

SAND2019-2456C

Normal Stresses in Frictional Granular Flows

PRESENTED BY

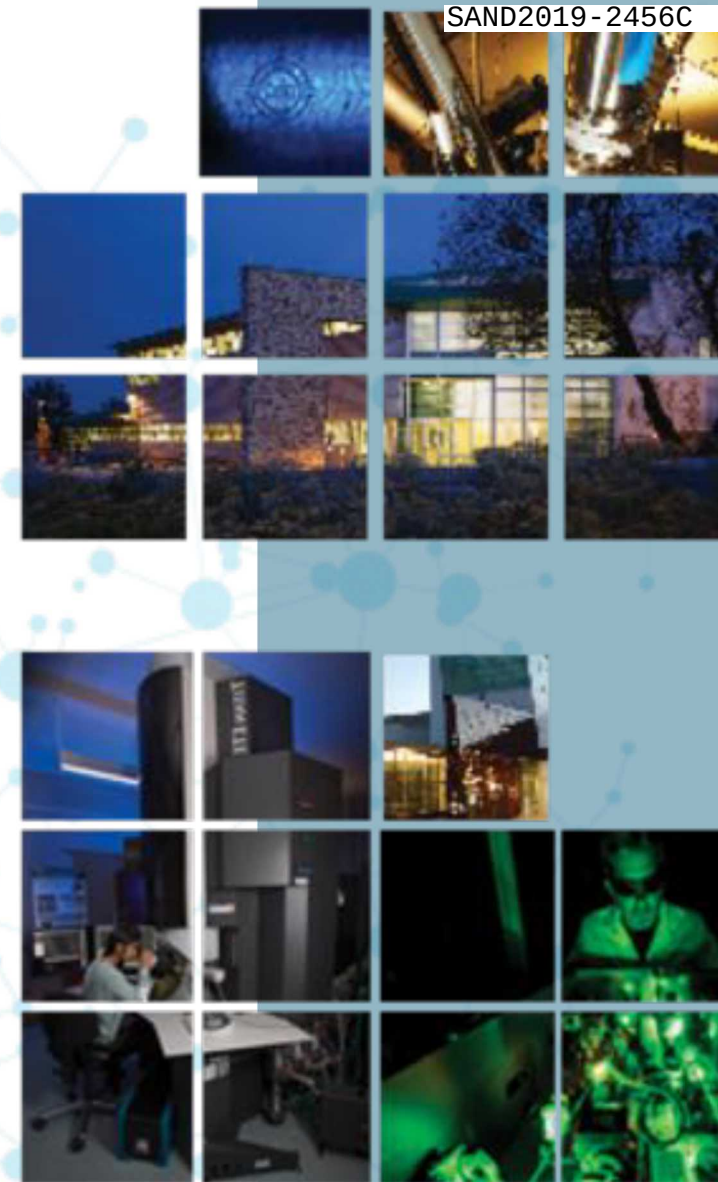
Ishan Srivastava (isriva@sandia.gov)

Leonardo E. Silbert, Gary S. Grest, Jeremy B. Lechman



Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA-0003525.

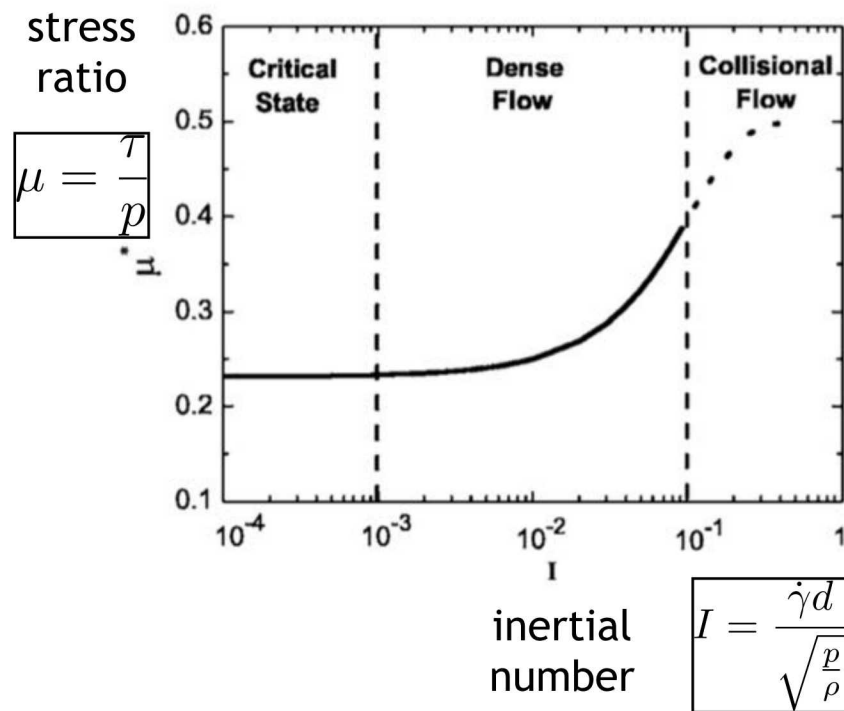
This work was performed, in part, at the Center for Integrated Nanotechnologies, an Office of Science User Facility operated for the U.S. Department of Energy (DOE) Office of Science.



Dense Granular Rheology

$\mu(I)$ rheology

co-directional flow

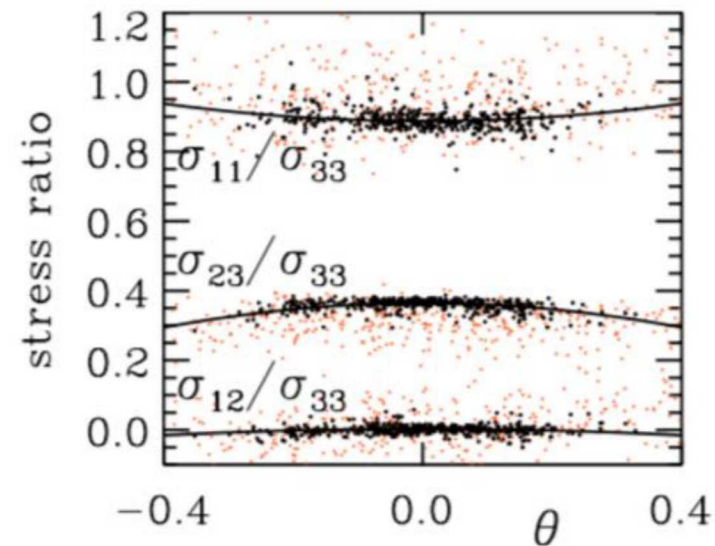
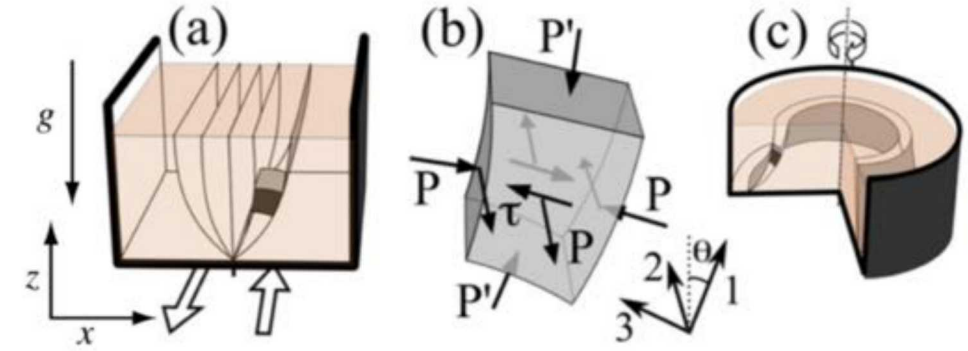


da Cruz et al., Phys. Rev. E, 72 (2005)

$$\mathbf{L} = \begin{pmatrix} 0 & \dot{\gamma} & 0 \\ \dot{\gamma} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$\Downarrow$

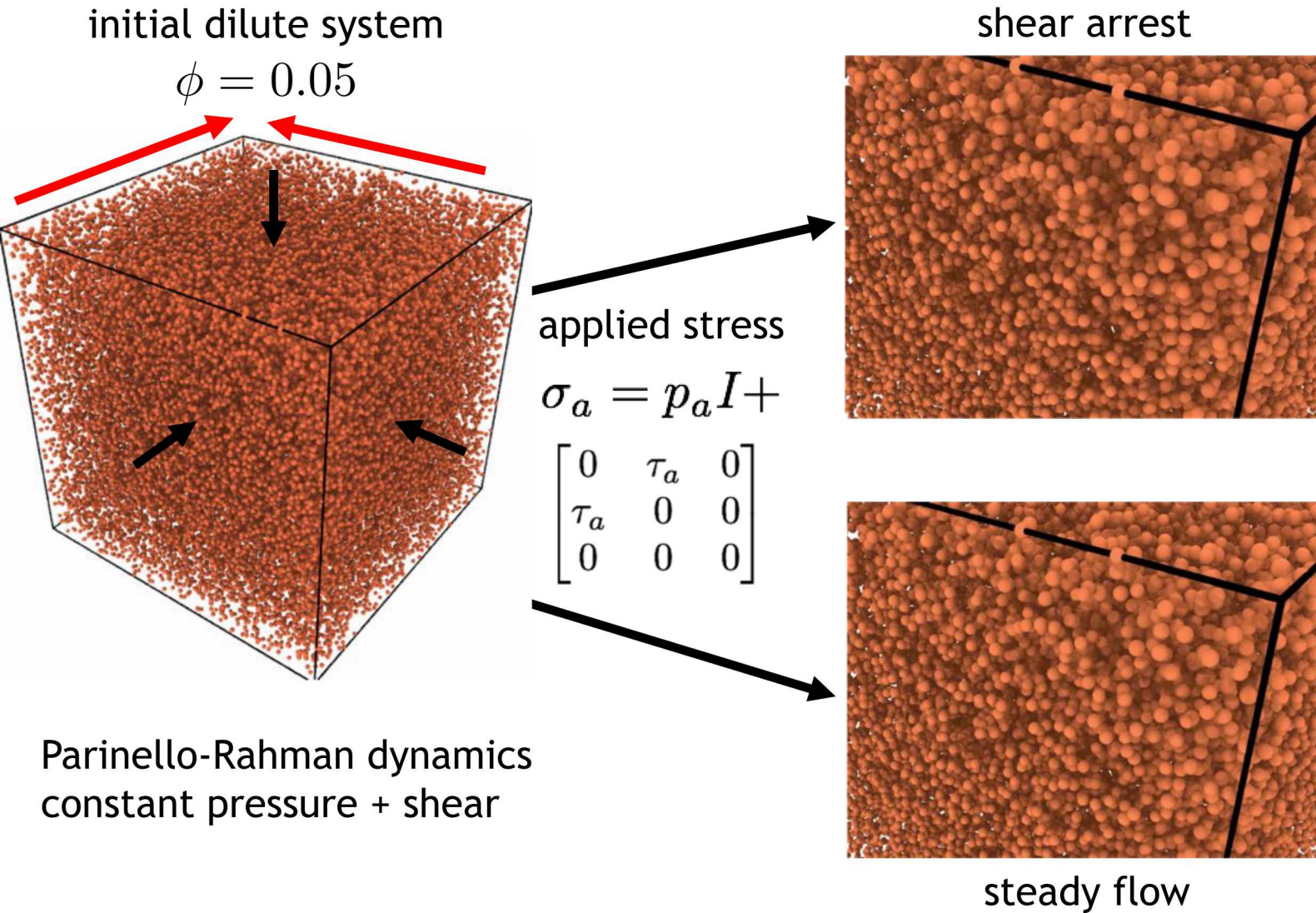
$$\boldsymbol{\sigma} = \begin{pmatrix} p & \tau & 0 \\ \tau & p & 0 \\ 0 & 0 & p \end{pmatrix}$$



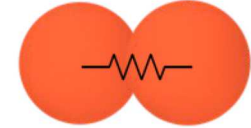
$$\begin{pmatrix} p' & 0 & 0 \\ 0 & p & \tau \\ 0 & \tau & p \end{pmatrix}$$

Depken et al., EPL, 78 (2007)

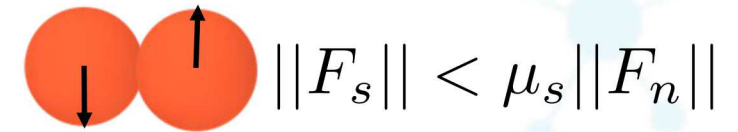
Fully Stress-Controlled Simulations



harmonic contacts



Coulomb microscopic friction



Macroscopic Observables:

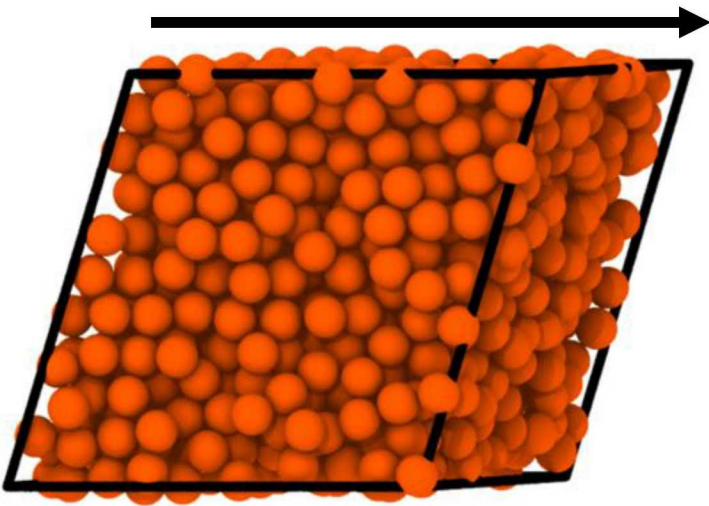
volume fraction: $\phi(t)$

deformation rate (3D): $\mathbf{L}(t)$

internal stress (3D): $\boldsymbol{\sigma}(t)$

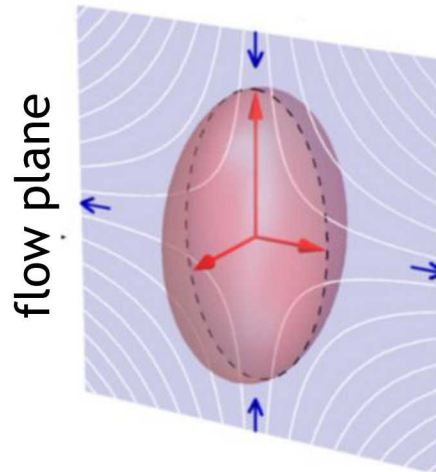
Rheology: Plane Shear Flows

$$\mathbf{L} = \mathbf{D} + \mathbf{W}$$



$$\sigma_a = p_a I + \begin{bmatrix} 0 & \tau_a & 0 \\ \tau_a & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

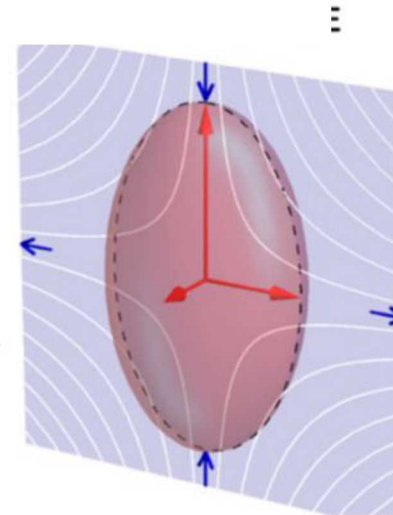
co-directional flow



$$\frac{\sigma}{|\sigma|} = \frac{\mathbf{D}}{|\mathbf{D}|}$$

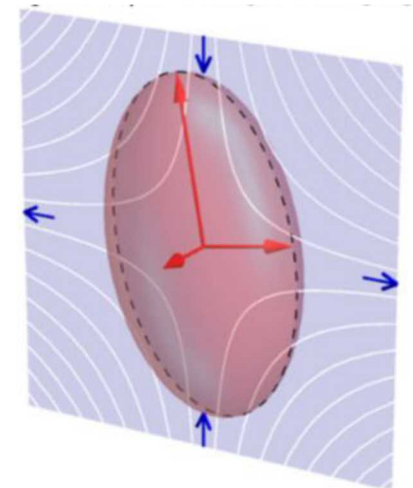
principal directions
of stress and strain rate
tensors coincide

co-axial flow

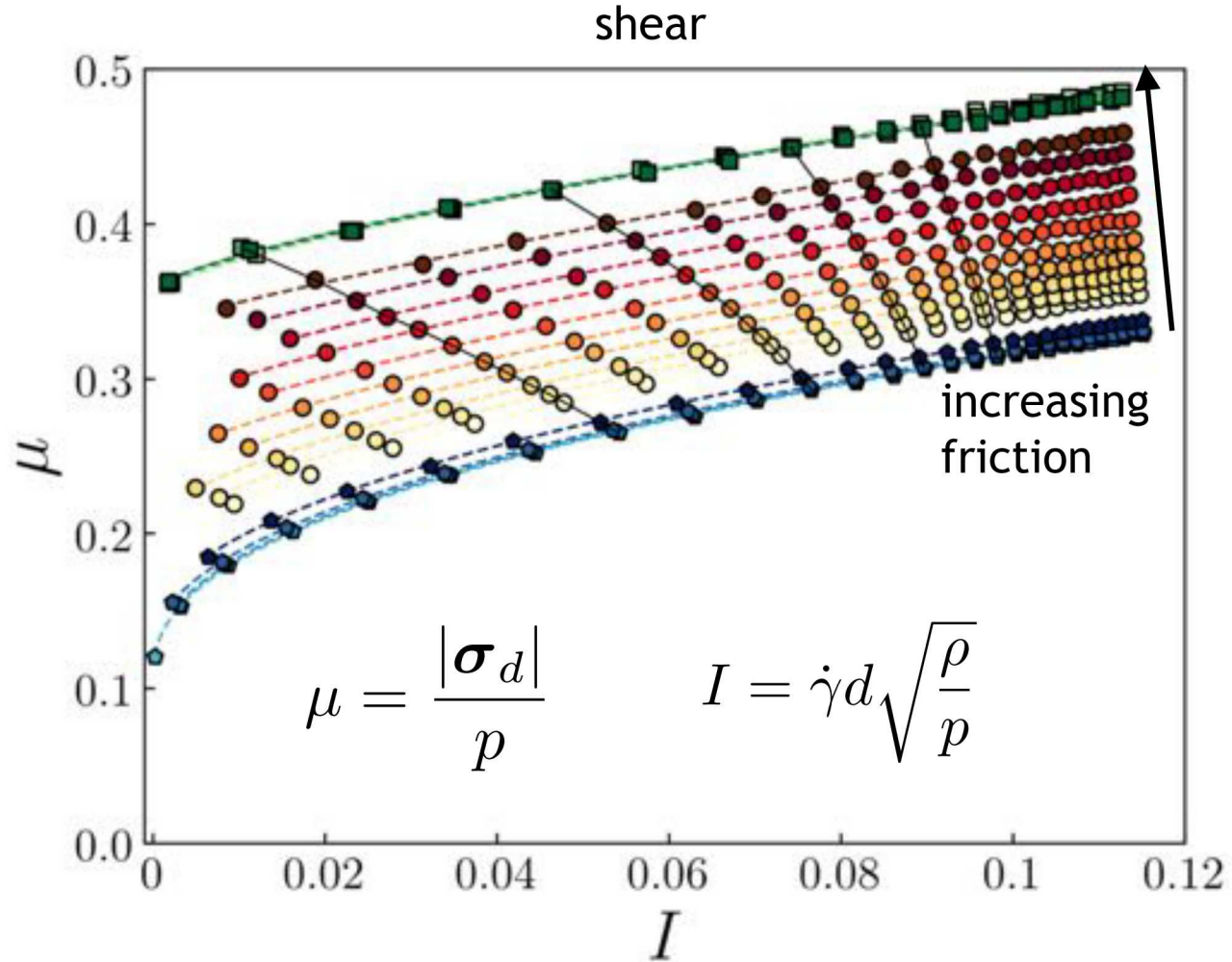


principal directions
of stress and strain rate
tensors do not coincide

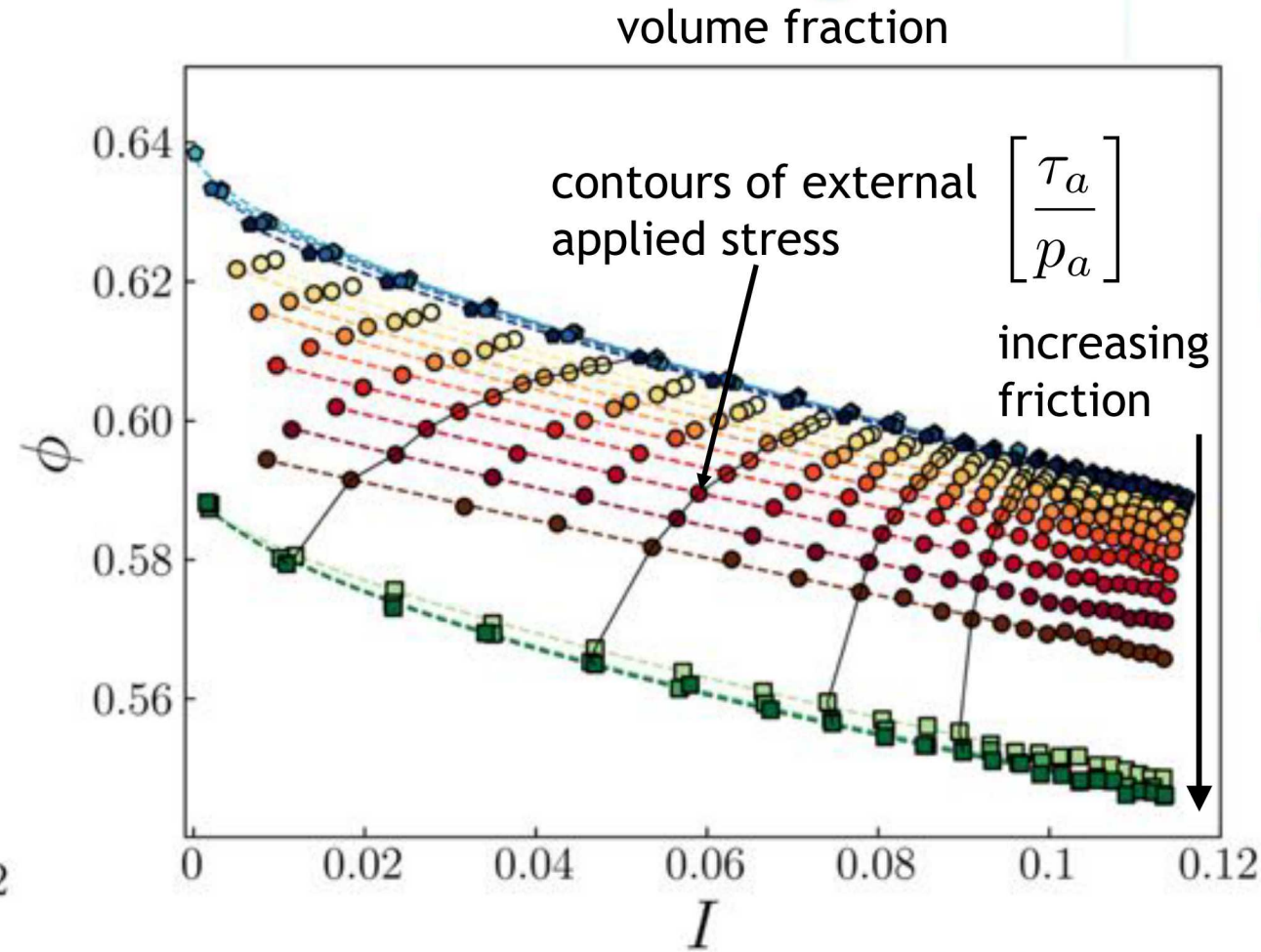
complex flow



Steady-State Rheology: Shear

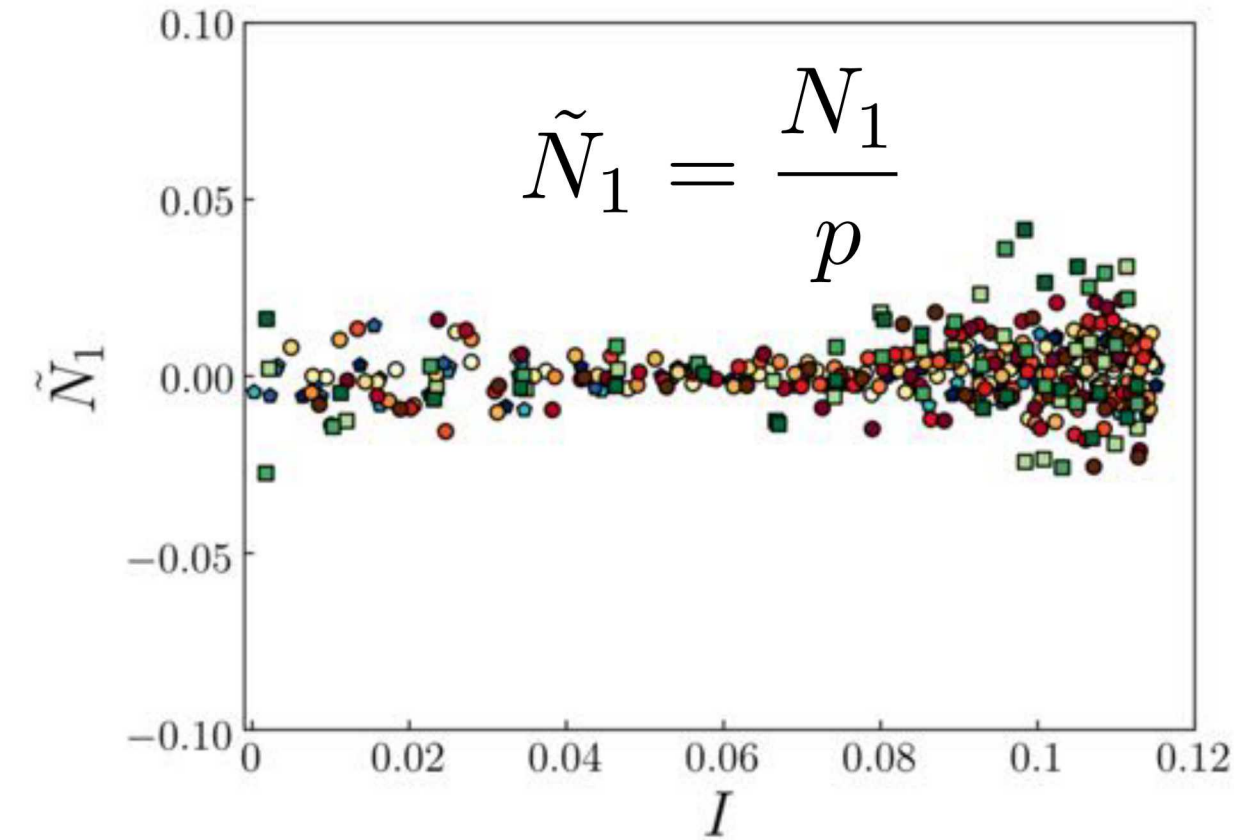


$$\mu = \mu_0 + aI^\alpha$$



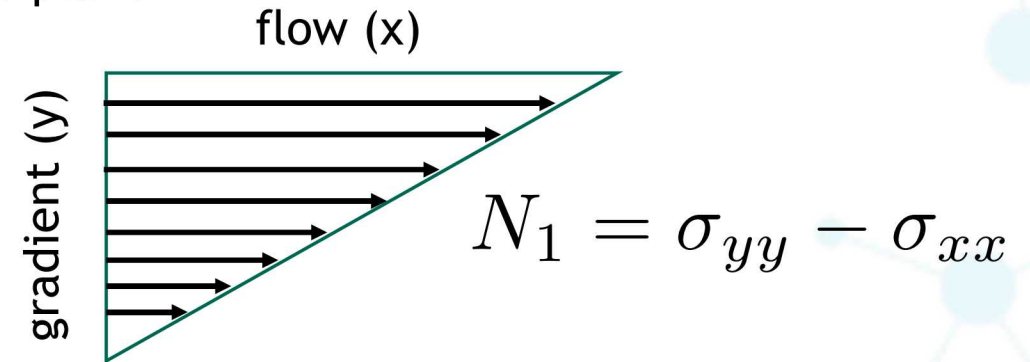
$$\phi = \phi_0 - bI^\beta$$

Steady-State Rheology: Co-axial Flow

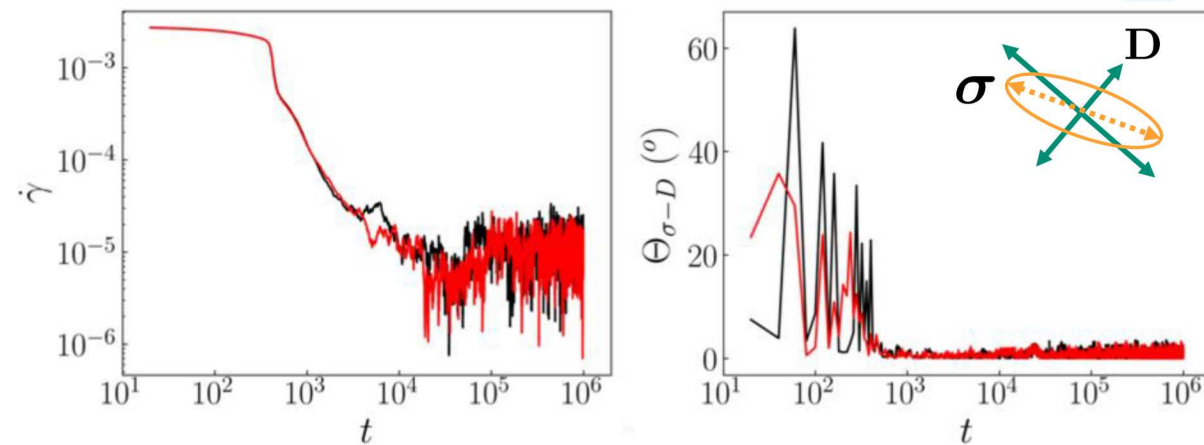


granular flows in simple shear are co-axial

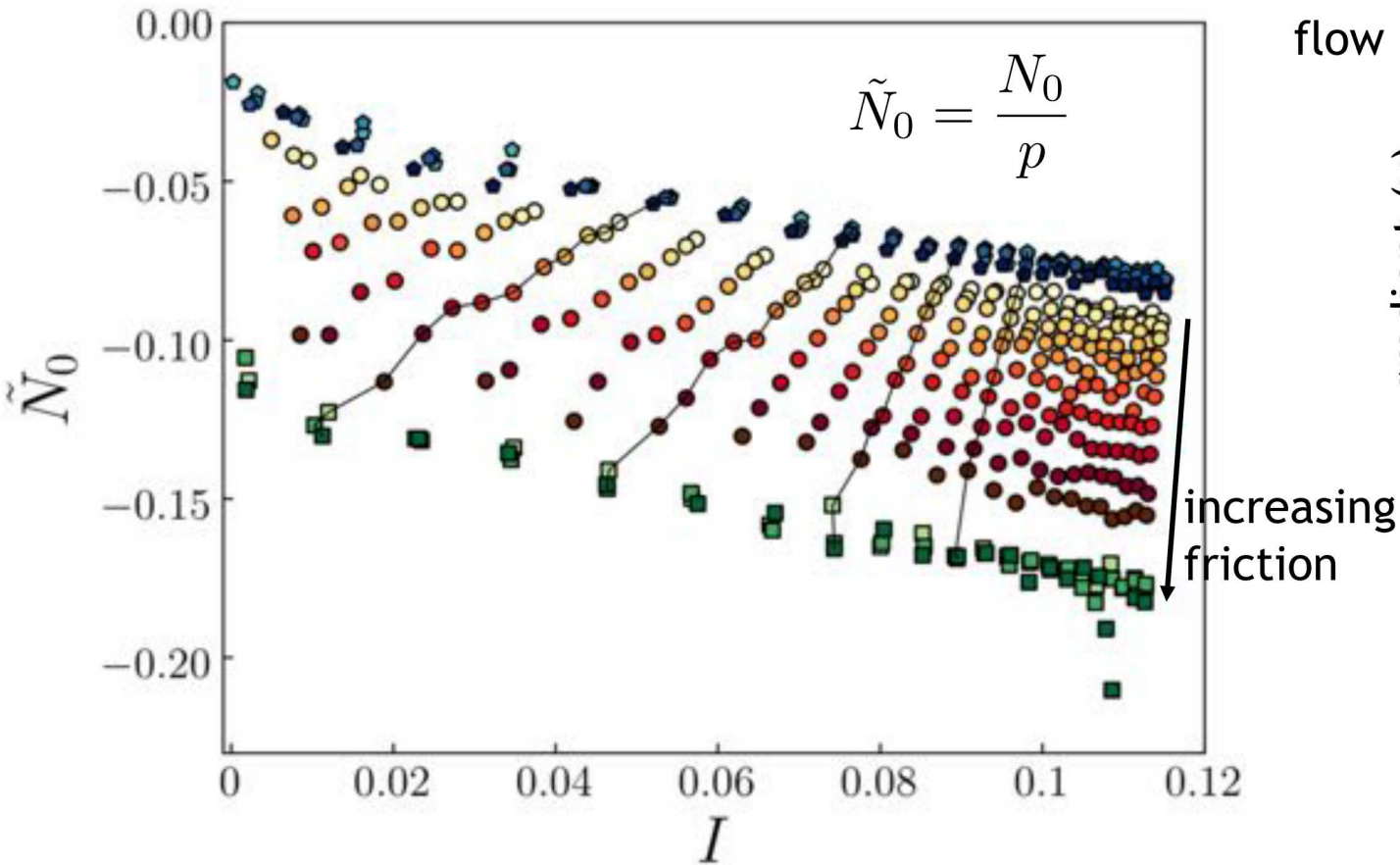
flow plane



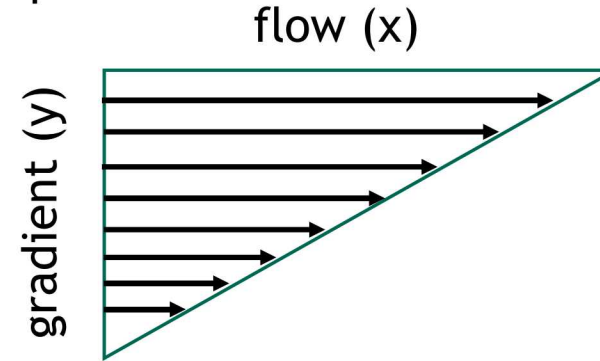
steady flow evolution



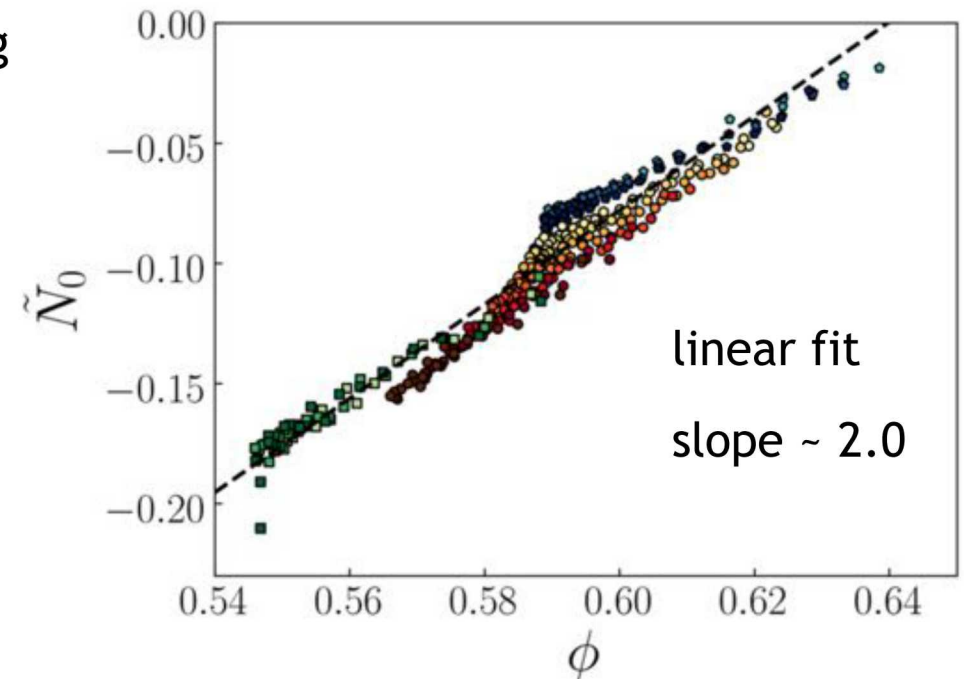
Steady-State Rheology: Co-directional Flow?



flow plane



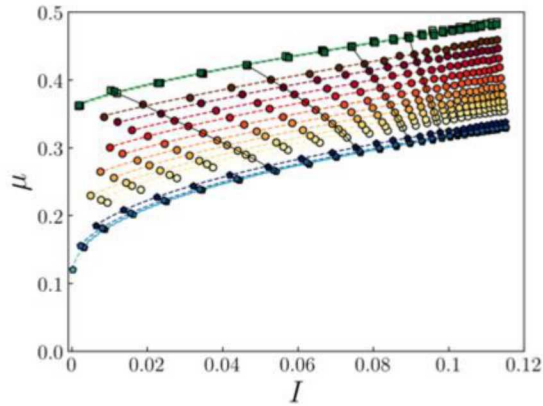
$$N_2 = \sigma_{zz} - \sigma_{yy}$$
$$N_0 = N_2 + \frac{N_1}{2}$$



granular flows in planar shear are not co-directional

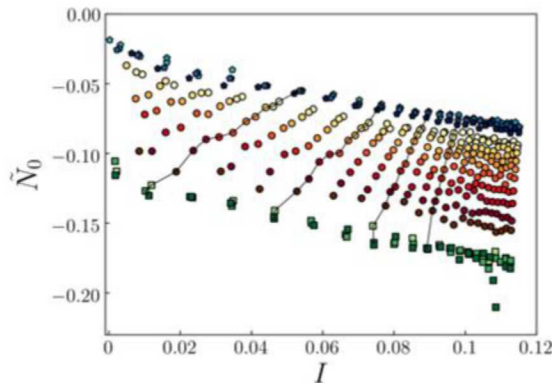
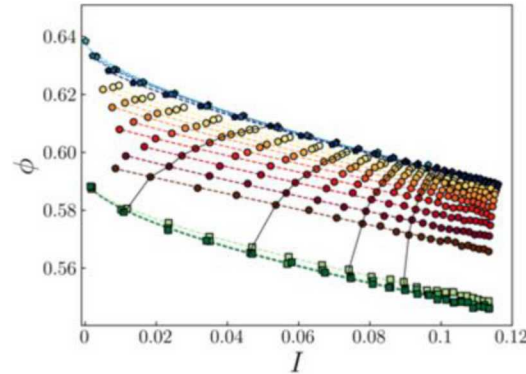
more compaction in the shear plane than normal to it

Conclusions & Outlook



stress tensor in
planar xy-shear

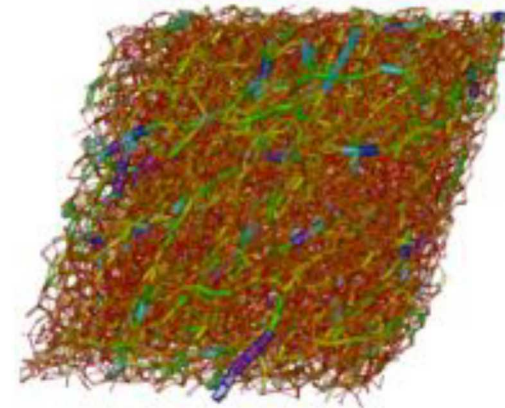
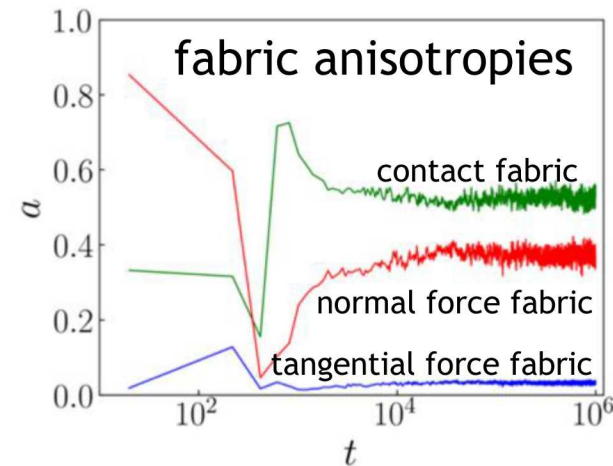
$$\sigma = \begin{pmatrix} p & \tau & 0 \\ \tau & p & 0 \\ 0 & 0 & p' \end{pmatrix} \quad p' < p$$



flow functions
in dense granular flows

$$\mu(I) \quad \phi(I) \quad \tilde{N}_0(I)$$

- How about non-planar shear flows?
Triaxial compression/extension?
Nature of stress tensor in complex loading scenarios?
- Correlate evolution of internal fabric to the normal stress difference for micromechanical constitutive modeling



Srivastava et al., arXiv (online on 03/05/19)
Srivastava et al., Phys. Rev. Lett., 122 (2019)