

Empty Room Closure Research Plan



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Jake Koester



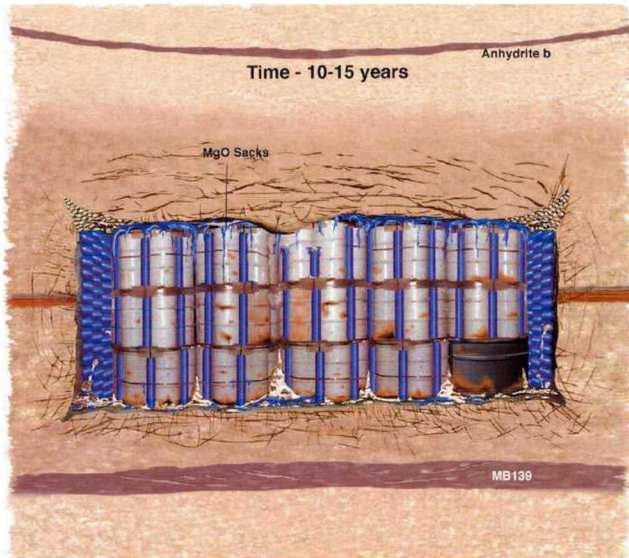
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1. Motivation
2. Research Plan Outline
3. Potential Numerical Methods
 - a. Finite element methods
 - b. Particle methods
 - c. Meshless methods
4. Meshless Method Assessment
 - a. Creep Closure
 - b. Damage and Fracture
 - c. Rubble Pile Compaction
5. Tentative Project Schedule

Motivation

Filled Room Closure vs. Empty Room Closure

Filled Rooms



Empty Rooms



Fracturing Around Empty Rooms

1. Controls the size and character of the rubble pile.

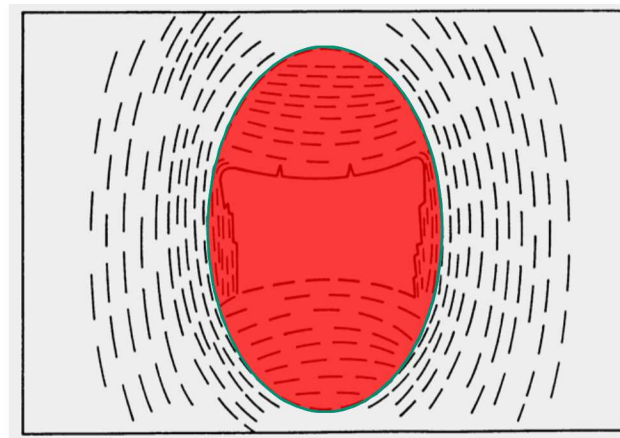
Lower Horizon



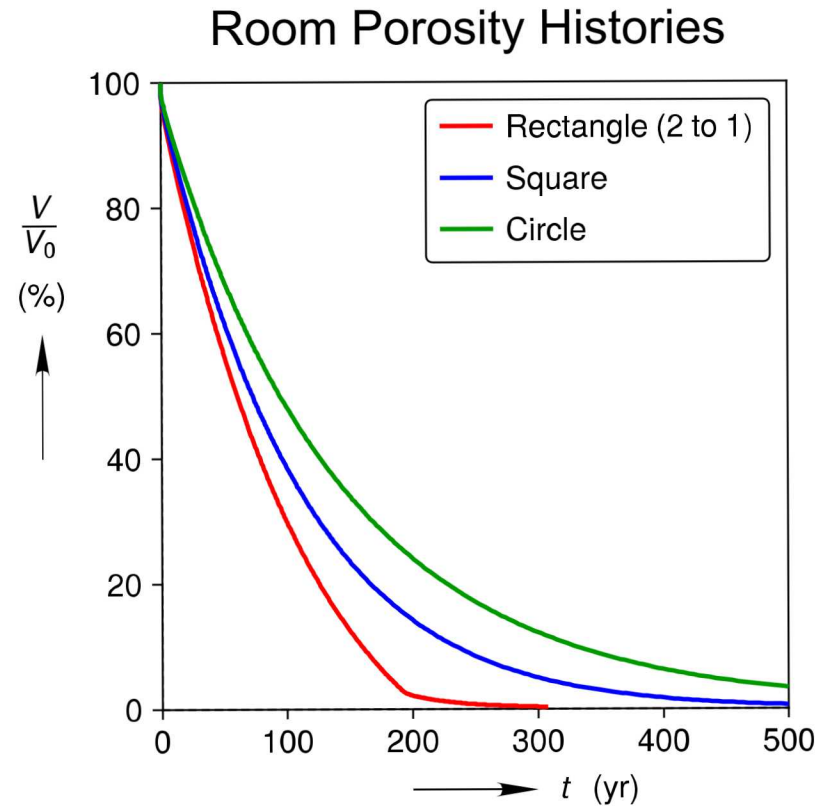
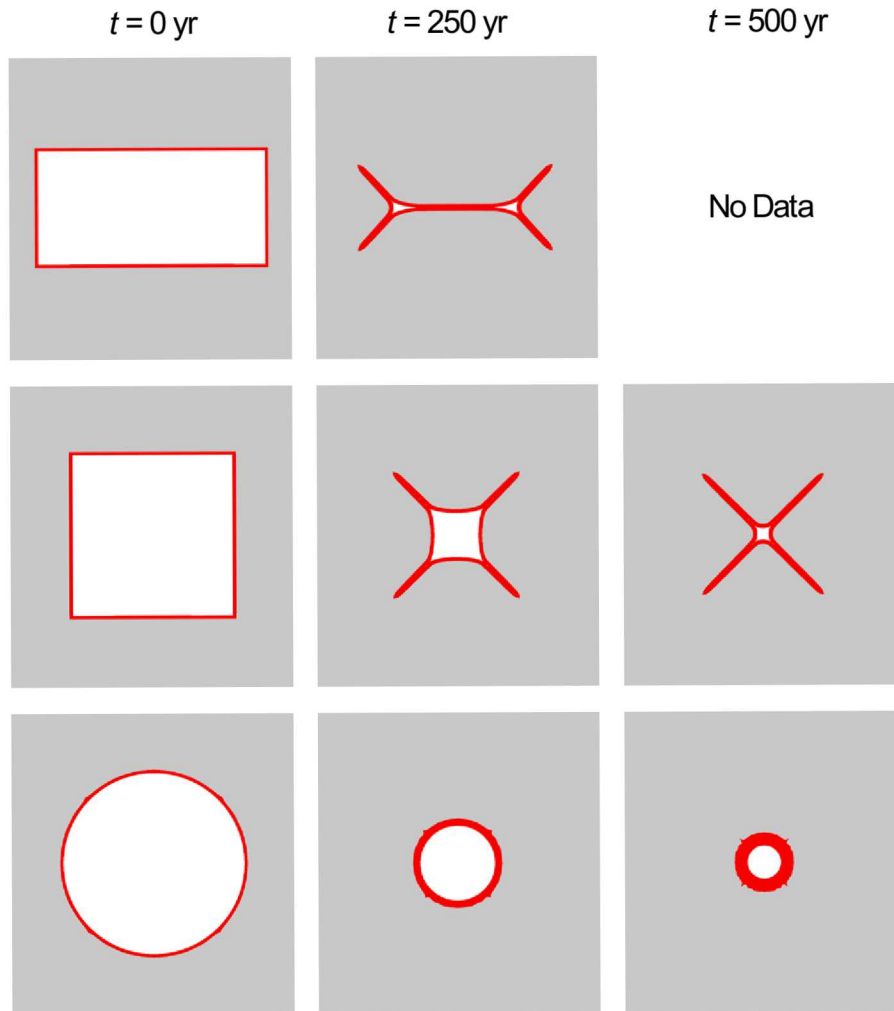
Upper Horizon



2. Changes room cross-section to a more stable, enduring, shape.



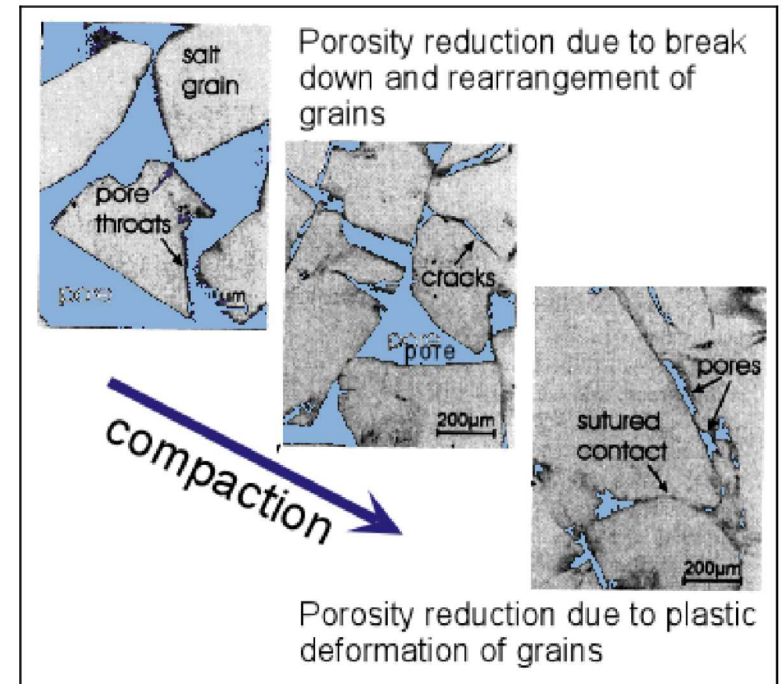
Room Shape affects Creep Closure



Rubble Pile Compaction

1. Important Processes

- a. Rubble reorganization
- b. Rubble fracture
- c. Creep
 - i. Dislocation
 - ii. Pressure solution

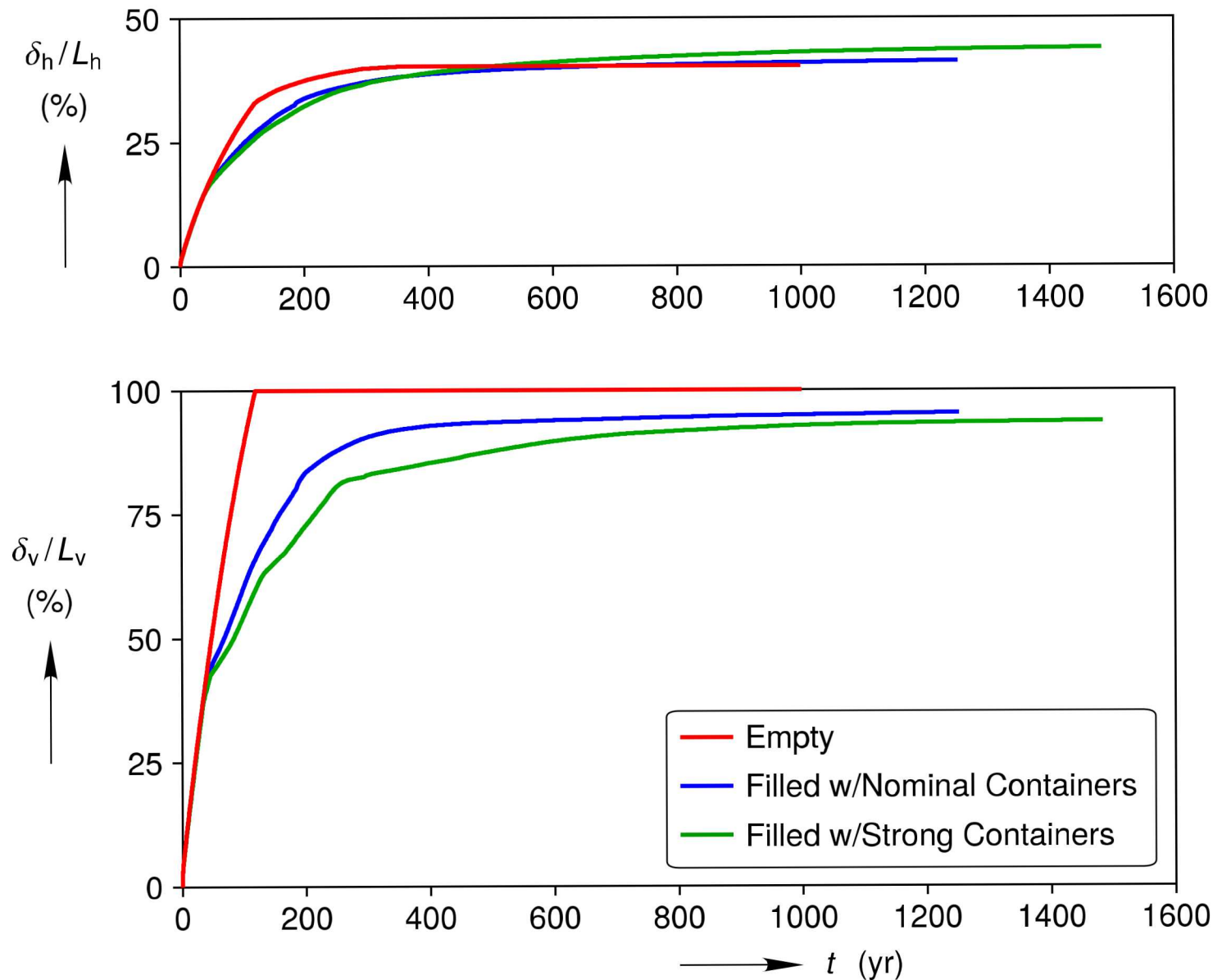


Spangenberg (1998) (Modified)

2. Impact

- a. Compaction processes control flow pathways
 - i. Two samples with same porosity can have different permeability
- b. Rubble pile supplies back pressure to surrounding rock formation
 - i. Larger rubble likely compacts slower than smaller rubble

Filled Rooms Creep Closed More Slowly



Crushed Salt vs. Rubble Pile

Crushed Salt



Bechthold, W., et. al. (2004). Backfilling and Sealing of Underground Repositories for Radioactive Waste in Salt (BAMBUS II Project), Final Report. European Commission, EUR 20621 EN

Rubble Piles



Nov 2016
Panel 7, Room 4



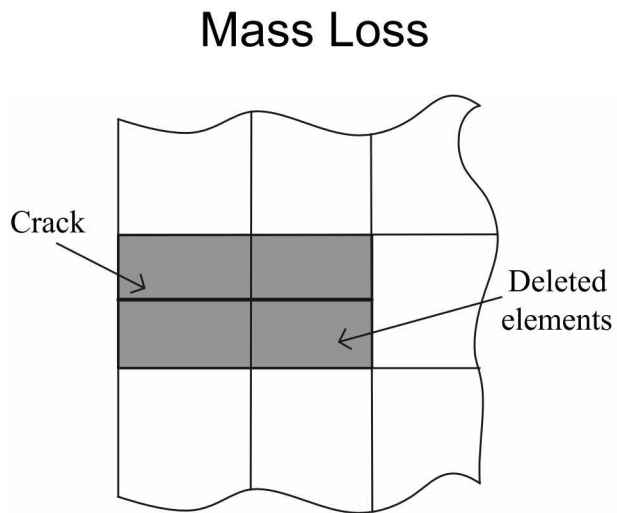
Sept 2016
E300-S3650

Research Plan Outline

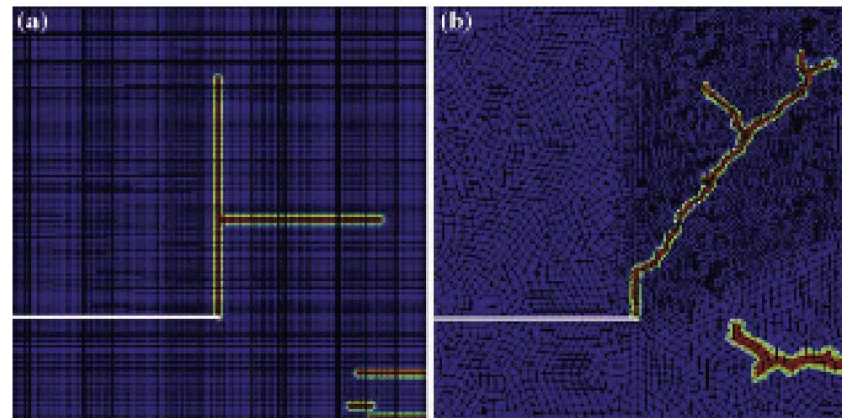
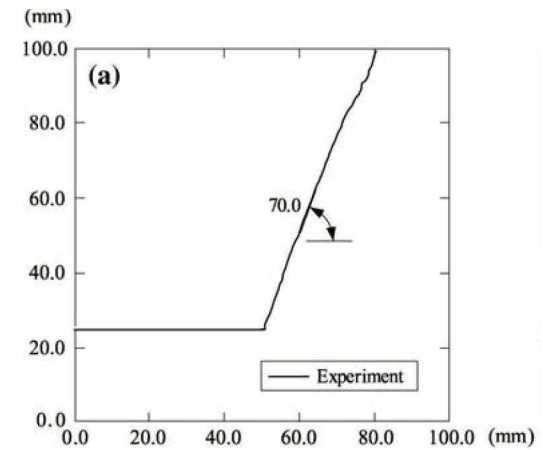
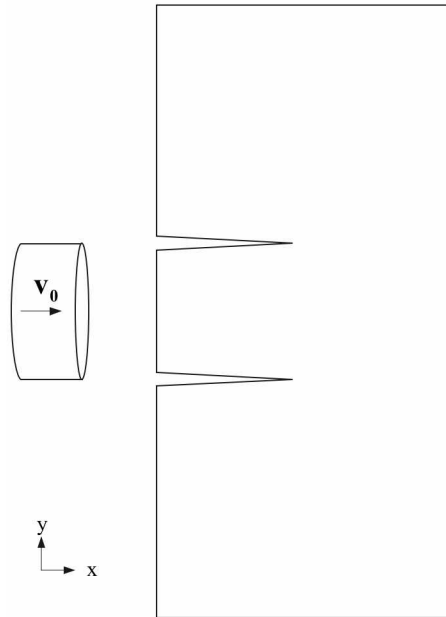
1. Creep closure
 - a. Already partially validated by room D, G, and Q data
2. Roof falls
 - a. Attempt to predict size and shape of roof falls
 - i. Stochastic distribution of defect sites?
 - b. Validate against lab-scale room collapse experiments and observations at WIPP
3. Rubble pile compaction
 - a. Flow channels
 - i. Explicitly represent macroflow channels
 - ii. Implicitly represent microflow channels
 - b. Ignore healing for now
 - c. Validate against crushed salt experiments
 - i. Vary grain size distribution
 - ii. Vary temperature and compaction pressure

Potential Numerical Approaches

1. Fundamental issue: we are trying to capture a discrete crack with a continuum level model
2. Potential numerical issues
 - a. Mass loss
 - b. Mesh structure dependence
 - c. Mesh size dependence
3. Candidate numerical methods
 - a. Finite elements with element death
 - b. Finite element with interelement cracks
 - c. Particle methods
 - d. Meshless methods

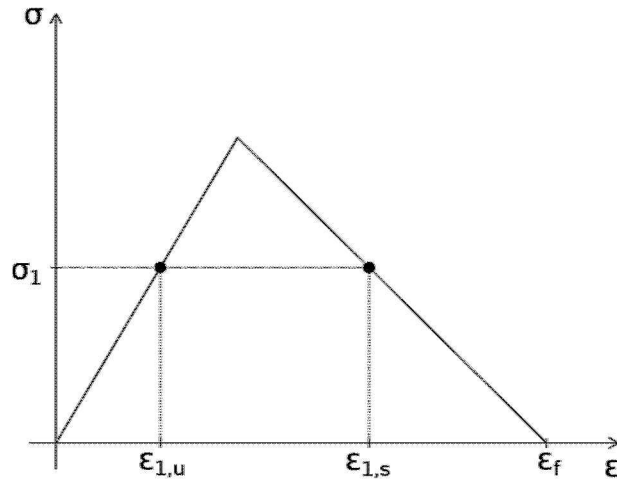


Mesh Structure Dependence

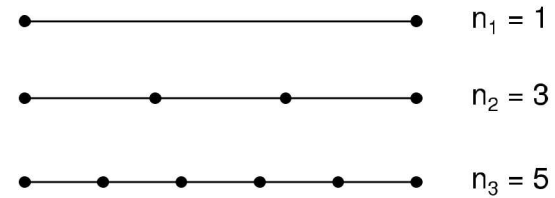


1D Example of Strain Softening Instability

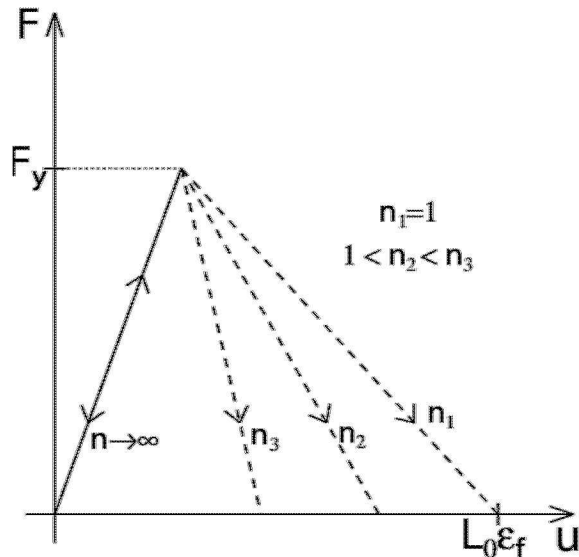
Local Stress-Strain Behavior



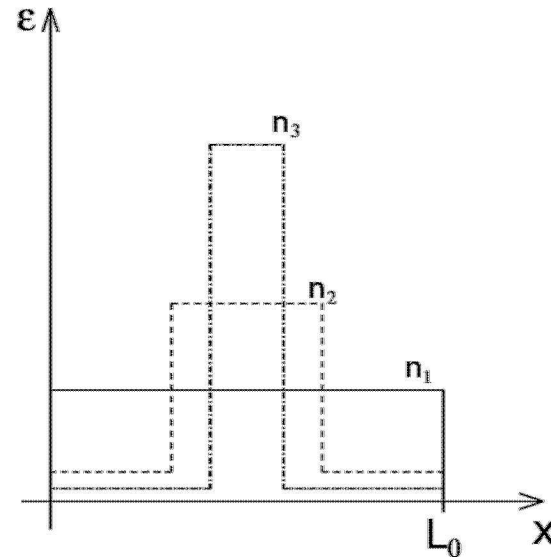
1-D Bar Meshes



Force-Displacement Behavior

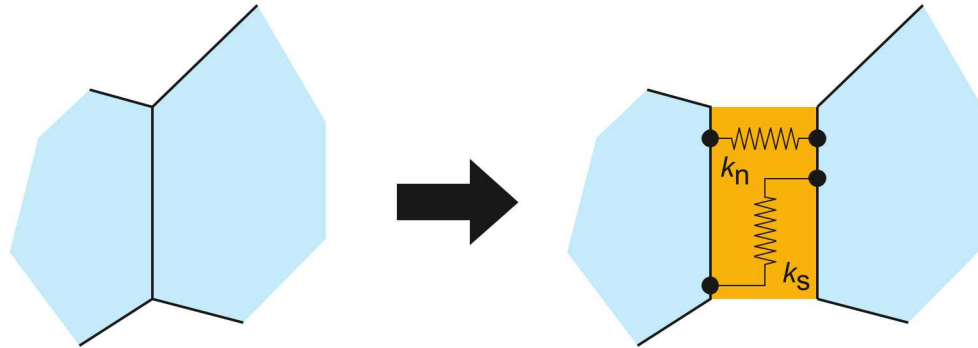


Strain Distribution

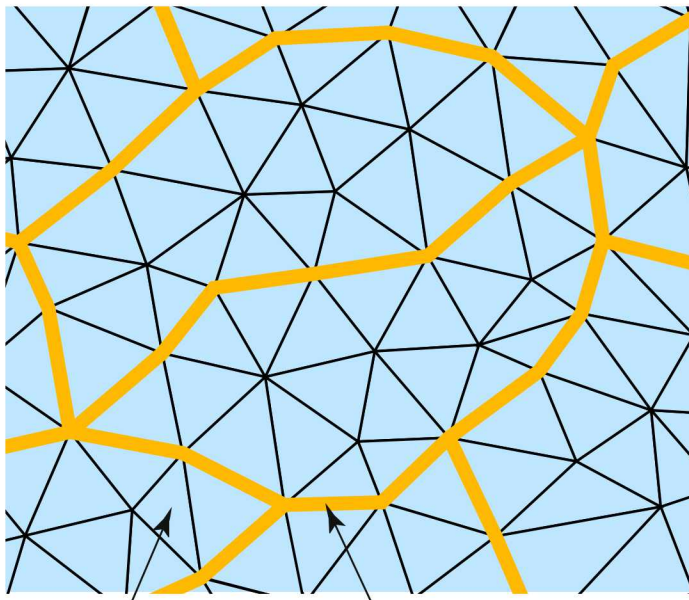


Interelement Crack Method

Cohesive Zone Element Insertion



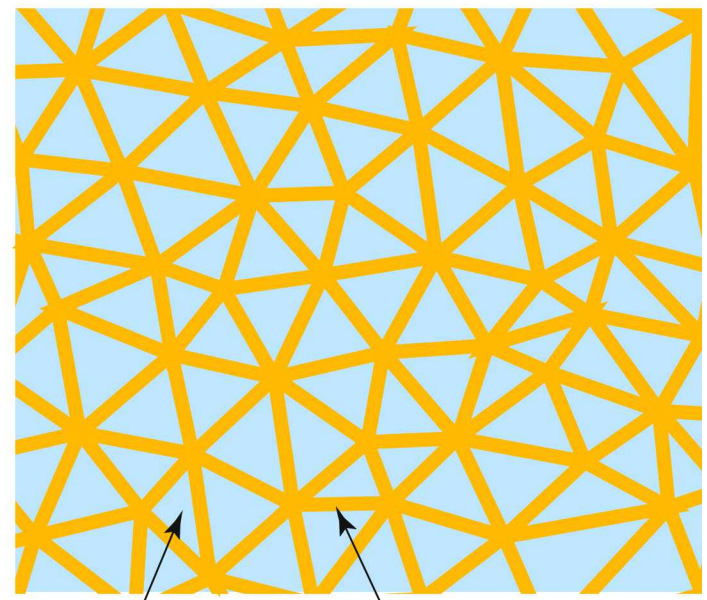
Selective Insertion



deformable
element

cohesive zone
element

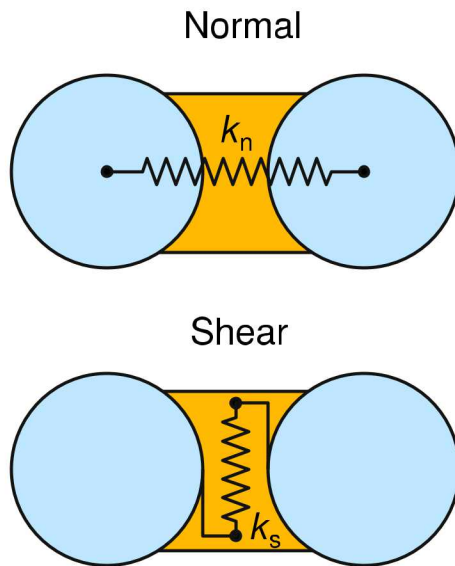
Blanket Insertion



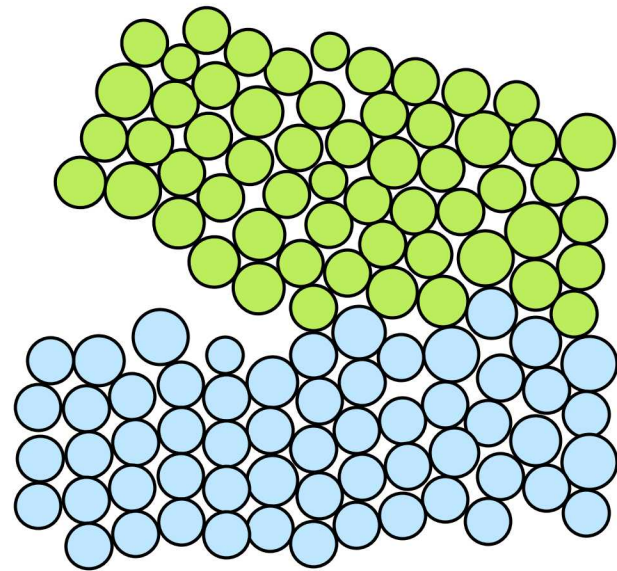
deformable
element

cohesive zone
element

Particle-to-Particle Interactions



Particle Method Fracture

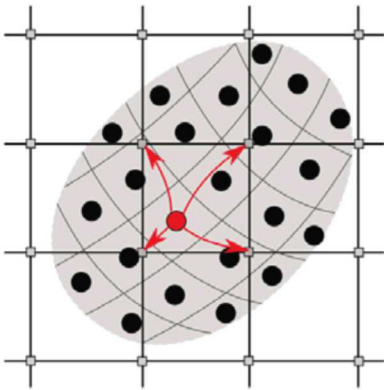


Material Point Method (MPM)

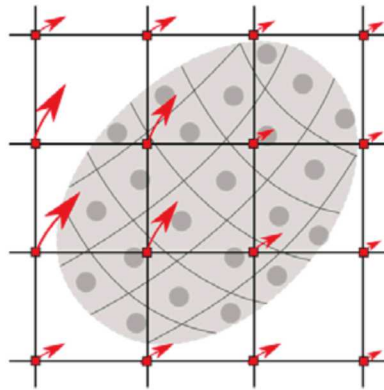
1. Descendent from Particle in Cell (PIC) method.
2. First published paper in 1994. Cited 943 times.
3. Codes
 - i. MPM Sim (Commercial)
 - ii. Anura3D (International Collaboration)
 - iii. Uintah (Open Source)
4. Miscellaneous
 - i. Used heavily by the computer graphics community
 - ii. Fern, J., et al. The Material Point Method for Geotechnical Engineering: A Practical Guide. 2019. CRC Press

Material Point Method (MPM)

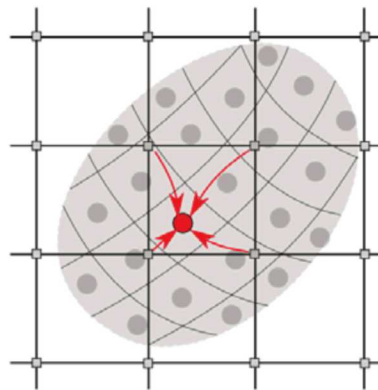
Evaluate material model and map info to nodes



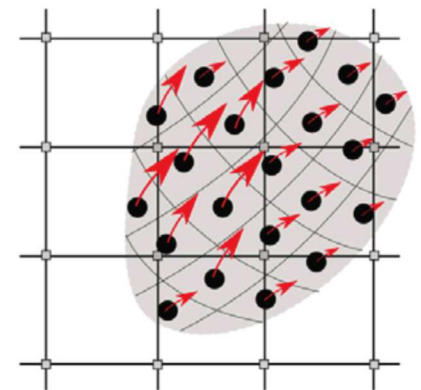
Solve equations of motion



Map accelerations to material points



Update positions of material points



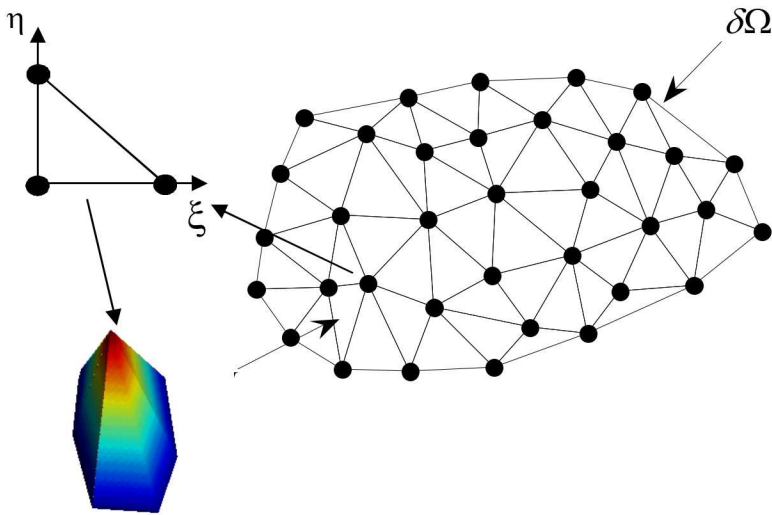
Reproducing Kernel Particle Method (RKPM)

1. Descendent from Smoothed Particle Hydrodynamics (SPH)
2. First published paper in 1996. Cited 828 times.
3. Codes
 - a. LS-DYNA has a RKPM capability
 - b. Sierra has a fledgling RKPM capability
4. 1500 has two staff who studied RKPM for their doctorate

Reproducing Kernel Particle Method (RKPM)

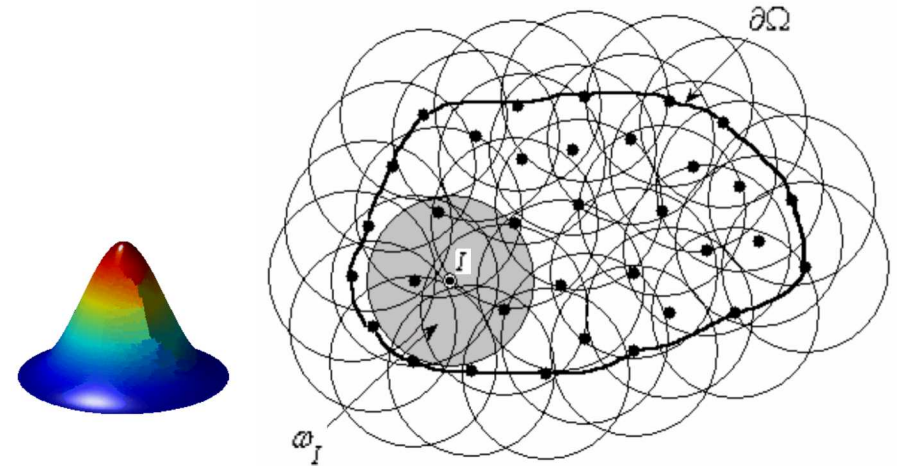
Finite Element Method

Shape functions and integration are both defined on the element domain.

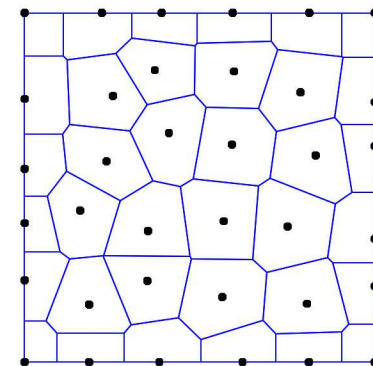


RKPM

Shape Functions



Domain Integration



1. Primary advantages
 - a. Designed to handle severe deformation ($>100\%$ strain)
 - b. Inherently captures normal contact without expensive interface tracking
 - c. Regularization techniques are relatively easy to implement
 - d. Adaptive particle insertion and deletion is relatively easy
 - e. Can utilize classical continuum material models
 - f. Healing just needs to be added to the material model
2. Primary drawbacks
 - a. Potential longer run times
 - b. Sliding contact is challenging
 - c. Surfaces must sufficiently separate to stop interacting
3. Sandia's nuclear weapon program will likely continue to invest in meshless methods



Assessment of Meshless Methods

1. Goal: Assess whether meshless methods are well suited to the simulation empty underground room closure in rock salt.
 - a. Identify which approaches work and which do not
2. Capability demonstration, not intensive code development
 - a. Minor code development is OK
3. Collaborate with Sandia to incorporate successful approaches into Sandia code(s).
 - a. Approaches should be implemented with an eye on production

Problem #1: Creep Closure

1. Supplied by Sandia:
 - a. Creep material model
 - b. Initial boundary value problem
 - c. Finite element results
2. Assess whether a chosen meshless method can accurately simulate 2D room closure due to creep alone (no fracturing)
 - a. Show discretization convergence
 - b. Record total CPU time
3. Compare discretization converged meshless simulation against a finite element simulation
 - a. Horizontal and vertical closure histories
 - b. Room porosity histories

Simple Odqvist Creep Model

Strain Decomposition

$$\dot{\boldsymbol{\varepsilon}} = \dot{\boldsymbol{\varepsilon}}^{\text{el}} + \dot{\boldsymbol{\varepsilon}}^{\text{vp}}$$

Isotropic, Linear, Hypoelasticity

$$\dot{\boldsymbol{\sigma}} = \mathbf{C} : \dot{\boldsymbol{\varepsilon}}^{\text{el}}$$

$$\mathbf{C} = (B - 2\mu/3) \mathbf{I} \otimes \mathbf{I} + 2\mu \mathbf{I}$$

Associated Flow Rule

$$\dot{\boldsymbol{\varepsilon}}^{\text{vp}} = \dot{\boldsymbol{\varepsilon}}^{\text{vp}} \frac{\partial \bar{\sigma}}{\partial \boldsymbol{\sigma}}$$

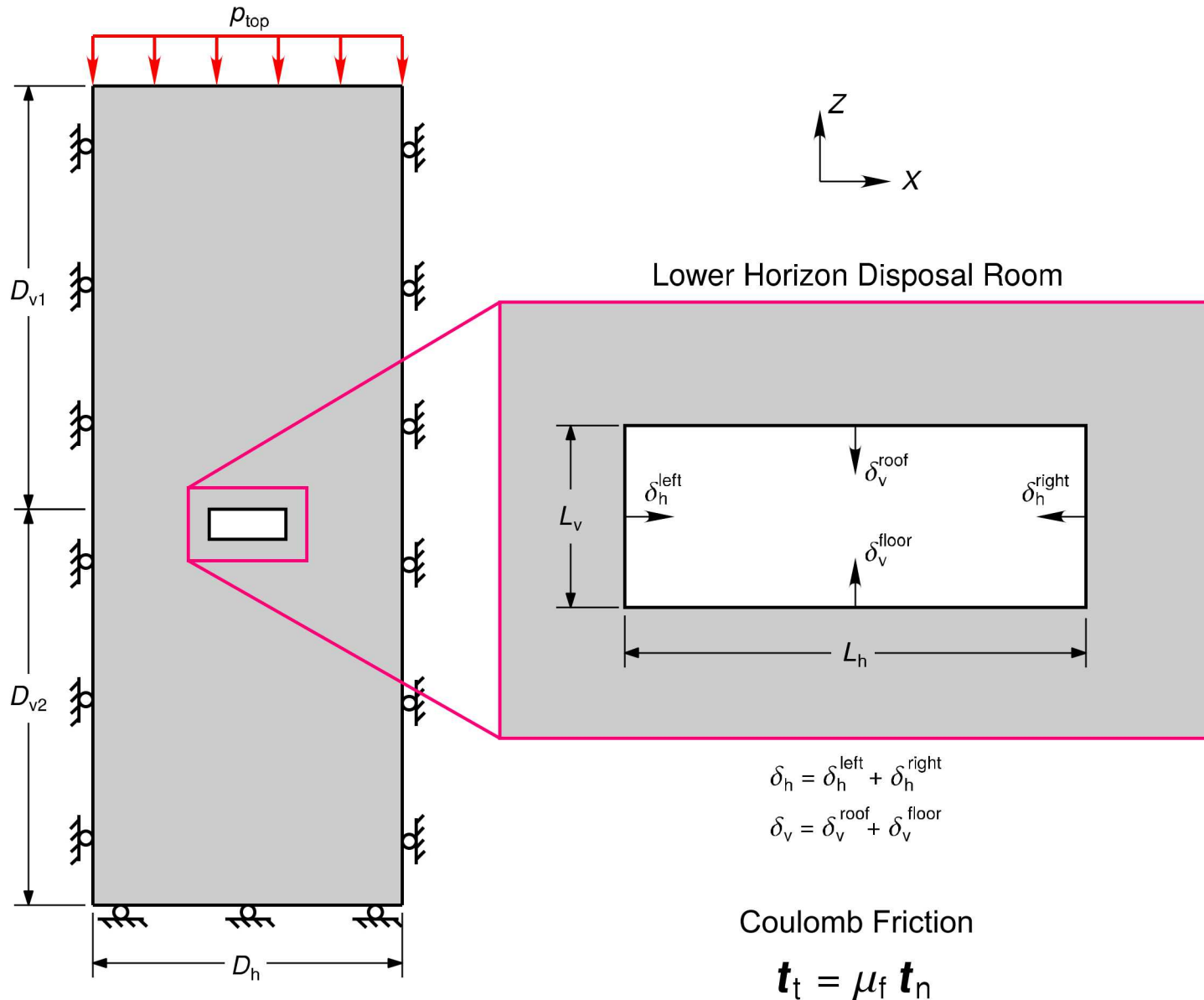
von Mises Equivalent Stress

$$\bar{\sigma} = \sqrt{3 J_2}$$

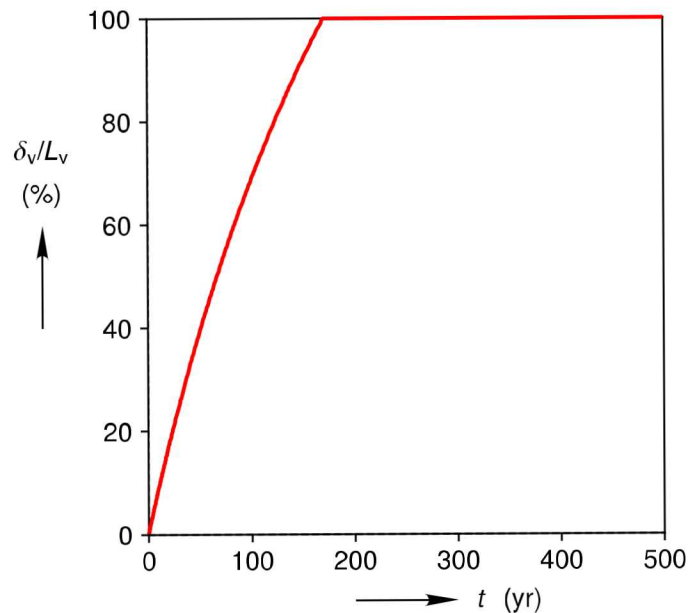
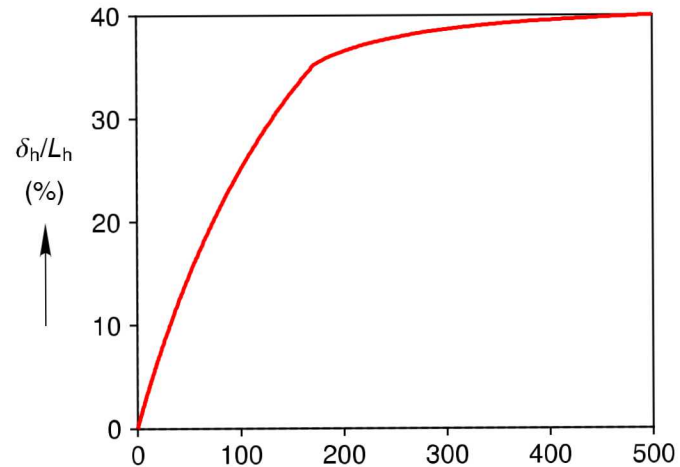
Equivalent Viscoplastic Strain Rate

$$\dot{\boldsymbol{\varepsilon}}^{\text{vp}} = \sum_{i=1}^2 A_i \left(\frac{\bar{\sigma}}{\mu} \right)^{n_i}$$

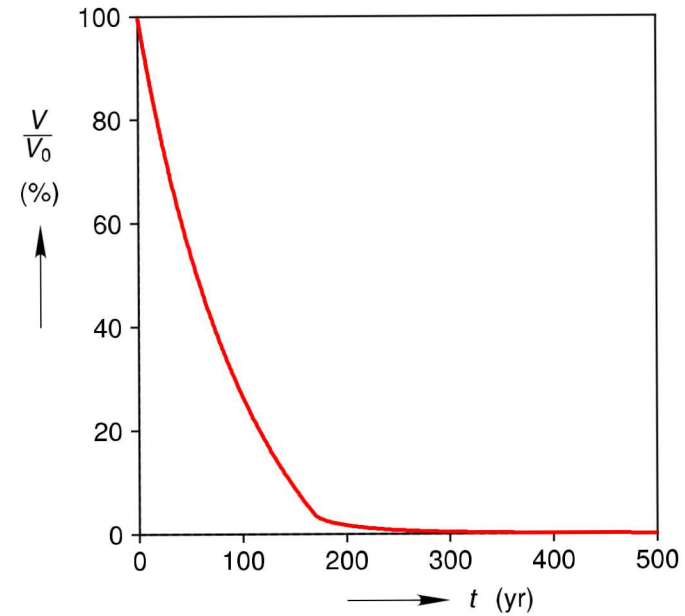
Creep Closure Simulation Setup



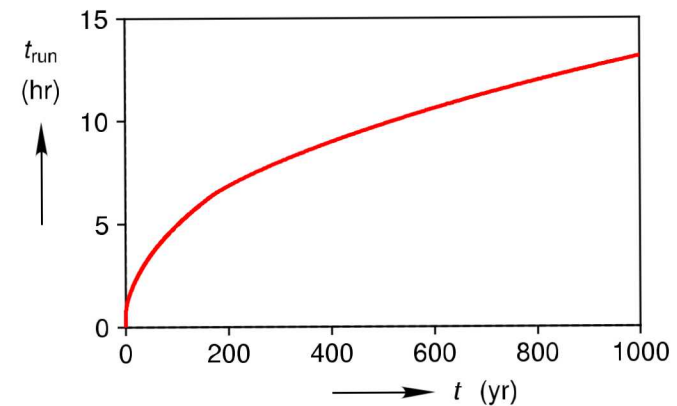
Horizontal and Vertical Closure Histories



Room Porosity History



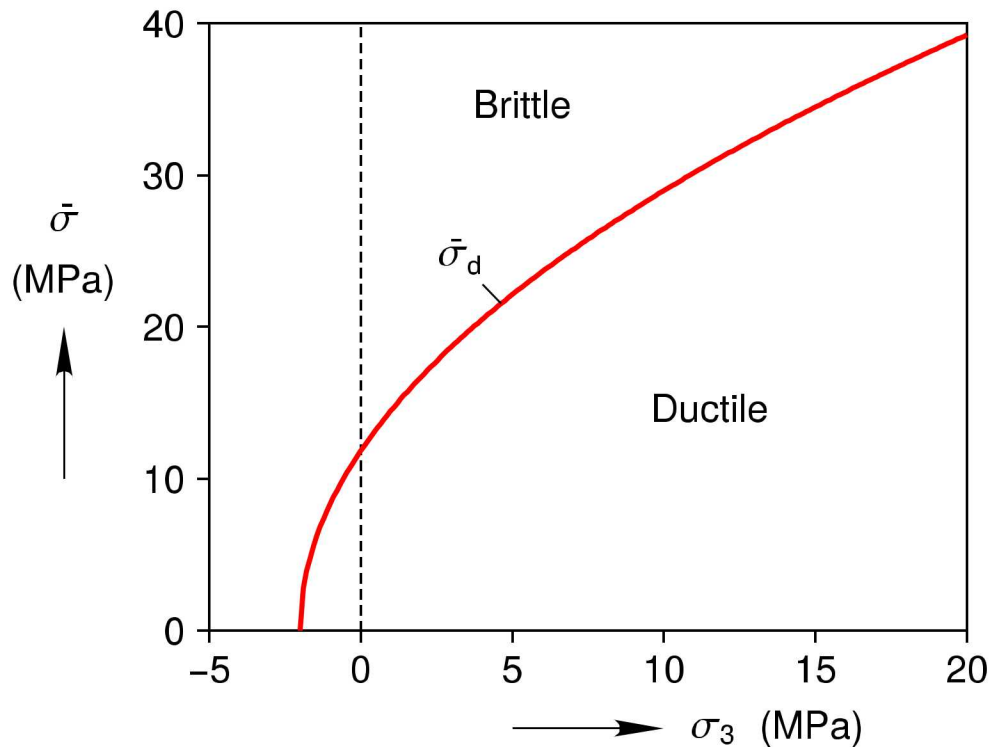
Run Time



Problem #2: Fracturing and Roof Falls

1. Supplied by Sandia:
 - a. Damage material model
 - b. Initial boundary value problem
2. Assess whether a chosen meshless method can simulate 2D fracturing around a room and roof falls
 - a. Show discretization convergence
 - b. Record total CPU time
3. Demonstrate 3D fracturing around a room and roof falls
 - a. Record total CPU time

Tentative Simple Damage Model



$$\bar{\sigma}_d = \sqrt{C (\sigma_3 - B)}$$

$$\dot{\omega} = \frac{\langle \bar{\sigma} - \bar{\sigma}_d \rangle \dot{\varepsilon}^{vp}}{D}$$

$$\dot{\sigma} = (1 - \omega) \mathbf{C} : \dot{\varepsilon}^{el}$$

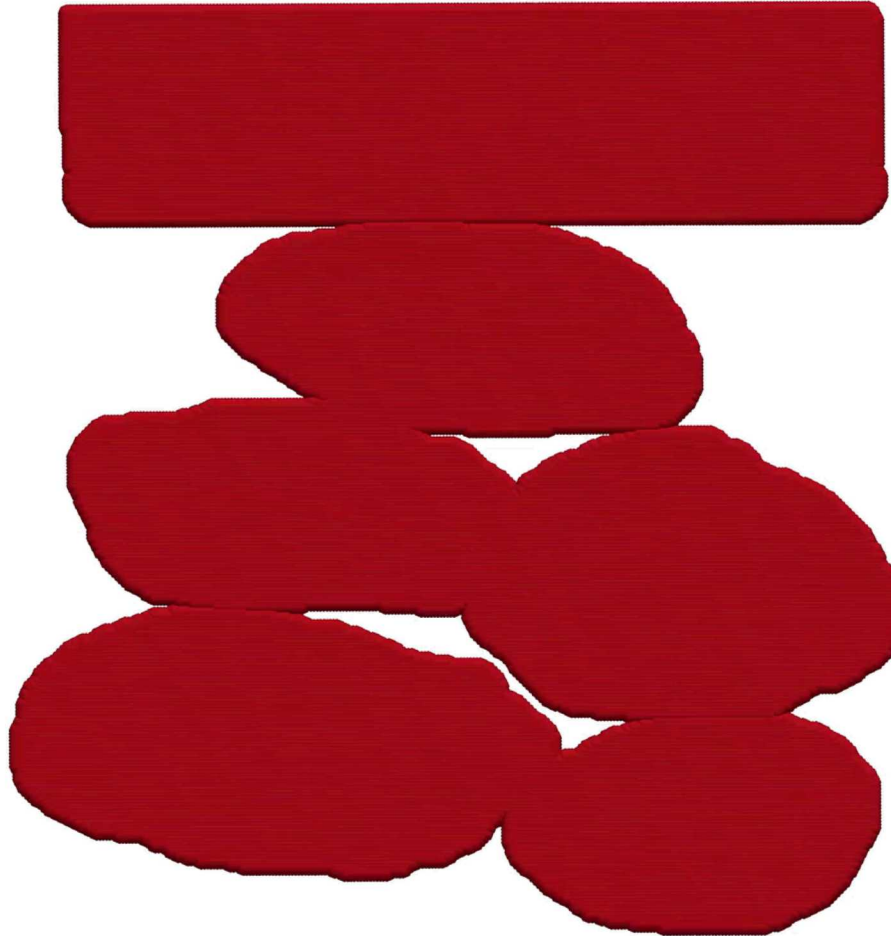
$$\dot{\varepsilon}^{vp} = \sum_{i=1}^2 A_i \left[\frac{\bar{\sigma}}{\mu (1 - \omega)} \right]^{n_i}$$

Problem #3: Rubble Pile Compaction

1. Supplied by Sandia:
 - a. Initial boundary value problem
2. Assess whether a chosen meshless method can simulate 2D rubble pile compaction due to room closure
 - a. Show room porosity discretization sensitivity
 - b. Record total CPU time
3. Demonstrate 3D rubble pile compaction
 - a. Compute room porosity history
 - b. Record total CPU time

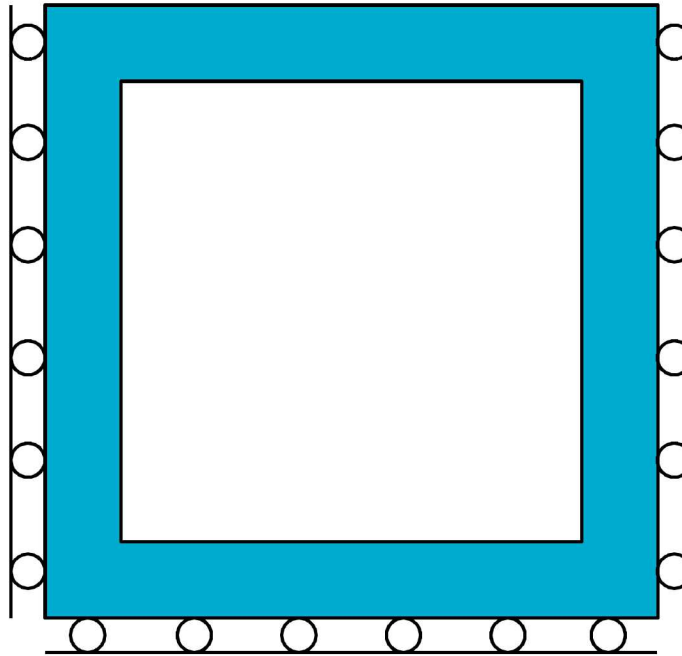
Meshless Method (Pre-)Preliminary Results

MPM Team (Pre-)Preliminary Results

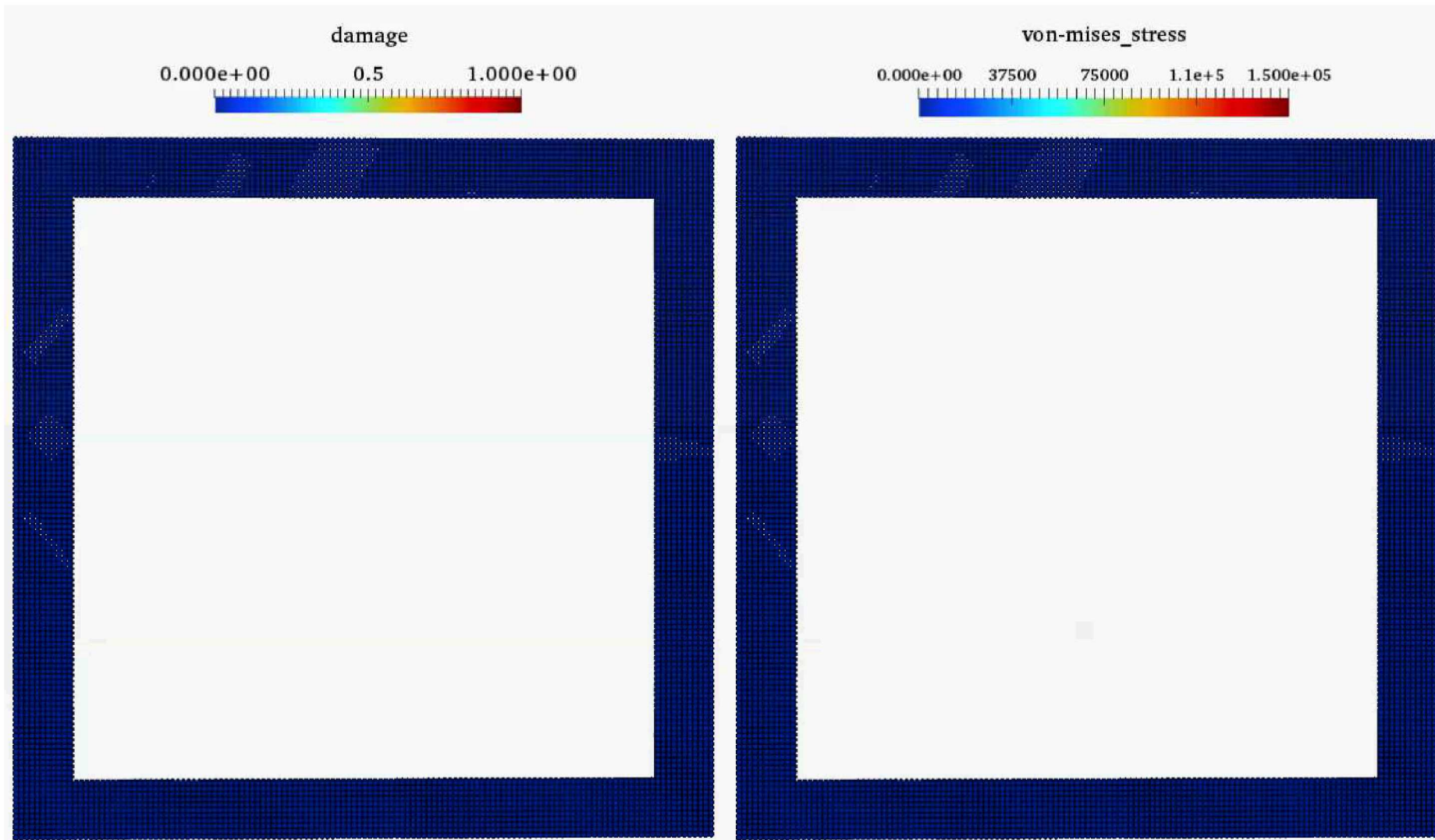


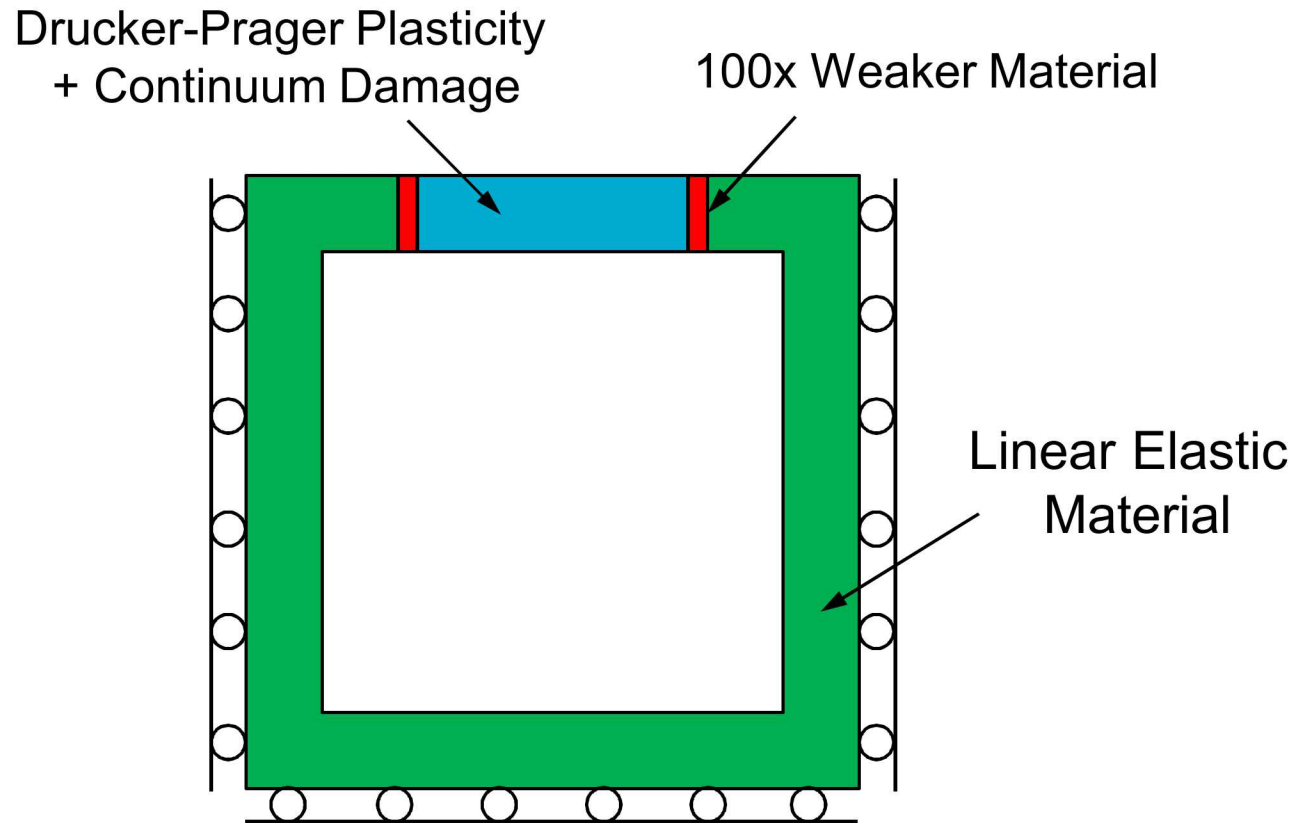


Homogeneous Material:
Continuum Damage + Drucker-Prager Plasticity



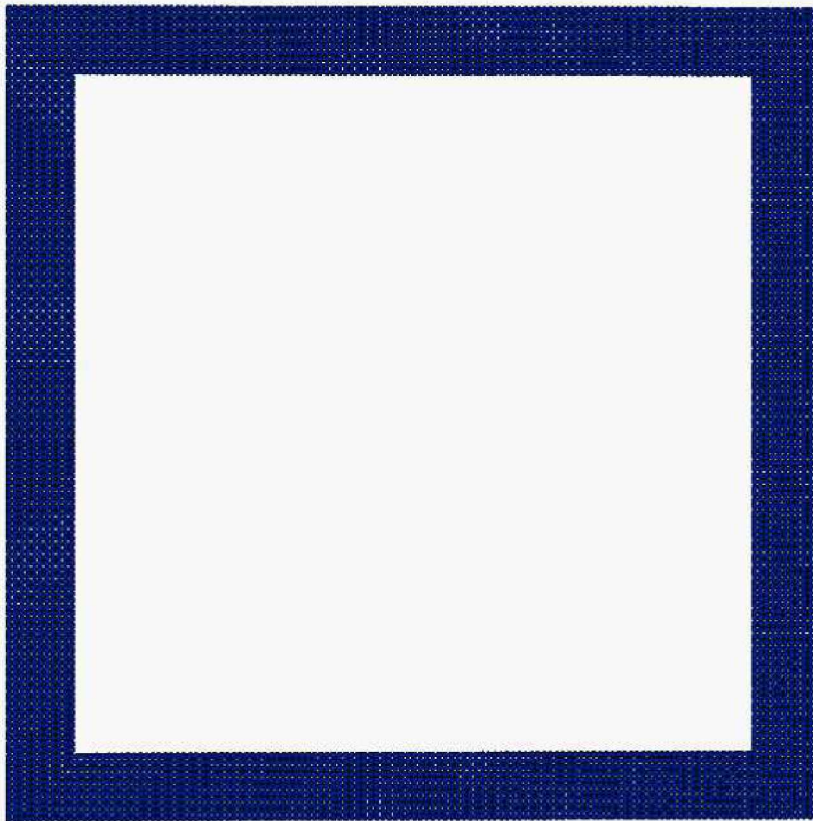
RKPM Team (Pre-)Preliminary Results



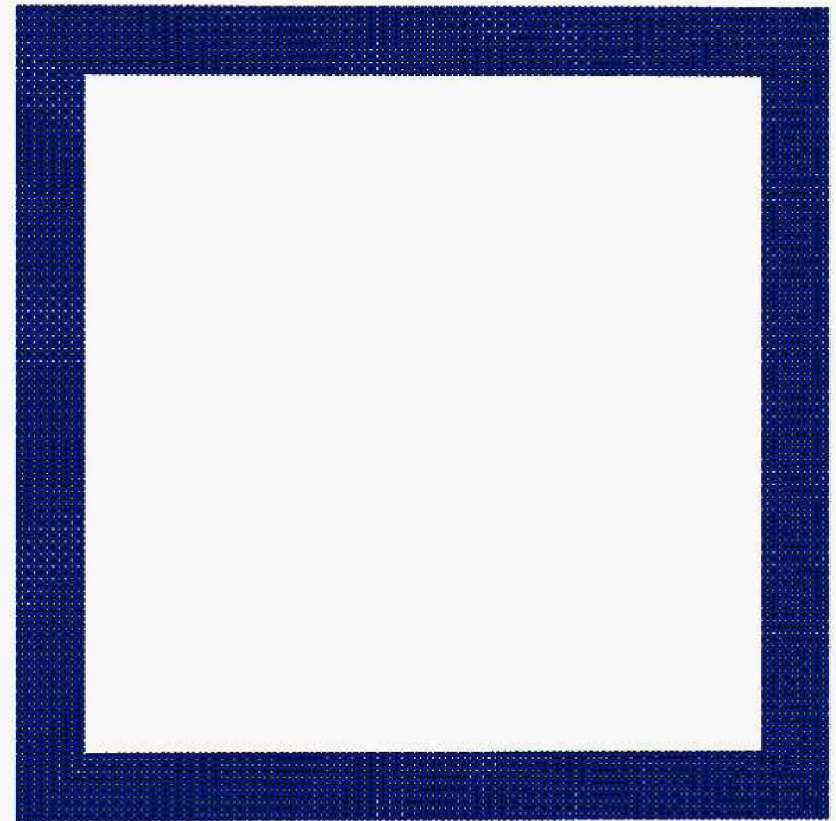


RKPM Team (Pre-)Preliminary Results

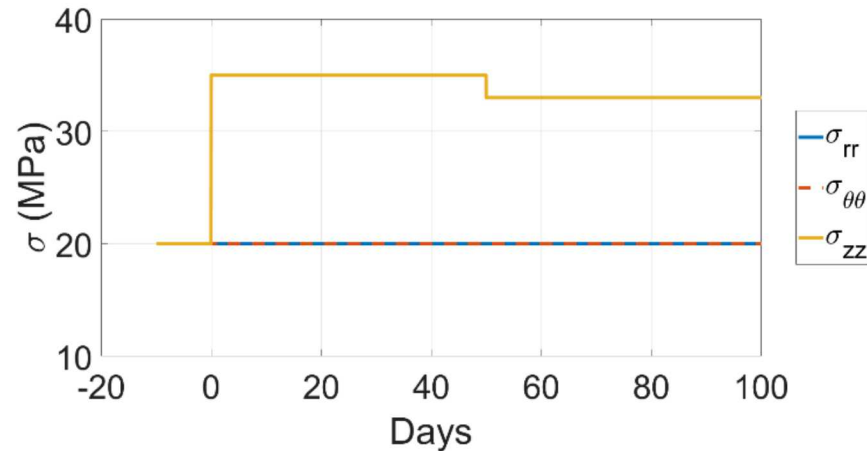
$$k_i = 5 \times 10^{-3}$$



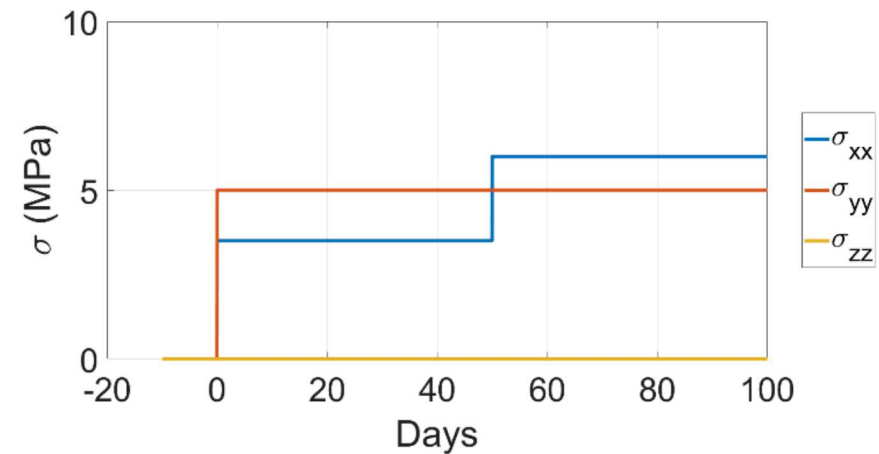
$$k_i = 1 \times 10^{-2}$$



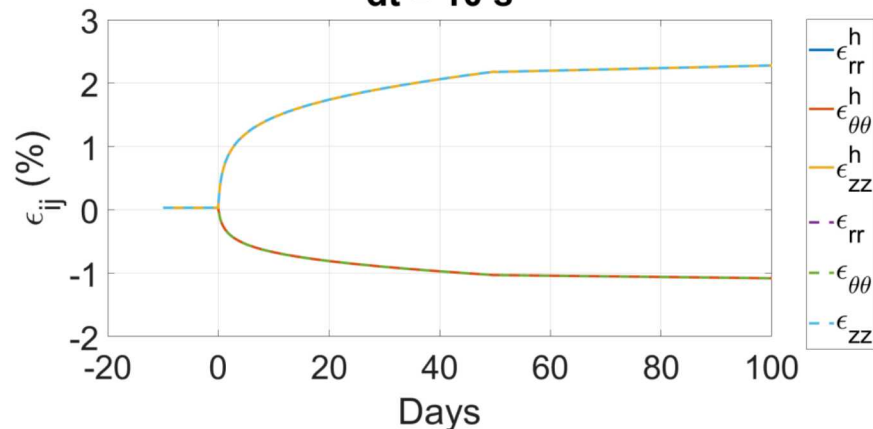
Triaxial Compression



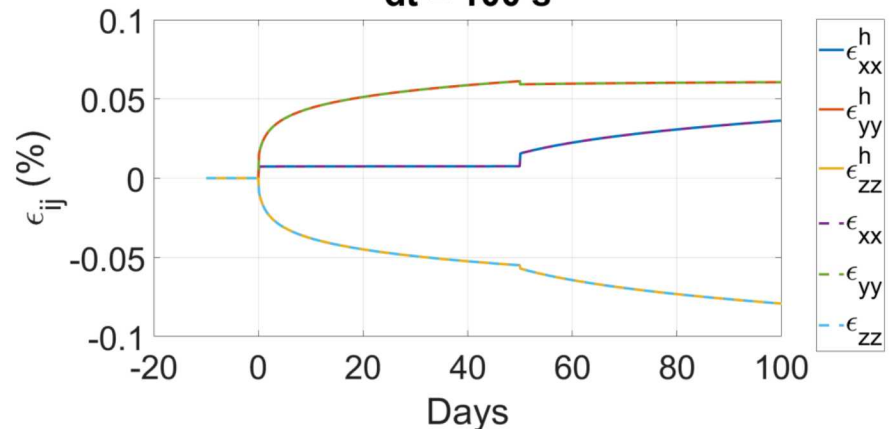
Unequal Biaxial Compression



dt = 10 s



dt = 100 s



Tentative Project Schedule

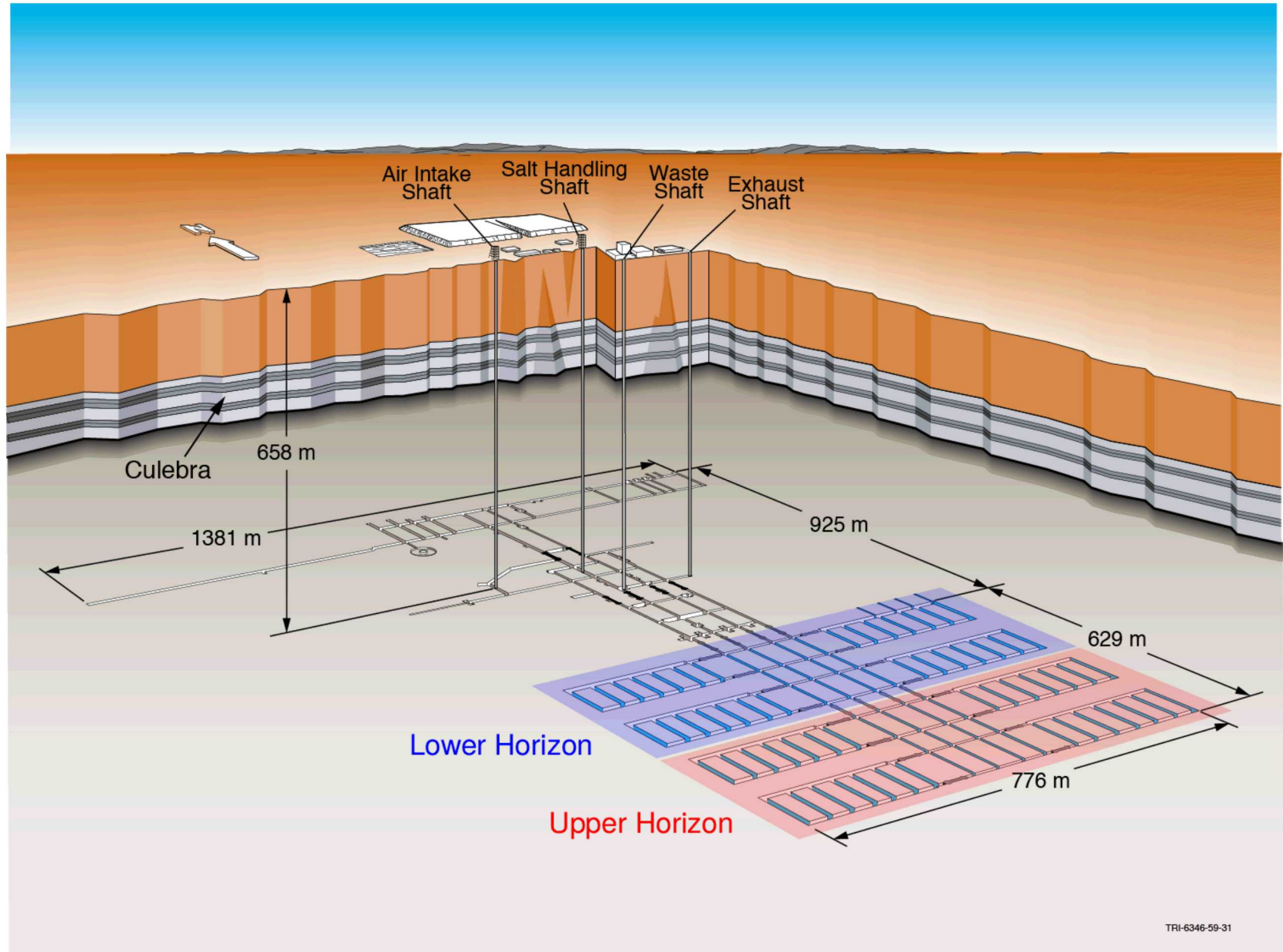
Rough Project Schedule

1. Numerical method
 - a. Investigation: April – September 2019
 - i. One day workshop in ABQ during week of Sept 23rd?
 - b. Implementation: April 2019 – April 2020
2. Continuum damage model
 - a. Preliminary model: May 2019
 - b. New model development: June – December 2019
 - c. New model implementation: January – April 2020
3. Empty room demonstration simulations
 - a. Proof-of-concept: June 2019 – April 2020
 - b. Semi-polished: April 2020 – ?
4. Crushed salt validation simulations
 - a. Proof-of-concept: June 2019 – April 2020
 - b. Semi-polished: April 2020 – ?



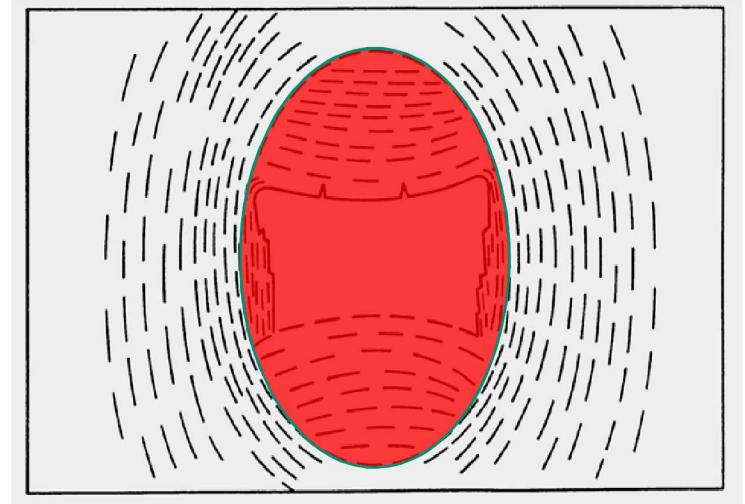
Extra Slides

Upper vs. Lower Horizon



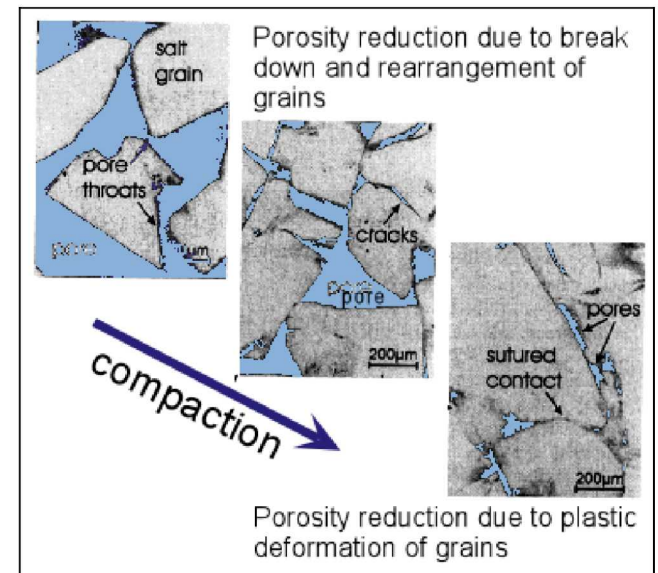
Empty Rooms Close More Slowly

1. Fracturing around room
 - a. Changes the room cross-section from a rectangle to a more enduring, stable shape
 - b. Controls the size and character of the rubble pile



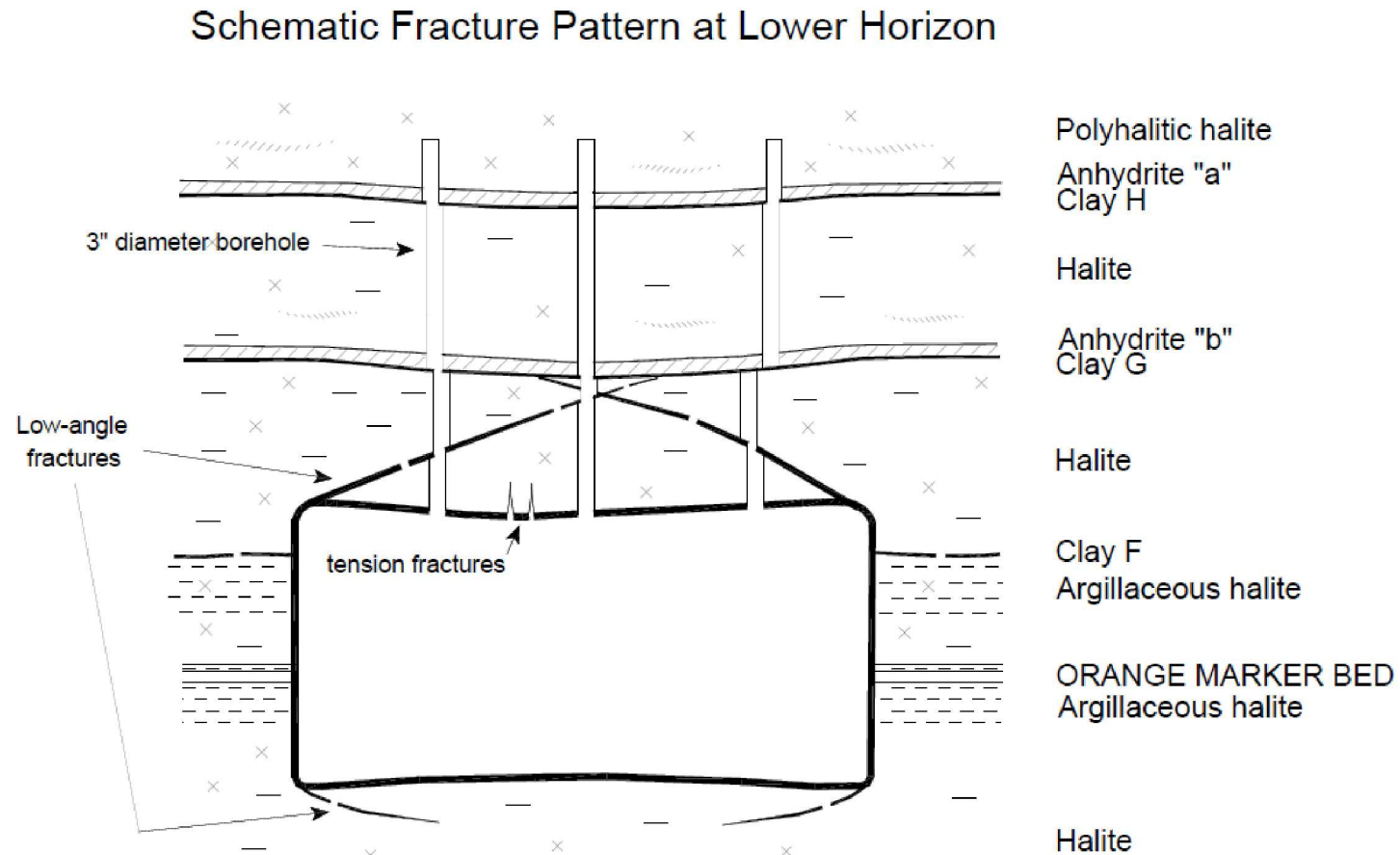
Borns, D.J. and J.C. Stormont. (1989) (Modified)

2. Rubble pile compaction
 - a. Involves reorganization, fracturing, and creep
 - b. Compaction processes control flow pathways
 - c. Rubble pile supplies back pressure to surrounding rock formation



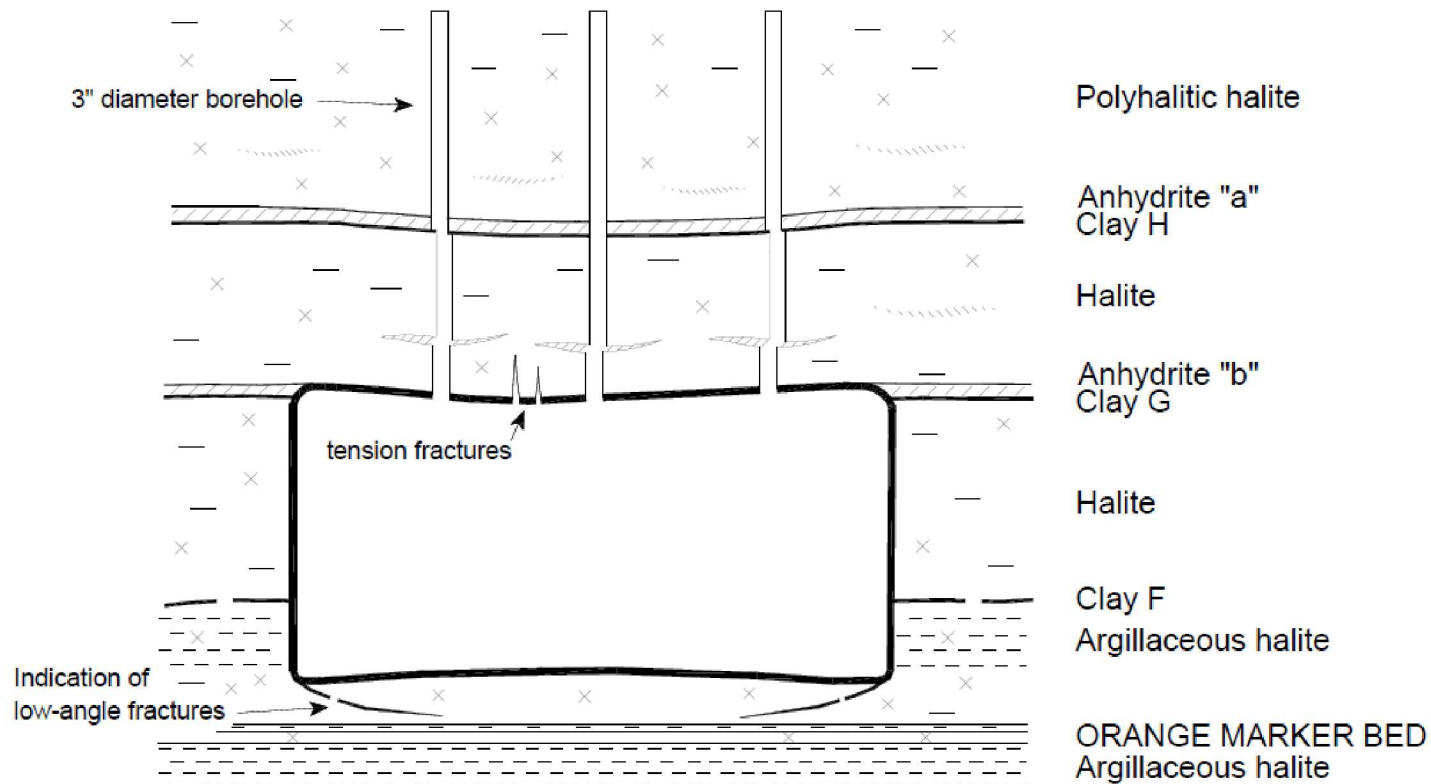
Spangenberg (1998) (Modified)

Typical Fractures on Lower Horizon



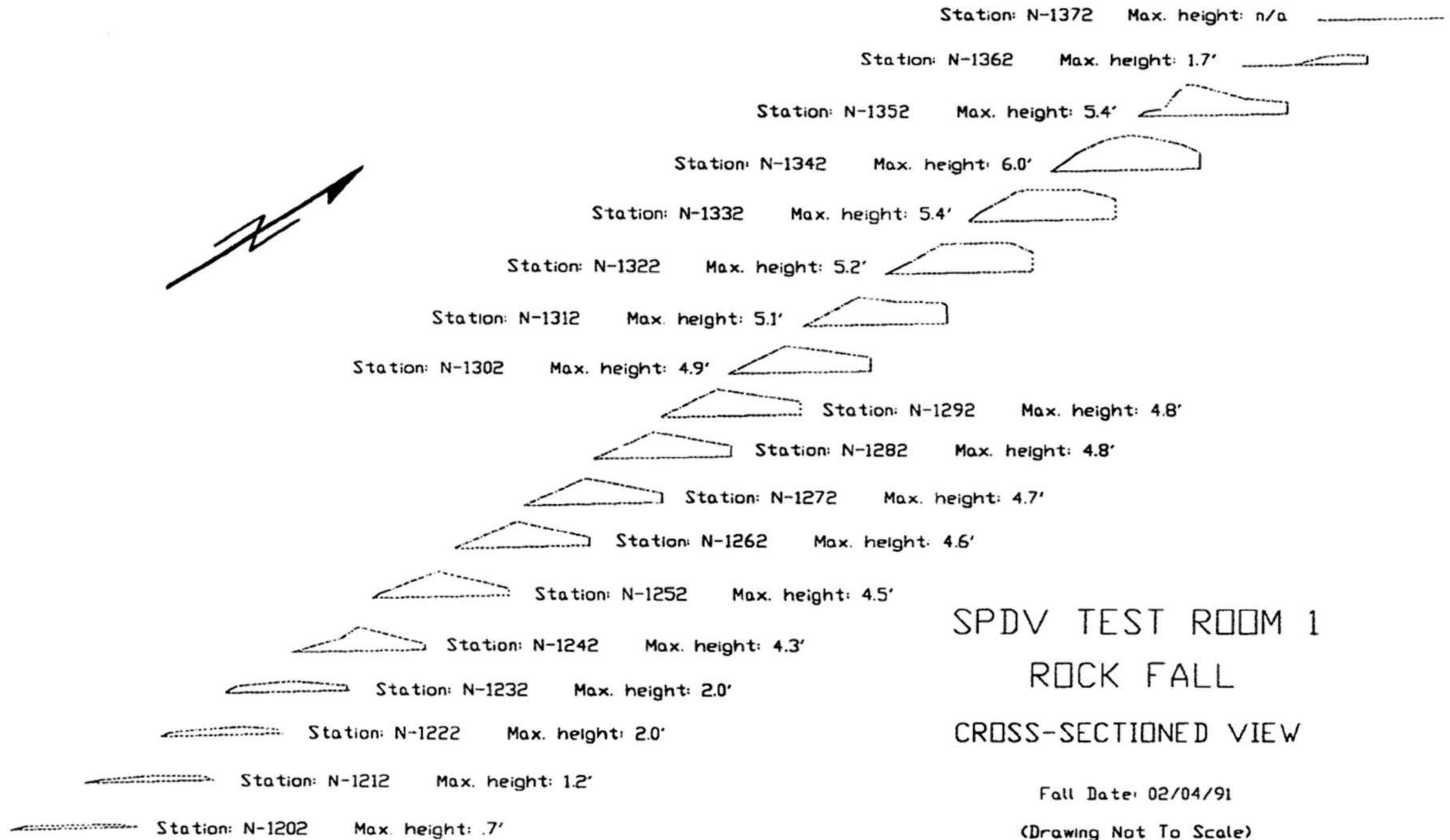
Typical Fractures on Upper Horizon

Schematic Fracture Pattern at Upper Horizon



NOT TO SCALE

Fallen Block Shapes (Lower Horizon)



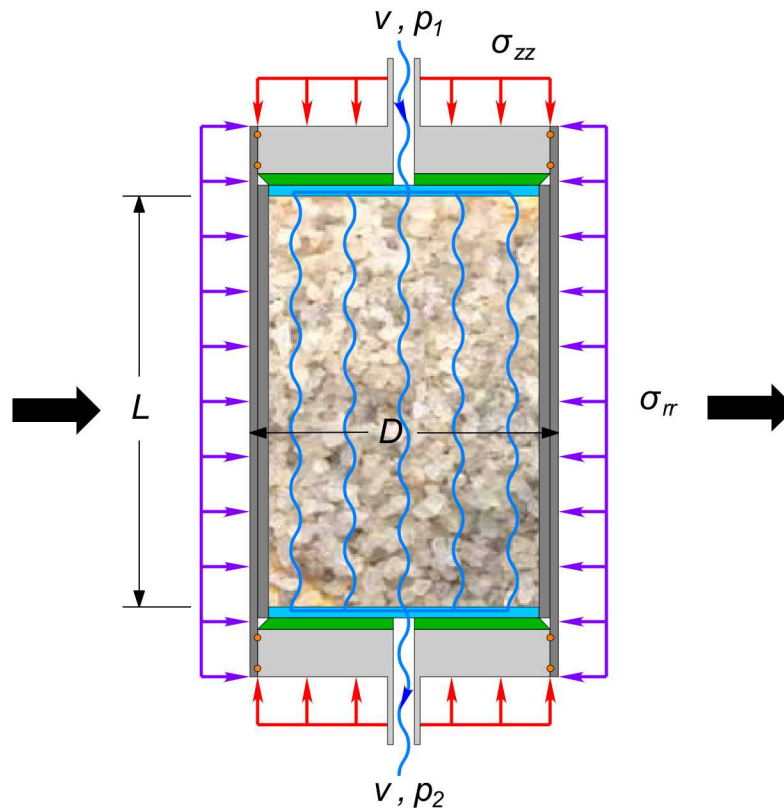
Crushed Salt Laboratory Testing

Specimen preparation

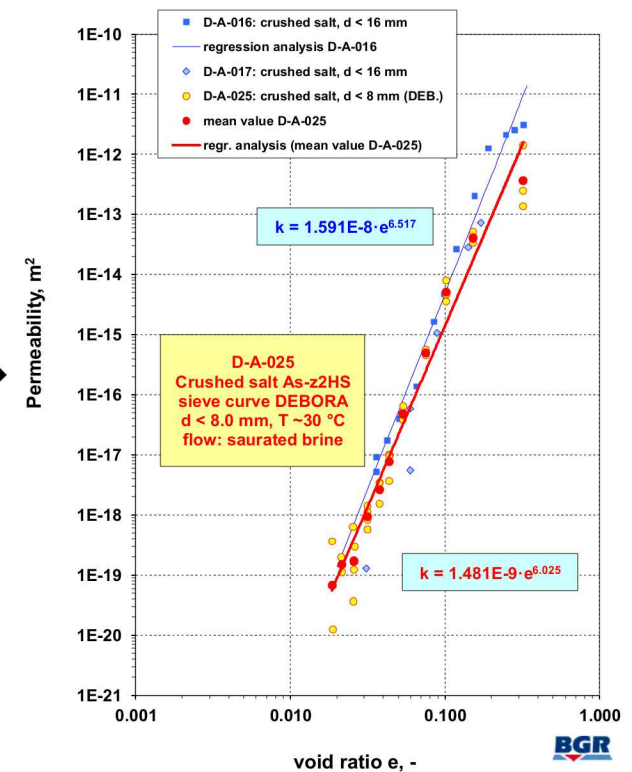


Photo courtesy of Scott Broome

Triaxial compression while measuring permeability



Permeability vs. Void Ratio (Porosity)



Kroehn, KP, et al. Mechanical and hydraulic behaviour of compacting crushed salt backfill at low porosities. Project REPOPERM. Phase 2. GRS GmbH. GRS – 450. 2017

Examples of Fracture on Lower Horizon

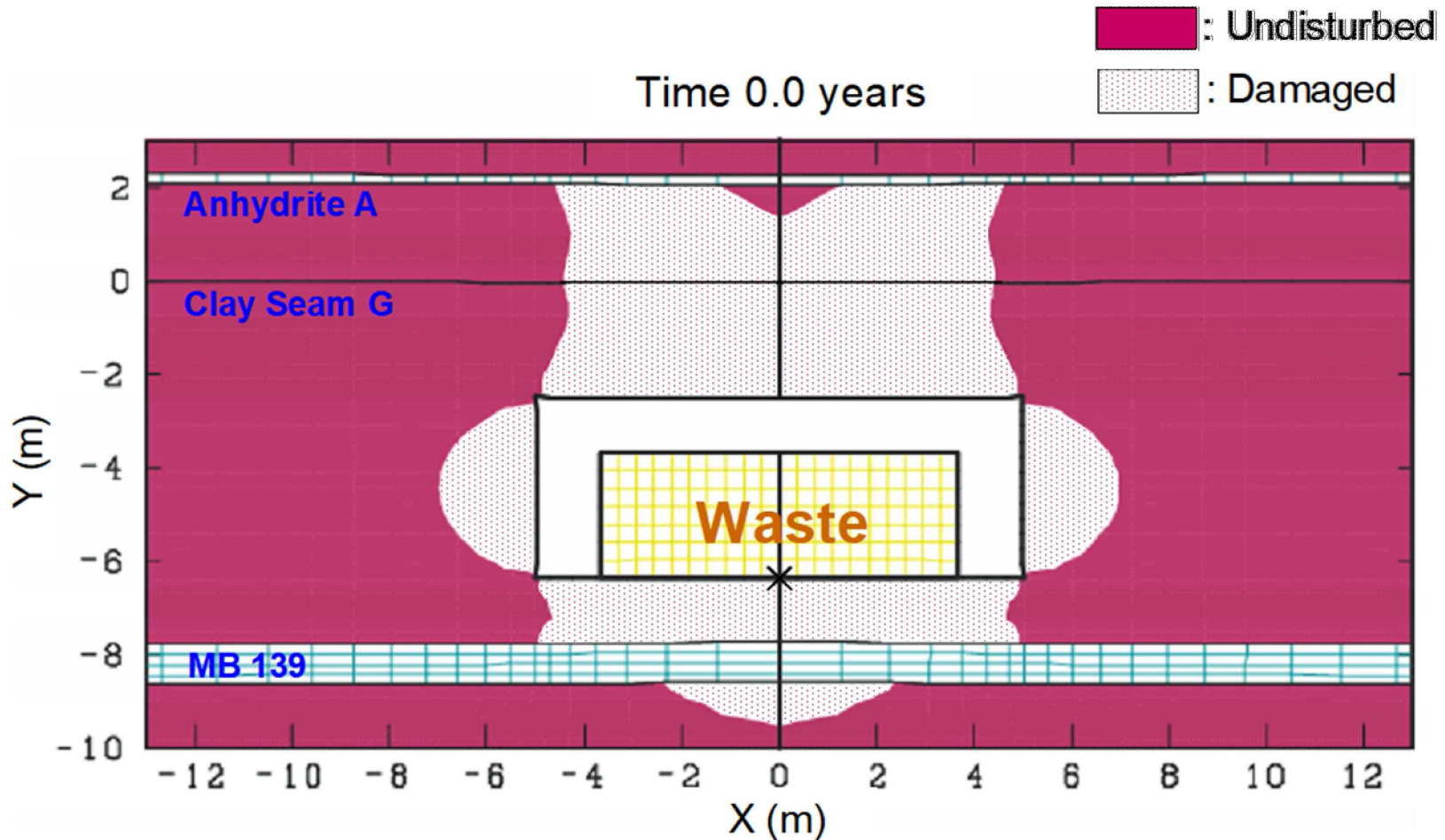


Roof Fall on Upper Horizon



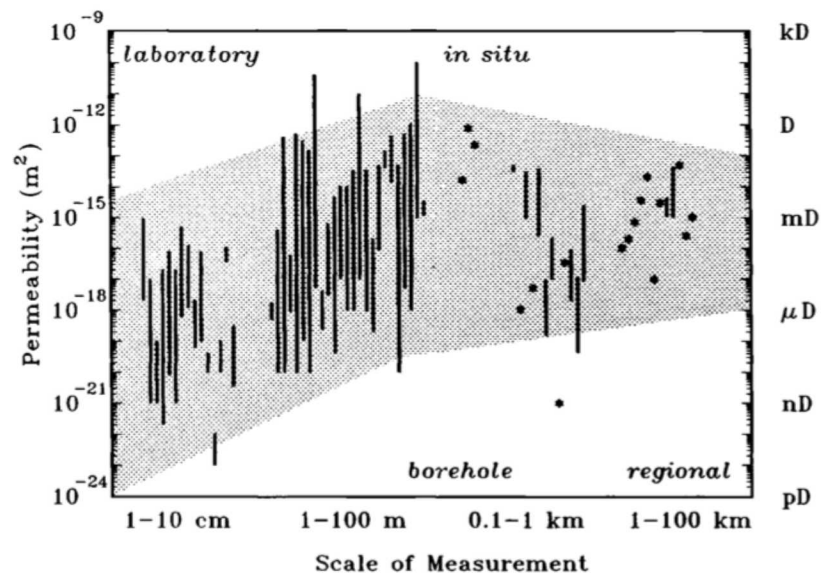
Oct 2016
Panel 3 Access Drift

Estimation of Excavation Damaged Zone



Compaction Scale Effect

Permeability Scale Effect



Clauser, C. (1992). Permeability of crystalline rocks. *Eos, Transactions American Geophysical Union*, 73(21), 233-238.

Speeding up the Viscoplasticity

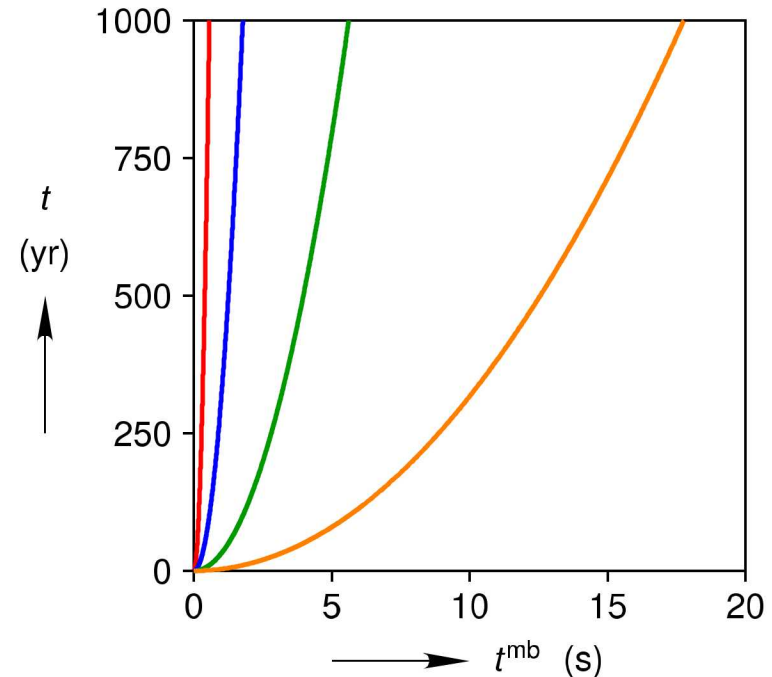
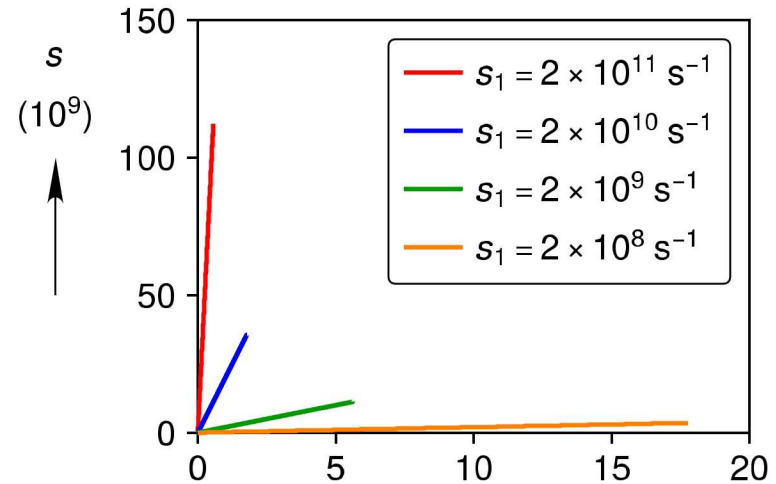
$$\dot{\bar{\epsilon}}^{\text{vp}} = \sum_{i=1}^2 A_i \left(\frac{\bar{\sigma}}{\mu} \right)^{n_i}$$



$$\dot{\bar{\epsilon}}^{\text{vp}} = s \sum_{i=1}^2 A_i \left(\frac{\bar{\sigma}}{\mu} \right)^{n_i}$$

$$dt = s dt_{\text{mb}}$$

$$s = s_0 + s_1 t_{\text{mb}}$$



Scaling Ramp Rate Selection

