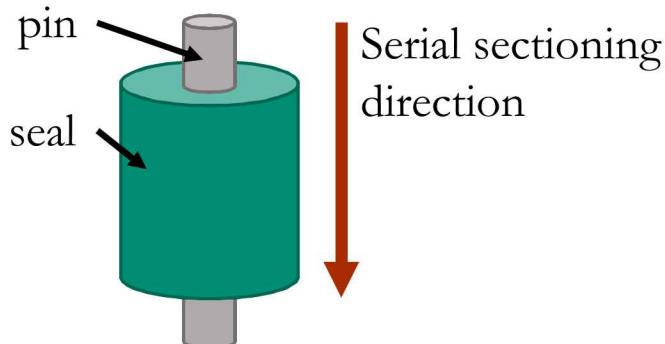
Determine extent of cracking in glass-to-metal seals and optimal method for inspection

DETAILS

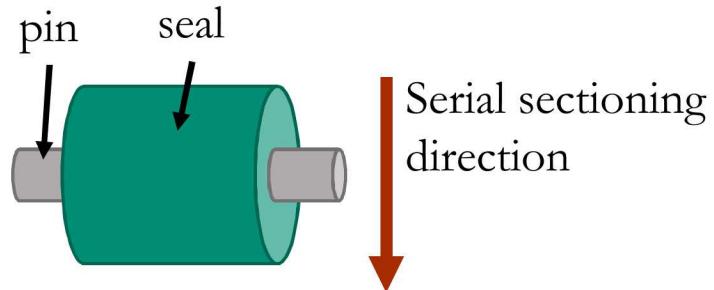
Seals are surrounded by a metal housing; significant residual stress is present in the seal after manufacture

True size/character of cracks cannot be identified without mechanical sectioning; preparing a single plane does not identify crack evolution.

Transverse Mount



Longitudinal Mount

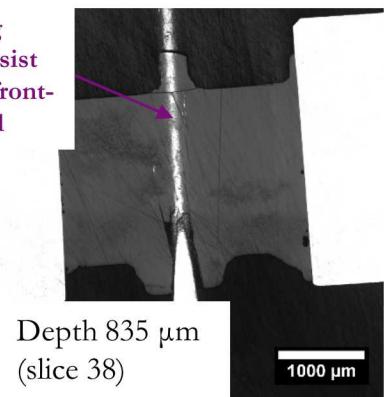
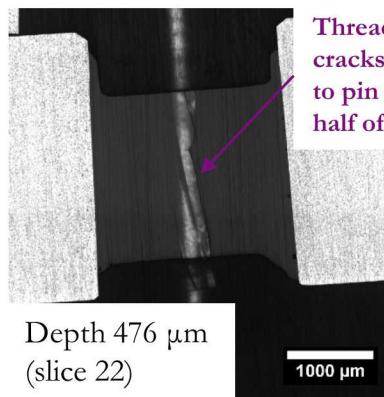
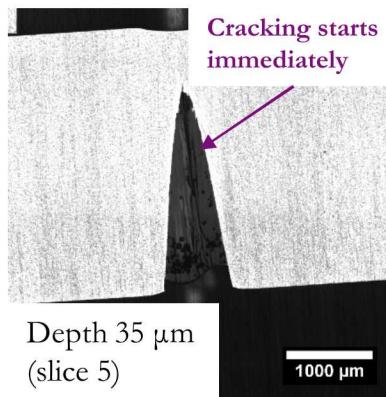
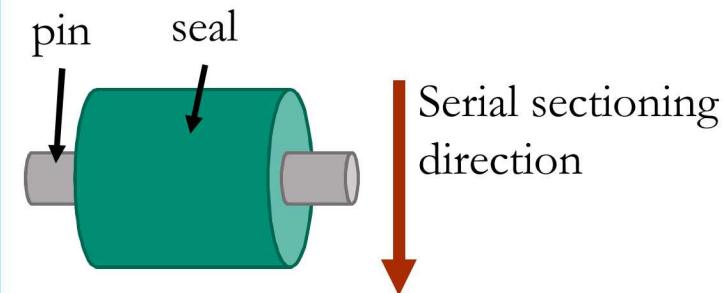


Cracks in Glass-to-metal Seals

Mechanical polishing effects cracks when mounted longitudinally.

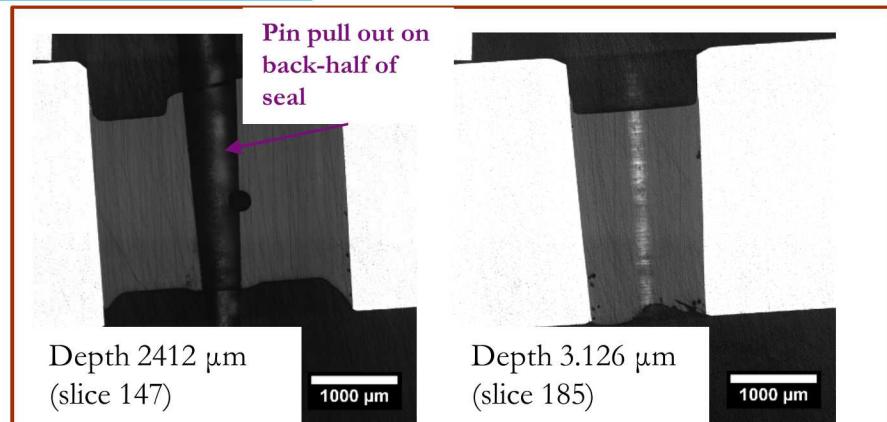
Cracks are opened on the front half of the pin but the bottom half of the pin exhibits less cracking.

Longitudinal Mount

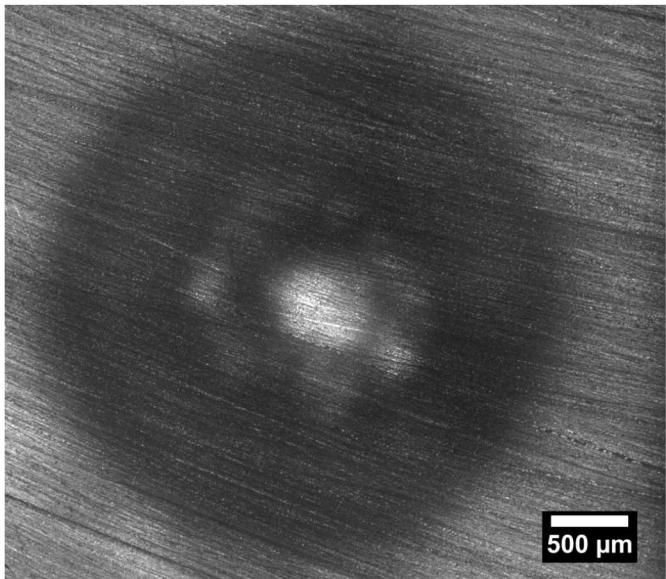


Back half of seal

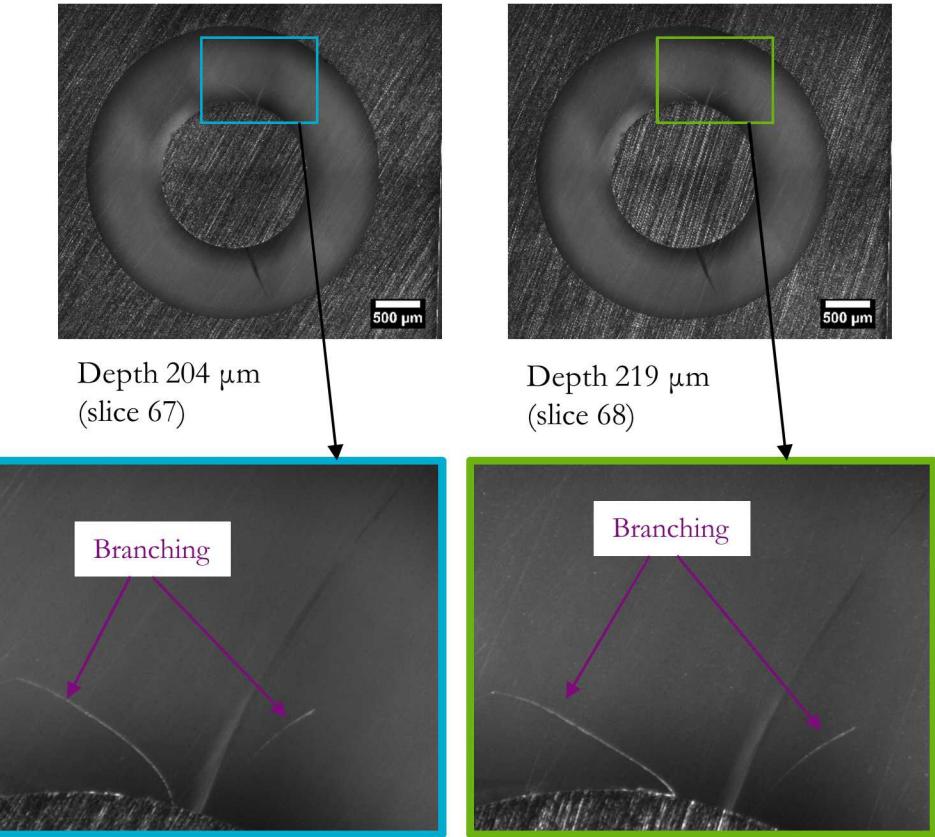
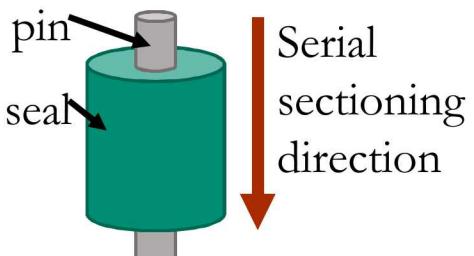
Front half of seal



Cracks in Glass-to-metal Seals



Transverse Mount



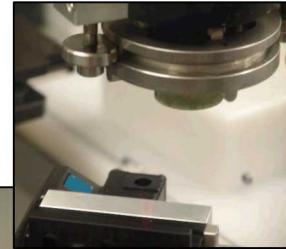
500 μm

Scale bar for enlargements

Robo-Met.3D

Robo-Met.3D is a fully automated characterization technique for 3D investigations of microstructure using mechanical serial sectioning

- Serial sectioning is the removal of material layer-by-layer and then optical imaging
- Robo-Met.3D provides 3D reconstructions of microstructure across volumes of cubic millimeters at resolutions of microns.



System Components

Automated robotic polisher with variable polishing wheel

Automated high resolution inverted microscope with montage imaging

Dual internal ultrasonic cleaning stations

Three internal compact chemical etching stages

External operator station for real-time observation of data collection

Imaging & Resolution

5X	--	2.10 um/pixel
10X	--	1.05 um/pixel
20X	--	0.53 um/pixel
50X	--	0.21 um/pixel



Benefits

Sectioning rates up to 10 times the baseline manual process

Elimination of variability caused by human handling or error due to automated handling of specimens

Precise repeatability and command over imaging location, illumination, contrast, exposure and feature focus

Demonstrated repeatable sectioning thicknesses from 0.2 – 10 mm per slice

Documented slice rates of up to 20 slices per hour

Applicable to high and low strength metals (e.g. Al, Cu, Ti, Steel, Ni), thermal spray & geology samples

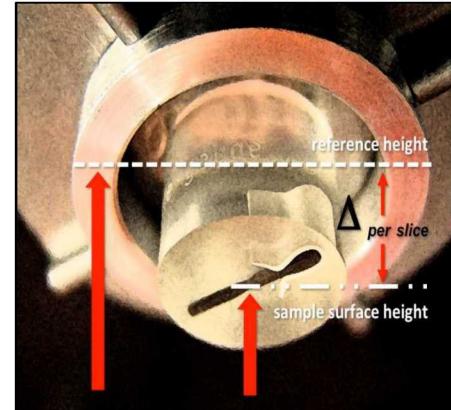
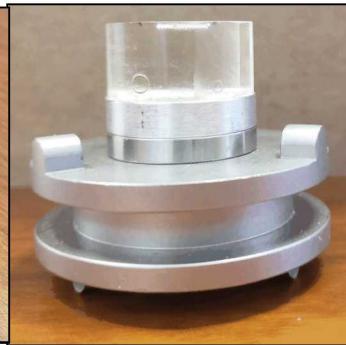


**Sandia
National
Laboratories**

Robo-Met.3D System Advances

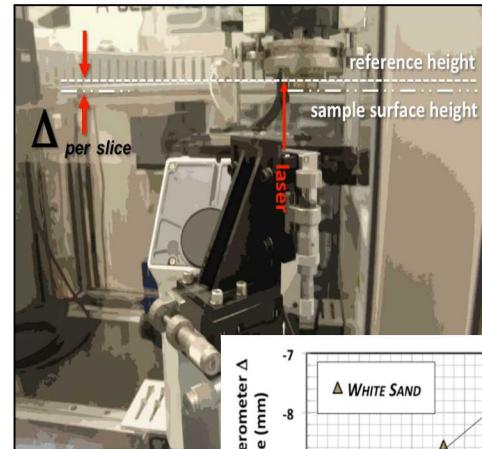
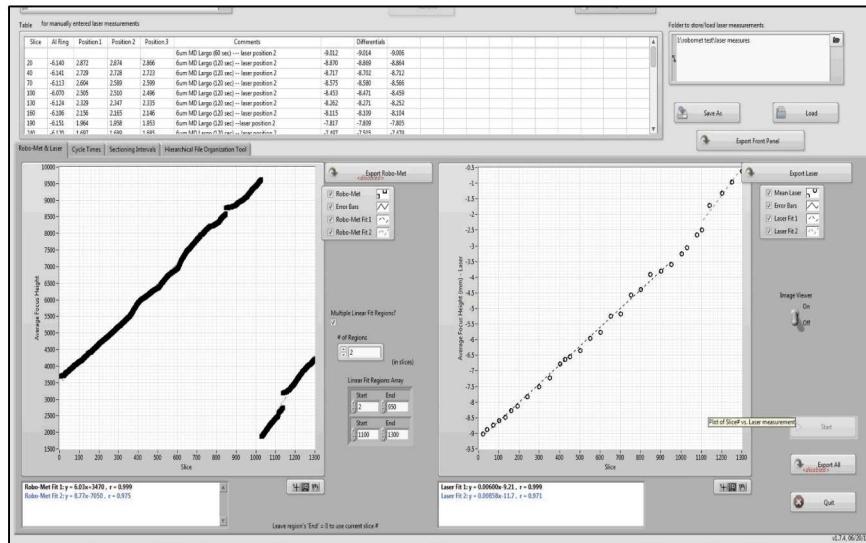


Kinematic specimen holder



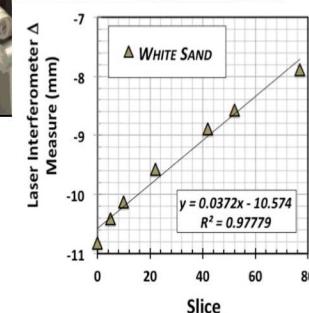
SANDIA TECHNICAL ADVANCE SD#13739

D.O.E. Commercial Software Copyright - J.D. Madison, G.A. Poulter, E.M. Huffman, DoE Commercial Software Copyright, SCR 2075.0 - 'Mechanical Serial-Sectioning Data Assistant (MECH-SSDA) v1.3'



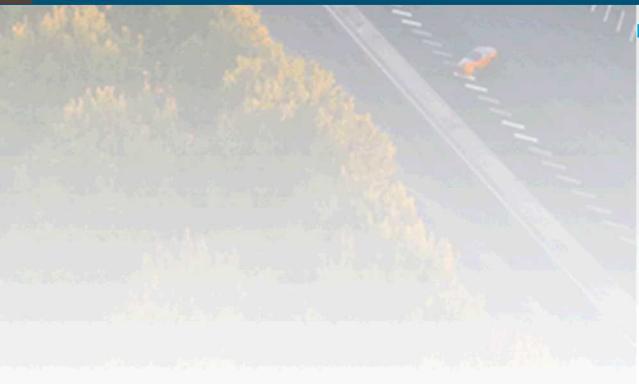
SANDIA TECHNICAL ADVANCE SD#13742

U.S. Patent No. 10,260,865 - J.D. Madison, E.M. Huffman, "HIGH RESOLUTION, NON-CONTACT REMOVAL RATE MODULE FOR SERIAL SECTIONING", issued April 16, 2019, SD13742.1/S142462





Questions



Publications

T. A. Ivanoff, T. J. Watt, and E. M. Taleff. “Characterization of Solidification Microstructures in Vacuum Arc Remelted Nickel Alloy 718,” *Metallurgical and Materials Transactions B*, vol. 50, no. 2, 2019, pp. 700-715.

T. A. Ivanoff, J. T. Carter, L. G. Hector, and E. M. Taleff. “Retrogression and Reaging Applied to Warm Forming of High-strength Aluminum Alloy AA7075-T6 Sheet,” *Metallurgical and Materials Transactions A*, vol. 50, no. 3, 2019, pp. 1545-1561.

J. A. Mitchell, **T. A. Ivanoff**, D. Dagel, J. D. Madison, and B. H. Jared “Linking Pyrometry to Porosity in Additively Manufactured Metals,” *Additive Manufacturing*, 2019, pp. 1-2.

- Accepted with revisions

S. L. B. Kramer, **T. A. Ivanoff**, J. D. Madison, and A. P. Lentfer. “Evolution of Damage in an Additively Manufactured 316L SS Structure: experimental reinvestigation of the third Sandia Fracture Challenge,” *International Journal of Fracture*, vol. 218, no. 1-2, 2019, pp. 63-84.

S. L. B. Kramer, ..., **T. A. Ivanoff**, ..., et. al. “The Third Sandia Fracture Challenge: predictions of ductile fracture in additively manufactured metal,” *International Journal of Fracture*, vol. 218, no. 1-2, 2019, pp. 5-61.

N. M. Heckman, **T. A. Ivanoff**, A. M. Roach, B. H. Jared, J. Rodelas, D. J. Tung, H. J. Brown-Shacklee, T. Huber, D. J. Saiz, J. R. Koepke, J. D. Madison, B. C. Salzbrenner, L. P. Swiler, R. Jones, B. L. Boyce. “Robust processing parameters for additively manufactured 316L stainless steel revealed through high-throughput tensile testing.”

- Submitting

T. A. Ivanoff, O. Underwood, J. D. Madison, L. Deibler, J. Rodelas, C. Finfrock, “Influence of Processing Parameters on Interface Character and Bond Quality in Explosively Bonded 304L Stainless Steel.”

- In progress

T. A. Ivanoff, J. A. Mitchell, J. D. Madison, D. Dagel, D. Saiz, J. R. Koepke and B. Jared. “Correlation of In-situ Thermal Pyrometry Signatures with Porosity Defects in Additively Manufactured 316L Stainless Steel.”

- In progress

T. A. Ivanoff and J. D. Madison. “Influence of Segmentation on the Quantitative Analysis of Three-dimensional Characterizations,”

- In progress

Technical Presentations

T. A. Ivanoff, J. D. Madison, N. W. Moore, and A. Olson. “Three-Dimensional Characterization of Microstructure and Elemental Segregation of Thermal Spray Coatings,” TMS 149th Annual Meeting & Exhibition (TMS 2020), San Diego, CA, February 2020.

- **Abstract Accepted**

T. A. Ivanoff, J. A. Mitchell, J. D. Madison, D. Dagel, D. Saiz, J. R. Koepke and B. Jared. “Correlation of Porosity Defects with In-situ Pyrometry in AM316L Stainless Steel,” MS&T 2019, Portland, OR, September – October 2019.

- **Monday September 27th**

T. A. Ivanoff, S. L. B. Kramer, J. D. Madison and A. P. Leftner. “3D Characterizations of Internal Porosity and Surface Topology and Their Influence on Local Fracture Behavior in AM 316L Stainless Steel,” Solid FreeForm Fabrication 2019, Austin, TX, August 2019.

T. A. Ivanoff, O. D. Underwood, J. D. Madison. “Three-dimensional Materials Science and Mechanical Serial Sectioning for Characterization of Microstructure,” ASM Webinar sponsored by UES, July 2019.

T. A. Ivanoff, O. D. Underwood, J. Madison, L. A. Deibler, and J. Rodelas, “Characterization of Interfacial Bond Surfaces in Explosively Bonded 304L Stainless Steel,” *2019 TMS Annual Meeting & Exhibition, Characterization of Minerals, Metals, and Materials*, San Antonio, TX, March 2019.

T. A. Ivanoff, J. D. Madison, J. R. Koepke, and B. H. Jared, “Assessing the Impact of Image Acquisition and Processing Methods on Three-Dimensional Microstructural Reconstructions”, *Materials Science & Technology Technical Meeting and Exhibition (MS&T 2018)*, Columbus, OH, October 2018.

T. A. Ivanoff, J. D. Madison, J. R. Koepke, E. Schwaller, B. H. Jared, J. A. Mitchell, and L. P. Swiler, “Three-Dimensional Registration of Part Design, Melt Pool History and Resultant Structure in Additively Manufactured 316L Stainless Steel”, *Materials Science & Technology Technical Meeting and Exhibition (MS&T 2018)*, Columbus, OH, October 2018.

T. A. Ivanoff, J. D. Madison, J. R. Koepke, B. H. Jared, J. A. Mitchell, and L. P. Swiler, “Three-Dimensional Characterization of Porosity Defects and their Correlation to Mechanical Properties in AM 316L Stainless Steel”, *29th Annual International Solid Freeform Fabrication Symposium- An Additive Conference*, Austin, TX, August 2018.

T. A. Ivanoff, T. J. Watt, and E. M. Taleff, “Digital Image Analysis for the Automated Measurement of Dendritic Microstructures in Vacuum Arc Remelted Nickel Alloy 718,” *TMS 2018 Annual Meeting & Exhibition*, Phoenix, AZ, March 2018.

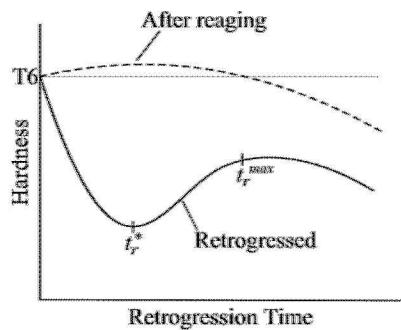
Education

Retrogression-Reaging and Hot Forming of AA7075

- Developed a new forming approach for high-strength aluminum alloy AA7075 for General Motors

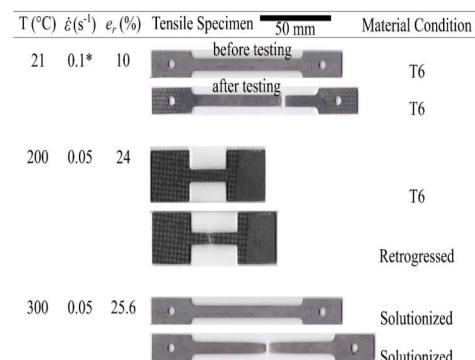
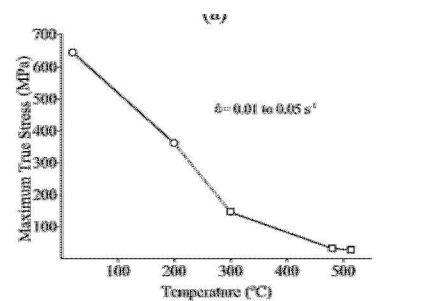
1

Adapt existing knowledge of RRA treatments to enable new processing technologies



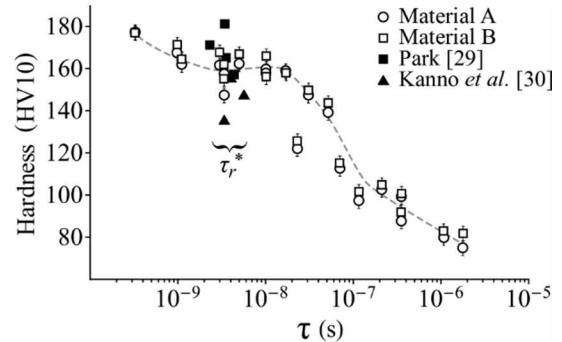
2

Evaluate mechanical response to treatment and relate to microstructure



3

Relate performance to microstructure



Arrhenius relationship for hardness with temperature-dependent retrogression time using diffusion rate for Zn

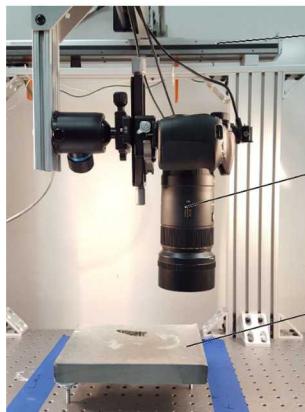
Testing on MTS load frames
Simulated forming conditions

Reconstruction of Solidification History from Cast Microstructure in Remelted Nickel Alloy 718

- Provided data for validation of a Nickel remelting model for AFRL and the LMPC

1

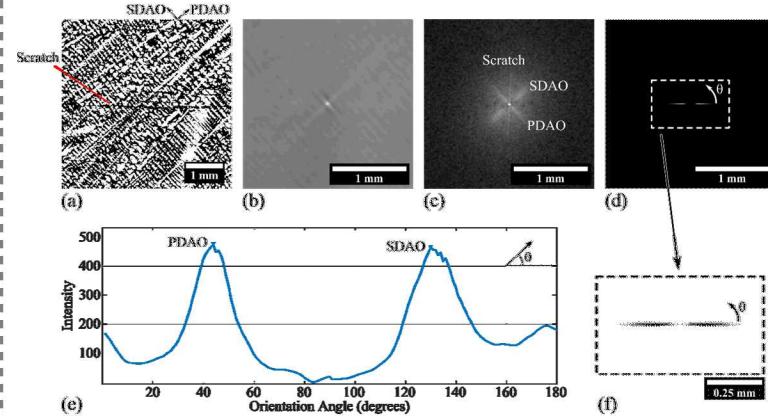
Determined validation data required for model and designed/implemented hardware



Mentored 2 undergraduates
(Katie Adams, Mykal Madrid)

2

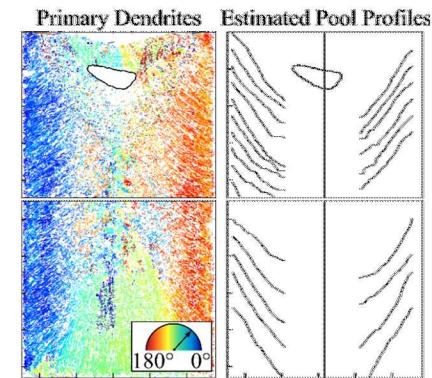
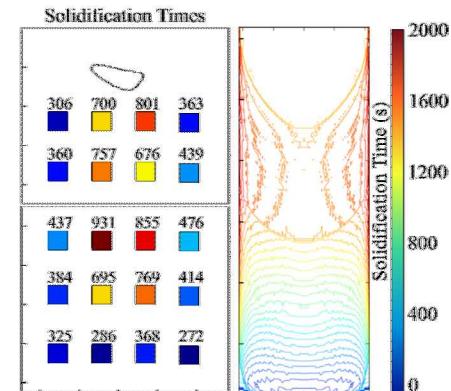
Developed automated analysis methods to quantitatively assess microstructures



Two-point correlation function

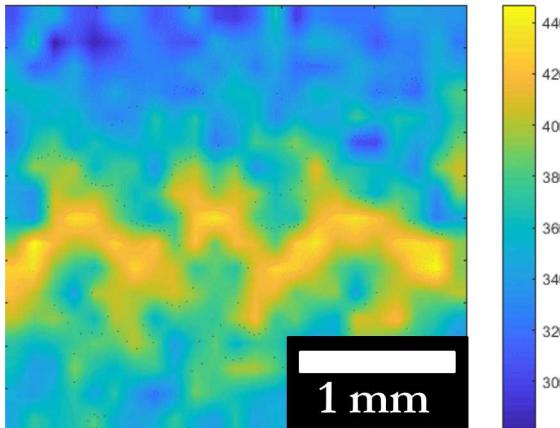
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Validate computational models

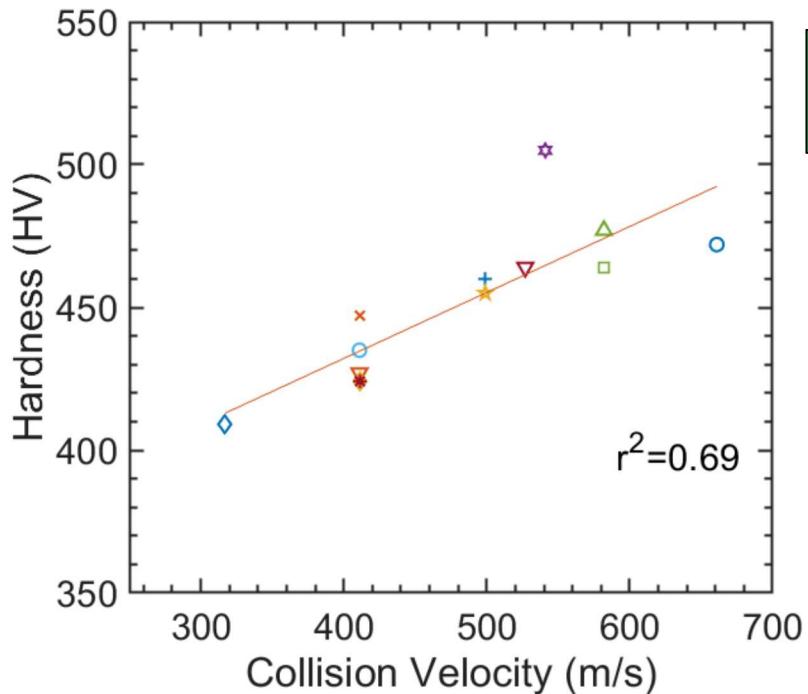


Vickers Microhardness

Study local hardness variation across the bond interface and into the parent material

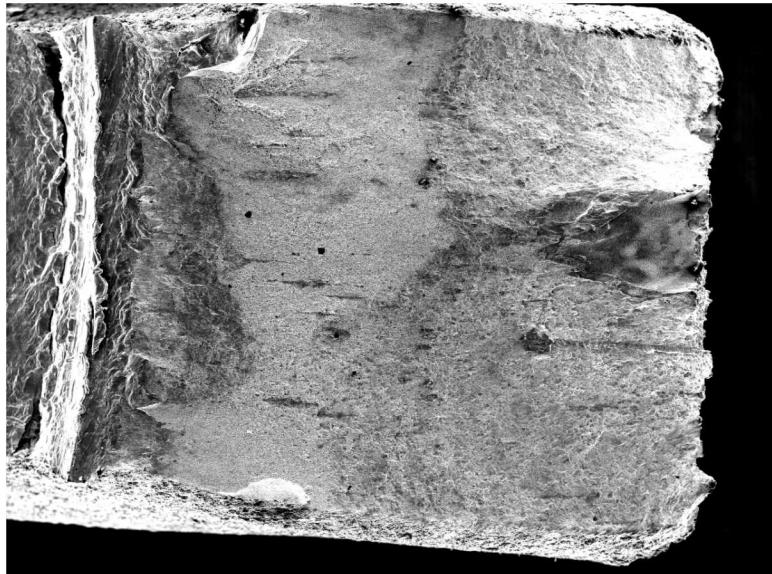


Relate peak hardness to processing parameters:

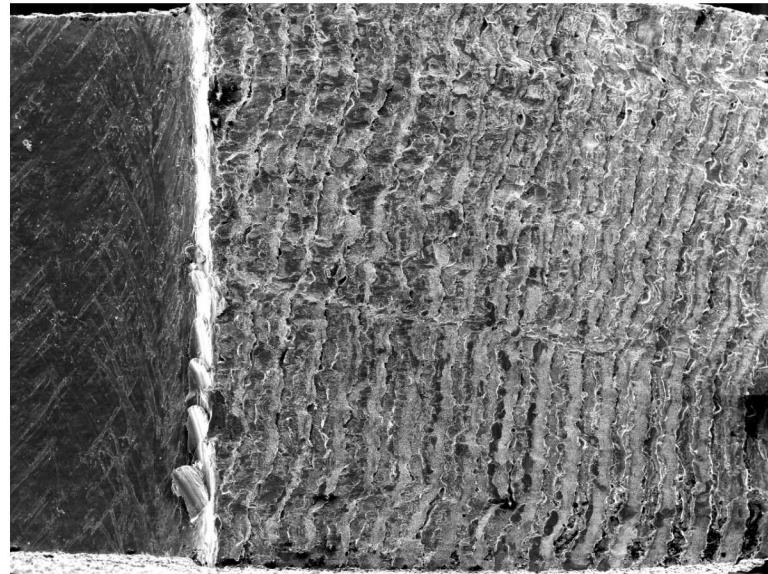


Hardness demonstrates a relationship with collision velocity

Explosive Bonding Full Area SEM

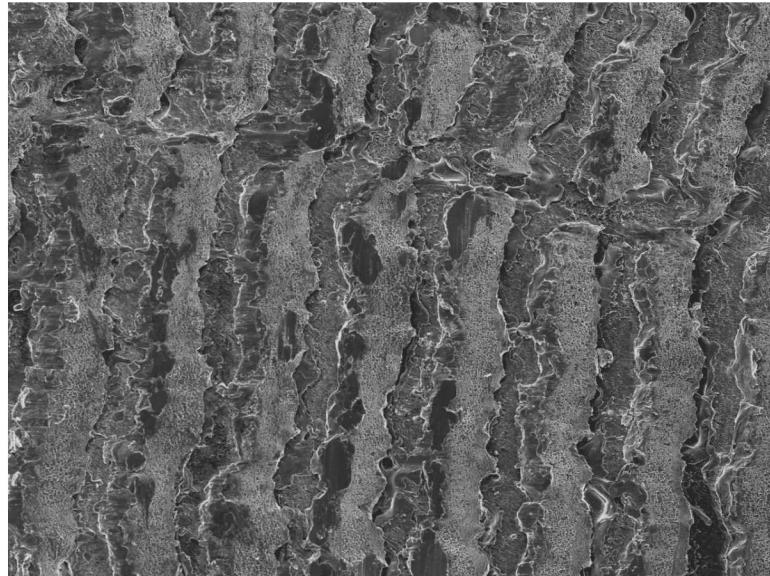


SEM image #4
SSP10-4 (highest performer) 100.6 ksi
-failed in parent material (mostly shear) 1540 lbs.

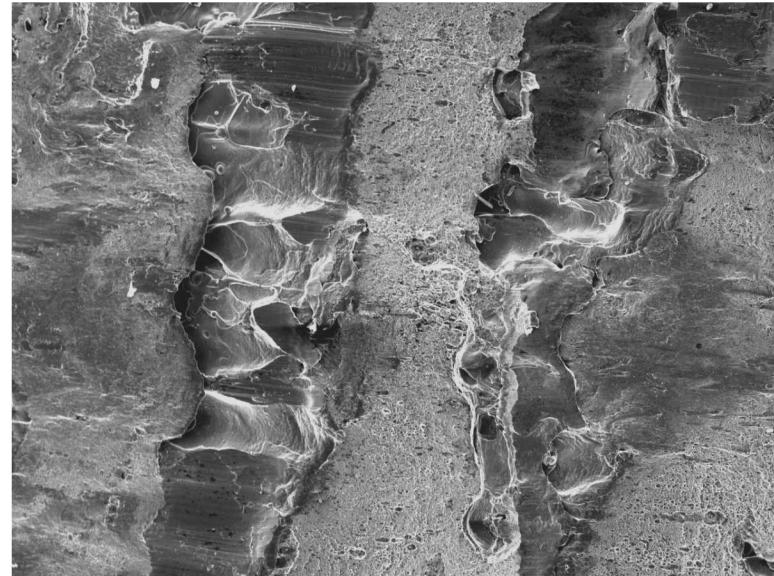


SEM image #2
SSP9-4 (highest performer) 68.6 ksi
-failed along interface 1050 lbs.

FOV: 1.422x1.067
mm

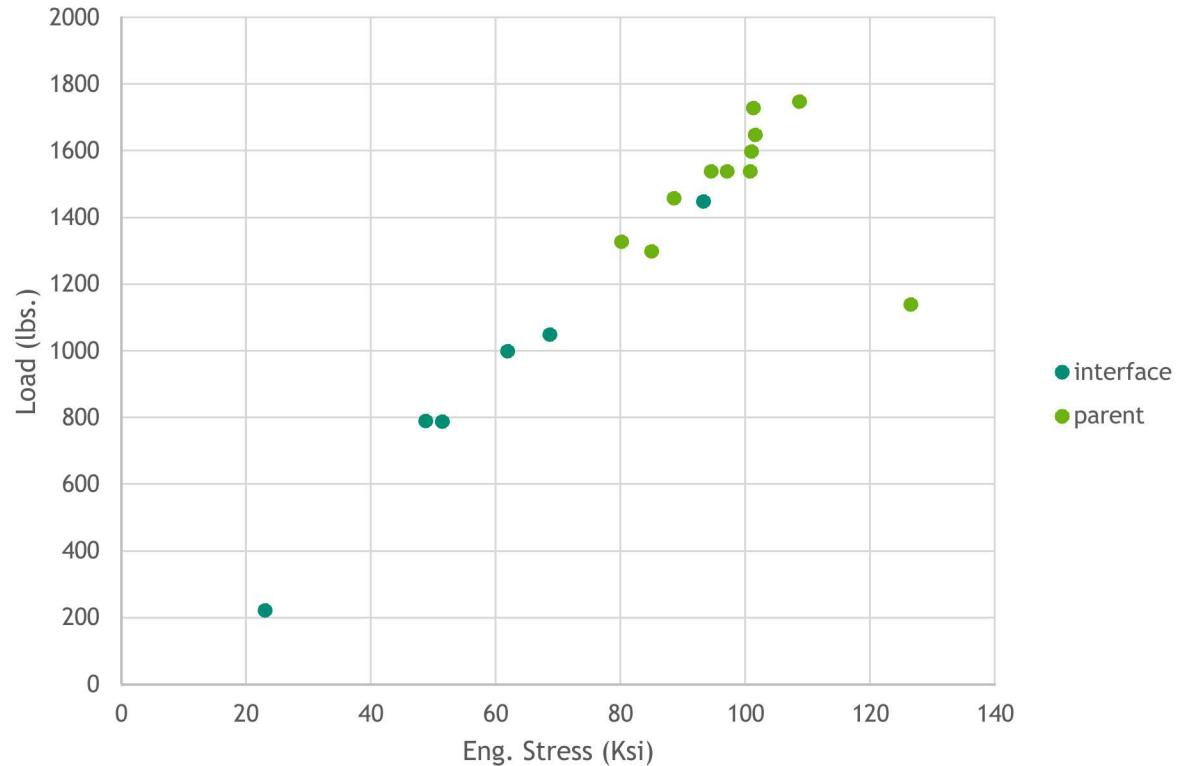


SEM image #19 (X003, Y003)
SSP9-4 (highest performer)
-failed along interface



SEM image #33 (X003, Y001)
SSP40-3 (lowest performer)
-failed along interface

Explosive Bonding Load vs Engineering Stress

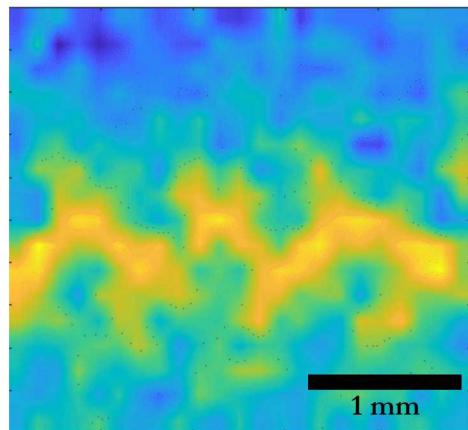
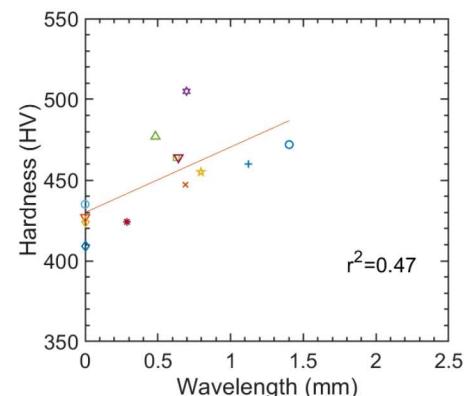
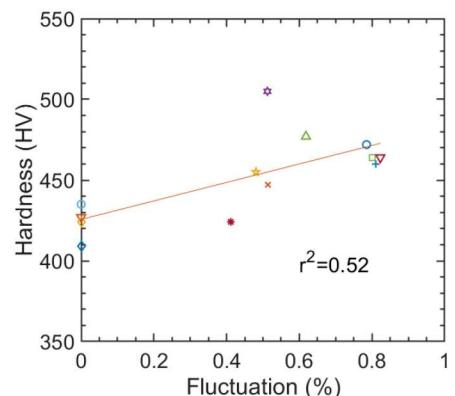
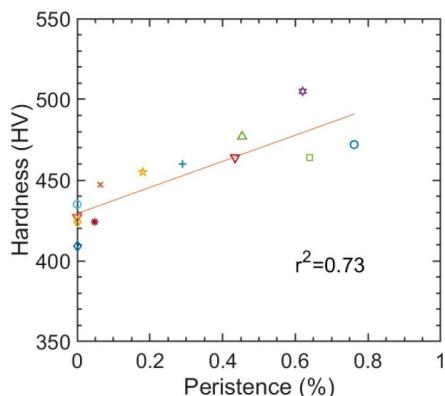
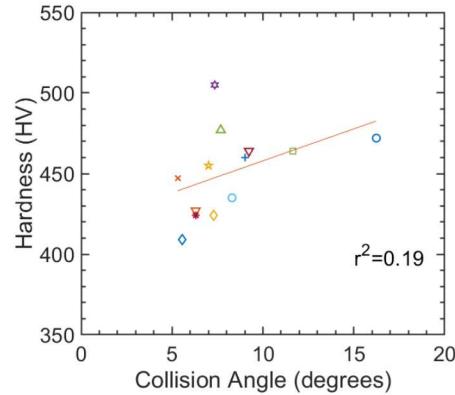
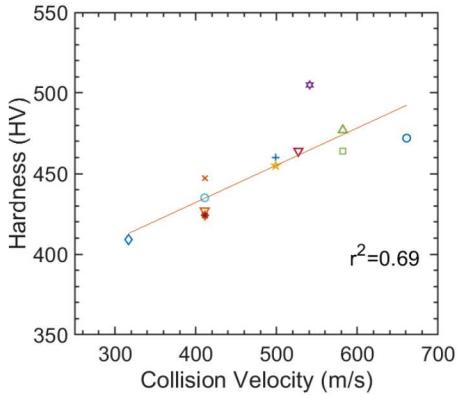


Vickers Microhardness

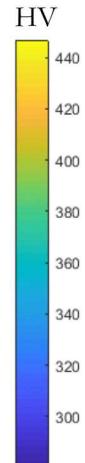
Microhardness provides greater spatial fidelity compared to lap-shear test

- Study local hardness variation across the bond interface and into the parent material

Relate peak hardness to interface parameters:



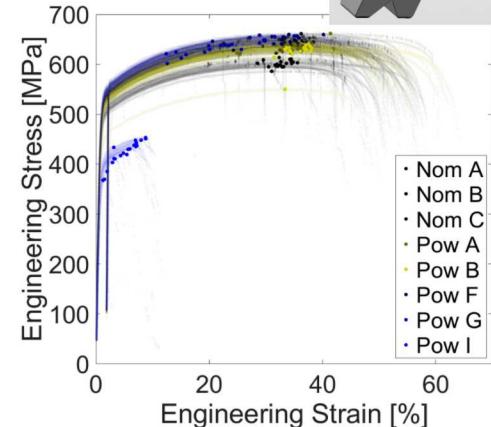
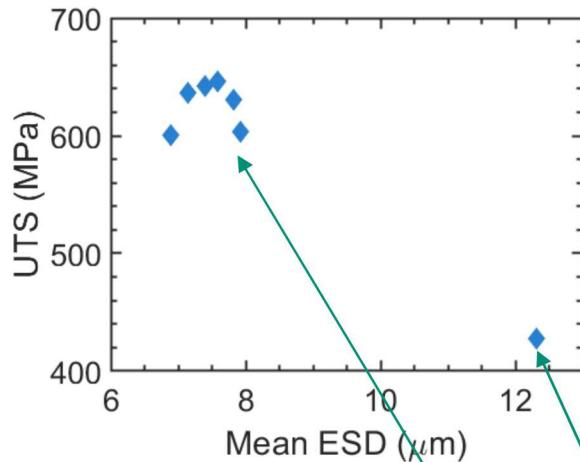
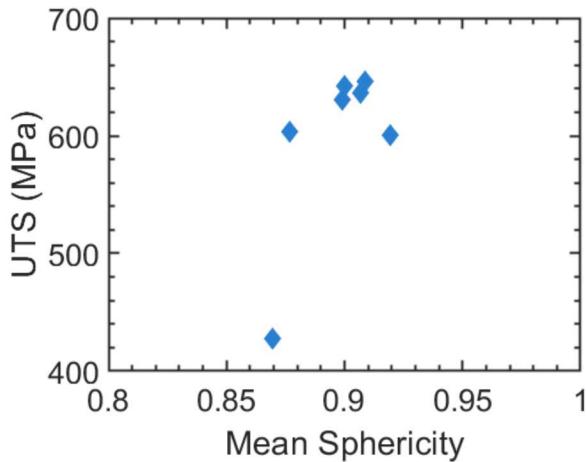
Hardness shows a relationship with collision velocity and persistence



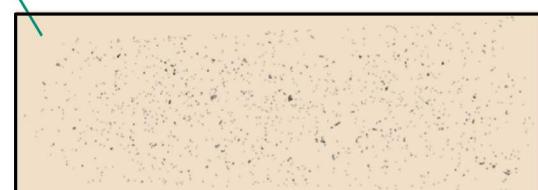
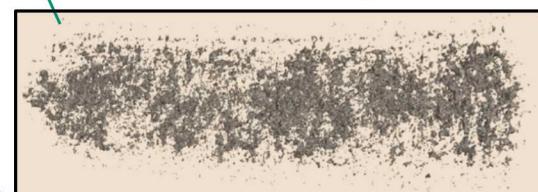
AM Defect Quantification

Prior work yet to discriminate high-correlation links between fine-scale changes in performance and porosity

- No trend between volume aggregate pore measures and fine-scale mechanical performance



Wilson-Heid et al. found that UTS and elongation to failure affected when pore diameter reaches 16% and 9% of the cross-sectional area of fabricated cylinders



Density

90%

≥95%