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# Dealing with nuisance parameters in Bayesian model calibration

PRESENTED BY

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# Statement



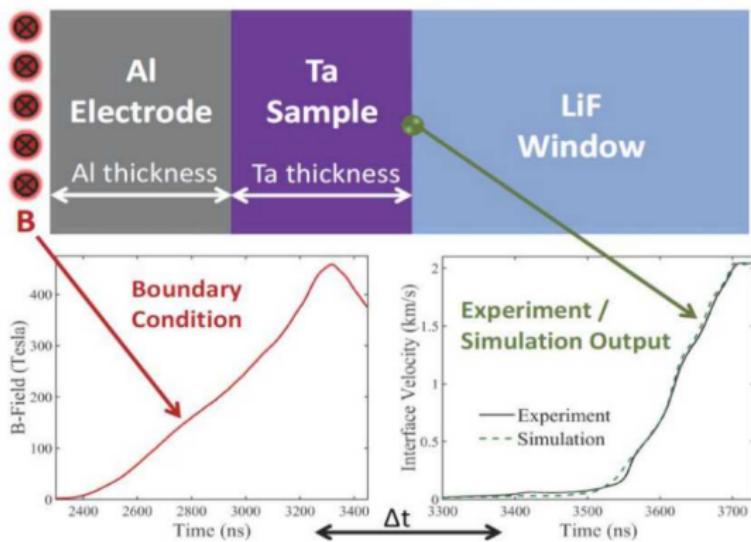
*This work was supported by a Sandia National Laboratories Laboratory Directed Research and Development (LDRD) grant. Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525. SAND 2019-*

# Background



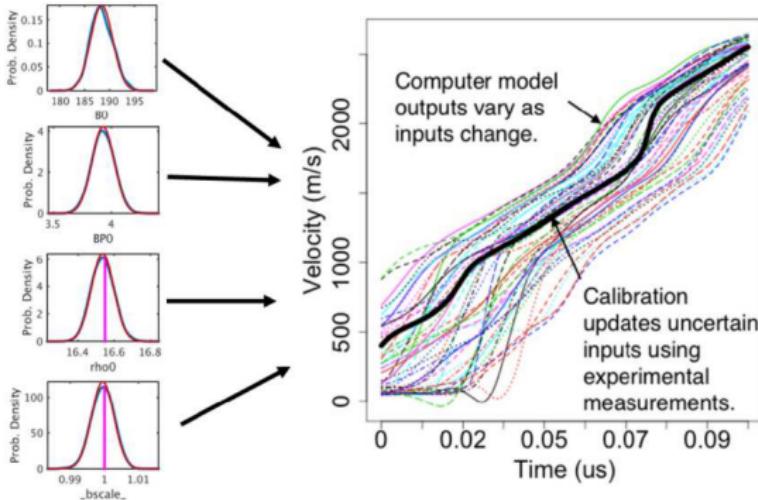
- **Dynamic material properties experiments:** access to the most extreme temperatures and pressures attainable.
- **Sandia National Labs Z-machine:** pulsed power driver that can deliver massive electrical currents over very short timescales (of the order of 60MA over  $1\mu\text{s}$  ).
- **Goal:** Understanding of material models at extreme conditions by coupling computational simulations with experimental data.
- **Parameters of interest are physical:** material properties with "true" value that is of interest.
- **Firstly:** Calibrate a well-understood model - two parameters of the equation of state of tantalum.

# Experimental setup



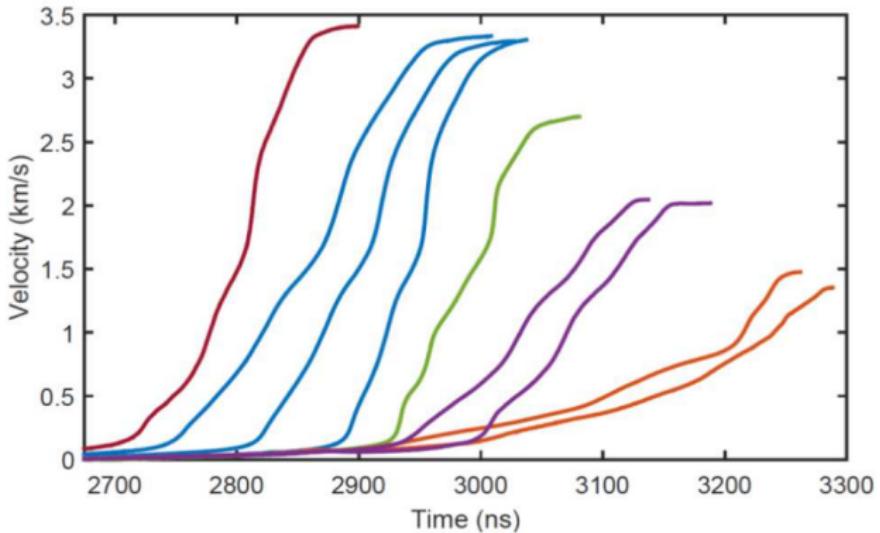
- "By coupling experimental and simulated velocity traces, parameters of the tantalum (Ta) equation of state (EOS) can be estimated".
- Massive electric currents treated as boundary conditions.
- Stress wave propagates thru system.

# Calibration



- Uncertain inputs generate velocity curves using a computer model.
- Probability distributions look for "agreement" of outputs and measurements.
- Bayesian framework is a natural in this context.

# Challenge



- How to accurately estimate uncertainties?
- Calibration parameters have physical interpretation.
- Lots of *nuisance* parameters.



# Our Framework

- Model the  $i^{th}$  observation in the  $j^{th}$  experiment as (Kennedy & O'Hagan 2001),

$$y(x_{ij}) = \eta(x_{ij}, \boldsymbol{\alpha}, \boldsymbol{\gamma}_j) + \delta(x_{ij}) + \epsilon_{ij}$$

- $\boldsymbol{\alpha}$  are the (unknown) values of the calibration parameters.
- $\boldsymbol{\gamma}_j$  unknown values of experimental uncertainties for experiment  $j$ .
- $y(x_{ij})$  is the observed velocity at time  $x_{ij}$ .
- $\eta(x_{ij}, \boldsymbol{\alpha}, \boldsymbol{\gamma}_j)$  is the computer model output at  $x_{ij}$ .
- $\delta(x_{ij}) \sim GP(\boldsymbol{\mu}_\delta, \boldsymbol{\Sigma}_\delta)$
- $\epsilon_{ij}$  are errors at  $x_{ij}$ .

# Dynamic material property calibration



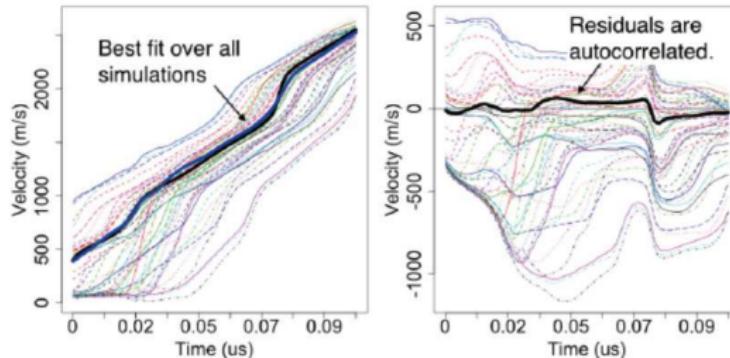
- BMC framework to obtain inference for two material properties of Tantalum.
- $B_0$  and  $B'_0$  are the Bulk modulus of tantalum and its pressure derivative.

$$\boldsymbol{\alpha} = (\alpha_1, \alpha_2) = (B_0, B'_0)$$

- Four nuisance that may vary across  $p = 9$  experiments
  - Tantalum density -  $\gamma_1$
  - Magnetic field scaling -  $\gamma_{2j}, j = 1, 2, \dots, 9$
  - Aluminum thickness -  $\gamma_{3j}, j = 1, 2, \dots, 9$
  - Tantalum thickness -  $\gamma_{4j}, j = 1, 2, \dots, 9$
- Potential for overfitting and lack of identifiability.

# Issues

- Model can fit well to data, solutions far from *true* parameter values.
- Can we diagnose such overfitting? Can we mitigate it?
- **Model discrepancy** can reduce the identifiability of the calibration parameters and lead to systematic bias.



# Nuisance parameters and overfitting

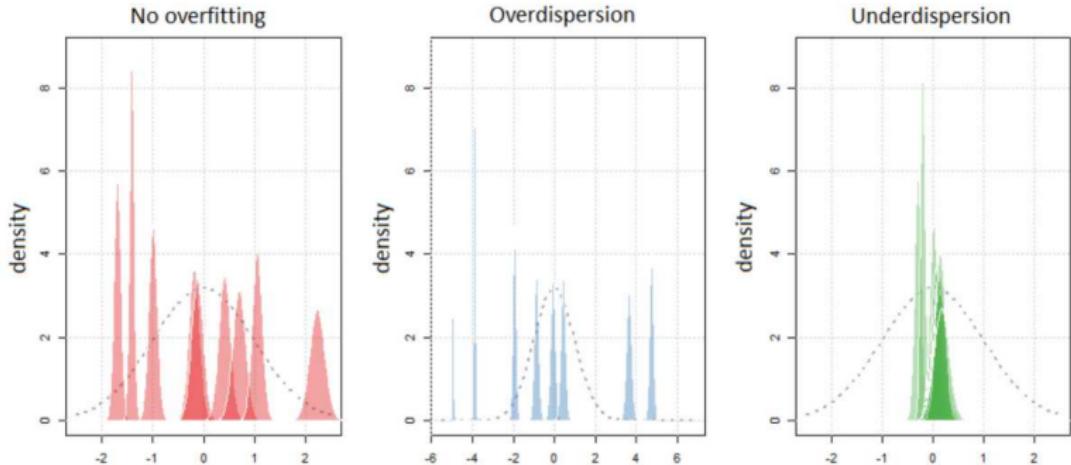


- **Aluminum and Tantalum thickness parameters:** These nuisance parameters are measured with a device which we believe to be well registered.
- Measurement error is *exclusive source* of uncertainty. The prior mean and variance of these nuisance parameters are well known.
- Nuisance parameters are standardized (mean 0, variance 1).
- The *standard informative (SI) prior* is:

$$(\gamma_{k1}, \gamma_{k2}, \dots, \gamma_{k9}) \sim N(0, I_9), \quad k = 2, 3, 4.$$

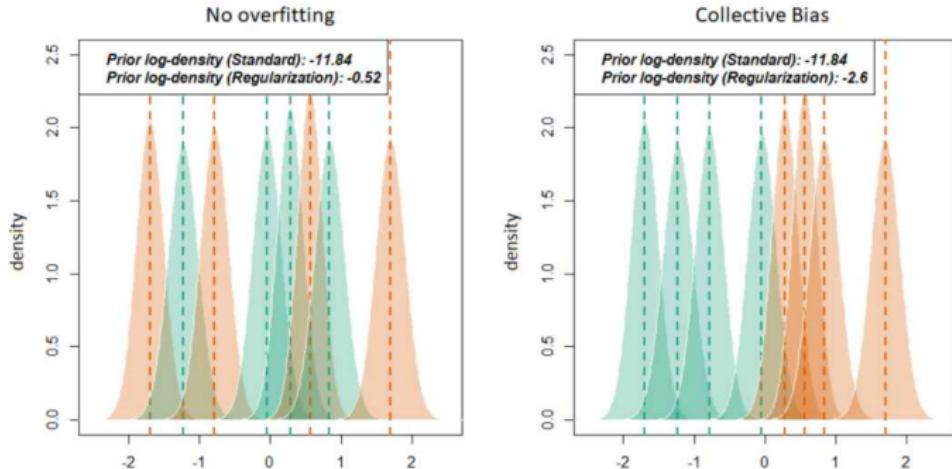
- “True values” are expected to look like a draw from a  $N(0, I_9)$  distribution.

# Nuisance parameters and overfitting



- Left panel: agrees with standard prior.
- Middle and left: can lead to overfitting.

# Collective Bias for 2 nuisance-sets



- Left: No grouping occurs.
- Right: Collective bias implies systematic overfitting across experiments.
- Standard prior assigns same values.



# A metric for overfitting

- We define,

$$M_\gamma = \frac{1}{p} \sum_{j=1}^p \gamma_j \quad V_\gamma = \frac{1}{p-1} \sum_{j=1}^p (\gamma_j - M_\gamma)^2$$

- Prior beliefs about problem structure suggests:

$$M_\gamma \approx 0 \quad V_\gamma \approx 1$$

- Under standard normal,

$$\pi_{M_\gamma, V_\gamma}(m, v) = N(m \mid 0, 1/p) \times [(p-1)\chi^2(v(p-1) \mid p-1)]$$

- Reasonable to check that the estimates  $\hat{M}_\gamma$  and  $\hat{V}_\gamma$  are *coherent* with prior.



# A metric for overfitting

- **Definition:** We say that  $(m, v)$  is *more coherent with the prior* than  $(m', v')$  if

$$\pi_{M_\gamma, V_\gamma}(m, v) > \pi_{M_\gamma, V_\gamma}(m', v')$$

- Define the set of all points which are less coherent with the prior than  $(\hat{M}_\gamma, \hat{V}_\gamma)$

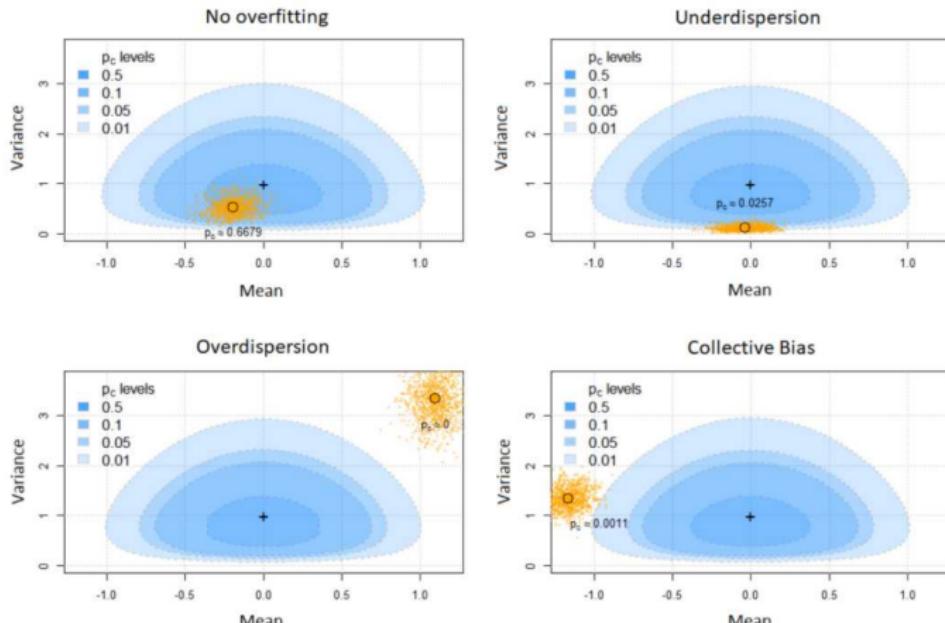
$$\Gamma_{\hat{M}_\gamma, \hat{V}_\gamma} = \left\{ (m, v) \mid \pi_{M_\gamma, V_\gamma}(\hat{M}_\gamma, \hat{V}_\gamma) > \pi_{M_\gamma, V_\gamma}(m, v) \right\}$$

- *Probability of prior coherency of  $(\hat{M}_\gamma, \hat{V}_\gamma)$*

$$p_c(\hat{M}_\gamma, \hat{V}_\gamma) = \int_{\Gamma_{\hat{M}_\gamma, \hat{V}_\gamma}} \pi_{M_\gamma, V_\gamma}(m, v) \, dm \, dv$$

$$\approx \frac{1}{L} \sum_{\ell=1}^L \mathbb{1} \left( \pi_{M_\gamma, V_\gamma}(\hat{M}_\gamma, \hat{V}_\gamma) > \pi_{M_\gamma, V_\gamma}(m_\ell, v_\ell) \right)$$

# Diagnostic plot for simulated case $p = 10$



- Orange: Point estimates and posterior draws of  $(M_\gamma, V_\gamma)$ .
- Blue: Prior probability contours.



# The moment penalization prior

- Overfitting of nuisance parameters leads to  $(\hat{M}_\gamma, \hat{V}_\gamma)$  with low prior coherency.
- The *moment penalization (MP) prior* **penalizes** solutions with low prior coherency.
- Using a square loss function,

$$pen_\lambda(\gamma) = \lambda_1(M_\gamma - 0)^2 + \lambda_2(V_\gamma - 1)^2$$

- Prior:

$$\pi_\gamma^{MP}(\gamma) \propto \exp(-pen_\lambda(\gamma))$$

- Tries to encourage solutions with  $M_\gamma \approx 0$  and  $V_\gamma \approx 1$ .



# The moment penalization prior

- Therefore,

$$\pi_{\gamma}^{MP}(\gamma) \propto \exp[-\lambda_1 M_{\gamma}^2] \exp[-\lambda_2 (V_{\gamma} - 1)^2]$$

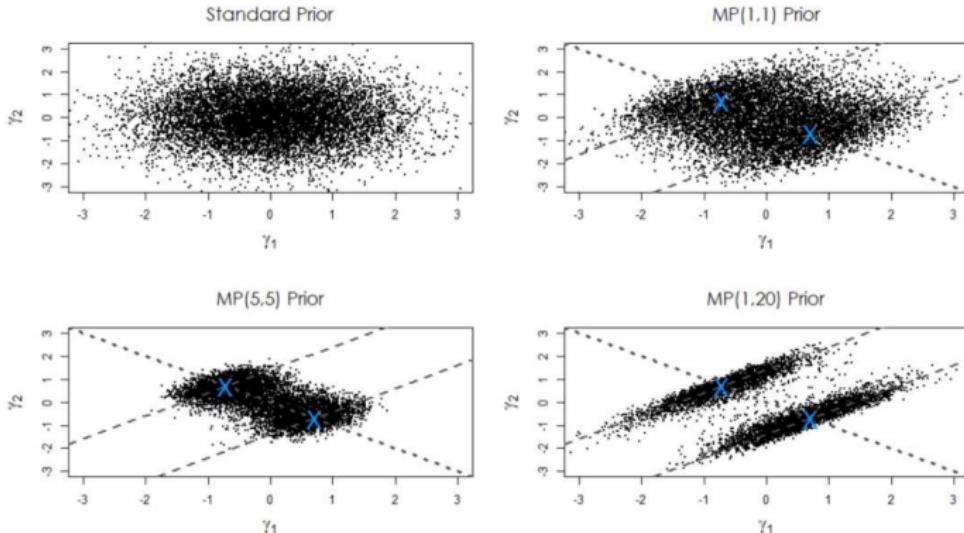
- $\lambda_1$  and  $\lambda_2$  control how strongly we want to enforce constraints.
- Reparameterize:  $\omega_1 = 2\text{Var}(M_{\gamma})\lambda_1$  and  $\omega_2 = 2\text{Var}(V_{\gamma})\lambda_2$
- Write  $\gamma \sim MP(\omega_1, \omega_2)$  to mean that,

$$\pi_{\gamma}^{MP}(\gamma) \propto \exp\left[-\frac{p\omega_1}{2} M_{\gamma}^2\right] \exp\left[-\frac{(p-1)\omega_2}{4} (V_{\gamma} - 1)^2\right]$$

- $\gamma \sim MP(1, 1)$  is the *standard moment penalization prior*.



# Samples from the Standard MP prior



- 10,000 draws via M-H for  $p = 2$ .
- As  $\omega_1, \omega_2 \rightarrow \infty$  all density is placed on  $\pm(1/\sqrt{2}, -1/\sqrt{2})$  (Z-regularization).
- As  $p$  grows, the induced marginal priors become  $N(0, 1)$ .



## Example: The simple machine

- Brynjarsdottir and O'Hagan (2014): The simple machine delivers work

$$\zeta(x) = \frac{Ex}{1+x/20}$$

- $x$  is the amount of *effort* put into the machine.
- $E$  is the *efficiency* of the machine.
- Denominator accounts for loss of work due to *friction*.
- The naive simulator introduces model discrepancy

$$\eta(x, E) = Ex$$



## Example: The simple machine

- We consider  $p = 10$  simple machines, and introduce base efficiency  $G_j$  as a machine-dependent nuisance parameter.
- Inputs  $x_1, x_2, \dots, x_n$  evenly spaced over  $[1, 4]$
- Data generating process:

$$y_{ij} = G_j + \frac{E x_i}{1 + x_i/20} + \epsilon_i$$

$$G_j \sim N(0, 0.05^2)$$

$$\epsilon_i \sim N(0, 0.01^2)$$

- Naive simulator:

$$\eta(x, E, G) = G + E x$$

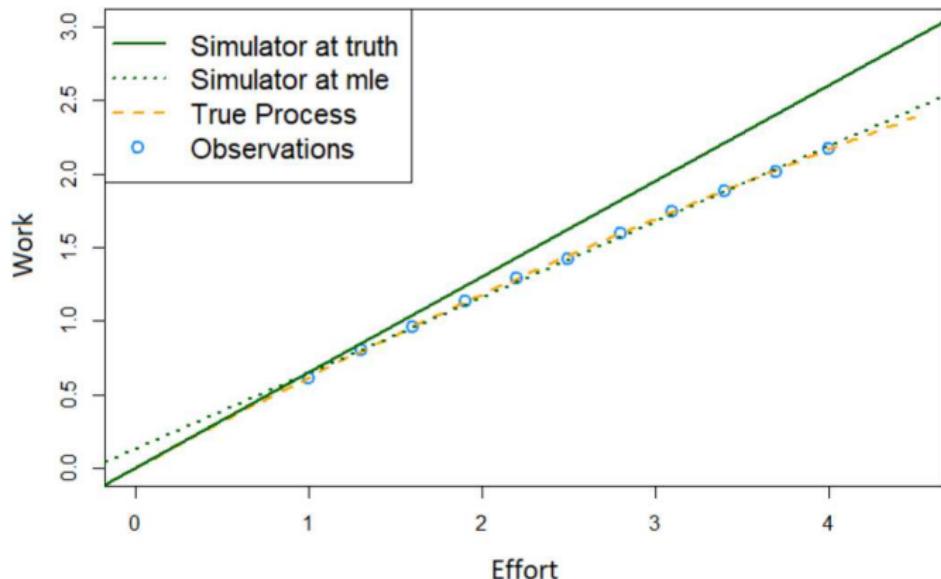
- True efficiency is  $E = 0.65$ . Standardize parameters:

$$\alpha = \frac{E - 0.65}{0.3} \sim N(0, 1)$$

$$\gamma_k = \frac{G_k - 0}{0.05} \sim N(0, 1)$$

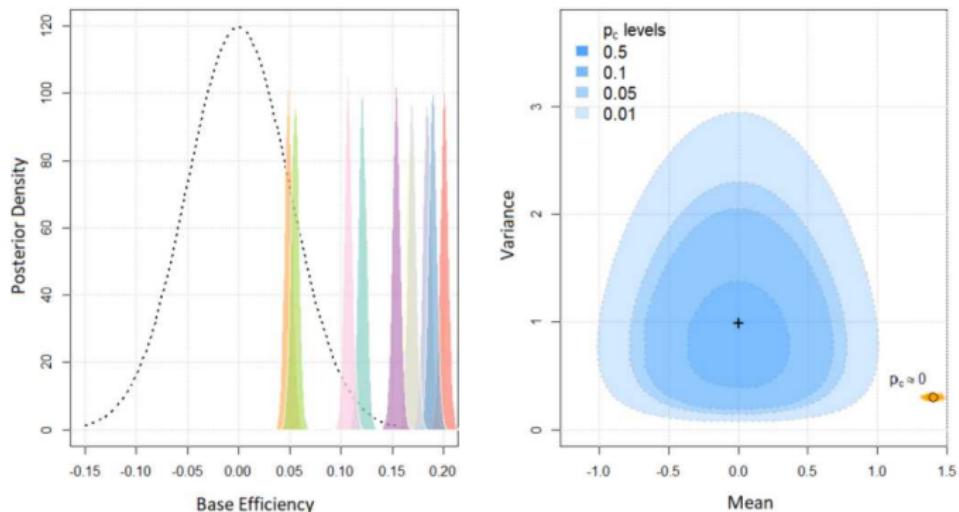
# Example: The simple machine

- Model discrepancy leads to systematic bias.



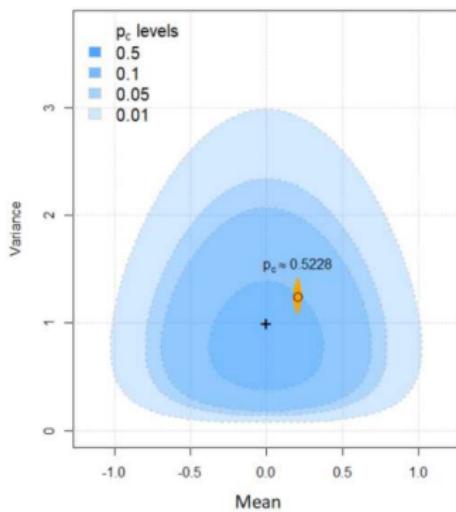
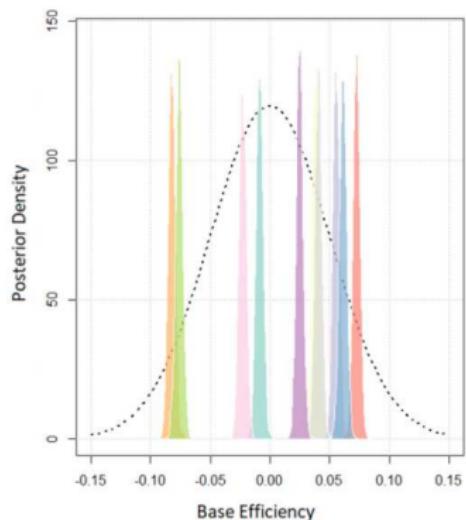
# Example: The simple machine

- Under standard informative prior

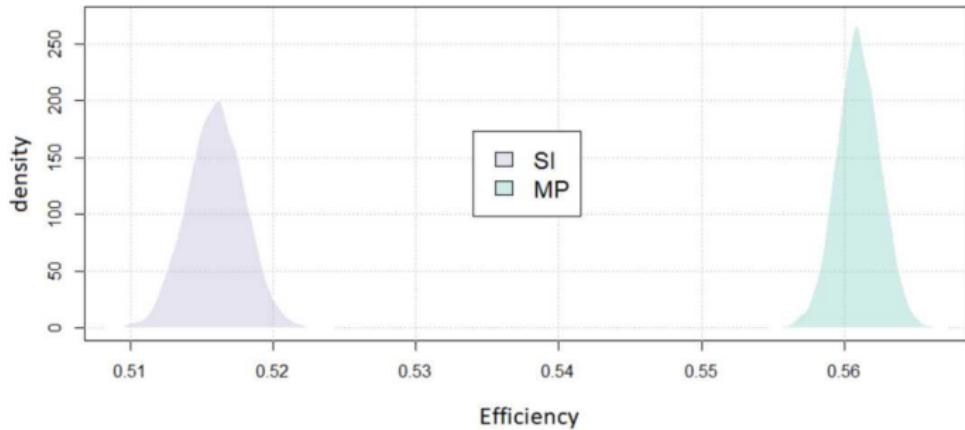


# Example: The simple machine

- Under moment penalization prior



# Example: The simple machine



- Posterior inference improves under MP, but is still far from truth.
- This is still valuable information! Model discrepancy is leading to biased inference on the parameter of interest.



## Dynamic material property calibration revisited

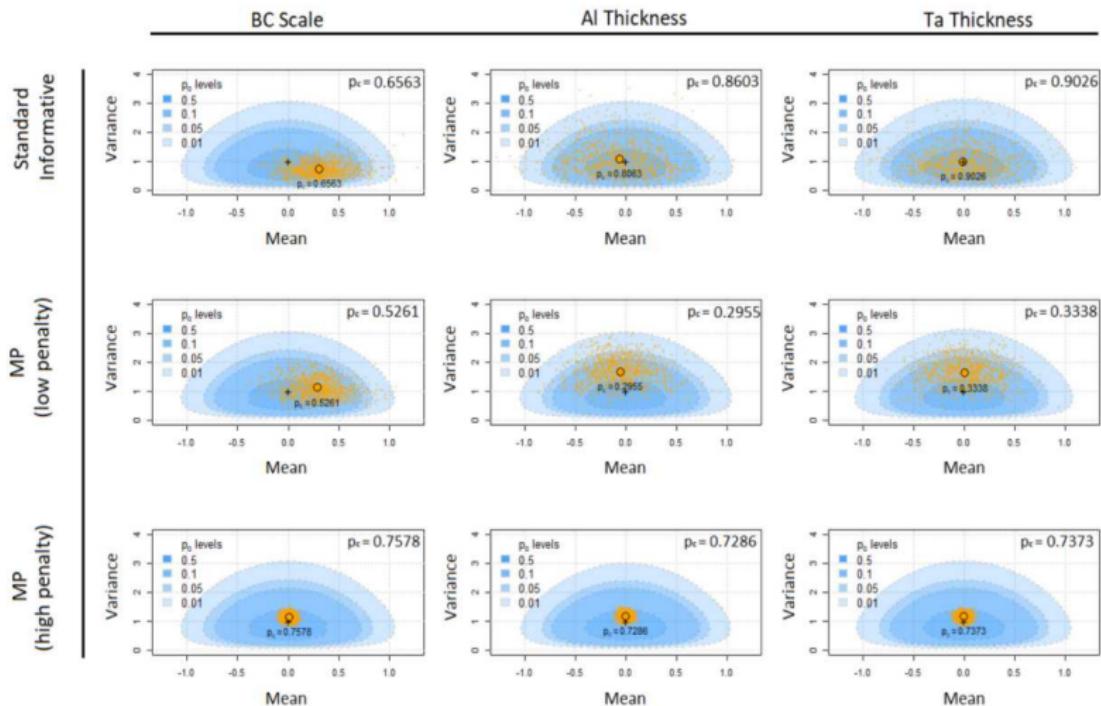
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  - Tantalum thickness -  $\gamma_{4j}, j = 1, 2, \dots, 9$
- Perform BMC for SI, SMP and MP(20, 40) priors.

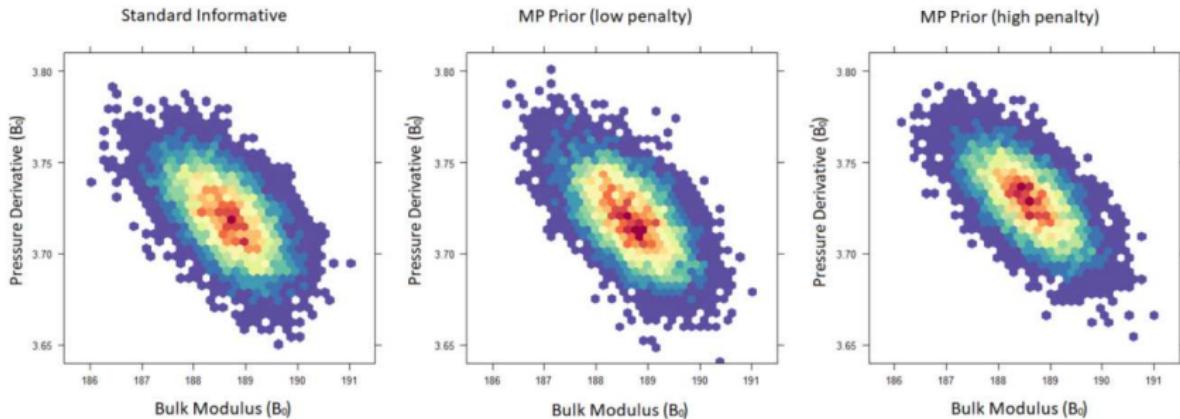
# Dynamic material property calibration

## Diagnostic plots



# Dynamic material property calibration

## Physical parameter posteriors



- Similar posterior inference in all cases.
- Indicates that model discrepancy is unlikely to be causing bias in the parameters of interest.

# Conclusions



- Overfitting of nuisance parameters leads to systematic bias which is often a symptom of model discrepancy.
- In complex high-dimensional problems, with appropriate problem structure, we can:
  - **Identify:** Probability of prior coherency identifies many types of overfitting, should it occur.
  - **Reduce:** The moment penalization prior reduces the systematic bias of the nuisance parameters.
  - **Diagnose:** Examine the sensitivity of posterior inference in order to diagnose the presence and effect of model discrepancy on the parameters of interest.

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