

Uncertainty Limits in Raman Derived Values of Temperature and Stress



PRESENTED BY

Elbara Ziade, 9144

March 4th 2018

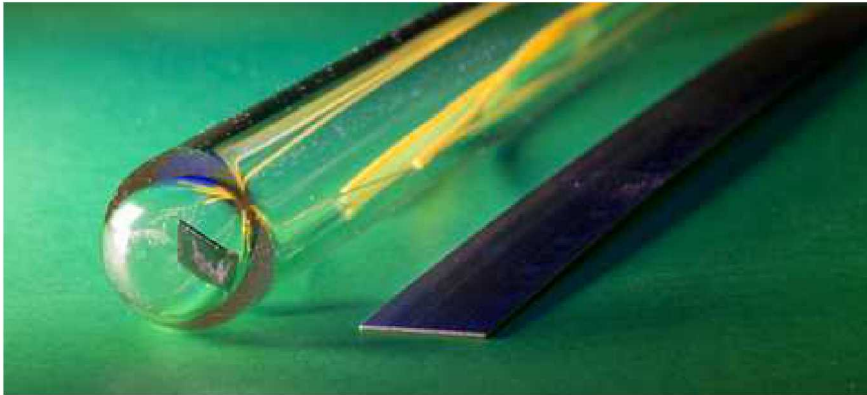


Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

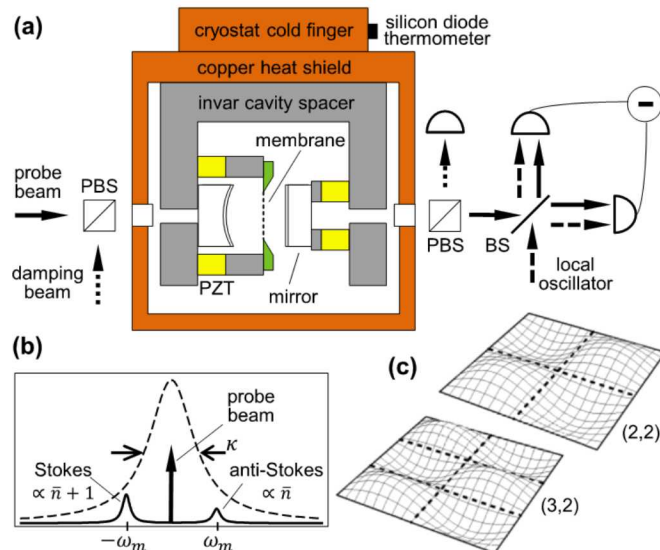
- 1. Physics of the Raman Measurement**
- 2. Voigt Function**
- 3. Traceability to SI**
- 4. Uncertainty in Raman data fitting (Temperature)**
- 5. Uncertainty in Spectrometer calibration**

3 Impact of Raman Microscopy

NIST-on-a-chip: Photonic Thermometry



<https://www.nist.gov/pml/nist-chip-photonic-sensors-temperature-and-light>

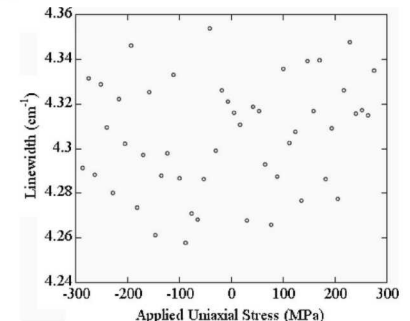
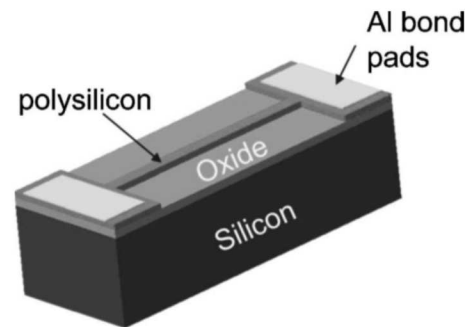


Purdy, T. P., Yu, P. L., Kampel, N. S., Peterson, R. W., Cicak, K., Simmonds, R. W., & Regal, C. A. (2015). Optomechanical Raman-ratio thermometry. *Physical Review A*, 92(3), 031802.

Residual Stress in Additive Manufactured Components



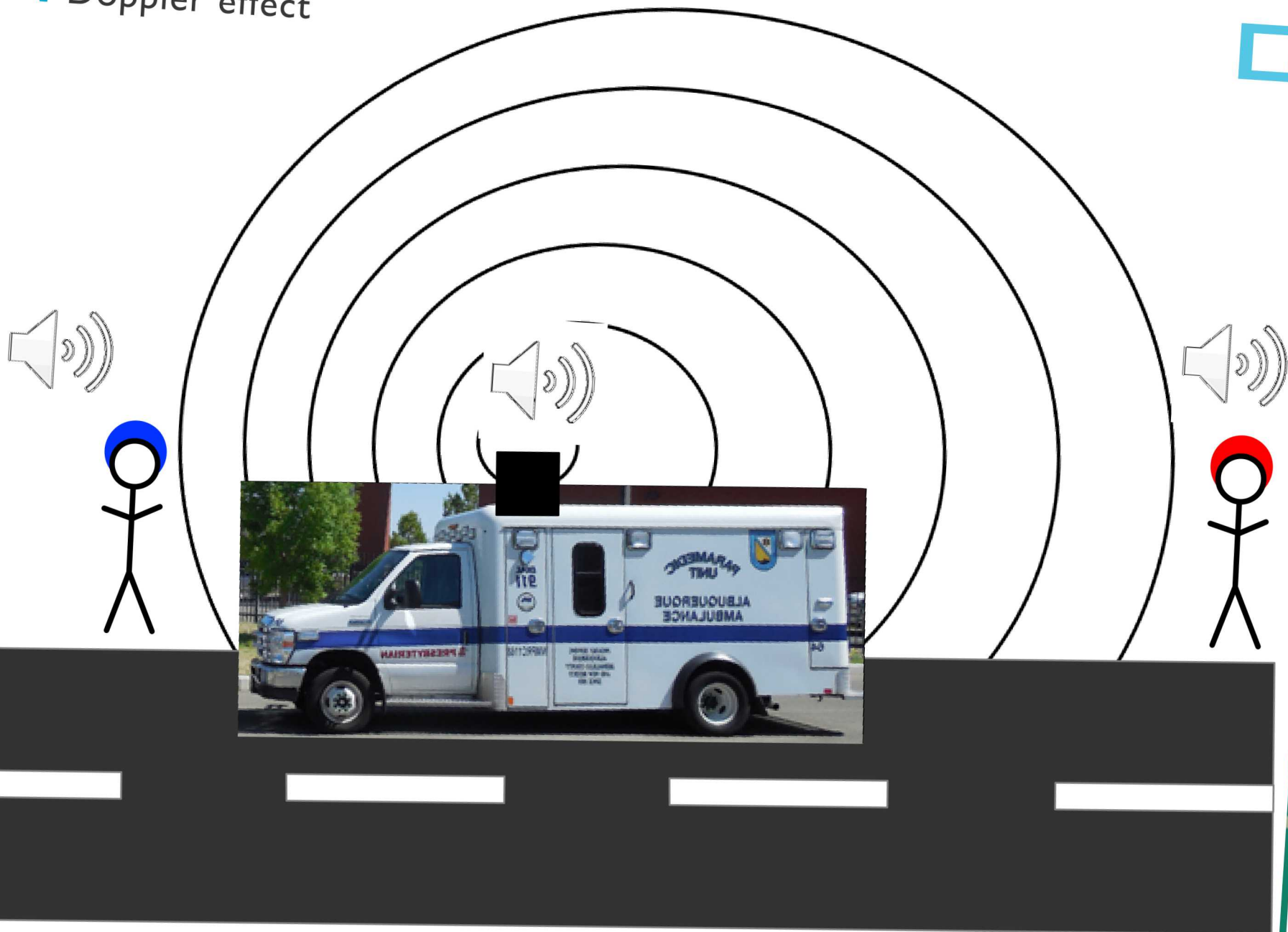
Photo from GE Arcam EBM Ti6Al4V brochure



NISTIR 8036

Abel, M. R., Graham, S., Serrano, J. R., Kearney, S. P., & Phinney, L. M. (2007). Raman thermometry of polysilicon microelectro-mechanical systems in the presence of an evolving stress. *Journal of Heat Transfer*, 129(3), 329-334.

4 Doppler effect



Rayleigh:

Photon reflects with
same energy

$$E_0 = \hbar\omega_0$$

Anti-Stokes:

photon gains
energy from
lattice

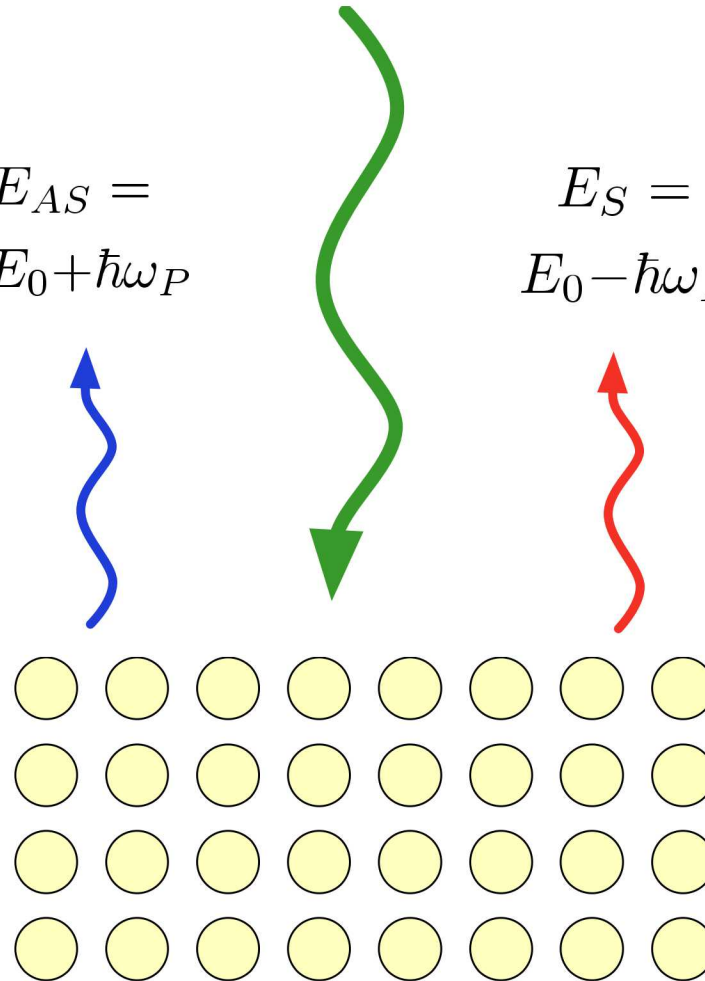
$$E_{AS} = E_0 + \hbar\omega_P$$

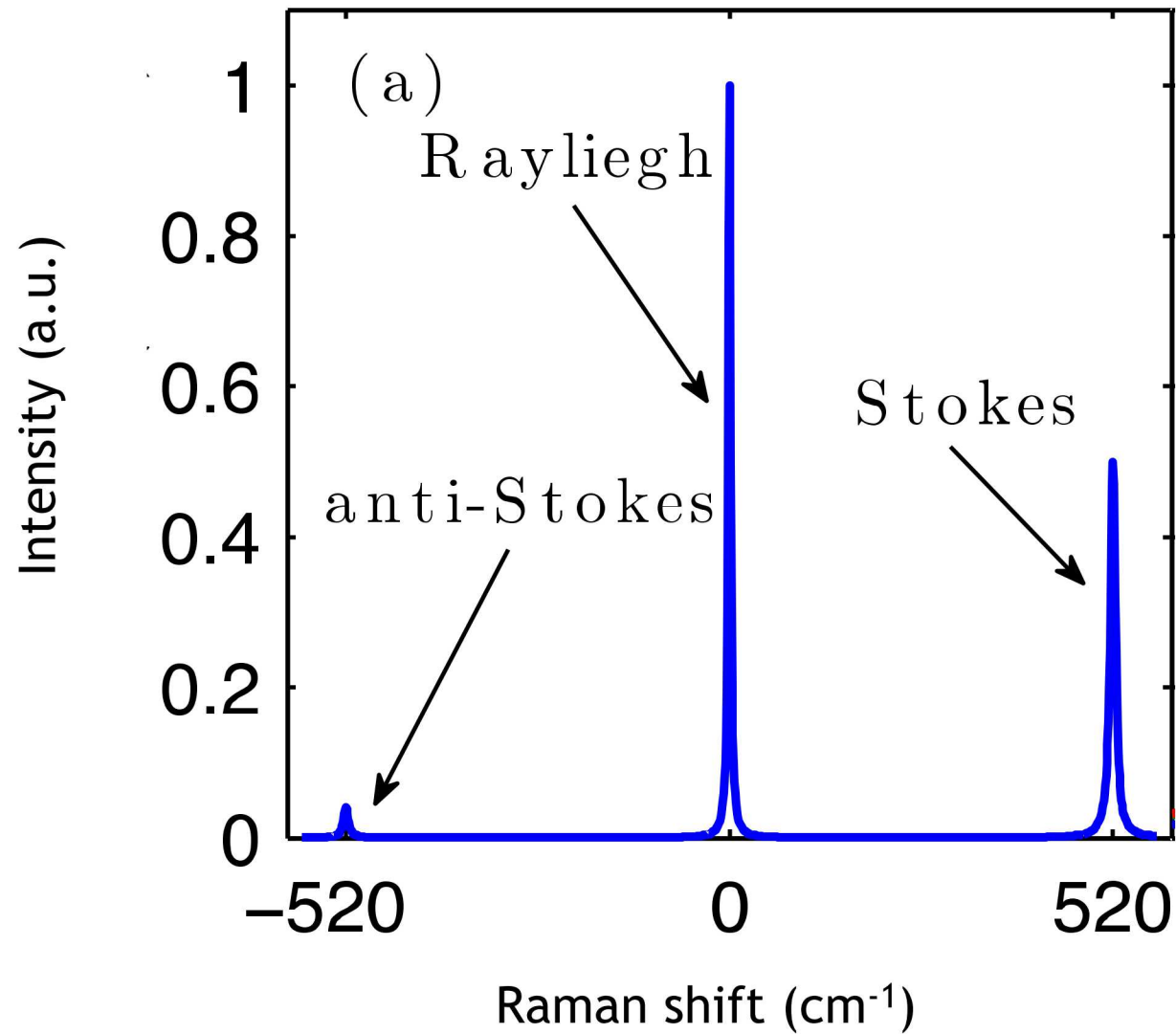
$$E_S =$$

$$E_0 - \hbar\omega_P$$

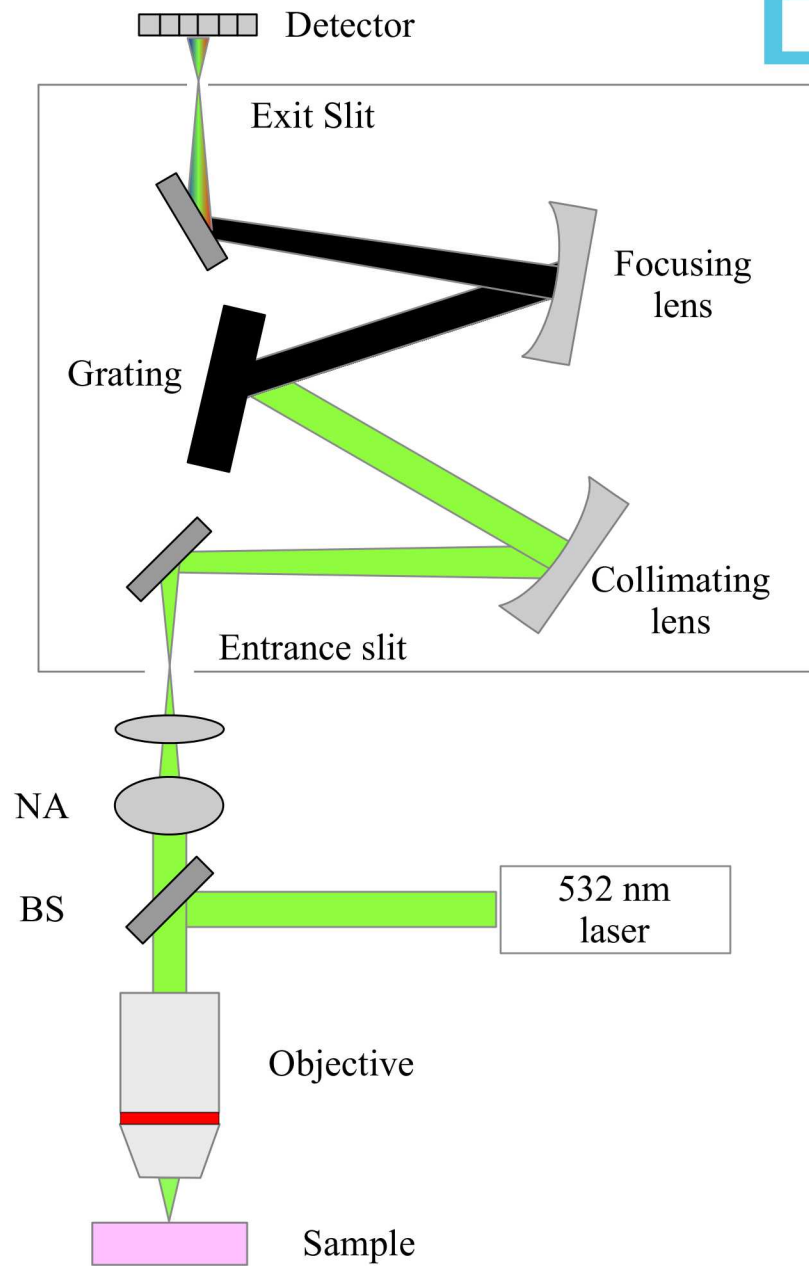
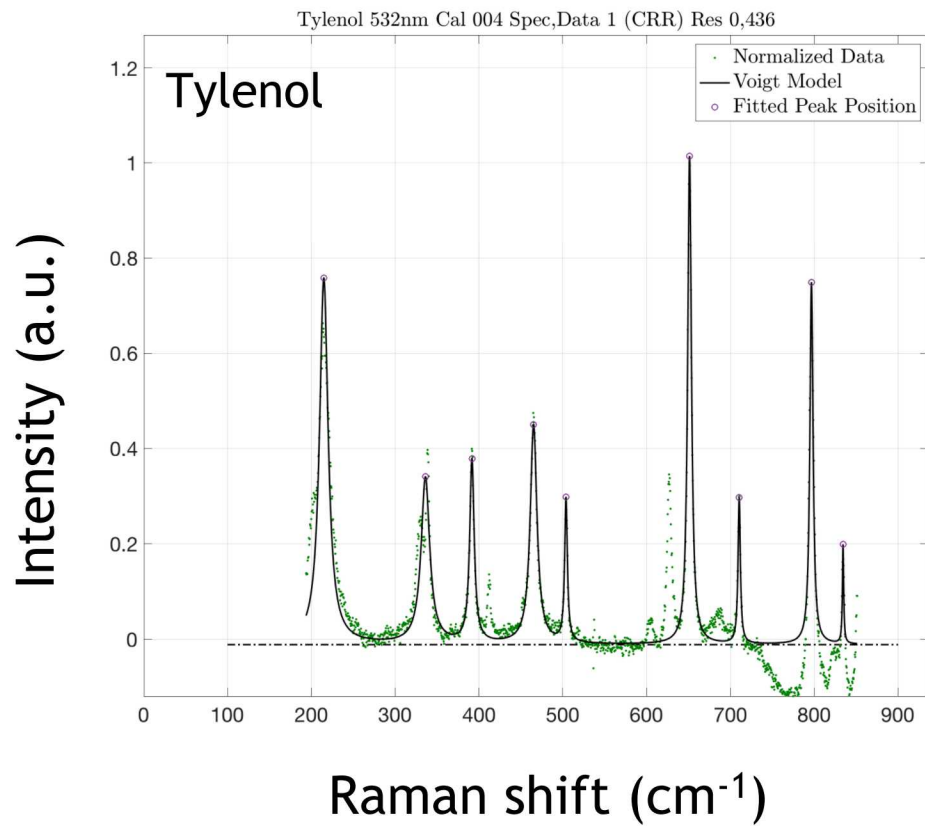
Stokes:

photon loses
energy to lattice



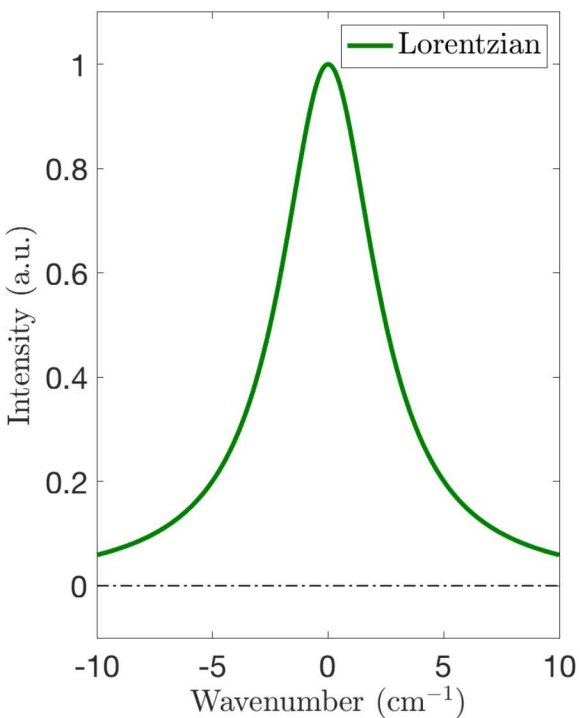


7 Raman Setup

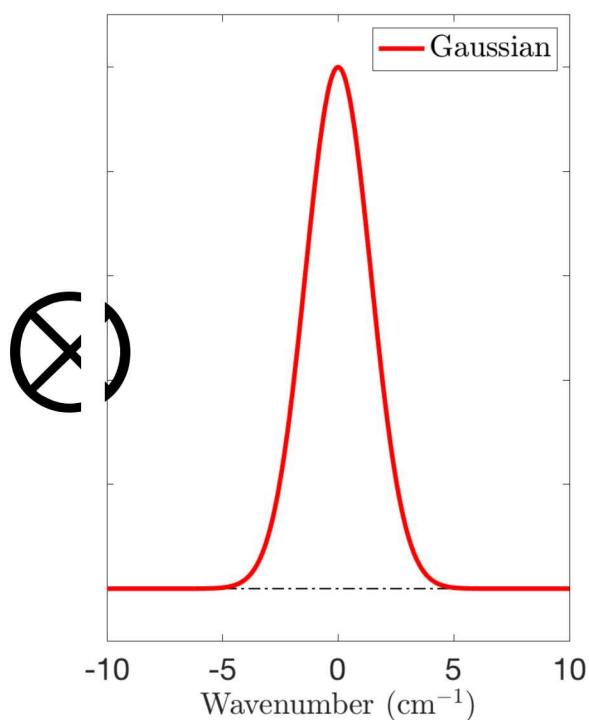


8 Voigt: Gaussian Convolution with Lorentzian

Pure Raman signal:
Lorentzian

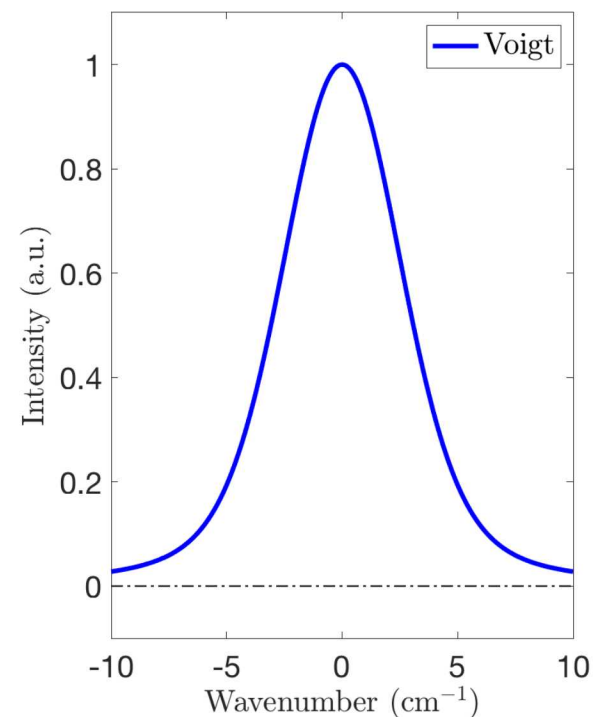


Gaussian noise
from measurement



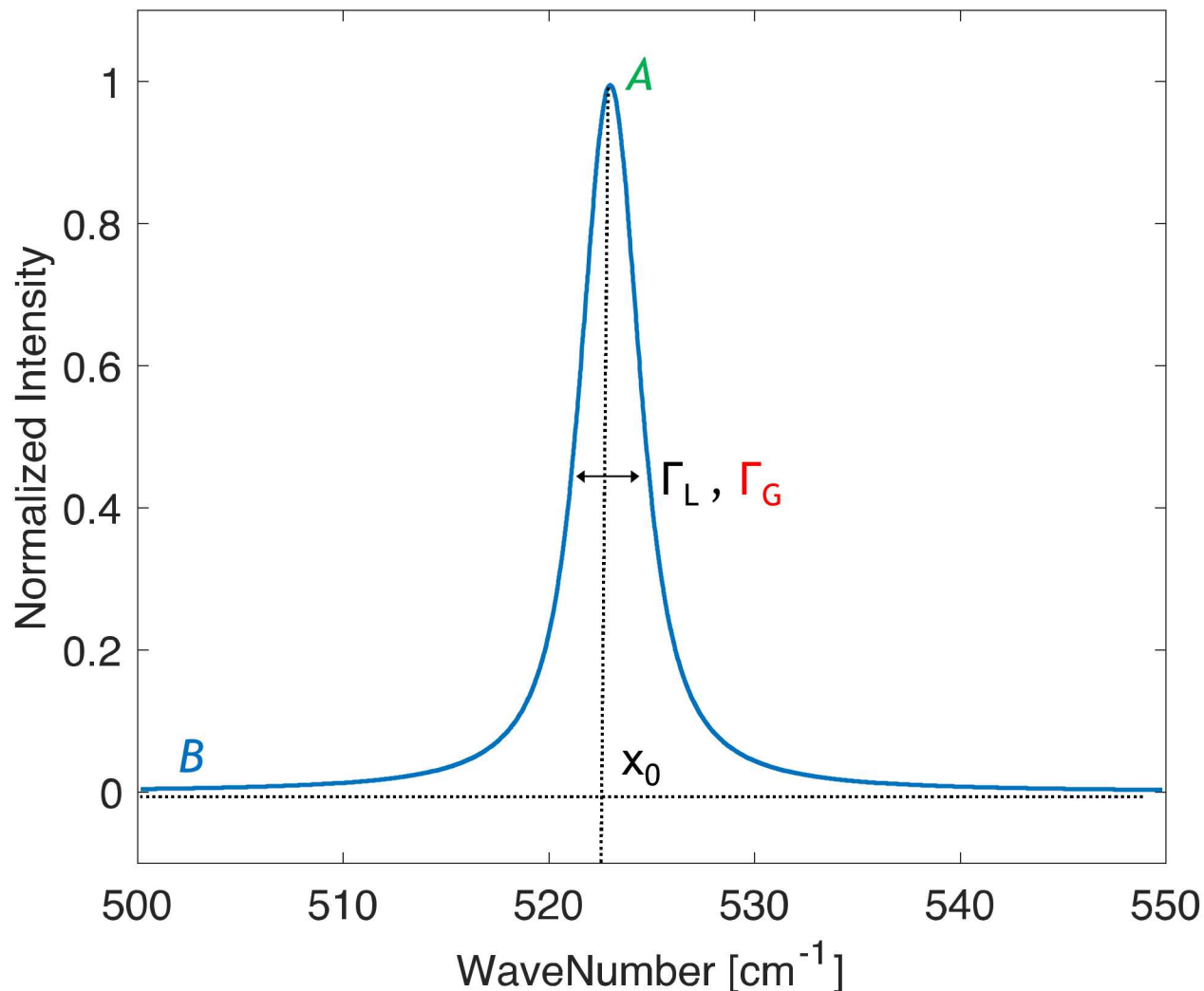
=

Measured signal:
Voigt



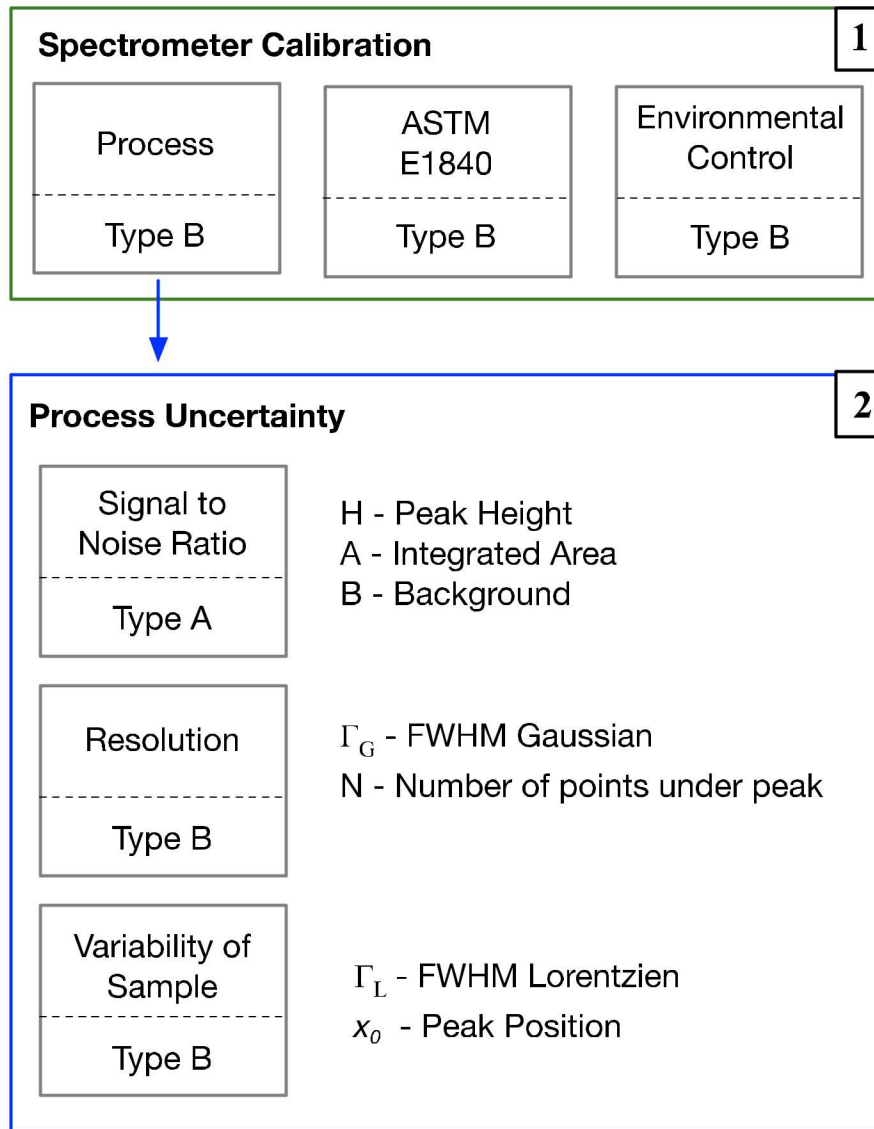
9 Voigt function: Gaussian & Lorentzian convolution

$$V(x) = f(\Gamma_L, \Gamma_G, x_0, A, B)$$



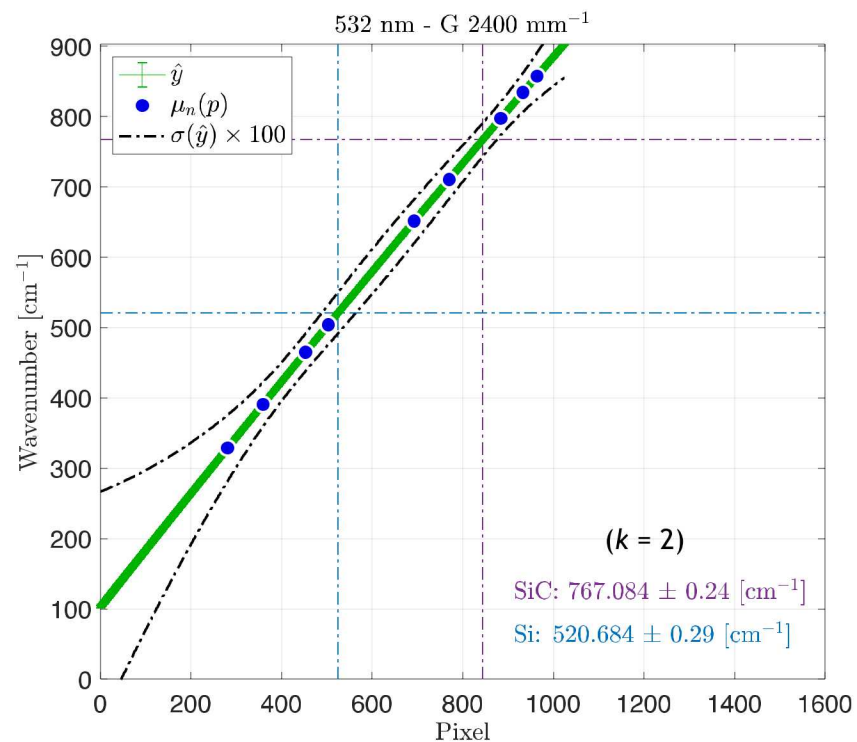
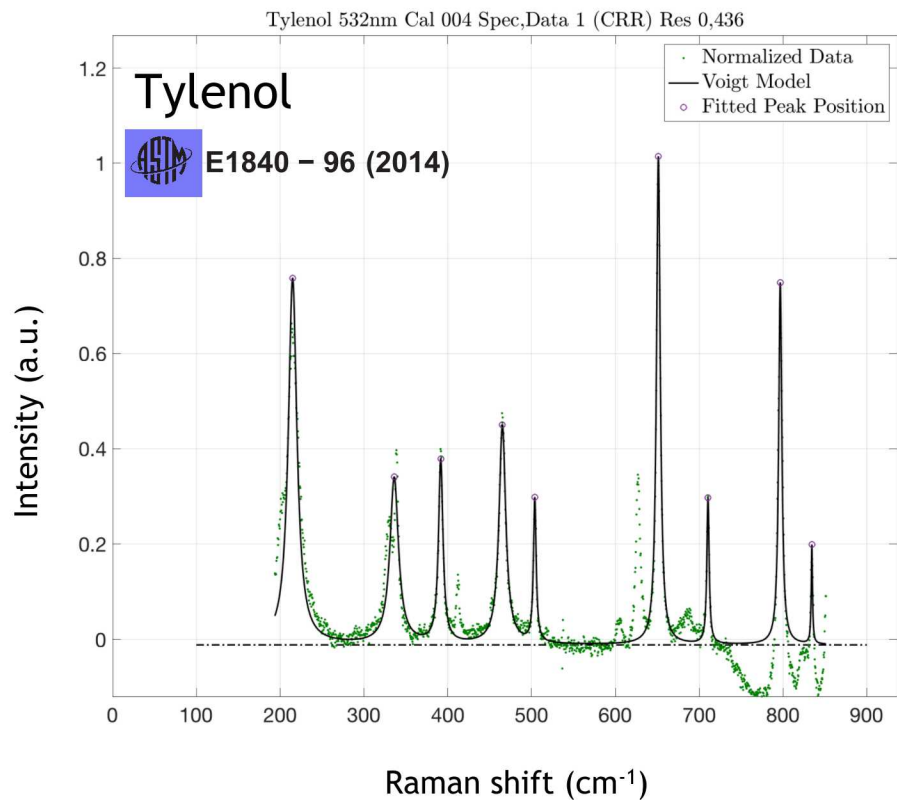
- Γ_L - Lorentzian FWHM
- x_0 - Peak Position
- Γ_G - Gaussian FWHM
- A - Integrated area
- B - Background level

Traceability to International System of Units (SI)



What is the lowest achievable uncertainty for:

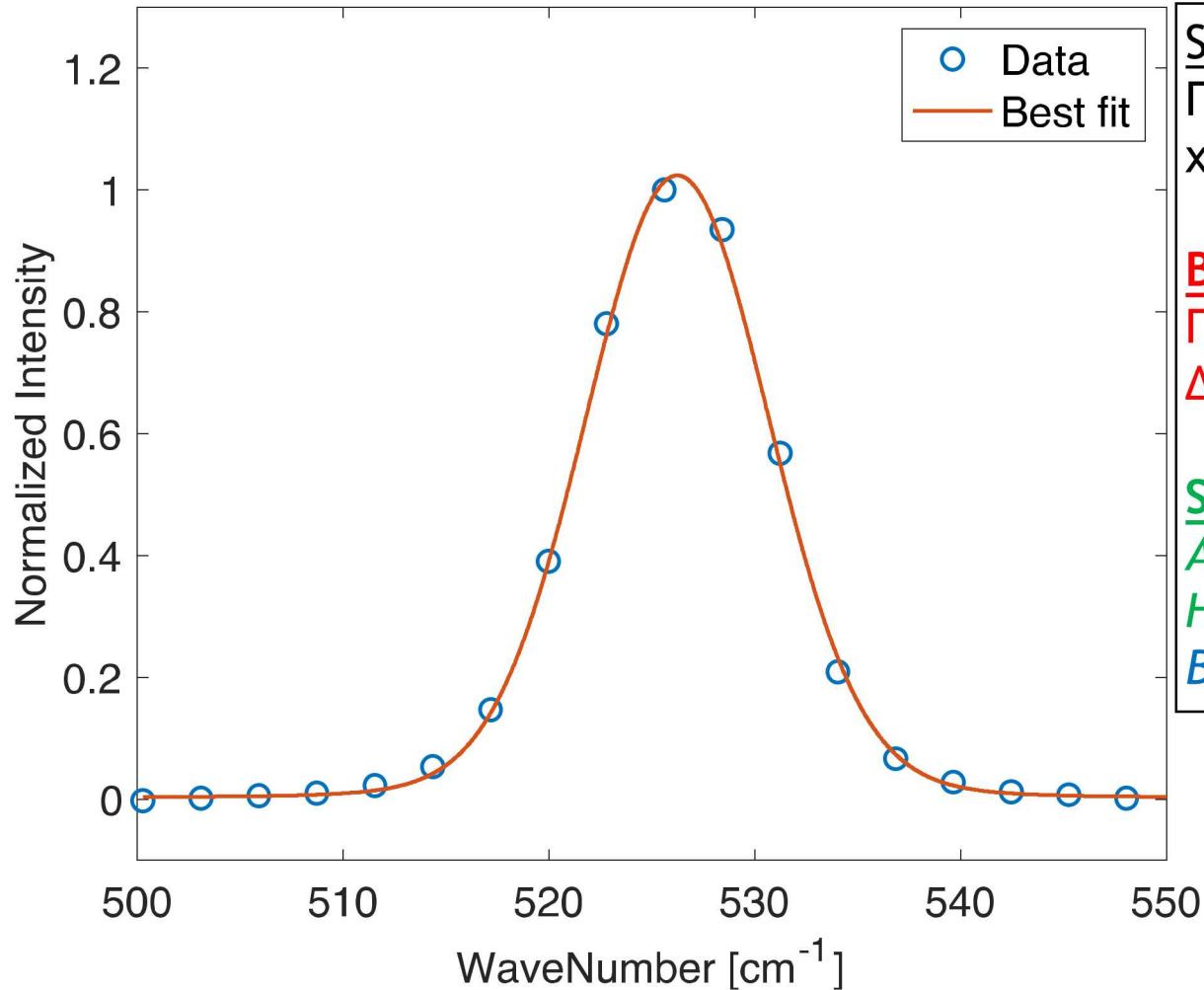
- 1. Relative Peak position for stress and temperature measurements**
- 2. Absolute peak position for stress and temperature measurements**



$$y_n = c_0 + c_1 x_n + c_2 x_n^2$$

where y_n is wavenumber of observation n ; c_0 , c_1 and c_2 are the best estimate fitting constants; and x is the pixel number.

$$V(x) = f(\Gamma_L, \Gamma_G, x_0, A, B)$$



Signal of Interest:

Γ_L - Lorentzian FWHM

x_0 - Peak Position

Binning:

Γ_G - Gaussian FWHM

Δ - Resolution

Signal to Noise Ratio (SNR):

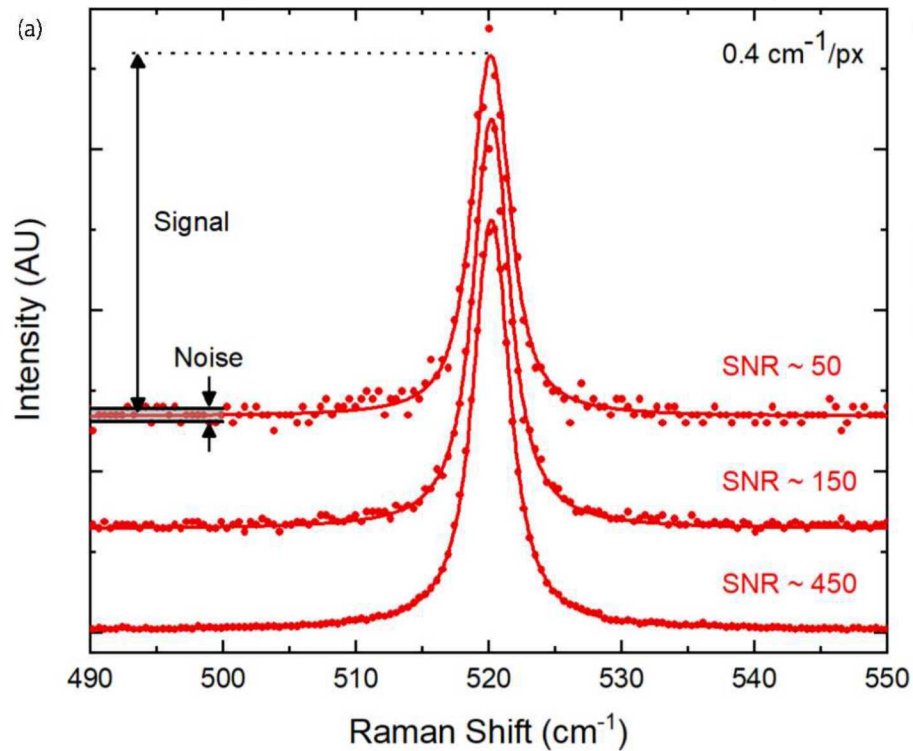
A - Integrated area

H - Peak height

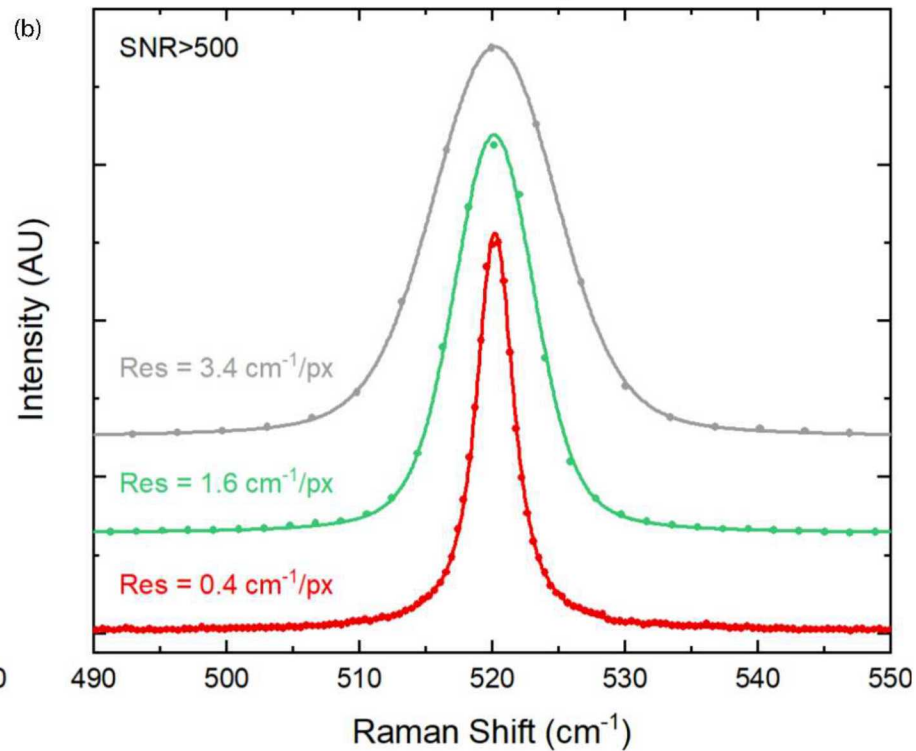
B - Background level



Signal to Noise Ratio (SNR)

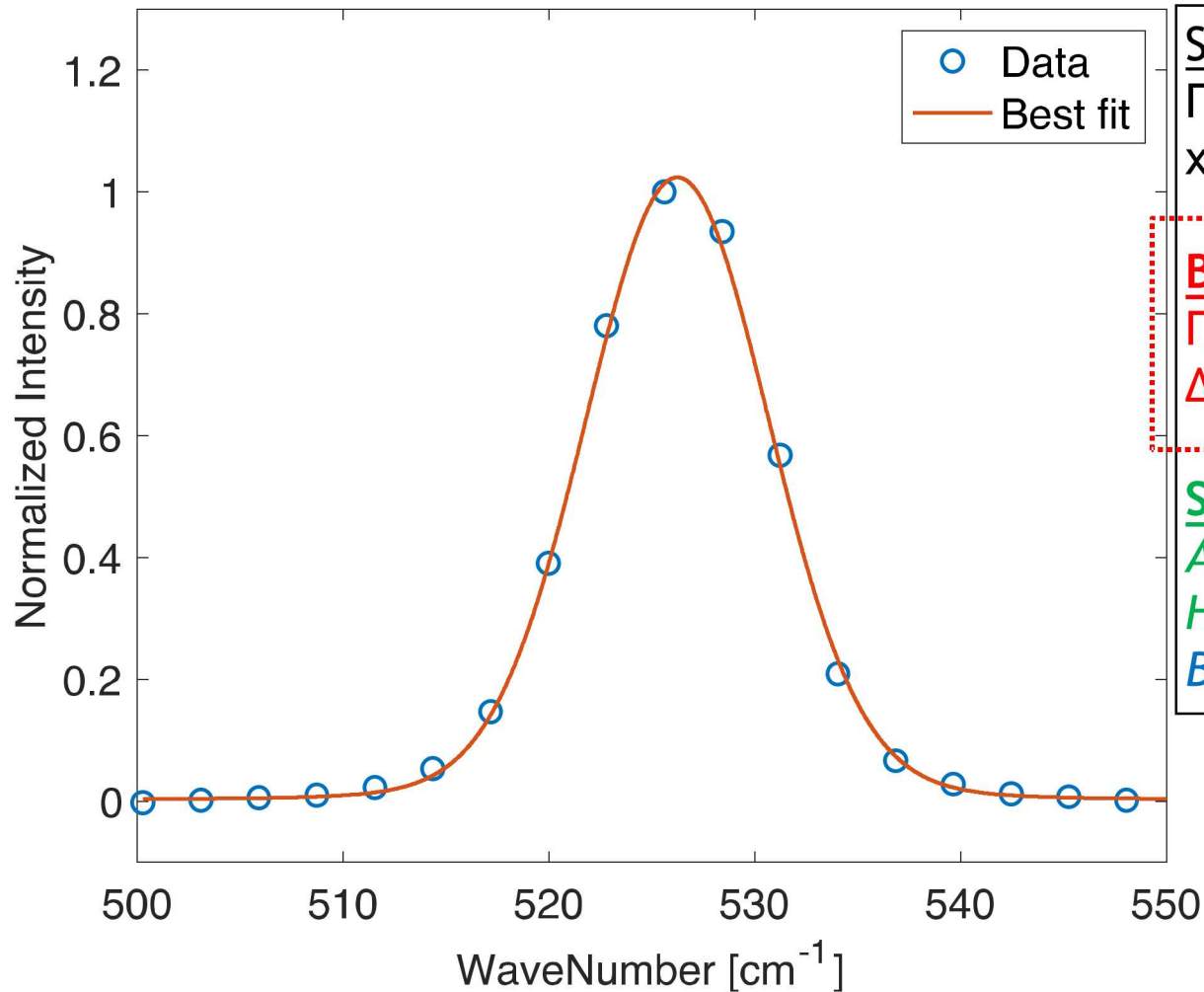


Binning



$$V(x) = f(\Gamma_L, \Gamma_G, x_0, A, B)$$

$$V(x) = f(\Gamma_L, \Gamma_G, x_0, A, B)$$



Signal of Interest:

Γ_L - Lorentzian FWHM

x_0 - Peak Position

Binning:

Γ_G - Gaussian FWHM

Δ - Resolution

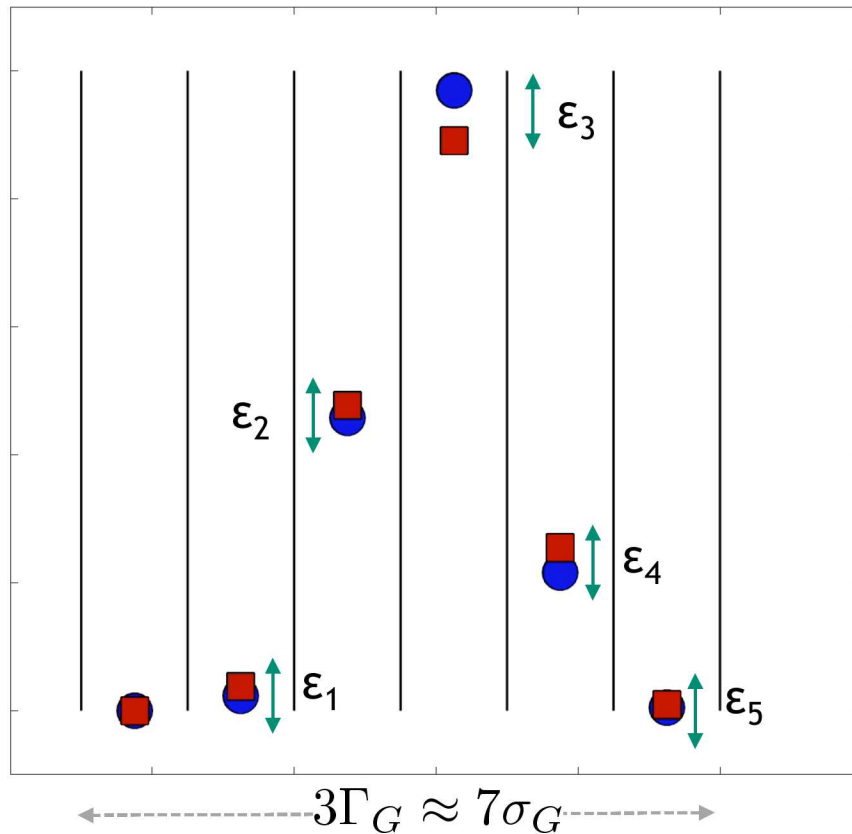
Signal to Noise Ratio (SNR):

A - Integrated area

H - Peak height

B - Background level

N = 6



● $V(x) = v(x)$

True value of Voigt function at position x

■ $V_P(x) = \int_{x-\Delta/2}^{x+\Delta/2} v(x) dx$

Integrated value (measured value)

$$\sigma_{\Delta,V}^2 = \sum_i^N \frac{\epsilon_i - \bar{\epsilon}}{N-1} \approx \frac{1}{(N-1)^3}$$

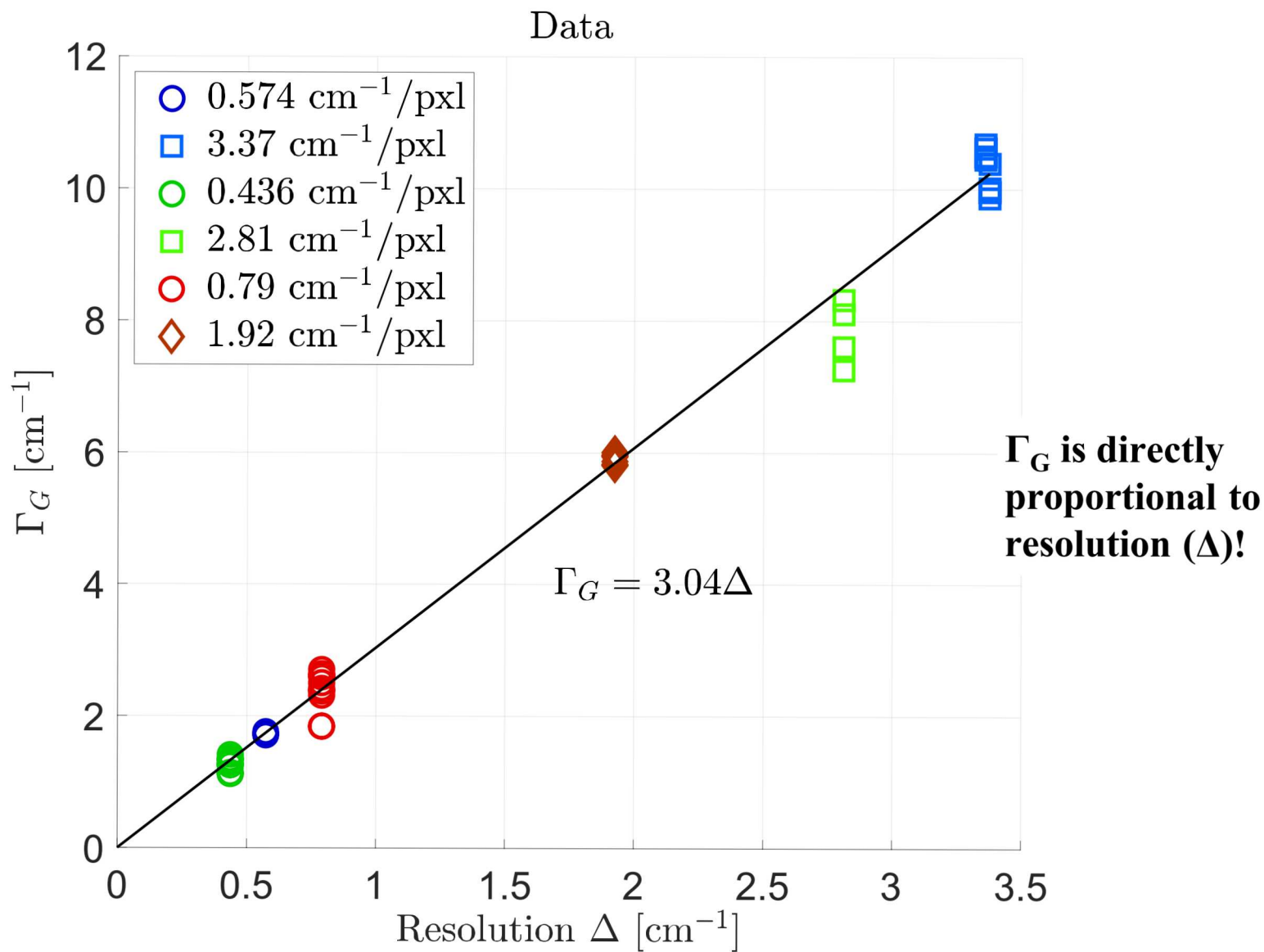
$$x_{\text{start}} = x_0 - 3\Gamma_V(\Gamma_G, \Gamma_L)$$

$$x_{\text{end}} = x_0 + 3\Gamma_V(\Gamma_G, \Gamma_L)$$

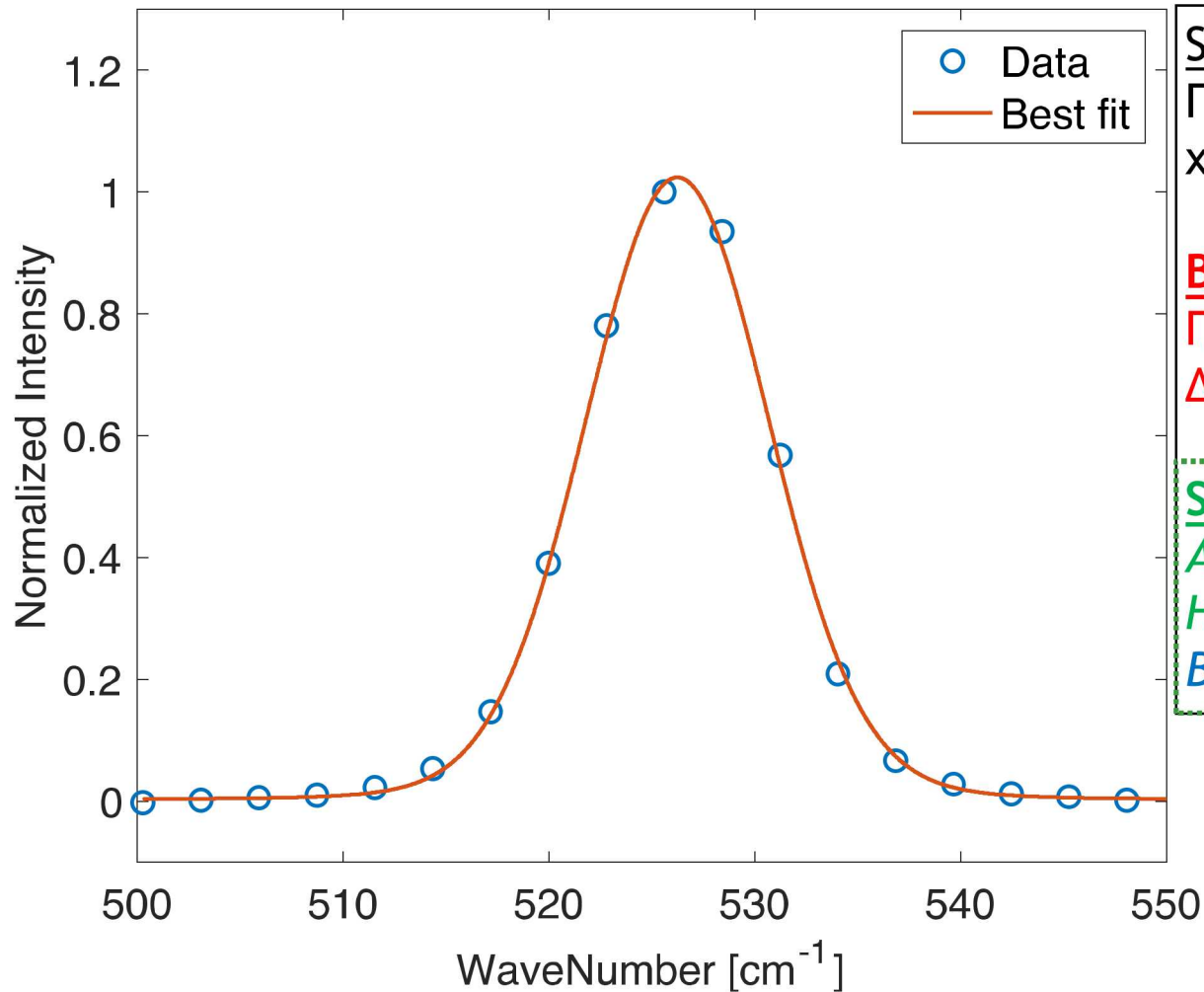
$$N = \frac{3\Gamma_V(\Gamma_G, \Gamma_L)}{\Delta}$$

Convert pixilation error
into wavenumber error

$$\sigma_{\Delta,x}^2 = (\mathbf{J}'\mathbf{J})^{-1} \mathbf{J}'[(1 \cdot \sigma_{\Delta,V} \cdot H)^2] \mathbf{J}(\mathbf{J}'\mathbf{J})^{-1}$$

Binning: $\Gamma_G(\Delta)$ 

$$V(x) = f(\Gamma_L, \Gamma_G, x_0, A, B)$$



Signal of Interest:

Γ_L - Lorentzian FWHM

x_0 - Peak Position

Binning:

Γ_G - Gaussian FWHM ✓

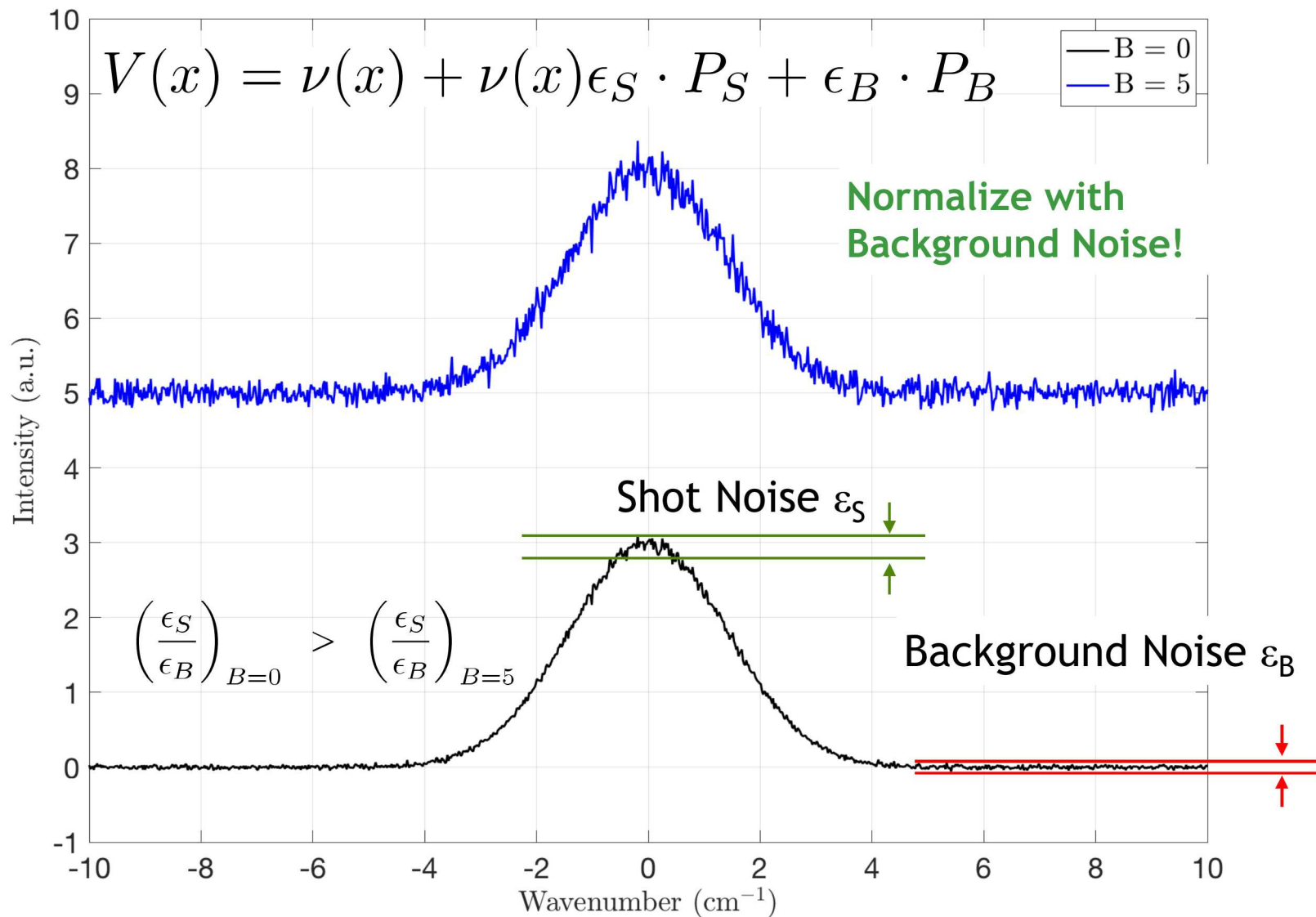
Δ - Resolution

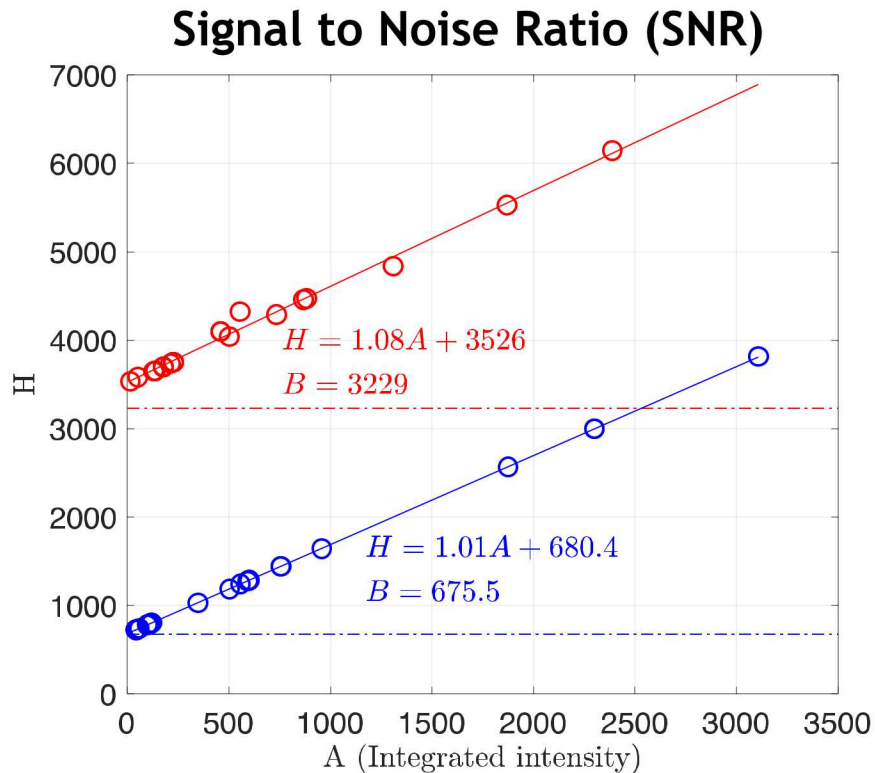
Signal to Noise Ratio (SNR):

A - Integrated area

H - Peak height

B - Background level





$$\text{SNR} = H/B$$

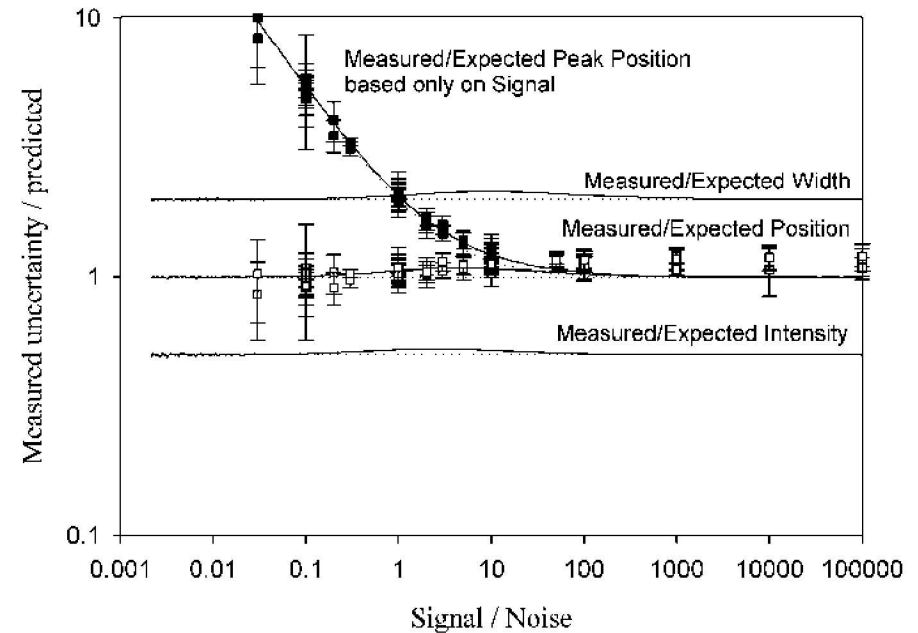
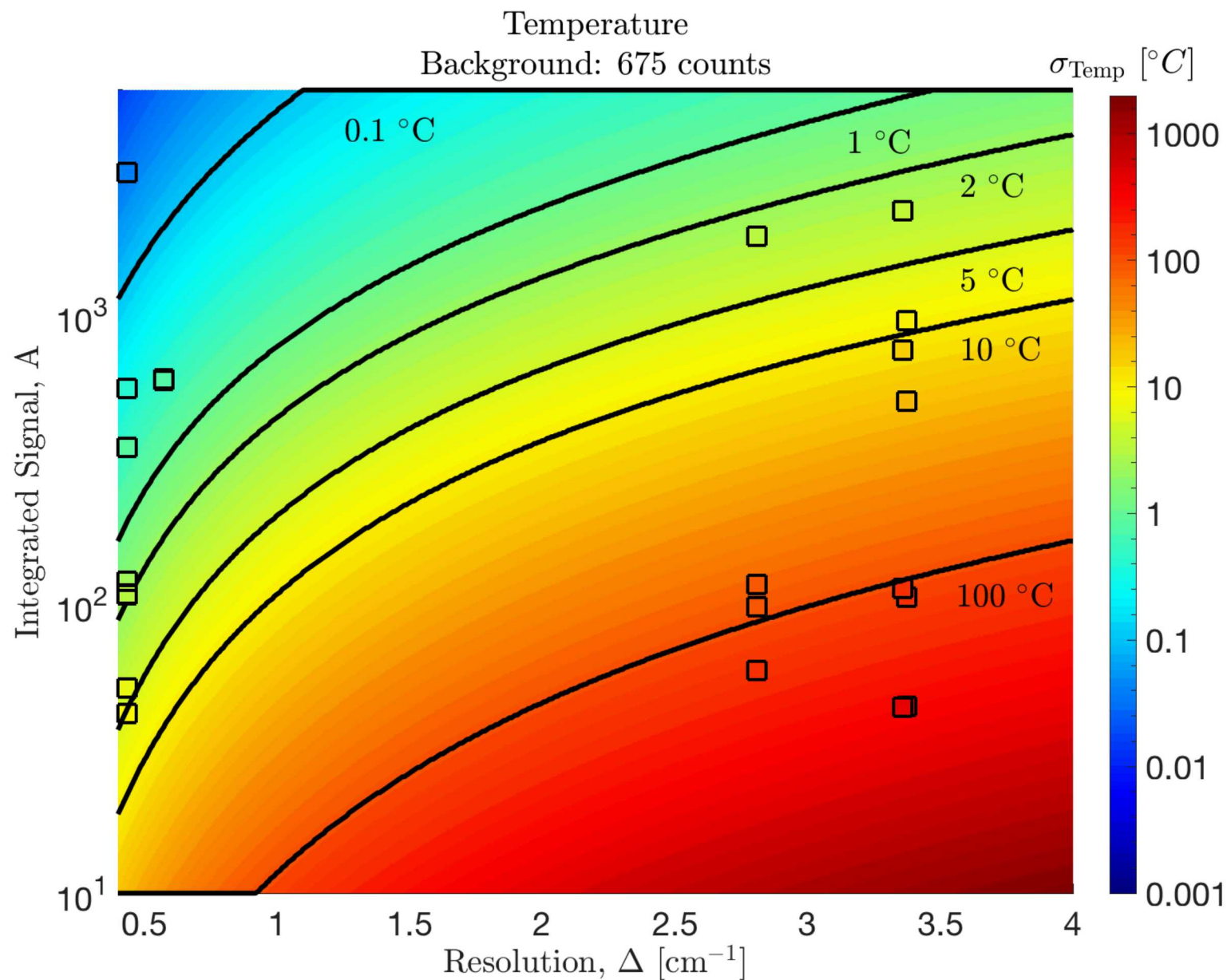
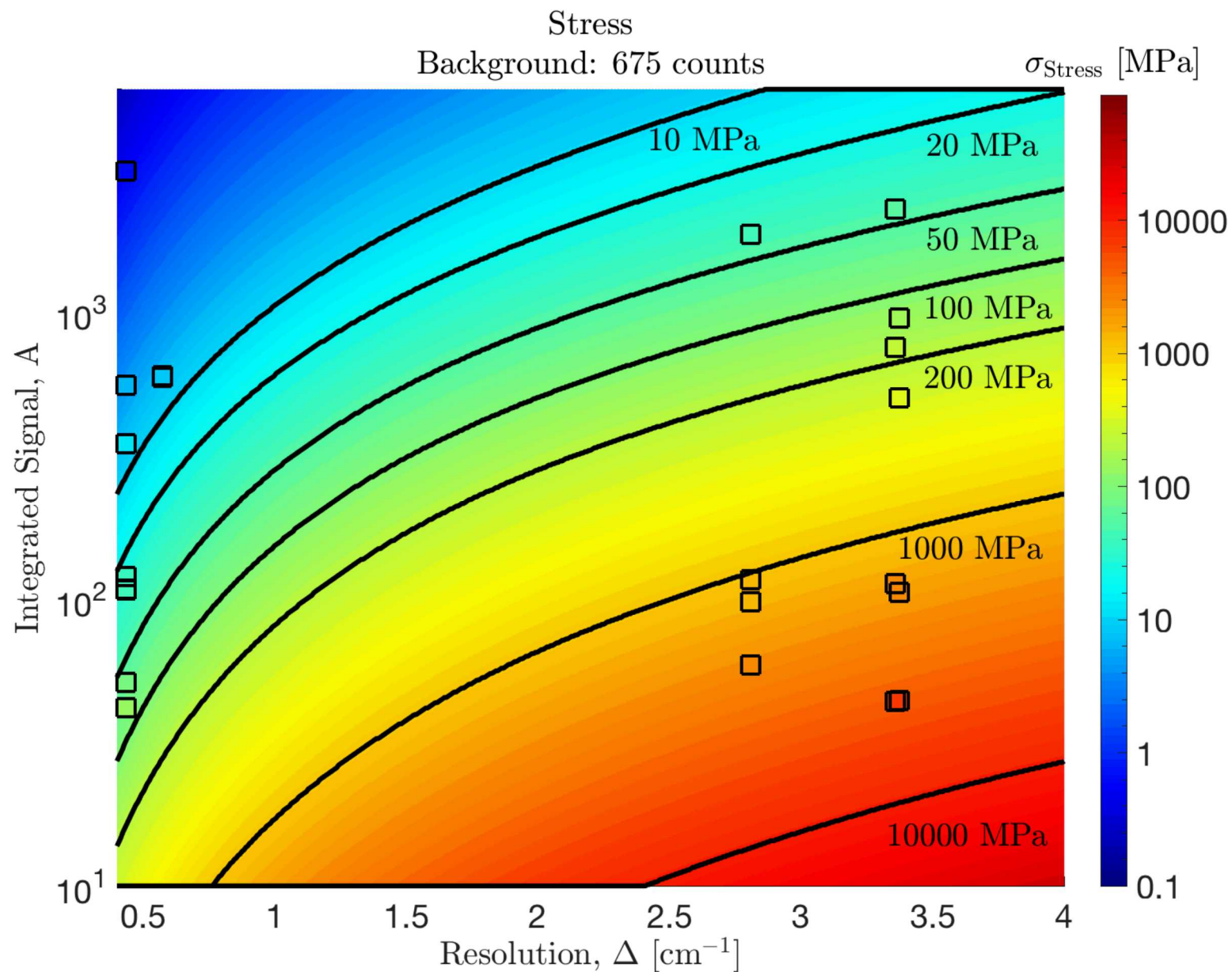


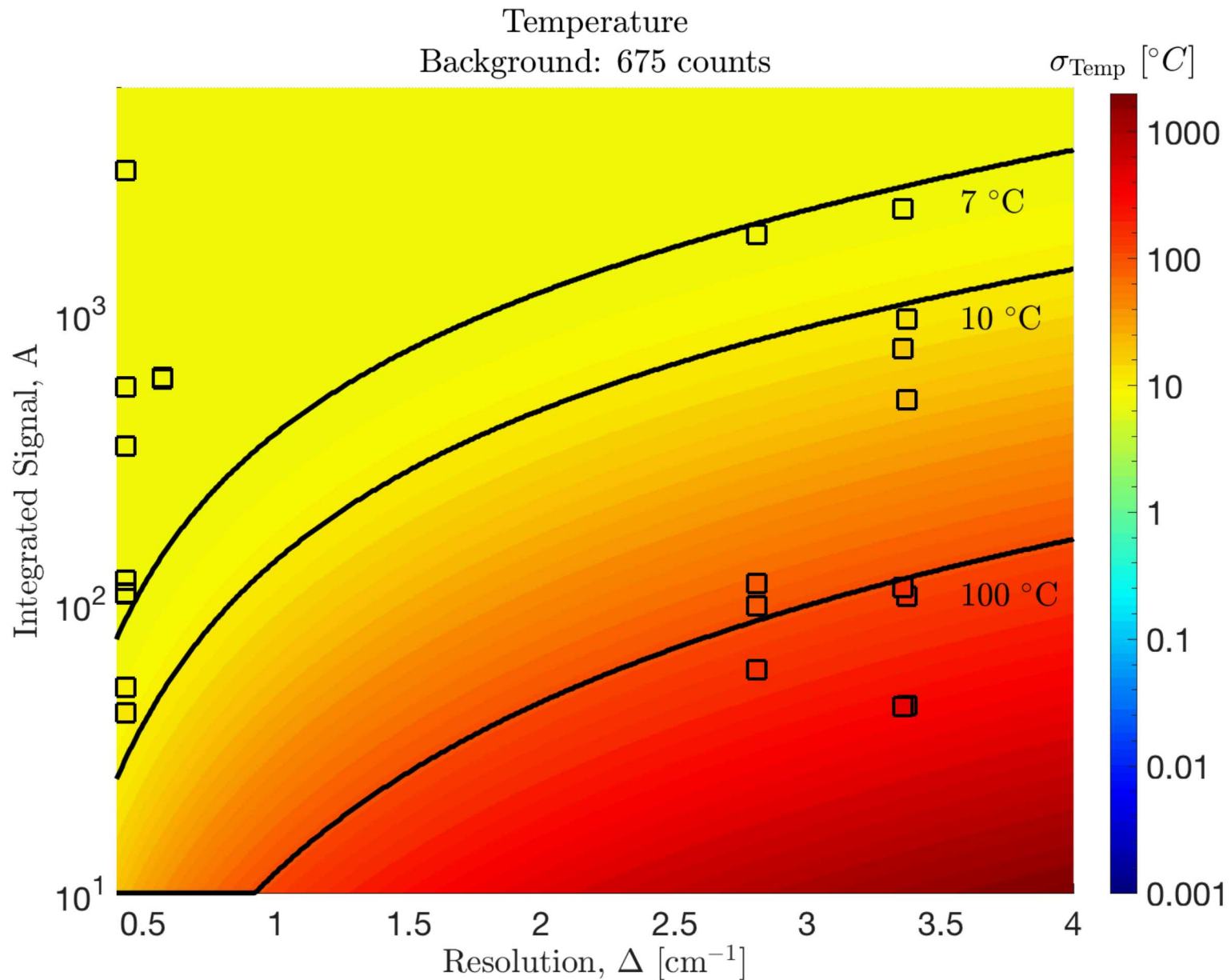
Figure 2. Plot of measured uncertainty in peak position, normalized by Γ_G^2/A without background (full symbols) or with background (open symbols), of the simulated data as a function of signal to noise (H/B). Four parameter weighted uncertainty fit.

$$\sigma_{\text{SNR},x}^2 \approx \frac{\Gamma_T(\Gamma_L, \Gamma_G)^2}{A} \left[1 + 2\sqrt{2} \left(\frac{H}{B} - 1 \right)^{-1} \right]$$

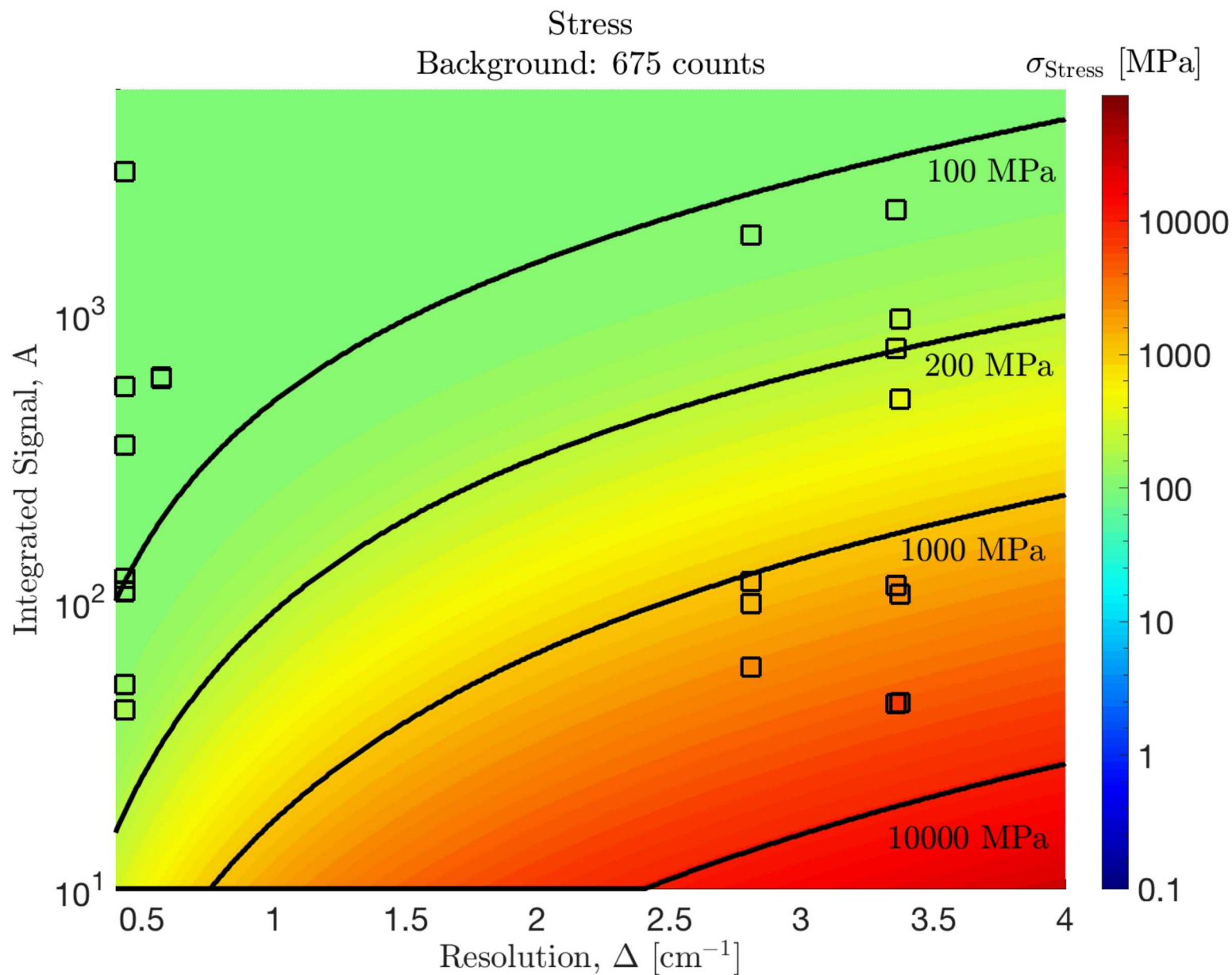
Relative Temperature Capabilities ($B = 675$) ($k = 1$)

Relative Stress Capabilities ($B = 675$) ($k = 1$)

Absolute Temperature Capabilities ($B = 675$) ($k = 1$)



Absolute Stress Capabilities ($B = 675$) ($k = 1$)



- $\text{SNR} = H/B$
- $\Gamma_G \approx 3.04 \Delta$
- Higher accuracy standard needed for Raman spectrometer calibration

Uncertainty due to binning

$$\sigma_{\Delta,V}^2 = \sum_i^N \frac{\epsilon_i - \bar{\epsilon}}{N-1} \approx \frac{1}{(N-1)^3}$$

$$x_{\text{start}} = x_0 - 3\Gamma_V(\Gamma_G, \Gamma_L)$$

$$x_{\text{end}} = x_0 + 3\Gamma_V(\Gamma_G, \Gamma_L)$$

$$N = \frac{3\Gamma_V(\Gamma_G, \Gamma_L)}{\Delta}$$

$$\sigma_{\Delta,x}^2 = (\mathbf{J}'\mathbf{J})^{-1}\mathbf{J}'[(\mathbf{1} \cdot \sigma_{\Delta,V} \cdot H)^2]\mathbf{J}(\mathbf{J}'\mathbf{J})^{-1}$$

Uncertainty due to SNR

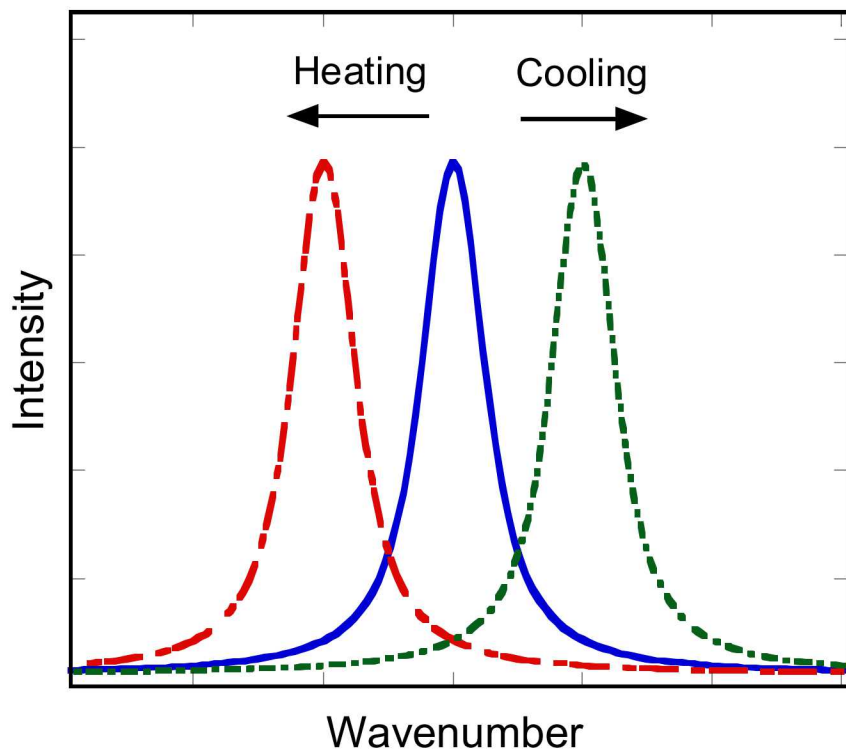
$$\sigma_{\text{SNR},x}^2 \approx \frac{\Gamma_T(\Gamma_L, \Gamma_G)^2}{A} \left[1 + 2\sqrt{2} \left(\frac{H}{B} - 1 \right)^{-1} \right]$$

Uncertainty due to Standard

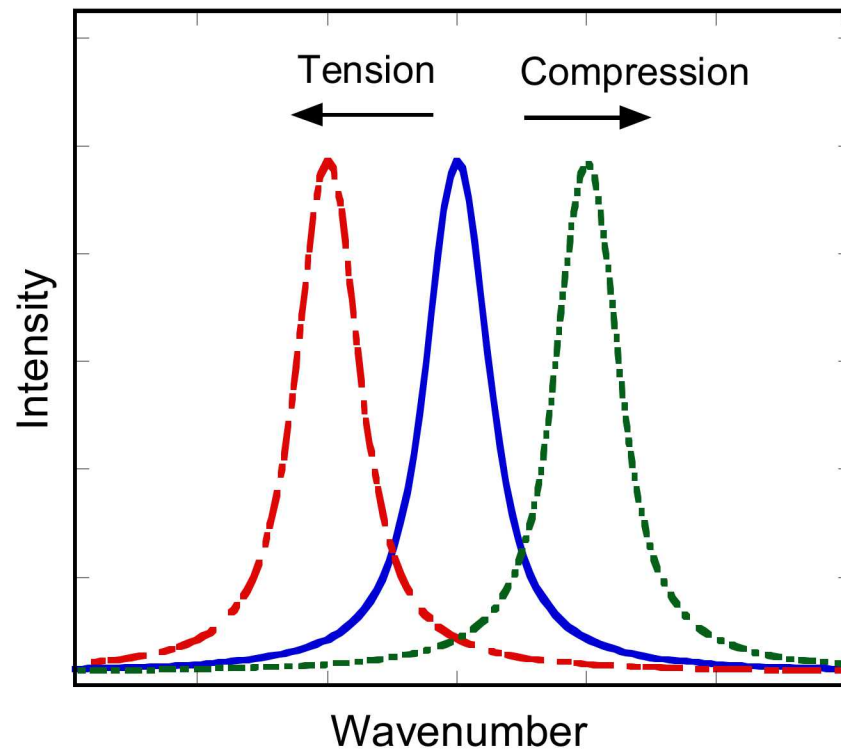
$$\sigma_{S,x}^2 = \frac{1}{n^2} \sum_{p=i}^n \sigma_i^2(p)$$

Questions?

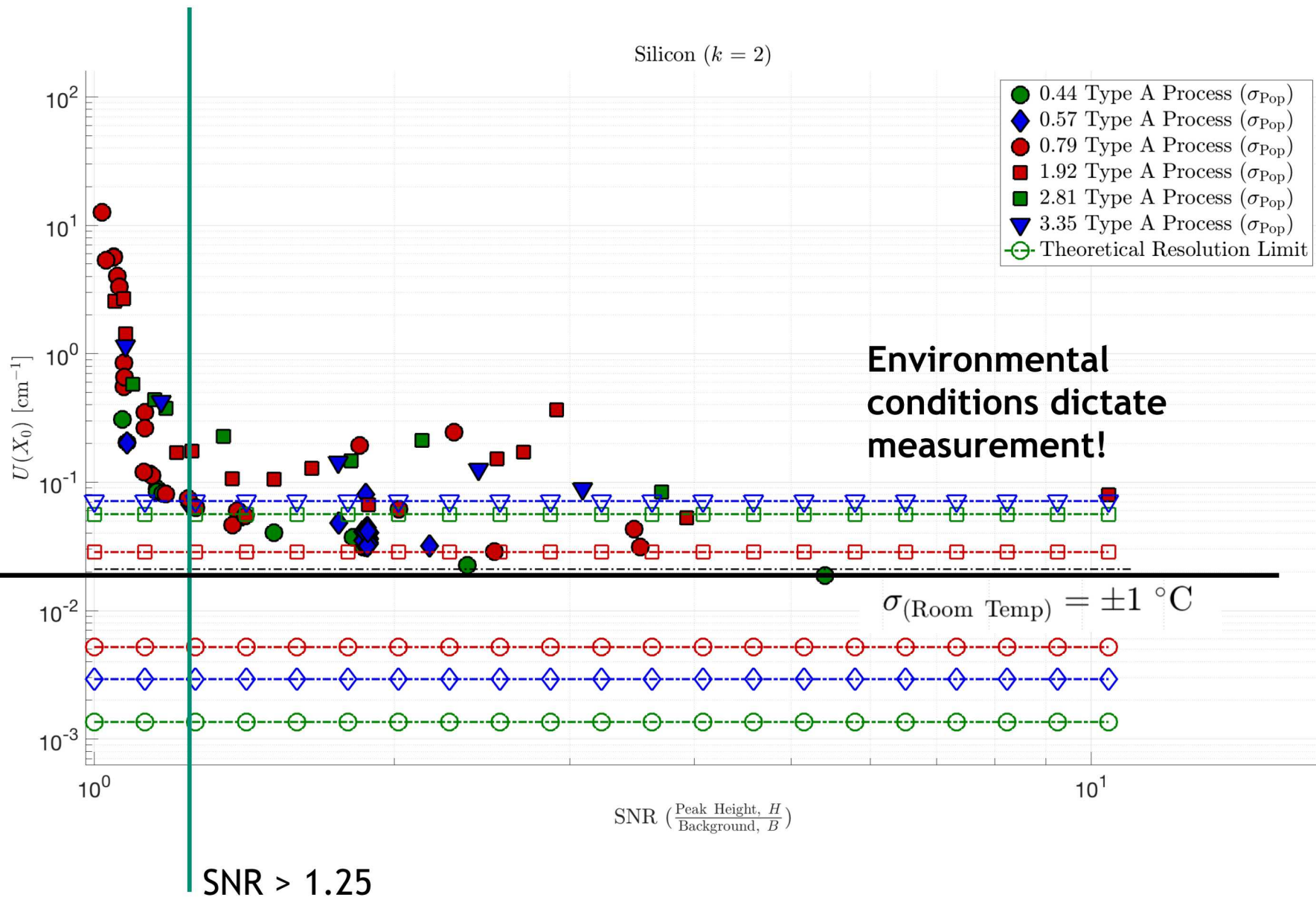
Temperature



Stress



Comparison of Analytical Model with **Population σ** ($n = 500$)



ASTM E1840

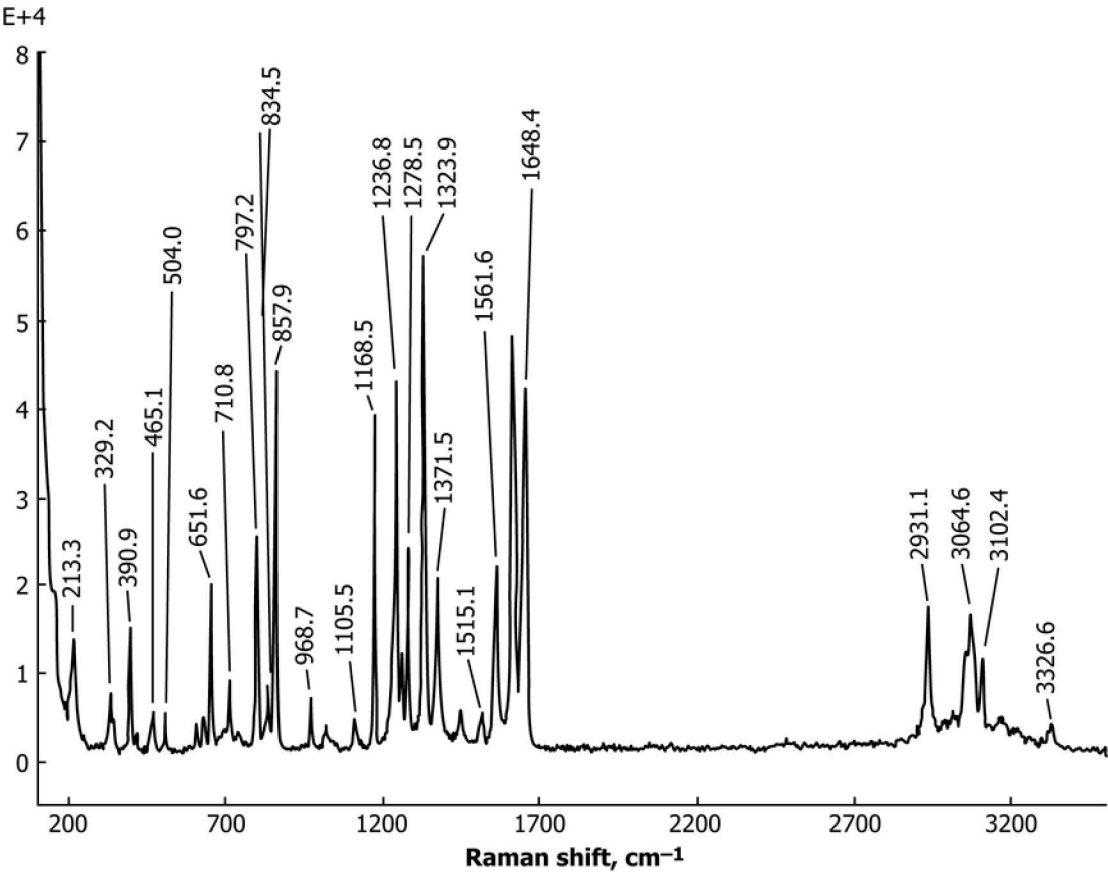


FIG. 5 4-Acetamidophenol (Tylenol)



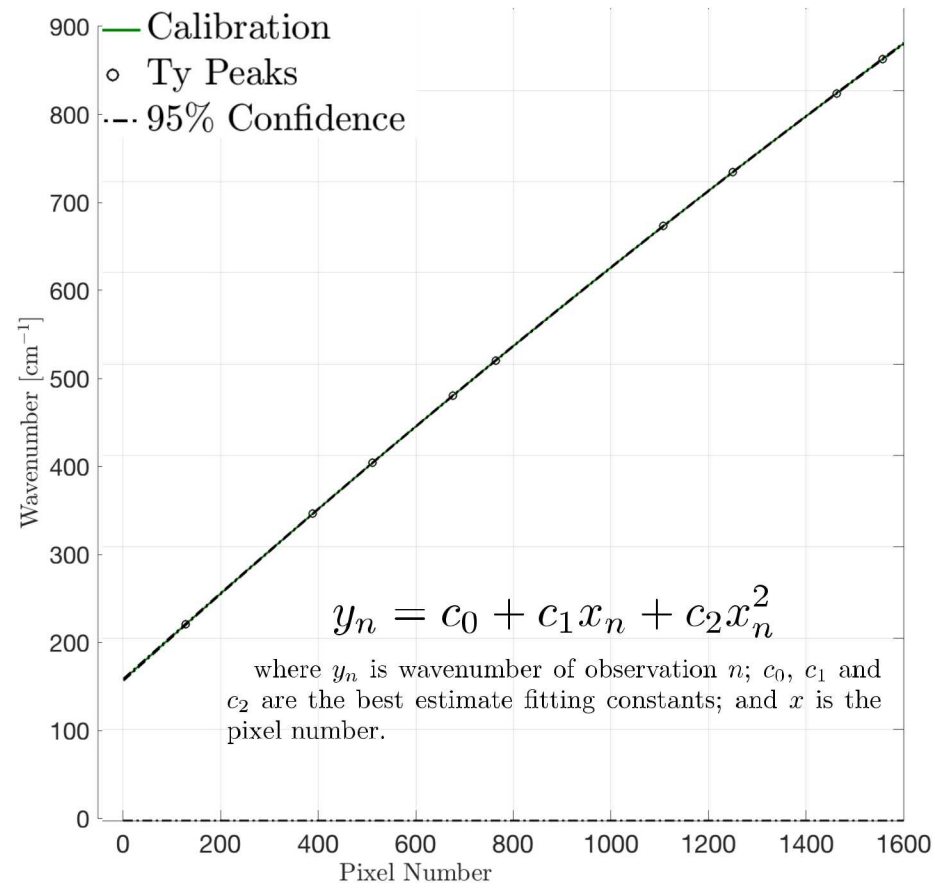
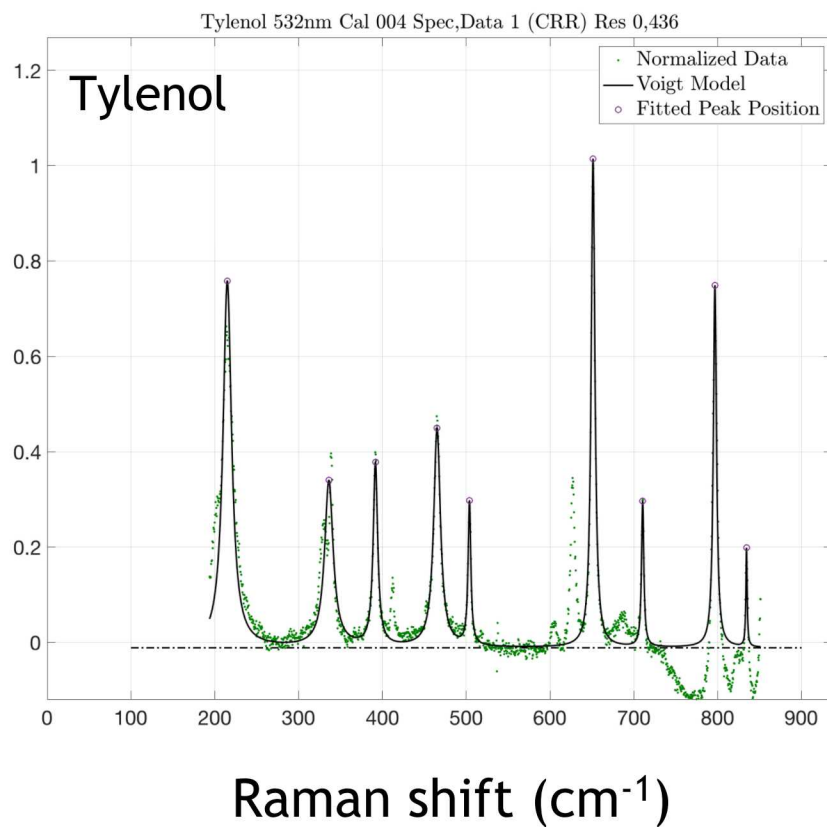
E1840 – 96 (2014)

TABLE 5 4-Acetamidophenol

Average (cm-1) ± Standard Deviation	Relative Intensity
213.3 ± 1.77	17
329.2 ± 0.52	11
390.9 ± 0.76	25
465.1 ± 0.30	11
504.0 ± 0.60	11
651.6 ± 0.50	33
710.8 ± 0.68	17
797.2 ± 0.48	45
834.5 ± 0.46	14
857.9 ± 0.50	82
968.7 ± 0.60	12
1105.5 ± 0.27	7
1168.5 ± 0.65	70
1236.8 ± 0.46	75
1278.5 ± 0.45	42
1323.9 ± 0.46	100
1371.5 ± 0.11	38
1515.1 ± 0.70	9
1561.5 ± 0.52	37
1648.4 ± 0.50	73
2931.1 ± 0.63	29
3064.6 ± 0.31	26
3102.4 ± 0.95	20
3326.6 ± 2.18	7

Active ingredient of Tylenol (see Footnote 6).

Intensity (a.u.)



$$y_n = c_0 + c_1 x_n + c_2 x_n^2$$

where y_n is wavenumber of observation n ; c_0 , c_1 and c_2 are the best estimate fitting constants; and x is the pixel number.

$$\mathbf{y} = \mathbf{M}\boldsymbol{\kappa} + \boldsymbol{\epsilon}$$

$$\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_N \end{bmatrix} \quad \mathbf{M} = \begin{bmatrix} 1 & x_1 & x_1^2 \\ 1 & x_2 & x_2^2 \\ \vdots & \vdots & \vdots \\ 1 & x_N & x_N^2 \end{bmatrix} \quad \boldsymbol{\kappa} = \begin{bmatrix} \kappa_0 \\ \kappa_1 \\ \kappa_2 \end{bmatrix} \quad \boldsymbol{\epsilon} = \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \vdots \\ \epsilon_N \end{bmatrix}$$

where $\mathbf{y}$ is a vector of $[N \times 1]$ measured peaks; N is the total number of measured peaks; $\boldsymbol{\kappa}$ is the true value of the fitted constants; and $\boldsymbol{\epsilon}$ is the error at each observation y_n , where $n = 1, 2, \dots, N$.

$$\mathbf{c} = (\mathbf{M}'\mathbf{M})^{-1}\mathbf{M}'\mathbf{y}$$

best estimate of $\boldsymbol{\kappa}$

$$\hat{\mathbf{y}} = \mathbf{M}\mathbf{c} + \mu_{\epsilon}$$

best estimate of $\mathbf{y}$

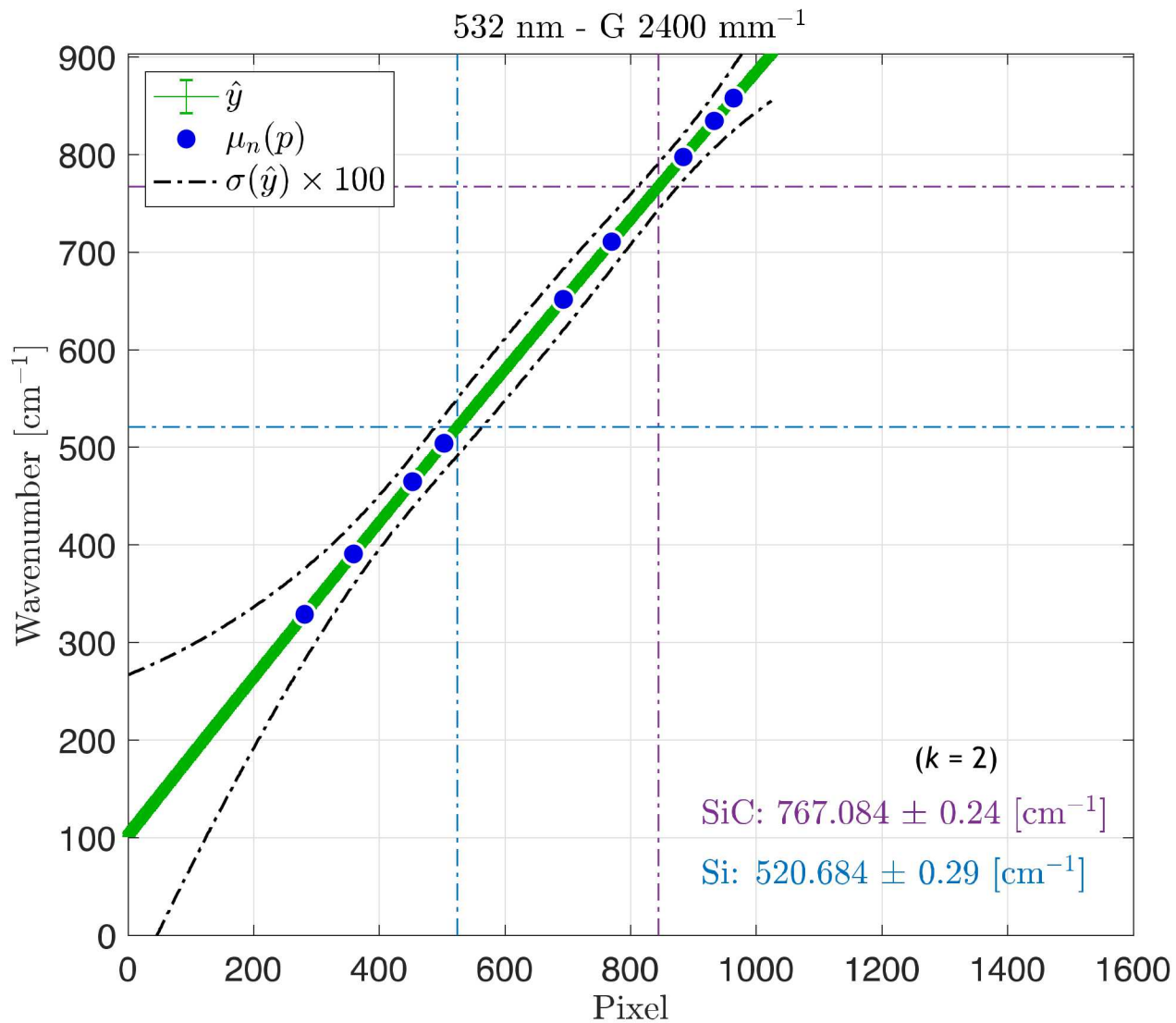
$$\sigma^2(\hat{\mathbf{y}}_s) = \text{Var}[\hat{\mathbf{y}}_s] = \text{diag}(\mathbf{M}_0 \times \text{Var}[\mathbf{c}_s] \times \mathbf{M}_0')$$

$$\text{Var}[\mathbf{c}_s] = \mathbf{A}\mathbf{M}' \times \text{Var}[\mu_n(p)] \times \mathbf{M}\mathbf{A}$$

$$\mathbf{A} = (\mathbf{M}'\mathbf{M})^{-1}$$

$$\text{Var}[\mu_n(p)] = \begin{bmatrix} \sigma_{(S,1)}^2 & 0 & 0 & \dots & 0 \\ 0 & \sigma_{(S,2)}^2 & 0 & \dots & 0 \\ 0 & 0 & \sigma_{(S,3)}^2 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & \sigma_{(S,P)}^2 \end{bmatrix}$$

Uncertainty from ASTM E1840





E1840 – 96 (2014)

Resolution [k/pxl]		0.44	0.57	0.74	1.6	2.34	3.36
μ_ASTM	σ_ASTM	532	488	785	785	532	488
[cm ⁻¹]		2400	2400	1200	600	600	600
213.3	1.77	213.30	213.30	213.30	213.30	213.30	213.30
329.2	0.52	329.20	329.20	329.20	329.20	329.20	329.20
390.9	0.76	390.90	390.90	390.90	390.90	390.90	390.90
465.1	0.3	465.10	465.10	465.10	465.10	465.10	465.10
504	0.6	504.00	504.00	504.00	504.00	504.00	504.00
651.6	0.5	651.60	651.60	651.60	651.60	651.60	651.60
710.8	0.68	710.80	710.80	710.80	710.80	710.80	710.80
797.2	0.48	797.20	797.20	797.20	797.20	797.20	797.20
834.5	0.46	834.50	834.50	834.50	834.50	834.50	834.50
857.9	0.5	857.90	-	857.90	857.90	857.90	857.90
968.7	0.6	-	-	-	968.70	968.70	968.70
1105.5	0.27	-	-	-	1105.50	1105.50	1105.50
1168.5	0.65	-	-	-	1168.50	1168.50	1168.50
1236.8	0.46	-	-	-	1236.80	1236.80	1236.80
1278.5	0.45	-	-	-	1278.50	1278.50	1278.50
1323.9	0.46	-	-	-	1323.90	1323.90	1323.90
1371.5	0.11	-	-	-	1371.50	1371.50	1371.50
1515.1	0.7	-	-	-	1515.10	1515.10	1515.10
1561.5	0.52	-	-	-	1561.50	1561.50	1561.50
1648.4	0.5	-	-	-	1648.40	1648.40	1648.40
2931.1	0.63	-	-	-	-	2931.10	2931.10
3064.6	0.31	-	-	-	-	3064.60	3064.60
3102.4	0.95	-	-	-	-	3102.40	3102.40
3326.6	2.18	-	-	-	-	3326.60	3326.60
U (s) (k = 2)		0.37	0.39	0.37	0.30	0.31	0.31
cm ⁻¹							

$$\sigma_{S,x}^2 = \frac{1}{n^2} \sum_{p=i}^n \sigma_i^2(p)$$

For absolute measurements, RSS uncertainty due to standard with Voigt uncertainty

(k = 2)
 SiC: 767.084 ± 0.24 [cm⁻¹]
 Si: 520.684 ± 0.29 [cm⁻¹]

