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Sandia National Laboratories

SAND2016-2901C

The SEARCH Software Suite

Code Capabilities and Experimental Comparison

The 5th International Symposium - Supercritical CO2 Power Cycles

March 28-31, 2016, San Antonio, Texas, USA

*Carlson, M. D, Bell, C., Schalansky, C., Fleming, D. F., Rochau, G.

U.S. DEPARTMENT OF ENERGY

NNSA National Nuclear Security Administration

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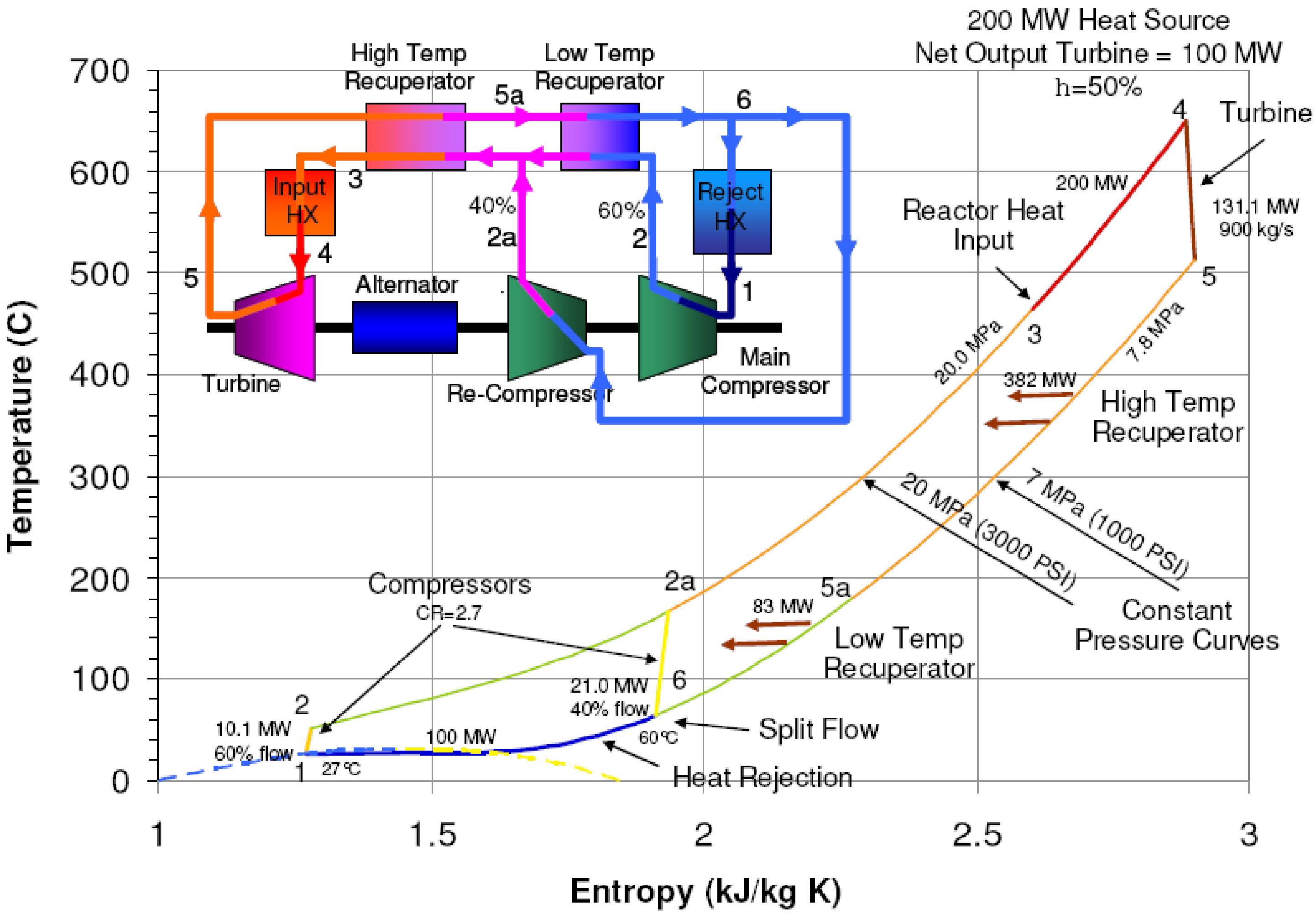
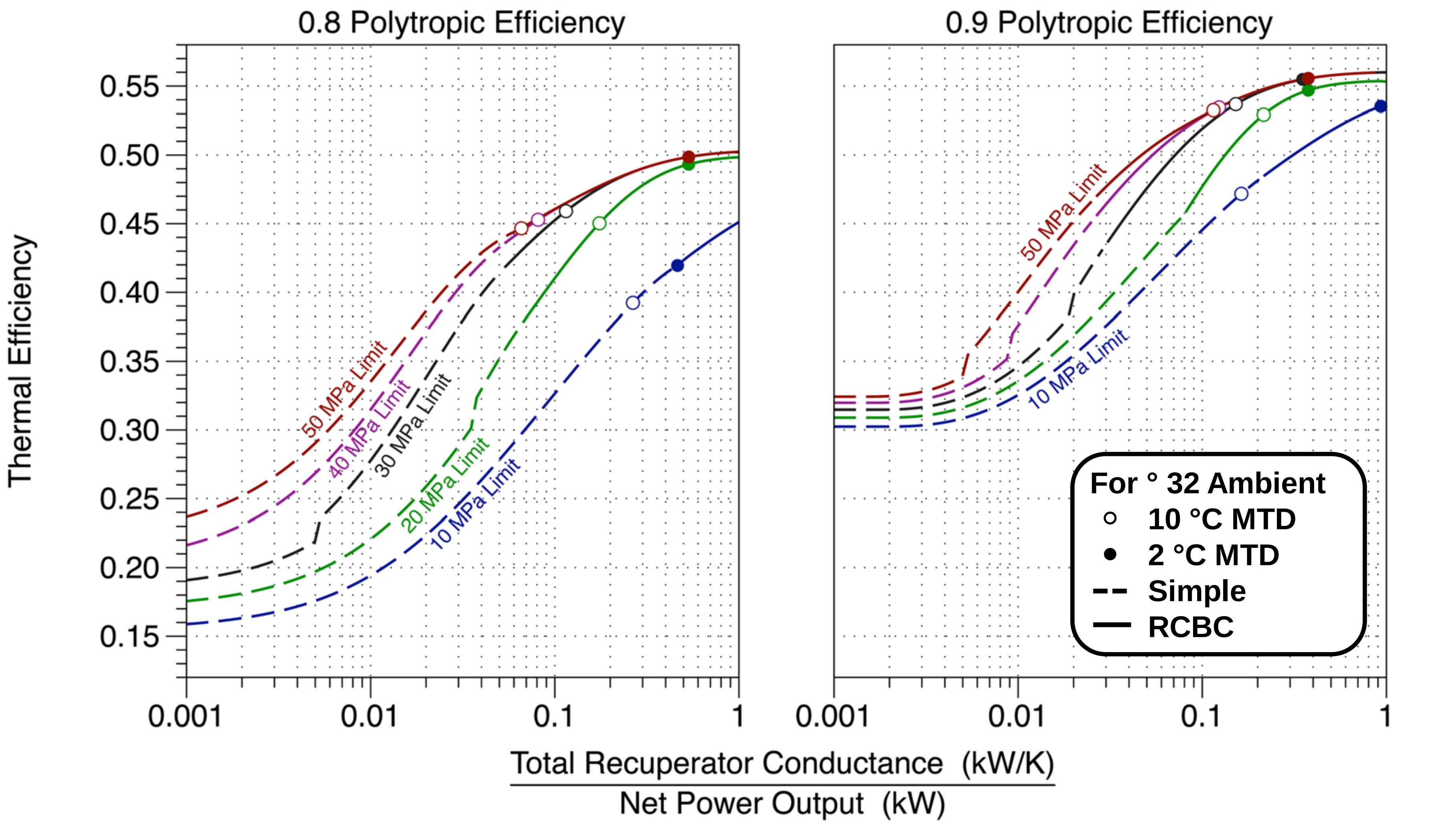
BACKGROUND

Supercritical CO_2 Brayton Cycle



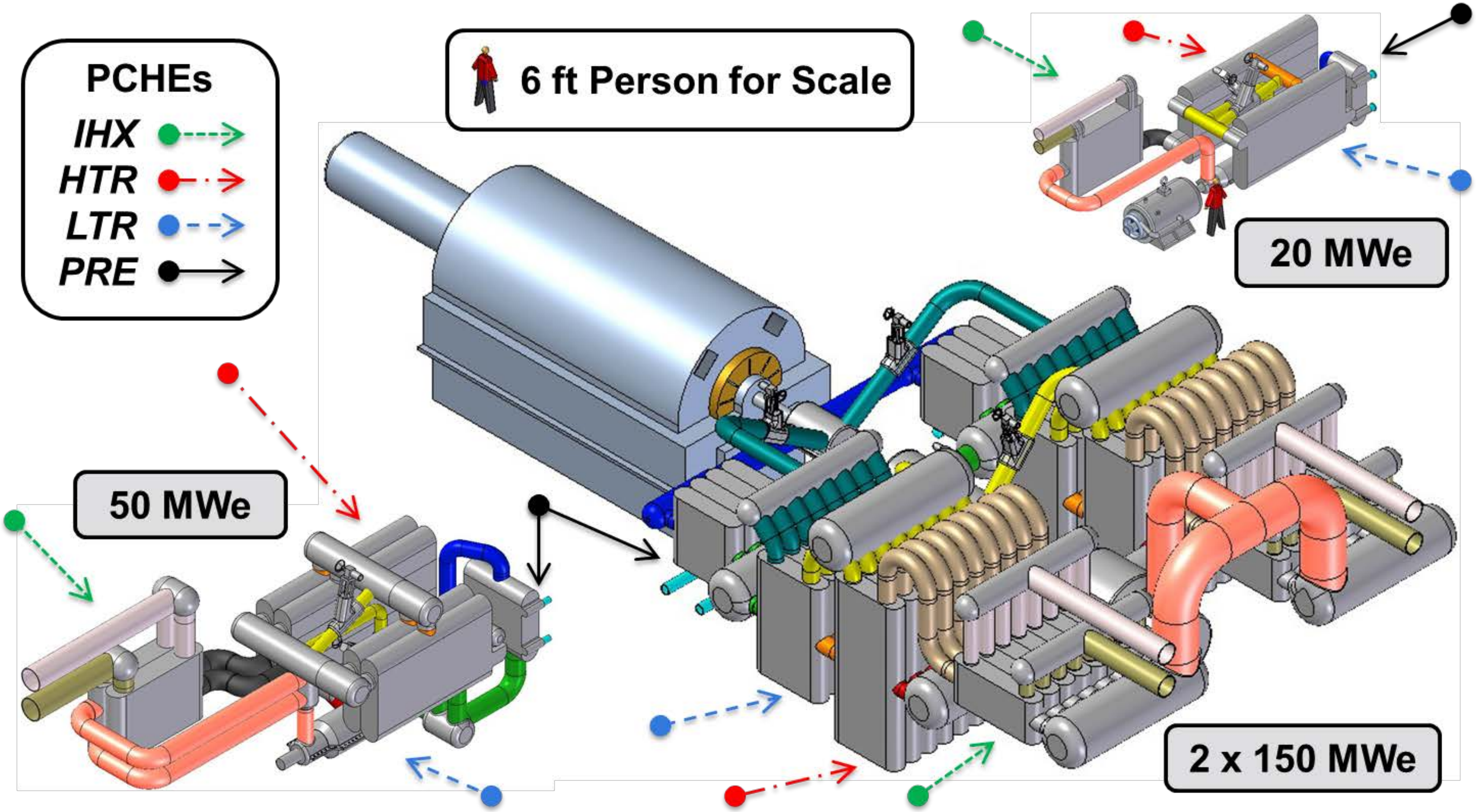
E. J. Parma, S. A. Wright, M. E. Vernon, D. D. Fleming, G. E. Rochau, A. J. Suo-Anttila, A. Al Rashdan, and P. V. Tsvetkov, "Supercritical CO2 Direct Cycle Gas Fast Reactor (SC-GFR) Concept," Sandia National Laboratories, Albuquerque, NM, USA, SAND 2011-2525, May 2011.

sCO2 Brayton Cycles Recuperation



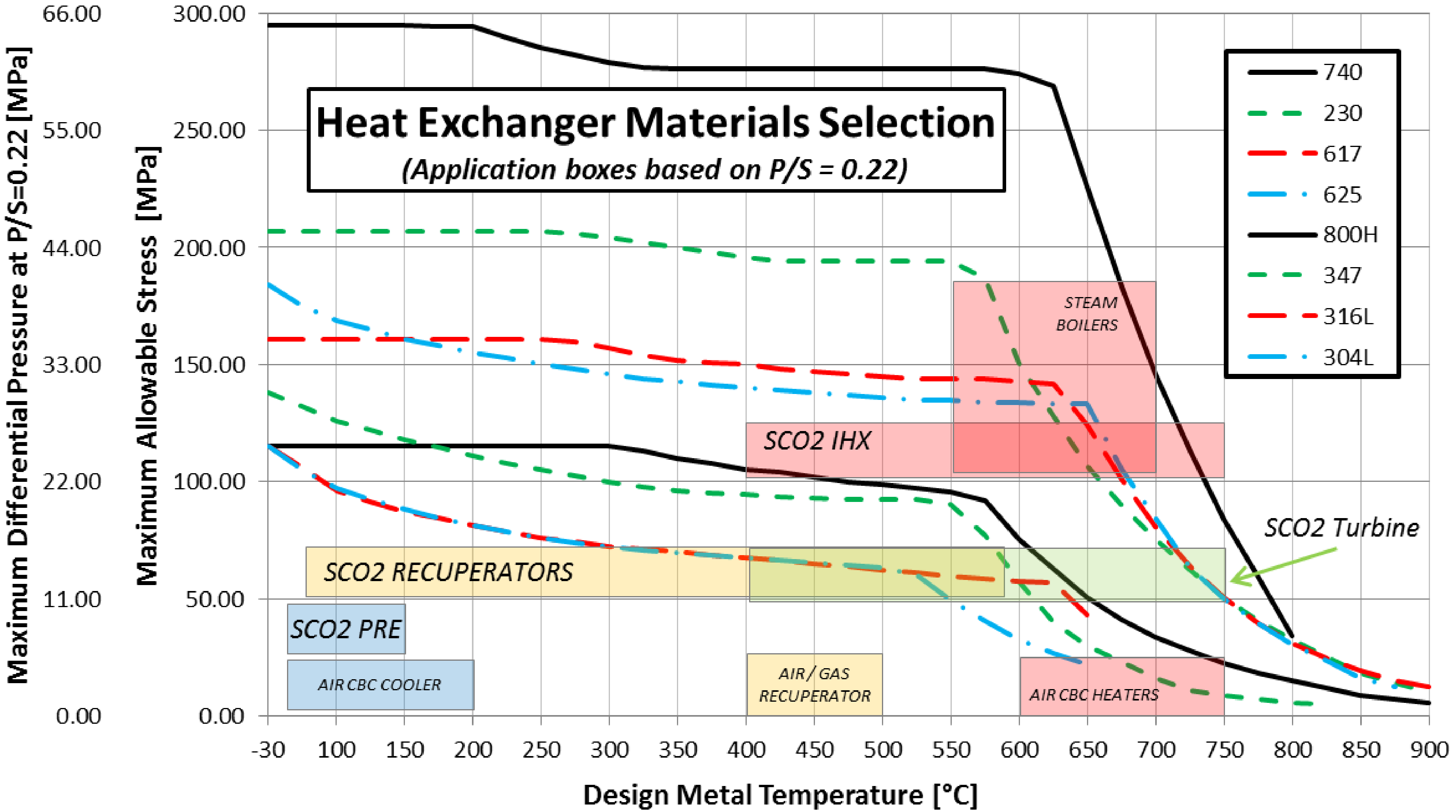
J. Dyreby, S. Klein, G. Nellis, and D. Reindl, "Design Considerations for Supercritical Carbon Dioxide Brayton Cycles With Recompression," *Journal of Engineering for Gas Turbines and Power*, vol. 136, no. 10, p. 101701, Jul. 2014.

Scalable SCO2 CBC Systems



J.P. Gibbs, P. Hejzlar, & M.J. Driscoll. (2006). *Applicability of Supercritical CO2 Power Conversion Systems to GEN IV Reactors* (Topical Report No. MIT-GFR-037) (p. 97). Cambridge, MA: Center for Advanced Nuclear Energy Systems MIT Department of Nuclear Science and Engineering.

Heat Exchanger Requirements



Approximate Cost Scaling

$$Cost = C_{ESDU} F_{mat} F_p F_i UA_{sp} P_{elec}$$

C_{ESDU} is the UA-specific cost value [$/(kW/K)]

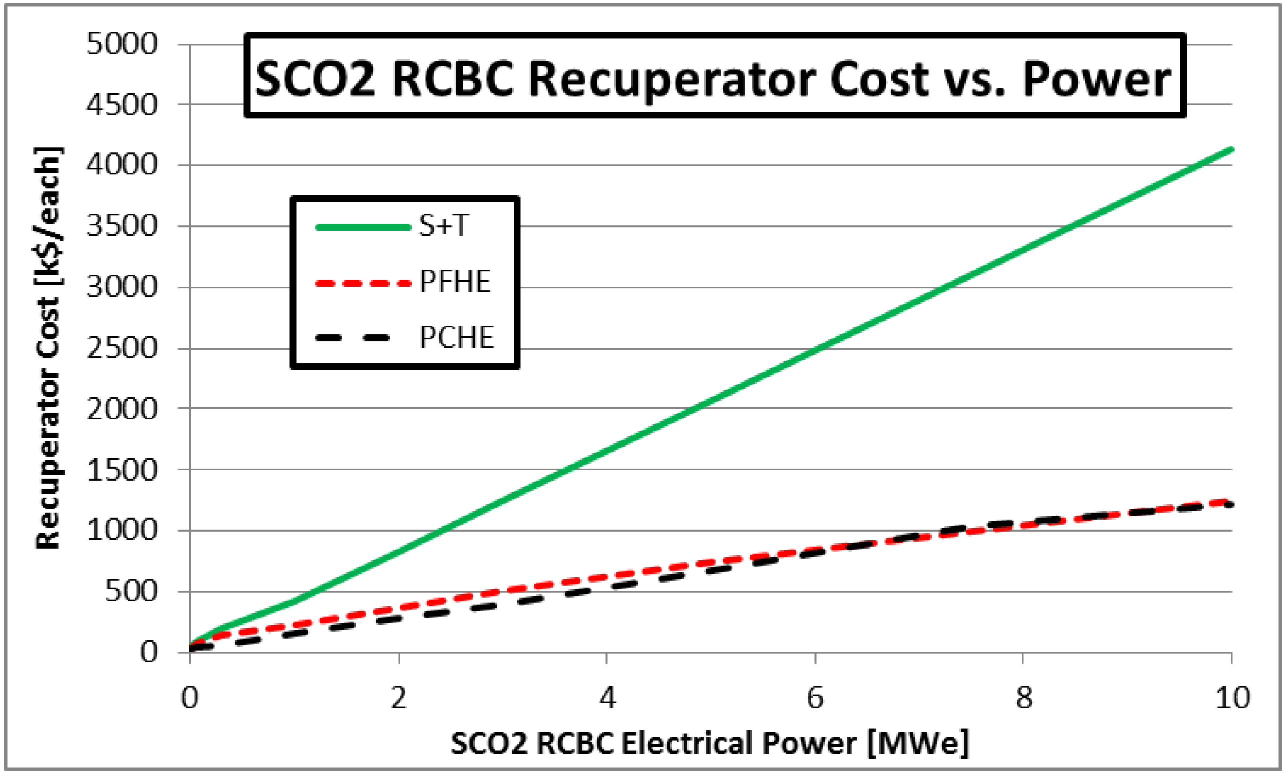
F_{mat} is a material cost factor

F_P is a pressure cost factor

F_i is an adjustment for inflation

UA_{sp} is the cycle power-specific UA [kW/(K-MWe)]

P_{elec} is the cycle power level [MWe]



ESDU, "Selection and Costing of Heat Exchangers," Engineering Sciences Data Unit, ESDU 92013, Dec. 1994.

Heat Exchanger Development Gaps

Technology Readiness Levels		from Direct Gas Combustion	from Exhaust Gas	from 3 MPa Helium	from Steam	from floride molten salts	from nitrate molten salts	from liquid sodium	from liquid lead-bismuth	from Heat Transfer Oil	from Combusting Particles	from Inert Solid Particles	from Geothermal Resources	from sunlight	Yet To Be Identified Materials	Advanced Nickel Alloys	Conventional Nickel Alloys	Austenitic Stainless Steels	to Water	to Humidified Air	to Dry Air	TIT / °C
Molten Salt Reactor	NE					3											4-5	6-8	6-8	2	2-4	700 to 850
Sodium Fast Reactor (SFR)	NE							3										6-8	6-8	2	2-4	550
Lead Fast Reactor (LFR)	NE								3								4-5	6-8	6-8	2	2-4	550 to 800
Helium Gas Reactor (GFR, VHTR)	NE			4-5											2	3	4-5	6-8	6-8	2	2-4	700 to 1000
Nuclear Shipboard Propulsion	NE																	6-8	6-8			200 to 300
Direct CSP Tower	EE													4-5			4-5	6-8	6-8	2	2-4	500 to 1000
CSP Tower with Thermal Storage	EE						3	2		2		3					4-5	6-8	6-8	2	2-4	500 to 1000
CSP Trough with Thermal Storage	EE						3			2								6-8	6-8	2	2-4	300 to 600
CSP Dish Generator	EE							2		2				4-5			4-5	6-8			2-4	500 to 1000
Direct Geothermal Plant	GT												2					6-8	6-8	2	2-4	100 to 300
Indirect Geothermal Plant	GT				4-5													6-8	6-8	2	2-4	100 to 300
Direct Natural Gas Combustion	FE	3-5	4												2	3	4-5	6-8	6-8	2	2-4	1100 to 1500
Integrated Gasification Coal	FE	3-5													2	3	4-5	6-8	6-8	2	2-4	1100 to 1500
Pulverized Coal Fluidized Bed	FE										4					3	4-5	6-8	6-8	2	2-4	550 to 900
Waste Heat Recovery	FE		4															6-8	6-8	2	2-4	230 to 650
Gas Turbine Bottoming	FE		4															6-8	6-8	2	2-4	230 to 650
Municipal waste to energy	FE		4															6-8	6-8	2	2-4	230 to 650
10 MWe Pilot	FE		4														4-5	6-8	6-8	2	2-4	550 to 700
50 MWe Demonstration	FE		4														4-5	6-8	6-8	2	2-4	550 to 700
		N/A	Gas			Liquid					Solid				>750	750	650	550	sCO2 Cooling			
		sCO2 Heating from Various Sources													Recuperation MDMT / °C							

Development Gaps Addressed

Sandia National Laboratories

Technology Readiness Levels		from Direct Gas Combustion	from Exhaust Gas	from 3 MPa Helium	from Steam	from floride molten salts	from nitrate molten salts	from liquid sodium	from liquid lead-bismuth	from Heat Transfer Oil	from Combusting Particles	from Inert Solid Particles	from Geothermal Resources	from sunlight	Yet To Be Identified Materials	Advanced Nickel Alloys	Conventional Nickel Alloys	Austenitic Stainless Steels	to Water	to Humidified Air	to Dry Air	TIT / °C
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			NE, Peregrine CRADA	NEUP		NEUP						SuNLaMP		SERIIUS			NE, NEUPs	NEUP, APOLLO, NE, CRADAs (VPE, Peregrine)				

Development Gaps Addressed

Sandia National Laboratories

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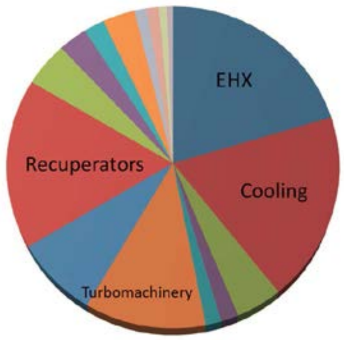
		sCO2 Heating from Various Sources													Recuperation MDMT / °C							

NE, Peregrine CRADA | NEUP | NEUP | SuNLaMP | SERIIUS | NE, NEUPs | NEUP, APOLLO, NE, CRADAs (VPE, Peregrine)

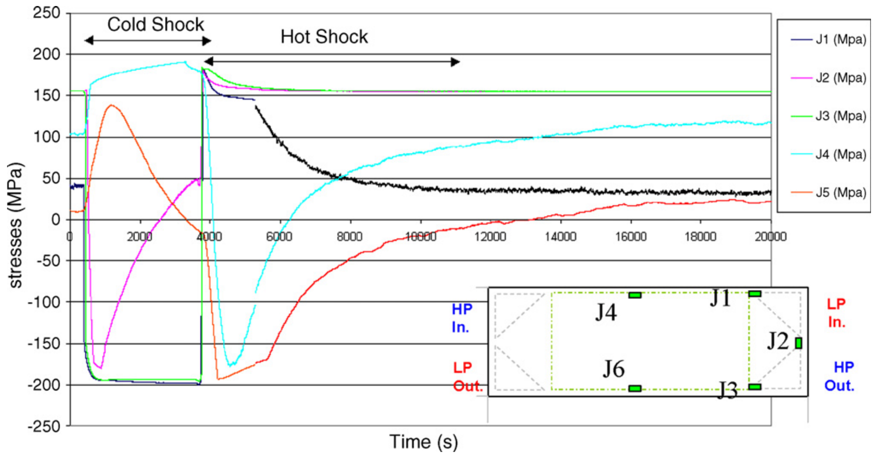
Key Development Metrics

- **Economics**
  - How do we optimize designs and reduce fabrication costs?
    - Efficiency vs. Effectiveness
    - Efficiency vs. pressure drop
    - Manufacturing techniques
- **Failure Modes**
  - How do we accommodate thermal stress and fatigue?
    - Pressure containment (material vs. geometry)
    - Higher Temperatures
    - Corrosion and fouling

Echogen



"[A] 30% reduction in HX cost would have [a] meaningful impact on system cost."



[1] T. Held, "Performance & cost targets for sCO2 heat exchangers," presented at the National Energy Technology Laboratory - EPRI Workshop on Heat Exchangers for Supercritical CO2 Power Cycles, San Diego, CA, USA, 15-Oct-2015.
[2] F. Pra, P. Tochon, C. Mauget, J. Fokkens, and S. Willemsen, "Promising designs of compact heat exchangers for modular HTRs using the Brayton cycle," *Nuclear Engineering and Design*, vol. 238, no. 11, pp. 3160–3173, Nov. 2008.

MCHE DESIGN ALGORITHM

The Printed Circuit Heat Exchanger

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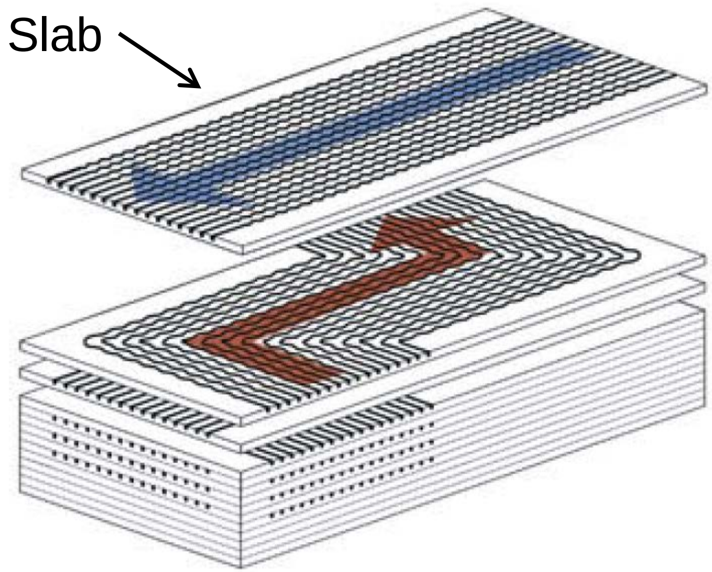
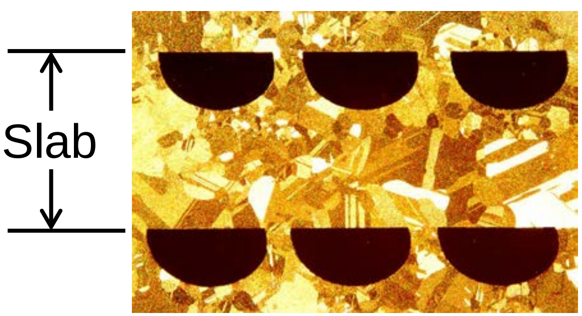
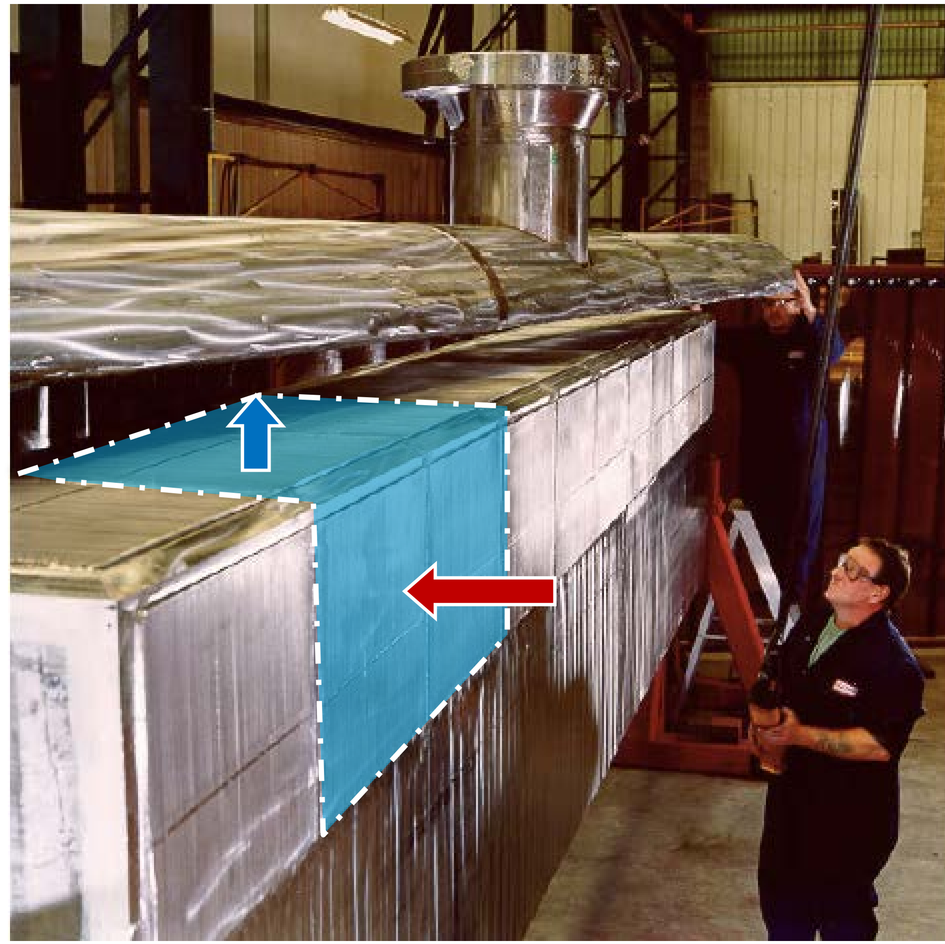
Heat Exchanger Core



Diffusion Bonding



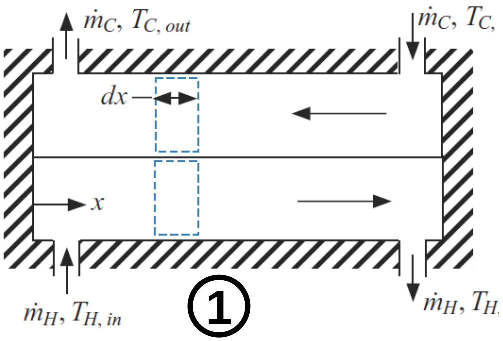
Core and Manifold Assembly

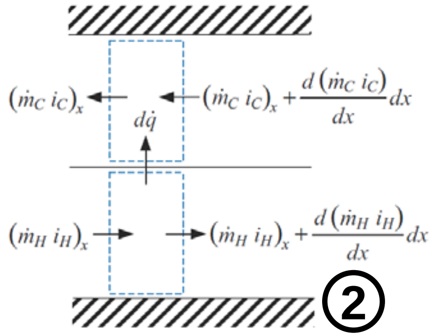


Methods of Heat Exchanger Design

- Effectiveness – NTU / LMTD Methods
  - Uses analytical solutions to various heat exchanger configurations
  - Explicit solution method with reasonable accuracy
- Compact Heat Exchanger Correlations
  - Correlations developed from experimental data for several geometries
  - Explicit accurate solution but for a limited number of correlations
- Sub-Heat Exchanger Method
  - Implements method 1 multiple times to capture property variations
  - Implicit solution needing fewer nodes / iterations than 1D solutions
- 1D Channel Solutions
  - Simulates channels identically or in parallel to determine performance
  - Iterative, intensive solution with the highest accuracy and flexibility
- More complex methods also exist (2D, 3D, CFD)

Effectiveness - NTU Derivation





③
$$\frac{dT_H}{dx} = -\frac{UA}{L\,\dot{m}_H\,c_H}(T_H - T_C)$$

③
$$\frac{dT_C}{dx} = -\frac{UA}{L\,\dot{m}_C\,c_C}(T_H - T_C)$$

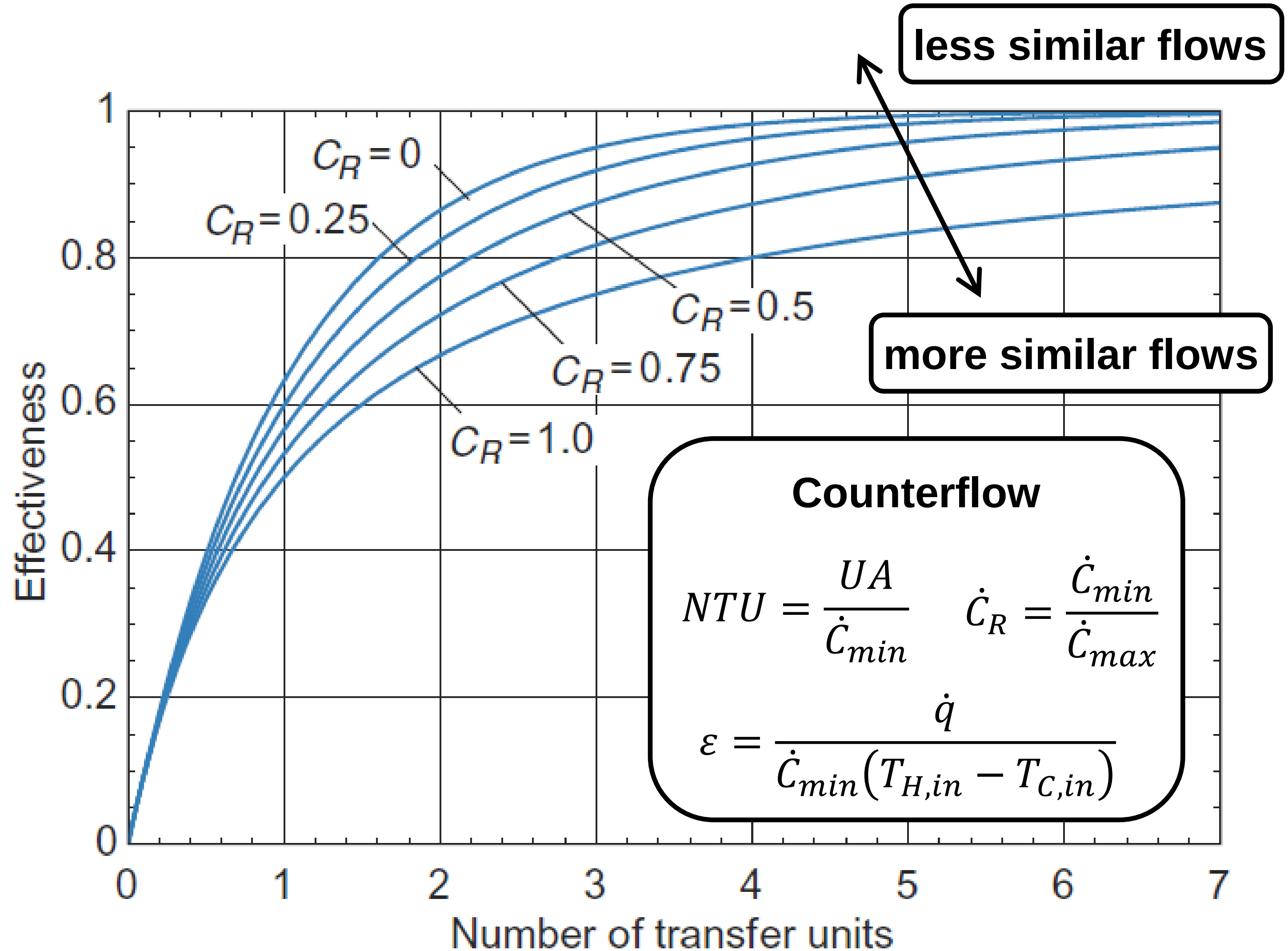
④
$$\ln\left(\frac{T_{H,out} - T_{C,in}}{T_{H,in} - T_{C,out}}\right) = -UA\left(\frac{1}{\dot{C}_H} - \frac{1}{\dot{C}_C}\right)$$

⑤
$$NTU = \begin{cases} \dfrac{\ln\left[\dfrac{1-\varepsilon\, C_R}{1-\varepsilon}\right]}{1 - C_R} & \text{for } C_R < 1 \\ \dfrac{\varepsilon}{1-\varepsilon} & \text{for } C_R = 1 \end{cases}$$

1. Assume:
   - Externally adiabatic
   - Incompressible flow
   - Constant specific heat capacity
   - Enthalpy independent of pressure
2. Finite difference method
   - Establish control volumes
3. Coupled differential equations
   - Hot and cold-side temperatures
4. General solution
   - Relate temperatures, UA, $\dot{C}$'s
5. Effectiveness-NTU formulation
   - $NTU = \frac{UA}{\dot{C}_{min}}$, and $\dot{C}_R = \frac{\dot{C}_{min}}{\dot{C}_{max}}$
   - $\varepsilon = \dot{q}/[\dot{C}_{min}(T_{H,in} - T_{C,in})]$

G. Nellis and S. A. Klein, *Heat Transfer*. Cambridge; New York: Cambridge University Press, 2009.

Effectiveness - NTU Solution



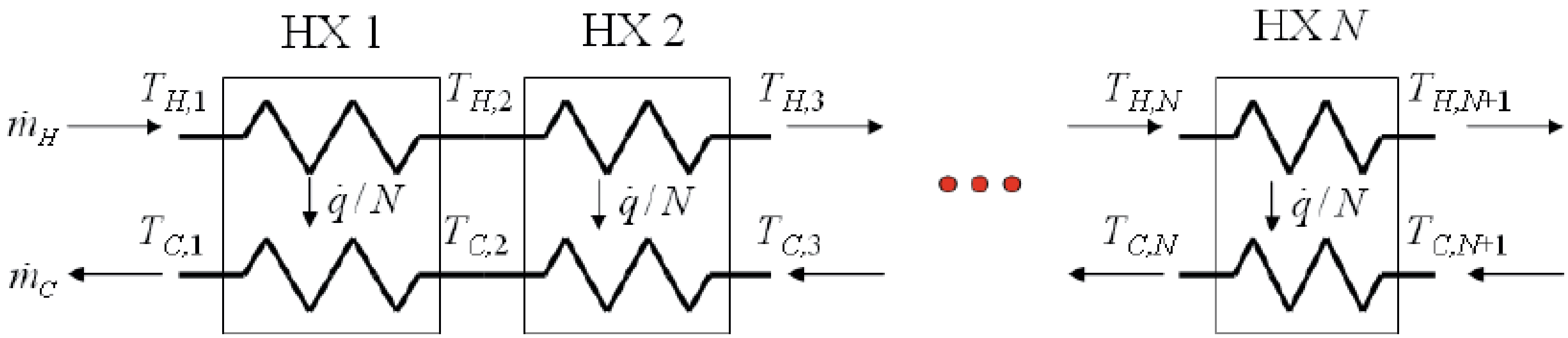
Counterflow

$$NTU = \frac{UA}{\dot{C}_{min}} \qquad \dot{C}_R = \frac{\dot{C}_{min}}{\dot{C}_{max}}$$

$$\varepsilon = \frac{\dot{q}}{\dot{C}_{min}\left(T_{H,in} - T_{C,in}\right)}$$

G. Nellis and S. A. Klein, *Heat Transfer*. Cambridge; New York: Cambridge University Press, 2009.

Sub-Heat Exchanger Method



$$\dot{C}_i = \dot{m}\,\frac{h_i - h_{i+1}}{\text{MAX}\left(1\text{e}{-4}\ [\text{K}],\ |T_i - T_{i+1}|\ \text{SIGN}(h_i - h_{i+1})\right)}$$

$$\varepsilon_i = \frac{\dot{q}_i}{\text{MIN}\left(\dot{C}_{A,i}, \dot{C}_{B,i}\right)\left(T_{A,i} - T_{B,i+1}\right)}$$

$$NTU_i = \begin{cases} \dfrac{\ln\left[\dfrac{(1-\varepsilon C_R)}{1-\varepsilon}\right]}{1 - C_R} & \text{for } C_R < 1 \\ \dfrac{\varepsilon}{1-\varepsilon} & \text{for } C_R = 1 \end{cases}$$

$$UA_i = NTU_i\ \text{MIN}\left(\dot{C}_{A,i}, \dot{C}_{B,i}\right)$$

- Divide into a series of HXers
- Extends e-NTU method
- Assumptions apply to each sub-heat exchanger (Δx)
- Best method to obtain UA accurately and quickly with variable property flows

G. Nellis and S. A. Klein, *Heat Transfer*. Cambridge; New York: Cambridge University Press, 2009.

ASME BPVC Design Equations

$$S_{m,stay} = \frac{Ph}{2t_4}\left[\frac{6 + K(11 - \alpha^2)}{3 + 5K}\right]$$

$$S_{m,1} = \frac{Ph}{2t_1}\left[3 - \frac{6 + K(11 - \alpha^2)}{3 + 5K}\right]$$

$$S_{m,2} = \frac{PH}{2t_2}$$

$$S_{b,stay} = 0$$

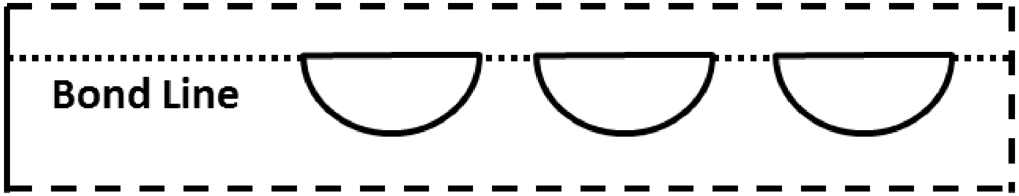
$$(S_{b,1})_{at\,N} = \frac{Pc_1}{24I_1}\left[-3H^2 + 2h^2\left(\frac{3 + 5\alpha^2K}{3 + 5K}\right)\right]$$

$$(S_{b,1})_{at\,Q} = \frac{Ph^2c_1}{12I_1}\left(\frac{3 + 5\alpha^2K}{3 + 5K}\right)$$

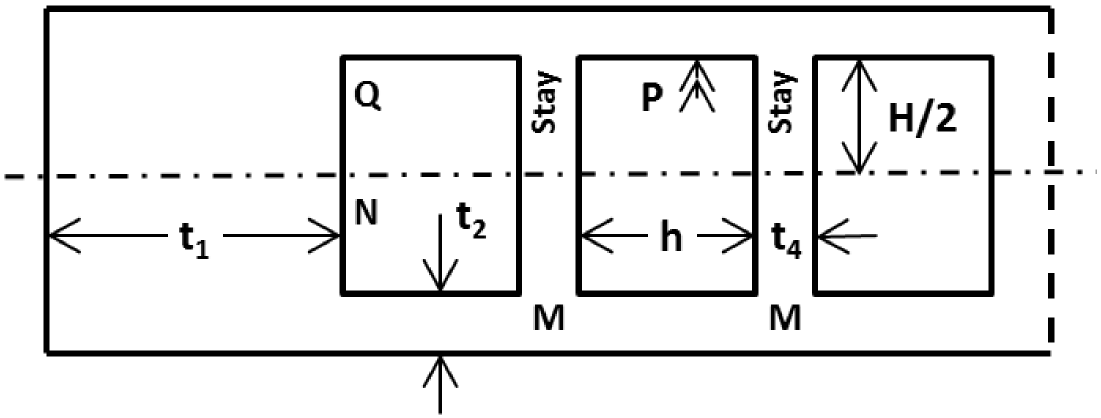
$$(S_{b,2})_{at\,M} = \frac{Ph^2c_2}{12I_2}\left[\frac{3 + K(6 - \alpha^2)}{3 + 5K}\right]$$

$$(S_{b,2})_{at\,Q} = \frac{Ph^2c_2}{12I_2}\left(\frac{3 + 5\alpha^2K}{3 + 5K}\right)$$

Section of a printed circuit heat exchanger



Vessel sketch from the ASME BPVC VIII-1-13-2(a)(8)



M. Carlson, T. Conboy, D. Fleming, and J. Pasch, "Scaling Considerations for SCO2 Cycle Heat Exchangers," in *Proceedings of the ASME Turbo Expo 2014: Turbine Technical Conference and Exposition*, Düsseldorf, Germany, 2014, pp. 1–5.

Non-Dimensionalized Equations

$$\frac{P}{SE} \le \left(\frac{1}{wf} - 1\right)$$

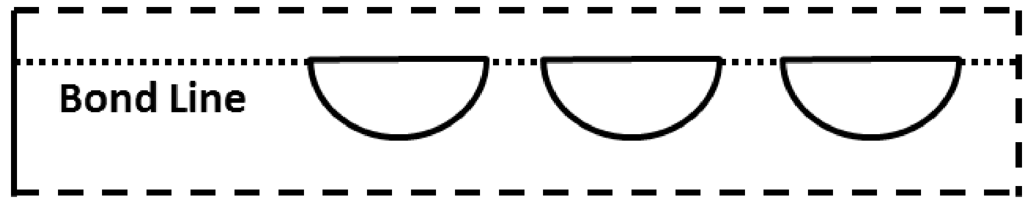
$$\frac{P}{S} \le 2\left(\frac{1}{df} - 1\right)$$

$$\frac{P}{S} \le 3\left(\frac{df}{1-df} + \frac{1}{AR^2}\left(\frac{df}{1-df}\right)^2\right)^{-1}$$

$$wf = \frac{h}{h + t_4}$$

$$df = \frac{H}{H + t_2}$$

Section of a printed circuit heat exchanger



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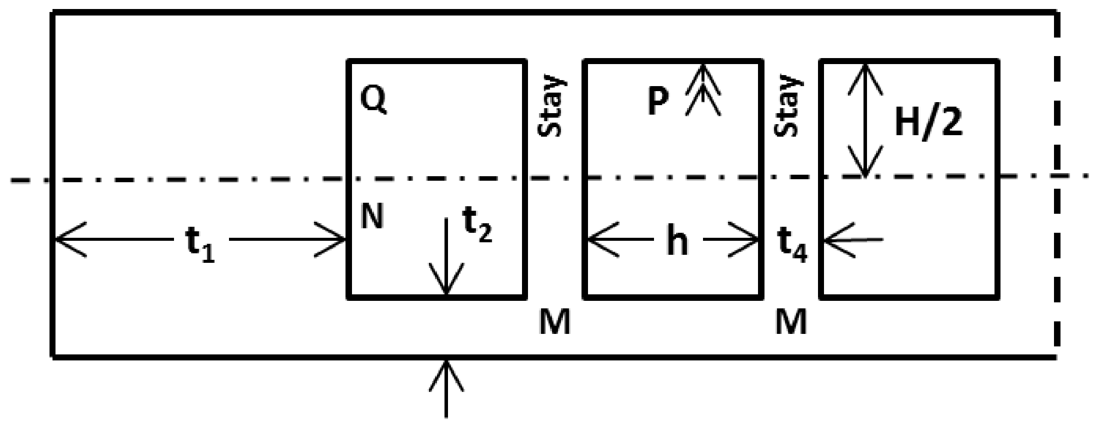

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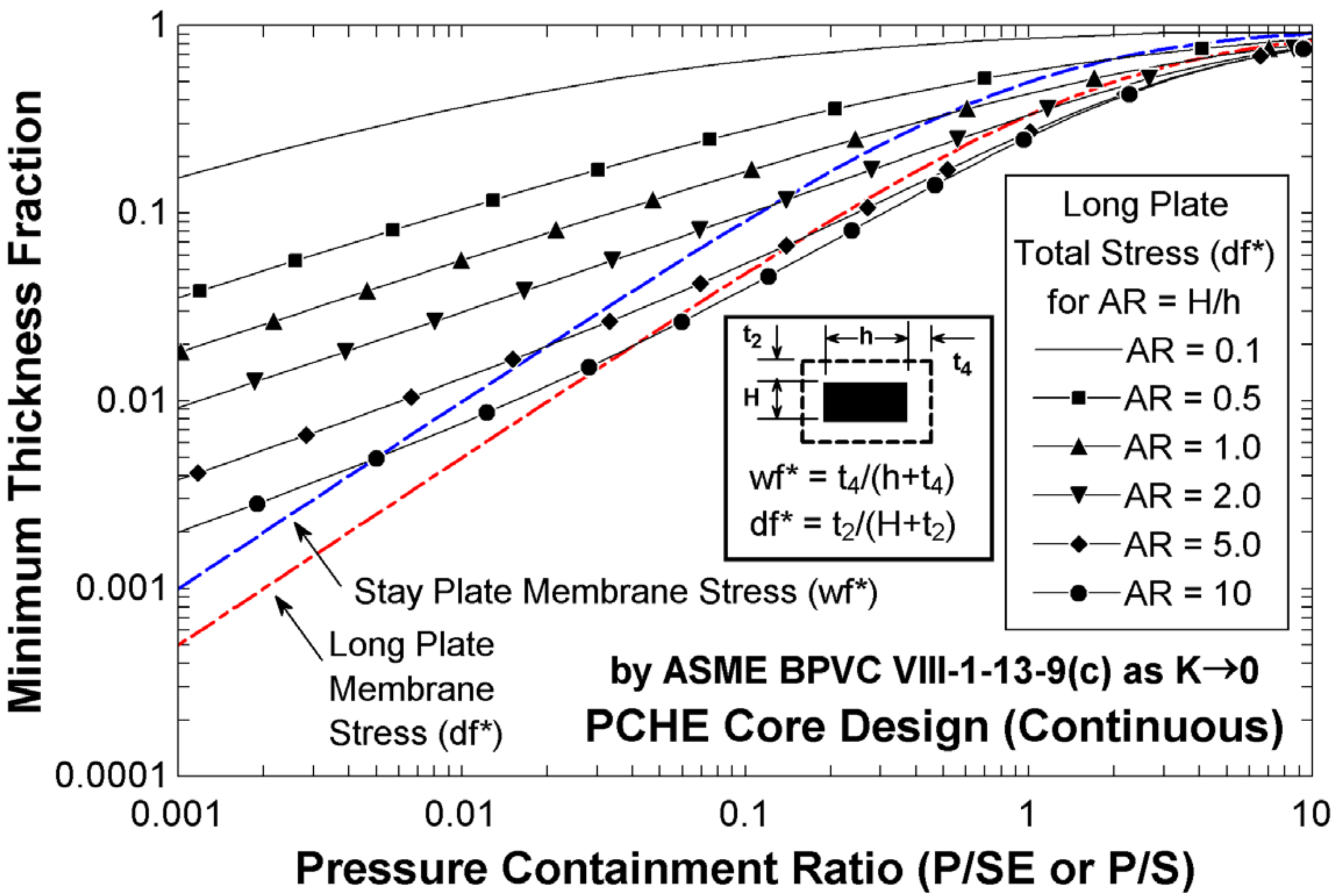
PCHE Core Pressure Containment



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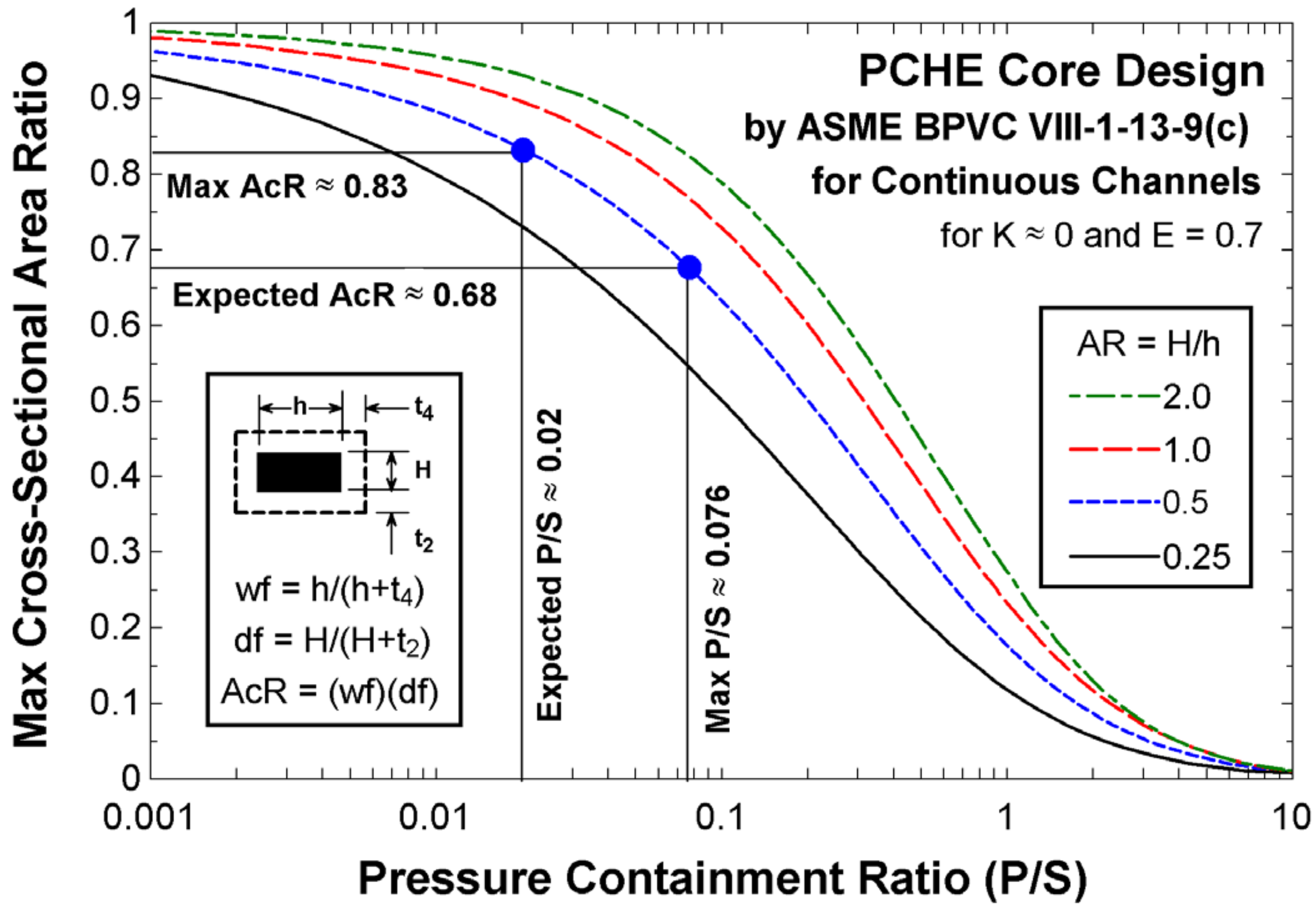
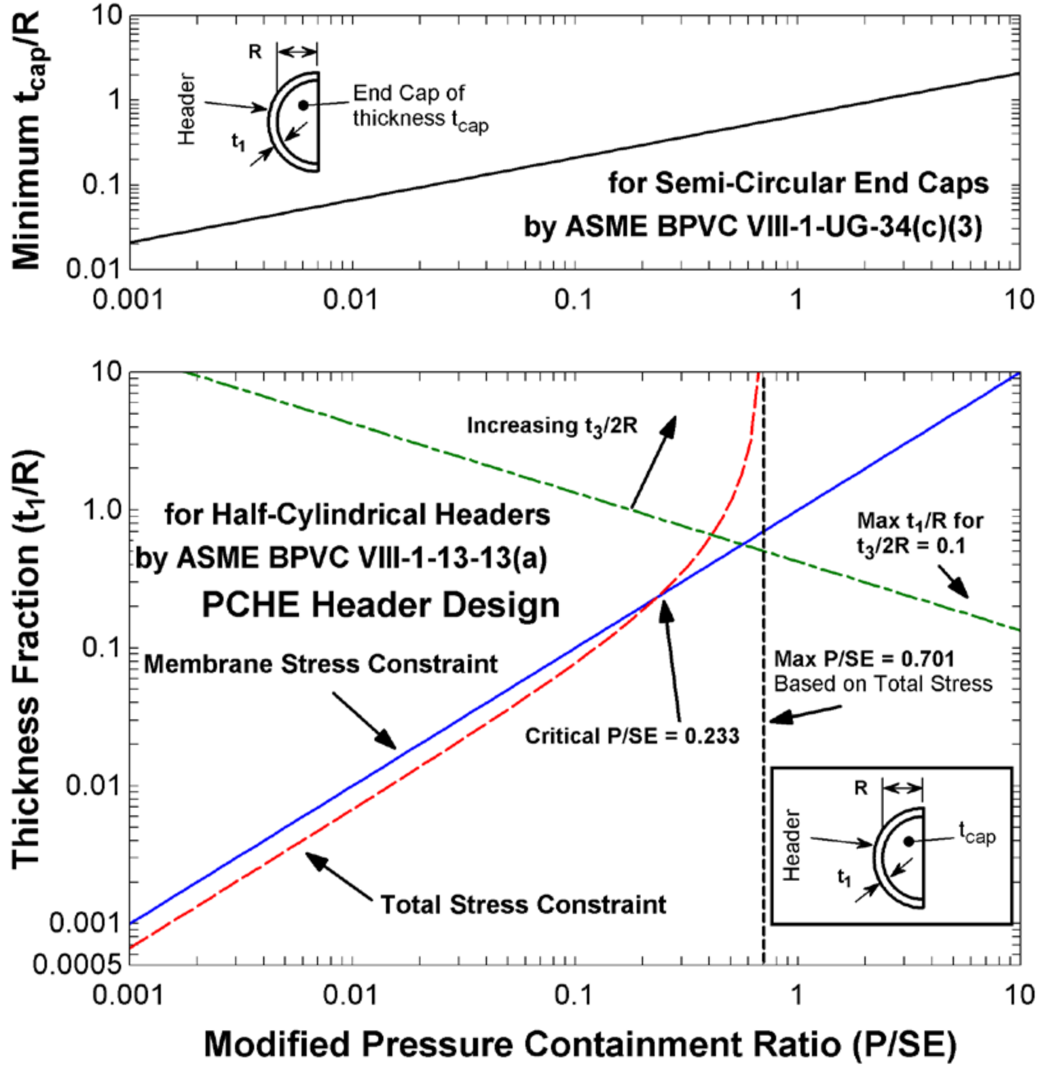


Carlson, M. (2012). *Measurement and Analysis of the Thermal and Hydraulic Performance of Several Printed Circuit Heat Exchanger Channel Geometries* (Master of Science). University of Wisconsin - Madison, Madison, WI.

Half-Cylindrical Headers



Thermal-Hydraulics

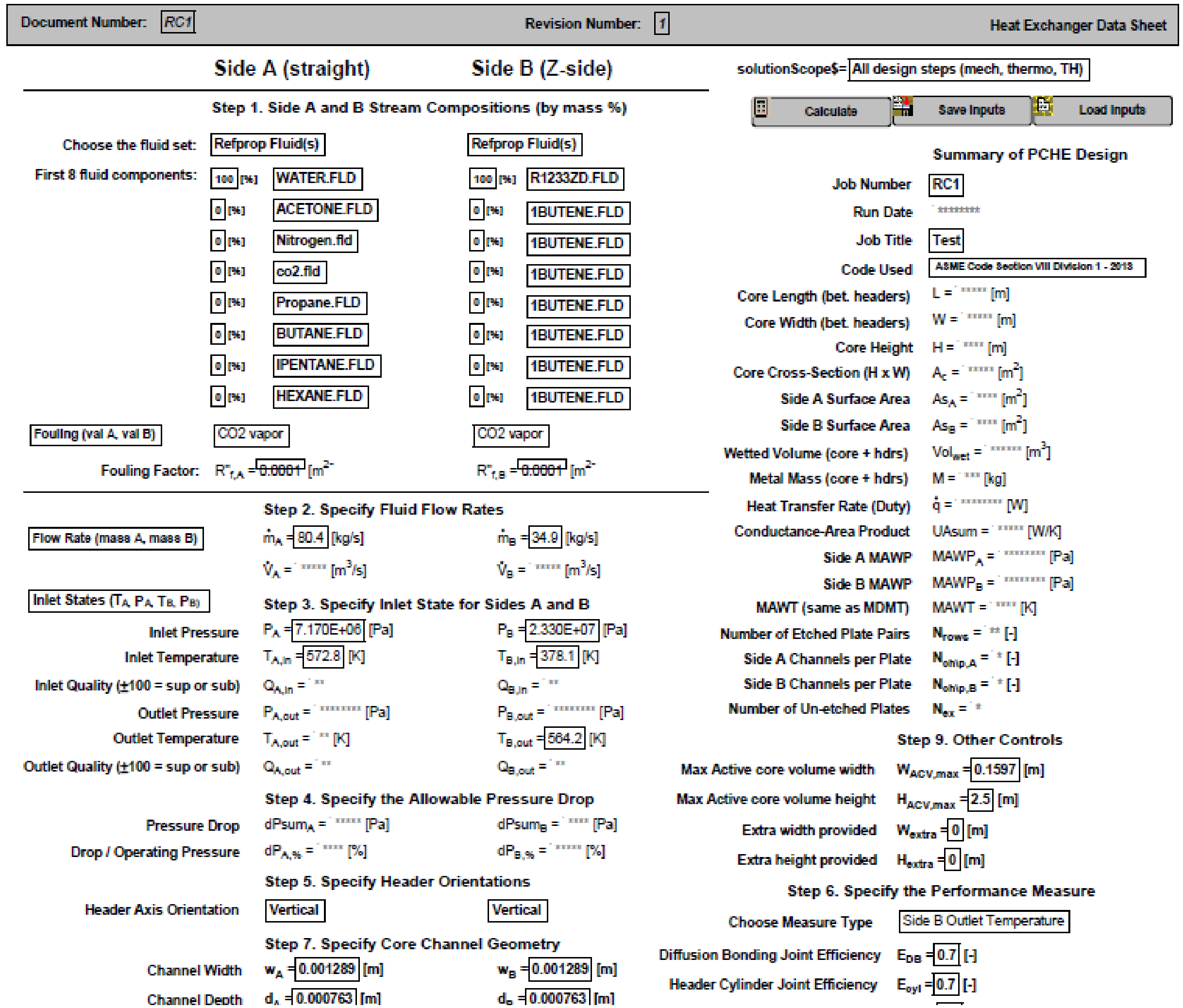
$$\Delta x_i = UA_i \left(\frac{1}{h_{A,i} N_{ch,A} p_{ch,A}} + \frac{R''_{f,A,i}}{N_{ch,A} p_{ch,A}} + \frac{t_m}{k_{m,i} W} + \frac{1}{h_{B,i} N_{ch,B} p_{ch,B}} + \frac{R''_{f,B,i}}{N_{ch,B} p_{ch,B}} \right)$$

(1) (2) (3) (5) (4) (3) (5)

1. Sub-heat exchanger length
2. Sub-heat exchanger conductance-area product
3. Convective thermal resistances
4. Conductive thermal resistance
5. Fouling thermal resistances

PCHE Design Software

- **Sub-hxer model**
- **ASME BPVC**
- **Single, two-phase, supercritical flows**
- **Over 400 fluids**



PROTOTYPE PCHE DESIGN

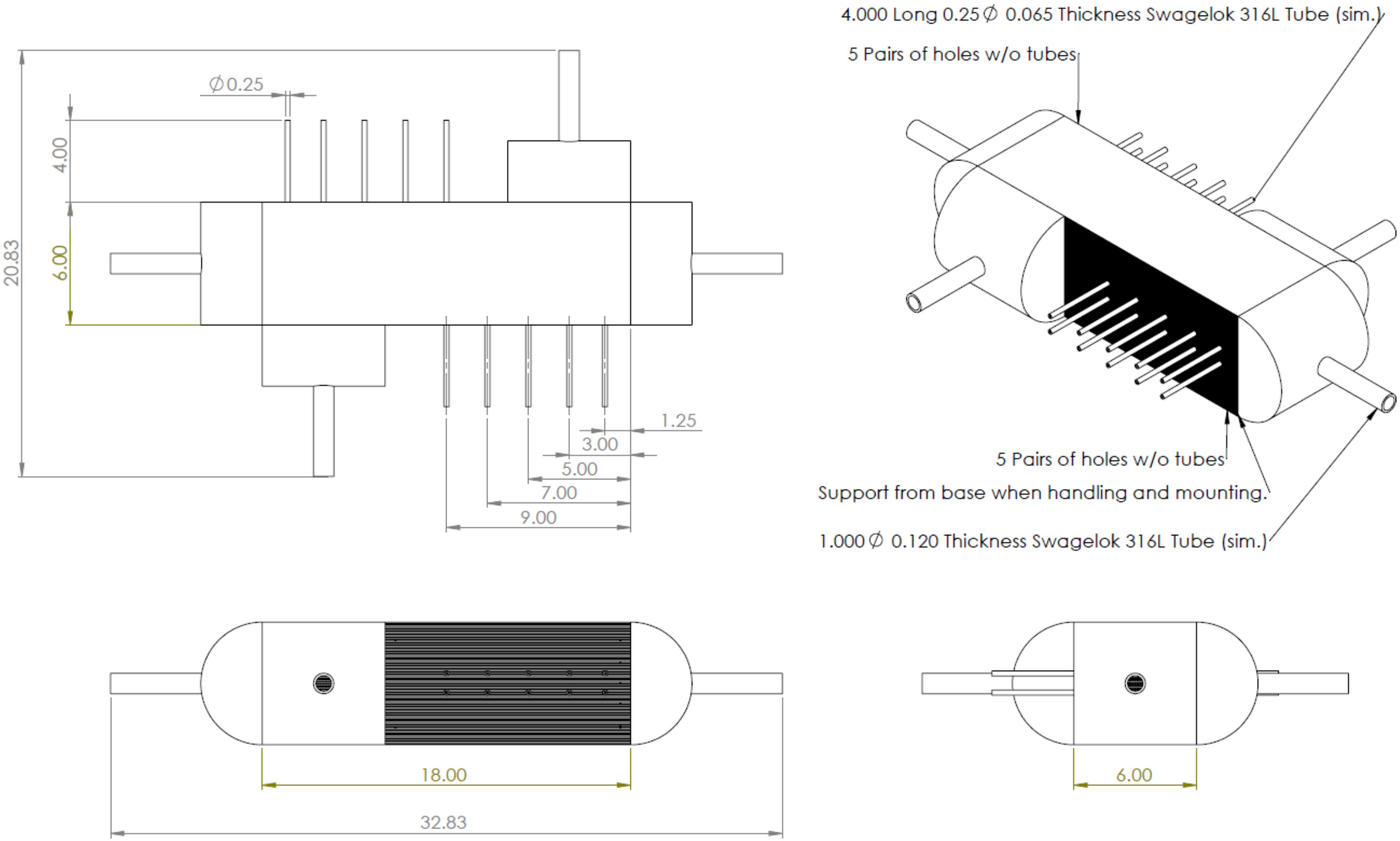
Heat Exchanger Data Sheet

Parameter	Unit	Side A (Straight)	Side B (Z)
Fluid	-	water	water
Mass Flow Rate	kg/s (lbm/hr)	1.5 (12000)	1.5 (12000)
Volumetric Flow Rate	m^3/s (gpm)	1.5e-3 (24)	1.5e-3 (24)
Inlet Temperature	°C (°F)	82 (180)	37 (98)
Inlet Pressure	kPa (psi)	300 (44)	300 (44)
Pressure Drop	kPa (psi)	55 (7.9)	62 (9.0)
Fouling Factor	m^2-K/W	8e-5	8e-5
MAWP	MPa (psi)	20 (2900)	
MAWT	°C (°F)	550 (1000)	
Duty	kW_{th} (Btu/hr)	103 (350000)	
Height x Width x Length	m (in)	0.15 x 0.15 x 0.46 (6 x 6 x 18)	
Active Surface Area	m^2 (in^2)	1.2 (13)	
Material	-	316L Stainless Steel	

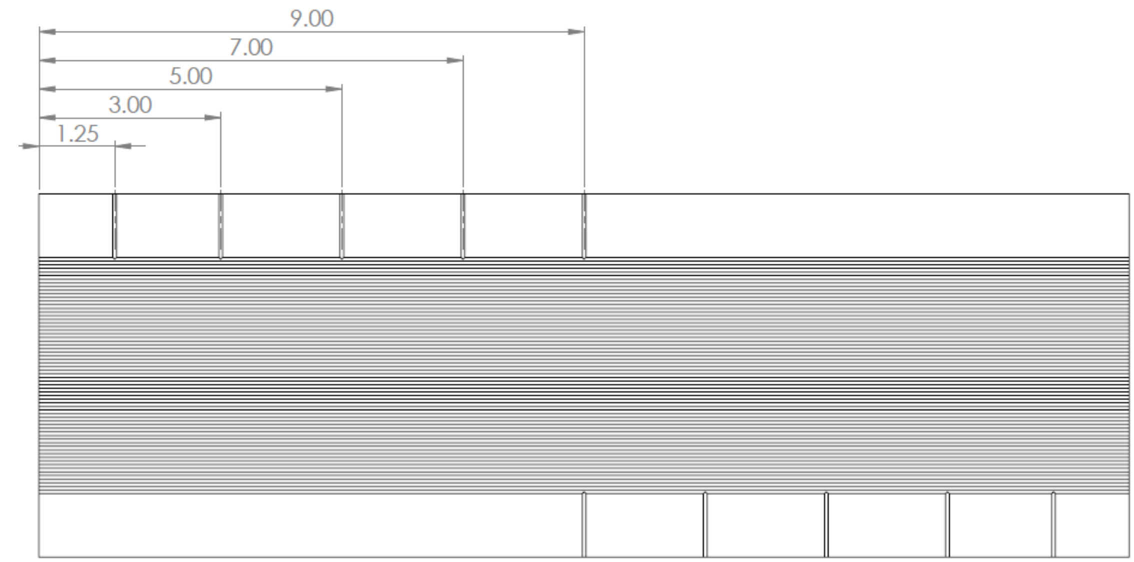
Design for Multiple Phases

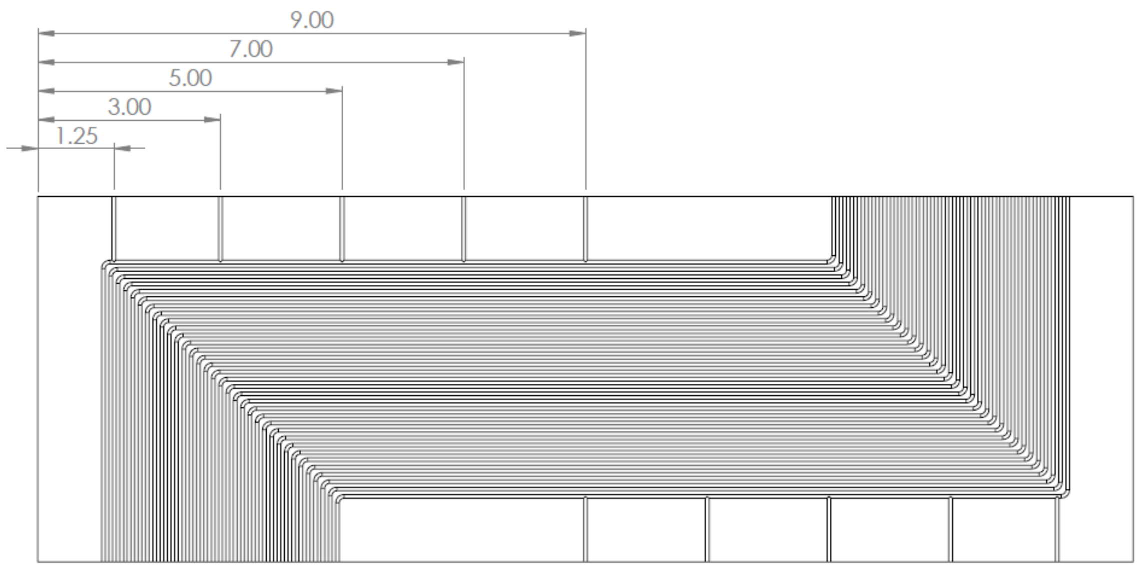
1. Pressure Containment
   - Evaluated by hydrostatic pressure testing
2. Single-phase Thermal Hydraulics
   - Evaluated in the NESL water test loop
3. Supercritical Thermal Hydraulics
   - Evaluated in the NESL sCO2 loop
4. Fatigue Lifetime (to failure)
   - Tested by thermal cycling under pressure

Instrumentation



Instrumentation – Tap Locations

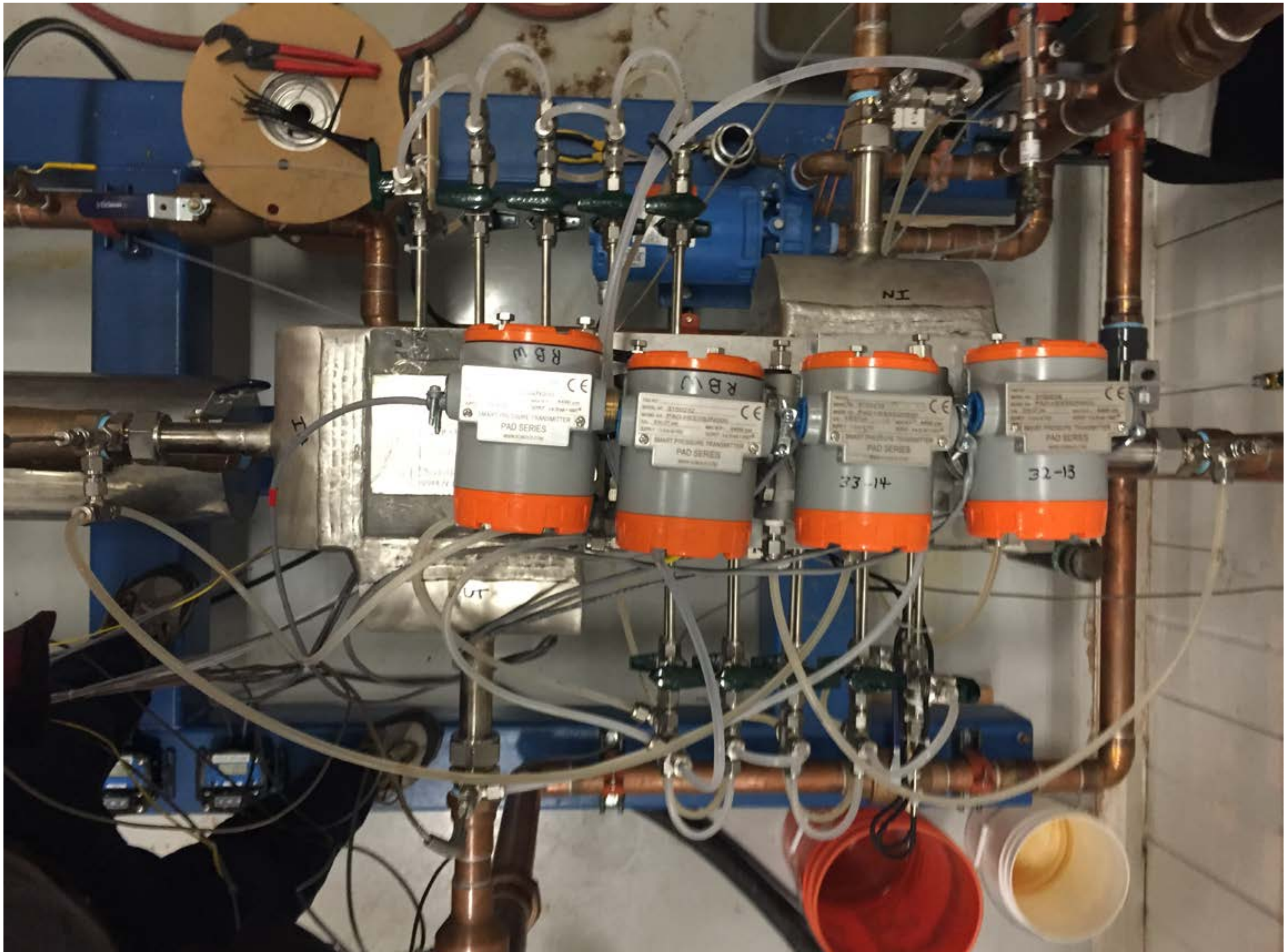




HEAT EXCHANGER TEST PLATFORM

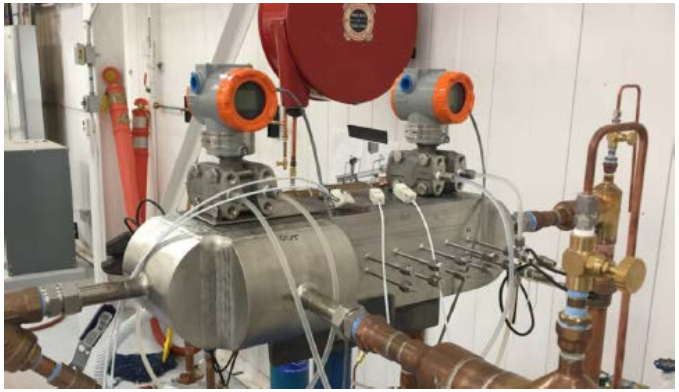
Test Platform Configuration

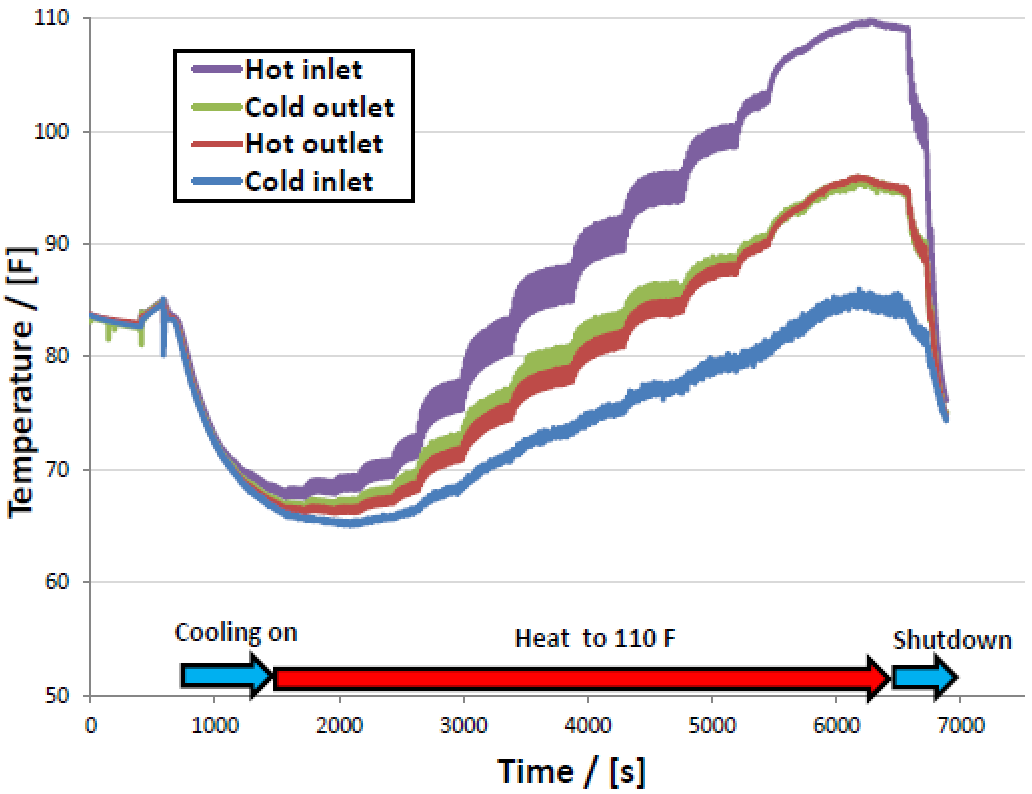
PCHE Instrumentation



PCHE PERFORMANCE COMPARISON

Performance Testing





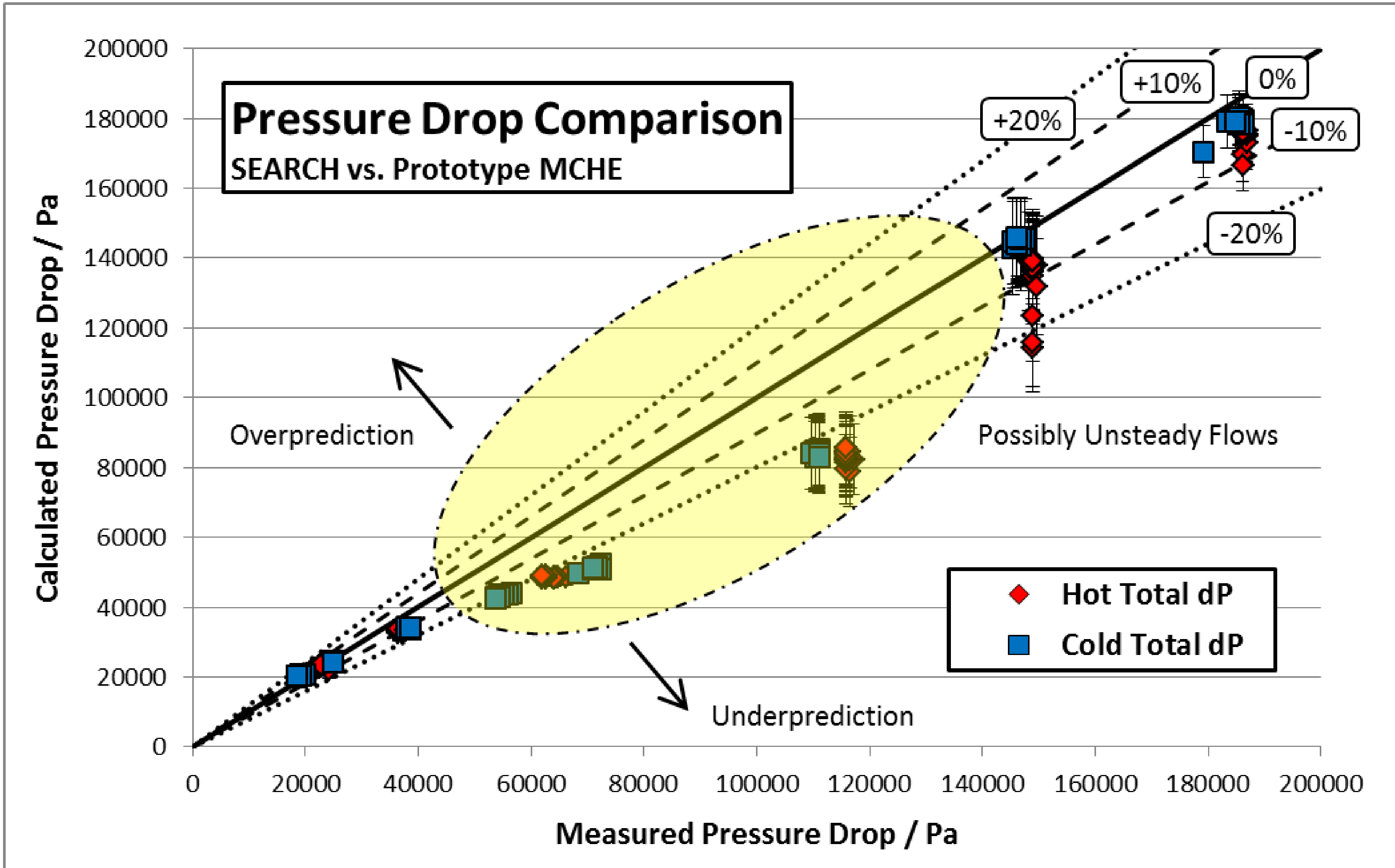
SEARCH appears conservative by at least 10% on q, UA, effectiveness

Performance Comparison

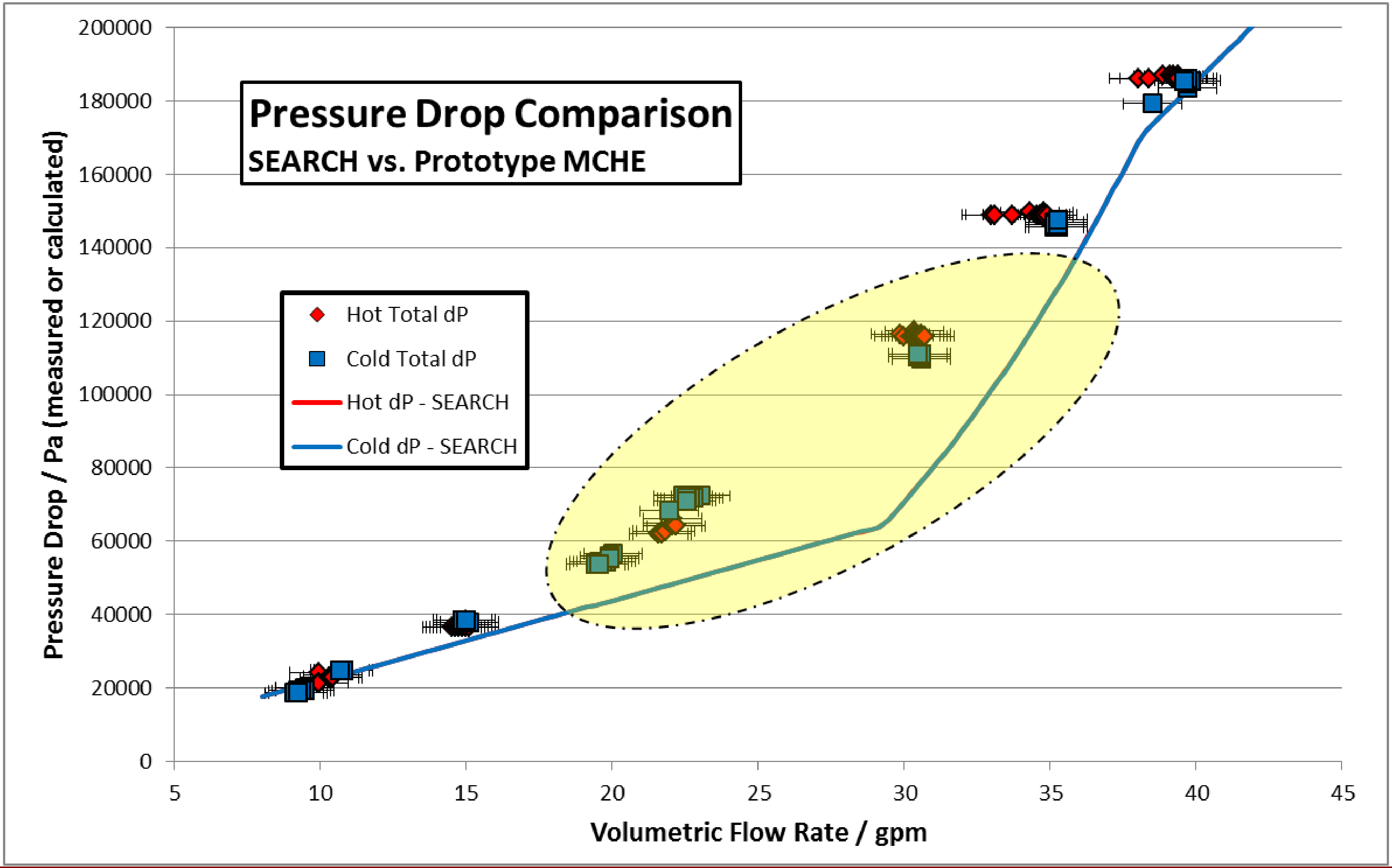
Time Range	Description
0-750	Baseline, prepare to start test. Hot flow started first, wait to reach steady state.
750-1500	Start cooling flow; keep at maximum rate until loop below 70°F.
1500-6500	Increased heater power gradually (5-10% increments) to 100% = 110°F.
6500-7000	Shut off heater power, cooling remains on.

	$\dot{q}$ / W		*UA* / (W/K)		ε	
Time / s	*SEARCH*	*Measured*	*SEARCH*	*Measured*	*SEARCH*	*Measured*
4200	44000	+7%	8100	+13%	43%	+6%
4700	44000	+12%	8200	+23%	43%	+11%
5100	54000	+13%	8400	+26%	43%	+12%
5400	61000	+14%	8500	+28%	44%	+13%
5700	67000	+14%	8600	+27%	44%	+13%
6260	67000	+16%	8700	+32%	44%	+15%

Calculated vs. Meas. Pressure Drop



Pressure Drop Prediction Capability



Conclusions

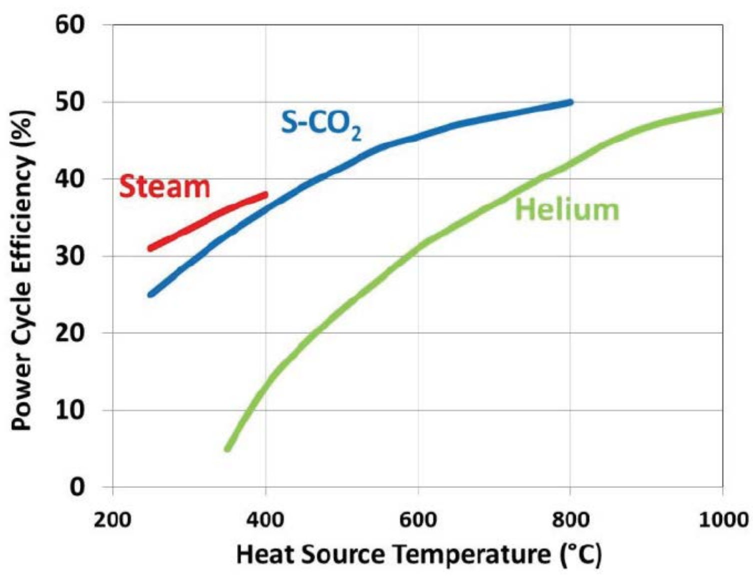
- Based on our first set of tests:
  - SEARCH is within 25% accuracy on key metrics
  - Thermal performance is predicted conservatively
  - Pressure drop is under-predicted in some regimes
- These results have already been applied
- Testing is planned after loop upgrades
  - Additional thermal-hydraulic observations
  - Intermediate state (T & P) profiles
  - Future test phases (sCO2, fatigue)

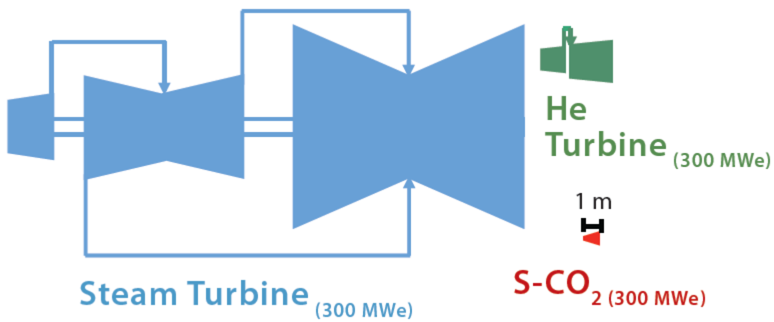
BACKUP SLIDES

The Argument for SCO2 Brayton

Versus Helium and Steam

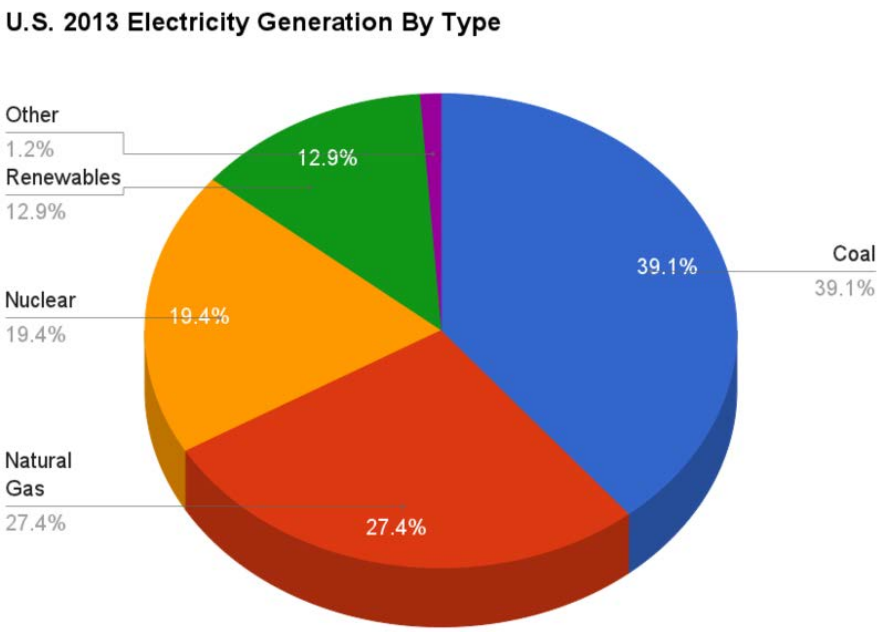
1. Higher efficiency
   - Sodium Fast Reactor operating at 550 °C
   - Concentrated Solar Power up to 700 °C
   - CCS Gasified Coal and Natural Gas up to 1150 °C
2. Compact turbomachinery
   - Smaller system footprint
   - Possibly reduced cost

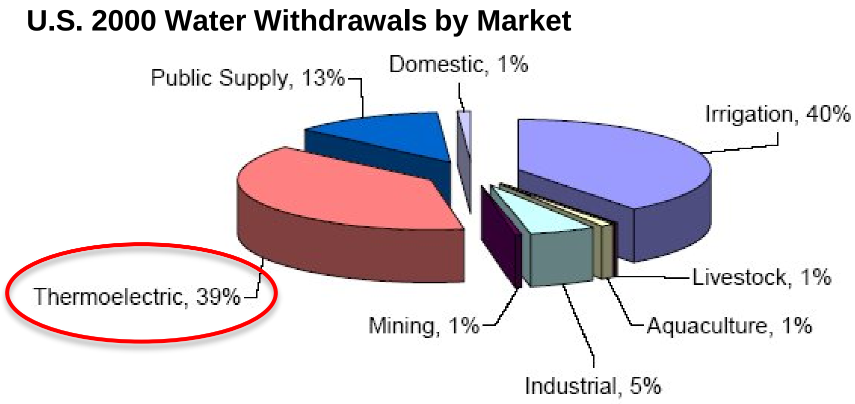




Current Electrical Generation

- Electrical Generation
  - Dominated by fossil
  - Nuclear is a critical part
  - Expected that natural gas and nuclear will grow; coal will shrink
- Two main technologies
  - Steam Rankine cycle
    - Coal, Nuclear, CCNG
  - Gas Brayton cycle
    - Natural gas





Supercritical CO_2 (sCO_2) Brayton Cycle

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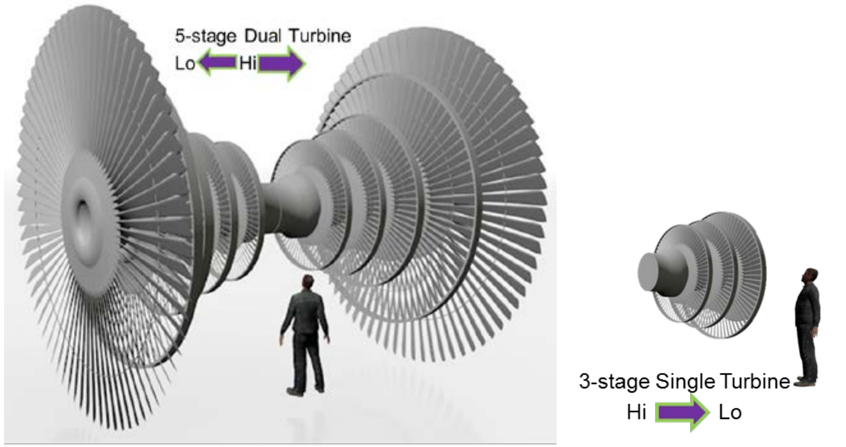
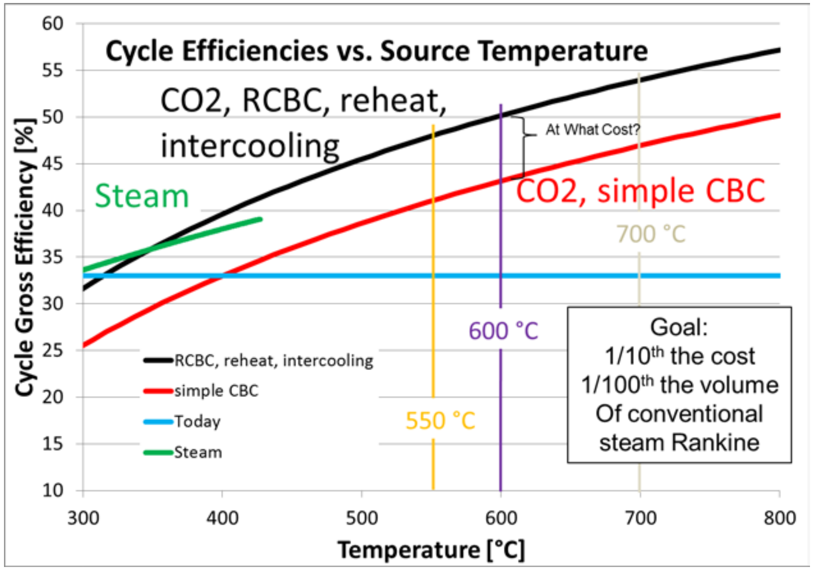
- Key Advantages over Steam
  - Smaller turbomachinery
  - Single-phase fluid (no quality issues)
  - Recuperation becomes practical



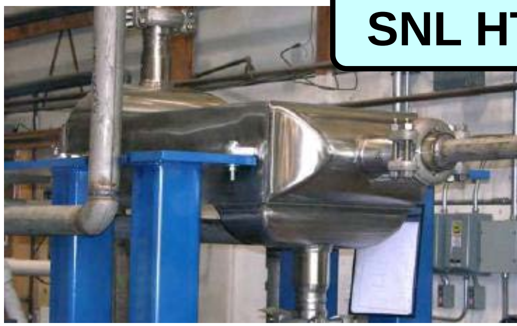
20 meter Steam Turbine (300 MWe) (Rankine Cycle)

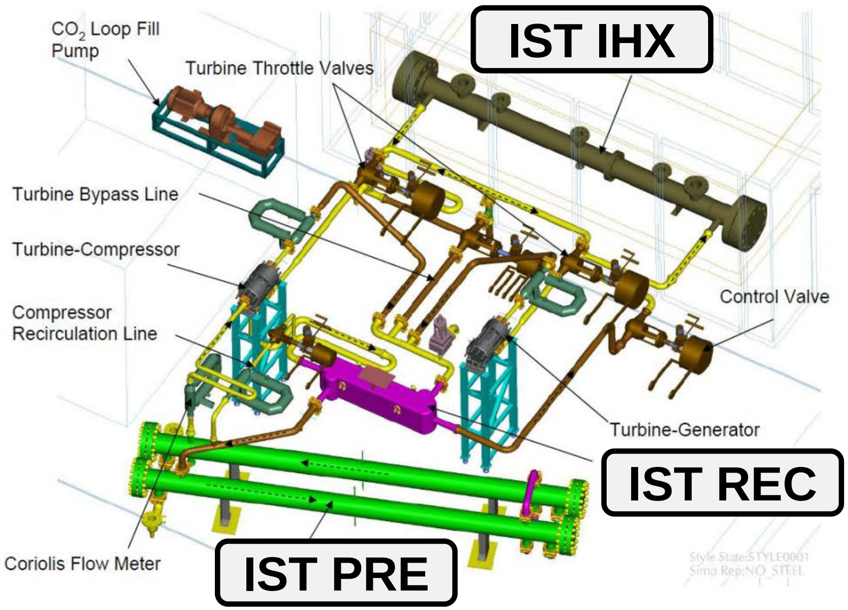
1 meter sCO_2 (300 MWe) (Brayton Cycle)

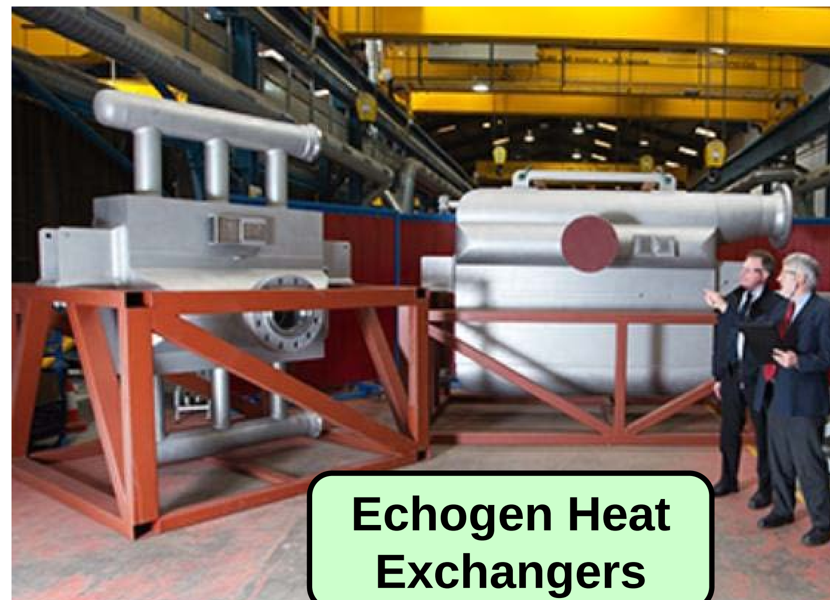
- Key Advantages over Gas
  - High efficiency at low temperatures
  - Lower compression work
  - Smaller turbomachinery



Current SCO2 CBC HXers







G. O. Musgrove, C. Pittaway, D. Shiferaw, and S. Sullivan, “Tutorial: Heat Exchangers for Supercritical CO2 Power Cycle Applications,” San Antonio, Texas, USA, 03-Jun-2013.

Commercial Unit Potential

Key Requirements:
- ✓ High Pressure
- ✓ High Temperature
- ✓ Corrosion Resistant
- ✓ High Reliability
- ✓ Compact Geometry
- ✓ Scalable to 150 MWe

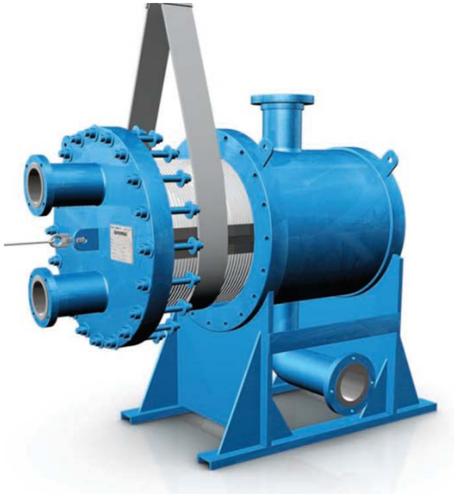
$$\beta = \frac{A_s}{V} = \frac{4\phi}{d_h}$$

Coil-Wound
10 to 300 [m^2/m^3]

Shell and Tube
10 to 200 [m^2/m^3]

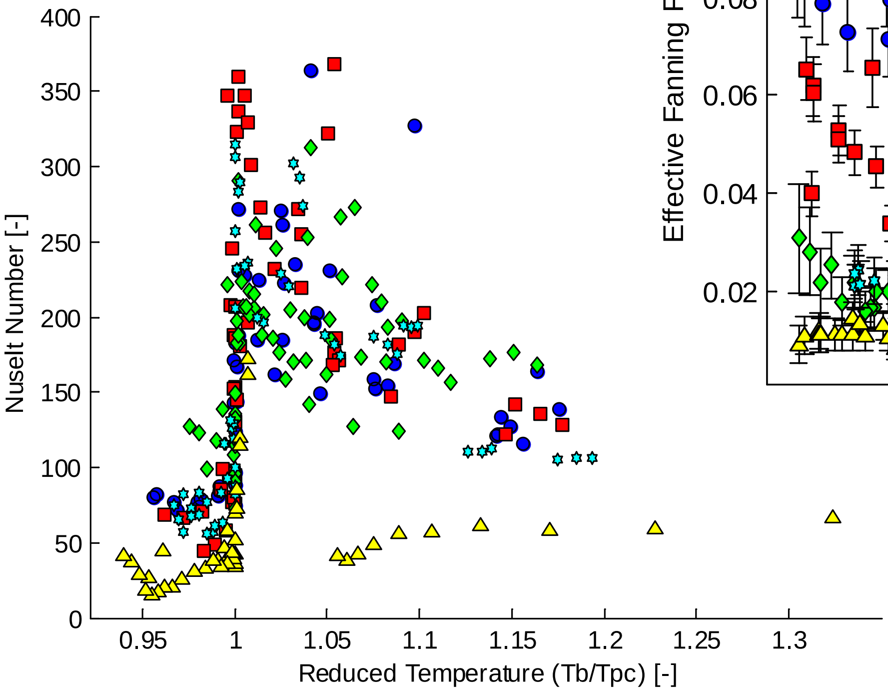
Plate-Fin
200 to 800 [m^2/m^3]

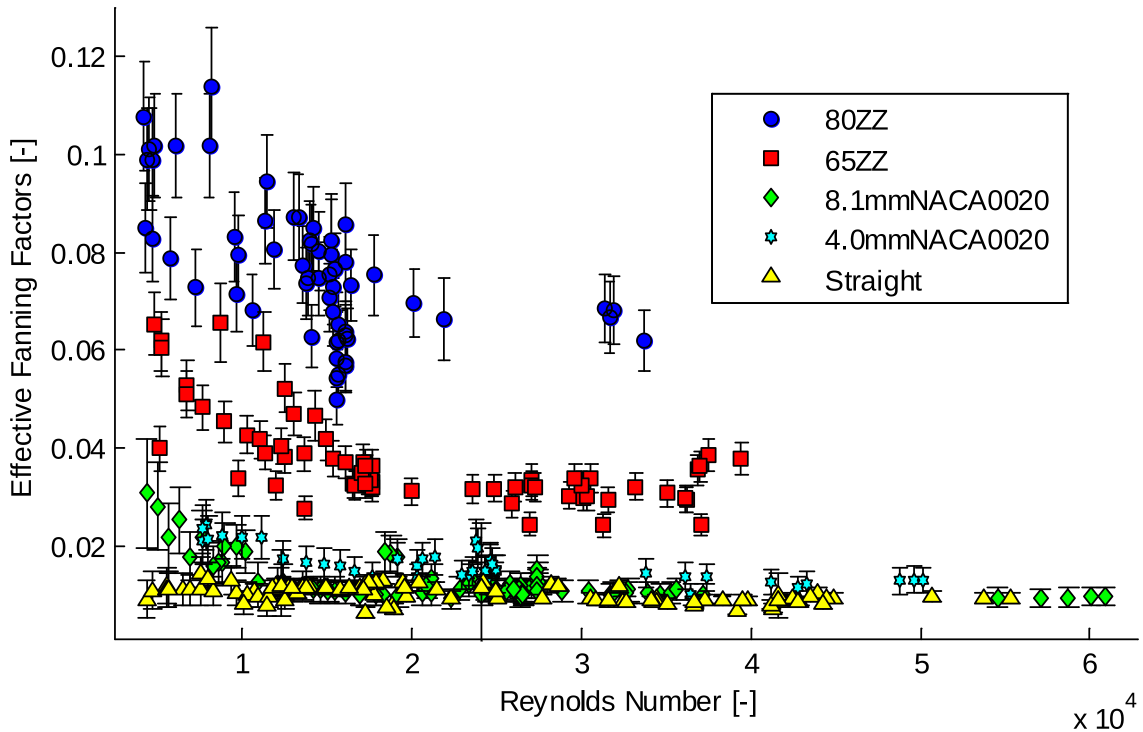
Printed Circuit
200 to 5000 [m^2/m^3]

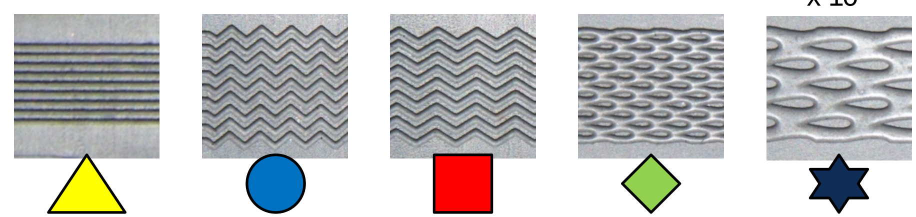


Shell and Plate
100 to 600 [m^2/m^3]

PCHE Thermal-Hydraulic Performance







Carlson, M. (2012). *Measurement and Analysis of the Thermal and Hydraulic Performance of Several Printed Circuit Heat Exchanger Channel Geometries* (Master of Science). University of Wisconsin - Madison, Madison, WI.

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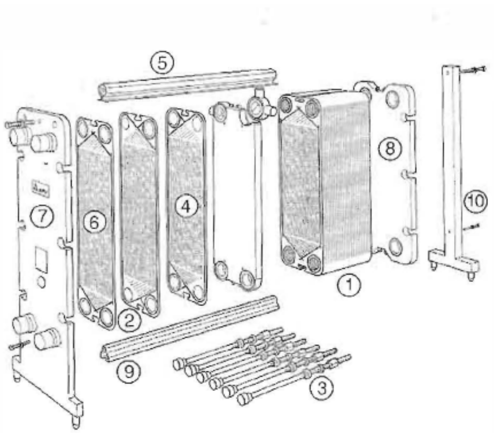
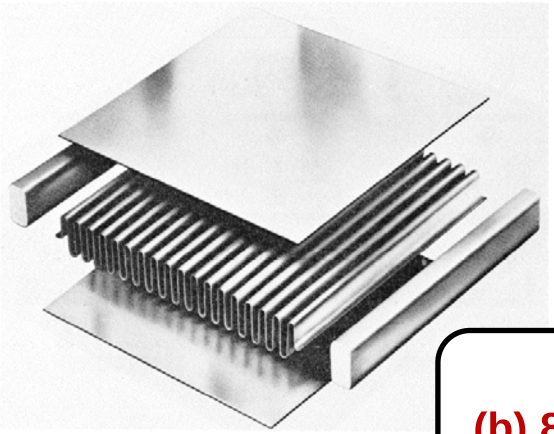
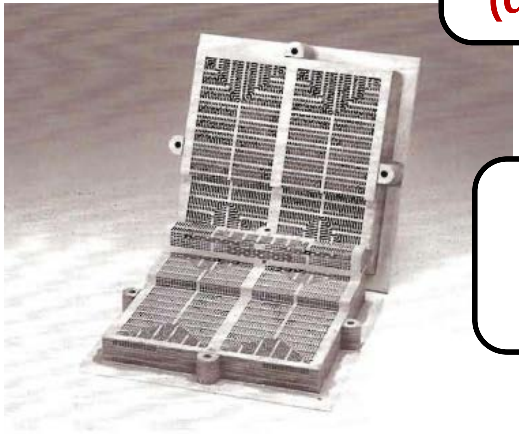
PHE
120 to 660





PFHE
(b) 800 to 1500
(d) 700 to 800

PCHE
(d) 200 to 5000



CBHE
(Marbond)
Up to 10000

HEAT EXCHANGER COMPACTNESS

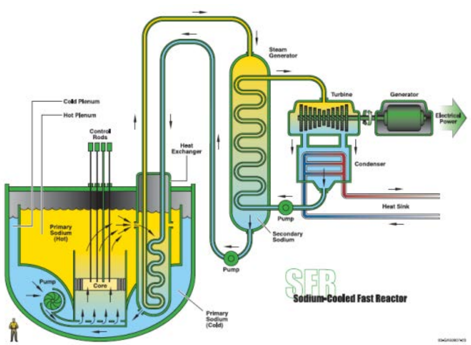
Surface Area Density: $\beta = \frac{A_s}{V} = \frac{4\phi}{d_h}$

Potential Applications

Coal / Nuclear
Steam Rankine

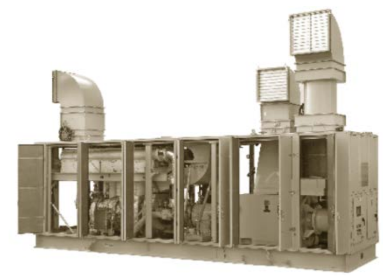
MARINE
Rolls-Royce WR-21
Type 45 Destroyer

VEHICULAR
Honeywell AGT1500
M1 Abrams Tank



GenIV Nuclear
Sodium Fast Reactor

Refrigeration
Commercial, Cryogenic



STATIONARY
Solar Turbines
Mercury 50

Effectiveness and Scaling Behavior

$$\dot{q} = UA\Delta T = \varepsilon(\dot{m}\bar{c}_p)_{min}(T_{H,in} - T_{C,in})$$

Heat Transfer Rate

Heat Transfer Surface Area

Temperature Differential

Hot Inlet

Cold Inlet

Overall Heat Transfer Coefficient

Effectiveness

Mass Flow Rate

Specific Heat Capacity

Minimum of the hot- and cold-side flow mass flow rate and specific heat capacity product (capacitance rates)

Fundamental Scaling Behavior

Sandia National Laboratories

Heat Transfer Rate

Heat Transfer Surface Area

Temperature Differential

$$\dot{q} = UA\Delta T$$

Overall Heat Transfer Coefficient

Fundamental Scaling Behavior

$$\dot{q} = UA\Delta T$$

Fluid	Transmission Surface	Fluid	Overall Heat Transmission Coefficient	
			(Btu/ft^2 hr ^{o}F)	*(W/m^2 K)*
Water	Cast Iron	Air or Gas	1.4	7.9
Water	Mild Steel	Air or Gas	2.0	11.3
Water	Copper	Air or Gas	2.3	13.1
Water	Cast Iron	Water	40 - 50	230 - 280
Water	Mild Steel	Water	60 - 70	340 - 400
Water	Copper	Water	60 - 80	340 - 455
Air	Cast Iron	Air	1.0	5.7
Air	Mild Steel	Air	1.4	7.9
Steam	Cast Iron	Air	2.0	11.3
Steam	Mild Steel	Air	2.5	14.2
Steam	Copper	Air	3.0	17
Steam	Cast Iron	Water	160	910
Steam	Mild Steel	Water	185	1050
Steam	Copper	Water	205	1160
Steam	Stainless Steel	Water	120	680

Effectiveness and Scaling Behavior

Heat Transfer Rate

Hot Inlet

Cold Inlet

$$\dot{q} = UA\Delta T = \varepsilon\left(\dot{m}\bar{c}_p\right)_{min}\left(T_{H,in} - T_{C,in}\right)$$

Effectiveness

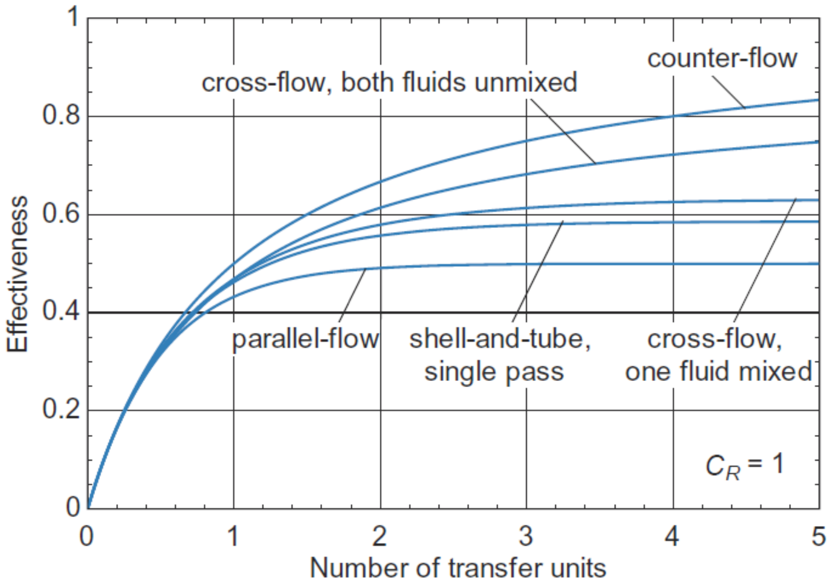
Mass Flow Rate

Specific Heat Capacity

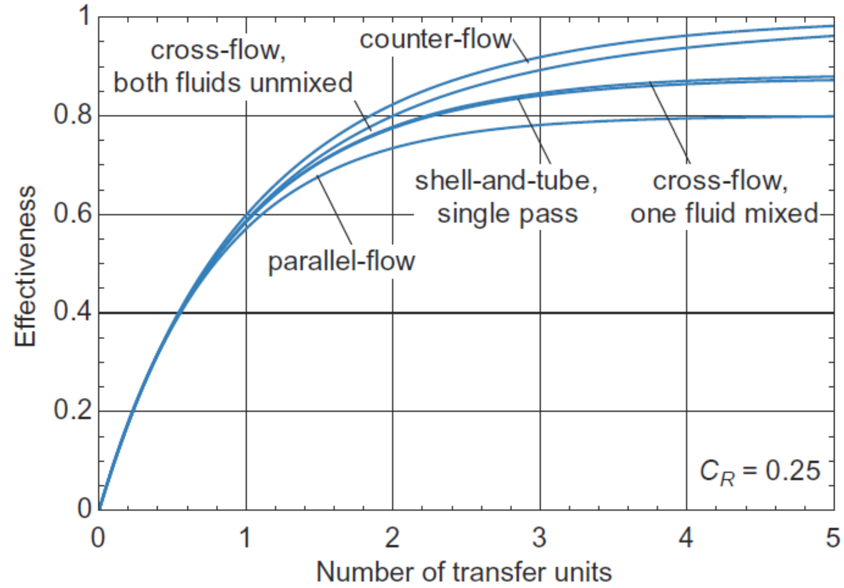
Minimum of the hot- and cold-side flow mass flow rate and specific heat capacity product (capacitance rates)

Other Useful e-NTU Scaling

- Configuration matters most for C_R = 1; counter-flow is best
- Effectiveness is asymptotic with NTU (size); 1 for counter-flow
- Configuration matters less as C_R approaches 0



C_R = 1



C_R = 0.25

Pressure Drop Correlations

$$\Delta P = \sum \Delta P_{friction} + \sum \Delta P_{local} + \sum \Delta P_{acceleration} + \sum \Delta P_{body\ \ forces}$$

- Body Forces

$$\Delta P_{gravity} = g\left(\frac{i_{out}\,\rho_{out} + i_{in}\,\rho_{in}}{i_{out} + i_{in}}\right) L sin(\theta)$$

- Local Form Losses

$$\frac{\Delta P_{local}}{G^2/2\rho} = K_{loss} = f\left(\frac{L_{equivalent}}{d_{hyd}}\right)$$

- Acceleration Difference

$$\Delta P_{acceleration} = G^2\left(\frac{1}{\rho_{out}} - \frac{1}{\rho_{in}}\right)$$

$$\Delta P_{friction} = f\,\frac{L_s}{d_{hyd}}\,\frac{1}{2}\,\frac{G^2}{\rho}$$

Blasius

$$f = 0.316Re^{-0.25}$$

Kondrat'ev

$$f = 0.188Re^{-0.22}$$

Haaland

$$f = \frac{1}{\left(1.8\log_{10}\left[\left(\frac{RR}{3.7}\right)^{1.11} + \frac{6.9}{Re}\right]\right)^2}$$

Filonenko

$$f = \frac{1}{(1.82\log_{10} Re_b - 1.64)^2}$$

Colebrook Equation

$$\frac{1}{\sqrt{f}} = -2\log_{10}\left(\frac{RR}{3.7} + \frac{2.51}{Re\sqrt{f}}\right)$$

Heat Transfer Correlations

Constant Property

Dittus-Boelter Correlation

$$Nu = C\, Re^n Pr^m$$

Gnielinski Correlation

$$Nu = \frac{\left(\frac{f}{8}\right)(Re - 1000)Pr}{1 + 12.7\sqrt{\frac{f}{8}}\left(Pr^{\frac{2}{3}} - 1\right)}$$

Supercritical Fluids

Jackson's Correlation

$$Nu = 0.0183 Re_b^{0.82} Pr_b^{0.5} \left(\frac{\rho_w}{\rho_b}\right)^{0.3} \left(\frac{\bar{c}_p}{c_{p,b}}\right)^n$$

Pitla Correlation

$$Nu = \left(\frac{Nu_w|_{Gnielinski} + Nu_b|_{Gnielinski}}{2}\right)\frac{k_w}{k_b}$$