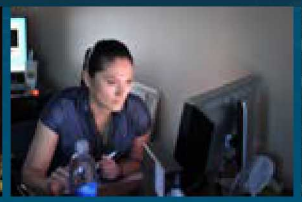
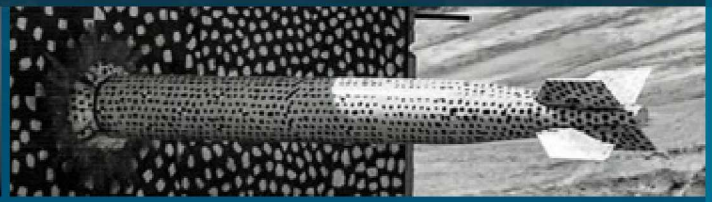
This paper describes objective technical results and analysis. Any subjective views or opinions that might be expressed in the paper do not necessarily represent the views of the U.S. Department of Energy or the United States Government.

SAND2019-5308C

Sandia National Laboratories

Atmospheric Flow Validation for Contaminant Transport





PRESENTED BY

Blake W. Lance, Alexander L. Brown, Kevin J. Dowding, Michael D. Clemenson, Sandia National Labs

Chris Elkins, Stanford University

Michael Benson, United States Military Academy

ASME Verification and Validation Symposium, Las Vegas, NV, May 15-17, 2019

Stanford University

SAND2019-XXXXX

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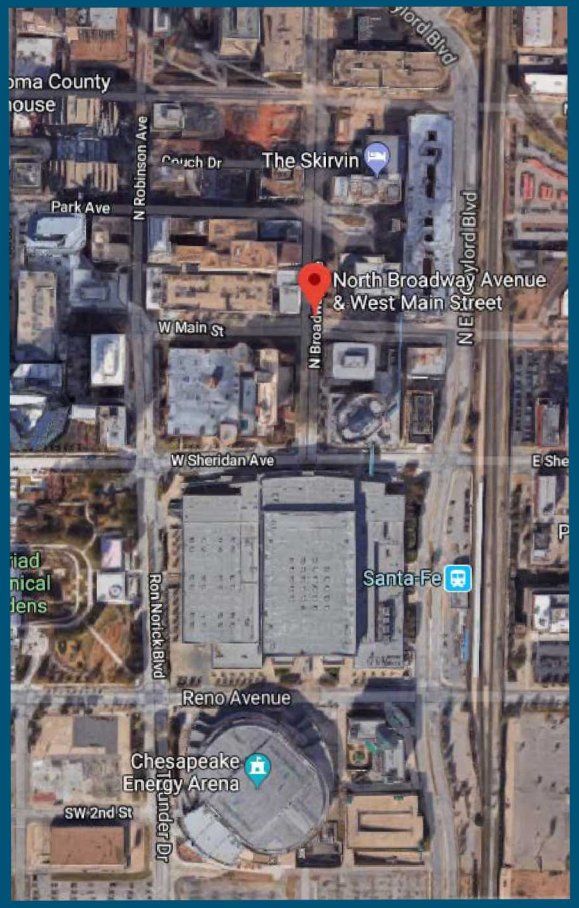
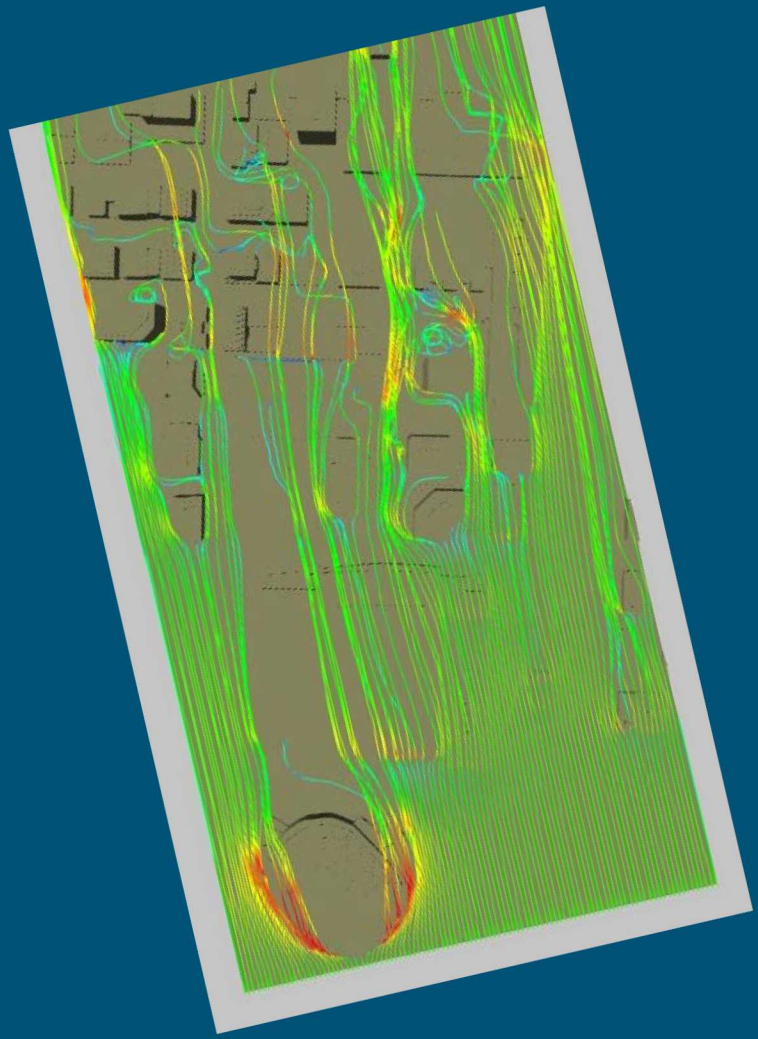
Atmospheric flow with contaminant transport is a challenging simulation problem

- Large length scales required
- Complex geometry with separated flow
- Little/sparse validation data available



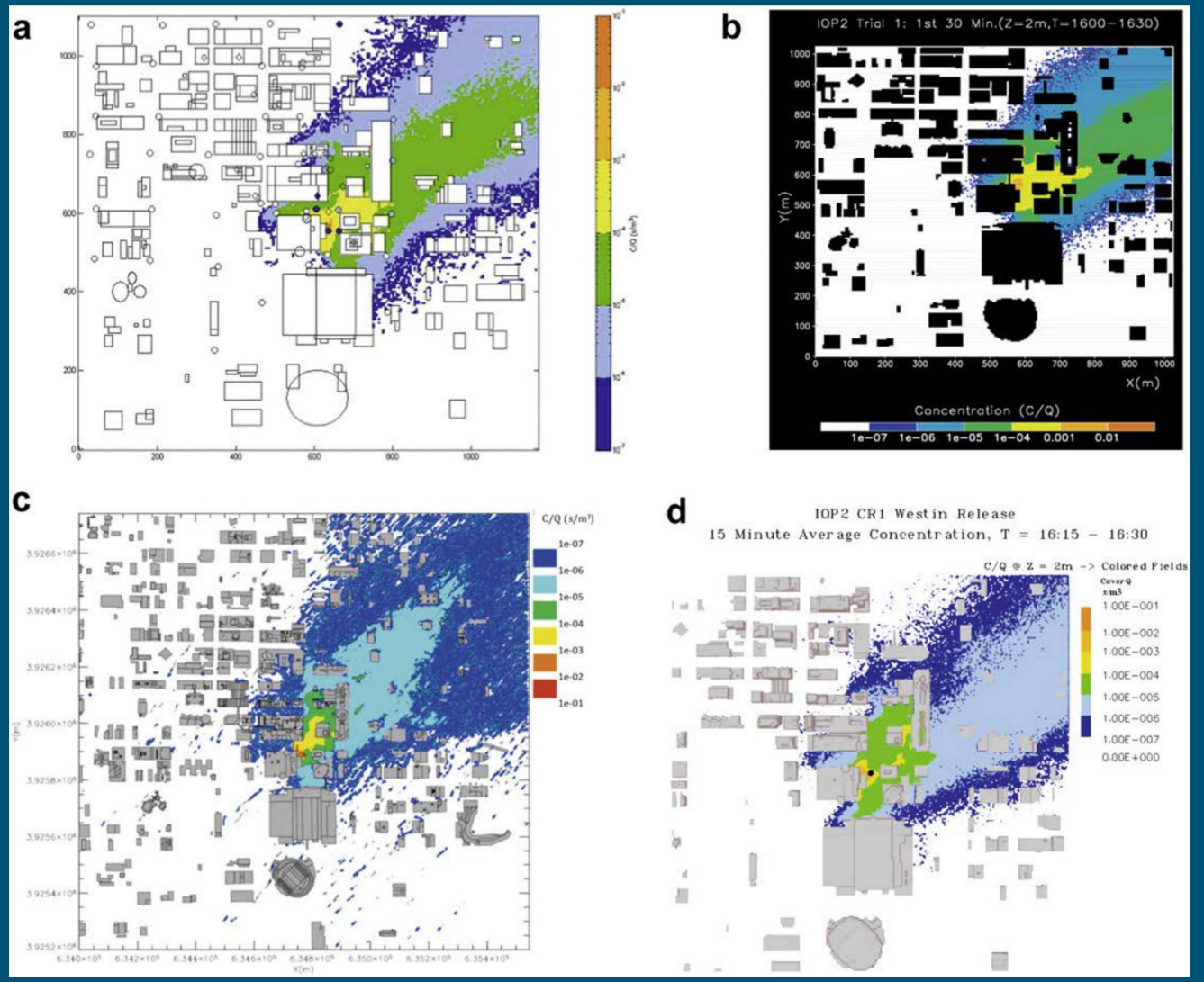


Oklahoma City Downtown Area – Result on right rotated for geometric alignment

Many dispersion approximation models have been used previously

- a – QUIC by Los Alamos National Laboratory
- b – 3DWF by Army Research Laboratory
- c – Urban Lagrangian Model by Israel Institute for Biological Research
- d – MSS by Aria Technologies and SAIC

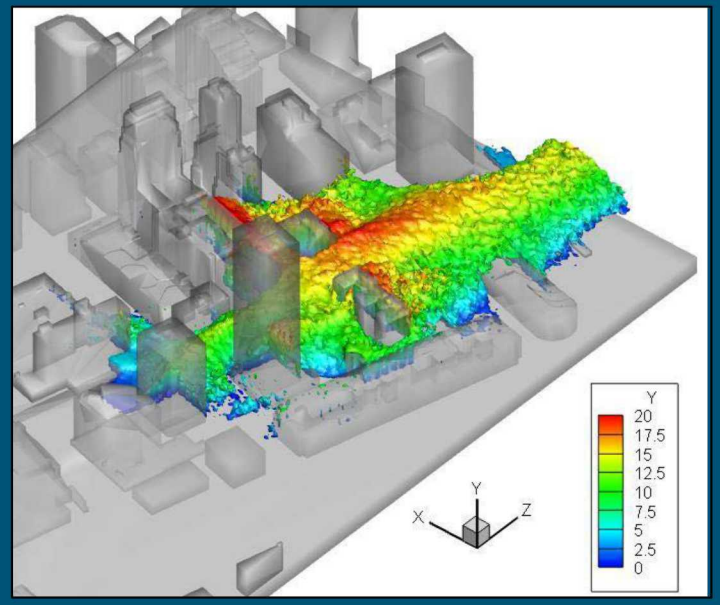
- Computational Fluid Dynamics (CFD) has higher fidelity and is likely to be more accurate

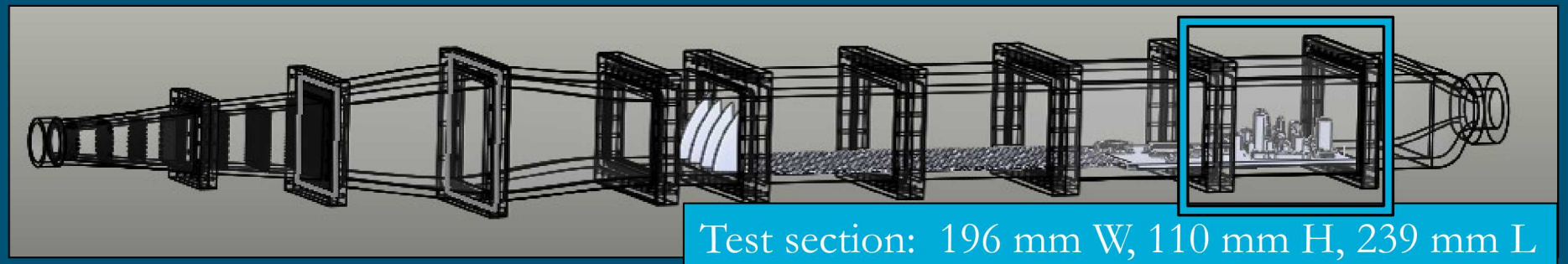


Hanna2011 - Comparisons of JU2003 observations with four diagnostic urban wind flow and Lagrangian particle dispersion models

Scaled validation data were measured in a medical MRI machine

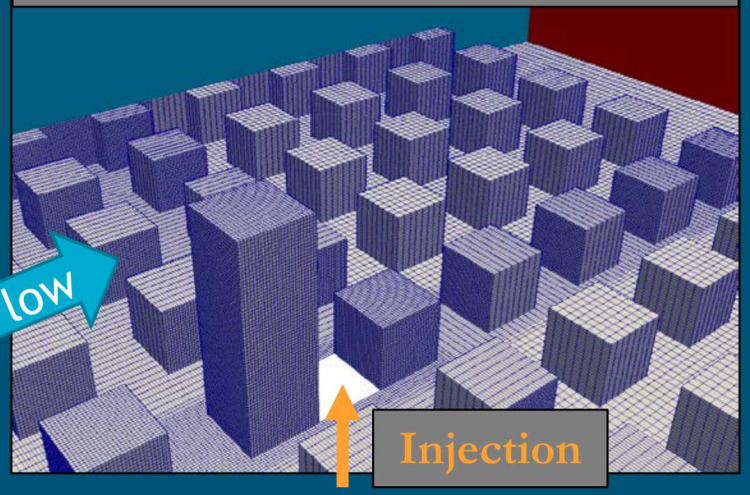
- Experiments conducted at Stanford
- Methods
  - Magnetic Resonance Velocimetry
  - Magnetic Resonance Concentration
- $CuSO_4$ tracer in water
- Full 3D data, $\mathrm{Re}_{D_H} = 36{,}000$
- Time-averaged over 60-90 minutes
- 0.8 mm resolution, 13.4 million voxels
- U_{velocity} = 4% of measured value
- $U_{\text{concentration}}$ = 5.5% of measured value
- U_{space} = 0.4 mm (1/2 voxel)



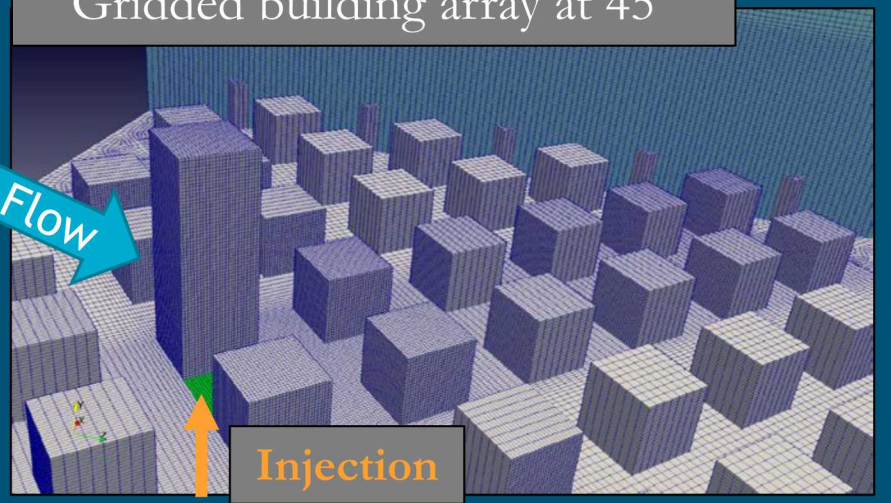


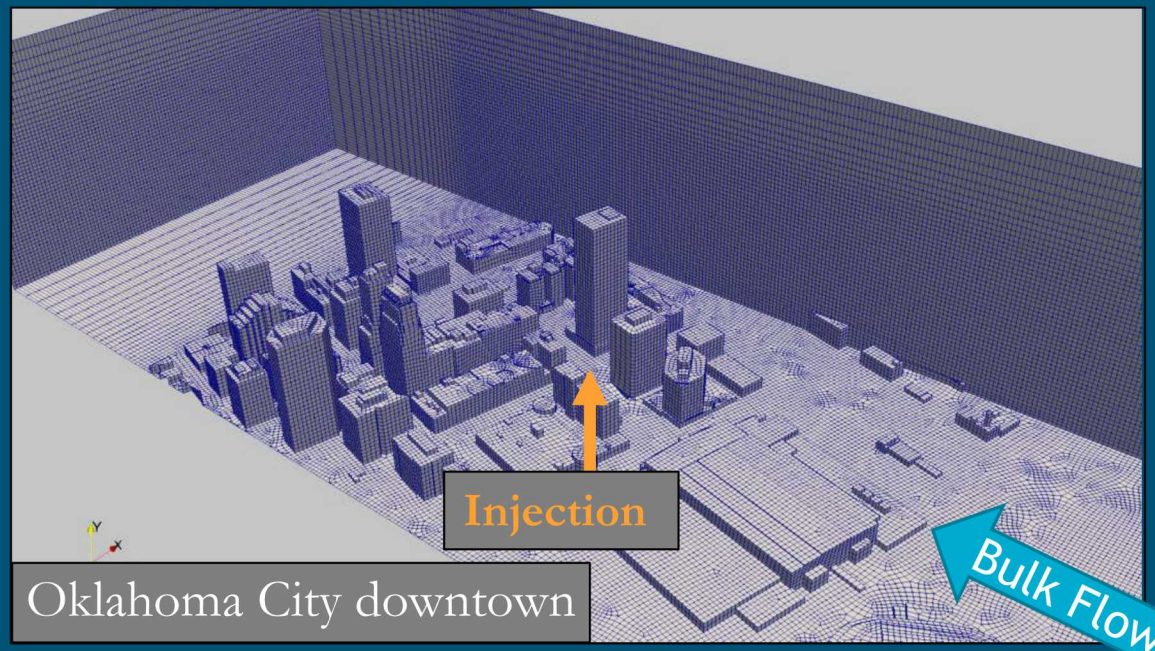
This program has investigated three urban geometries

Gridded building array at 90°

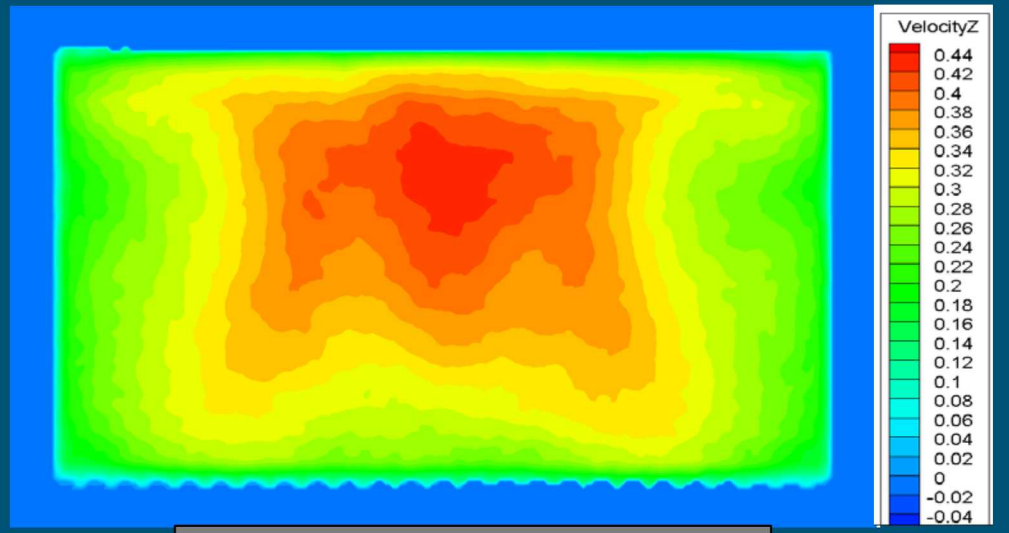


Gridded building array at 45°





Oklahoma City downtown



Measured inflow example

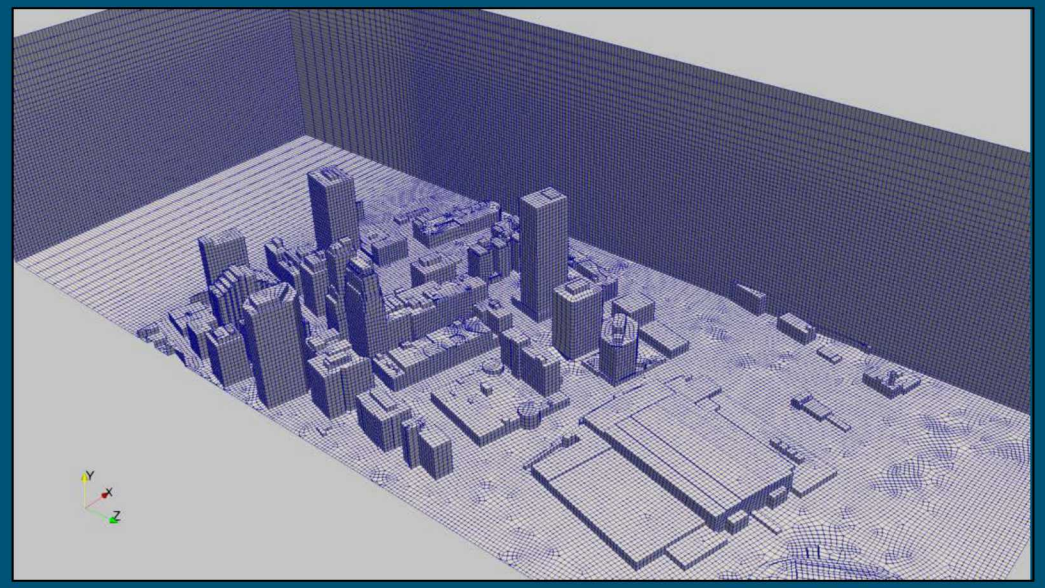
Three models were used and compared

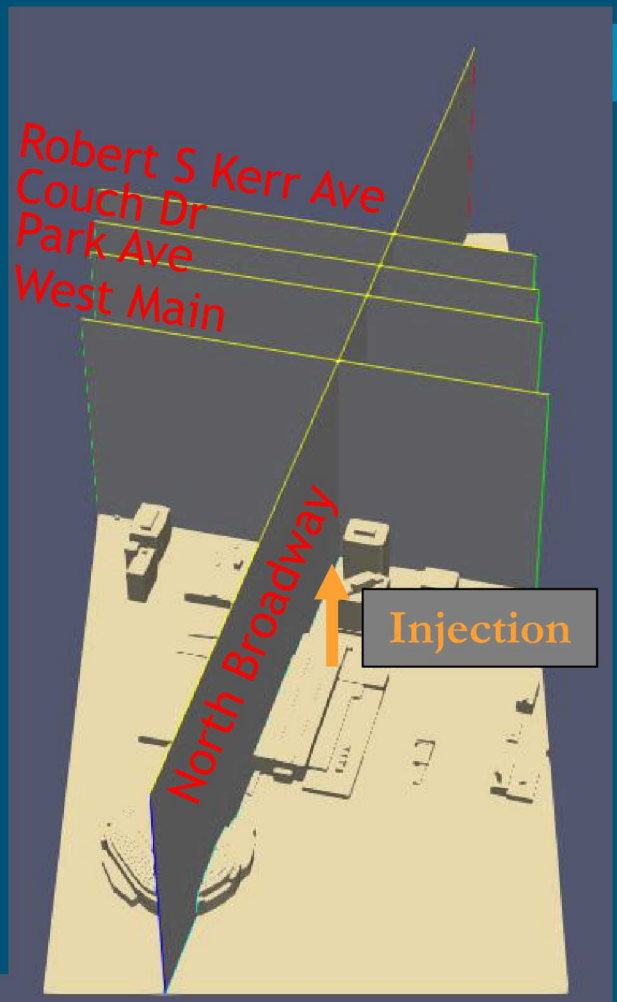
- Large Eddy Simulation (LES) subgrid scale kinetic energy (KSGS) (Kim and Menon, 1997)
- Time-filtered Navier-Stokes (TFNS)
- $k - \epsilon$ RANS model

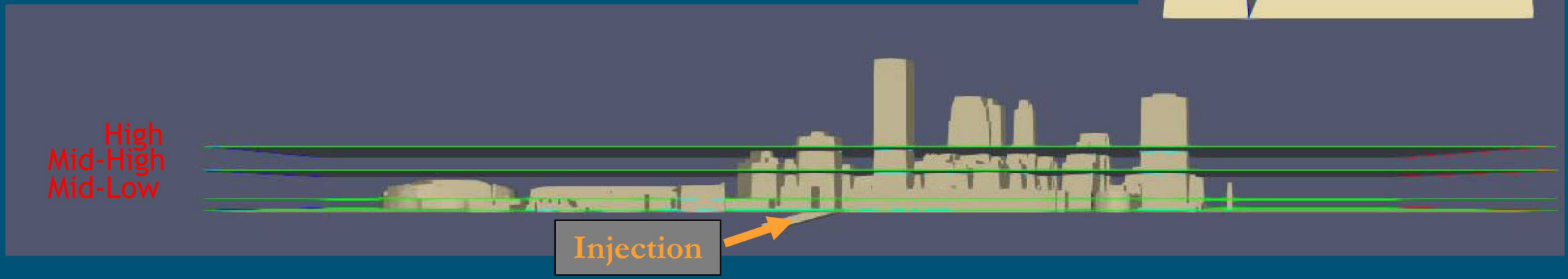
LES prediction for 90° case shows large separation area downstream of tall building

This work details the Oklahoma City case

- Real urban environment
- Reliable validation data
- Best practices on grid refinement setup
- 1:2500 scale



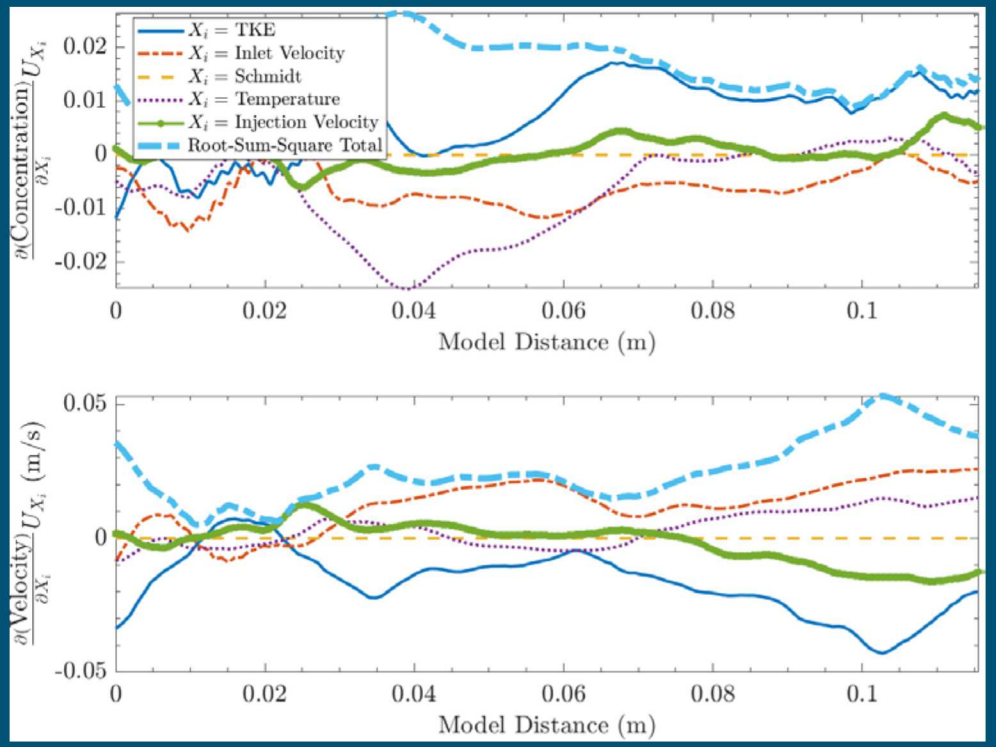




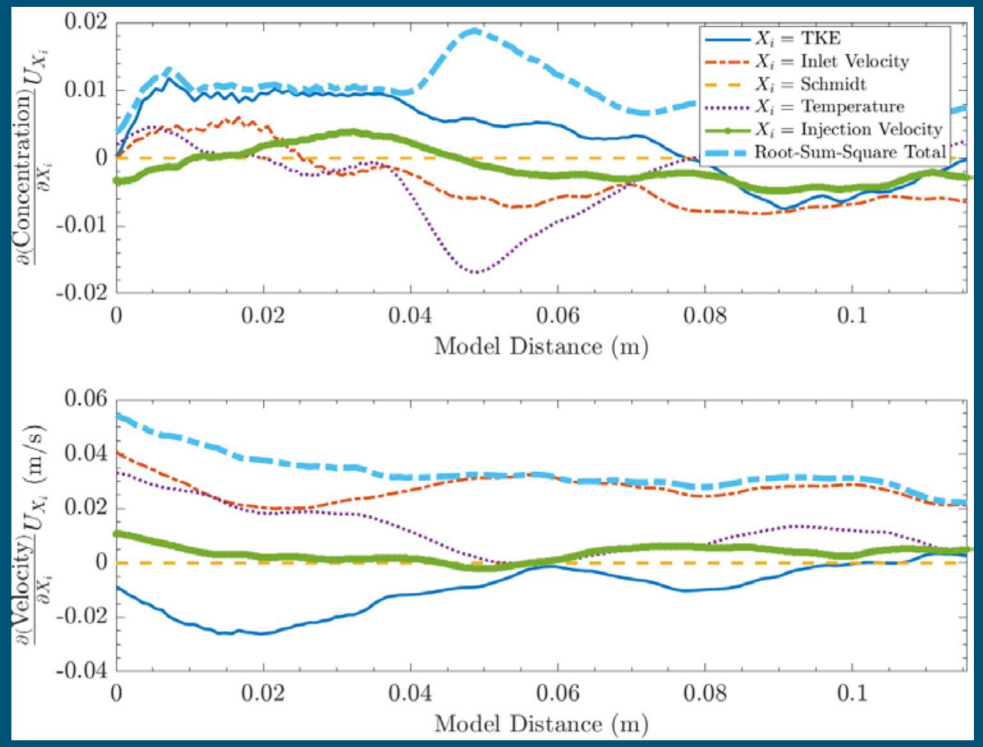
A parameter study was performed with five parameters

Parameter	Baseline	Variation
Turbulent kinetic energy	0%	+10%
Inlet velocity	Measured	±5%
Schmidt number	0.9	±0.2
Temperature	21°C	±25%
Injection velocity	22.5 cm/s	±10%

- Concentration was sensitive to TKE
- Velocity was most sensitive to inlet velocity



North Broadway-Medium Low

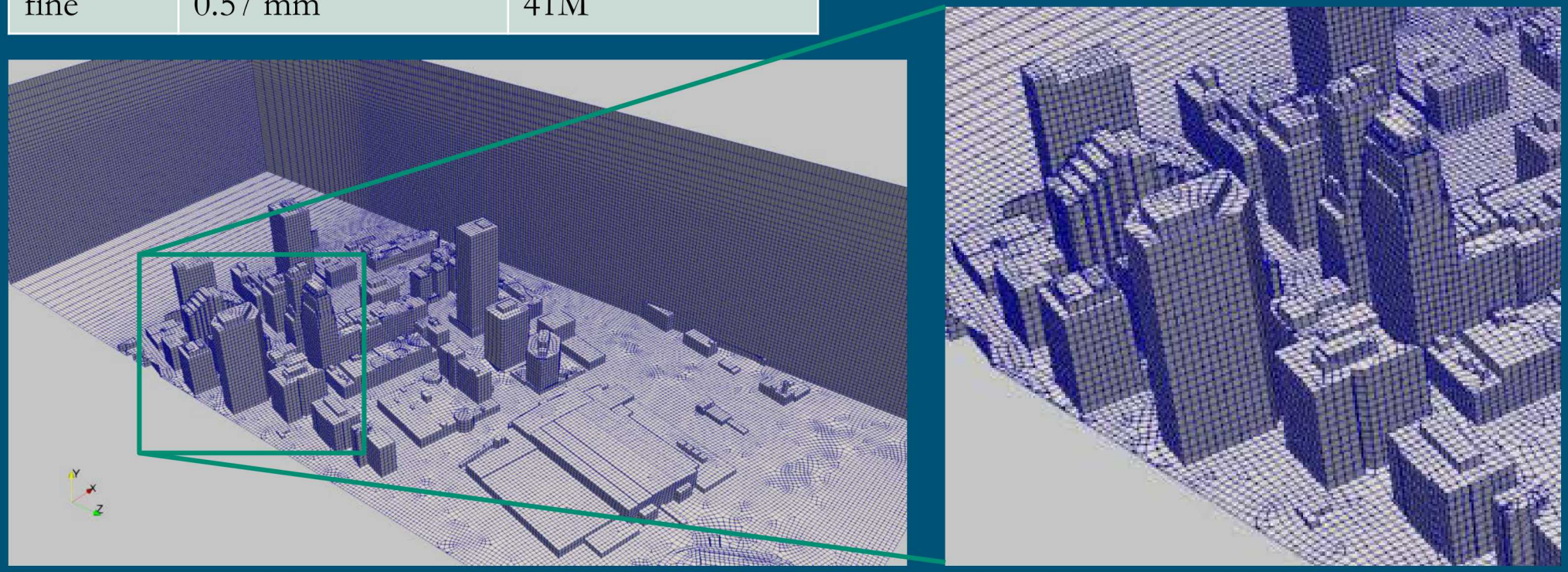


North Broadway-Medium High

Grid refinement was systematic with Hexagonal elements

Experimental resolution is 0.8 mm

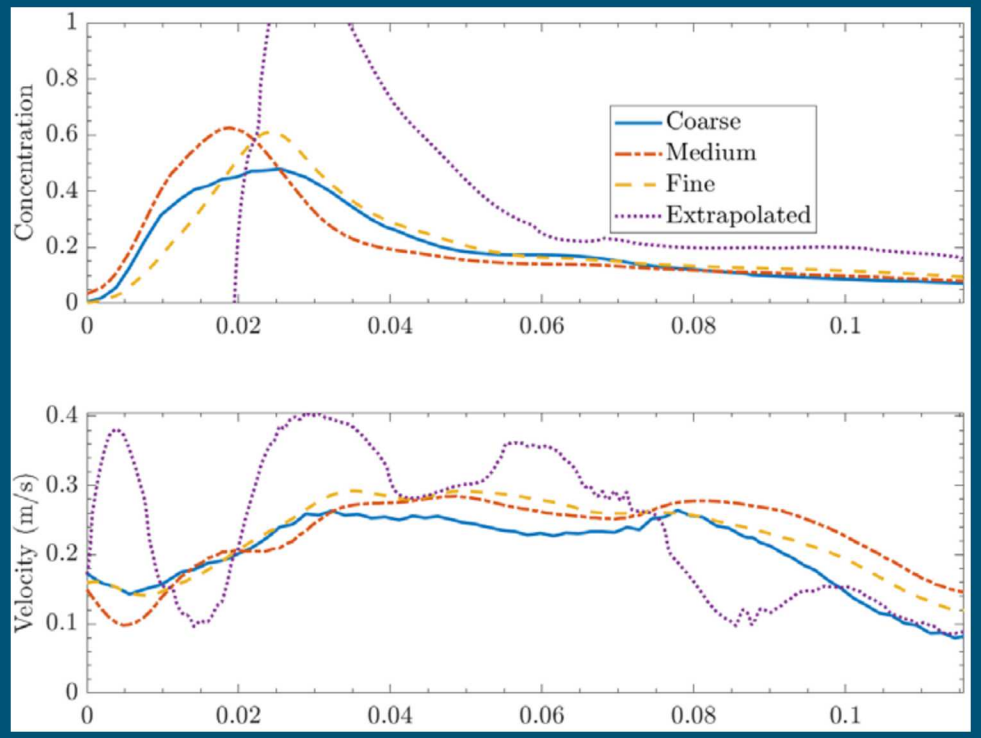
Mesh	Hex Typical Size	Nodes
Coarse	1.7 mm	1.5M
Medium	0.85 mm	12M
fine	0.57 mm	41M



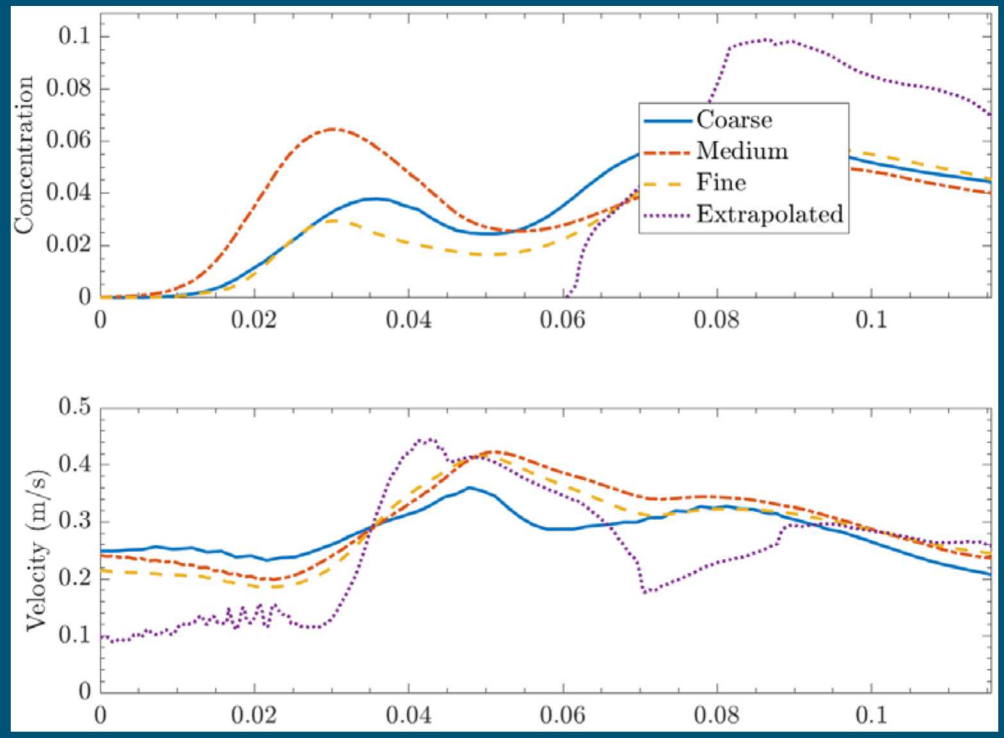
Full Hexahedral Mesh

Grid convergence issues for LES

- Because the level of eddy resolution changes with mesh refinement, the results are a compound of mesh resolution and the changing eddy resolution scale
- Richardson Extrapolation and uncertainty quantification using V&V-20 methods need adaptation
- Best practices need to be developed (perhaps maintaining filter length scale as in Bunge2005)



North Broadway-Medium Low

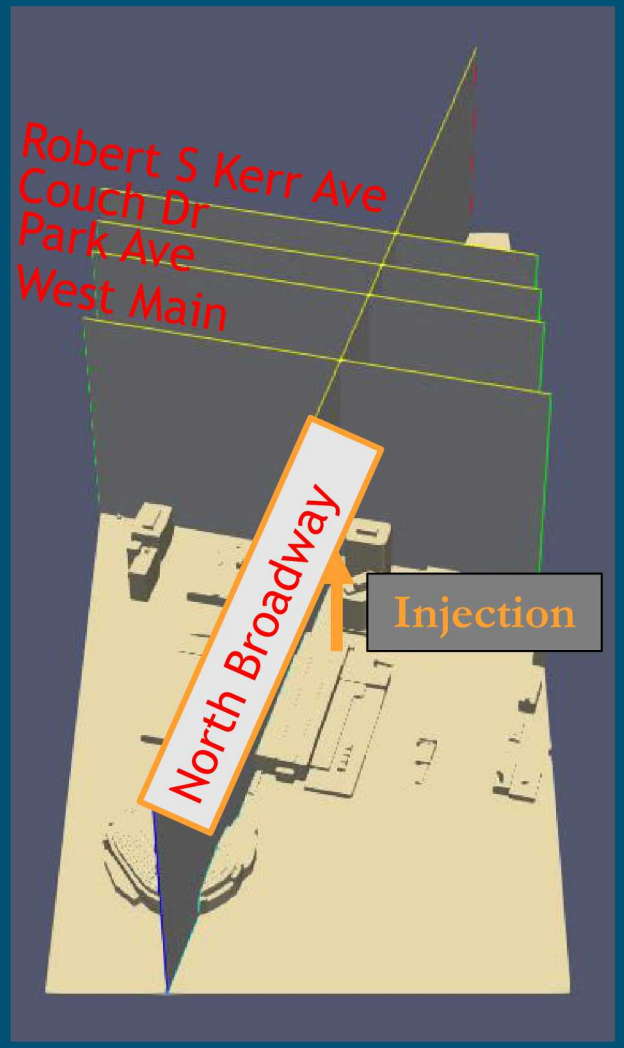


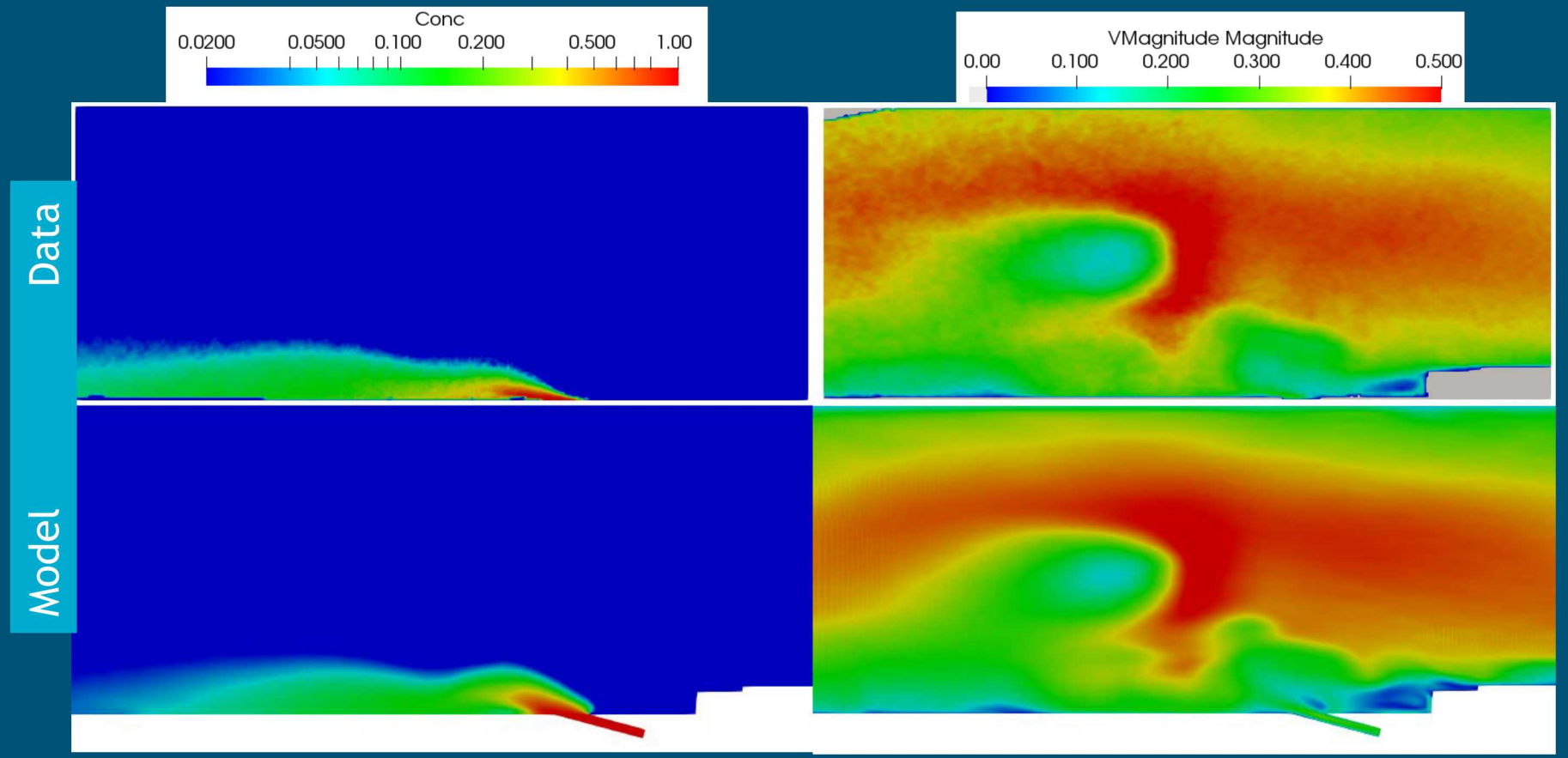
North Broadway-Medium High

Viewgraph norm comparisons

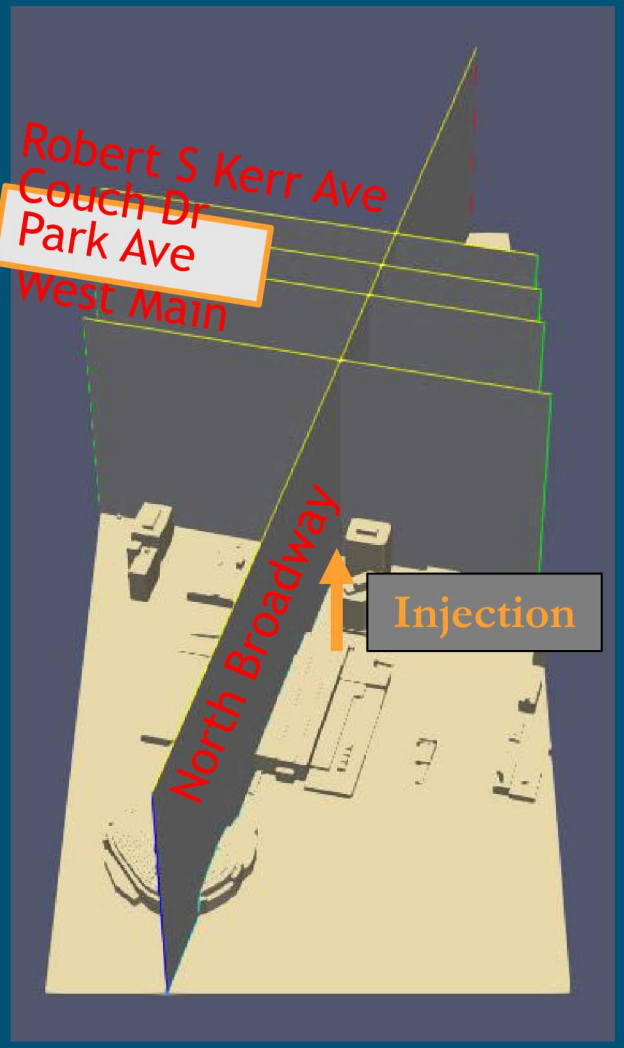
Baseline simulation results

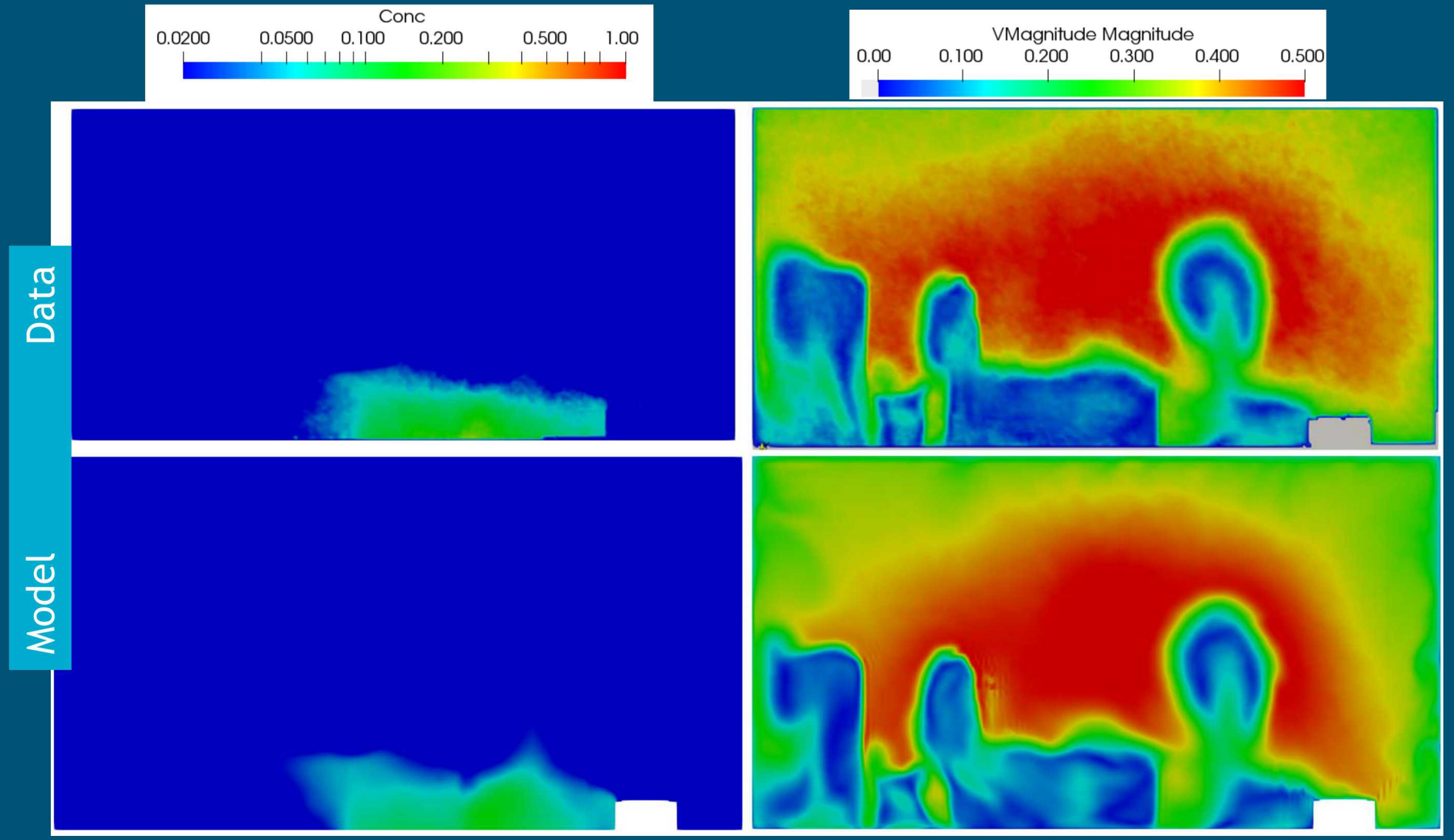
- LES, Medium mesh, hexagonal elements



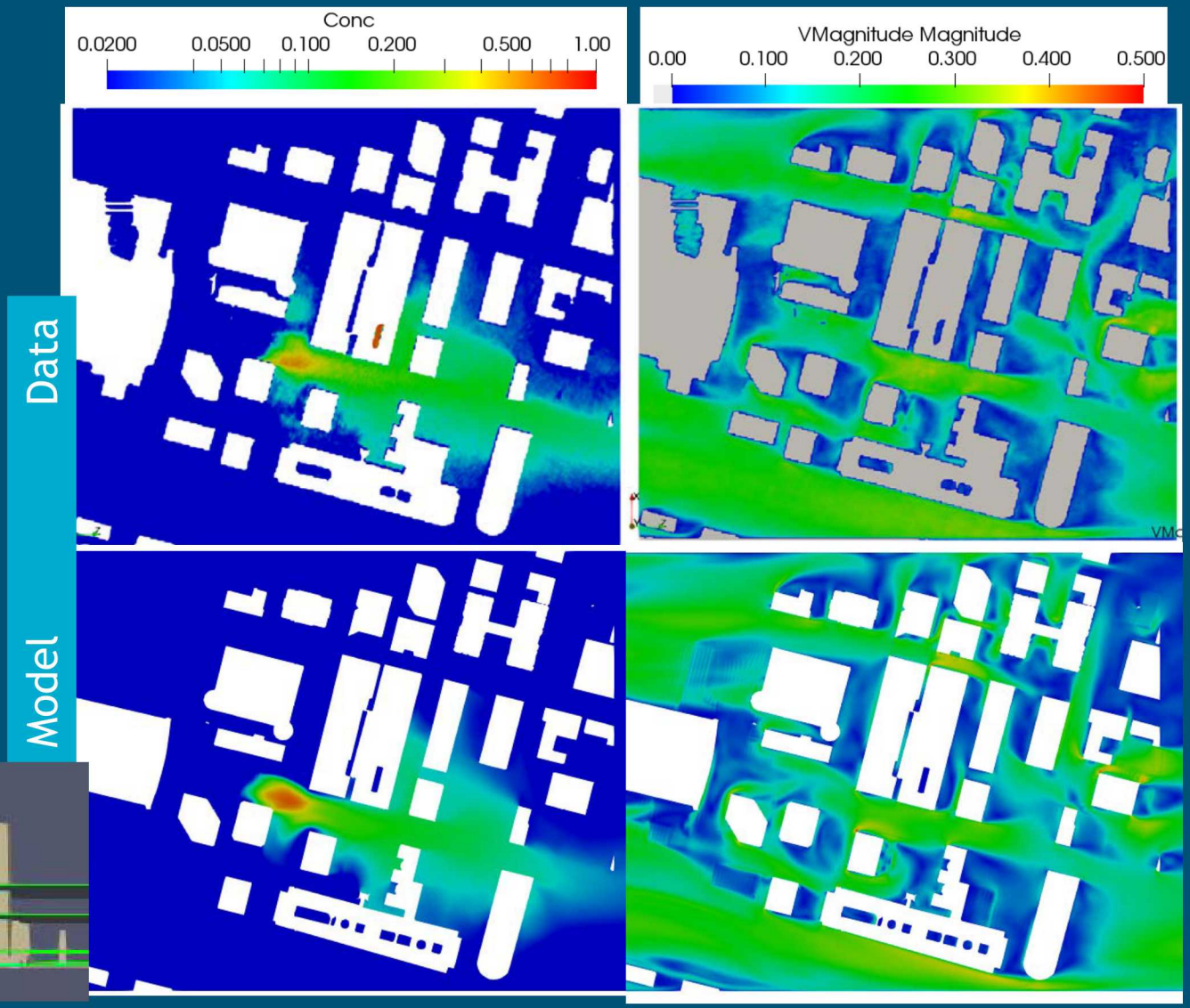


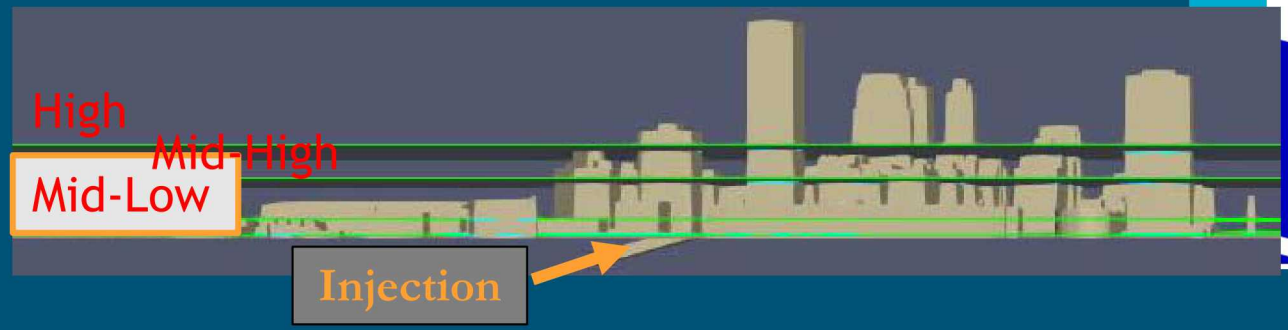
Viewgraph norm comparisons



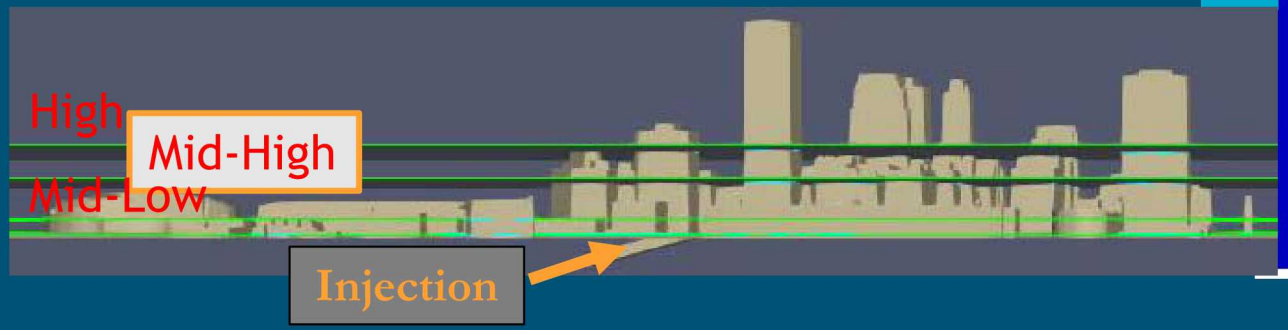


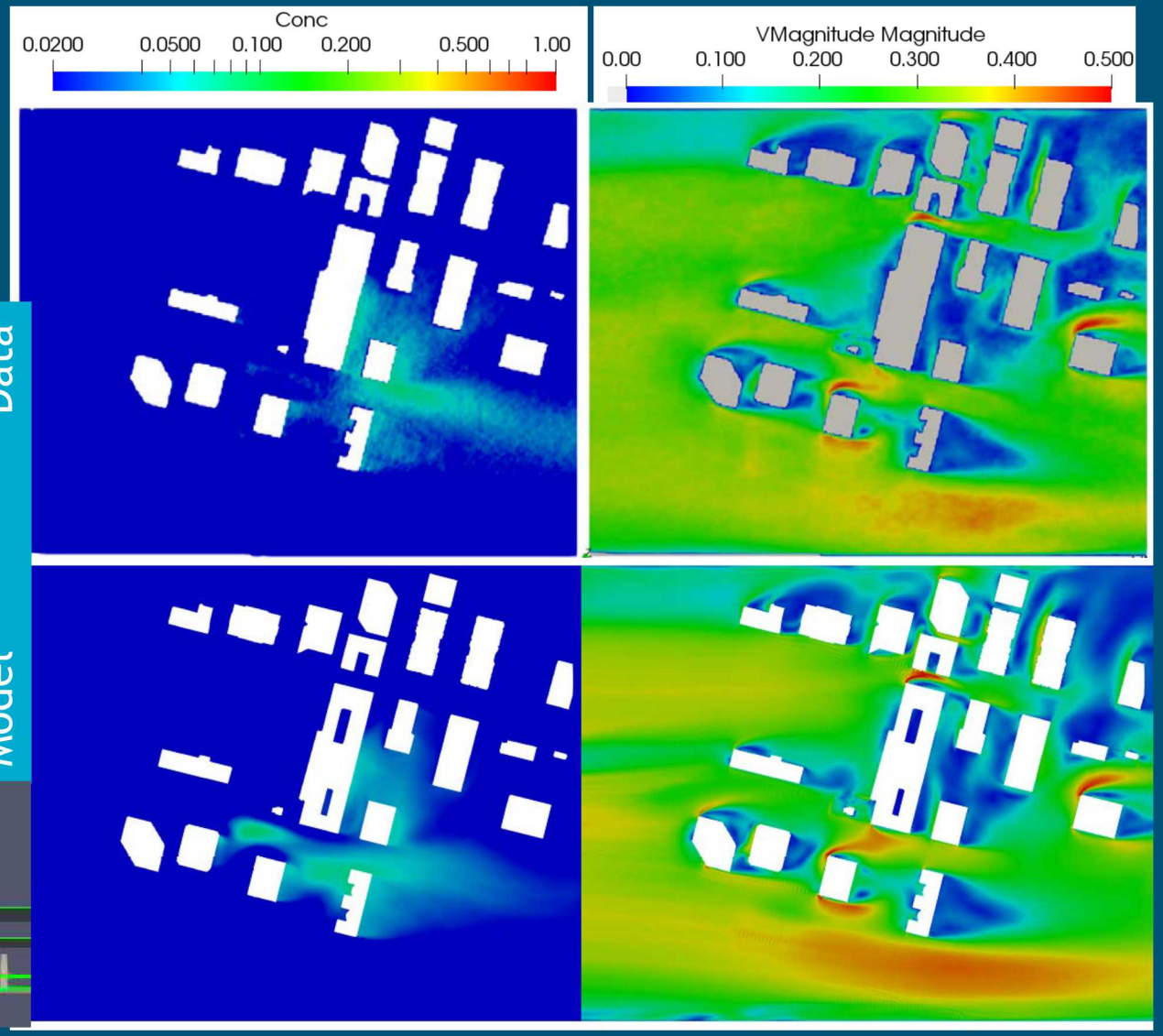
Viewgraph norm comparisons



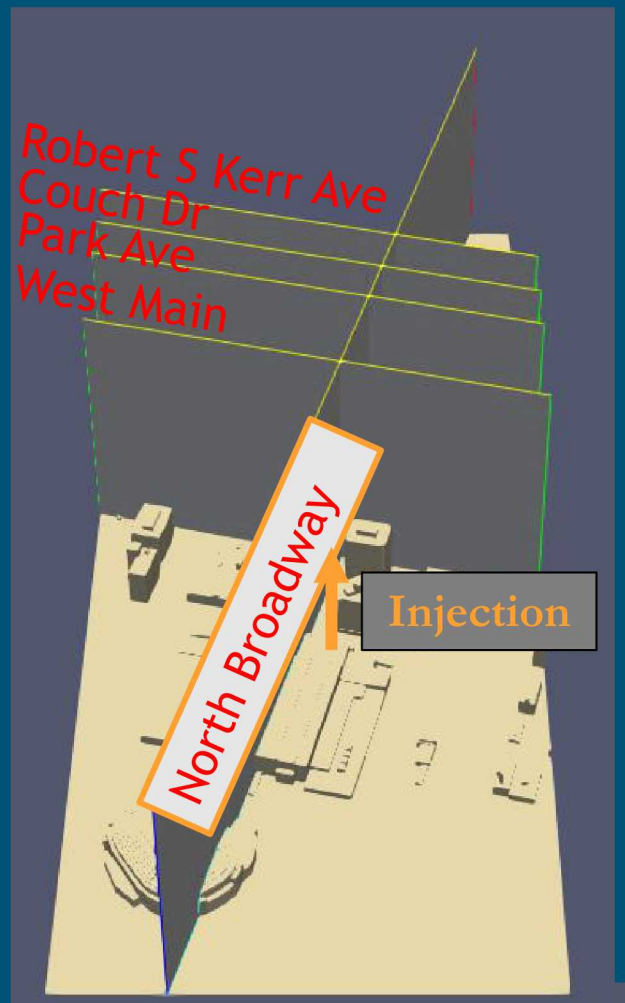


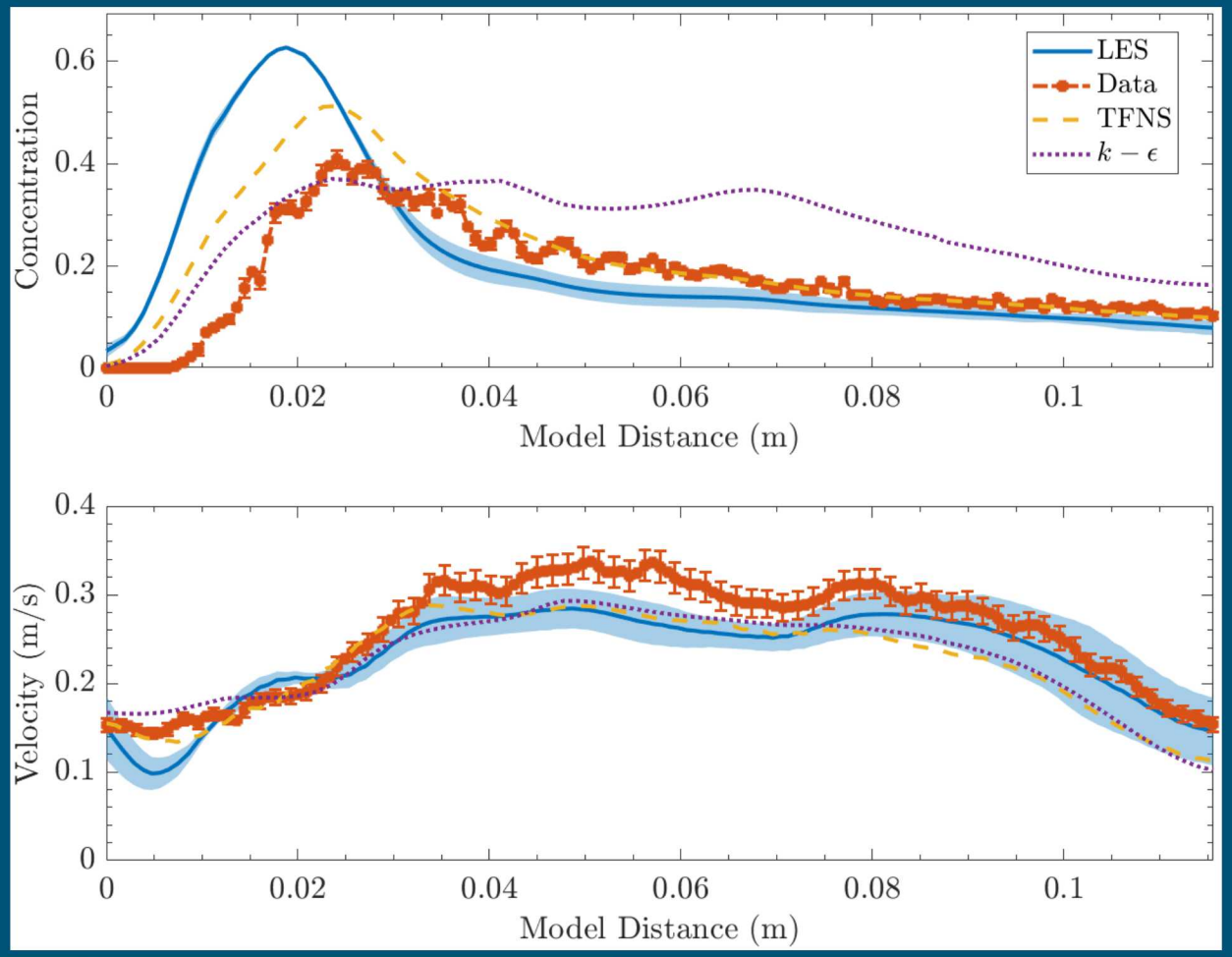
Viewgraph norm comparisons

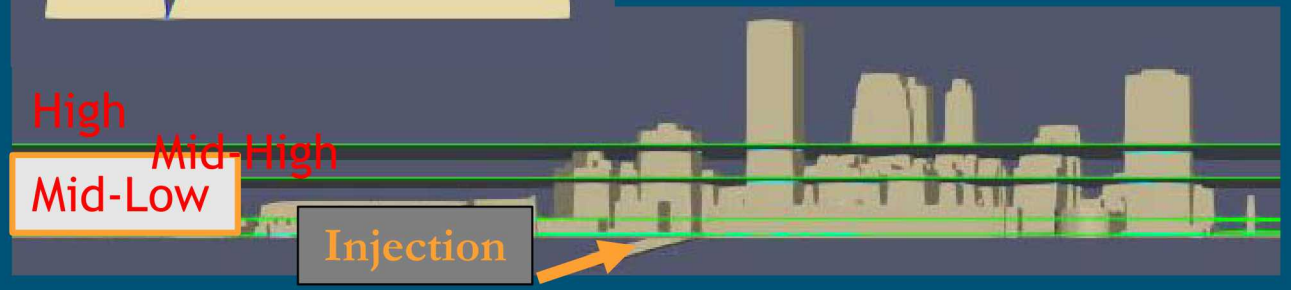




Line plots provide a detailed comparison







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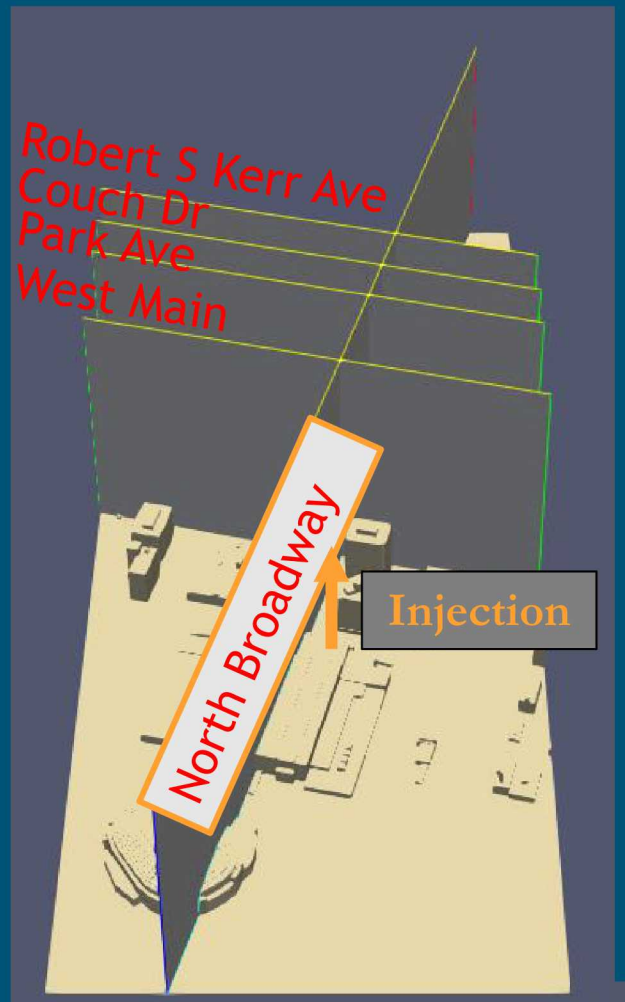
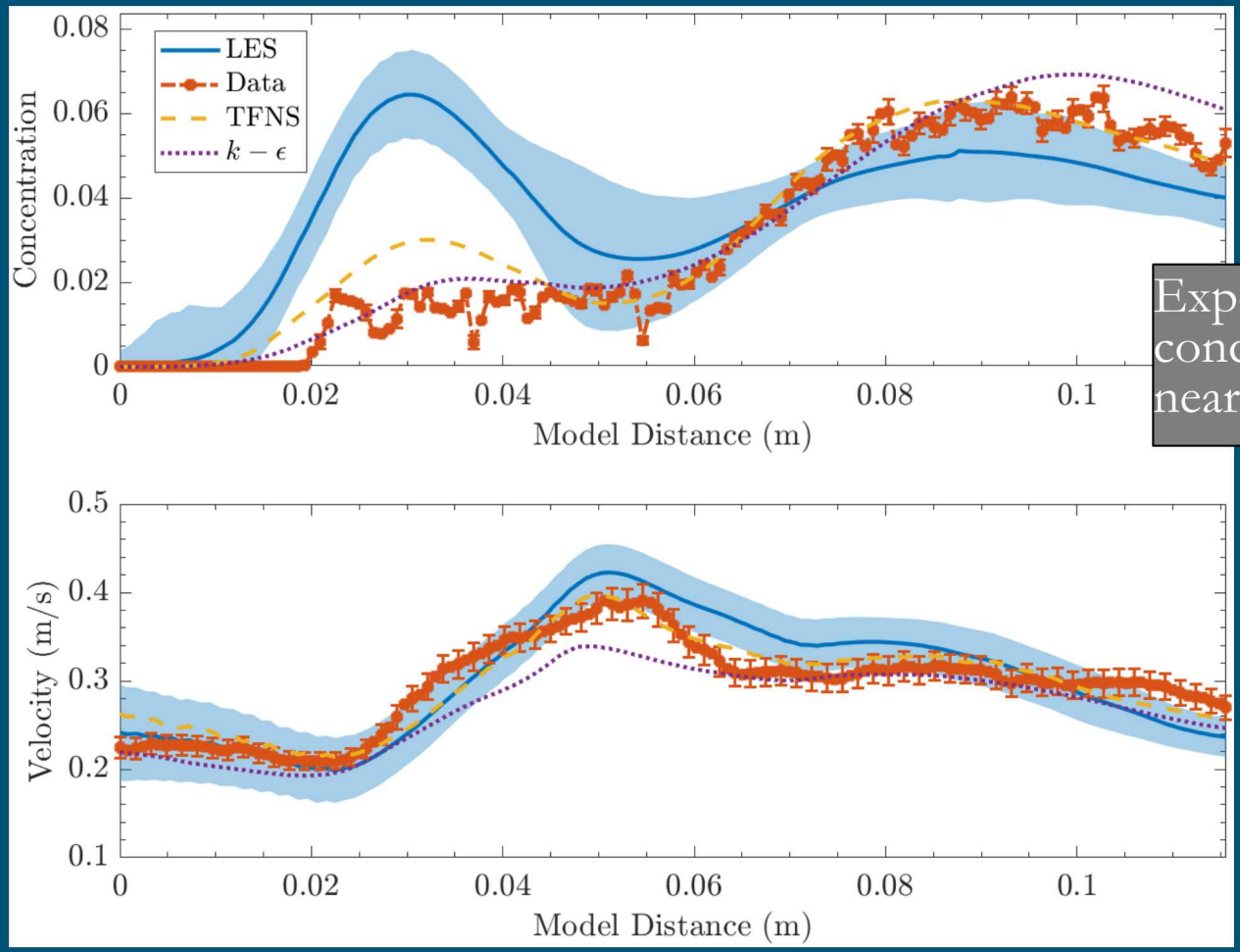
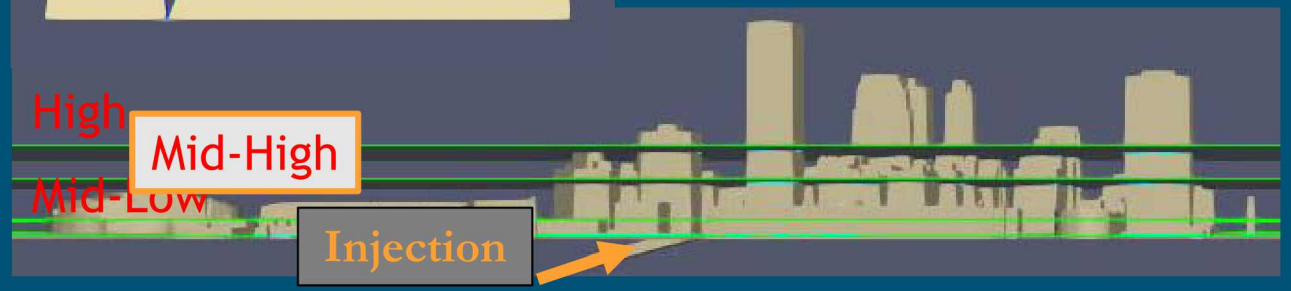




Experimental concentrations are near noise floor



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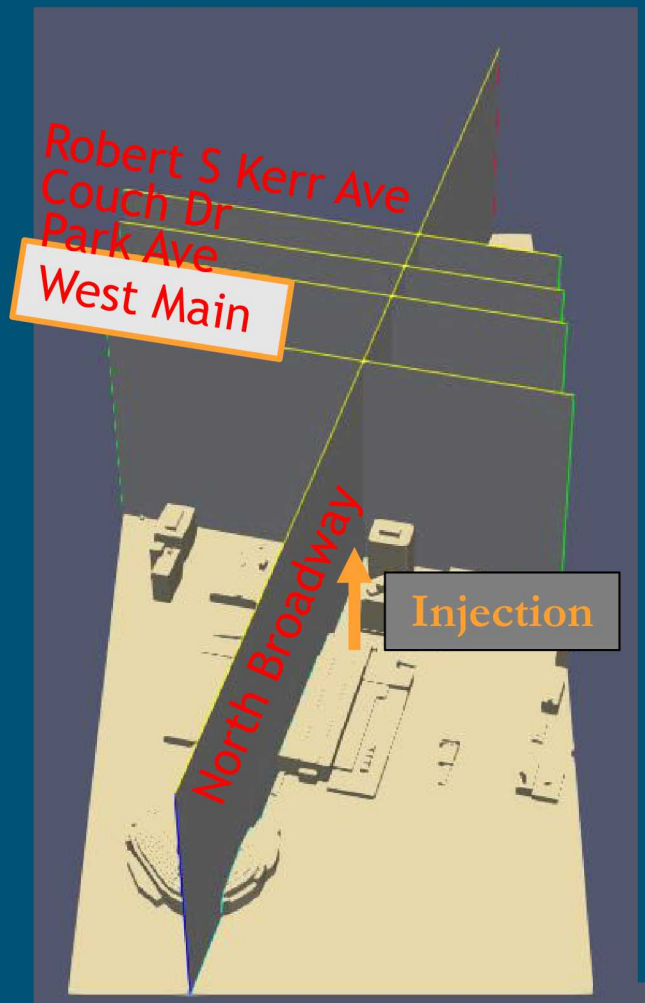
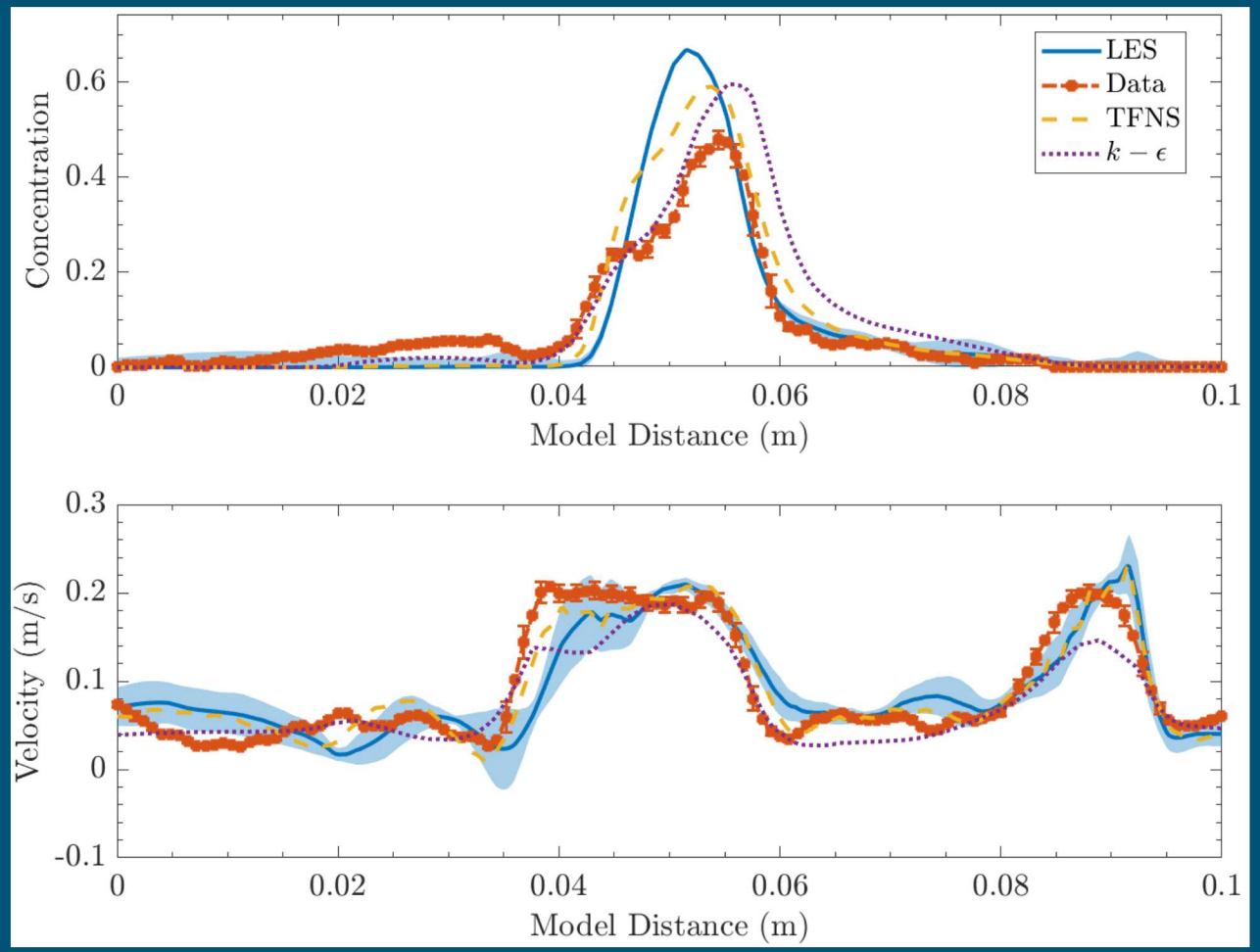
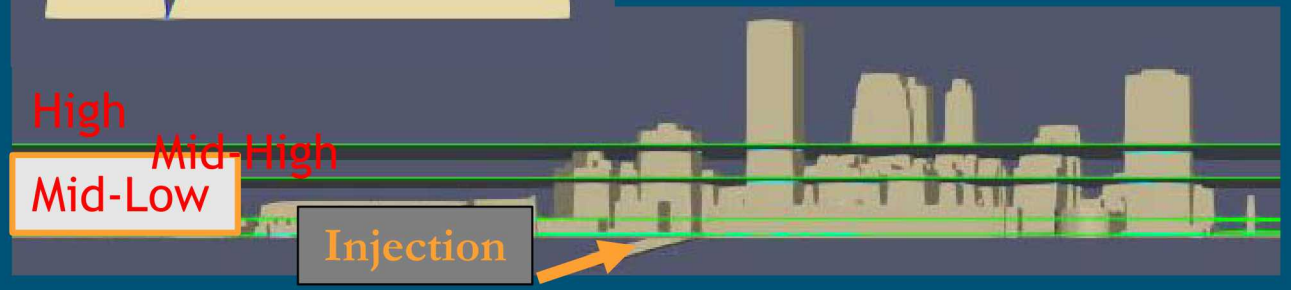
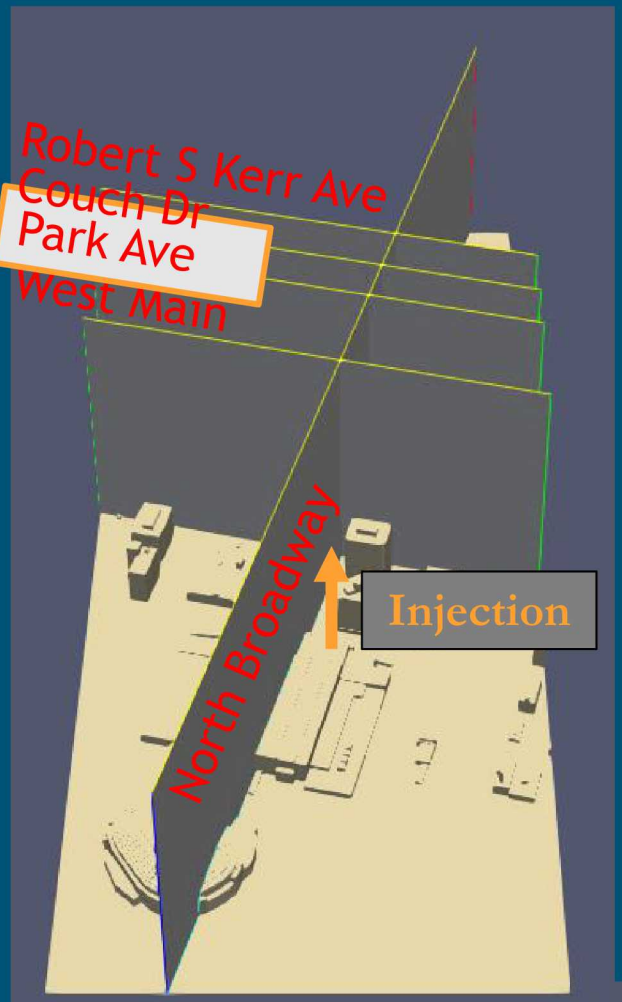
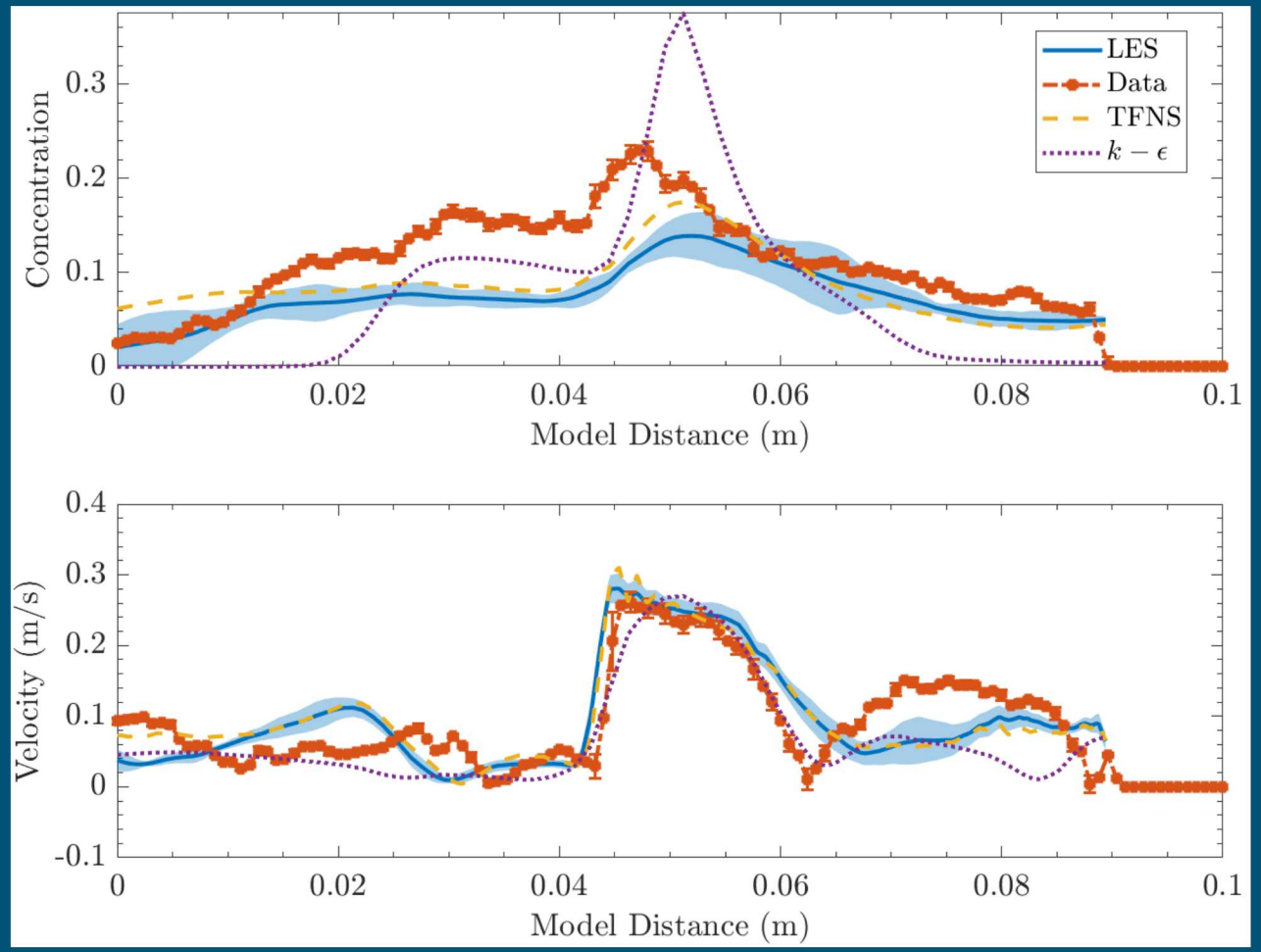


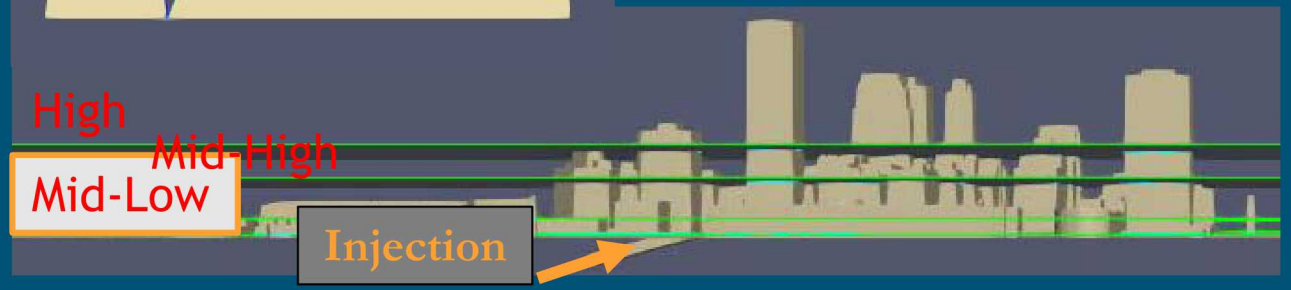




Line plots provide a detailed comparison

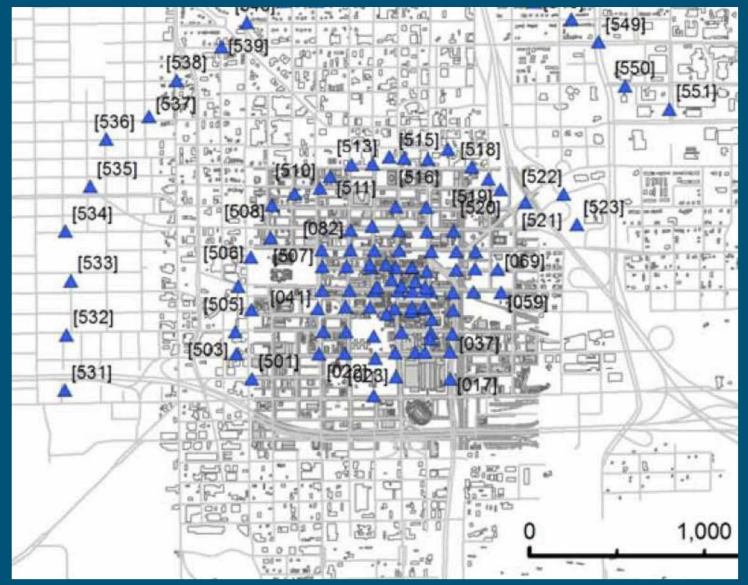




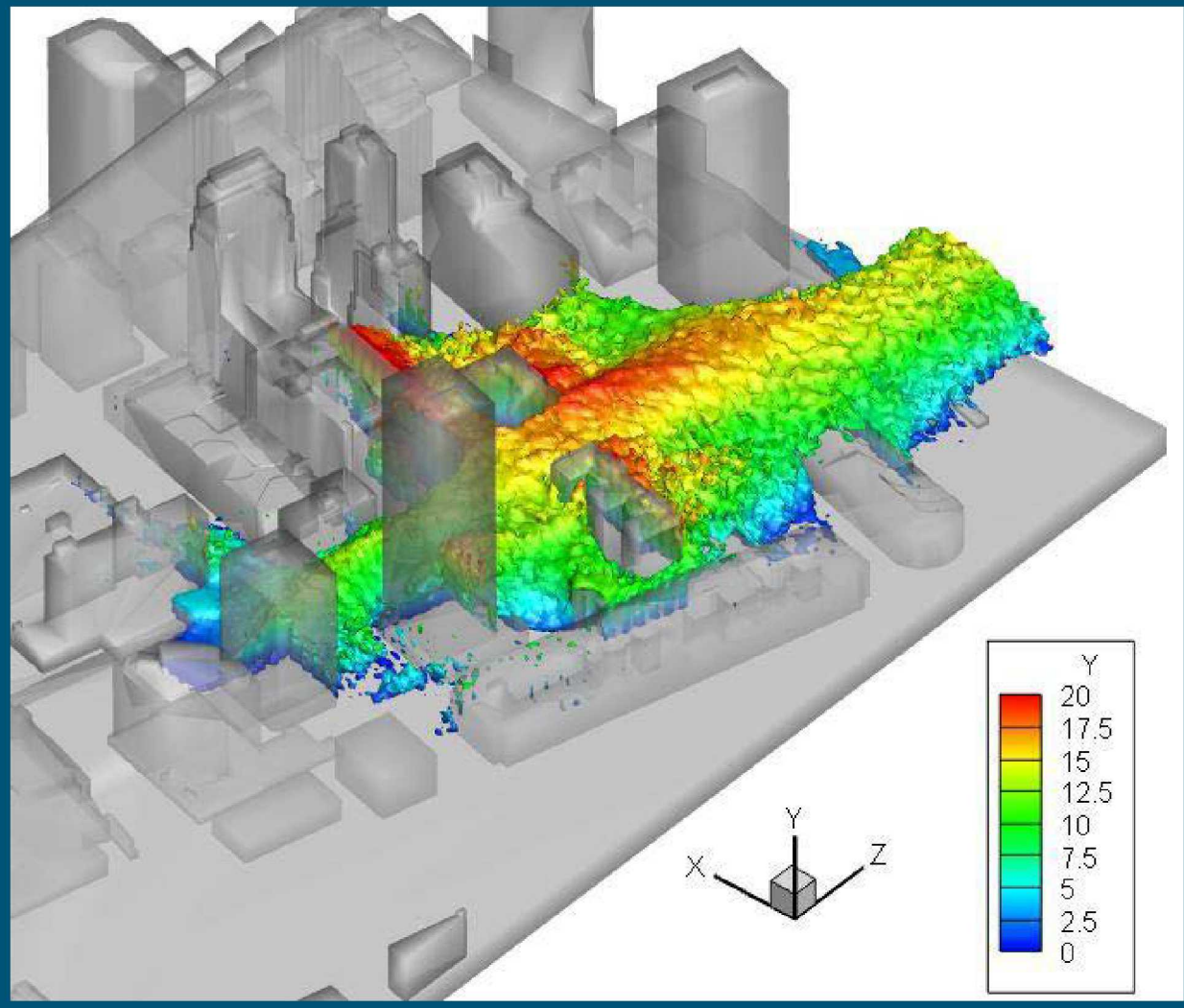


The data have excellent coverage to enable further comparisons

- The experimental data have the best known coverage for fluid dynamics with contaminant transport (not to mention complex geometry)
- Hanna et al. in 2011 proposed several validation metrics
- Validation metrics could be developed further, leveraging the wealth of data available for these physics



Some JU2003 OKC experiment locations, Allwine et al. 2006



Experimental 4% concentration isosurface colored by elevation, Benson, M., Wilde, N., Brown, A., and Elkins, C., "Detailed Measurements of a Contaminant Dispersed in an Oklahoma City Model", Pre-publication print

Conclusions

- The MRV and MRC techniques provide excellent coverage for validation data
- The simulations appear to have good accuracy (application-specific metrics should be evaluated)
- Future Work
  - Best practices for grid converge studies for LES should be developed
  - Terrain geometry

Purple is a 1% concentration

Backup

Scaled validation data were measured in a medical MRI machine

- Experiments conducted at Stanford
- Methods
  - Magnetic Resonance Velocimetry
  - Magnetic Resonance Concentration
- $CuSO_4$ tracer in water
- Full 3D data, $\mathrm{Re}_{D_H} = 36{,}000$
- Time-averaged over 20 minutes
- 0.8 mm resolution, 13.4 million voxels
- U_{velocity} = 4% of measured value
- $U_{\text{concentration}}$ = 5.5% of measured value
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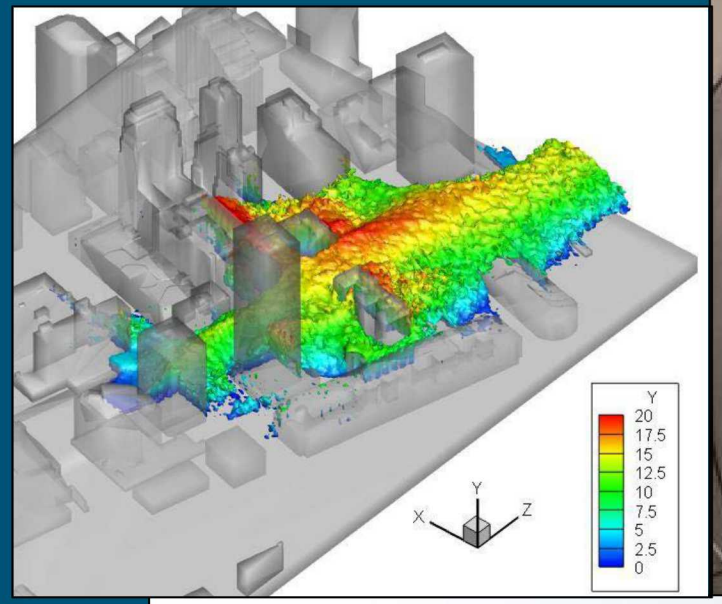
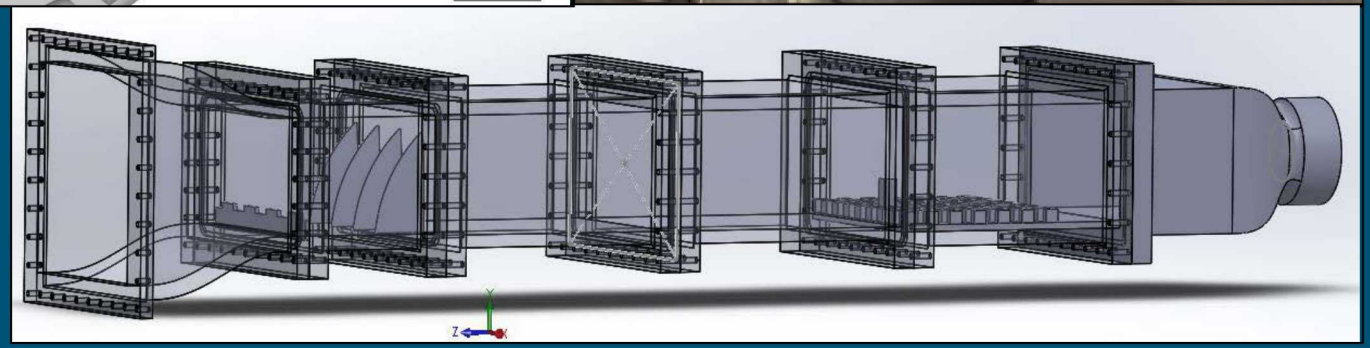
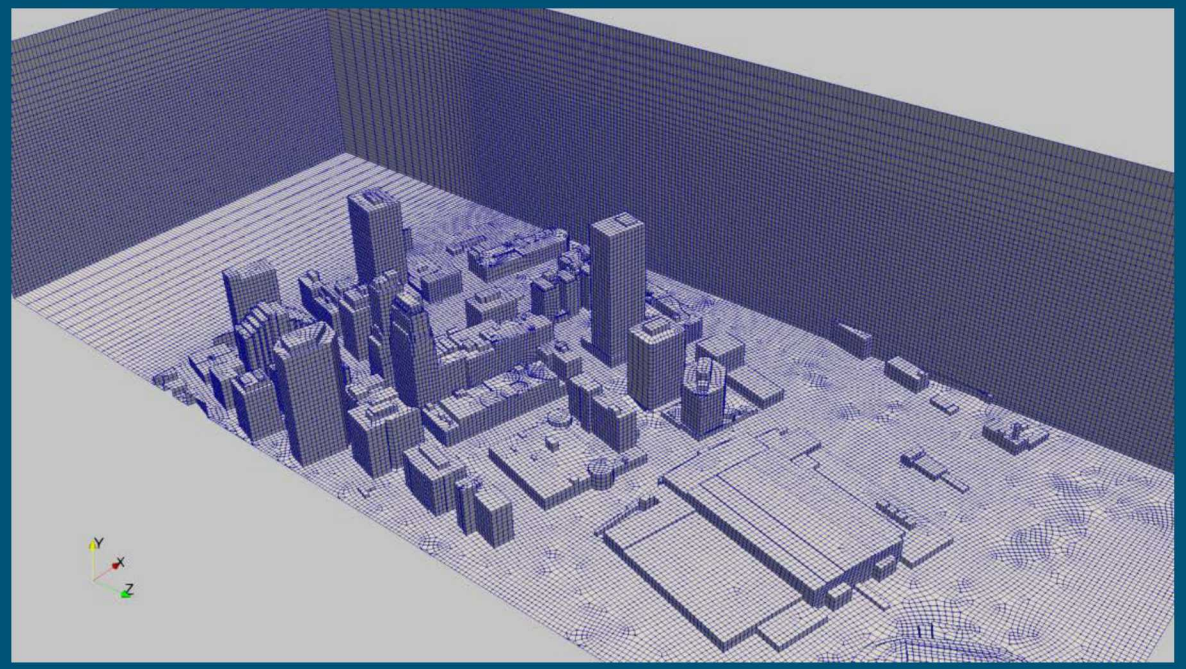




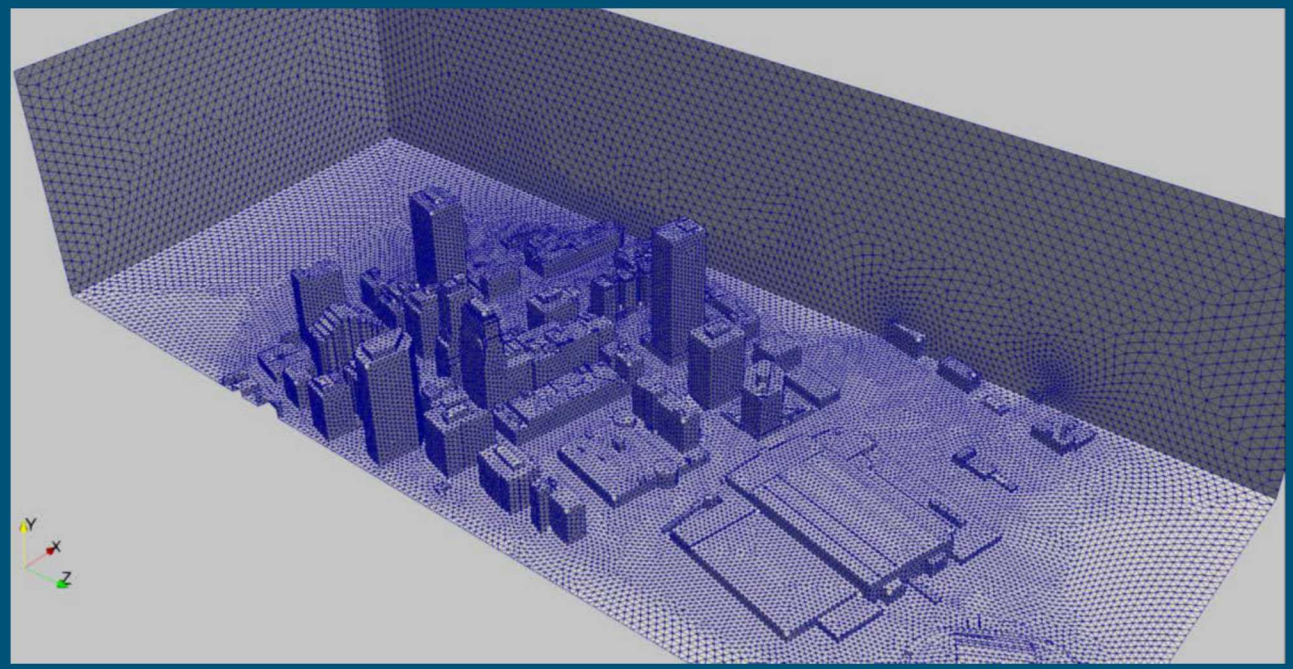
Test section: 196 mm W, 110 mm H, 239 mm L

Grid refinement was systematic on both Hex and Tet element types

Mesh	Hex Typical Size	Tet Typical Size
Coarse	1.7 mm	2 mm
Medium	0.85 mm	1 mm
fine	0.57 mm	0.5 mm



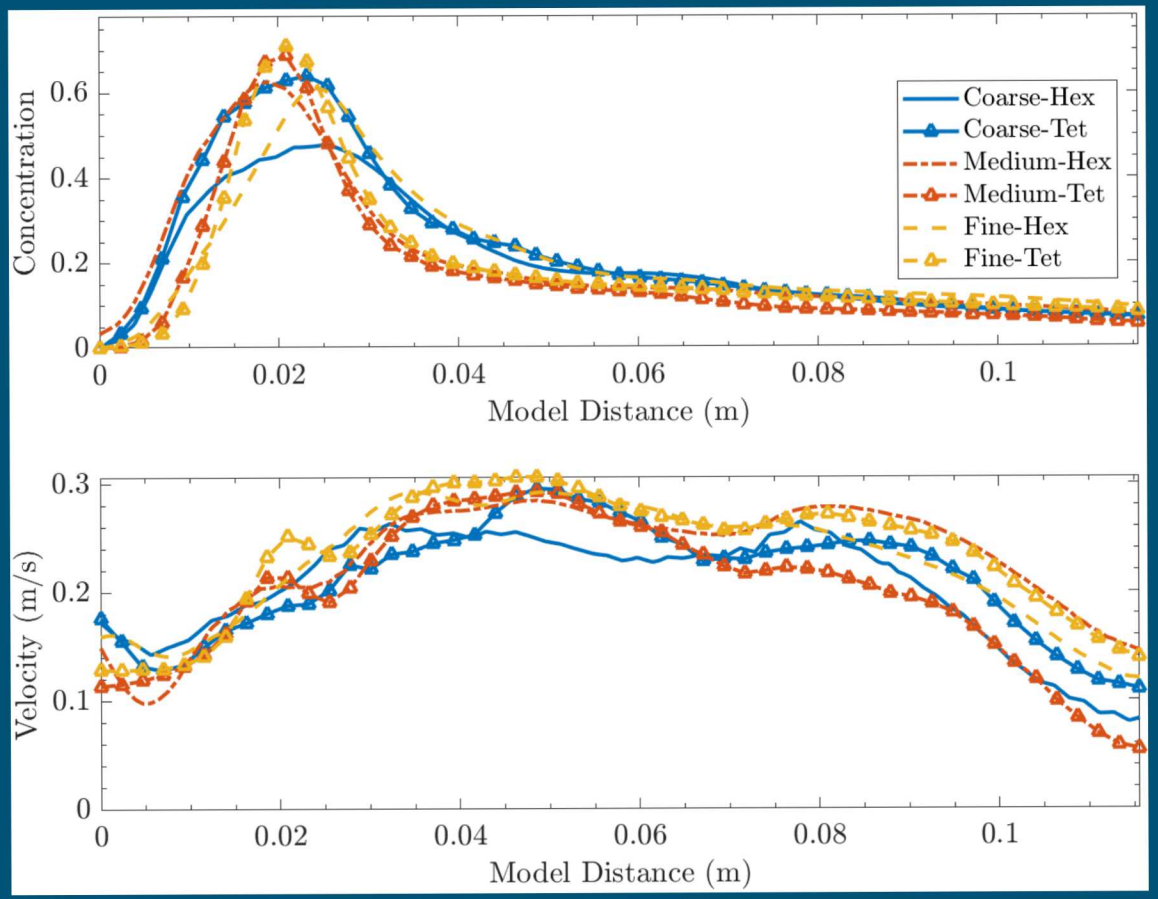
Hexahedral Mesh



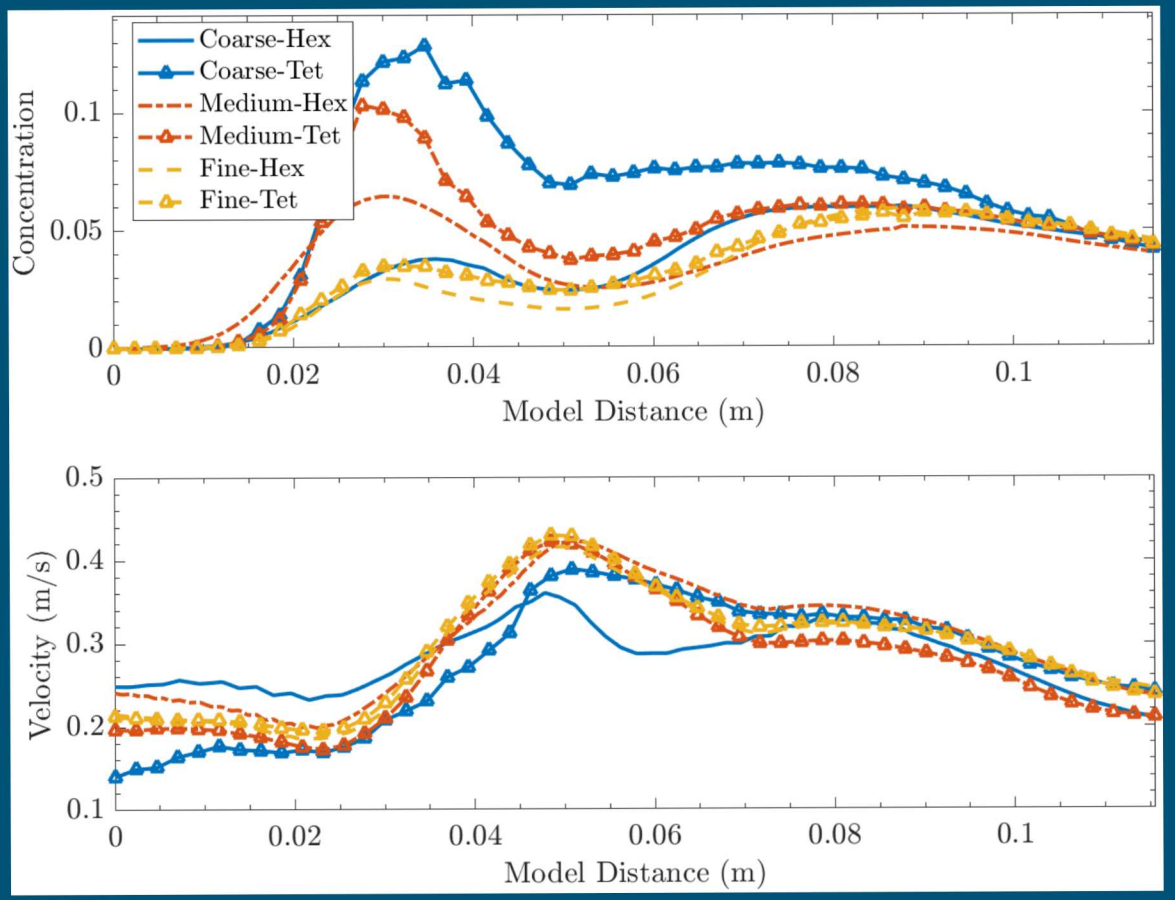
Tetrahedral Mesh

The results can be compared on different meshes

- Greater consistency between Hex and Tet results is observed with greater refinement
- Tets predict higher concentrations

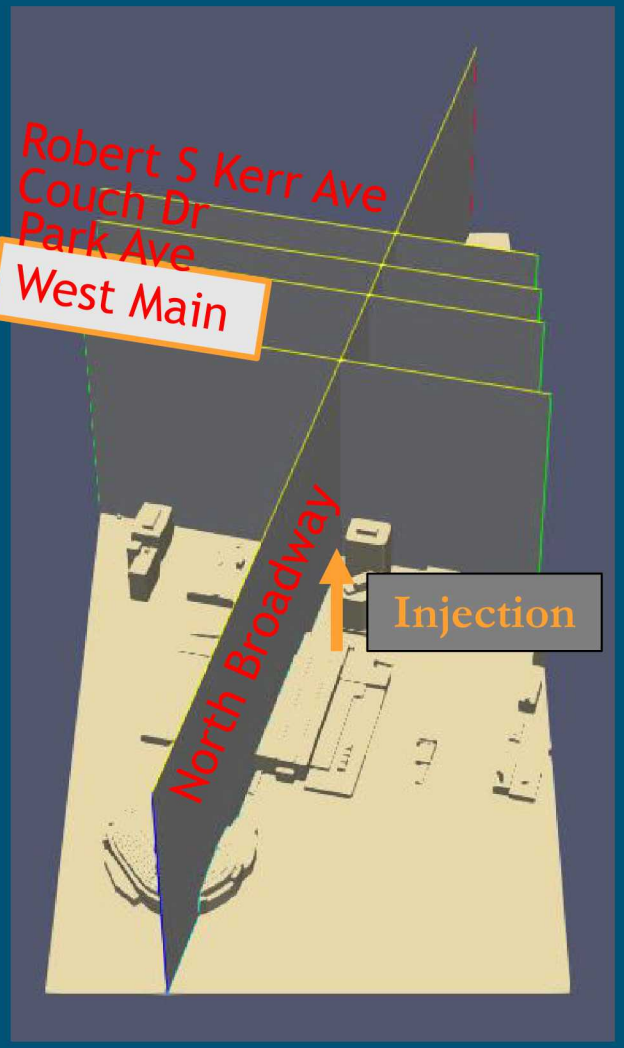


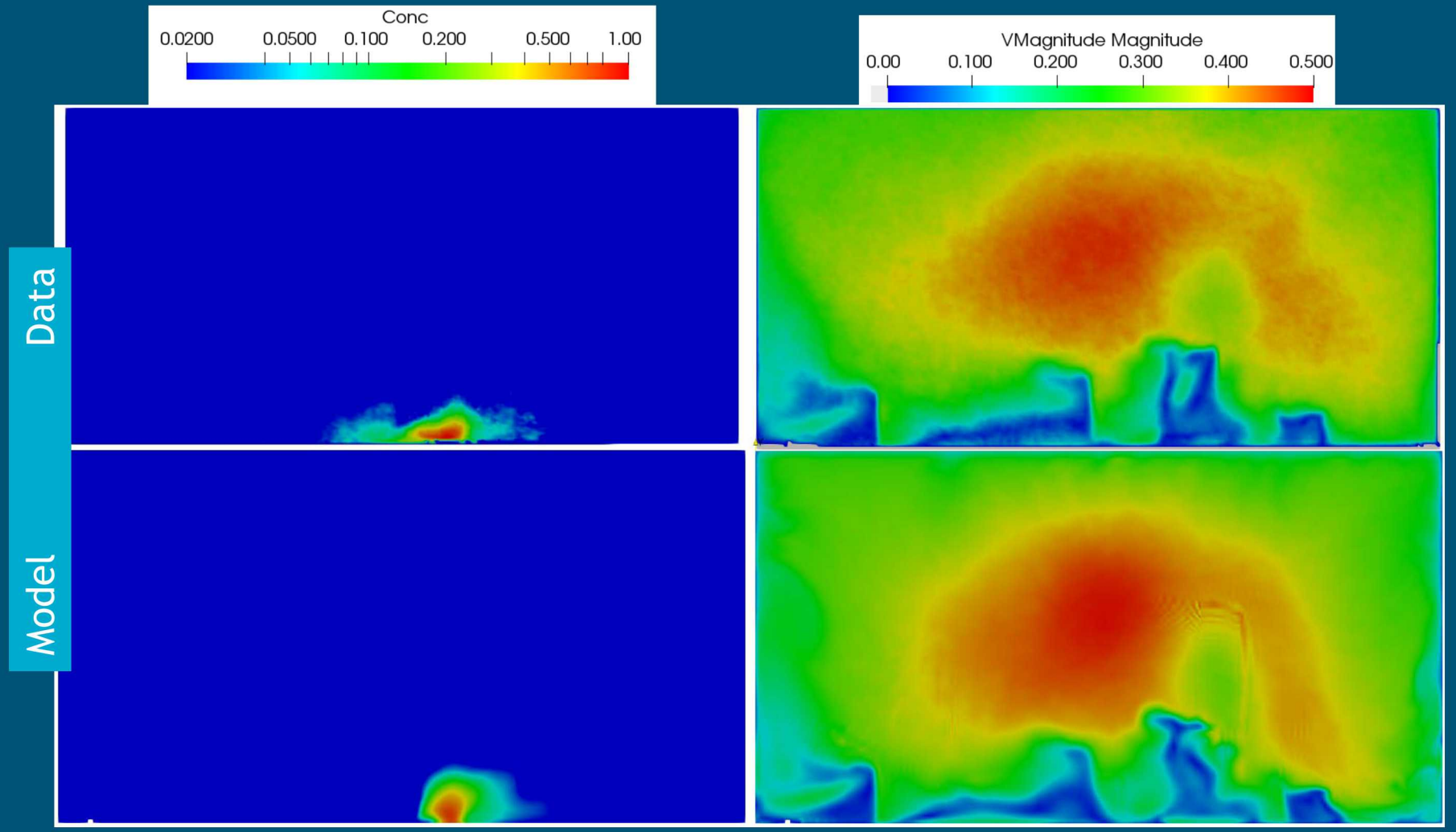
North Broadway-Medium Low



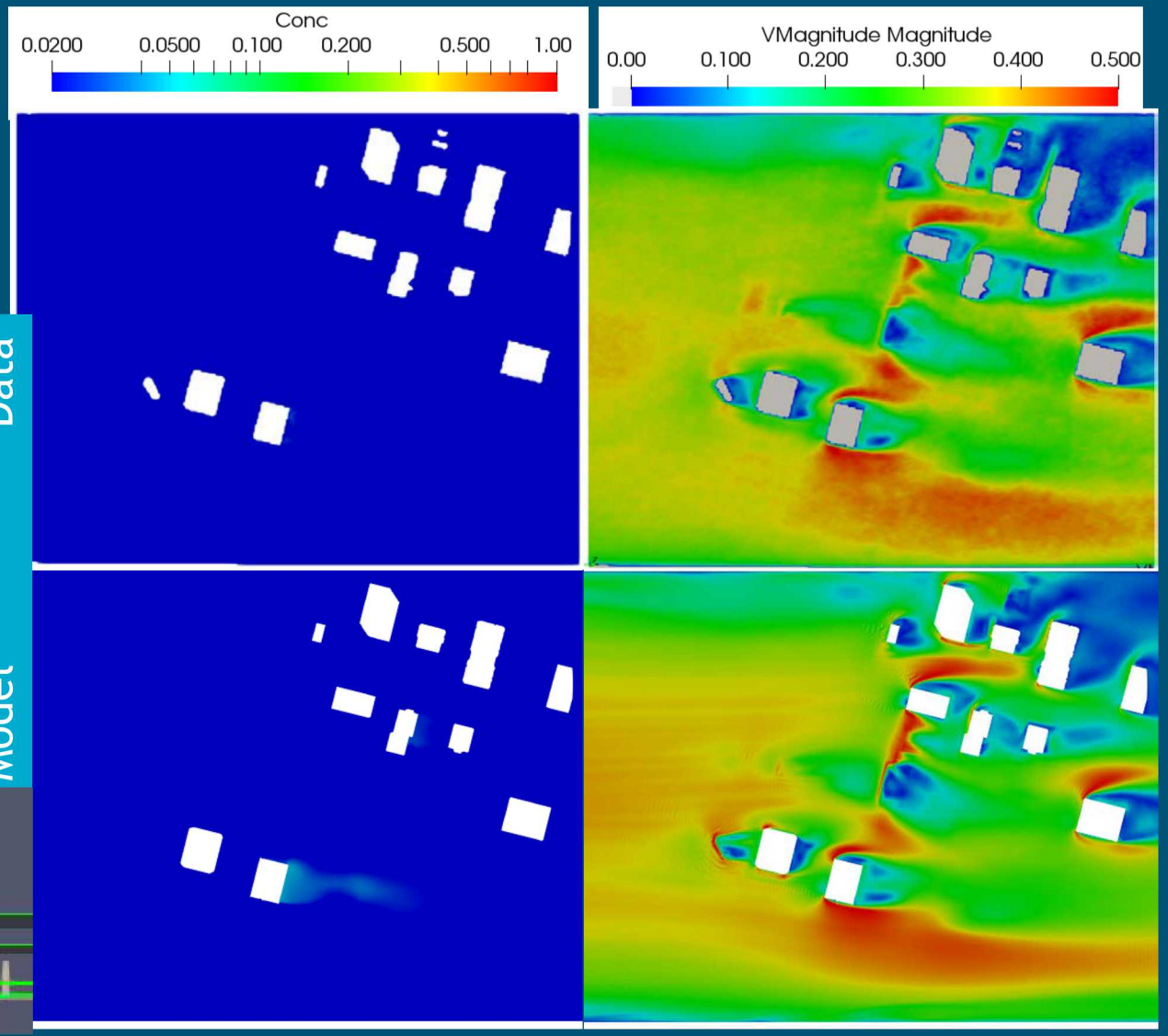
North Broadway-Medium High

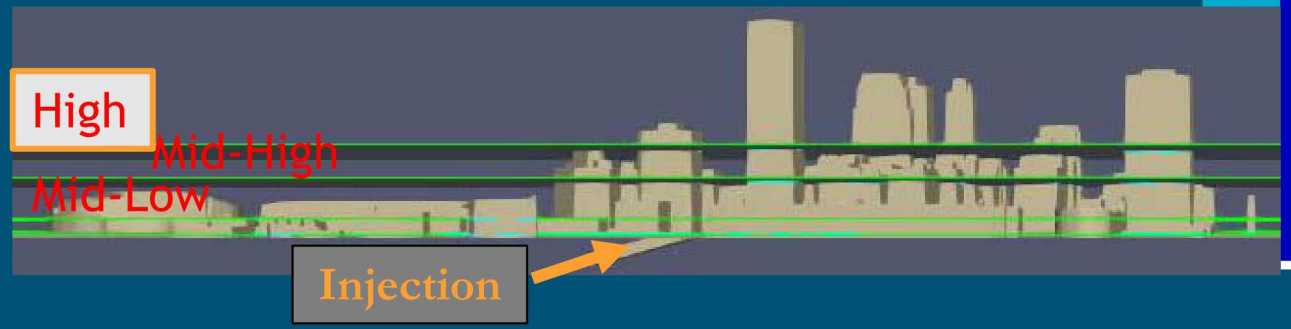
Viewgraph norm comparisons



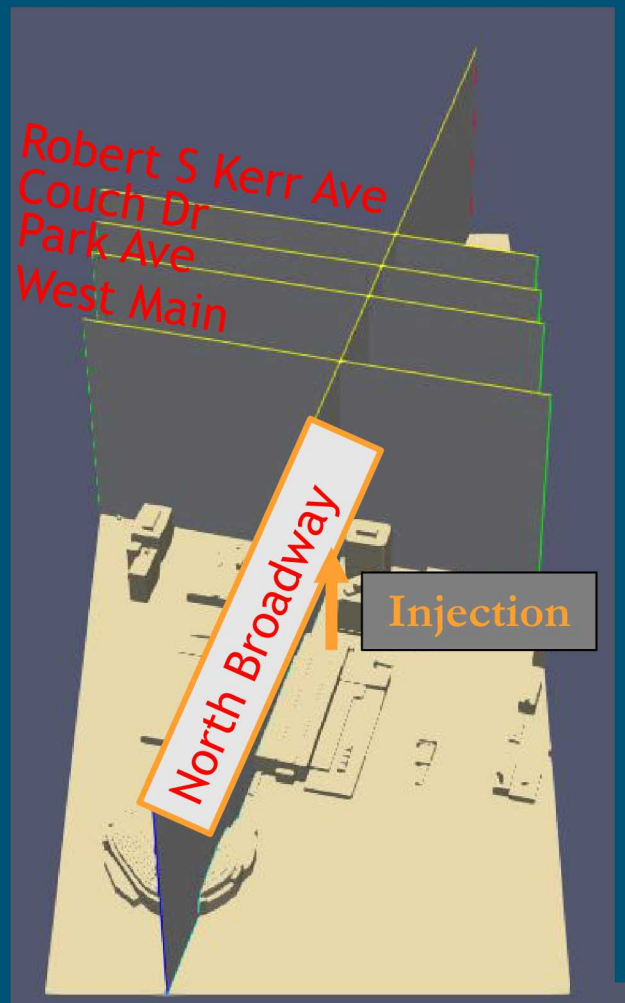


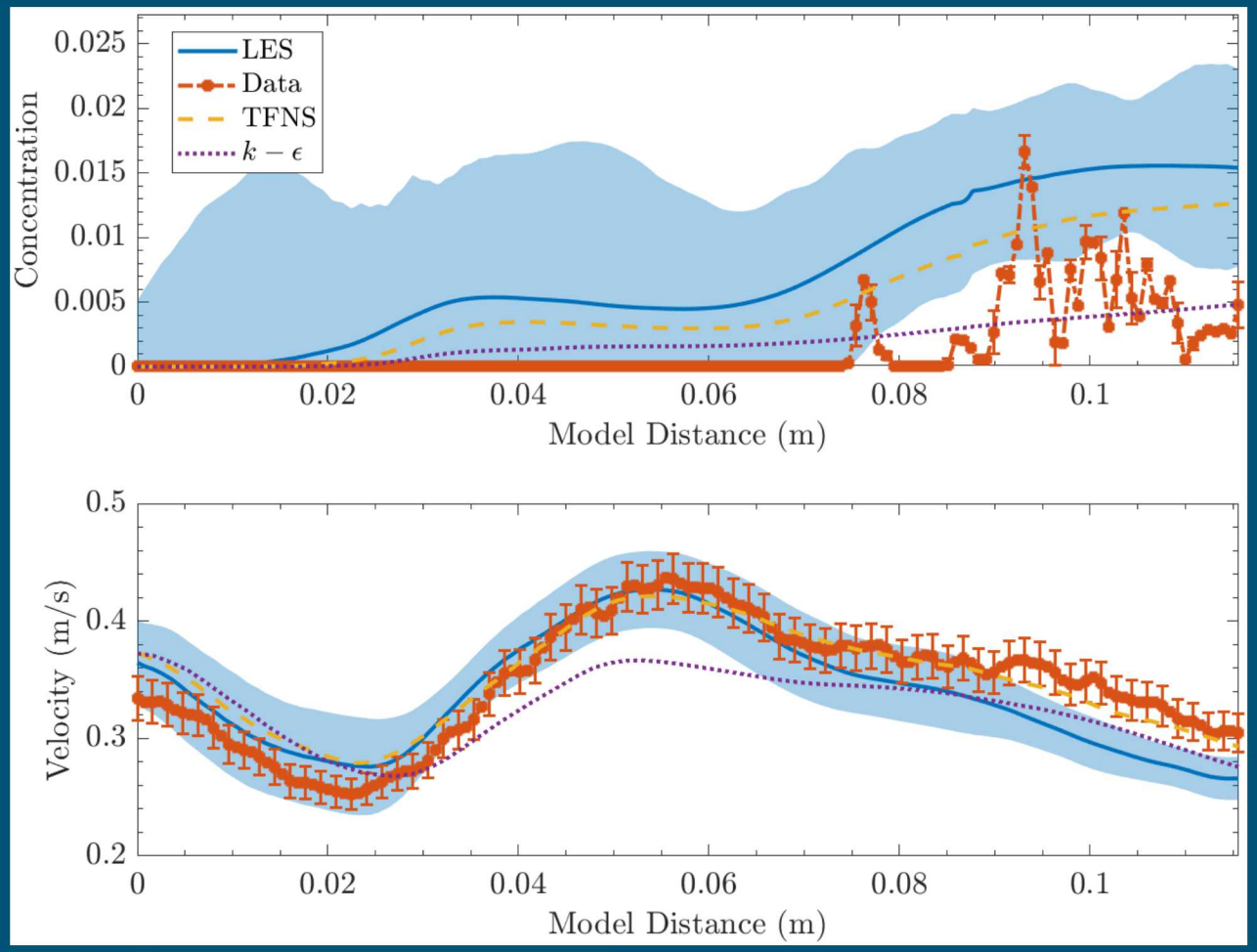
Viewgraph norm comparisons

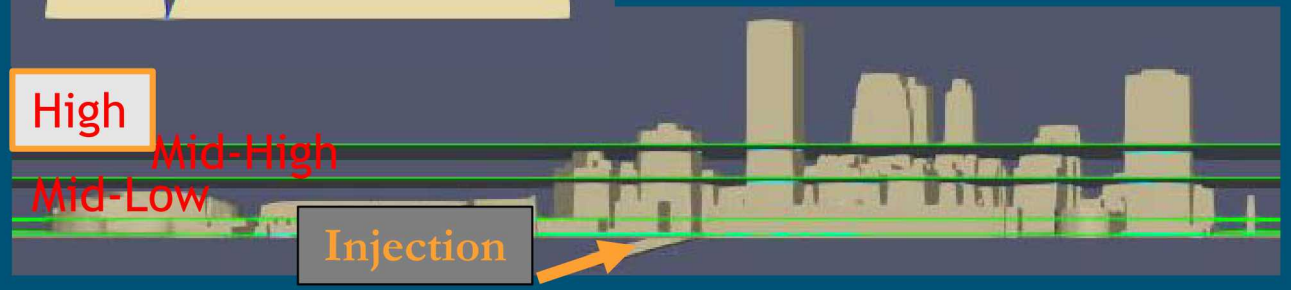




Line plots provide a detailed comparison







The data have excellent coverage to enable further comparisons

- Several metrics exist in literature for contaminant dispersion in atmospheric flows
- There are acceptance criteria for each metric, but the authors state they are arbitrary
- Preliminary results for this work suggest that LES predictions can easily pass all criteria, much better than many Lagrangian models

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ORIGINAL PAPER

Acceptance criteria for urban dispersion model evaluation

Steven Hanna · Joseph Chang

Fractional mean bias

$$FB = 2(\overline{C_o} - \overline{C_p})/(\overline{C_o} + \overline{C_p}) \quad (1)$$

Normalized mean-square error

$$NMSE = \overline{((C_o - C_p)^2)}/(\overline{C_o} * \overline{C_p}) \quad (2)$$

Geometric mean

$$MG = \exp(\overline{\ln C_o}) - (\overline{\ln C_p}) \quad (3)$$

Geometric variance

$$VG = \exp\overline{((\ln C_o - \ln C_p)^2)} \quad (4)$$

Fraction of C_p within a factor of two of C_o

$$FAC2 \quad (\text{fraction} \quad \text{where } 0.5 < C_p/C_o < 2) \quad (5)$$

Normalized absolute difference

$$NAD = \overline{|C_o - C_p|}/(\overline{C_o} + \overline{C_p}) \quad (6)$$