

# Measurement of Shock and Detonation Propagation Along Pentaerythritol Tetranitrate (PETN) Thin Films

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National  
Laboratories**



U.S. DEPARTMENT OF  
**ENERGY**



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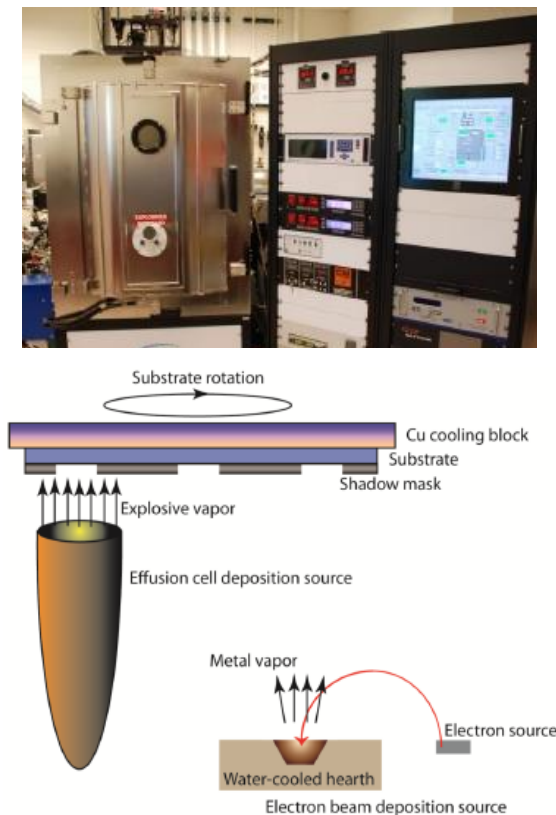
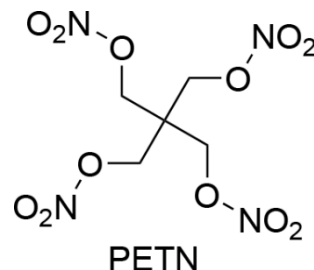
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# Outline

- Background and introduction
  - Physical vapor deposition (PVD) of explosives
  - Detonation failure
- Experimental methods
- Experimental results
- Computational methods
- Computational results
- Conclusions

# Physical Vapor Deposition (PVD)

- PVD is a process used to deposit thin films of elements, compounds or molecules.
- PVD uses a heat source to evaporate the material of interest, which is then deposited onto a substrate.
- PVD enables creation of unique microstructure and morphology compared to pressed explosives.



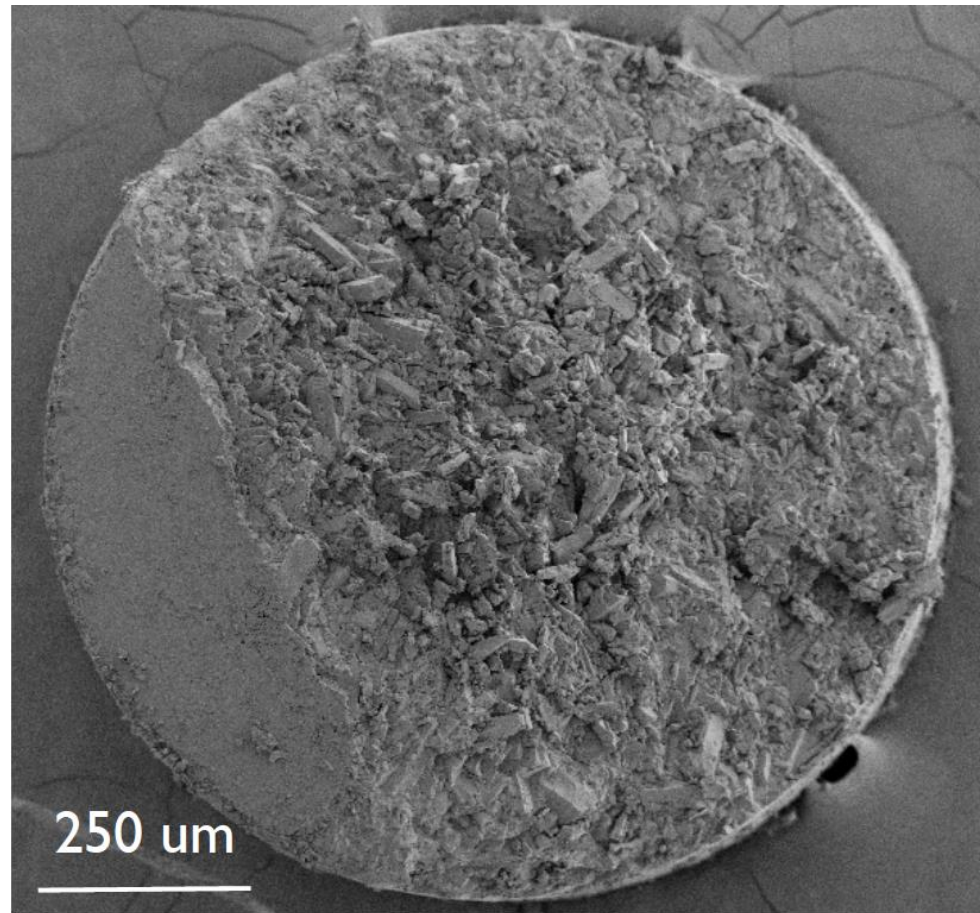
Custom high vacuum chamber for PVD of energetics (top) and schematic of deposition process (bottom)  
[Knepper 2014].

# Typical explosive manufacturing methods do not allow controlled variation in microstructure

- Local variation in microstructure is common [Knepper 2011].



Comp A-5 Pellets  
[<https://explosives.k2si.com>].

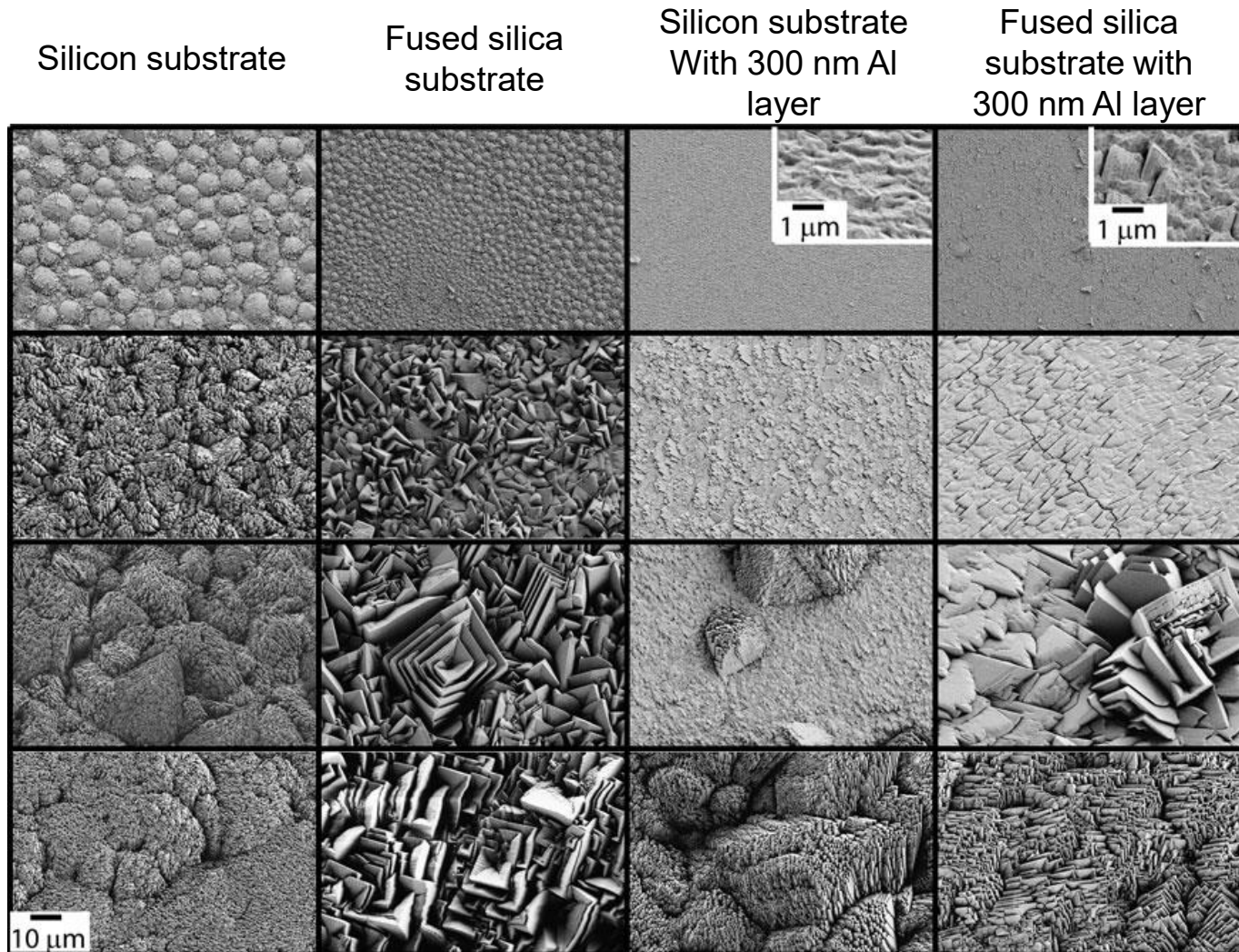


PETN Pellet Microstructure [Wixom 2008].



# Morphology of PVD explosives can be controlled by deposition conditions

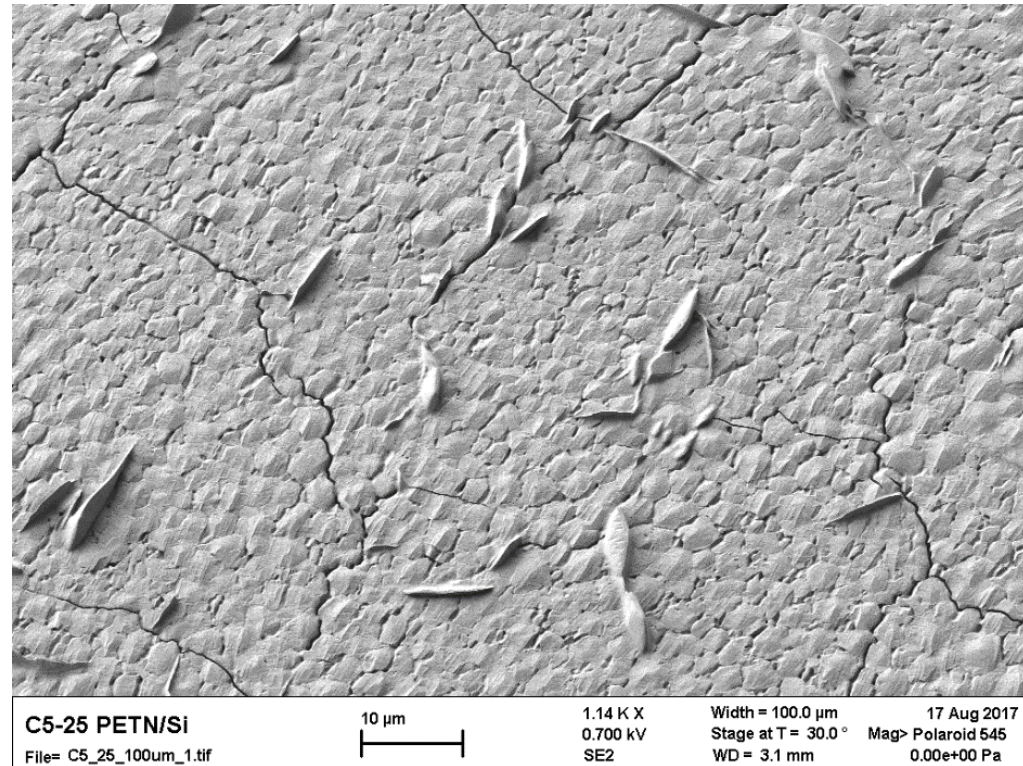
Increasing film  
Thickness



[Knepper 2011]

# Microcracking can occur in high density pentaerythritol tetranitrate (PETN) films

- Films deposited onto substrates with higher surface energy:
  - Have higher density.
  - Have an increased detonation velocity [Forrest 2017, Knepper 2018].
- Effect of microcracks on detonation propagation in thin films is unknown.***



Scanning electron micrograph (SEM) of dense 10 µm thick PETN film on silicon substrate. Note cracking from residual thermal stress.

# Detonation can fail at a length scale referred to as the critical dimension

- Typical critical dimension measurements are performed on cylinders.
- The critical thickness of a slab has been shown to roughly be equal to the critical diameter of a cylinder [Gibbs 1980, Campbell 1976, Dobratz 1985, Starkenberg 1998].
- PVD can create films close to their critical thickness [Knepper 2011, Tappan 2010, Tappan 2012].
  - Allows for study of films at near failure conditions.

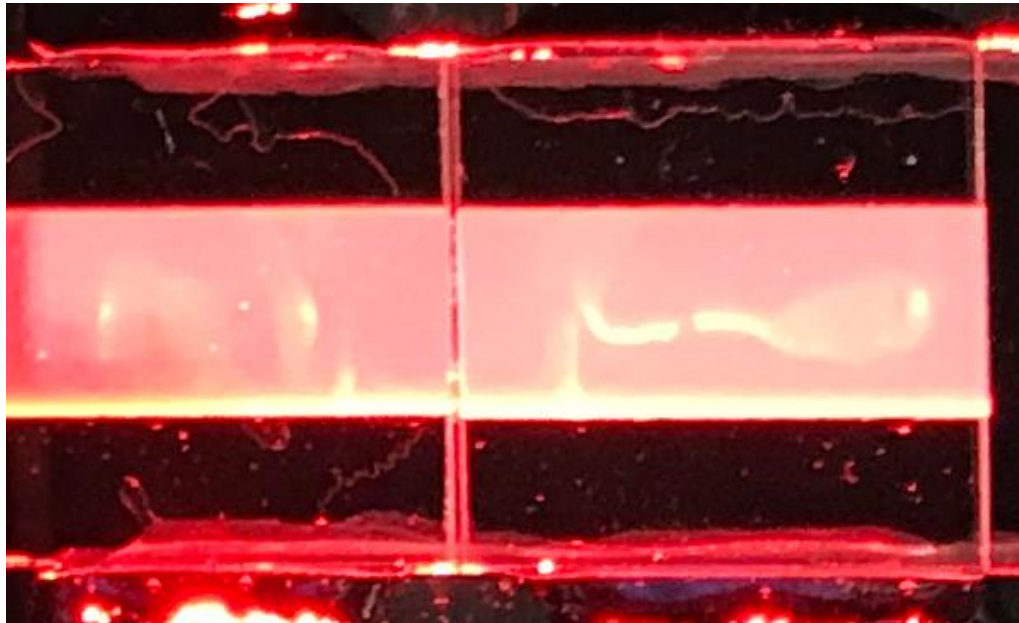


# Research here is to understand effect of microcracking on detonation failure of PETN

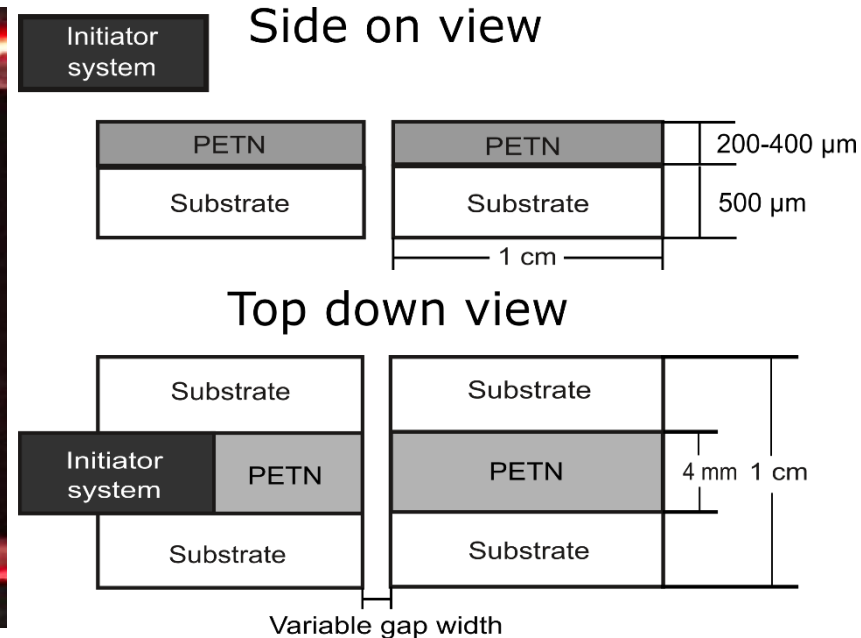
- Implementing artificial gaps between two films to determine size of gap detonation can propagate across.
- Using image processing techniques to extract position and velocity data.
- Modeling the PETN films with CTH.

# PETN films were deposited onto polycarbonate substrates

- Unconfined PETN films were deposited at a thickness of:
  - 200  $\mu\text{m}$ .
  - 400  $\mu\text{m}$ .



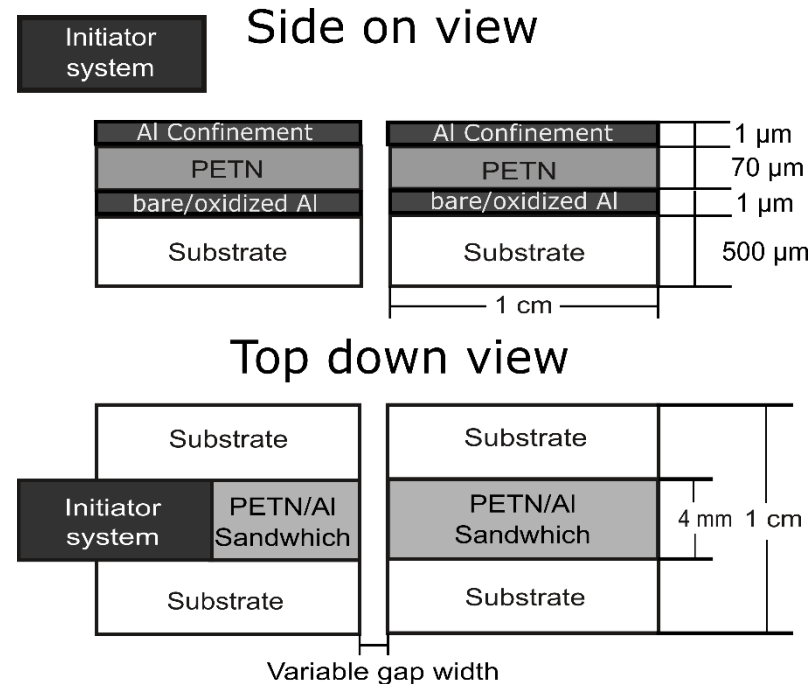
Top down view of PETN films with 95  $\mu\text{m}$  gap.





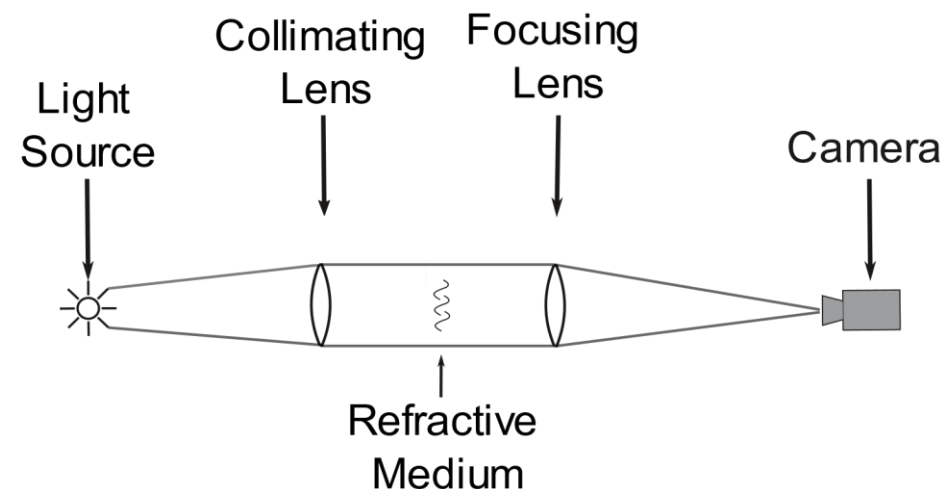
# PETN films with a 1 $\mu\text{m}$ -thick aluminum (Al) confinement layer were deposited onto polycarbonate

- Two configurations were used:
  - An Al layer that remained in vacuum (bare aluminum, high surface energy).
  - An Al layer that was exposed to the atmosphere (oxidized Al, low surface energy).
- Confinement was used here to study the films at near failure conditions.
  - The effects of confinement were not explicitly explored.

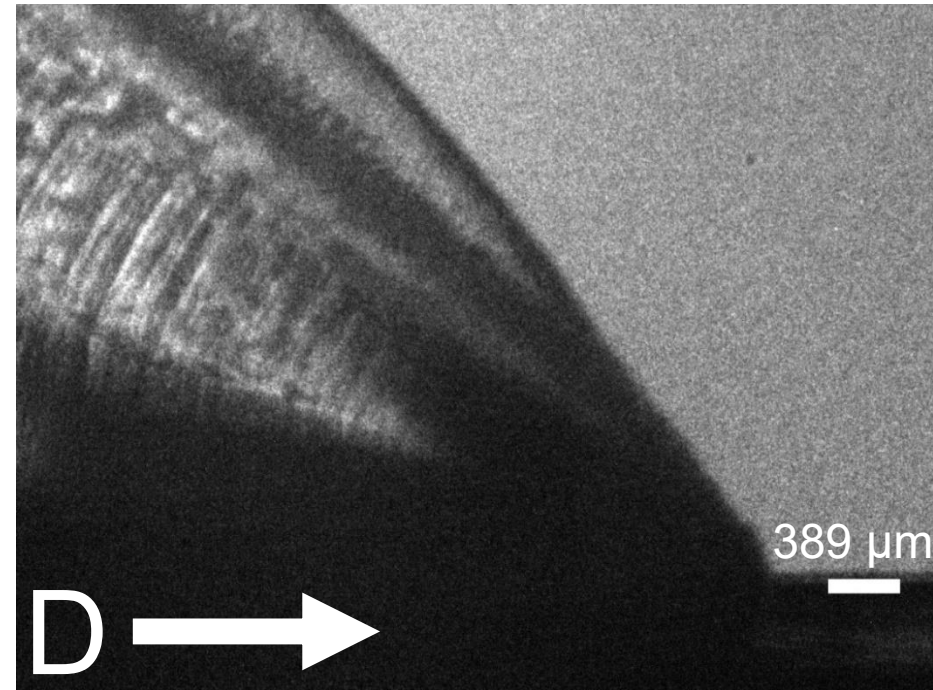


# Refractive imaging visualizes shock in air

- Focused Shadowgraph visualizes the second derivative of the refractive index.
- Schlieren visualizes the first derivative of the refractive index.



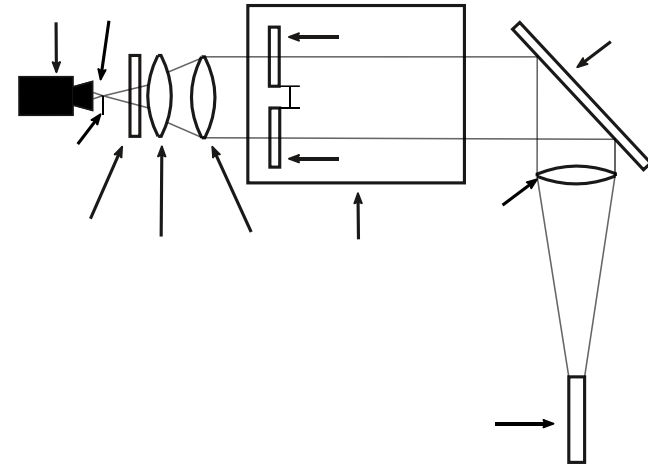
Focused shadowgraph system.



Schlieren image of a PVD PETN film detonating.

# Imaging setup for measurement of the shock front

- Specialised Imaging SI-LUX 640 spoiled coherence laser used as light source for test.
- Camera was a Specialised Imaging SIMX-15.
  - Camera is capable of recording 15 full resolution images at a frame rate of up to 1 billion frames per second.
- Test was conducted in two series.
  - First test series used focused shadowgraph.
  - Second test series used schlieren.
- A 1 mm x 1 mm square calibration grid was used for converting pixel location to spatial location.



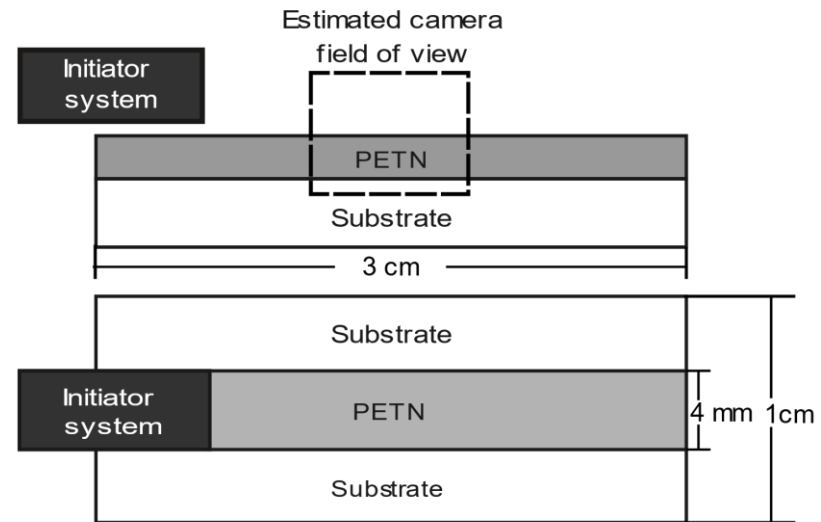
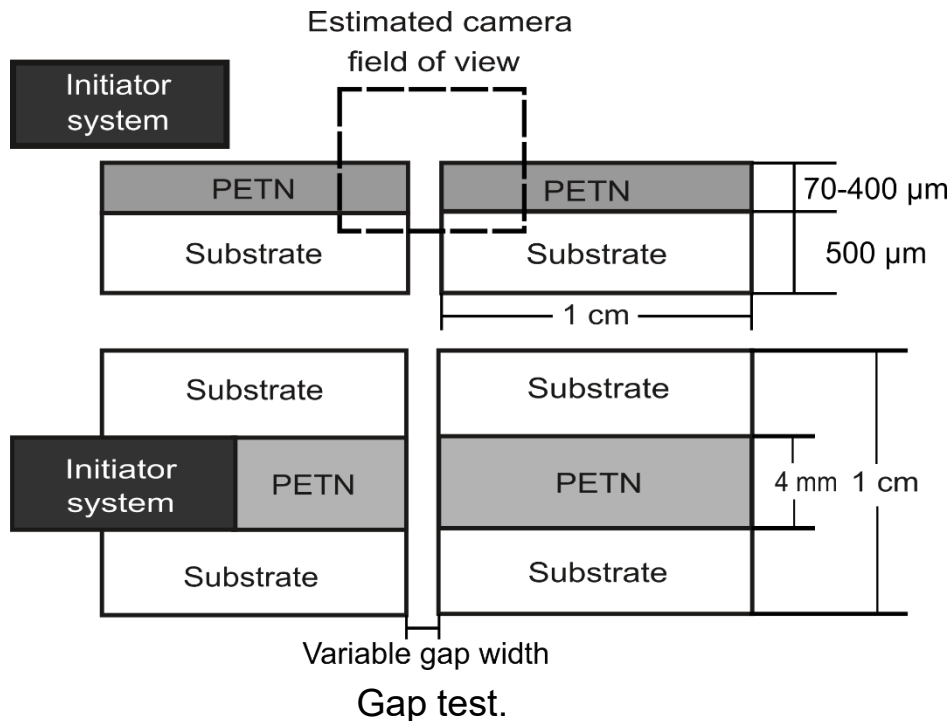
Test Series 2 schlieren with a horizontal field of view (FOV) of ~5.2 mm.



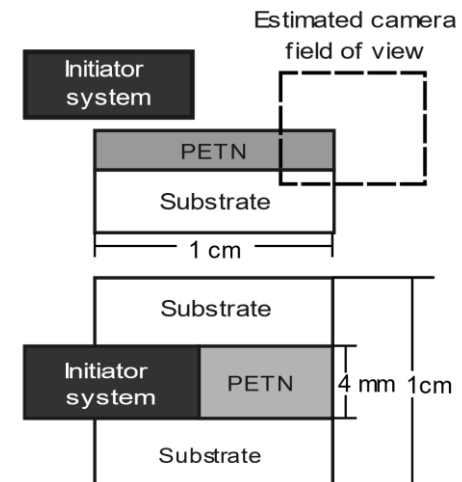
PETN Film fixture inside BoomBox.

# Detonation tests to determine PETN failure

- Detonation tests include:
  - Continuous film test.
  - Gap test.
  - Infinite gap test.



Continuous film test.



Infinite gap test.



# 70 $\mu\text{m}$ -thick continuous film test

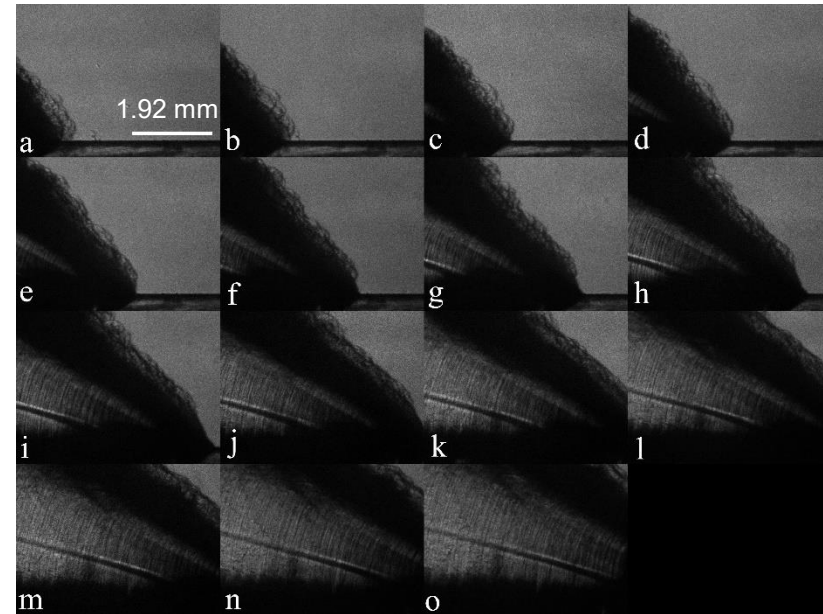




# 70 $\mu\text{m}$ -thick continuous film test

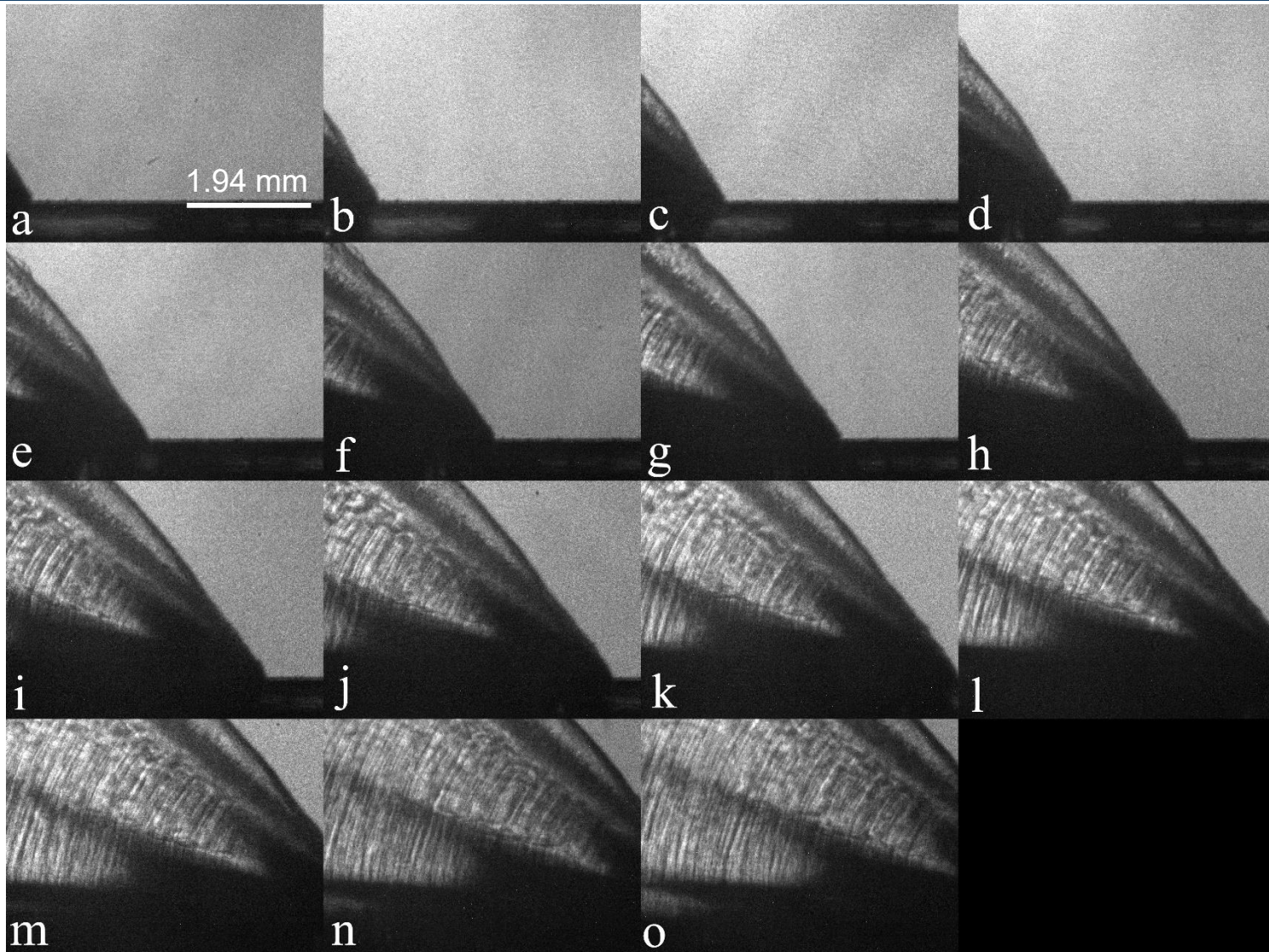
- The 70  $\mu\text{m}$ -thick aluminum confined PETN films display a rough shock front.
- The roughness could be caused by porosity within the microstructure.
- This effect is similar to Ramsay

rough shock front caused by small discontinuities in explosives [Ramsay 1965].



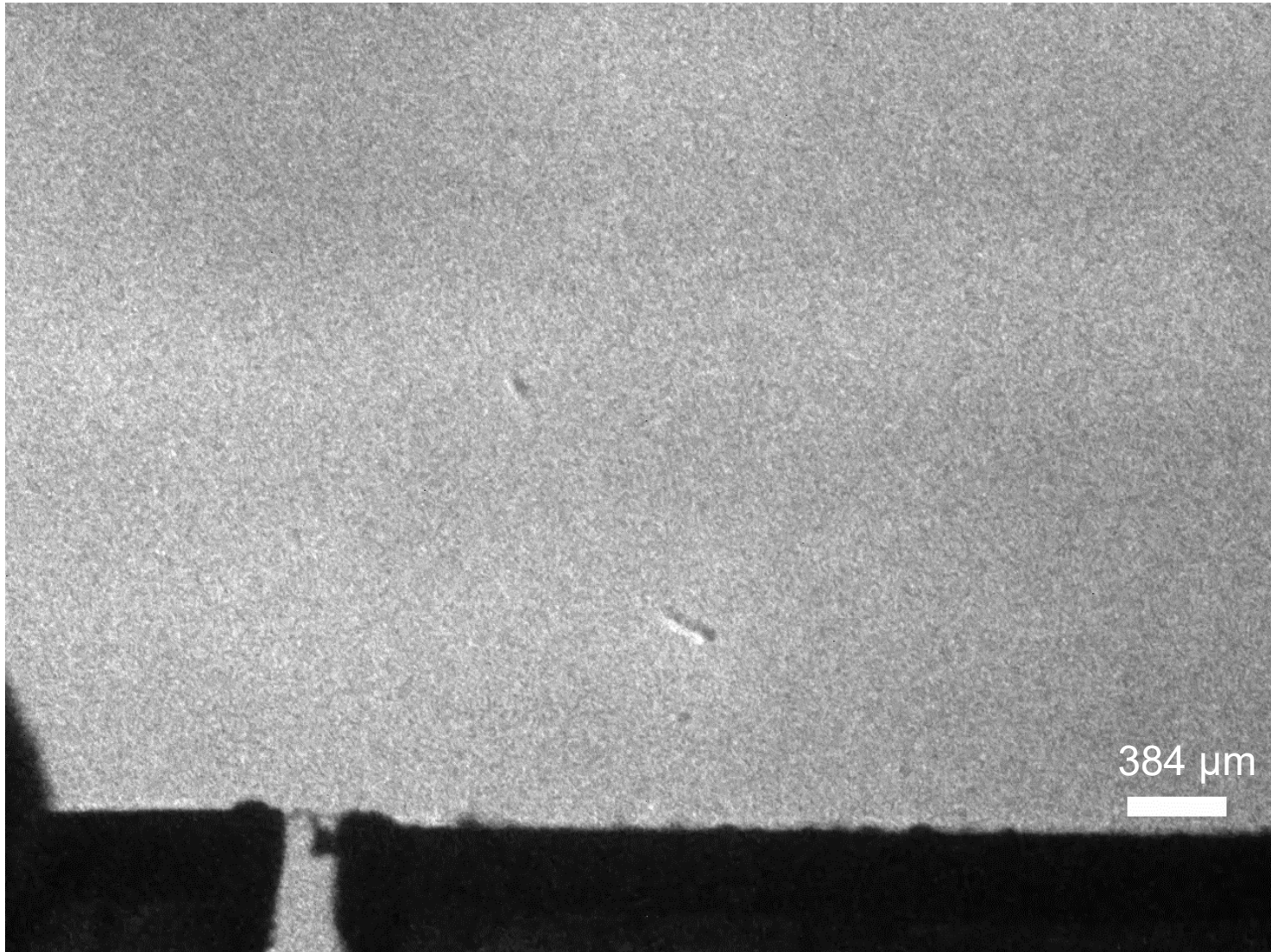
Schlieren detonation sequence of a 70  $\mu\text{m}$ -thick Al confined film deposited on bare Al.

The shock produced by the 200  $\mu\text{m}$  film is significantly more uniform than the 70  $\mu\text{m}$  confined

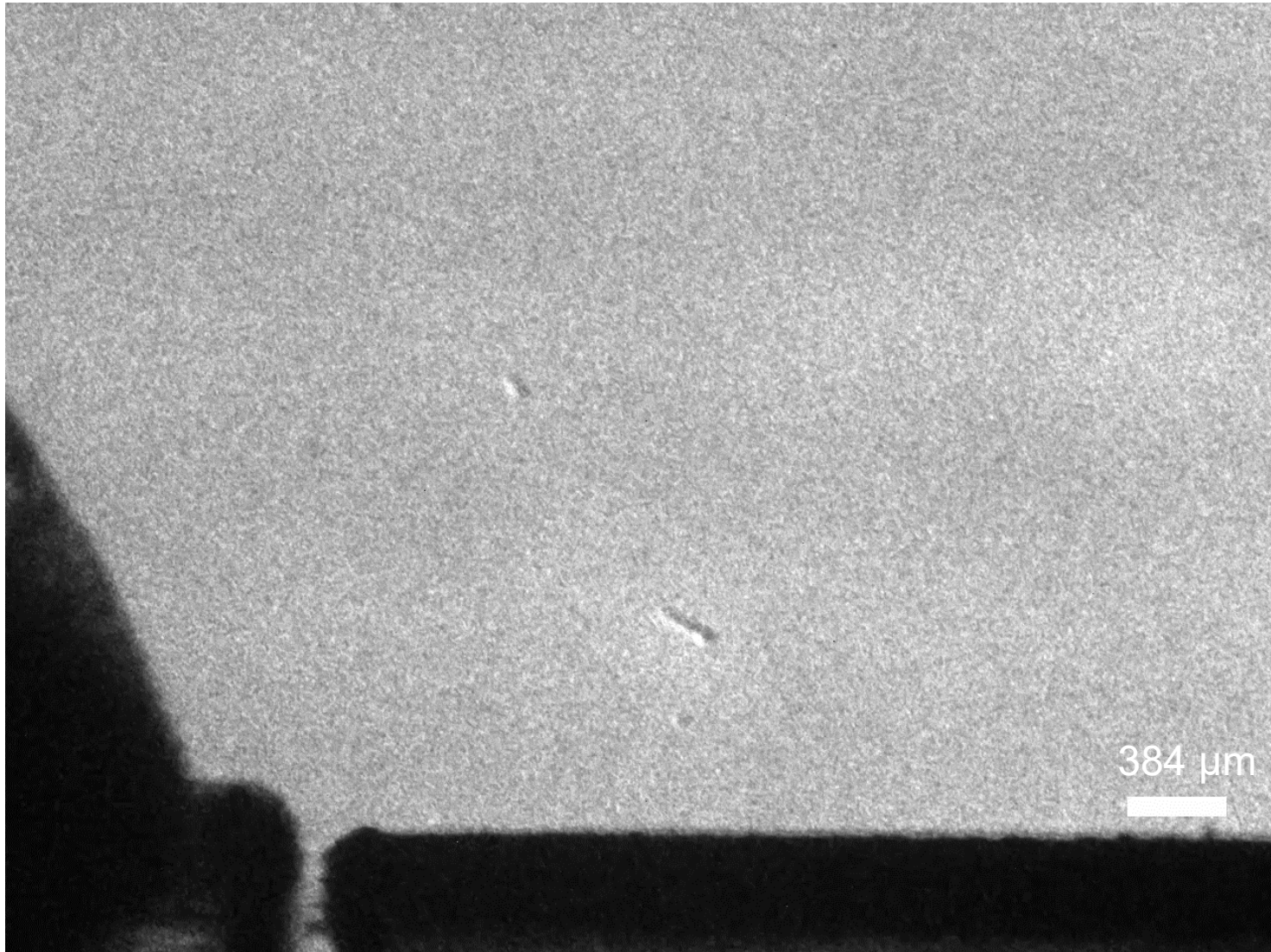




# 400 $\mu\text{m}$ -thick film – Successful initiation across gap



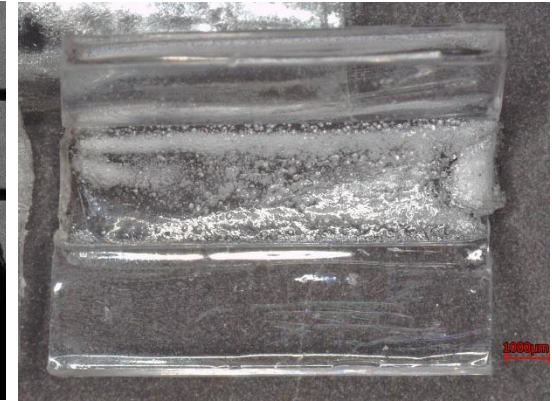
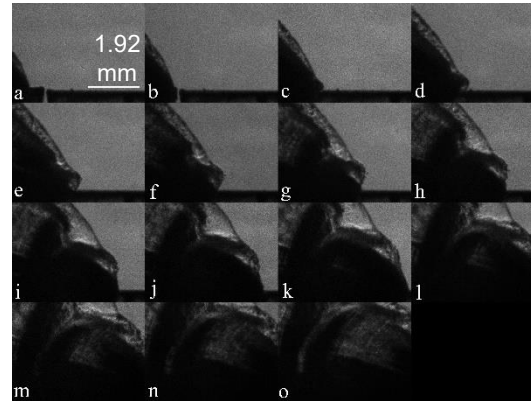
# 400 $\mu\text{m}$ -thick film – Failure to initiate across gap



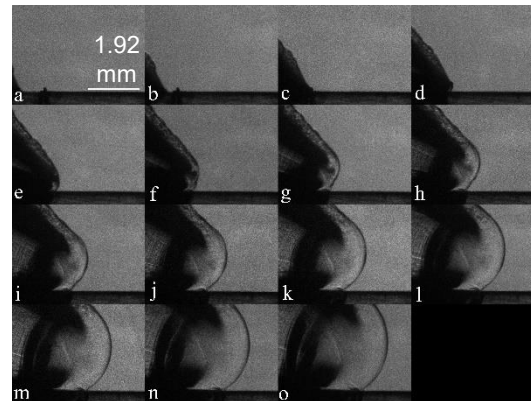


# The post detonation substrates provide a supplementary indication of test results

- Detonation propagation was determined:
  - Successful if shock returned to steady-state shape.
  - Unsuccessful if shock front became circular.



Successful detonation propagation.

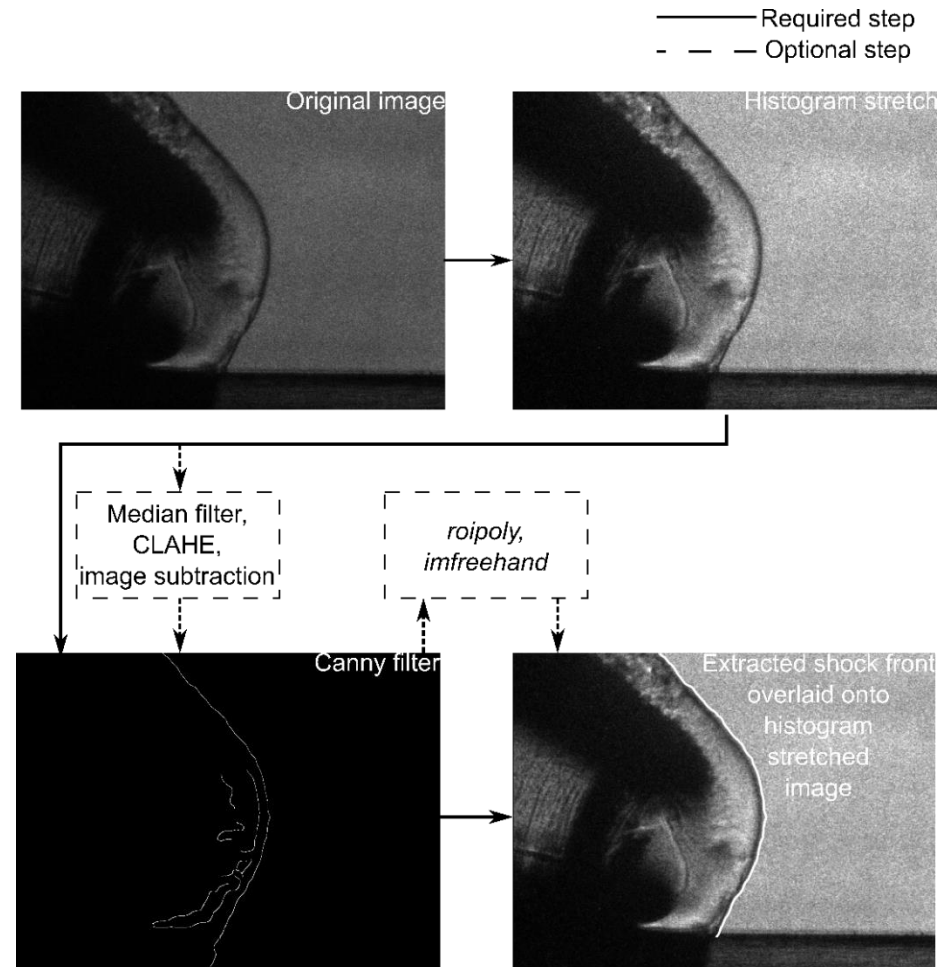


Failed detonation propagation.



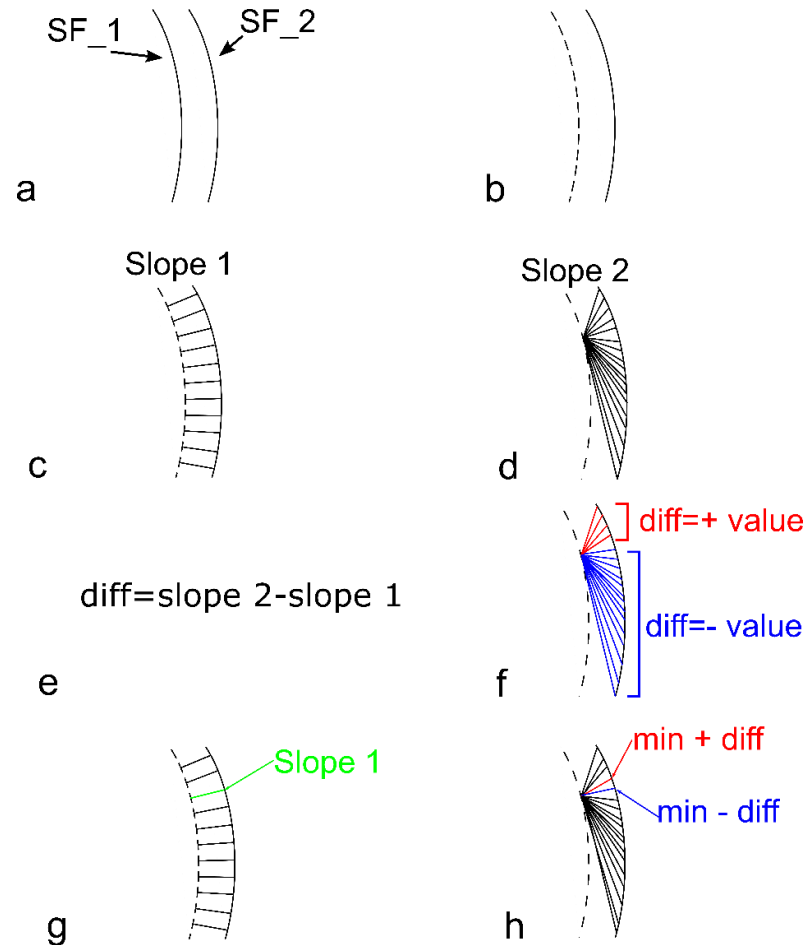
# Image processing to extract spatial data

- A custom-developed image processing routine was built to:
  - Highlight the shock wave.
  - Automatically extract and measure:
    - Shape.
    - Spatial coordinates.
    - Velocity.
- Canny filter [Canny 1986] alone was sufficient for extracting shock front in most images.
- Noisier images required use of additional image processing techniques.



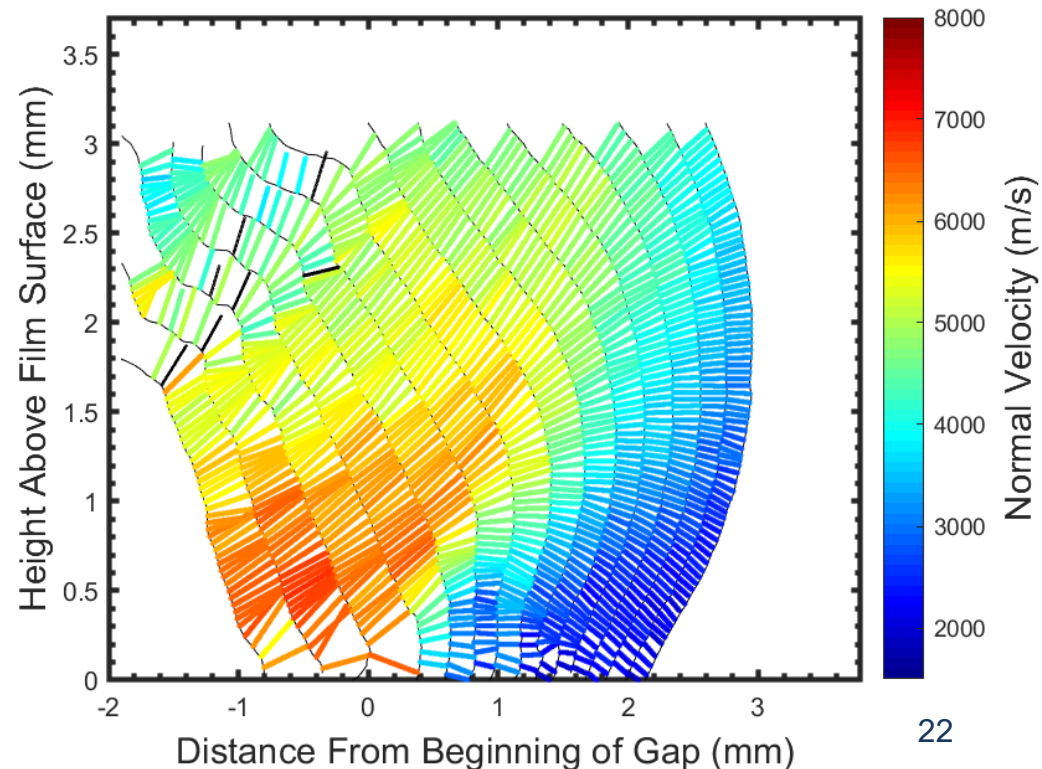
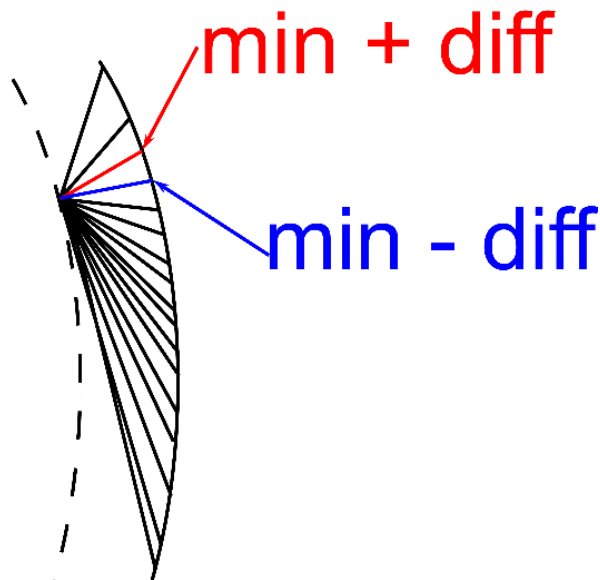
# Normal velocity method for determining velocity of a pressure driven flow

- Velocity of shock wave is calculated from spatial data in successive frames [Chapra 2015].
- New method for automatically determining shock front velocity was developed that:
  - Calculates velocity in direction of dynamic pressure driven flow.



# Normal velocity plots were made to visualize velocity of the shock front

- The plots are color coded to specify velocity.
- Black vectors are rejected due to an uncertainty in slope matching  $> \pm 50$  m/s.



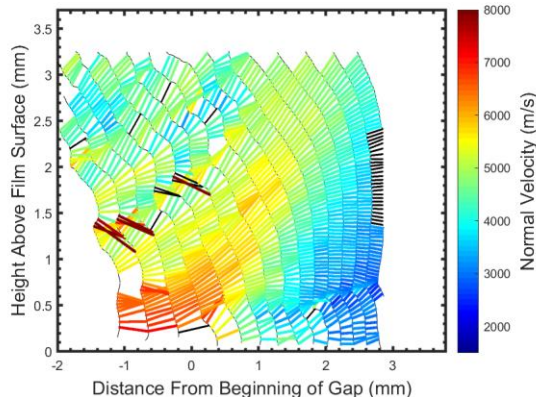
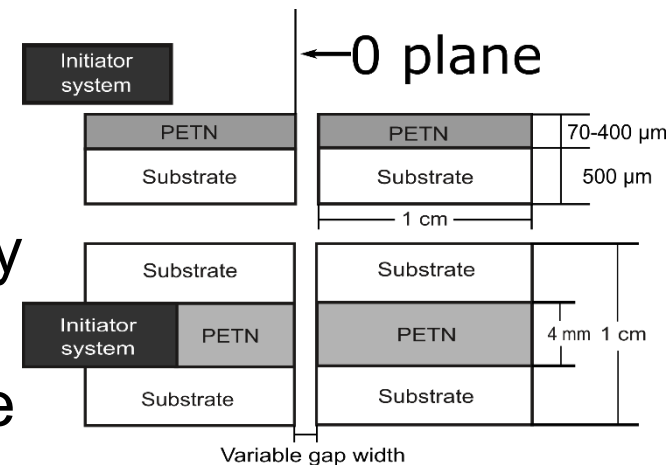
# Continuous film test with transient shock



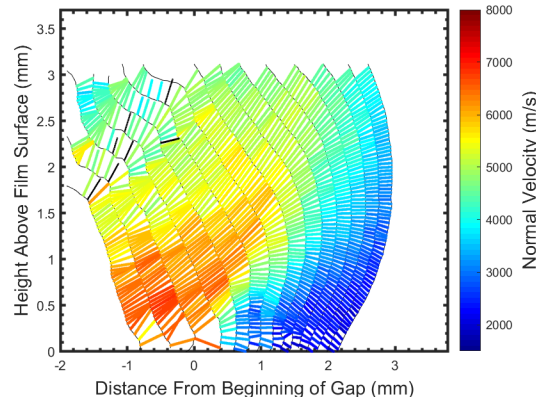


# Transient velocity is an indicator of when detonation reached steady-state

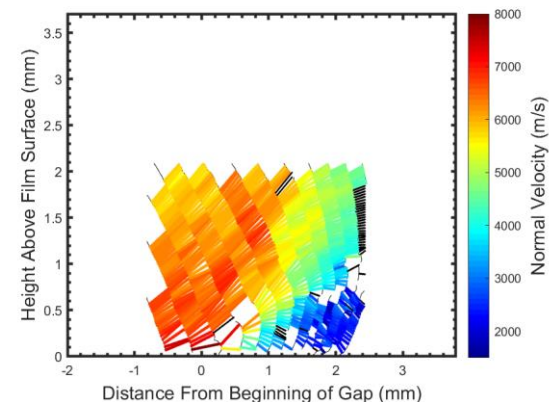
- The velocity of the shock front increases as the shock front reaches steady-state.
- The height of the steady-state velocity was recorded for each of the tests at:
  - The vertical plane representing the beginning of the gap (0 plane).



70 μm-thick film deposited on oxidized aluminum.  
1 mm above the film surface.



70 μm-thick film deposited on bare aluminum.  
1.5 mm above the film surface.

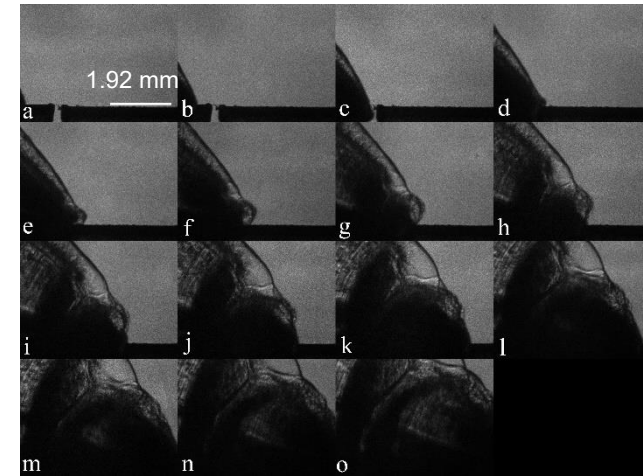


200 μm-thick film.  
v

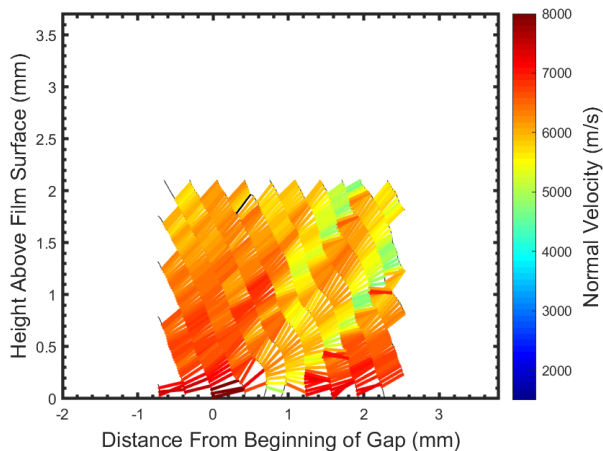


# Successful initiation

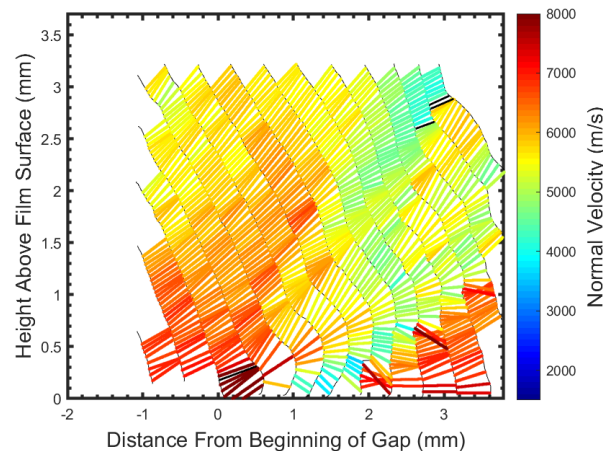
- The distance the shock front traveled before returning to its steady-state wave shape for a:
  - 200  $\mu\text{m}$  film with a 25  $\mu\text{m}$ -gap-width was about 875  $\mu\text{m}$ .
  - 400  $\mu\text{m}$  film with a 220  $\mu\text{m}$ -gap-width was about 1700  $\mu\text{m}$ .



Schlieren images of a 400  $\mu\text{m}$ -thick film gap test.



200  $\mu\text{m}$  film velocity plot.



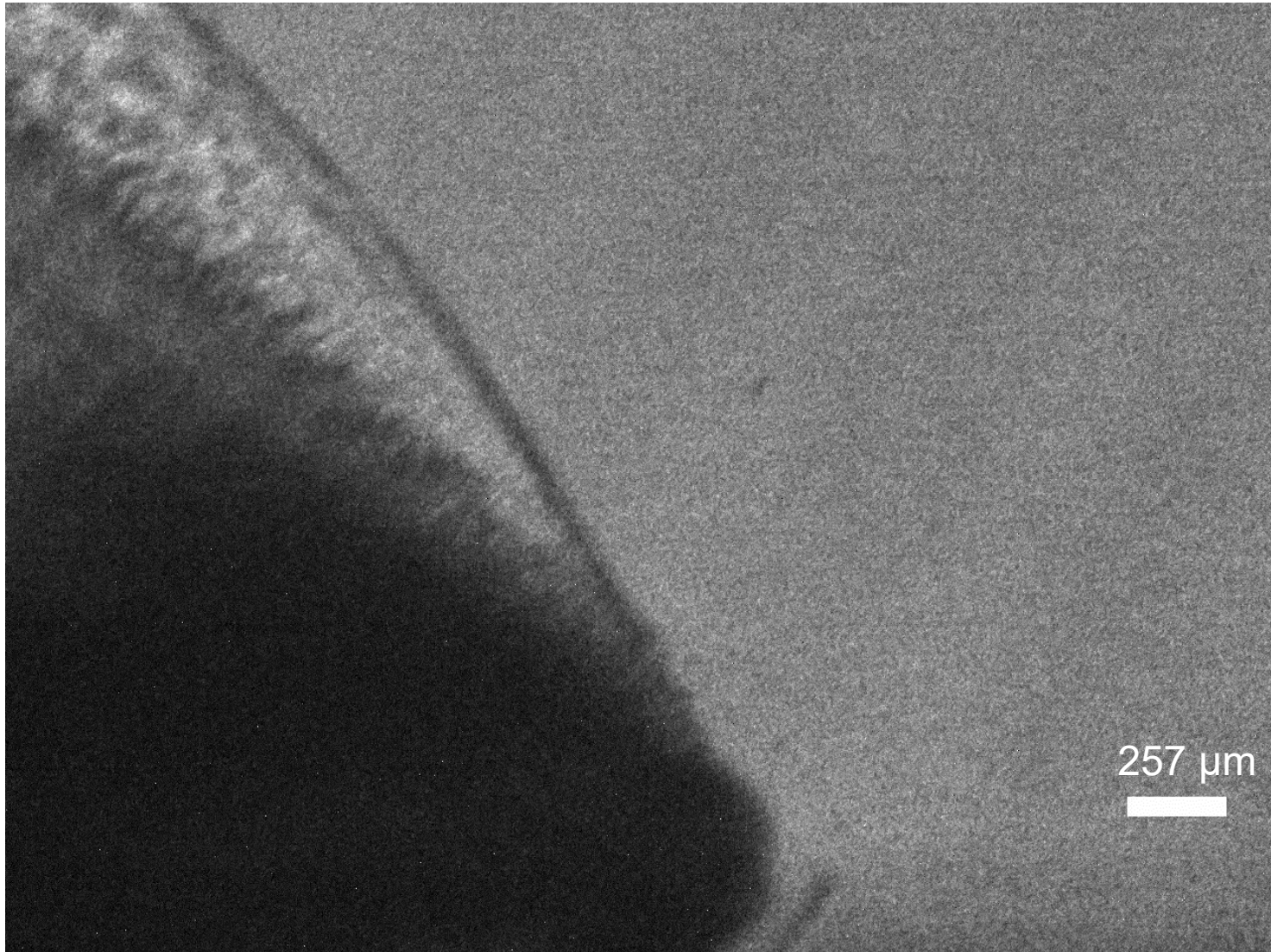
400  $\mu\text{m}$  film velocity plot.

# Critical gap width is the largest gap width for reliable initiation

- Neither of the 70  $\mu\text{m}$ -thick Al confined films propagated across an abutment gap.
  - Close to critical thickness of Al confined films (55  $\mu\text{m}$ ) [Knepper 2018].
- The 200 and 400  $\mu\text{m}$ -thick films both had detonations occur in gaps larger than the critical gap width.
  - May be due to roughness at edge of films.
  - No detonation failed below critical thickness.

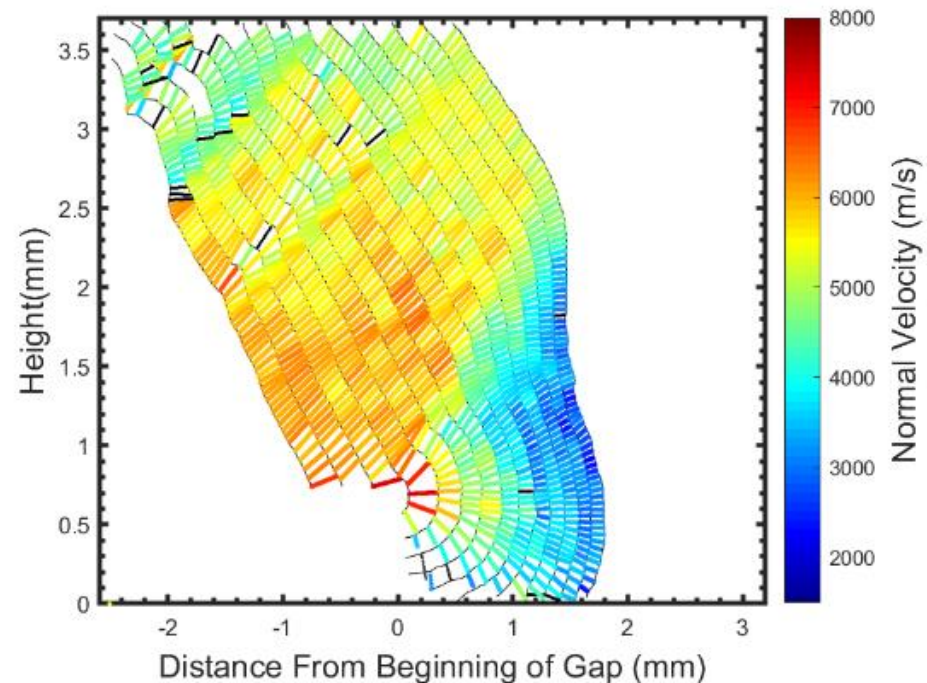
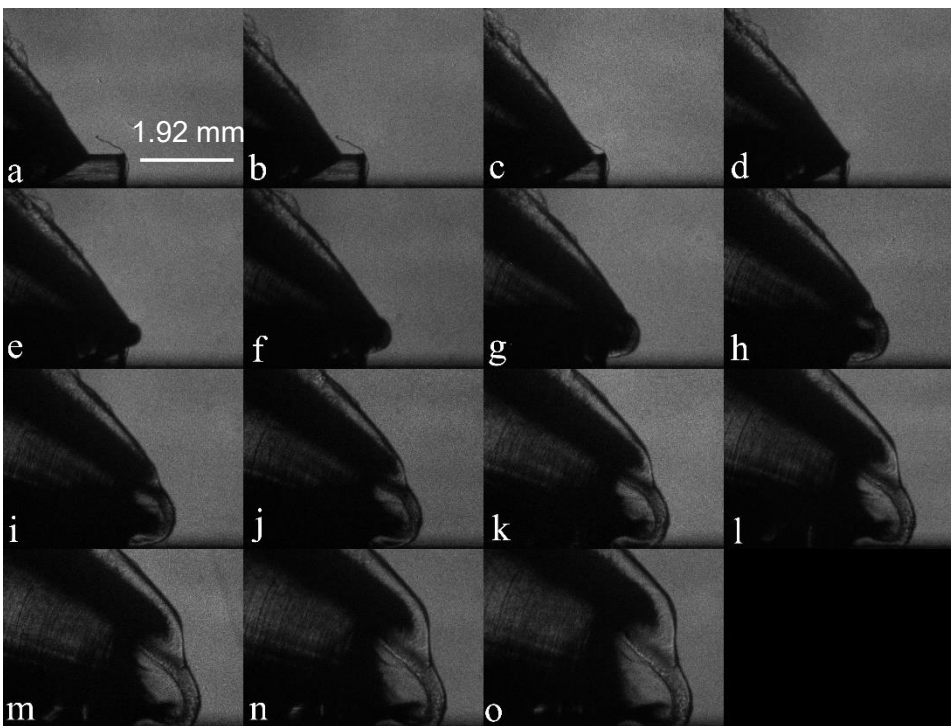
Film Thickness ( $\mu\text{m}$ )	Critical Gap Width ( $\mu\text{m}$ )	Substrate Material
70	0	Oxidized aluminum
70	0	Bare aluminum
200	80	Polycarbonate
400	180	Polycarbonate

# 200 $\mu\text{m}$ -thick film infinite gap test





# The velocity of the shock front within the gap is determined with the infinite gap test



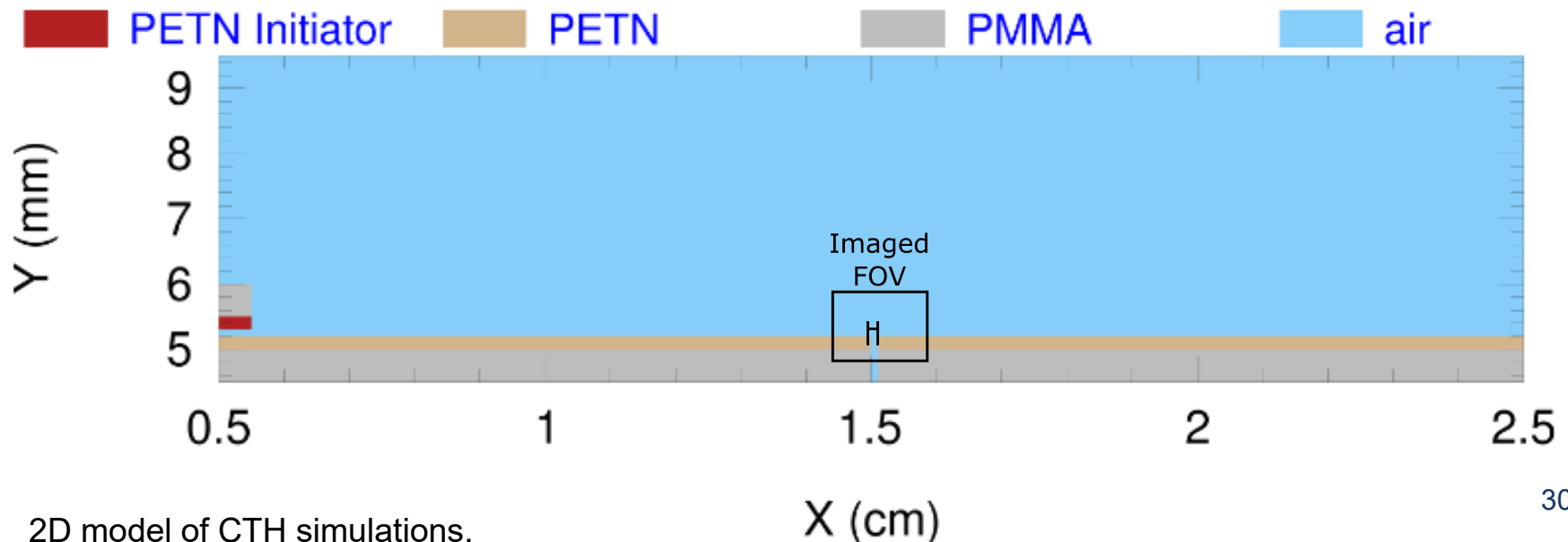


# Hydrocodes numerically solve conservation equations

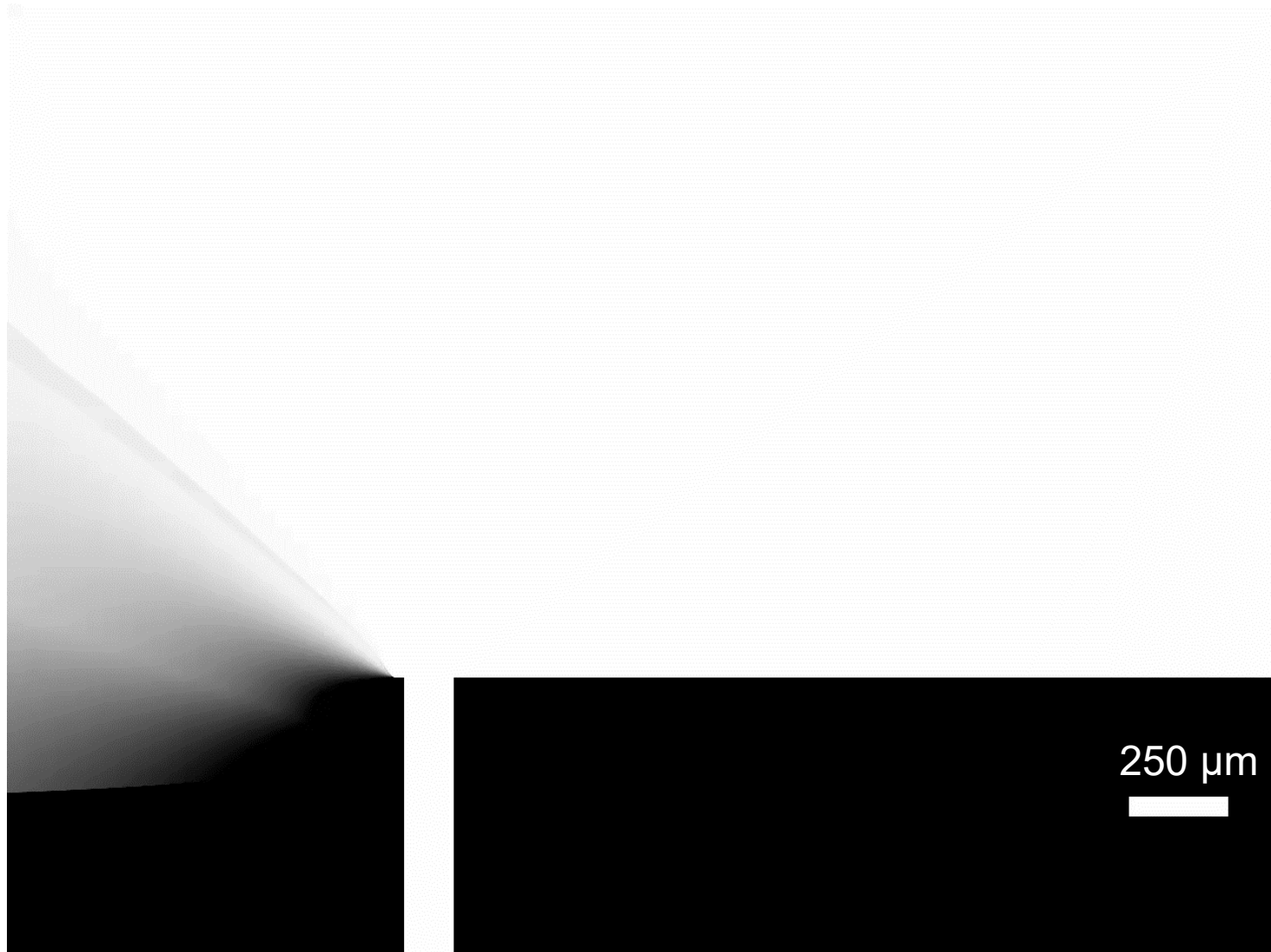
- CTH is an Eulerian hydrocode developed by Sandia National Labs.
- Hydrocodes typically use composite models to describe an energetic material.
- The composite models relate two equations of state (EOS) that describe:
  - The unreacted material properties.
  - The reaction product properties.
- The composite model relates the EOSs using an empirically derived burn rate.

## 2-Dimensional CTH model of PETN films

- The model consisted of:
  - PETN initiator (Jones Wilkins Lee (JWL) EOS).
  - PETN films with history variable reactive burn (HVRB) composite model:
    - Mie Grüneisen solid EOS.
    - Sesame tabular reaction product EOS.



# CTH density output



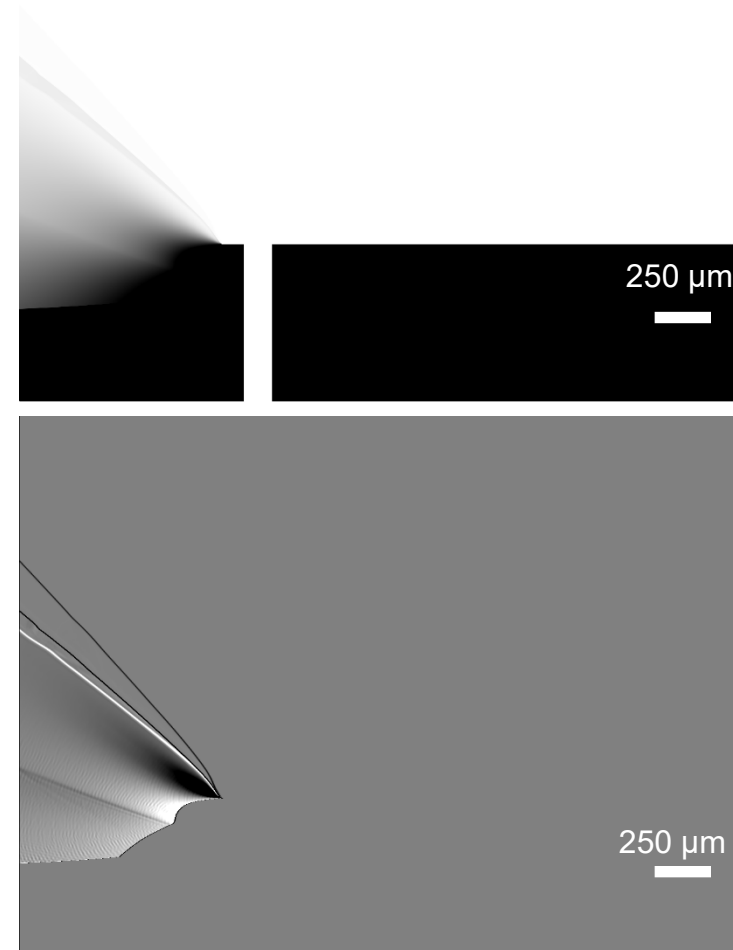


# Derivative of the density field yields schlieren

- Schlieren images are the first derivative of the refractive index field.
- Density,  $\rho$ , is linearly proportional to the refractive index,  $n$ .

$$\rho = \frac{n - 1}{k}$$

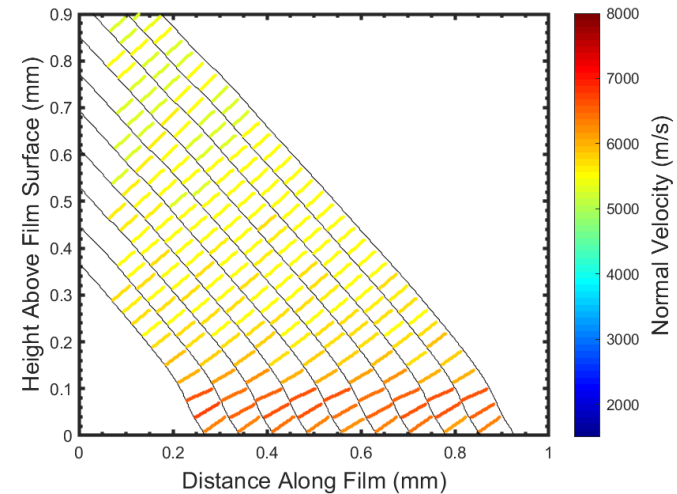
$k$  is the Gladstone-Dale Coefficient.



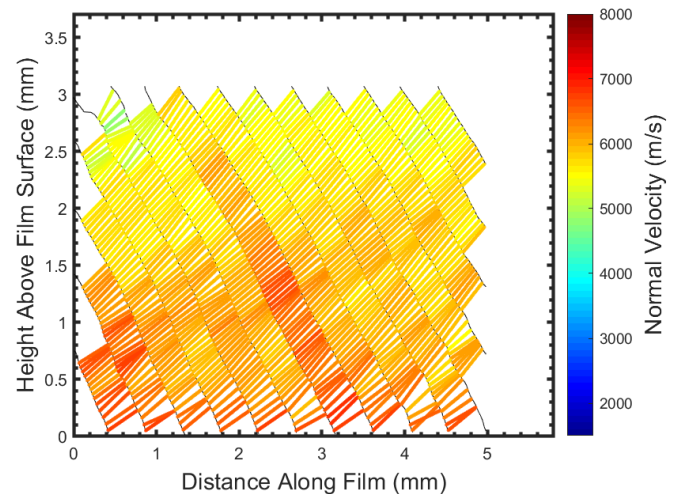
# CTH continuous film test

- The detonation velocity was calculated for each of the continuous film tests.
- The calculation of the detonation velocity was performed by:
  - Manually clicking on the shock front along the edge of the film on successive frames.
- A total of 9 centered difference velocity calculations were performed for each test.
- The mean and standard deviation of the calculations is reported below.

Expt. / CTH	Film Thickness ( $\mu\text{m}$ )	Detonation Velocity (m/s)	Substrate Material
Expt.	70	$7450 \pm 116$	Oxidized aluminum
Expt.	70	$7910 \pm 53$	Bare aluminum
Expt.	200	$7651 \pm 197$	Polycarbonate
CTH	200	$7319 \pm 88$	PMMA



Continuous film CTH test.



Continuous film experimental test.

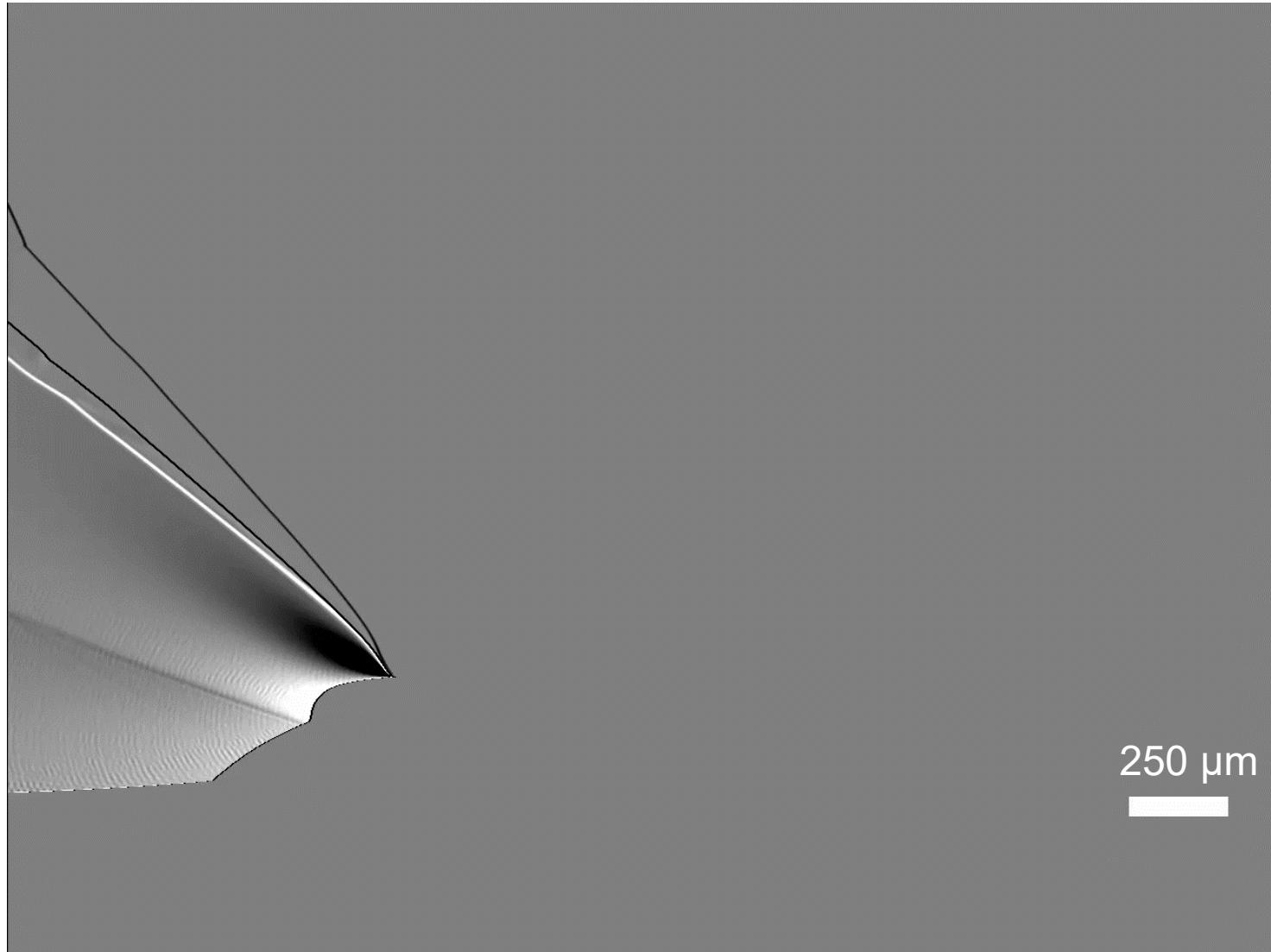
# 200 $\mu\text{m}$ -thick films were modeled with CTH

- The models were calibrated to initiate at a 200  $\mu\text{m}$ -thickness.
  - HVRB
    - Calibration constants [Starkenbergs 1998]
      - $\text{Pr}=1\text{e}10$
      - $\text{Z}=3.9$
      - $\text{Pl}=4\text{e}10$  Threshold pressure for reaction
  - Mie Grüneisen
    - $\rho=1.5$  Density of PETN
  - Tuned until critical thickness was roughly that of experiment.
- The critical gap width of the CTH tests was found to be 125  $\mu\text{m}$ .

Expt./ CTH	Film Thickness ( $\mu\text{m}$ )	Critical Gap Width ( $\mu\text{m}$ )	Substrate Material
Expt.	70	0	Oxidized aluminum
Expt.	70	0	Bare aluminum
Expt.	200	80	Polycarbonate
CTH	200	125	PMMA
Expt.	400	180	Polycarbonate

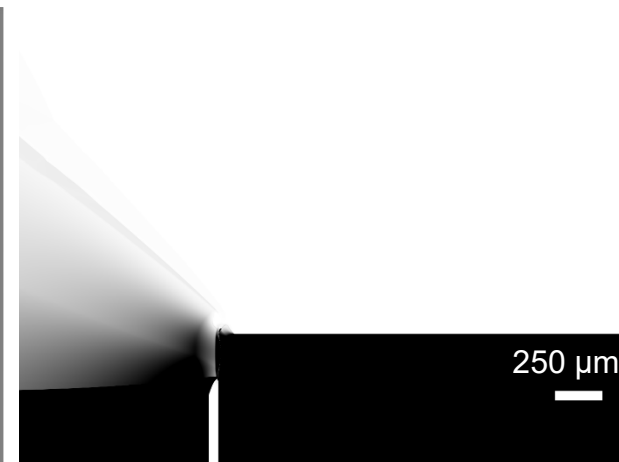
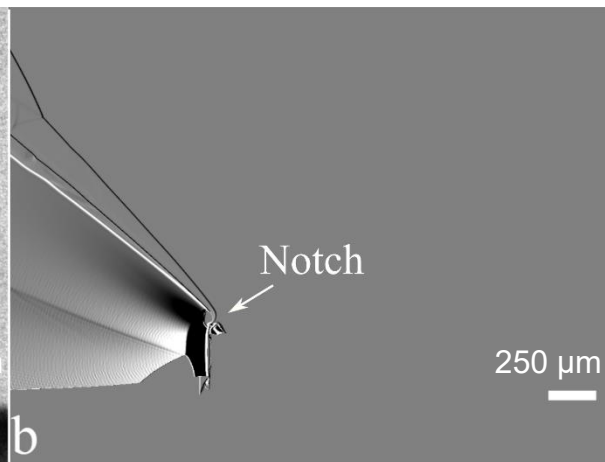
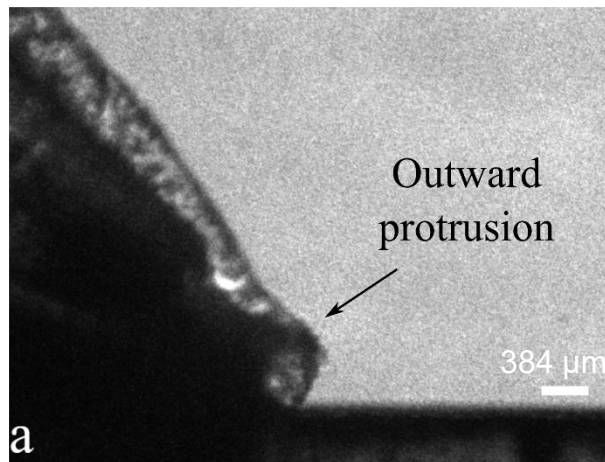


# Successful initiation video 125 $\mu\text{m}$ gap computer generated schlieren (CGS)



# CTH successful initiation comparison

- In the experiments the outward protrusion in the shock front after the detonation passes the gap is now in the shape of a notch.
- The second film initiates almost immediately without allowing the air shock from the first film to create an outward protrusion:
  - Due to a lower run distance in the CTH films.



Experimental image.

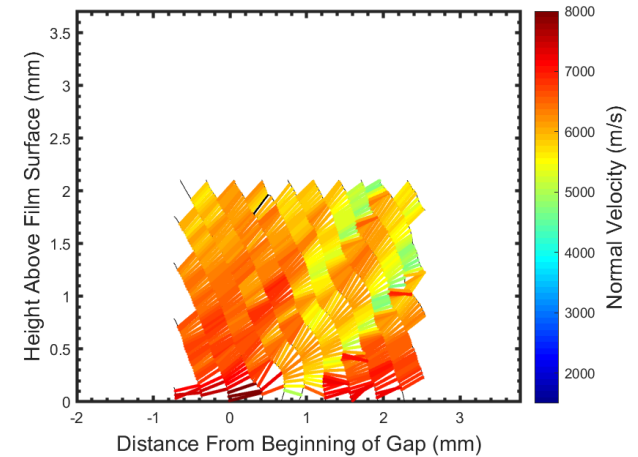
CGS image.

CTH density image.

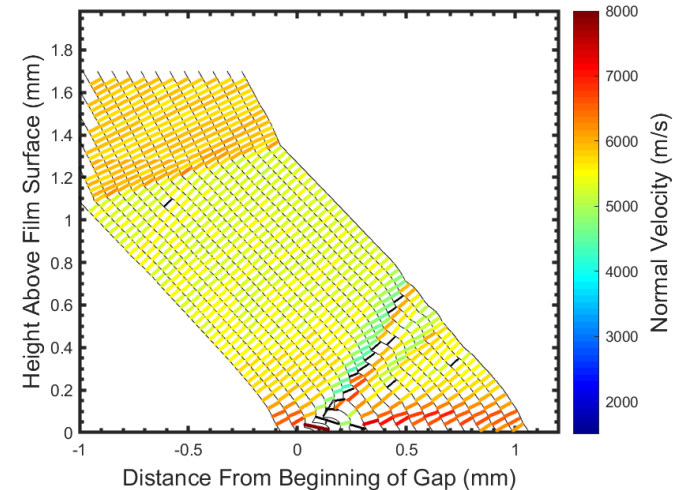
# There is significantly less disruption to the shock front in CTH

- The disruption in the shock front returns to steady-state rapidly.
- The distance to a steady-state wave shape is significantly shorter than in the experiments.

Expt./ CTH	Film Thickness ( $\mu\text{m}$ )	Gap Width ( $\mu\text{m}$ )	Distance to steady state wave shape
Experimental	200	25	875 $\mu\text{m}$
CTH	200	100	200 $\mu\text{m}$



200  $\mu\text{m}$ -thick film experimental gap test with a 25  $\mu\text{m}$ -gap-width.



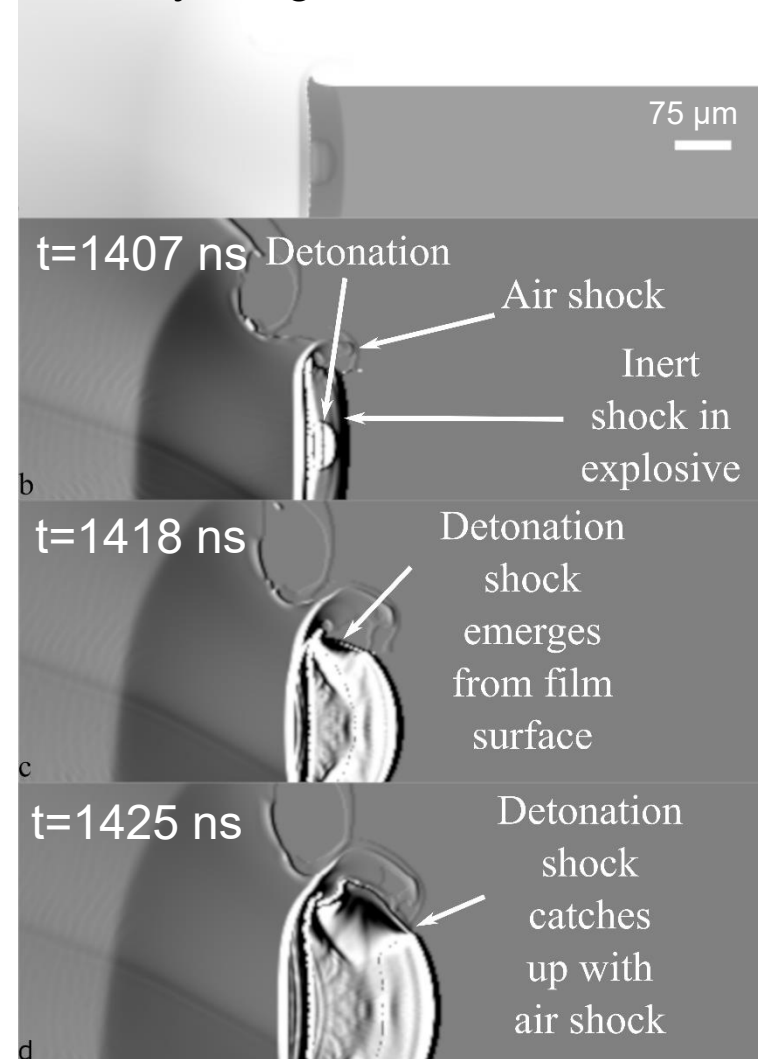
200  $\mu\text{m}$ -thick film gap test with a 100  $\mu\text{m}$ -gap-width.



# Distance to steady-state state wave shape

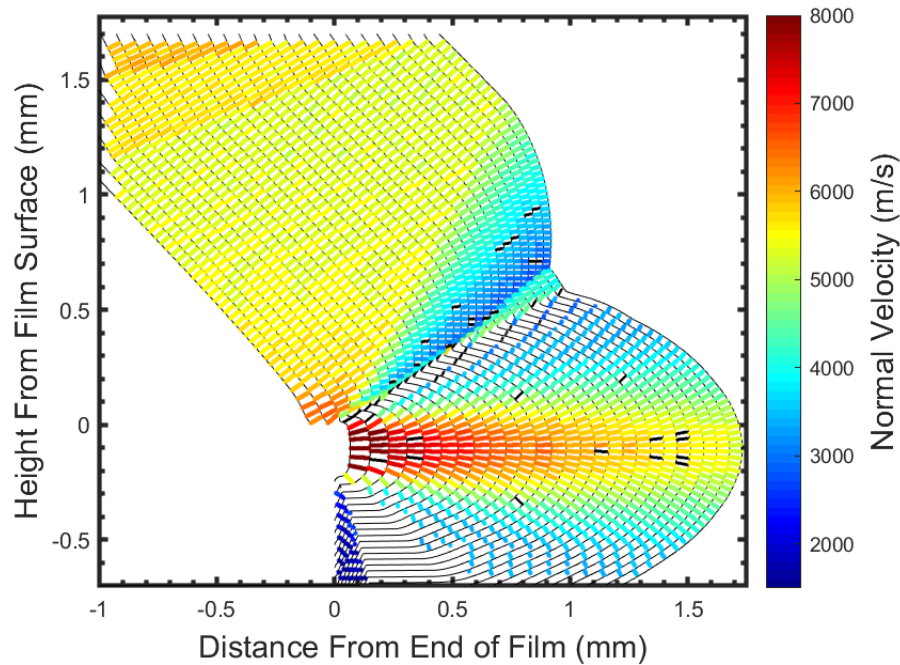
- Detonation in film is seen in CGS images with a histogram shift.
- At  $t=1407$  ns, film has already initiated and detonation propagates outward.
- At  $t=1418$  ns, detonation emerges from film surface.
  - Detonation is significantly behind the air shock.
- At  $t=1425$  ns, detonation catches up with air shock from initial film.

Density image at  $t=1407$  ns

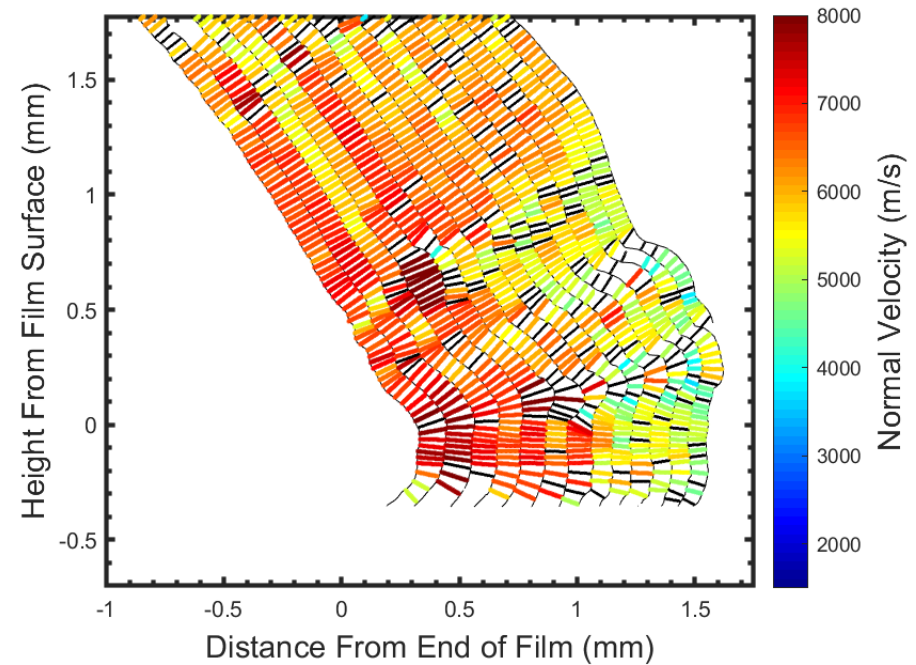


# CTH infinite gap test

- There is a significant drop in velocity above and below the film height, that is not seen in experimental images.



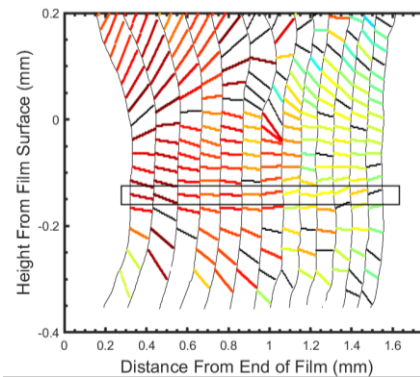
CTH infinite gap velocity plot.



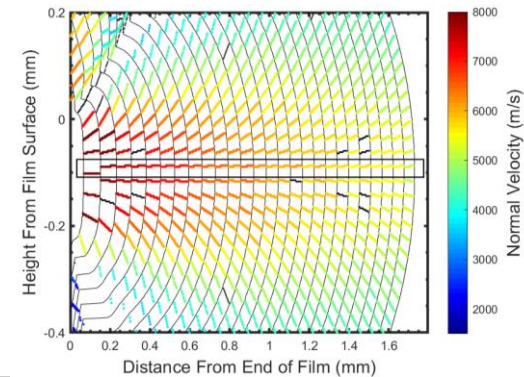
Experimental infinite gap velocity plot.

# The trend between the CTH and experimental data matches fairly well.

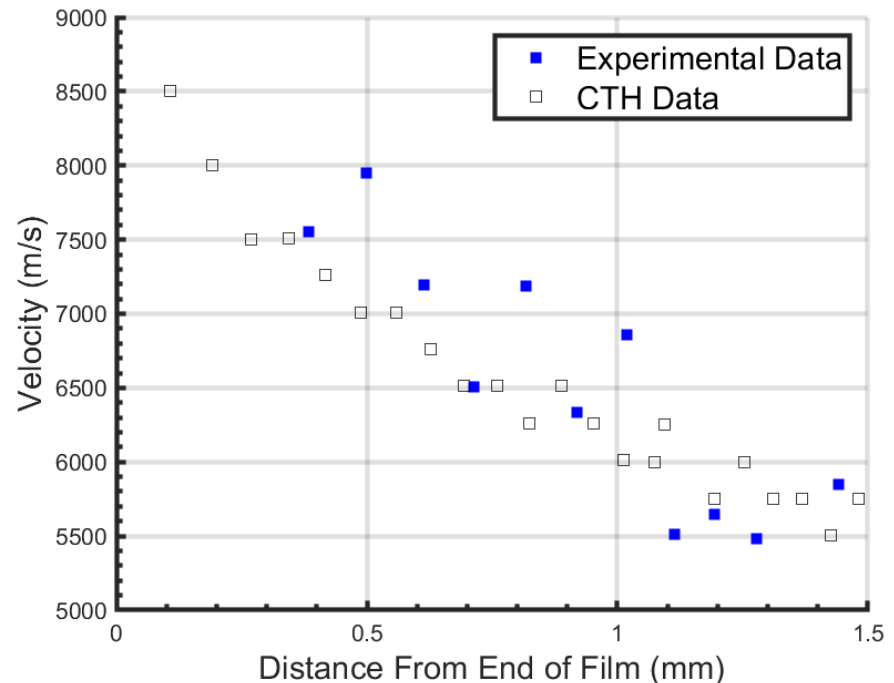
- Computational data trend was slightly lower than trend of experimental data.
  - Expected since the 200  $\mu\text{m}$ -thick PETN films in experiments had a higher detonation velocity than 200  $\mu\text{m}$ -thick PETN films in simulations.



Experimental data



CTH data



# Experiments and computations were performed to visualize PETN films detonating across microcracks

- A new image processing algorithm was developed to:
  - Extract spatial data.
  - Quantify velocity:
    - Locally across dynamic wave shapes.
    - Of a pressure driven flow.
- CTH model provided further insight of experiments.
- As a result:
  - A critical gap width was determined.
  - Cracks were found to cause a large disturbance in the shock front.
    - Significantly larger than the crack itself.



# Future work

- Perform statistical analysis to ascertain repeatability of gap test results.
- Develop an algorithm to calculate the average uncertainty in velocity found in the normal velocity plots.

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This report describes objective technical results and analysis. Any subjective views or opinions that might be expressed in the paper do not necessarily represent the views of the U.S. Department of Energy or the United States Government. Unclassified, unlimited release  
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# Backup Slides

# Gap Test Failure Tables

70  $\mu\text{m}$ -thick film failure table

Film Thickness ( $\mu\text{m}$ )	Gap Width ( $\mu\text{m}$ )	Detonation Propagation	Substrate
70	0	No	Oxidized Al
70	0	No	Bare Al
70	10	No	Oxidized Al
70	10	No	Bare Al
70	25	No	Oxidized Al
70	25	No	Bare Al
70	50	No	Oxidized Al
70	50	No	Bare Al

200  $\mu\text{m}$ -thick film failure table

Film Thickness ( $\mu\text{m}$ )	Gap Width ( $\mu\text{m}$ )	Detonation Propagation
200	25	Yes
200	25	Yes
200	25	Yes
200	25	Yes
200	25	Yes
200	50	Yes
200	50	Yes
200	75	Yes
200	75	Yes
200	80	Yes
200	75-120	Yes
200	93	No
200	95	No
200	100	No
200	110	Yes
200	110	No
200	170	No

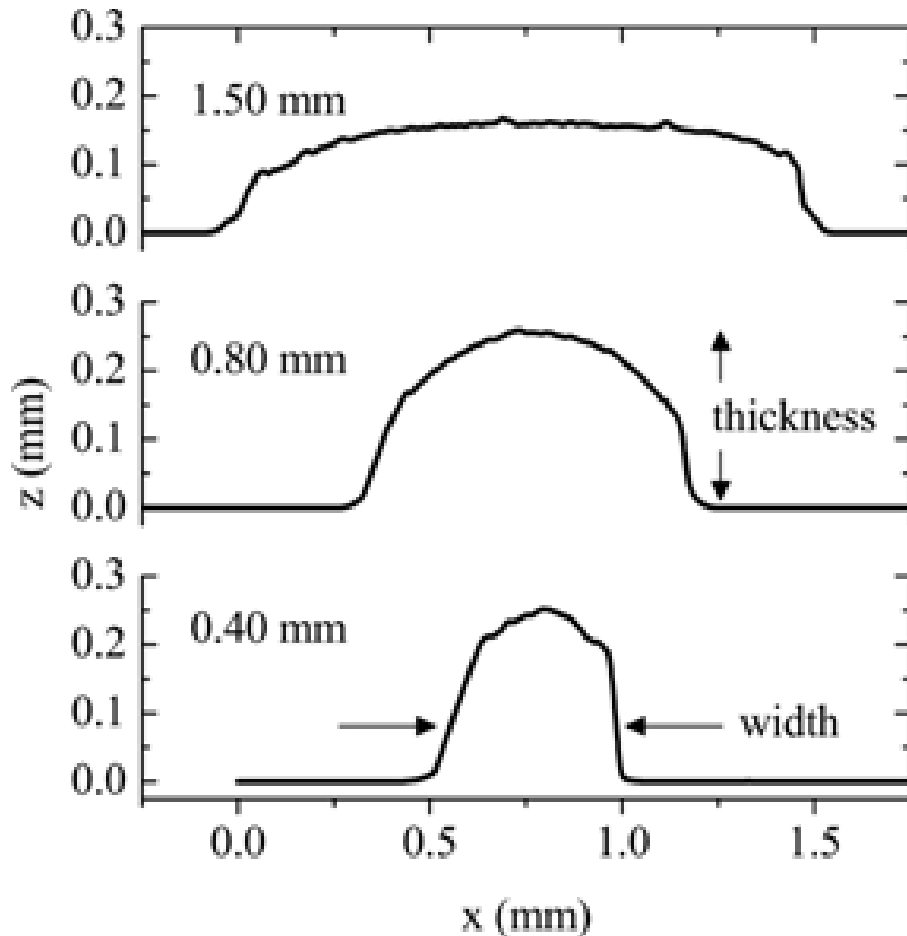
Note: the film with the gap width of 75-120  $\mu\text{m}$  is due to a rough edge.

400  $\mu\text{m}$ -thick film failure table

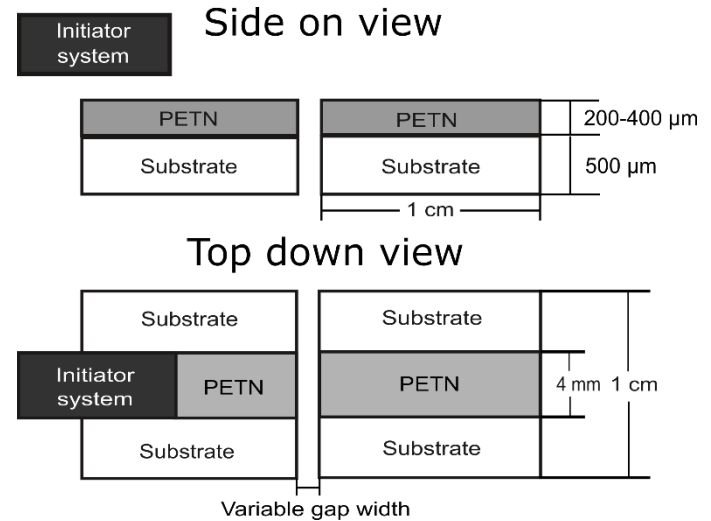
Film Thickness ( $\mu\text{m}$ )	Gap Width ( $\mu\text{m}$ )	Detonation Propagation
400	80	Yes
400	100	Yes
400	125	Yes
400	160	Yes
400	180	Yes
400	180	Yes
400	200	Yes
400	200	No
400	220	yes



# Rounded Edges of PETN Films



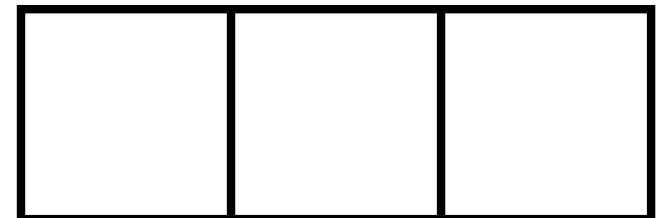
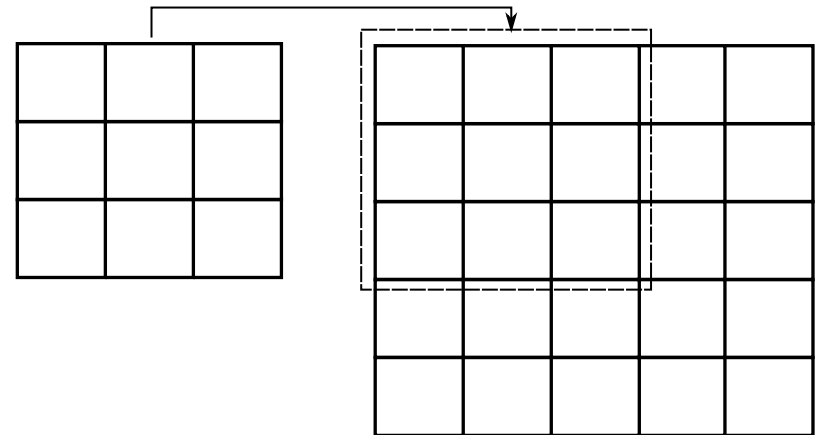
Surface profilometer measurements of PETN films deposited at various widths [Tappan 2010]. The view is from the front.



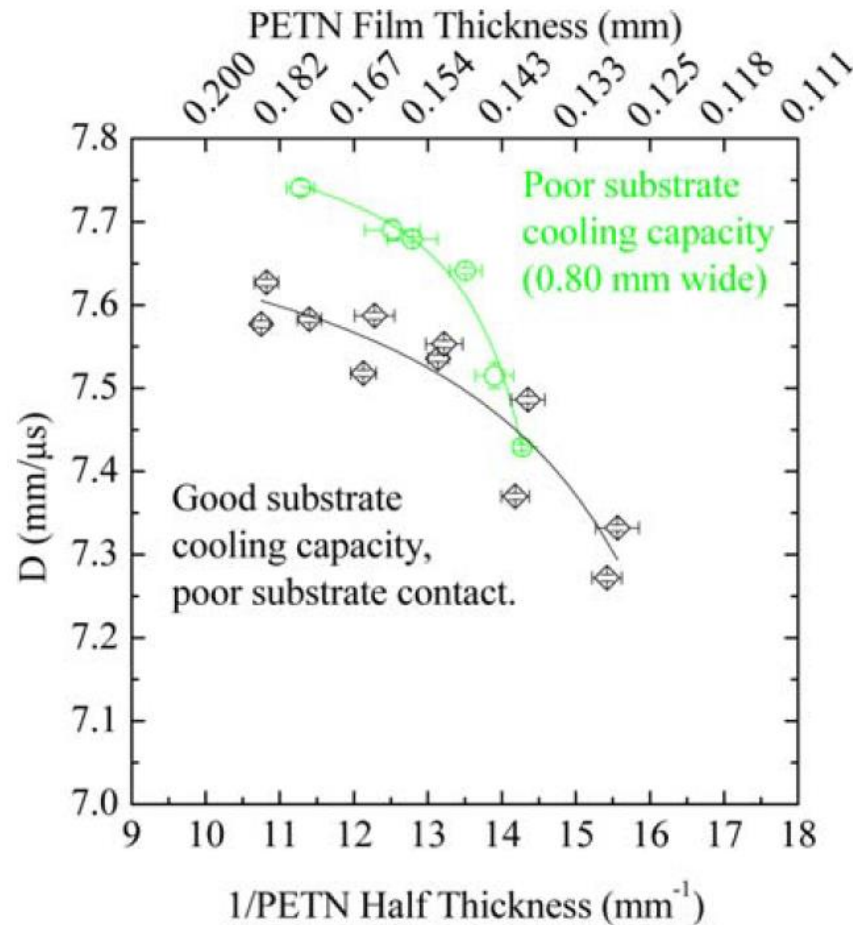
# Computation of the Derivative of the Density Field

- A center difference numerical derivative can be performed with the equation shown.
- Spatial Filtering [Gonzalez 2009] can be used to perform the numerical derivative.
- Spatial filtering is performed by applying a mask composed of multiplication factors,  $C_i$ , to a region of pixels on the image.
- Applying the mask shown on the bottom yields the same answer as the numerical derivative shown above.

$$\frac{dx}{dy} = \frac{x_{n+h} - x_{n-h}}{2h}$$



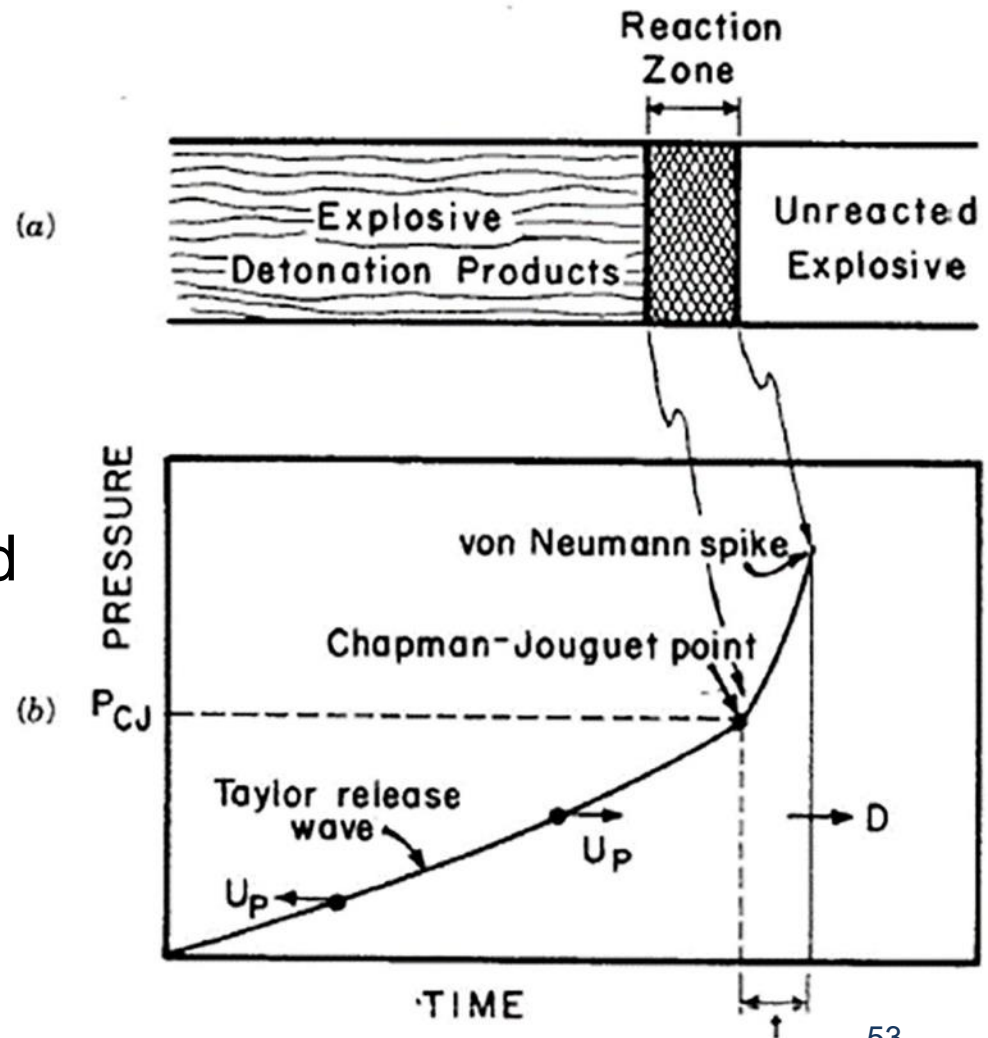
# Unconfined PETN Critical Detonation Thickness



[Tappan2012]

# Detonation is a rapid combustion driven by shock

- A chemical reaction in an explosive is initiated by a shock wave propagating through the explosive.
- The energy produced by this chemical reaction drives the shock front and thus the detonation.

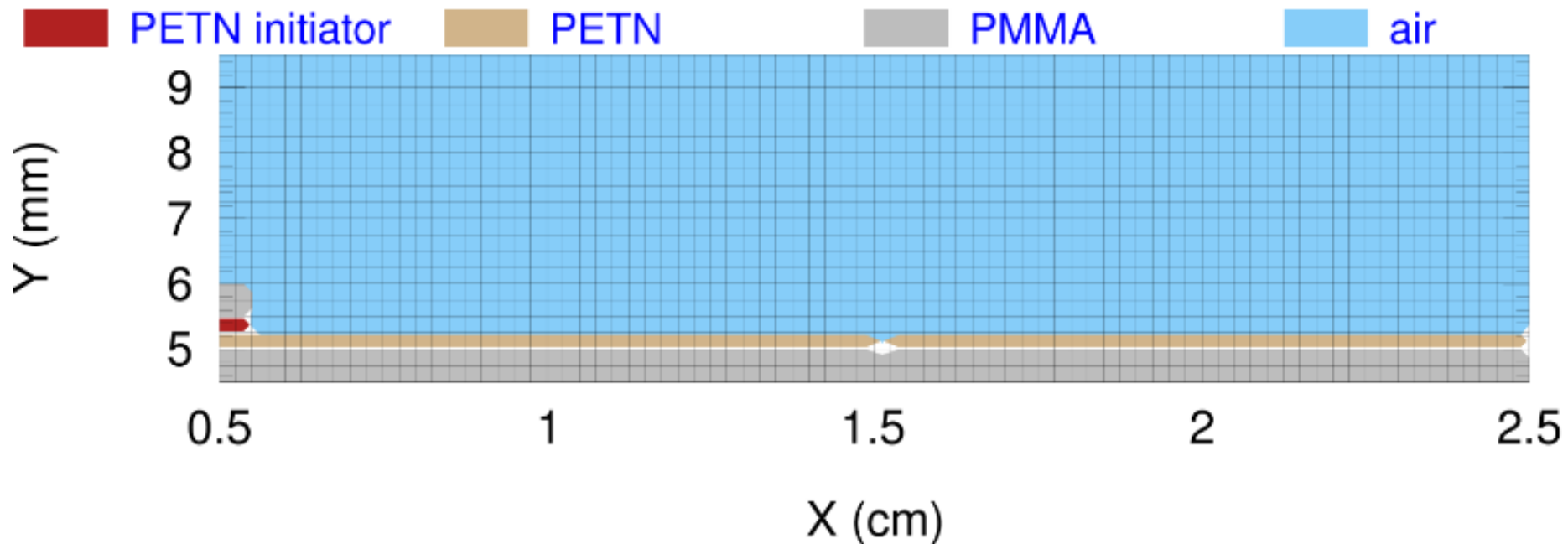




# Burn Rate Calibration

- The burn models are typically calibrated with shock-to-detonation experiments, such as the wedge test [Menikoff2010, Starkenberg2002].
- The wedge test is used to determine the run distance versus input pressure.
- The run distance is the length an input pressure needs to travel before initiation.

Mesh resolution was 8000 x 2000 cells.



2D model with 80 x 20 mesh grid overlay. Each cell represents a 100 x 100 cell grid.