

Jacqueline H. Chen

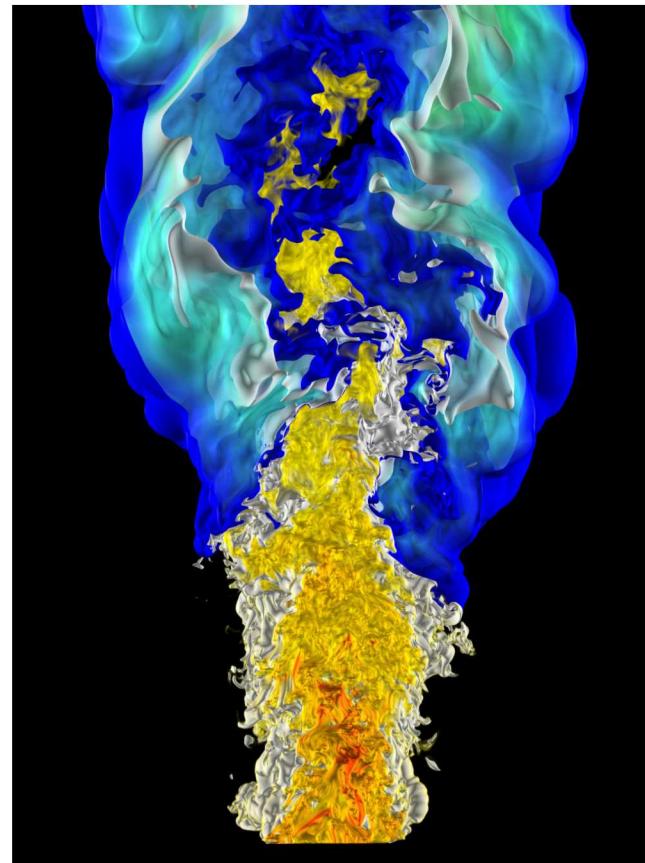
Sandia National Laboratories

[jhchen@sandia.gov](mailto:jhchen@sandia.gov)

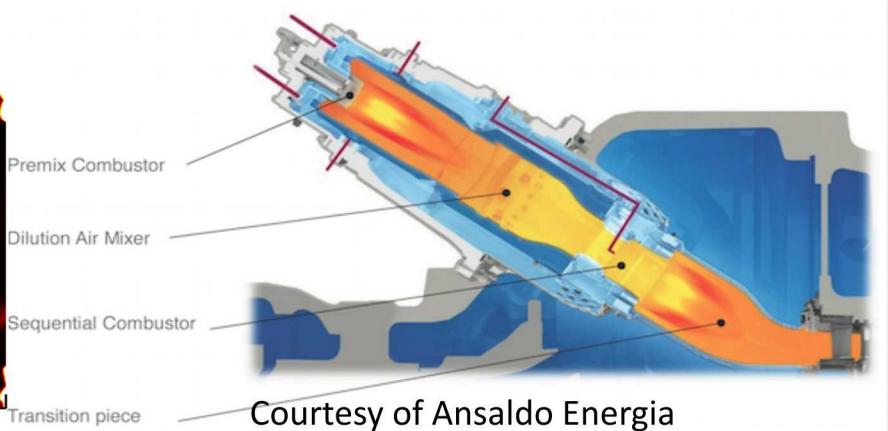
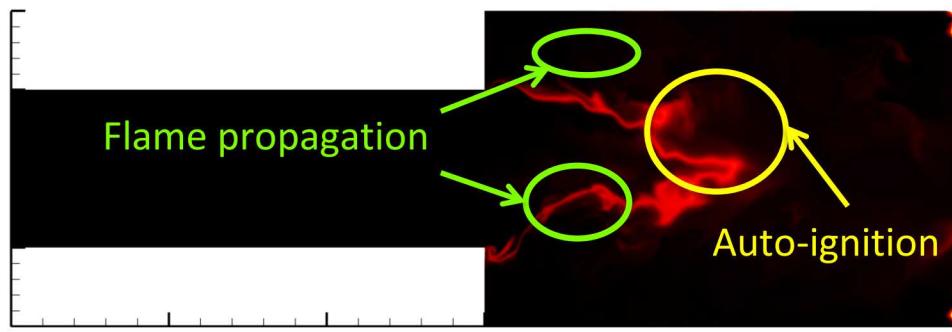
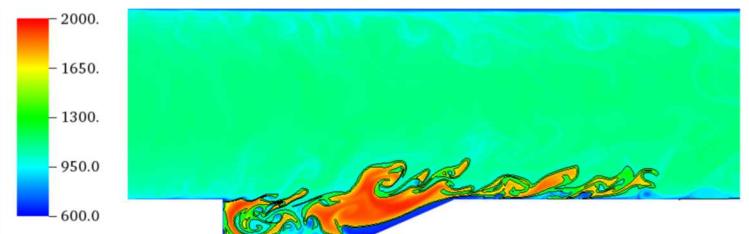
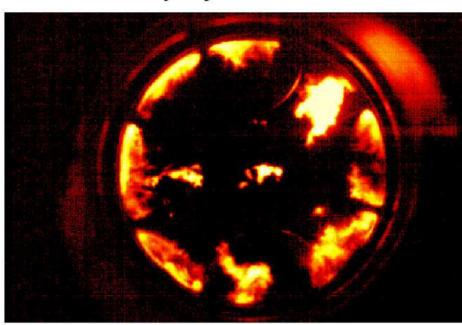
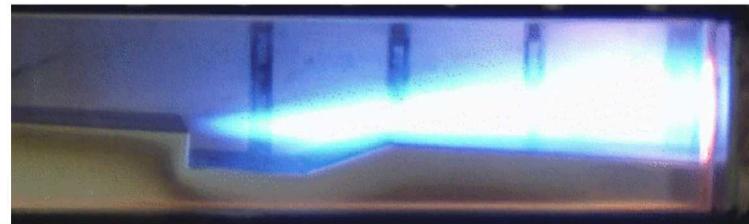
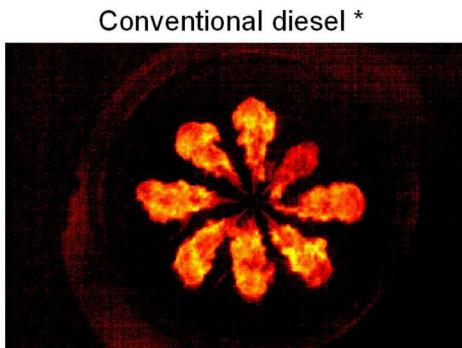
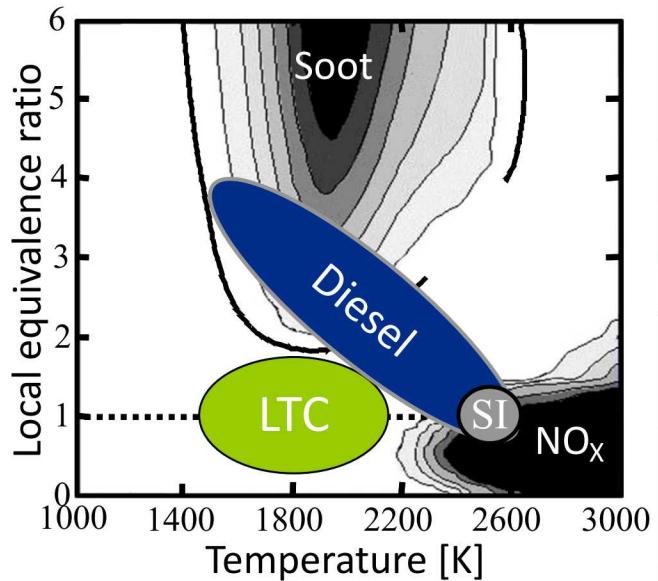
*11<sup>th</sup> Mediterranean Combustion  
Symposium*

Tenerife, Spain

June 16-20, 2019



# Autoignition and Flame Stabilization in Engines



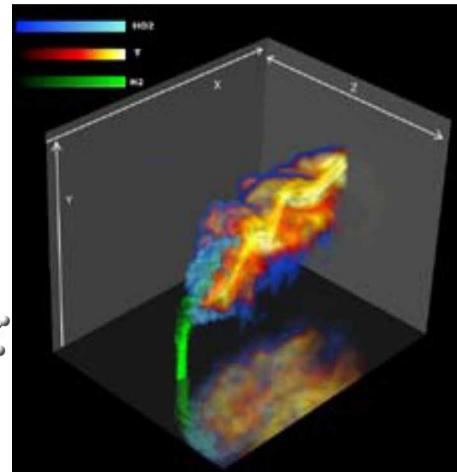
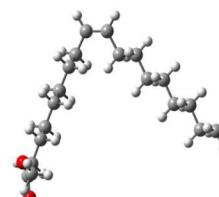
# Exascale Simulation of Turbulent Combustion

- Fundamental insights into multi-physics in highly turbulent flames to formulate physics-based LES models



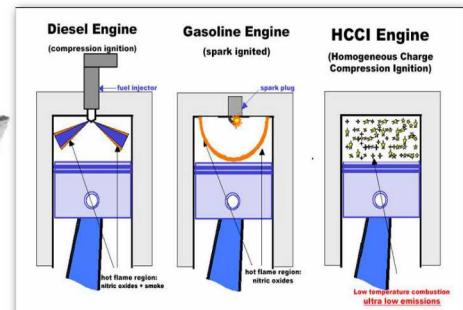
- High Reynolds number, high pressure, large turbulent velocity fluctuations, compressibility

- LES SGS closures inherited from nonreacting flows
- Multi-scale energy transfer processes
- Complex thermo-chemical trajectories through flames and ignition fronts



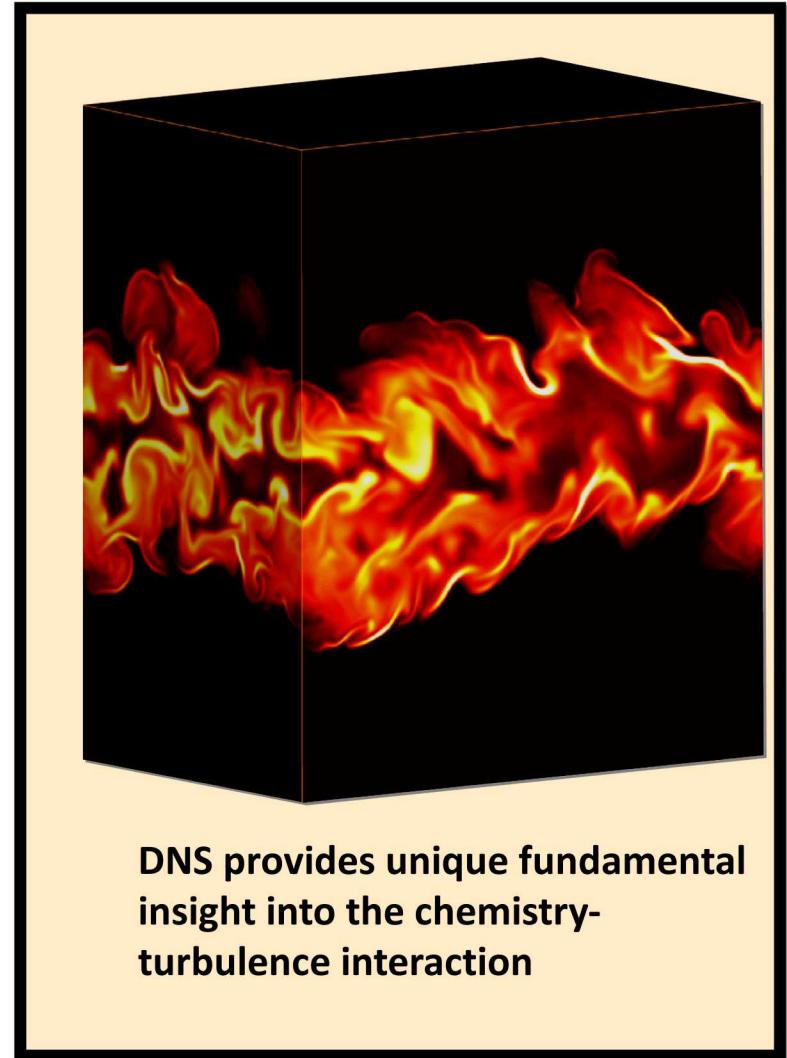
- High-fidelity direct numerical simulation (DNS) and hybrid DNS/LES methodologies

- sufficient chemical fidelity to differentiate effects of fuels where there is strong turbulence-chemistry interactions
- complex flows

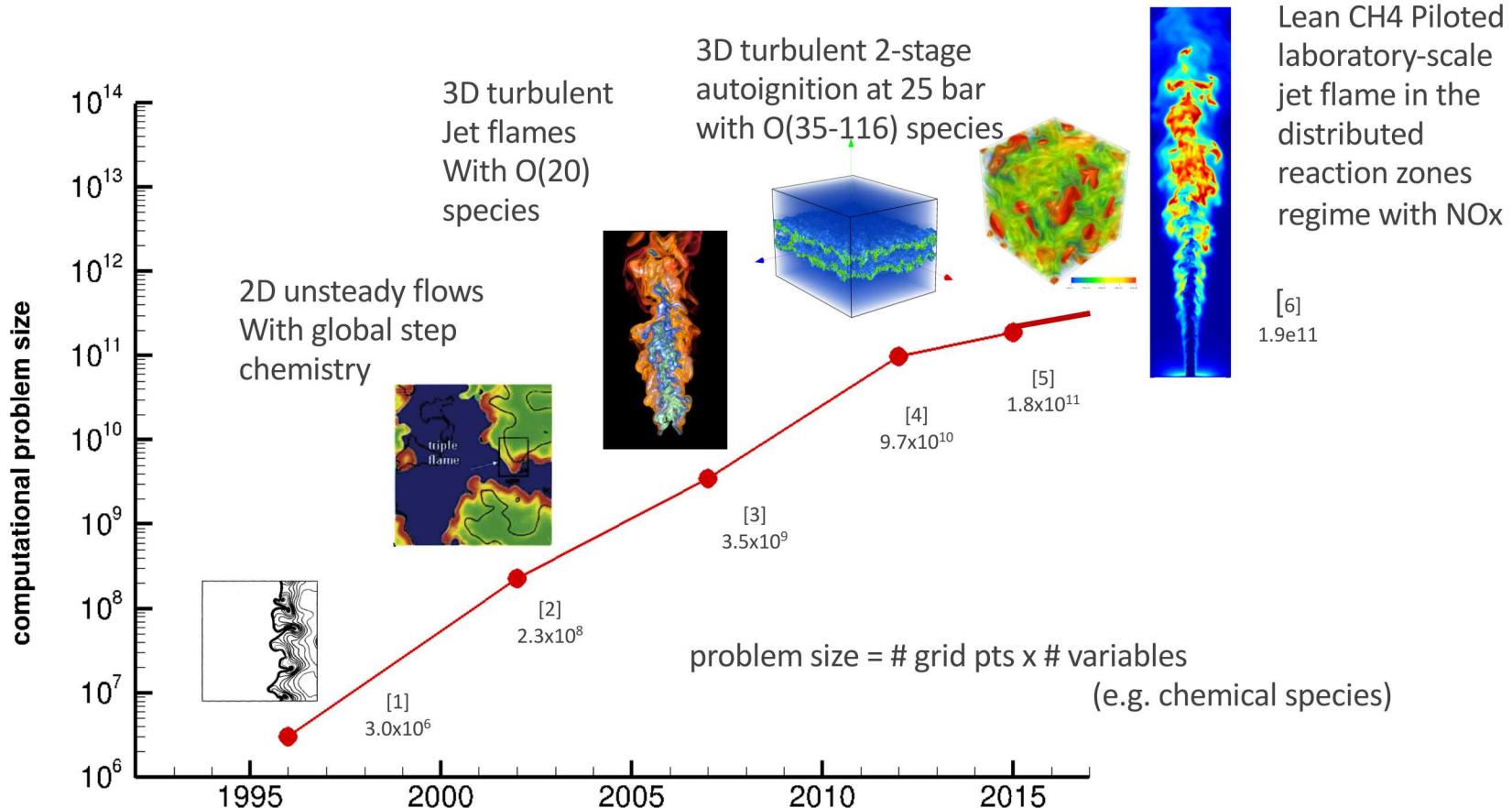


# Direct Numerical Simulation – S3D

- DNS of turbulent reacting flows
- Solves compressible reacting Navier-Stokes, total energy and species continuity equations
- High-order finite-difference methods
- Detailed reaction kinetics and molecular transport models
- Lagrangian particle tracking (tracers, spray, soot)
- In situ analytics and visualization
- Refactored for multi-threaded, many core heterogeneous architectures



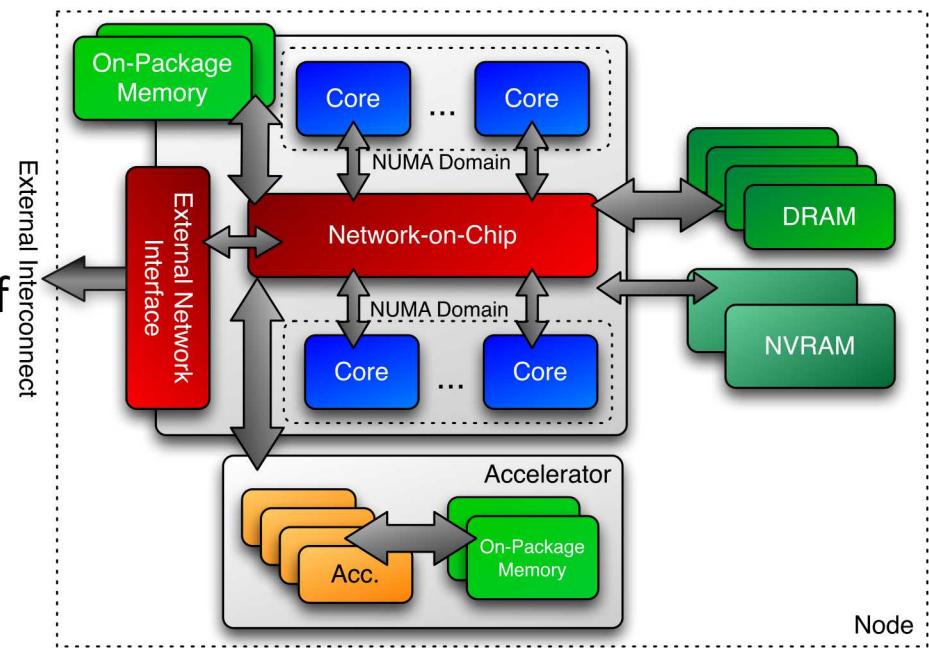
# Computational intensity of DNS scales with Moore's Law



- [1] T. Echekki, J.H. Chen, *Comb. Flame*, 1996, vol.106.
- [2] T. Echekki, J.H. Chen, *Proc. Comb. Inst.*, 2002, vol. 29.
- [3] R. Sankaran, E.R. Hawkes, J.H. Chen, *Proc. Comb. Inst.*, 2007, vol. 31.
- [4] E.R. Hawkes, O. Chatakonda, H. Kolla, A.R. Kerstein, J.H. Chen, *Comb. Flame*, 2012, vol. 159.
- [5] 2015 submission for Gordon Bell prize
- [6] H. Wang, E. Hawkes, J. H. Chen, *Comb. Flame* 2017

# Constraints imposed by exascale architecture

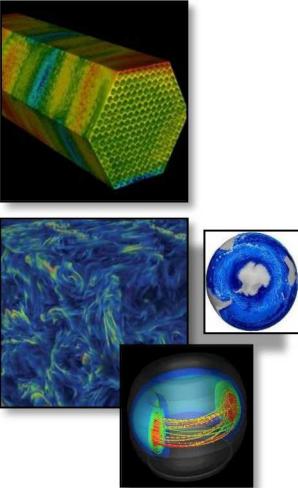
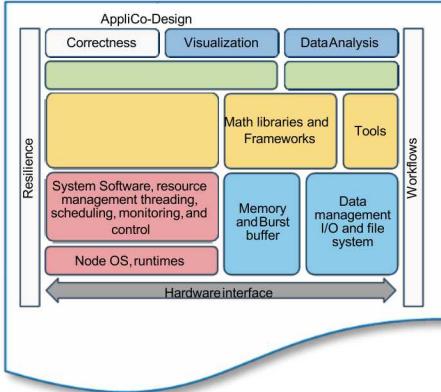
- **Power:** primary design constraint for future HPC system design
- **Cost:** Data movement dominates: optimize to minimize data movement
- **Concurrency:** Exponential growth of parallelism within chips
- **Locality:** must reason about data locality and possibly topology
- **Memory Scaling:** Compute growing 2x faster than capacity or bandwidth,
- **Heterogeneity:** Architectural and performance nonuniformity



Conceptual model of future HPC node

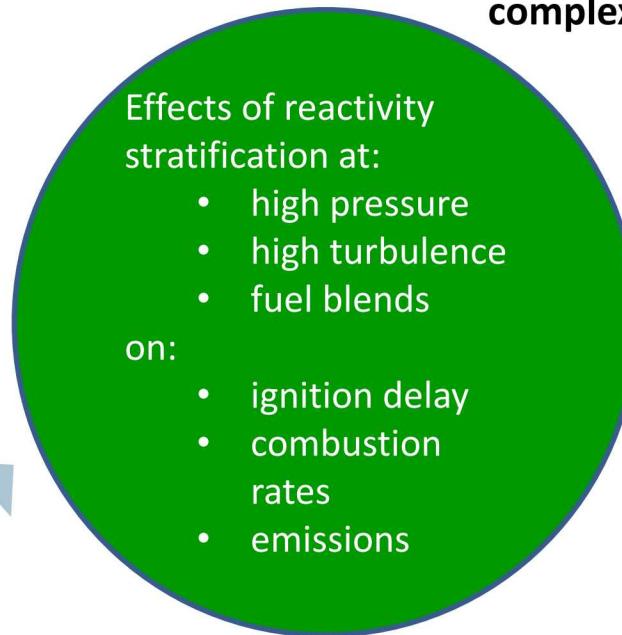
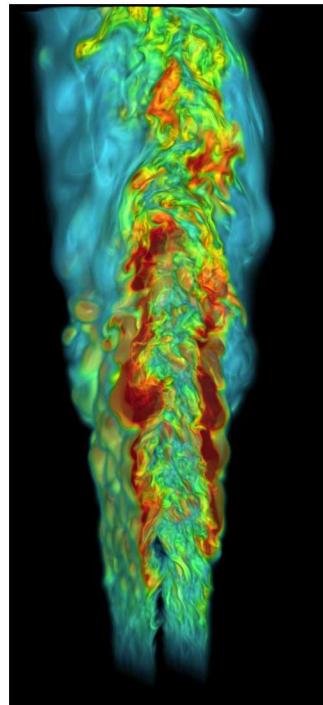
Express data locality and independence, express massive parallelism,  
minimize data movement and reduce synchronization, detect and address faults

# DOE Exascale Computing Project (ECP) will achieve capable exascale machines in 2021-2023

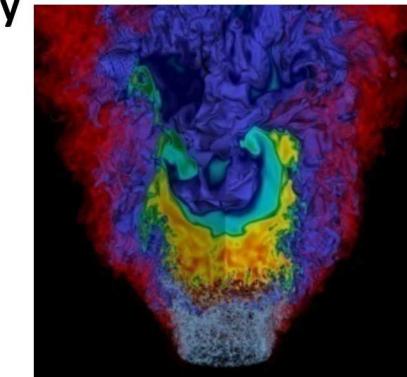
Application Development	Software Technology	Hardware Technology	Exascale Systems
Science and mission applications	Scalable and productive software stack	Hardware technology elements	Integrated exascale supercomputers
			

ECP's work encompasses applications, system software, hardware technologies and architectures, and workforce development

# ECP application: transforming combustion science and technology through exascale simulation (Pele)



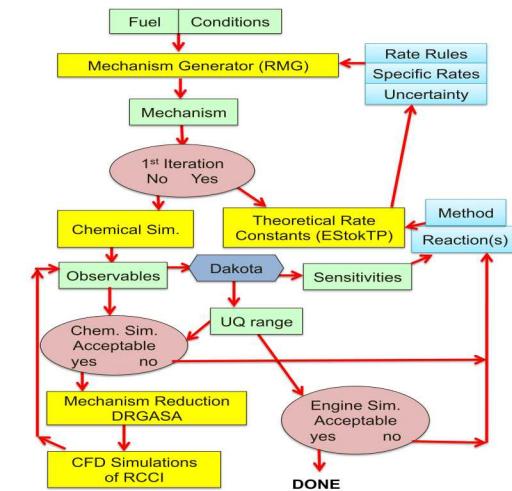
PeleC and PeleLM: Block-structured adaptive mesh refinement, multi-physics: spray, soot, and radiation, real gas, complex geometry



S3D: multi-block compressible reacting  
DNS multi-physics validation: spray,  
soot, radiation



## Automated Mechanism Generation



# Outline

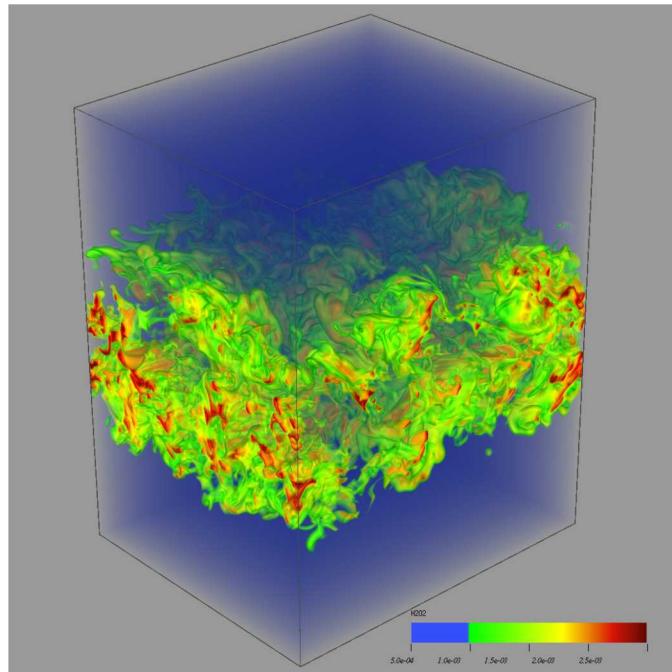
- Examples of DNS of turbulent combustion relevant to engines:
  - DNS of turbulent autoigniting nDodecane diesel jets (S3D and PeleLM)
  - DNS of high-speed flame stabilization behind a step
  - DNS of reheat combustion in staged gas turbines
- Path to Exascale Combustion Simulations (2021-2023)
  - Programming models
  - Composable in situ workflows (analytics, machine learning)
  - Unsupervised anomaly detection

# DNS of a Turbulent Autoigniting n-Dodecane temporal jet at 25 Bar

Giulio Borghesi<sup>1</sup>, Alex Krisman<sup>1</sup>, Tianfeng Lu<sup>2</sup> and Jackie Chen<sup>1</sup>

<sup>1</sup>Combustion Research Facility, Sandia National Laboratories

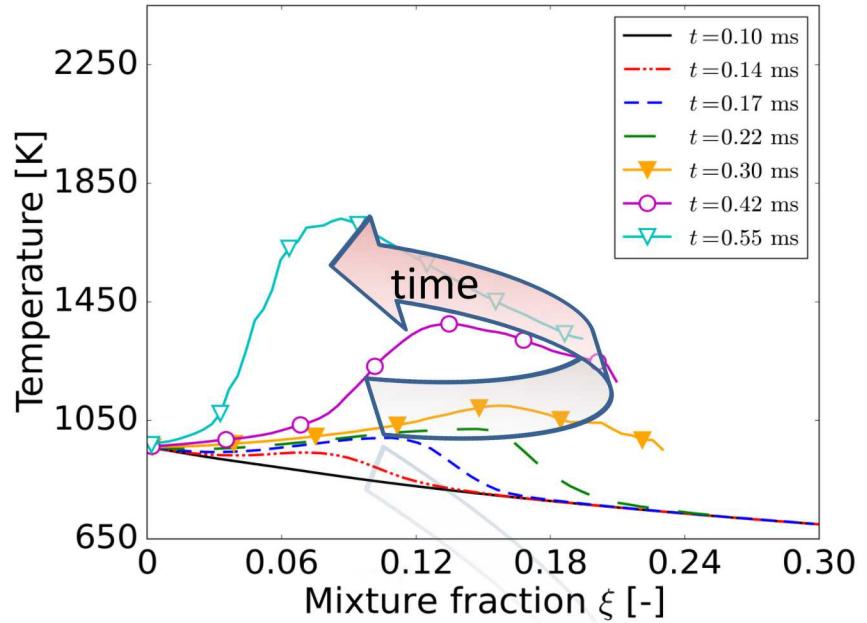
<sup>2</sup>University of Connecticut



*Ketohydroperoxide mass fraction*

# Background and Objective

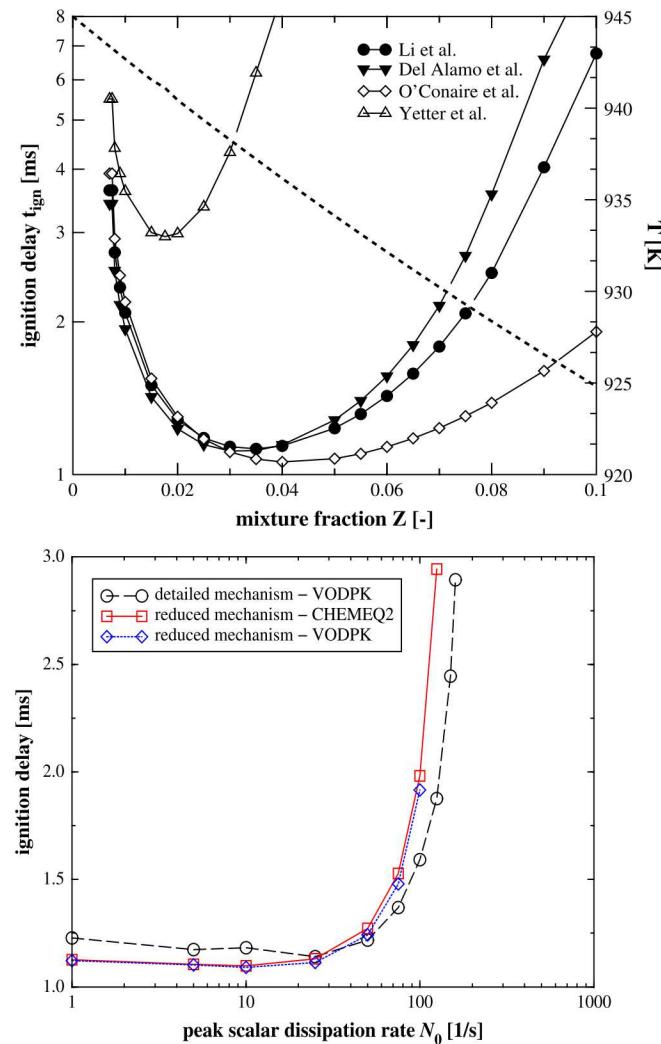
- Low-temperature combustion (LTC) aims at increasing fuel efficiency and reducing emissions
- Under LTC conditions, combustion occurs in a mixed mode and in multiple ignition stages
- Ignition is now very sensitive to the fuel chemistry, especially to the low temperature reactions branch



**Question: How does transport and low-temperature chemistry affect ignition in low-temperature diesel combustion?**

# Background on high-temperature ignition

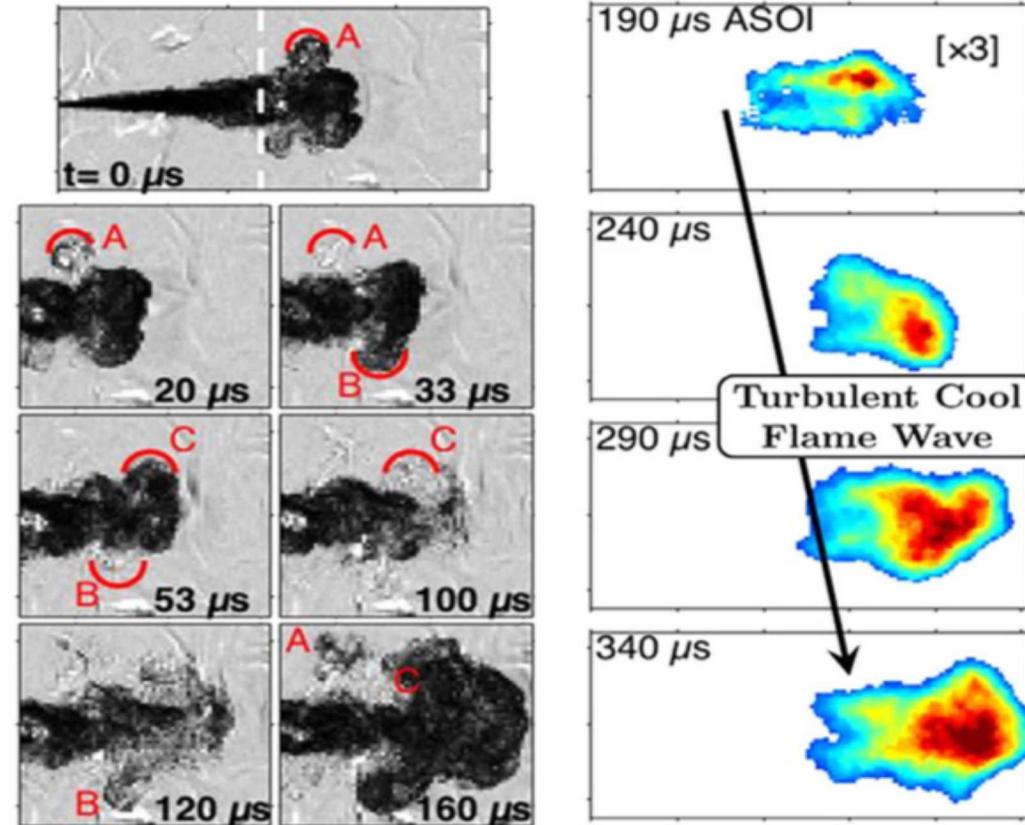
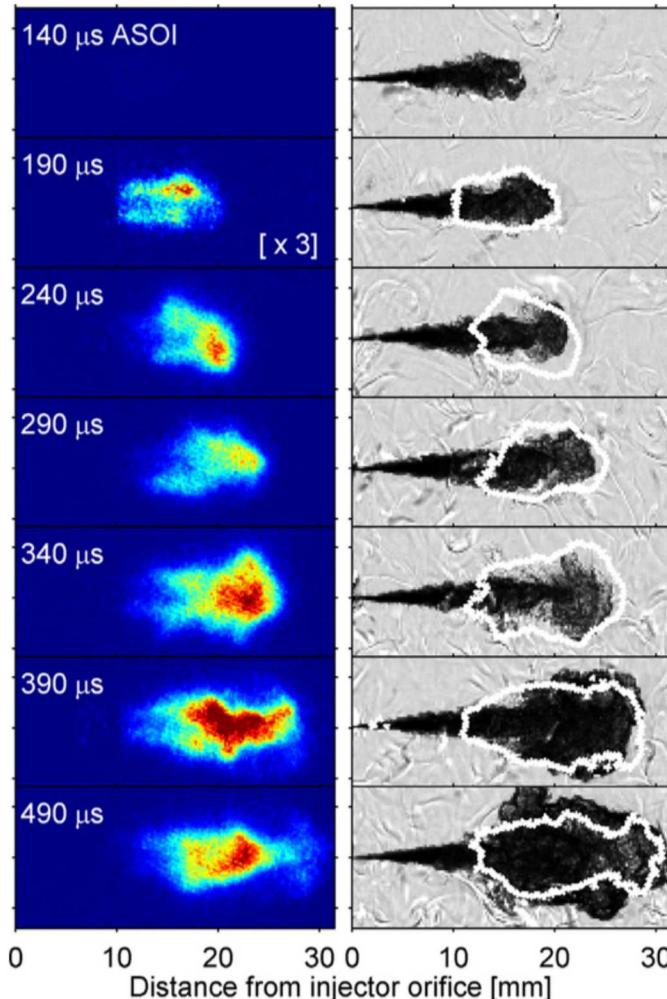
- Homogeneous PSR calculations show the existence of  $x$  value,  $x_m$ , where ignition delay has a minimum;
- Flamelet simulations show the ignition delay increases with scalar dissipation  $N$  until a critical value is reached;
- In practical systems, ignition occurs at locations close to  $x_m$  where  $N$  is low. The ignition delay is longer than in PSR;
- **Question:** which features of high- $T$  ignition carry over to low- $T$  ignition?



**Figure:** ignition delay time in PSR and in nonpremixed flamelet simulation<sup>1</sup>

[1] E. Mastorakos, PECS (2009), pp. 57-97

# Low Temperature Diesel Combustion Experiments – Engine Combustion Network

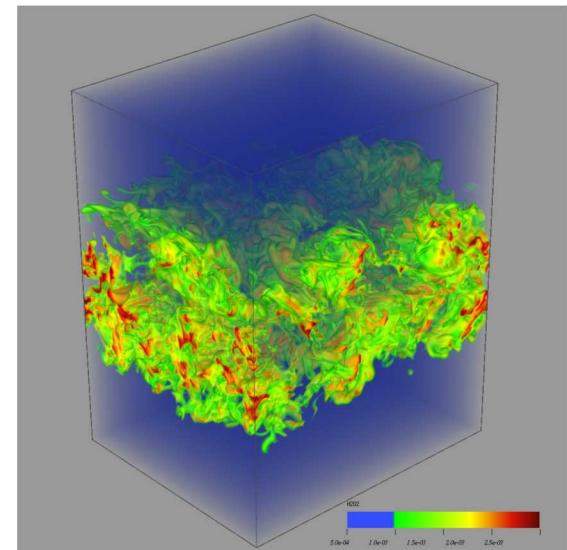
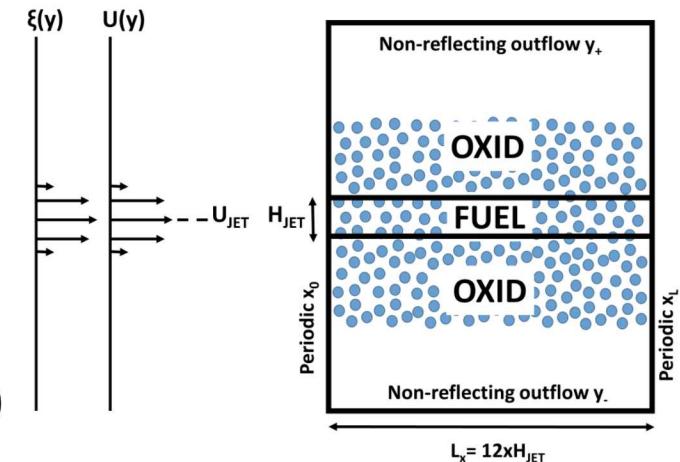


Skeen et al., PROCI 35 (2015)  
3167-3174

Dahms et al., PROCI 36 (2017) 2615-  
2623

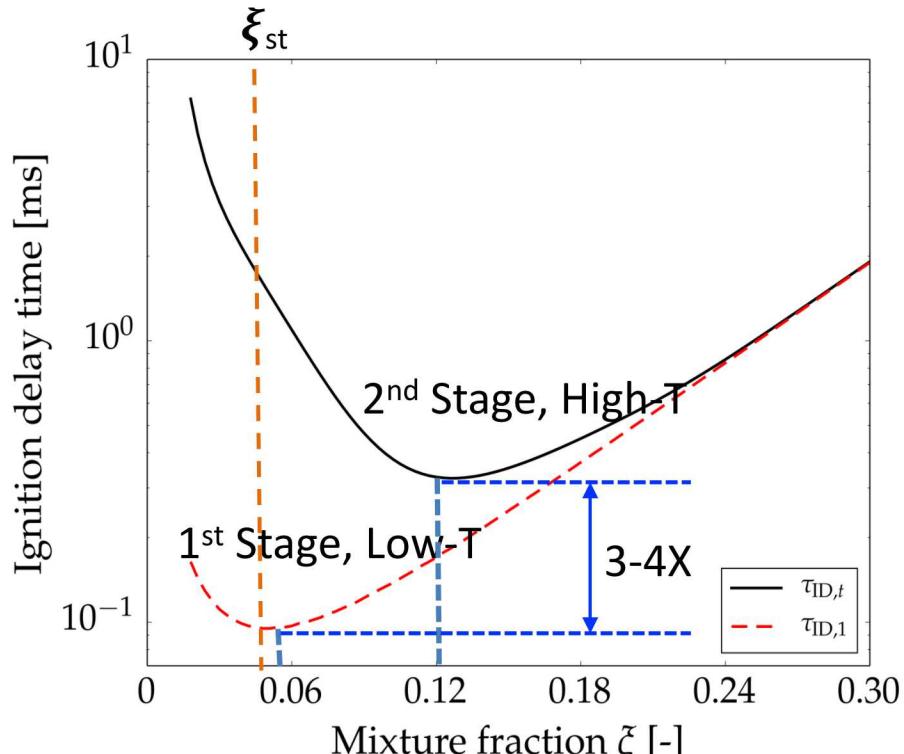
# DNS Configuration and Physical Parameters

- **Pressure:** 25 bar
- **Air stream:** 15%  $X_{O_2}$ +85%  $X_{N_2}$ ,  $T=960$  K
- **Fuel stream:**  $n$ -dodecane at  $\xi=0.3$ ,  $T=450$  K
- **Kinetics:** 35-species non-stiff reduced (Lu)
- **Fuel jet velocity:** 21 m/s,  $Re_j = 7000$ ,  $Re_t \sim 950$
- **Code and cost:** S3D Legion, 60M CPUh
- **Setup:**
  - 3 billion grids
  - 3 microns spatial grid resolution
  - Dimensions: 3.6 mm x 14.0 mm x 3.0 mm
  - 1 ms of physical time with 4 ns timesteps to observe ignition and propagation of burning flames throughout the domain
  - BCs: X and Z periodic, Y NSCBC outflows

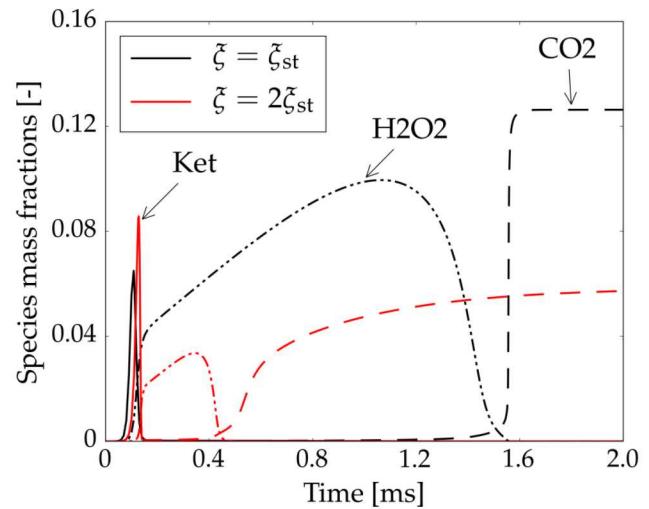
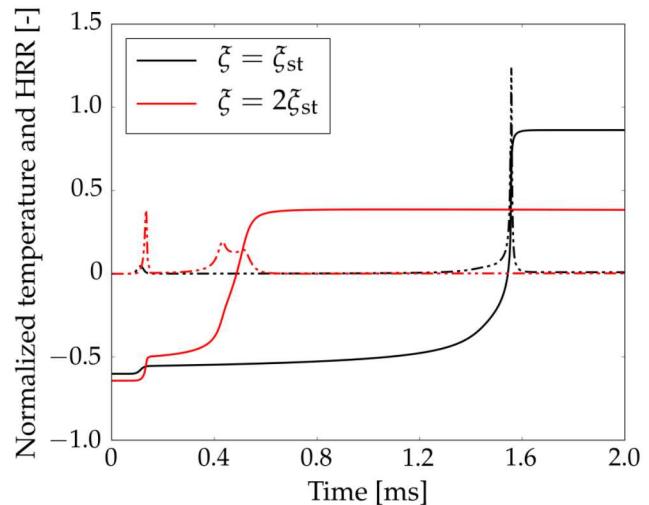


**Figure:**  $H_2O_2$  mass fraction at  $t=0.17$  ms after start of reactions

# Homogeneous Multi-Stage Autoignition



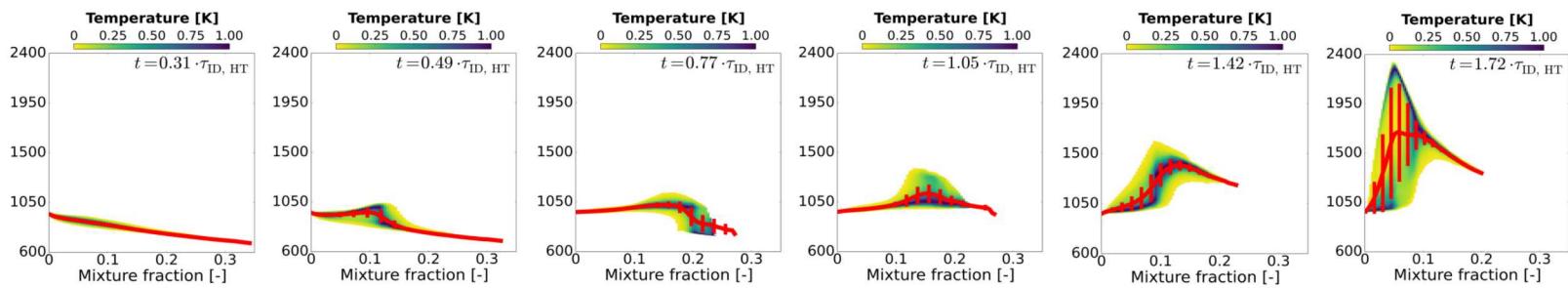
Homogeneous ignition delay time



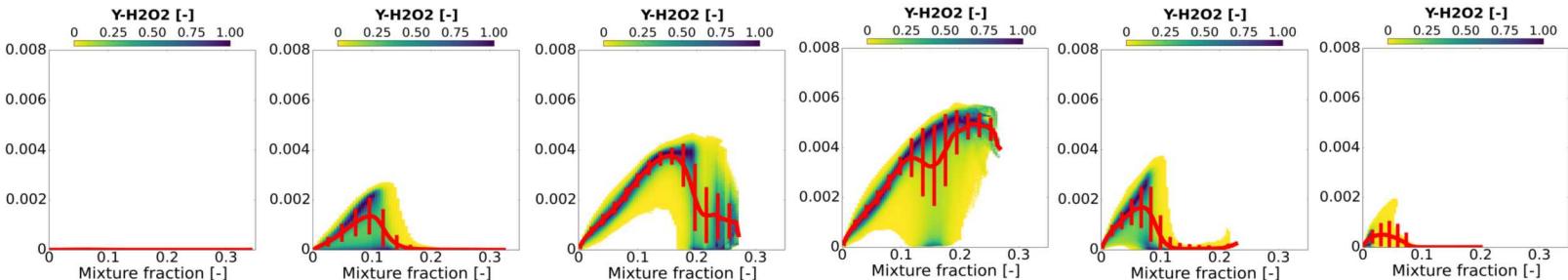
Temporal evolution of selected reactive scalars

# Conditional statistics reveal ignition dynamics

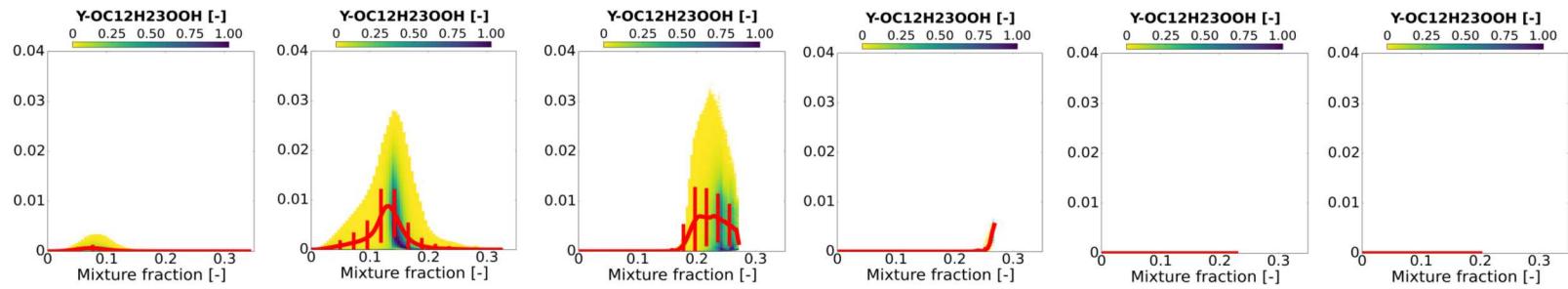
Temperature



H<sub>2</sub>O<sub>2</sub>

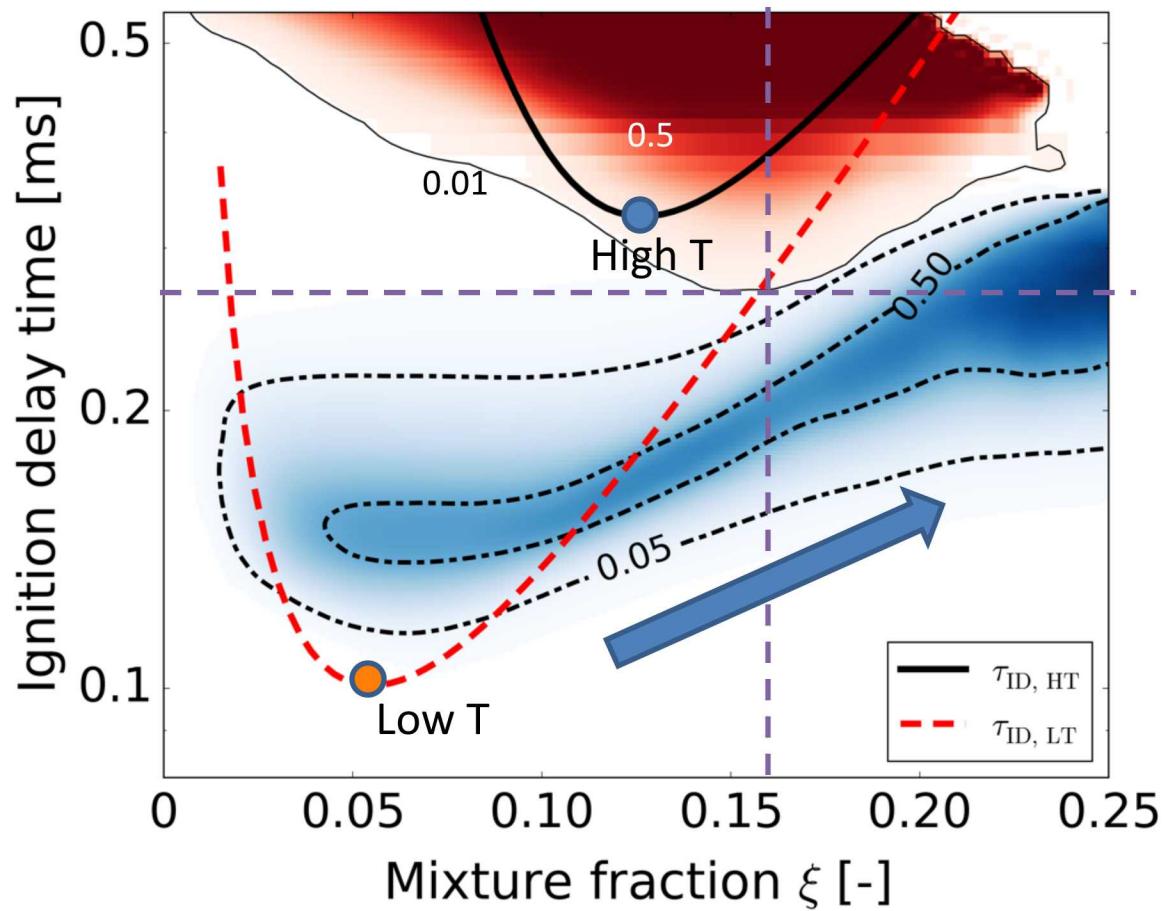


Ketohydro-  
peroxide



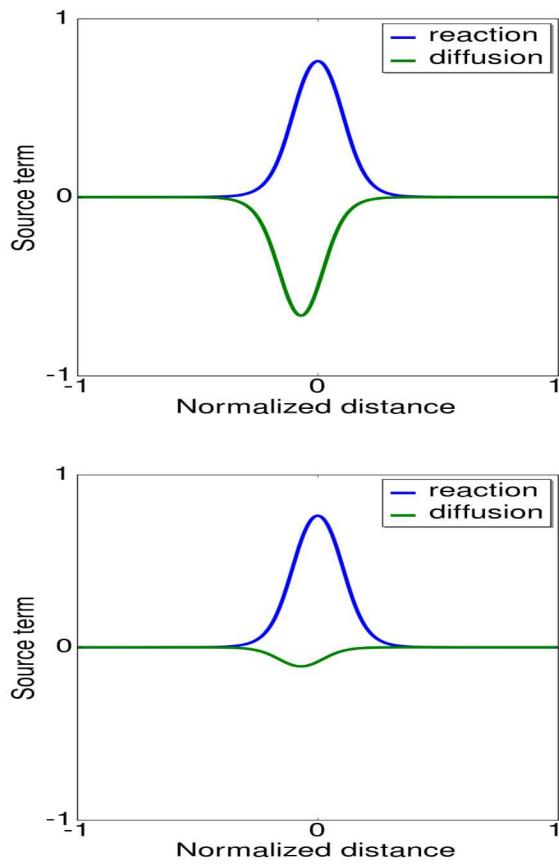
time

# Turbulent versus homogeneous ignition



**Low-T and high-T ignition in jet can be faster and than in a PSR !**

# Propagation mechanism for low-T reaction front



Sketch of reaction / diffusion balance along normal for KET for flame and ignition kernel

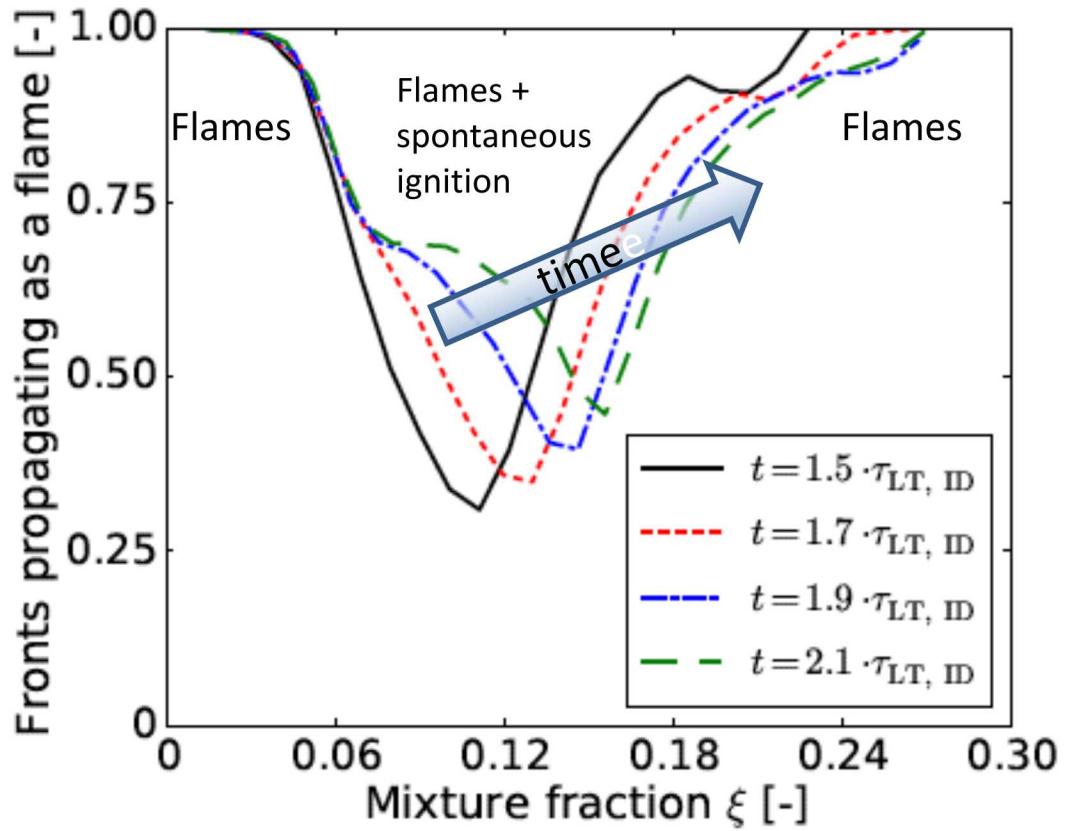
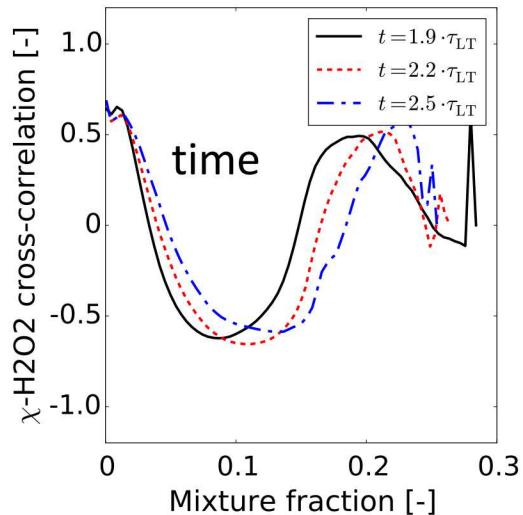
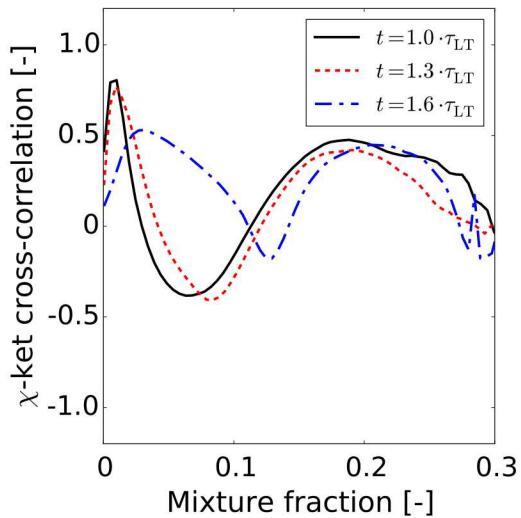


Figure: Fraction of reactive low-T fronts propagating as a flame

**Low-T fronts propagate through diffusively supported flame**

# Effect of Scalar Dissipation Rate on Low Temperature Ignition



# Conclusions

- Low-temperature reactions create the conditions for high-temperature ignition to occur faster than under homogeneous conditions;
- Low-temperature front appears to propagate through a diffusively supported cool flame;
- High scalar dissipation appears to delay low-temperature ignition; however, it leads to faster ignition at very rich mixture conditions;
- High-T ignition starts at conditions richer-than-homogeneous conditions ( $\xi=0.16$  compared to  $\xi=0.12$ ). Edge flames are seen to form around  $\xi_{st}$ . High-T flame ignites mainly by propagation of rich premixed flames following hot ignition to  $\xi_{st}$ .

# DNS of multi-injection mixing and combustion at compression ignition engine conditions

M. Rieth<sup>a</sup>, M. Day<sup>b</sup>, C.-B. Kweon<sup>c</sup>, Jacob Temme<sup>c</sup>

J.B. Bell<sup>b</sup>, J.H. Chen<sup>a</sup>

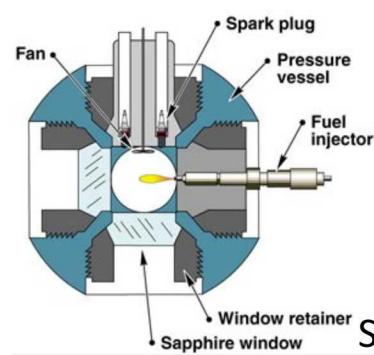
<sup>a</sup>Sandia National Laboratories

<sup>b</sup>Lawrence Berkeley National Laboratory

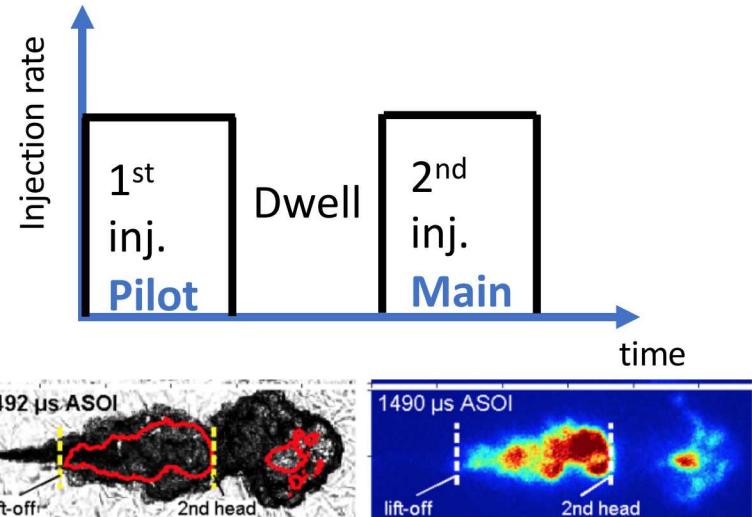
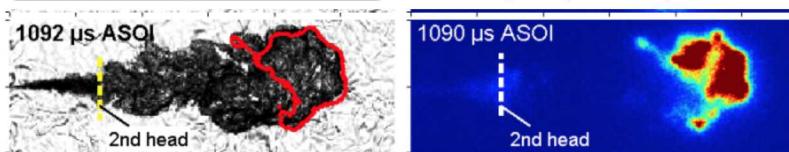
<sup>c</sup>U.S. Army Research Laboratory



# Objectives & Setup



Sandia Spray A experiment<sup>2</sup>



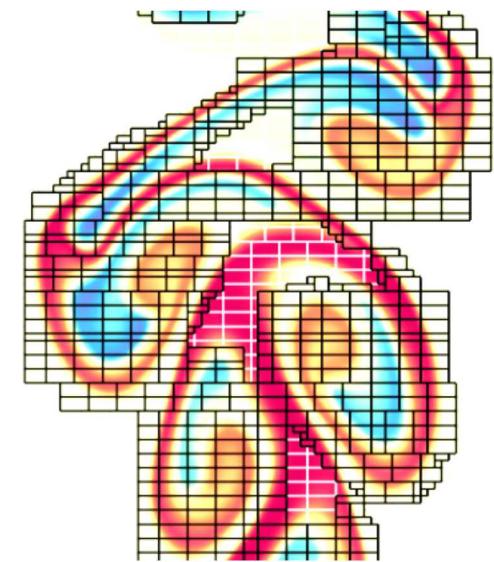
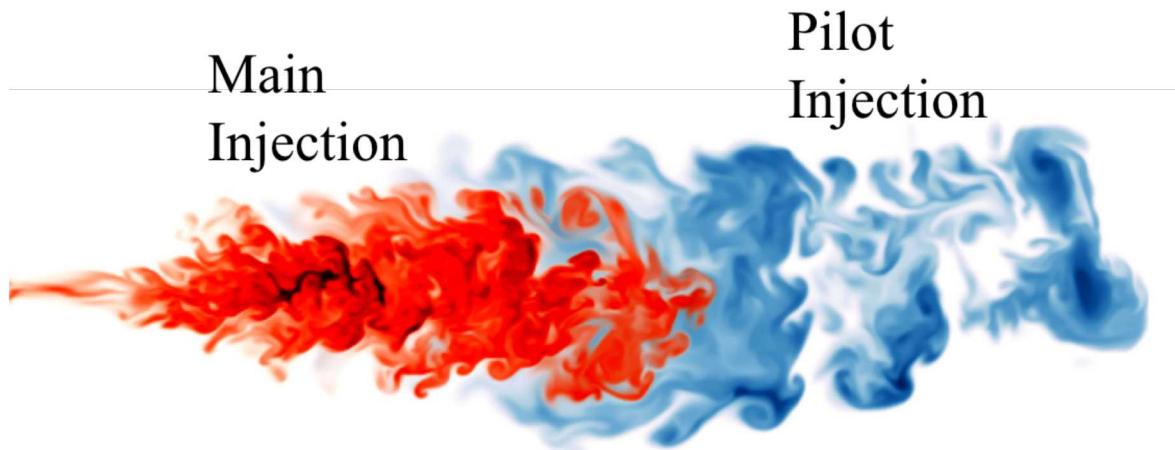
Ignition delay of 2<sup>nd</sup> injection decreased by roughly factor 2<sup>3</sup>

- Purely gaseous n-dodecane/air jet @ T=470K, Z=0.45
- Ambient conditions: 900K, 15% O<sub>2</sub>, 85% N<sub>2</sub>, 60atm
- Conditions adapted from Dalakoti et al.<sup>1</sup>  
→ **downscaled ECN Spray A, keeping Da constant (Re≈19,000, Da<sub>jet</sub>≈0.02)**
- Multi-injection: 0.5 ms pilot, 0.5 ms dwell, 0.5 ms main
- **Main injection sees very different conditions compared to pilot injection**
- **How do mixing and different thermo-chemical conditions affect ignition in the main injection?**

<sup>1</sup>Dalakoti et al., ICDERS, 2017. <sup>2</sup>[www.crf.sandia.gov](http://www.crf.sandia.gov). <sup>3</sup>Skeen et al., JSTOR, 2015.

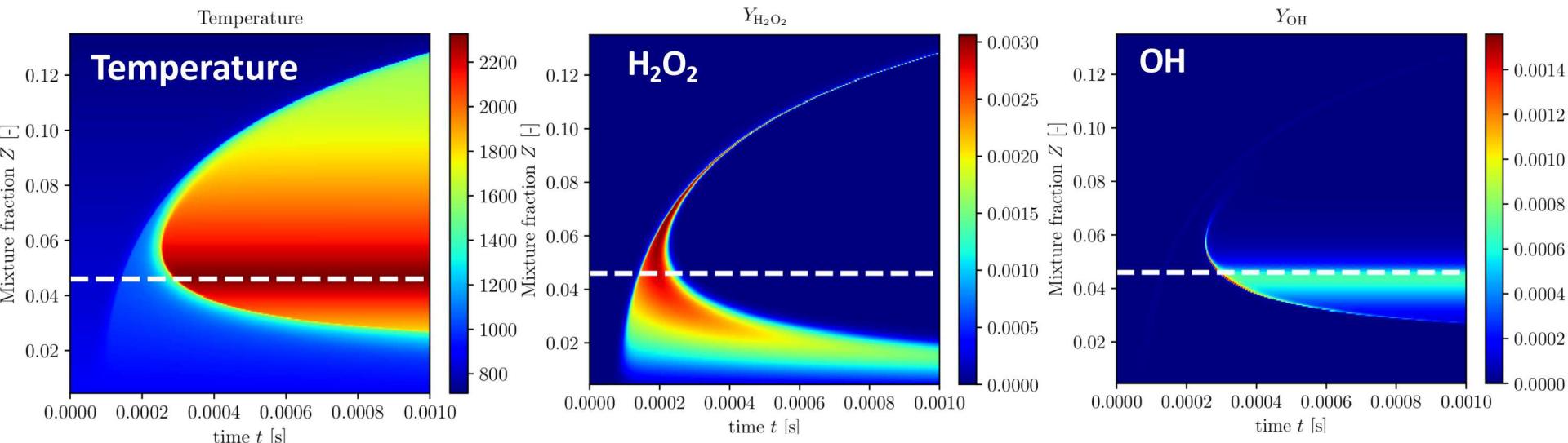
# PeleLM Code & Numerical Setup

- **PeleLM** – low-Mach adaptive mesh refinement code based on AMReX
- Spectral deferred correction scheme for fluid dynamics-chemistry coupling
- Code is open-source at <https://amrex-combustion.github.io/>
- Resolution ~1.25 micron required for rich premixed cool flames,  
**currently 5 micron for full multi-injection run**
- Size of simulation: 0.5B cells ( $O(100)B$  cells full run without AMR)
- 35 species reduced n-dodecane mechanism  
(Yao et al., 2017; Borghesi et al., 2018)



Emmett et al., arxiv, 2018.  
E. Motheau AMReX gallery.

# Zero-dimensional n-dodecane ignition

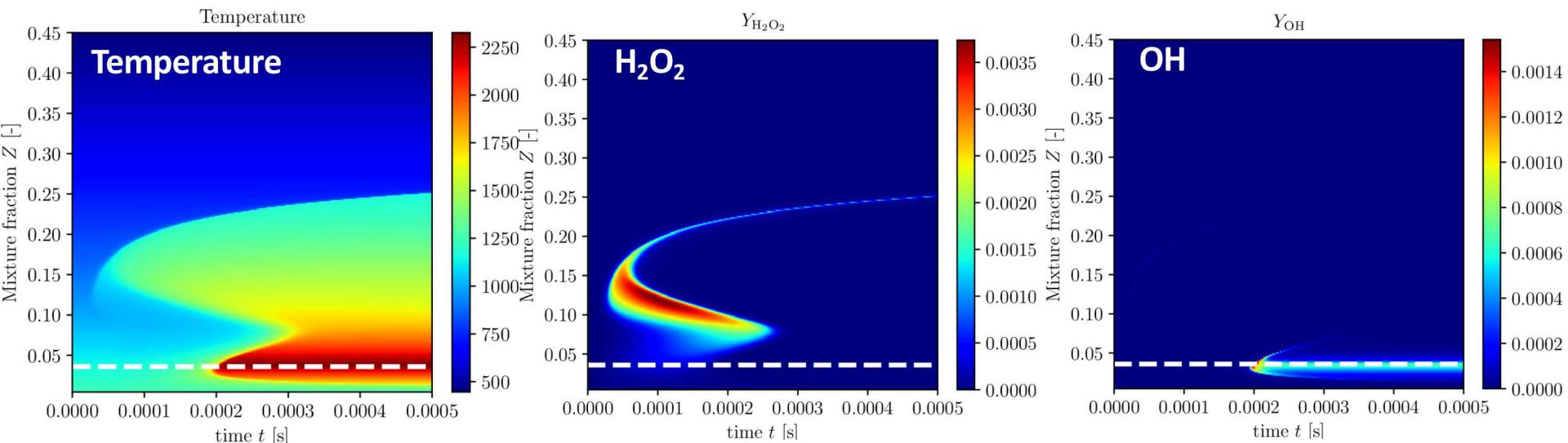


- N-dodecane exhibits two-stage ignition with minimum ignition delay at 'preferred mixture fraction' for each stage<sup>1</sup>
  - $H_2O_2$  is a marker for low temperature combustion
  - OH is a marker for high temperature combustion

<sup>1</sup>Mastorakos, PECS, 2009.

# Zero-dimensional n-dodecane ignition with products

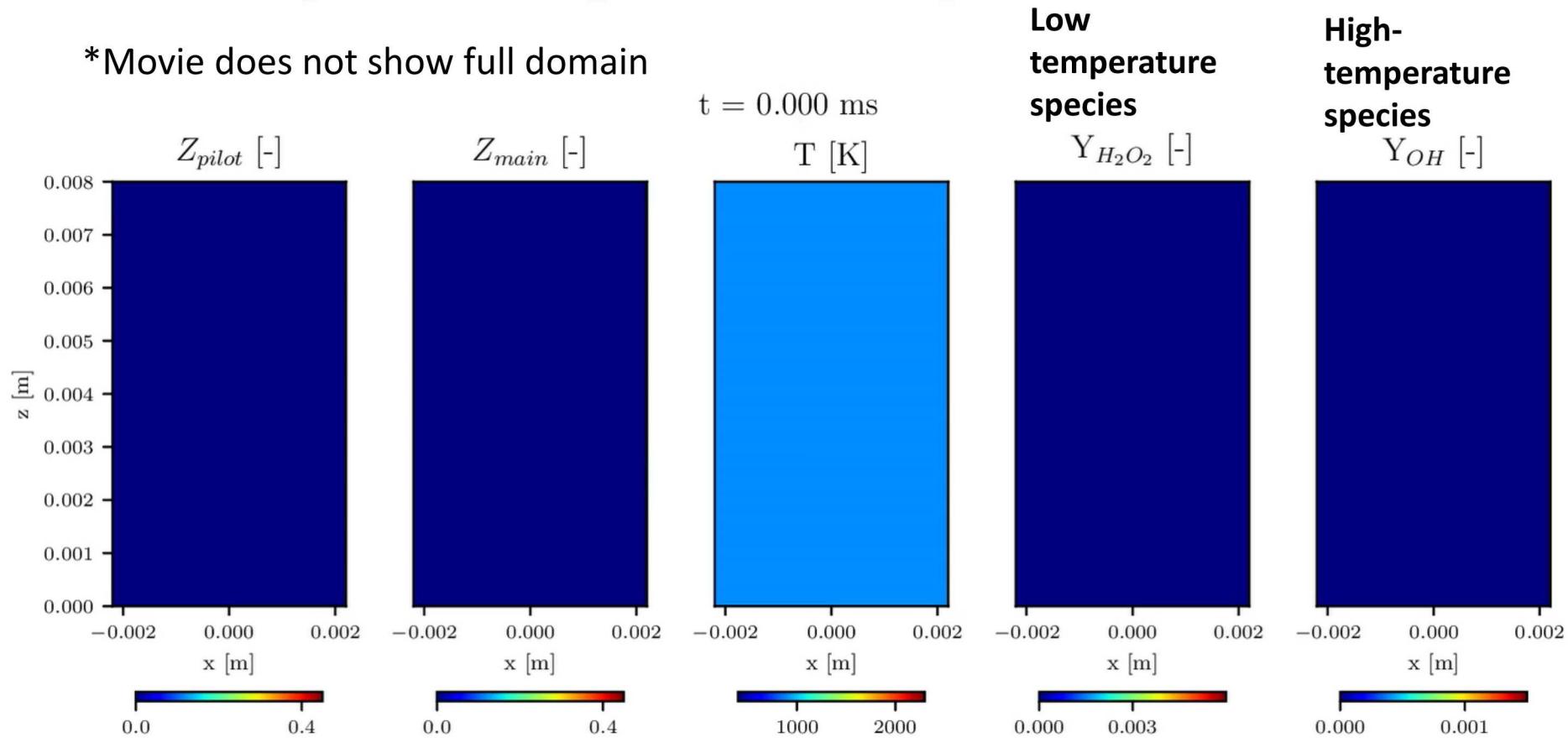
Oxidizer now consists of an equilibrated lean mixture with  $Z=0.01$



- Low temperature ignition shifts toward richer mixtures (by almost a factor of 3, has a much shorter ignition delay while hot ignition remains the same)

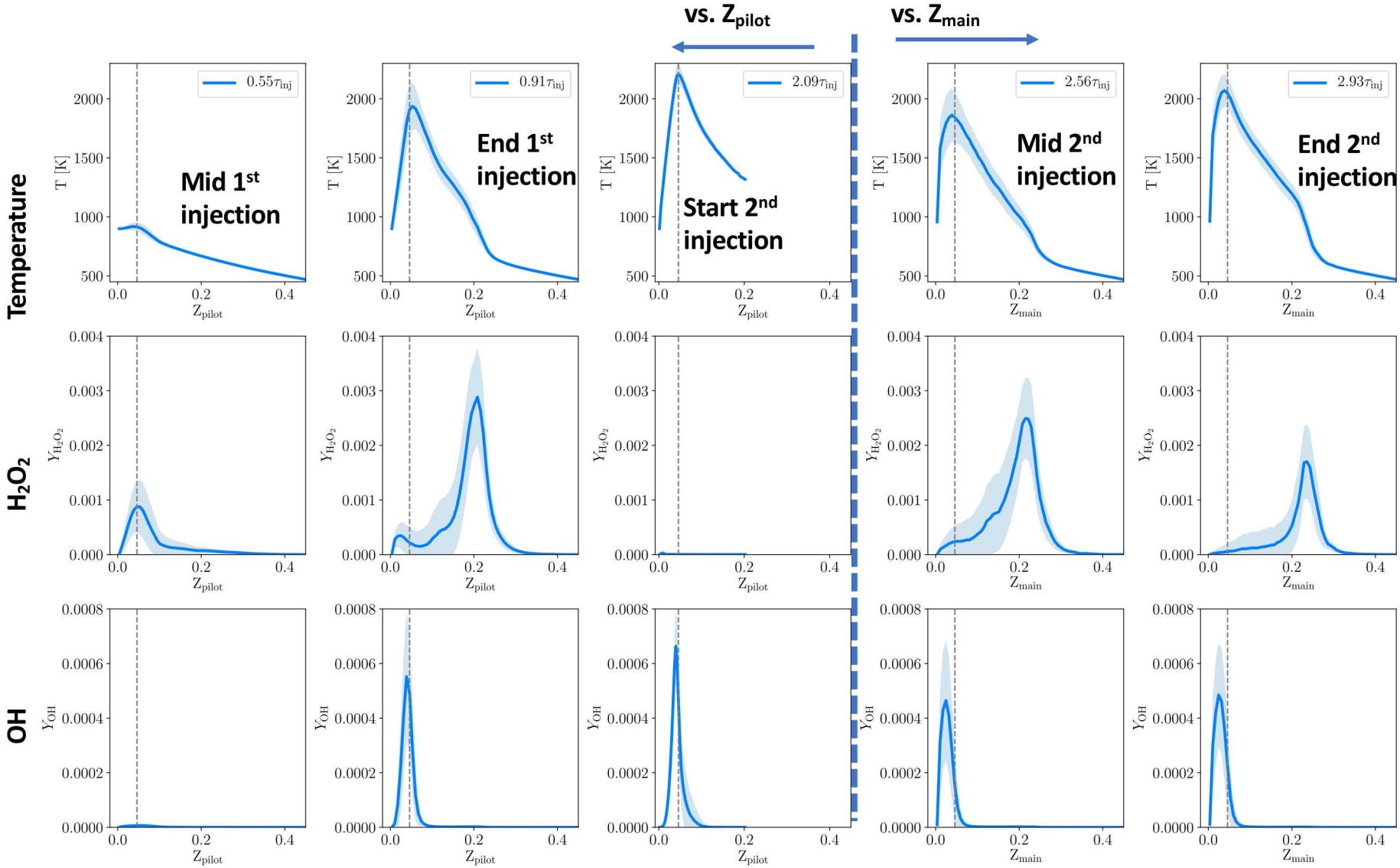
# Multi-injection ignition sequence

\*Movie does not show full domain

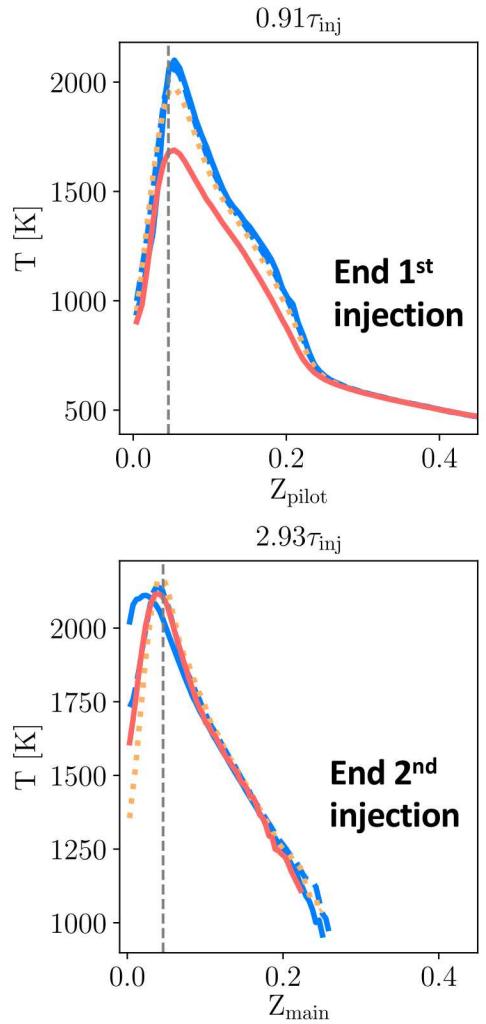
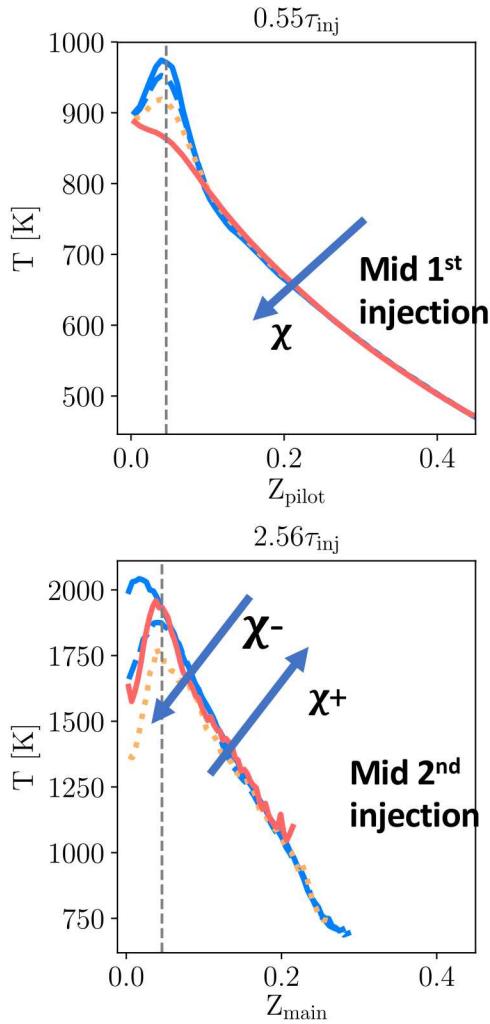


Mixture fractions track fluid from individual injections (two additional transport equations)

# Conditional statistics



# Effect of mixing on ignition



$$\chi_{\text{pilot}} = 2D(\partial Z_{\text{pilot}} / \partial x_j)^2$$

- $P(\chi_{\text{pilot}}) \leq 0.25$
- $0.25 < P(\chi_{\text{pilot}}) \leq 0.50$
- $0.50 < P(\chi_{\text{pilot}}) \leq 0.75$
- $0.75 < P(\chi_{\text{pilot}}) \leq 1.00$

$$\chi_{\text{cross}} = 2D(\partial Z_{\text{pilot}} / \partial x_j \cdot \partial Z_{\text{main}} / \partial x_j)$$

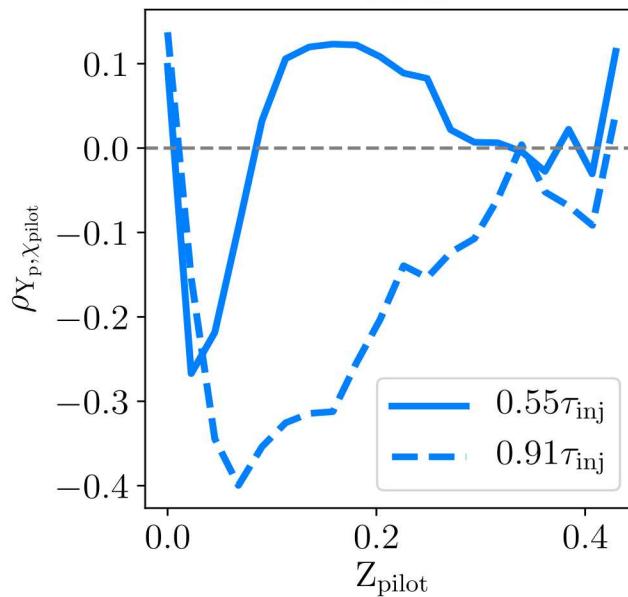
- $P(\chi_{\text{cross}}^-) \leq 0.50$
- $0.50 < P(\chi_{\text{cross}}^-) \leq 1.00$
- $P(\chi_{\text{cross}}^+) \leq 0.50$
- $0.50 < P(\chi_{\text{cross}}^+) \leq 1.00$

Bins based on pilot scalar dissipation rate

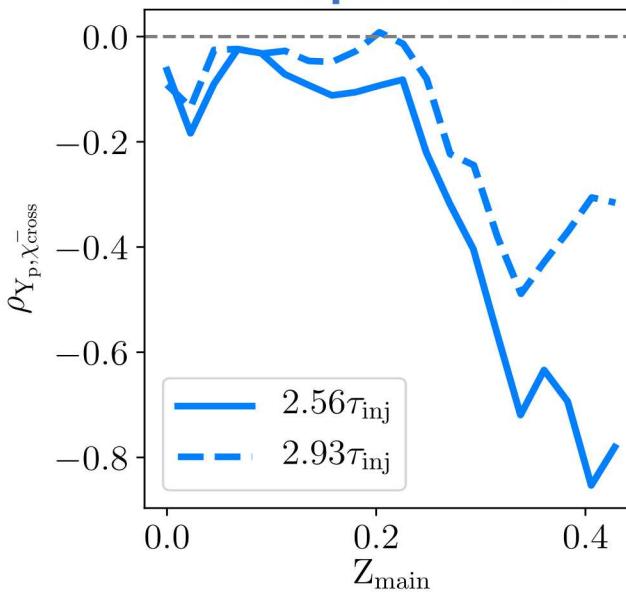
Bins based on cross scalar dissipation rate

# Effect of mixing on ignition

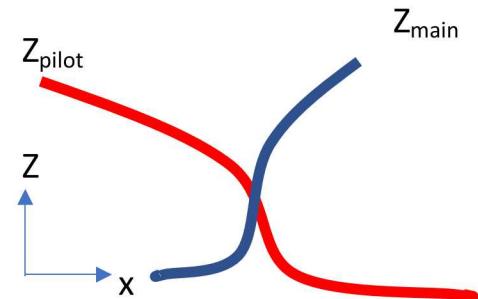
1<sup>st</sup> injection  
**Correlation**  
between progress  
variable and pilot  
scalar dissipation  
rate



2<sup>nd</sup> injection  
**Correlation**  
between progress  
variable and  
cross scalar  
dissipation rate



Only negative  
values of cross  
scalar dissipation  
rate taken into  
account



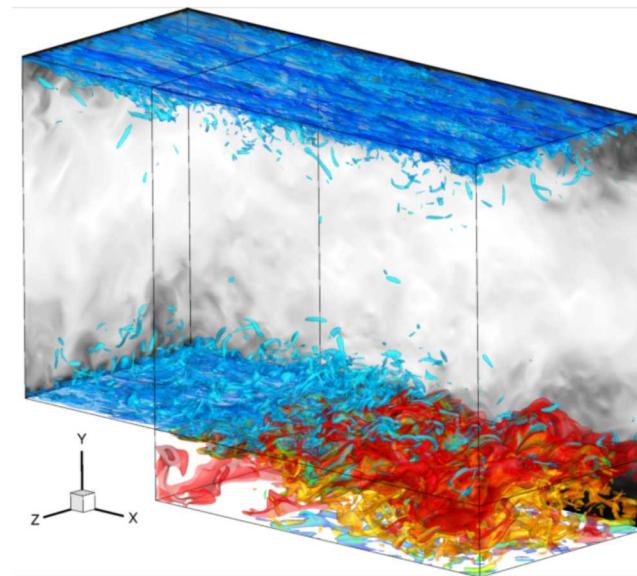
1<sup>st</sup> injection consistent to work by Borghesi et al., C&F, 2018.

# Conclusions

- First- and second stage pilot ignition consistent with previous numerical studies
- Accelerated ignition for main injection observed consistent with experiments
- Pilot/main mixture fraction scalar dissipation rates show similar log-normal-like pdfs
- Cross SDR pdf has sharp peak and stretched exponential tails, skewed toward negative values
- **Strong mixing inhibits ignition of first injection, promotes ignition of second injection**

# DNS of a turbulent premixed flame stabilized over a backward facing step

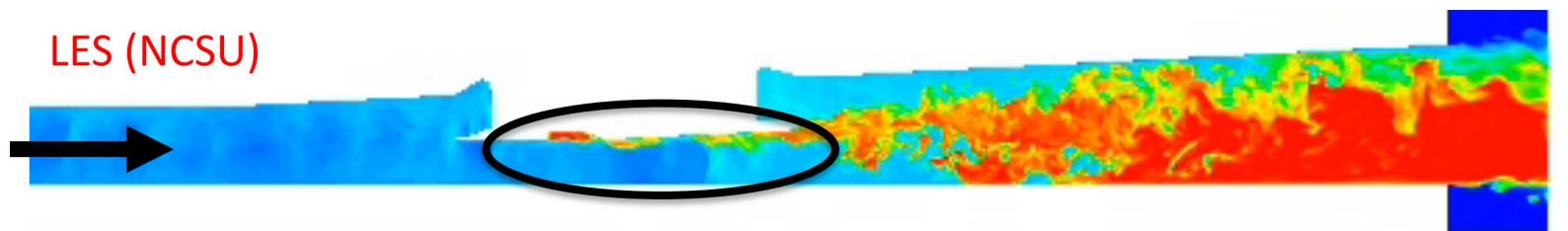
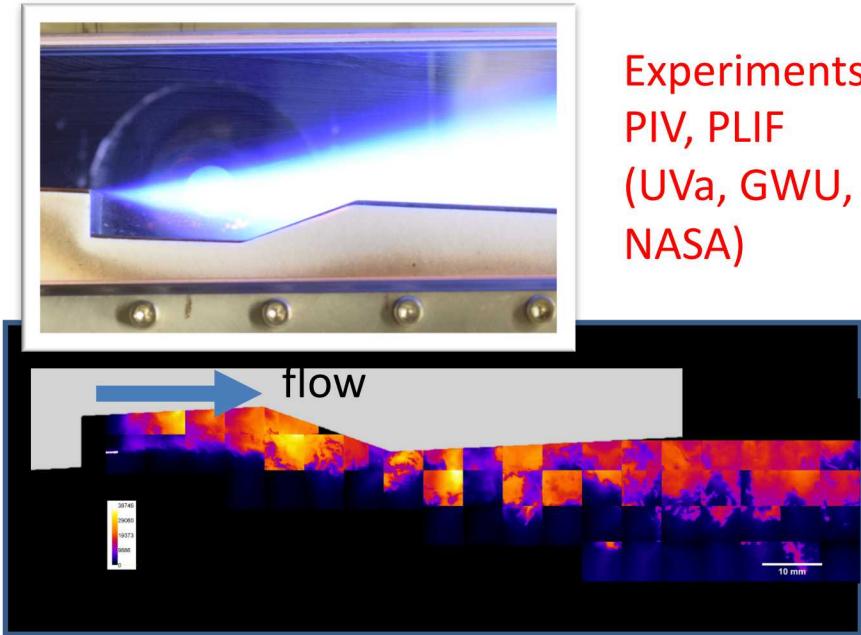
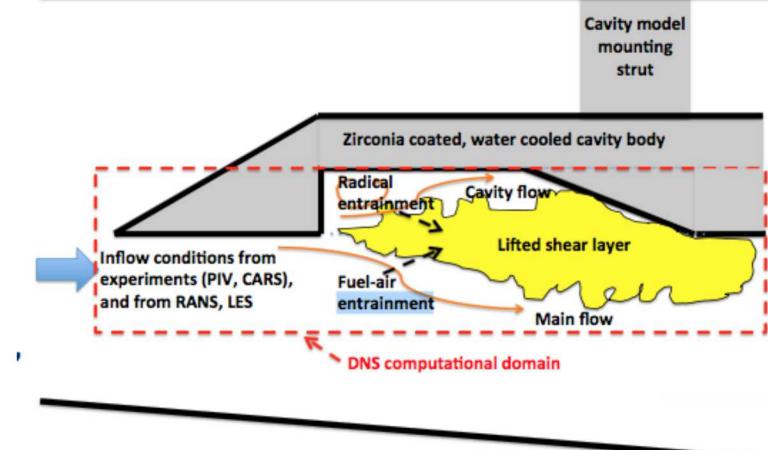
Konduri Aditya, Hemanth Kolla and Jacqueline H. Chen  
*Sandia National Laboratories*



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OLCF, NERSC

# Overview



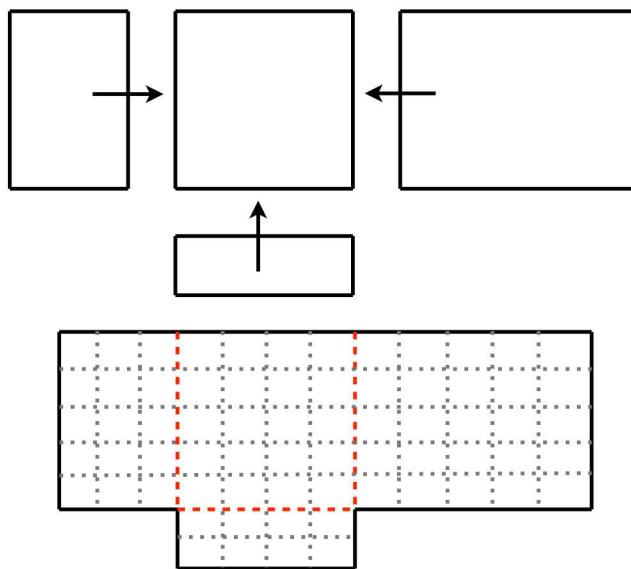
Gain insights into:

- Flame stabilization mechanism
- Effect of heat release
- Turbulence and chemistry interactions

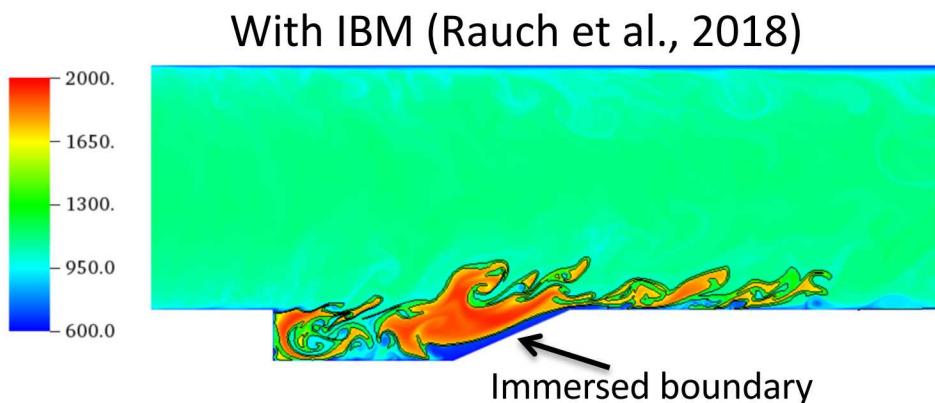
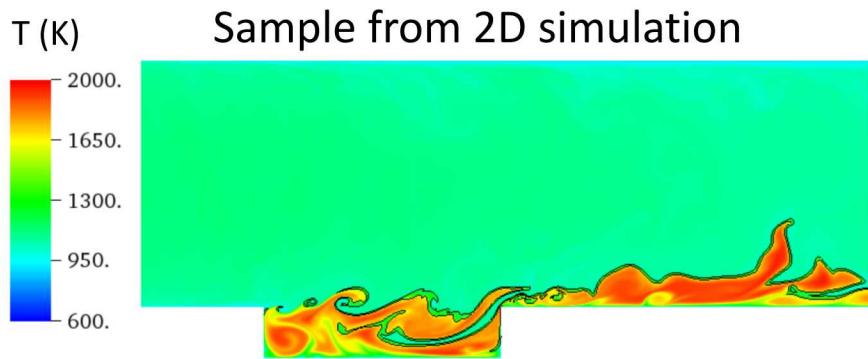
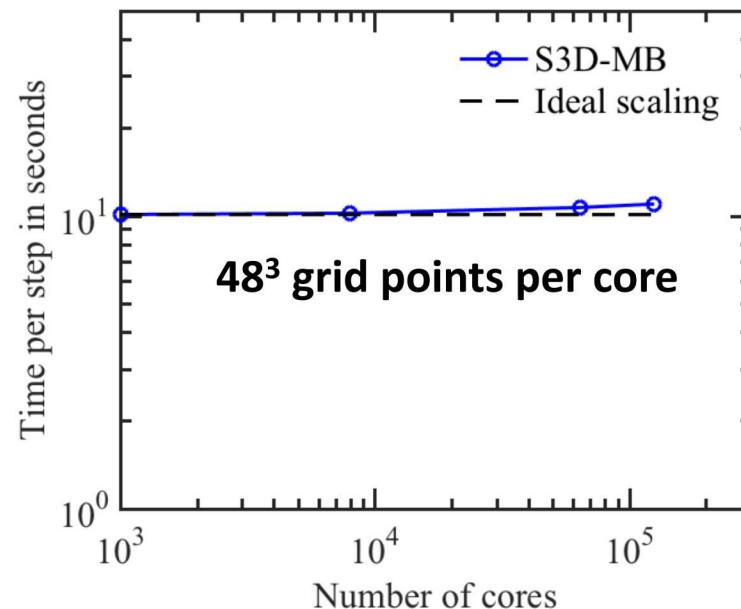
Experiments  
PIV, PLIF  
(UVa, GWU,  
NASA)

# S3D - Multiblock

## Multiblock construction



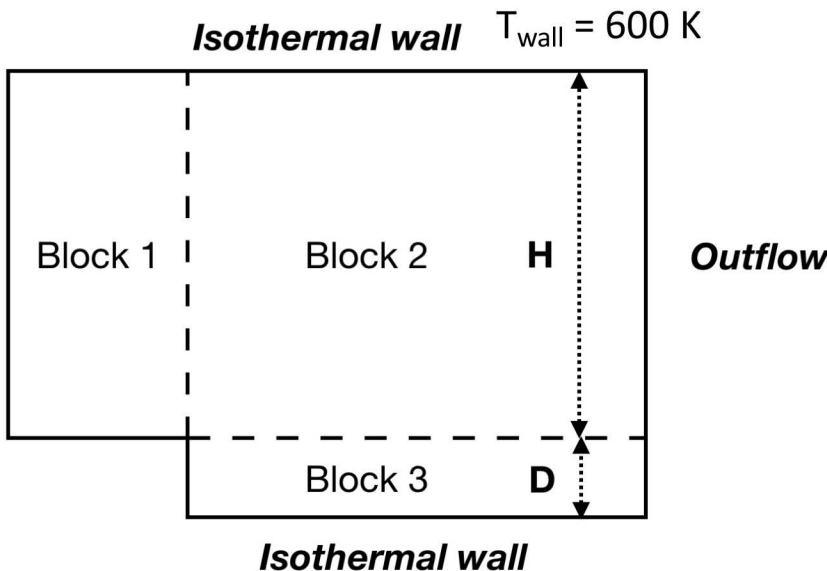
## Weak scaling on Titan



# Backward-facing step

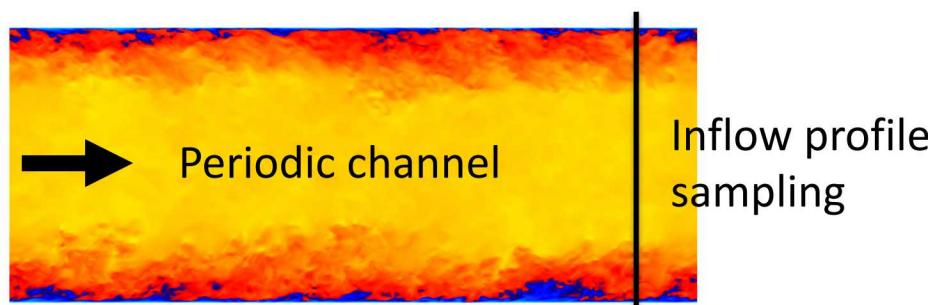
Ethylene-air  
 $\Phi = 0.42$   
 $U = 200 \text{ m/s}$   
 $u' = 10\%$   
 $T = 1125 \text{ K}$

**Inflow**



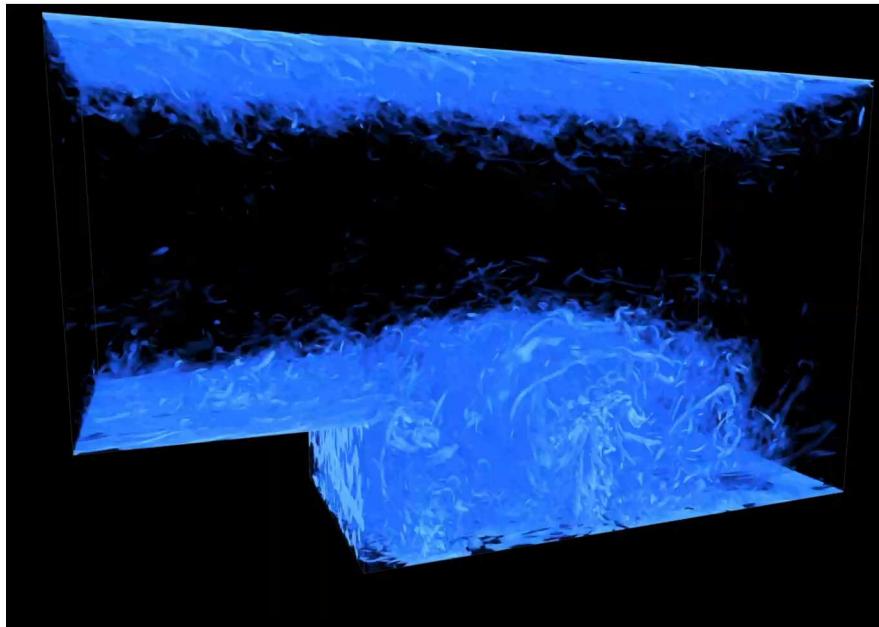
H	1.47 cm
D	0.3048 cm
$Re_H$	35000
$Re_T$	788
Grid count	2.6 billion
CPU hrs	25 million

- **Mechanism:** 22 species non-stiff reduced ethylene-air (Lu et al. 2012)
- **Transport model:** mixture averaged
- **Turbulent inflow profile:** feed data generated from a separate 3D DNS of channel

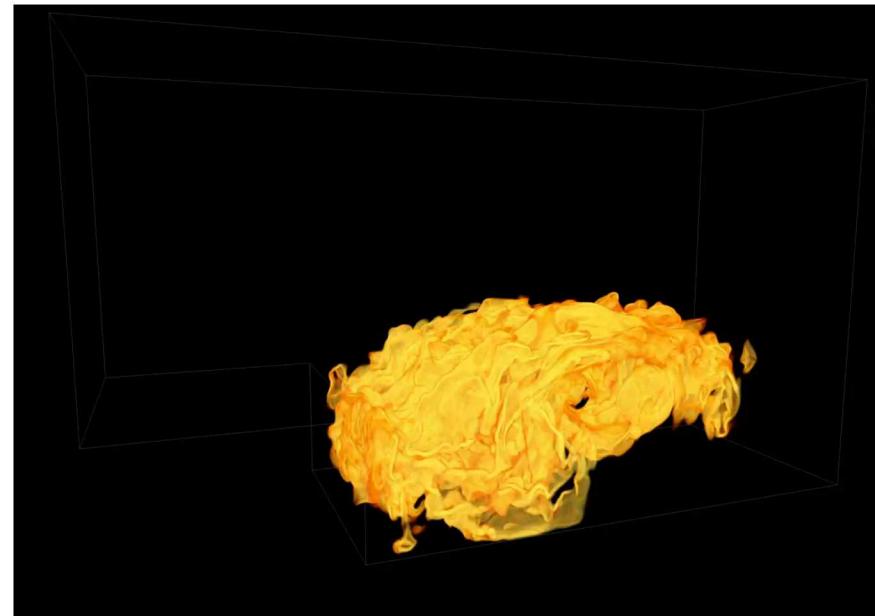


# Flame stabilization

Vorticity magnitude

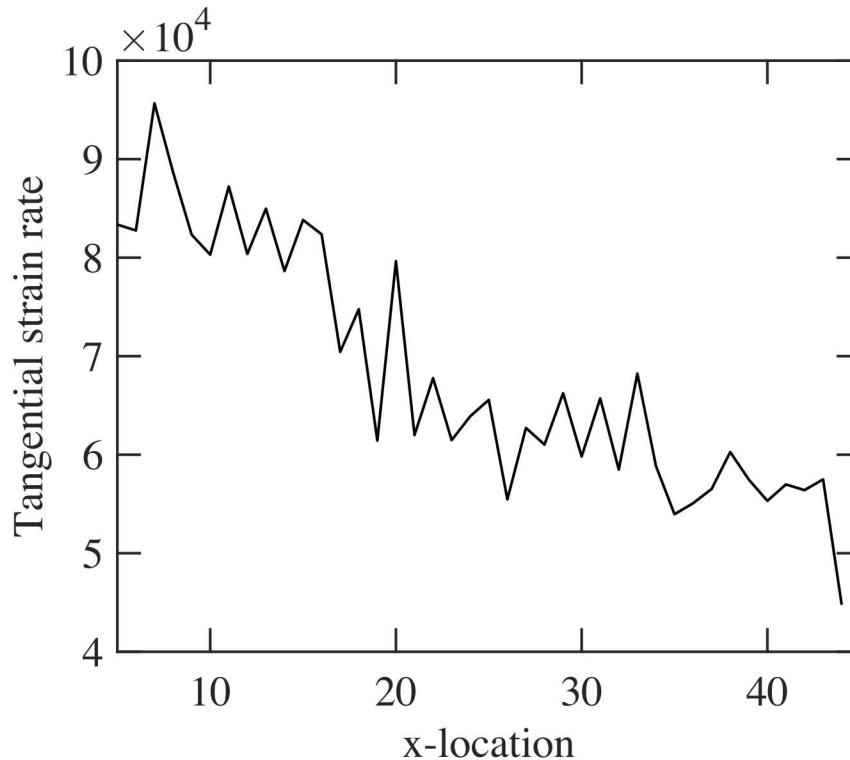


Heat release rate



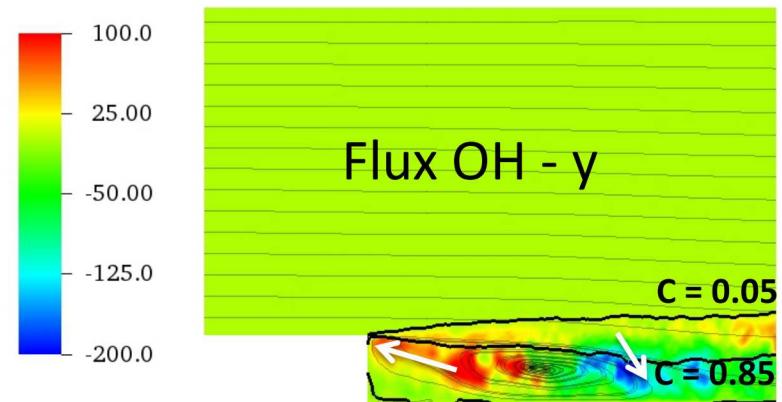
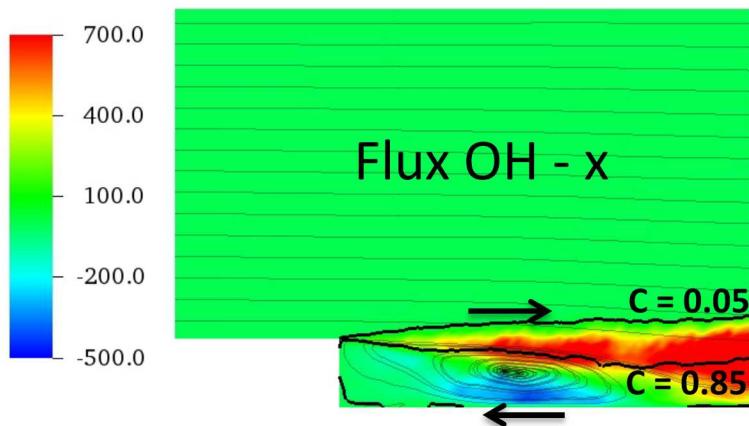
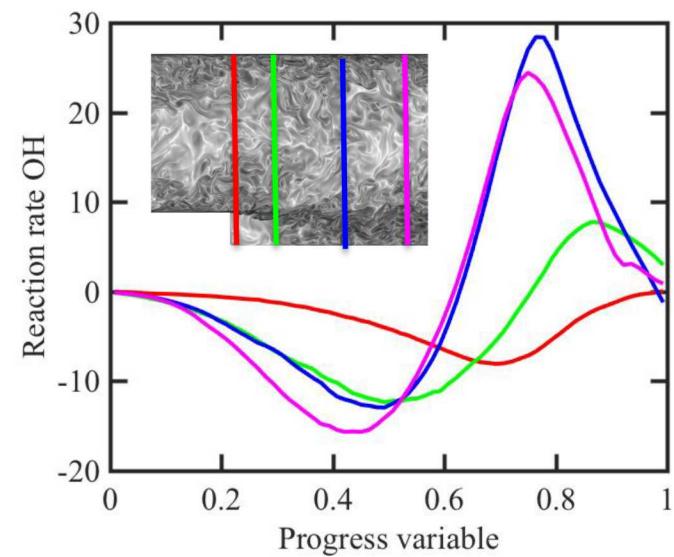
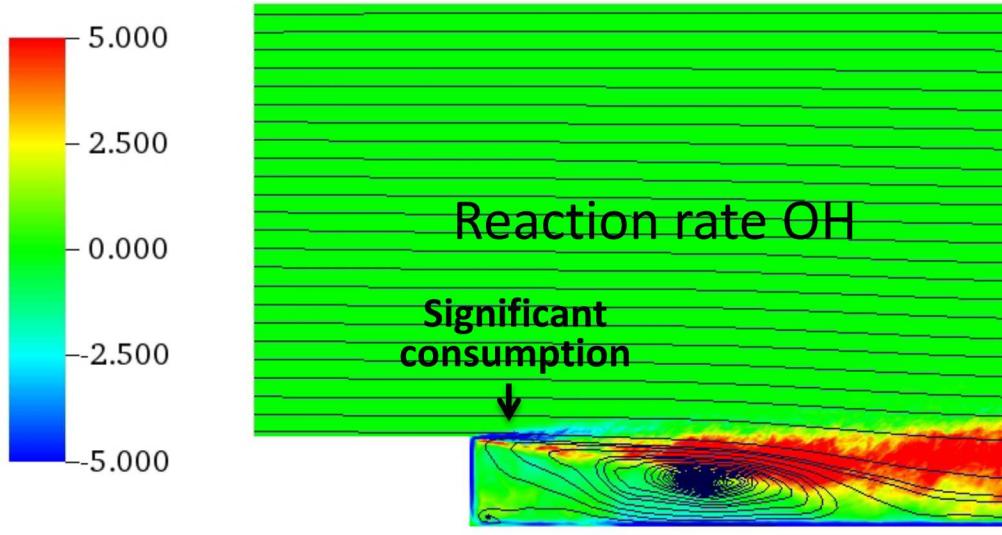
- Flame stabilizes near the corner of the step
- Extends downstream in the shear layer
- Flame inhibits rapid expansion of the channel flow

# Flame - tangential strain rate



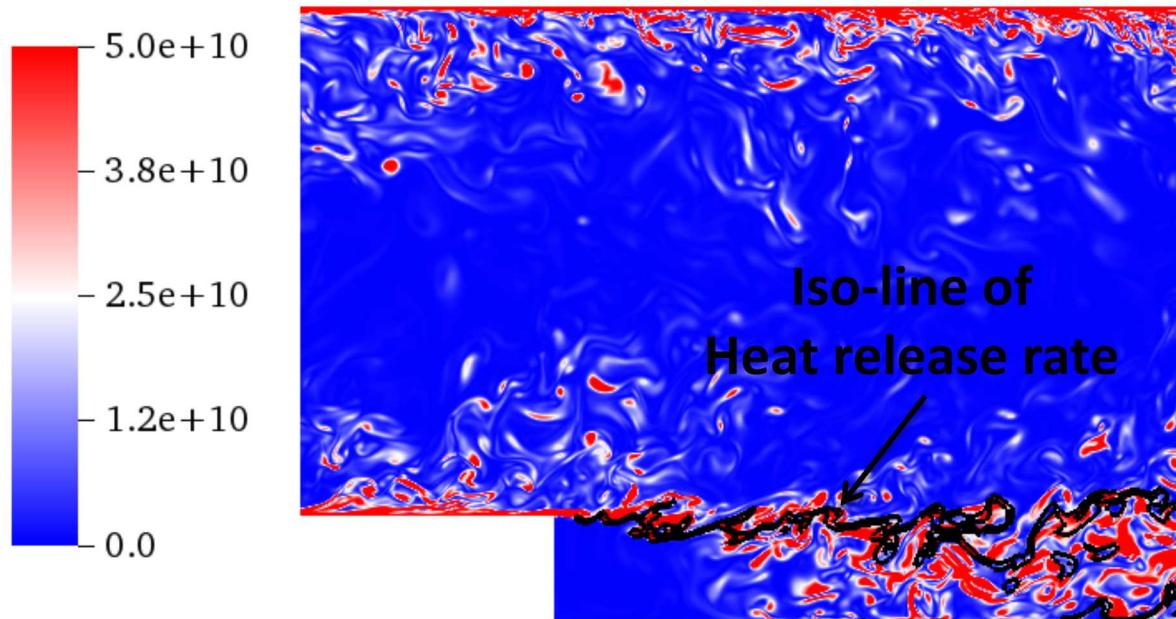
- Strain rate relaxes downstream
- Affects flame structure

# Flame stabilization



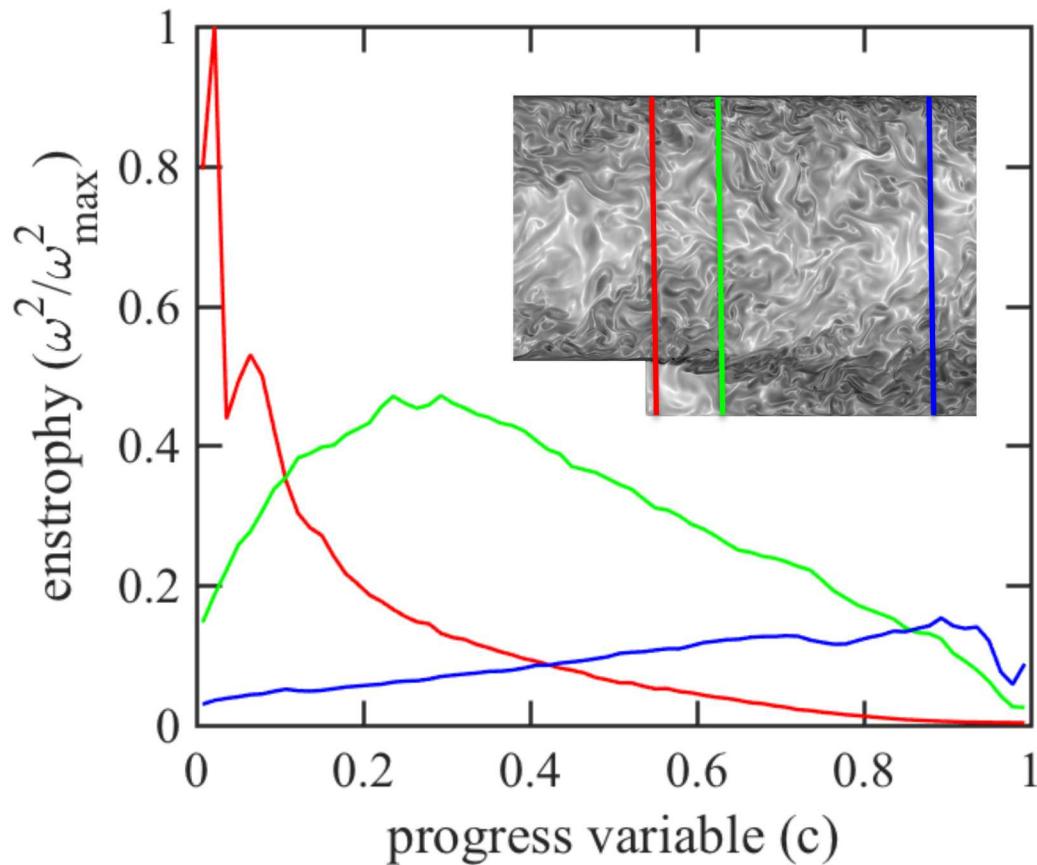
# Vorticity dynamics

## Enstrophy



- Closer to the step: near-wall structures present on the reactant side
- Downstream: significant vorticity present on the product side

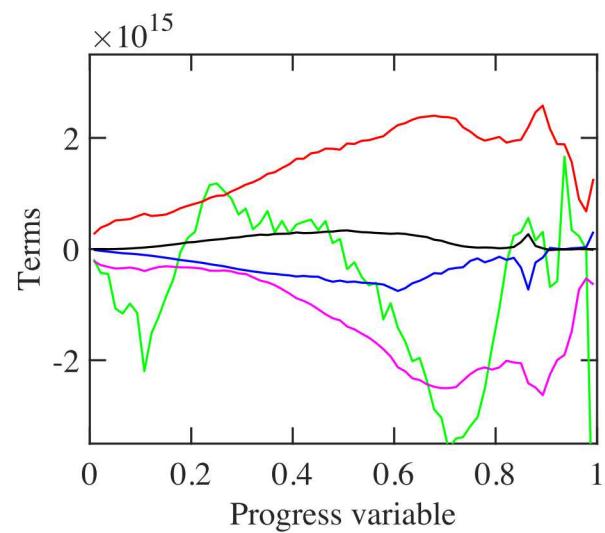
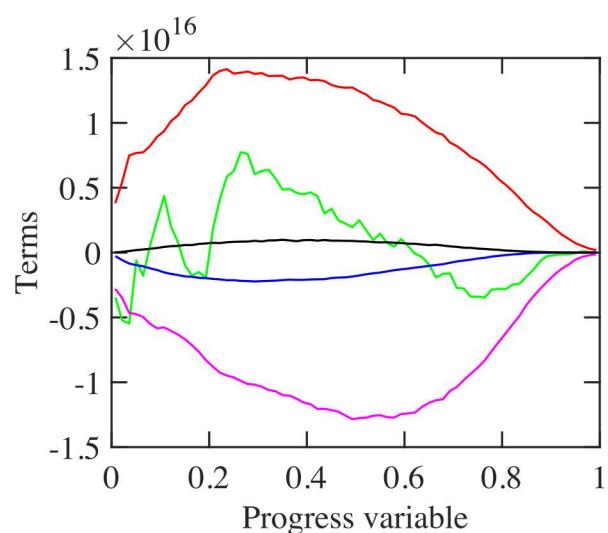
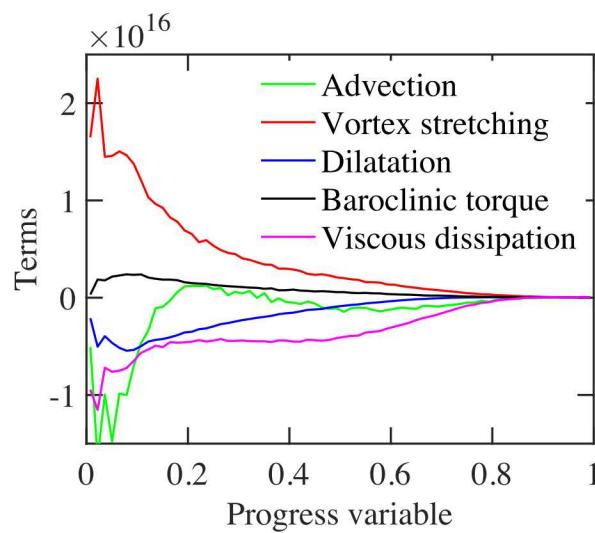
# Vorticity dynamics



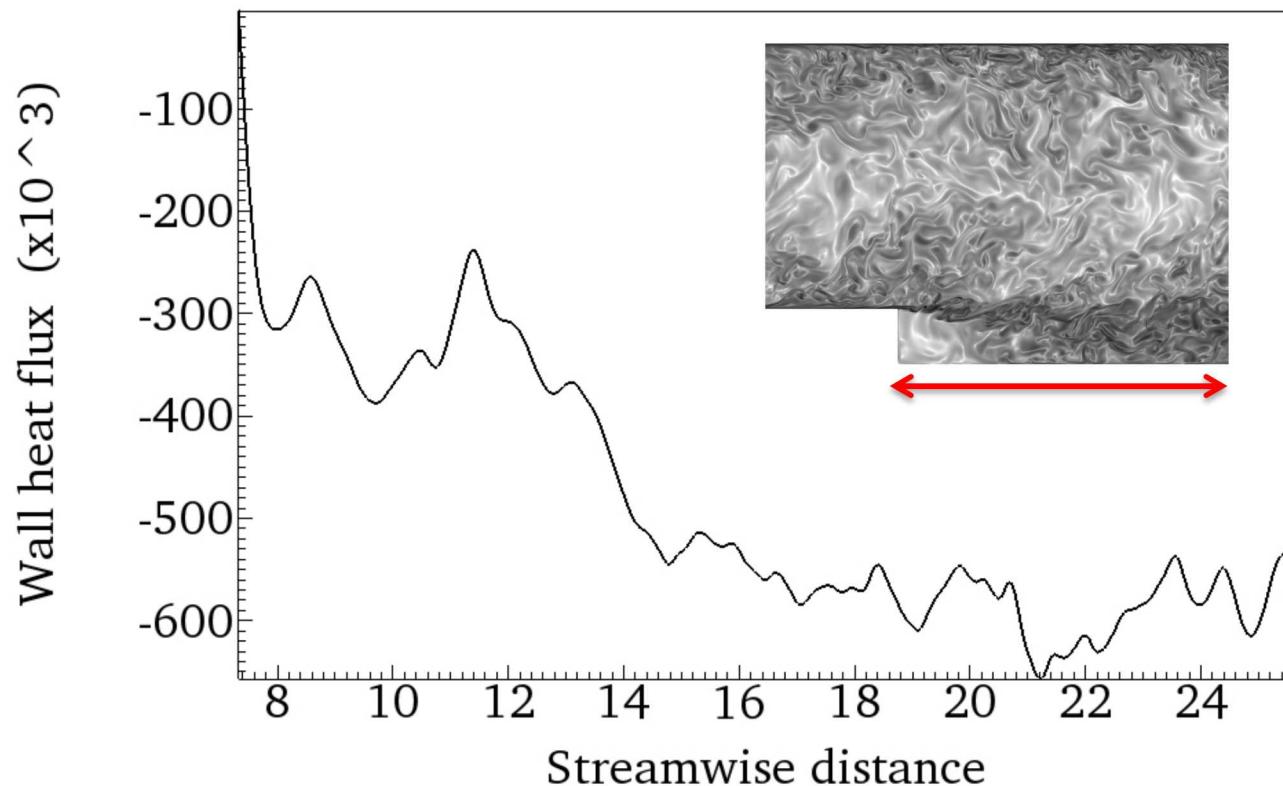
# Enstrophy balance shows advection, vortex stretching and viscous dissipation are dominant

$$\frac{\partial}{\partial t} \left( \frac{\omega^2}{2} \right) + u_i \frac{\partial}{\partial x_i} \left( \frac{\omega^2}{2} \right) = \omega_i \omega_j \frac{\partial u_i}{\partial x_j} - \omega^2 \frac{\partial u_j}{\partial x_j} + \frac{\omega_i}{\rho^2} \epsilon_{ijk} \frac{\partial \rho}{\partial x_j} \frac{\partial P}{\partial x_k} + \omega_i \epsilon_{ijk} \frac{\partial}{\partial x_j} \left( \frac{1}{\rho} \frac{\partial \tau_{kl}}{\partial x_l} \right)$$

Advection      Vortex stretching      Dilatation      Baroclinic torque      Dissipation



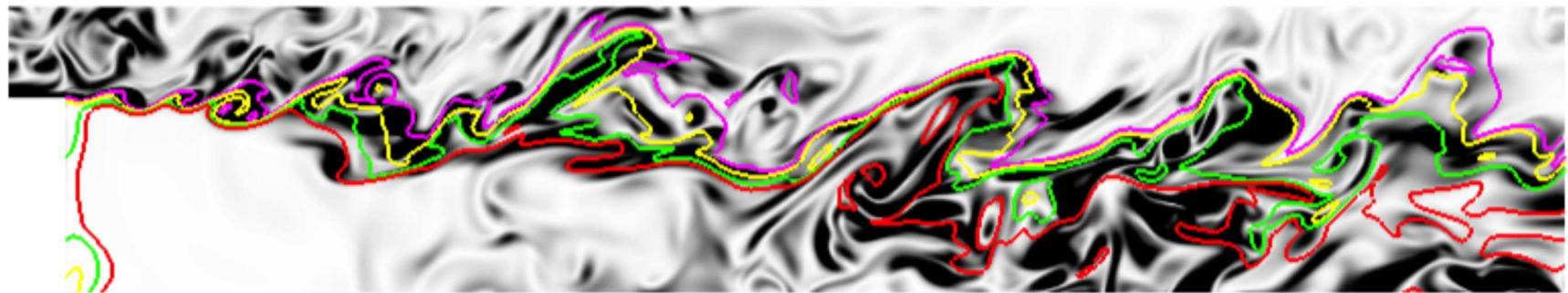
# Increased wall heat flux downstream



# Flame structure

Grey scale: enstrophy

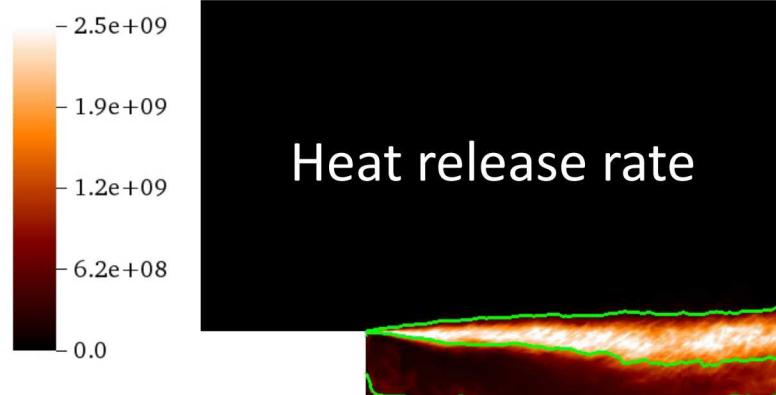
$c = 0.2 \ 0.5 \ 0.8 \ 0.9$



Affects preheat zone

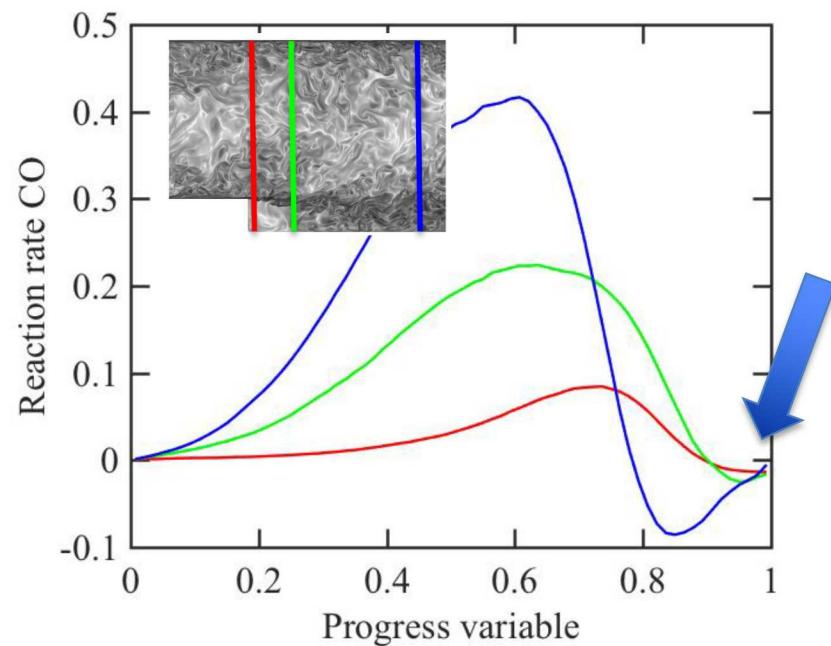
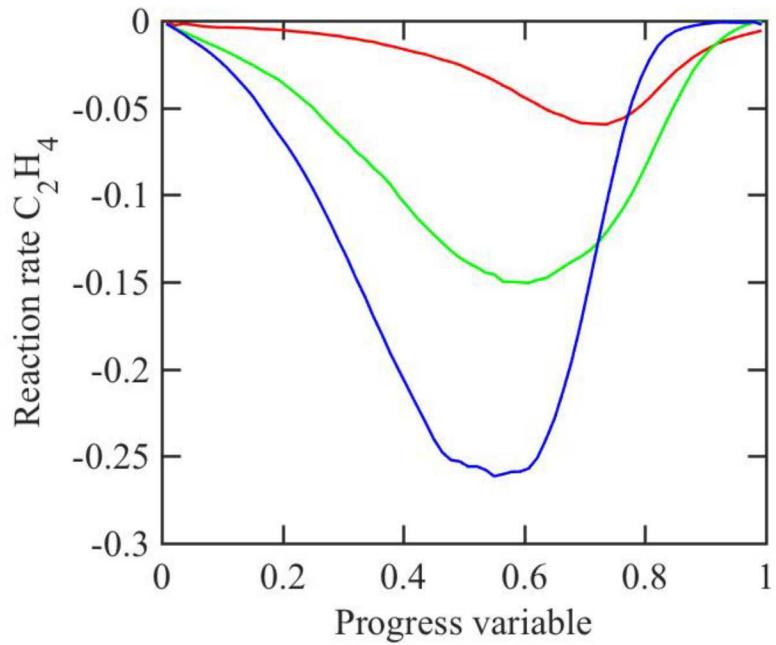
Affects oxidation layer

Flame-flame interaction



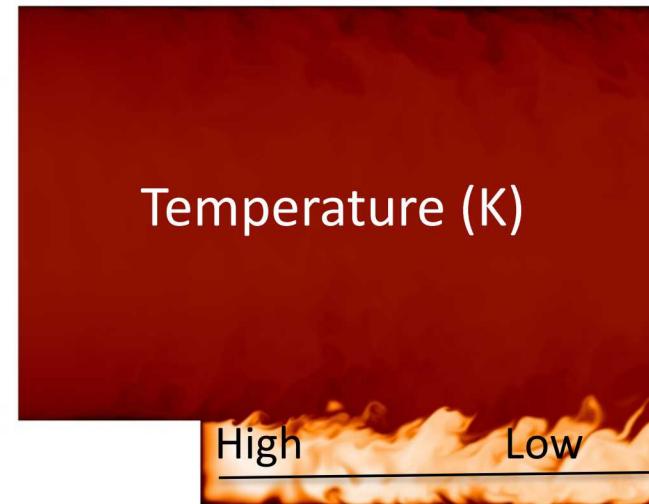
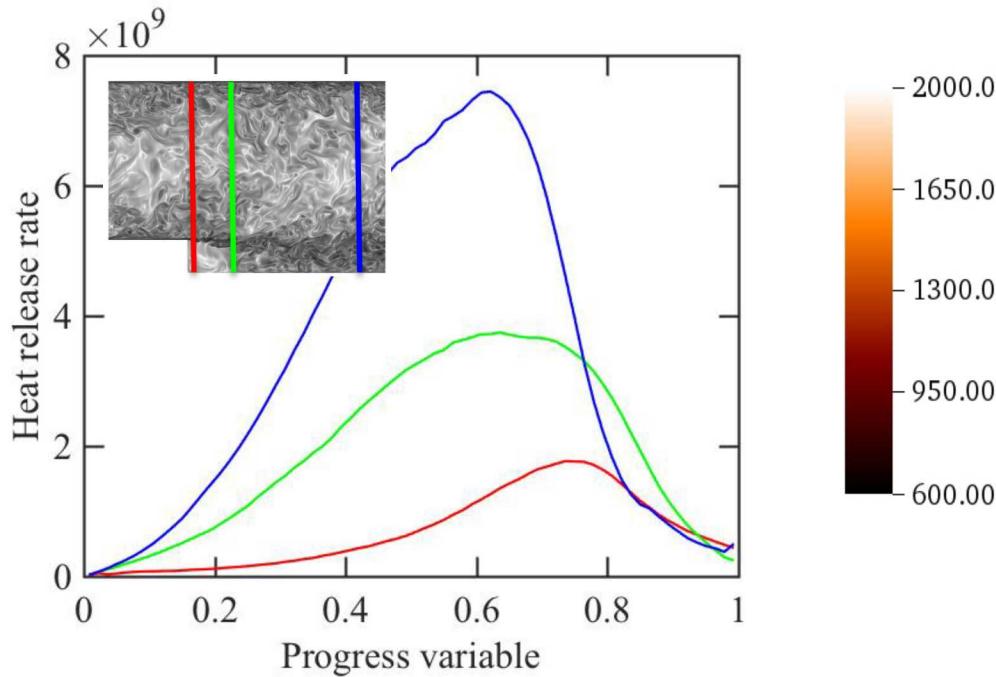
Heat release rate

# Flame structure

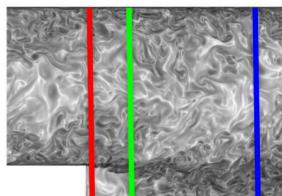


- Due to the high strain rate near the step, fuel is consumed at high progress variable as the flame is pushed into the products (Libby & Williams)
- CO and H<sub>2</sub> consumption quenched near the step

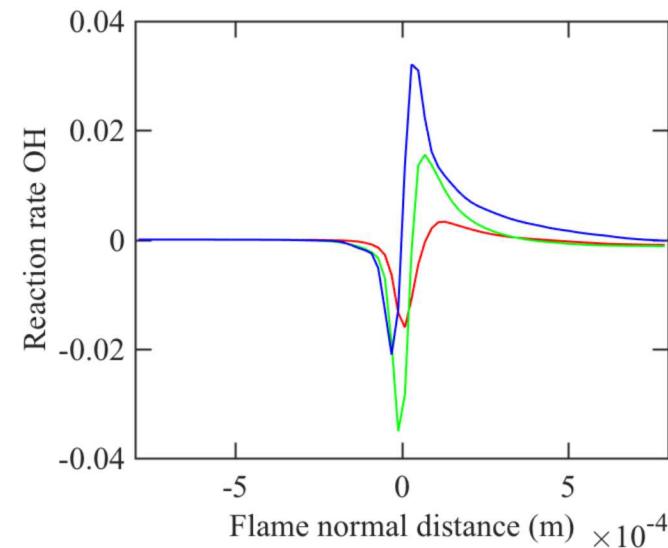
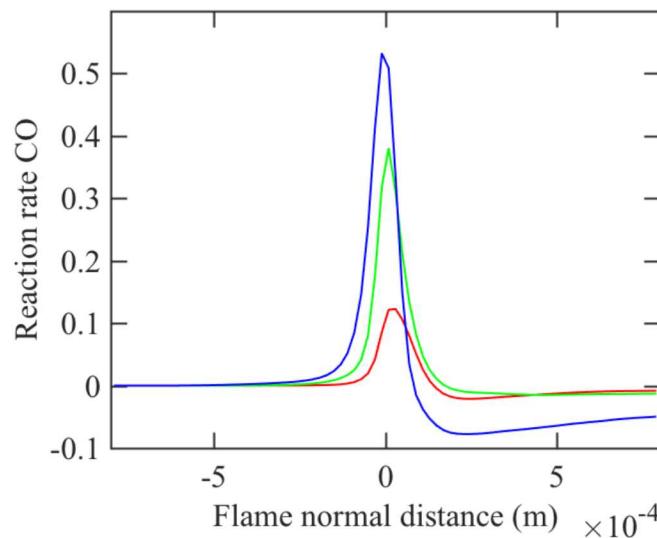
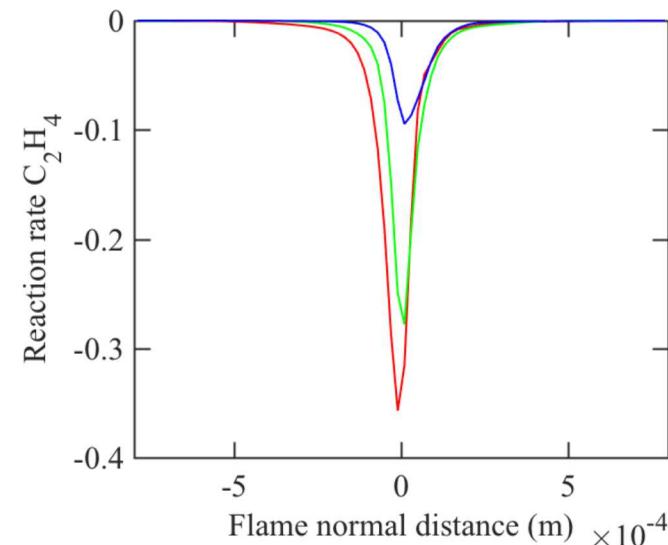
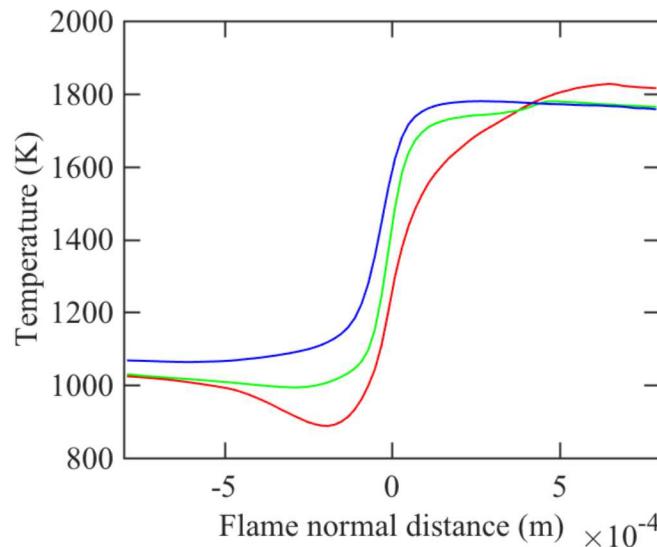
# Flame structure



- Heat release rate increases downstream and occurs at intermediate progress variable
- Temperature decreases downstream, due to enhanced mixing in the products



# Flame normal statistics



# Conclusions

- DNS of C<sub>2</sub>H<sub>4</sub>/air flame stabilization behind a backwards facing step
- Strong interaction between recirculation zone, shear layer, and flame brush
- Radicals from the recirculation zone assist in anchoring the flame
- Turbulence generated near-wall migrates towards products downstream of the stabilization point
- Turbulence affects the flame structure and heat losses to the wall

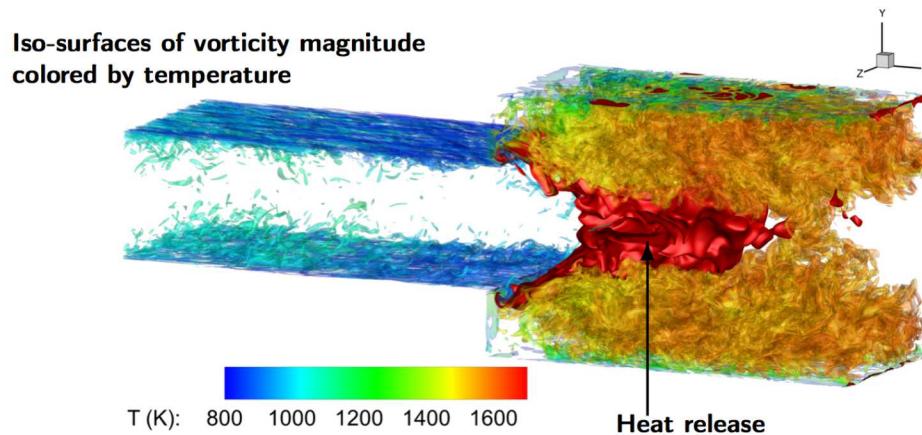
# Direct Numerical Simulation of flame stabilization assisted by auto-ignition at *reheat* conditions

Konduri Aditya<sup>a</sup>, Andrea Gruber<sup>b</sup>, Mirko Bothien<sup>c</sup> and Jacqueline H. Chen<sup>a</sup>

<sup>a</sup>Combustion Research Facility, Sandia National Laboratories, Livermore, CA, USA

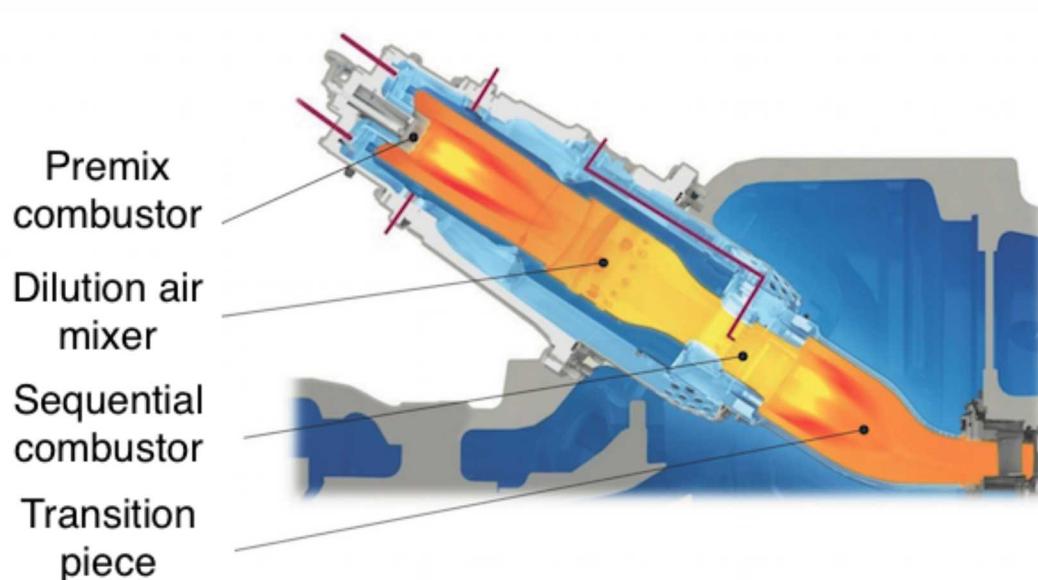
<sup>b</sup>SINTEF Energy Research, Trondheim, Norway

<sup>c</sup>Ansaldo Energia, Baden, Switzerland



Acknowledgements:  
Basic Energy Sciences, Office of Science, DOE  
OLCF, NERSC, Norwegian CCS Research Centre (NCCS)

# Staged gas turbine combustion



- Originally developed by ABB for high efficiency, load flexibility and low emissions
- Recently improved and simplified (reduced cost) for the H-class GT36
- First (premix) combustion stage based on flame propagation
- Second (sequential) combustion stage based on auto-ignition

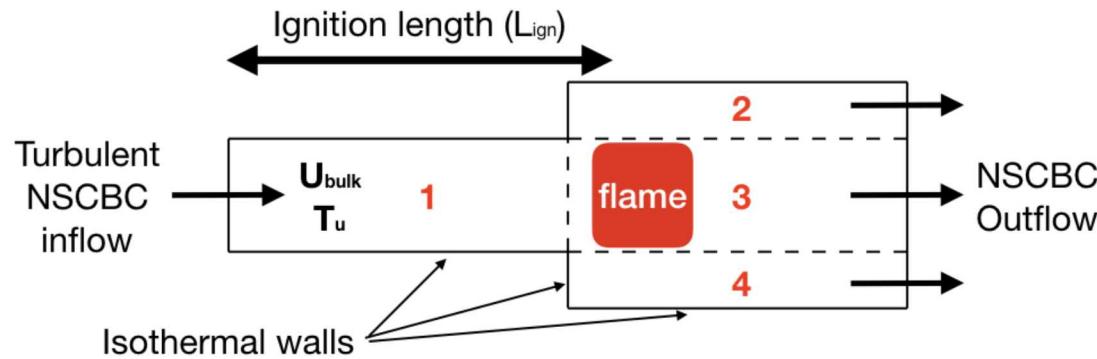
# Reheat burner

DNS of idealized reheat burner configuration from Ansaldo Energia  
Operating conditions:

- Inlet temperature:  $\sim 1100$  K
- Pressure:  $\sim 20$  atm

Scaled conditions:

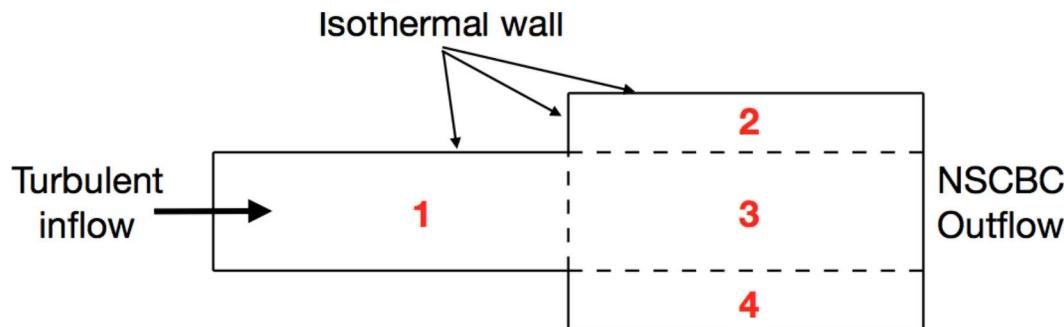
- Mean inlet temperature:
- Pressure: 1 atm
- Fuel: hydrogen



Objective:

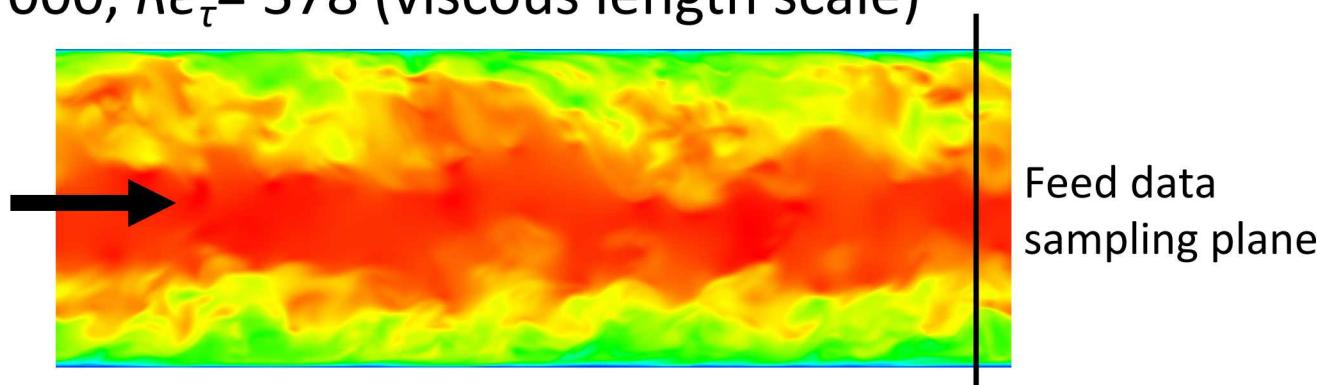
- Understand the flame stabilization
- Identify the modes of combustion
- Quantify the role of autoignition

# Simulation details



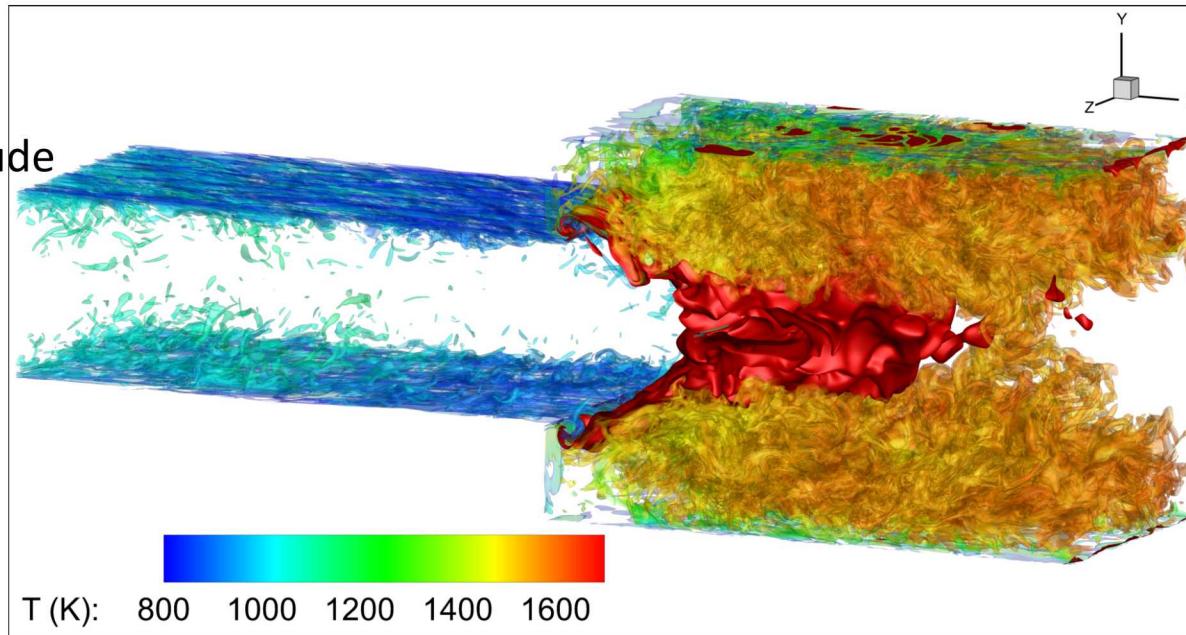
1.25 billion grid points  
20 million CPU hours  
 $Re_b = 13000$

- **Chemical mechanism:** 9 species hydrogen-air (Li et al., 2004)
- **Inflow composition:** premixed  $H_2 + O_2 + N_2 + H_2O$  ( $\phi = 0.35$ )
- $U_{bulk} = 200\text{m/s}$ ,  $u' = 20\text{m/s}$ ,  $T_{inlet} = 1100\text{K}$ ,  $T_{wall} = 750\text{K}$
- **Inflow profile:** feed from DNS of a fully developed channel flow,  $Re_b \sim 13,000$ ,  $Re_\tau = 378$  (viscous length scale)



# Enstrophy conditioned on temperature, and heat release rate (red)

Iso-surfaces of vorticity magnitude colored by temperature

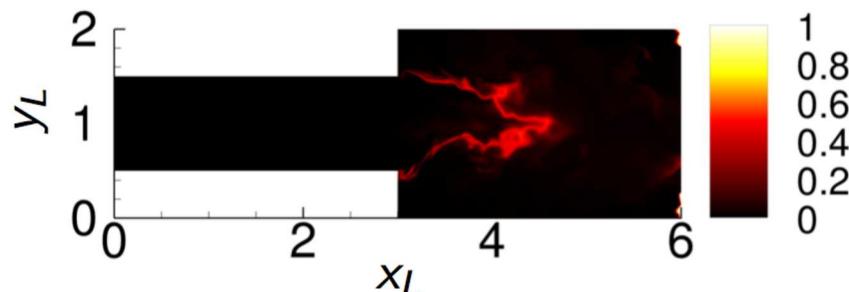


Two combustion configurations are observed:

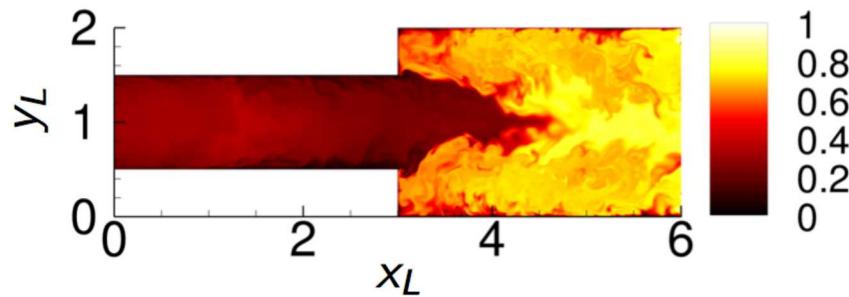
- Design state: mainly auto-ignition in the combustion chamber
- Intermittent auto-ignition state: ignition in mixing section

# Design combustion state

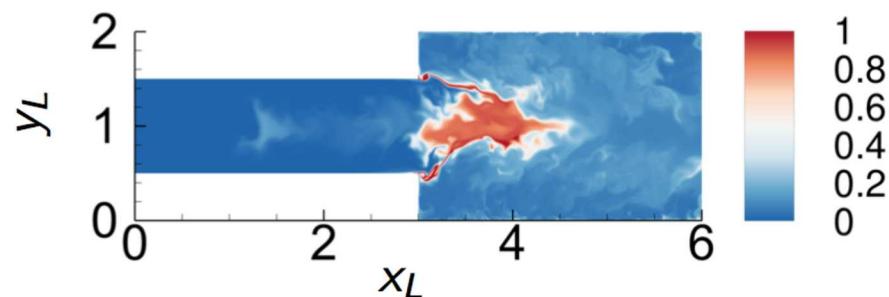
Heat release rate



Temperature



Mass fraction of  $HO_2$



Combustion modes:

- Autoignition along center-line
- Flame propagation near corners
- $HO_2$ : indicative of chain branching

# Combustion mode: OH budget analysis

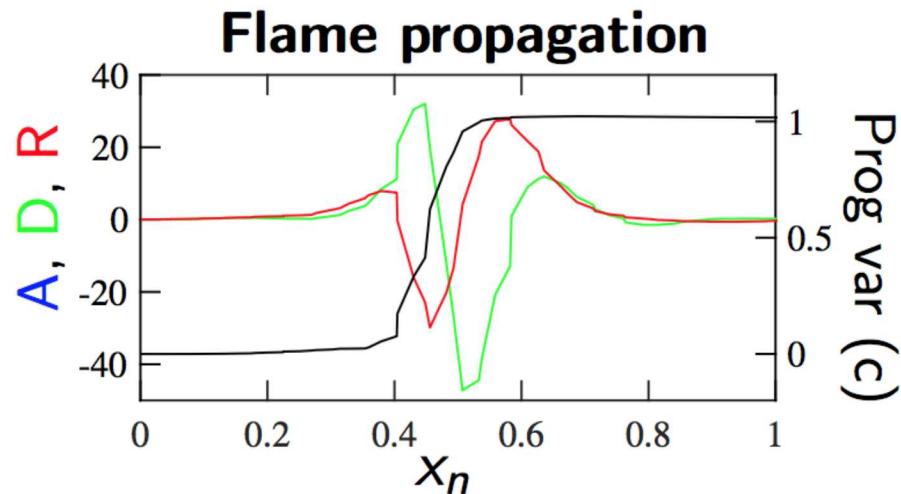
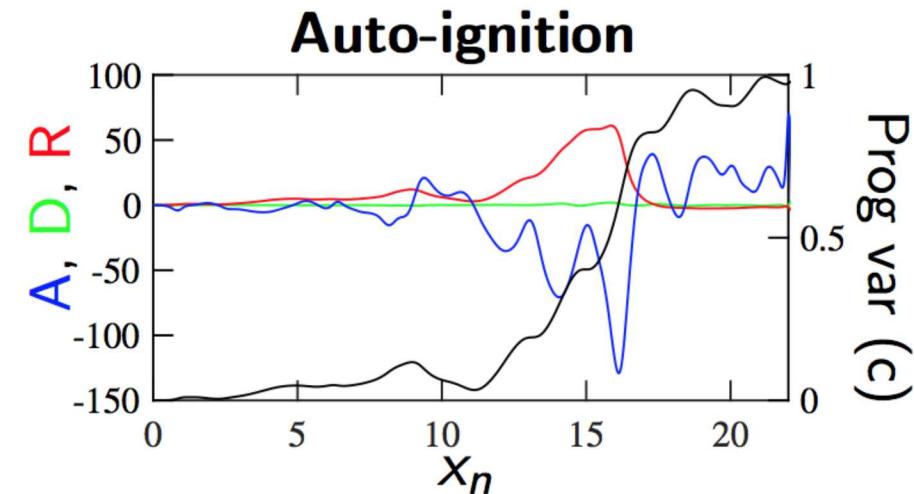
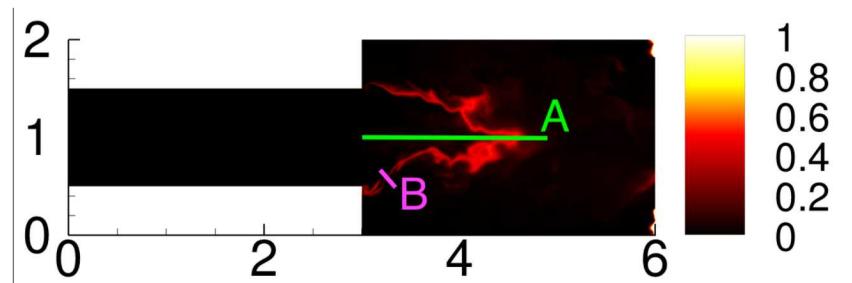
$$\frac{\partial(\rho Y_{OH})}{\partial t} = -\nabla_\beta \cdot (\rho Y_{OH} \mathbf{u}_\beta) - \nabla_\beta \cdot (\rho Y_{OH} \mathbf{v}_{\beta, OH}) + W_{OH} \dot{\omega}_{OH}$$

Advection

Diffusion

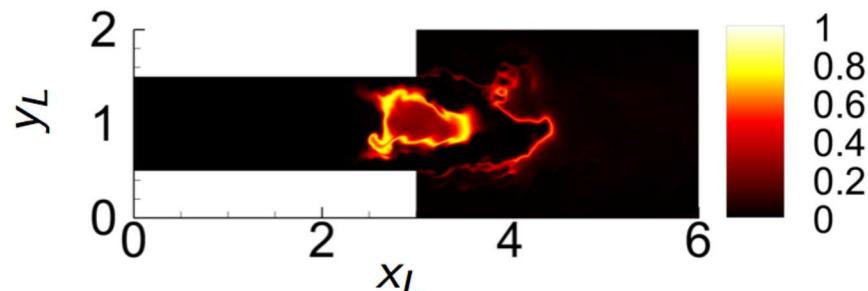
Reaction

- Auto-ignition: balance between **advection** and **reaction**
- Flame propagation: balance between **diffusion** and **reaction**



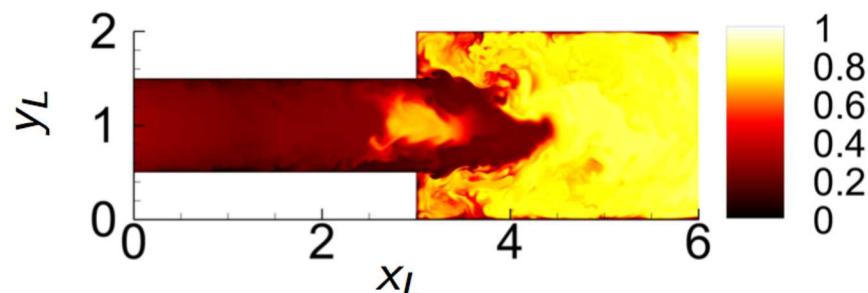
# Intermittent auto-ignition state

Heat release rate

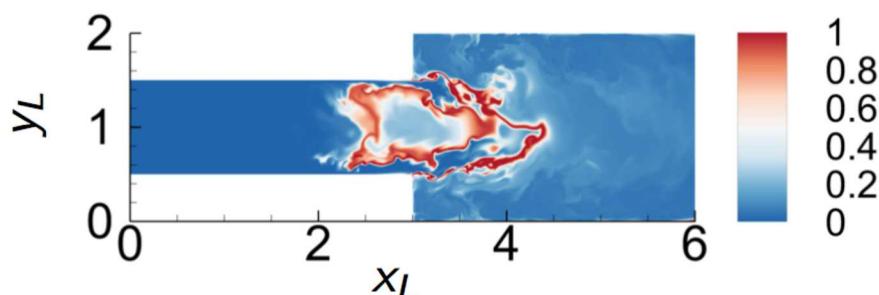


- Early auto-ignition in the mixing section
- Ignition kernel advects downstream
- Occurs intermittently

Temperature



Mass fraction of  $HO_2$

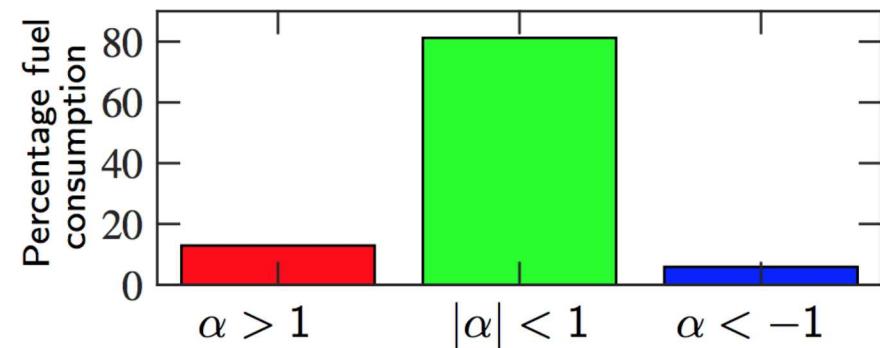
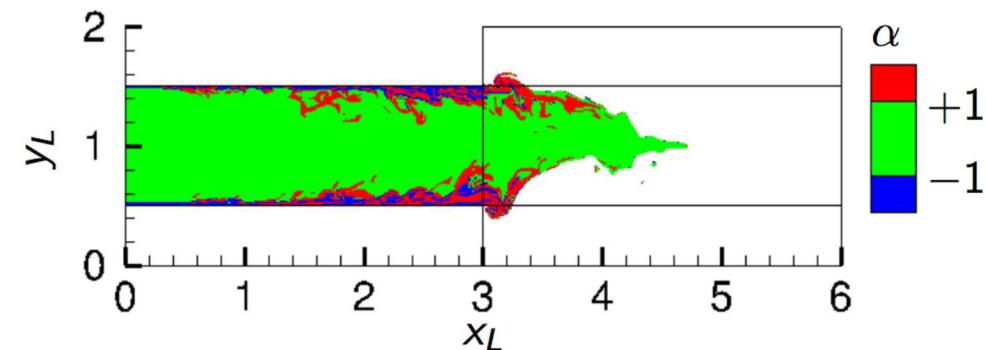


# Chemical Explosive Mode Analysis

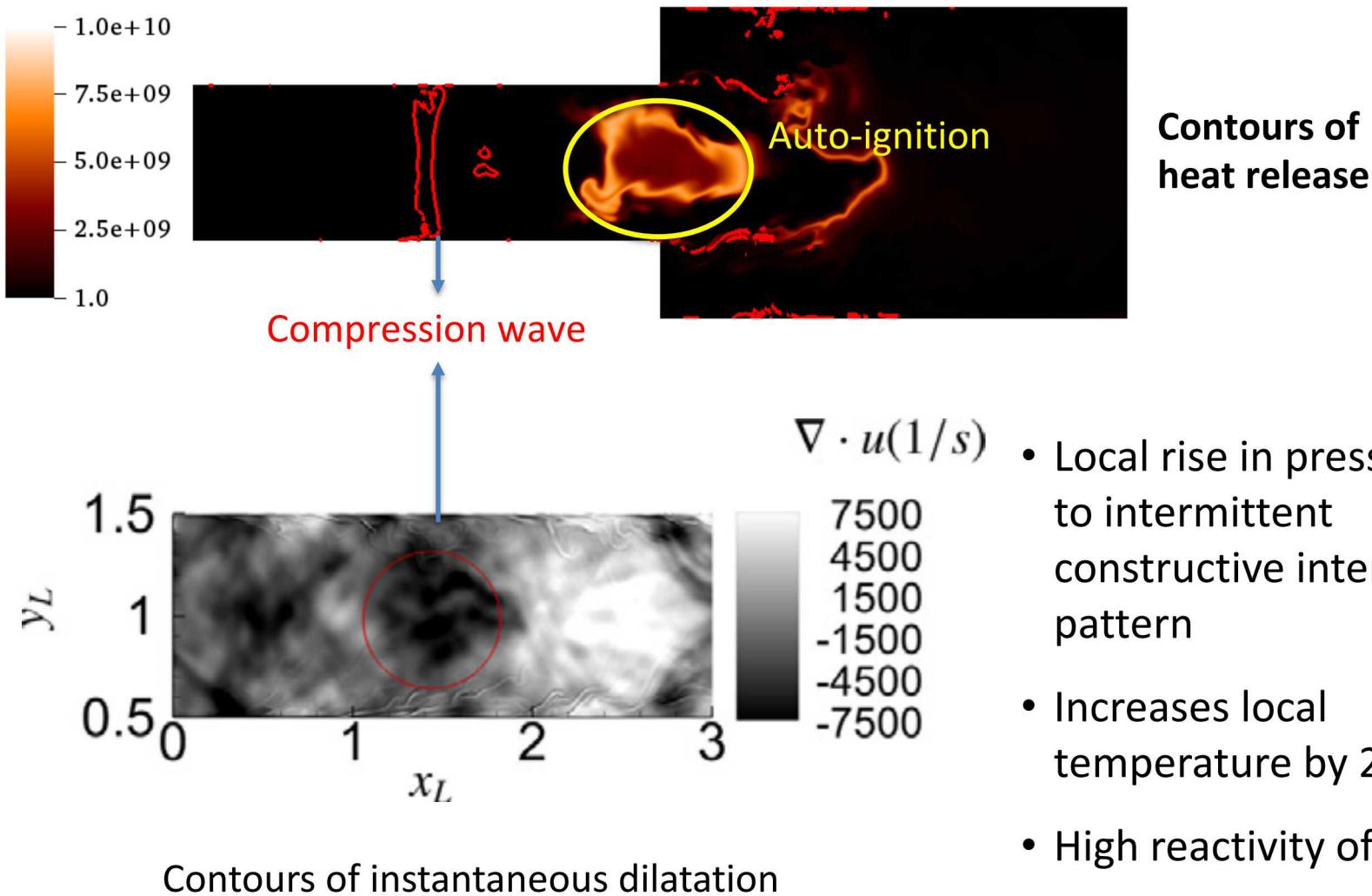
- $\alpha = \phi_s / \phi_\omega$  : ratio of the projected non-chemical source term and the projected chemical source term (C. Xu et al., PROCI 2018 )

Three mode are identified:

- **Assisted-ignition ( $\alpha > 1$ )**: diffusion significantly promotes reaction
- **Auto-ignition ( $-1 < \alpha < 1$ )**: chemistry plays a dominant role
- **Extinction zone ( $\alpha < -1$ )**: diffusion dominates chemistry and suppresses ignition



# Intermittent auto-ignition state



- Local rise in pressure due to intermittent constructive interference pattern
- Increases local temperature by 20-30 K
- High reactivity of hydrogen
- Decrease in ignition delay time (30%)

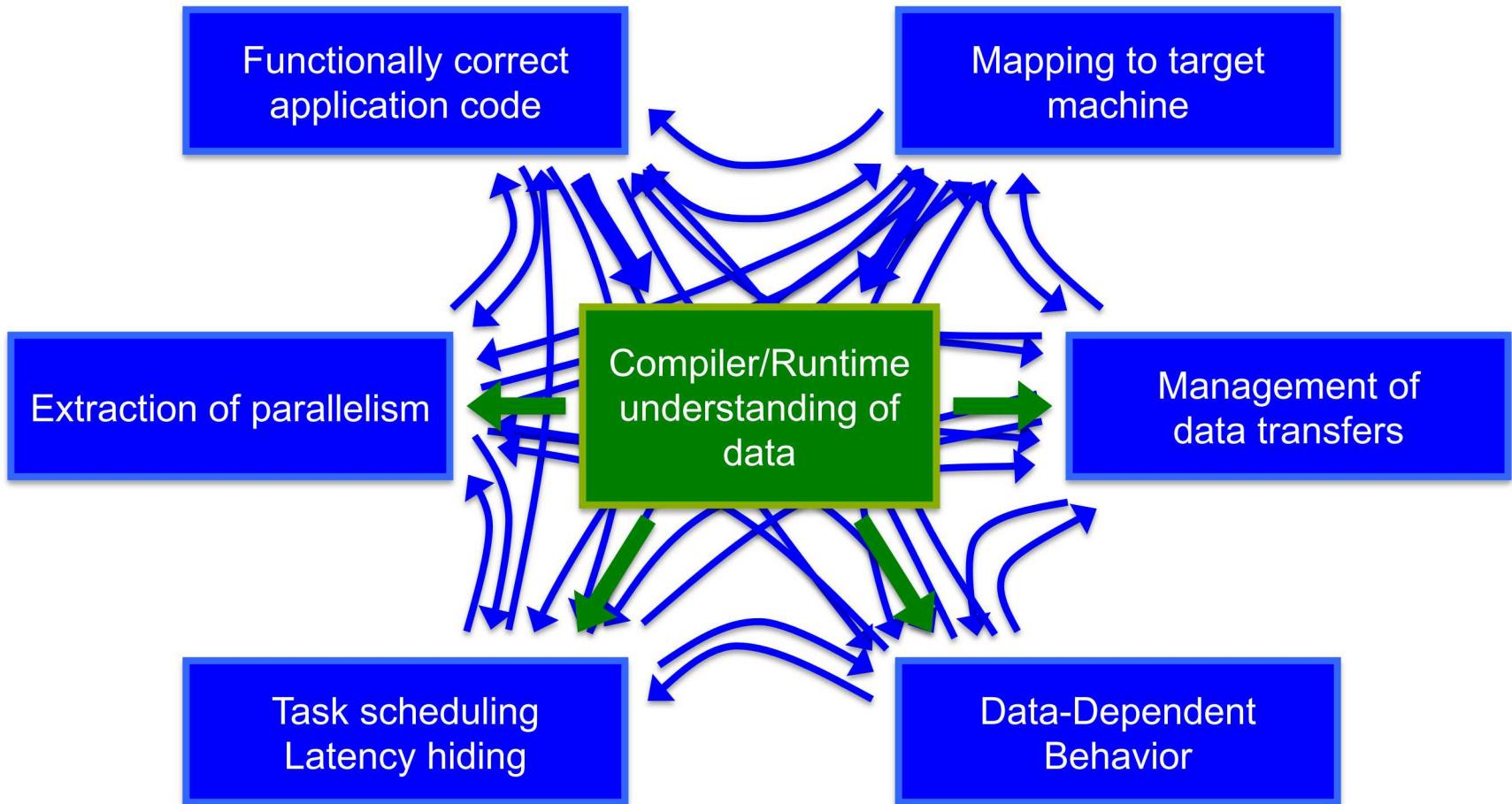
# Conclusions

- Performed DNS of a reheat burner at scaled conditions
- Two states of hydrogen/air combustion have been observed:
  - design state: flame propagation and auto-ignition in the combustor
  - intermittent auto-ignition in mixing section
- Premature auto-ignition arises due to pressure (and following temperature) rise in mixing section
- Quantified the contribution of different modes towards heat release using chemically explosive mode analysis (CEMA)
- Future work:
  - characterize the unstable flame behavior and the conditions leading to it
  - find the inlet conditions for statistically stationary reheat flame
  - perform 2D and 3D simulations with varying fuel composition and its stratification

# Parallel Programming 101 - Productivity

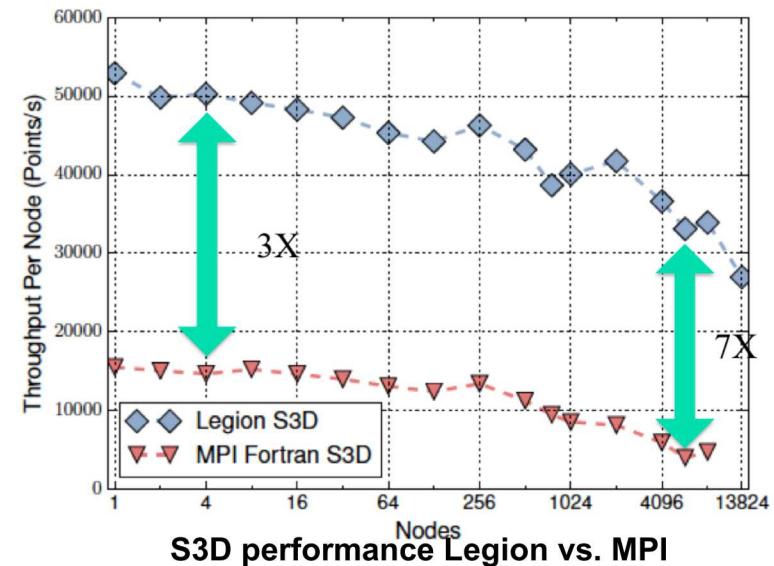
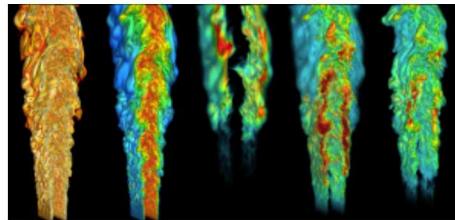


# Parallel Programming 101



# Legion Programming System applied to S3D

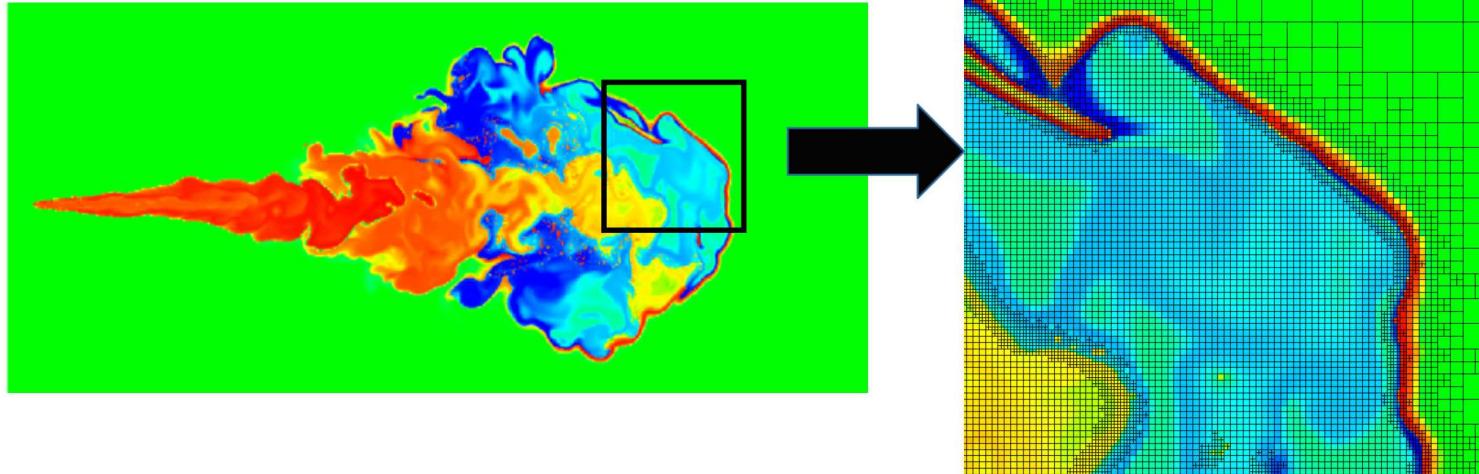
- A data-centric parallel programming system
- A programming model for **heterogeneous, distributed machines**
  - Automates many aspects of achieving high performance, such as extracting task- and data-level parallelism
  - Automates details of scheduling tasks and data movement (*performance optimization*)
  - Separates the specification of tasks and data from the mapping onto a machine (*performance portability*)
- Legion application example: S3D
  - Production combustion simulation
  - Written in ~200K lines of Fortran
  - Direct numerical simulation using explicit methods



*S. Treichler et al., “S3D-Legion: An Exascale Software for Direct Numerical Simulation (DNS) of Turbulent Combustion with Complex Multicomponent Chemistry,” CRC Book on Exascale Scientific Applications: Programming Approaches for Scalability Performance and Portability, 2017.*

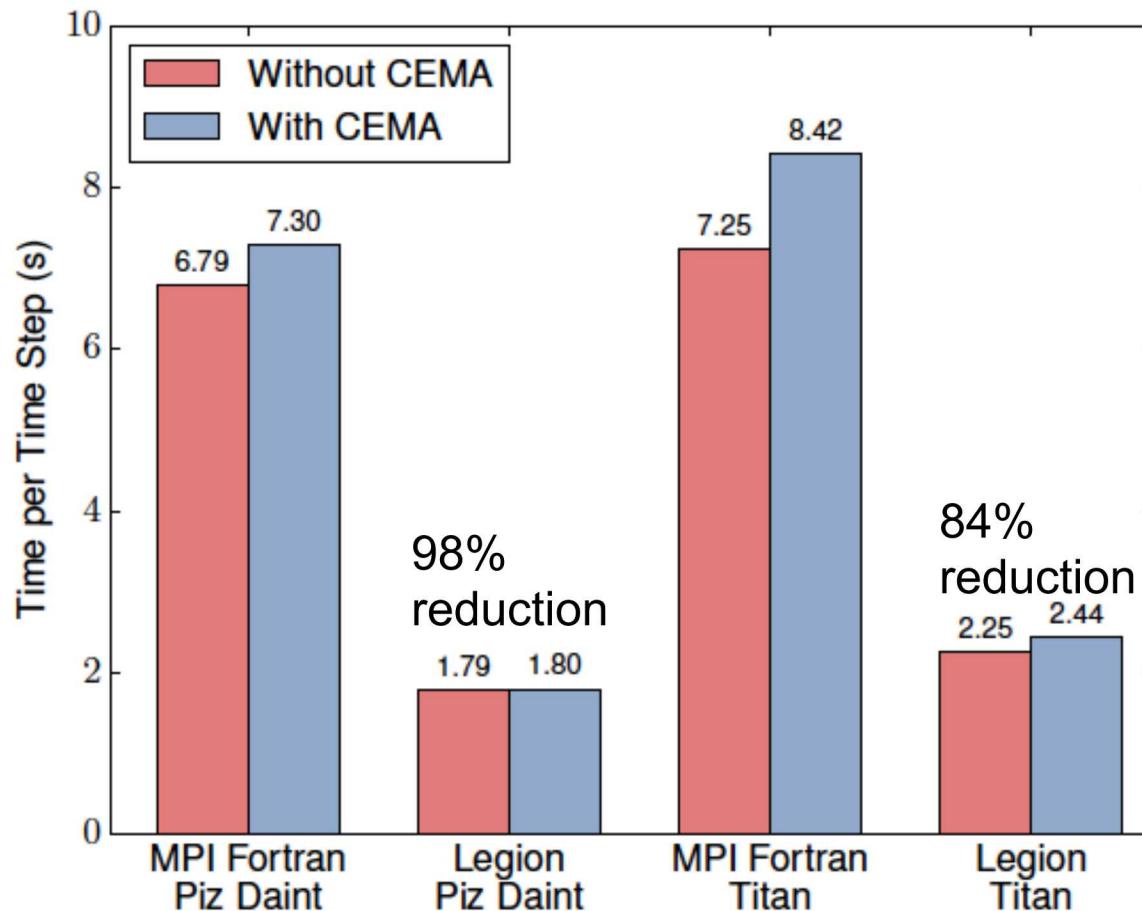
# In-situ Data Analytics in Legion Chemical Explosive Mode Analytics (CEMA)

- CEMA: eigenvalue solve on the reaction rate Jacobian to determine the mode of combustion



- Run CEMA at each time step as a diagnostic to steer mesh refinement
- CEMA computation takes longer than a single explicit RK stage (6 stages/timestep)
- Dividing CEMA across RK stages and interleaving with other computation so as not to impact other critical operations would be hard to schedule manually
- Asynchronous task execution, schedule CEMA on CPU resources
- Interoperate Fortran CEMA with Legion code – took a day to implement

# Execution Overhead of In-situ Analytics (CEMA) in S3D-Legion (Titan & Piz Daint)



# Legion S3D Lessons Learned

- **Legion**
  - S3D shows potential of data-centric, task-based models
  - Enables new simulation capabilities (physics, and in situ analytics)
  - Code is easier to modify and maintain
    - Ports are just new mappings, easy to tune for performance
    - New functionality usually just means new tasks
    - Legion will figure out the dependences and scheduling
    - Productivity requires higher level abstraction layer for scientists to write in
- **Co-Design and ECP**
  - The Legion/S3D experience is a tribute to co-design
  - Computer and computational scientists worked closely
  - Major progress on important problems resulted

# Exascale Targets: Science at Relevant Conditions

- **Hybrid DNS/LES (near DNS) with dynamic adaptive mesh refinement, multi-physics (sprays, soot, radiation at high pressure) in geometry**
- **Reactivity Stratified Compression Ignition IC Engines** - multi-stage, high pressure autoignition of a liquid hydrocarbon fuel blend
- **Natural Gas IC Engines – ignition and knock**
- **Scramjets** – cavity stabilized shear driven lean turbulent premixed flames, effect of products recirculation coupled with high  $Re$ , high  $Ka$ , compressible flames
- **Gas Turbines** – swirl stabilized spray combustion gas turbines with lean premixed combustion, flame stabilization, nitric oxide emissions, thermo-acoustics
- **Include in-situ analytics & visualization**

