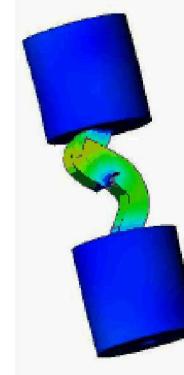


Nonlinear Modal Analysis and Dynamics
with Applications to Nuclear Power Plants

Nonlinear Modal Analysis
with Applications to Nuclear Power Plants

N=O=MAD



Influences of Modal Coupling on Nonlinear Modal Models

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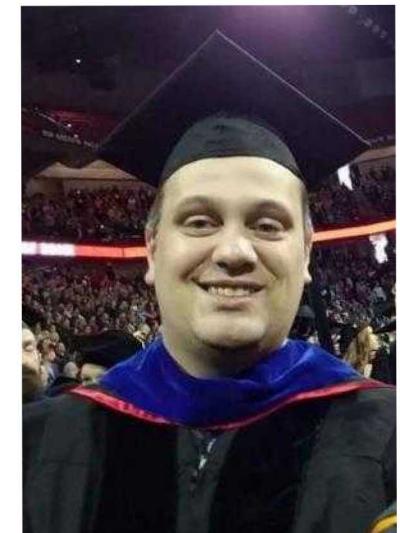
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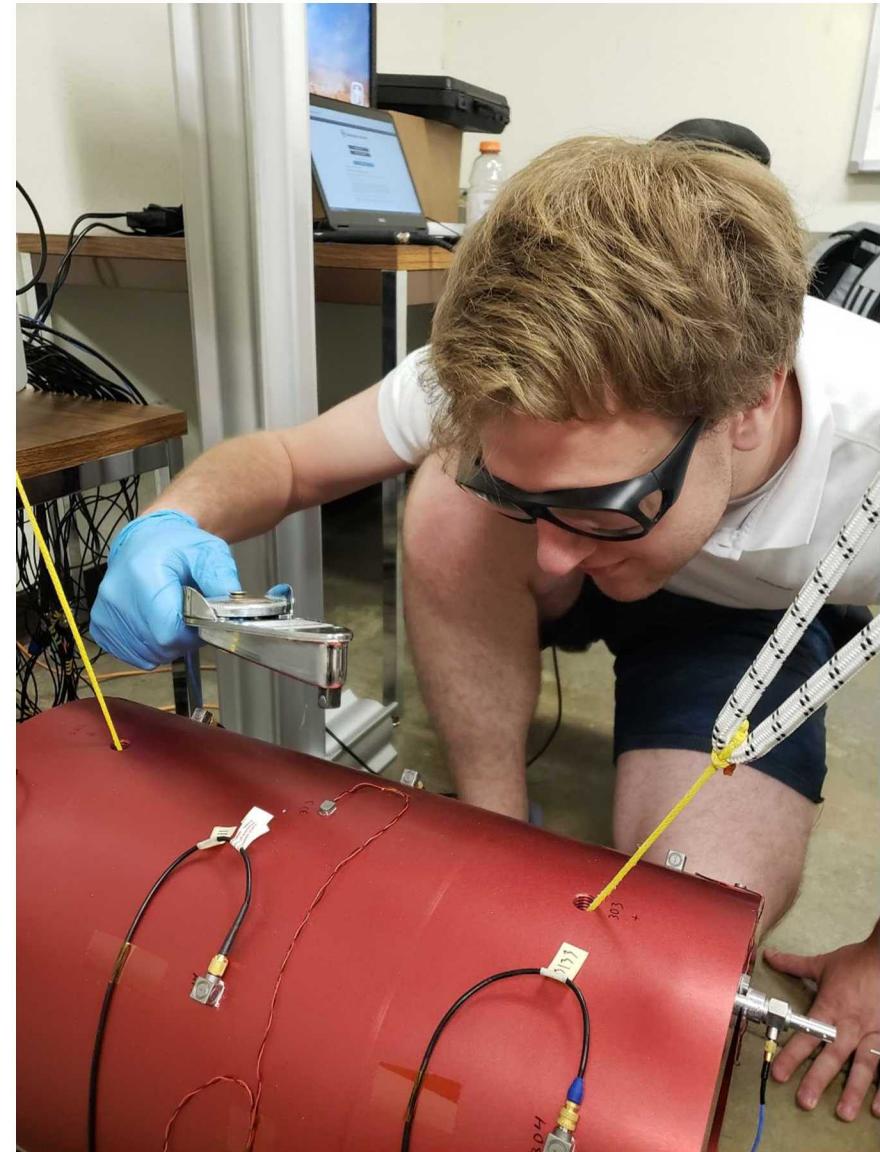
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Agenda

1. Motivation
2. Test Structure
3. Experimental Process
 - a. Linear Testing
 - b. Nonlinear Testing
4. Nonlinear Coupling Data
5. Closing Remarks



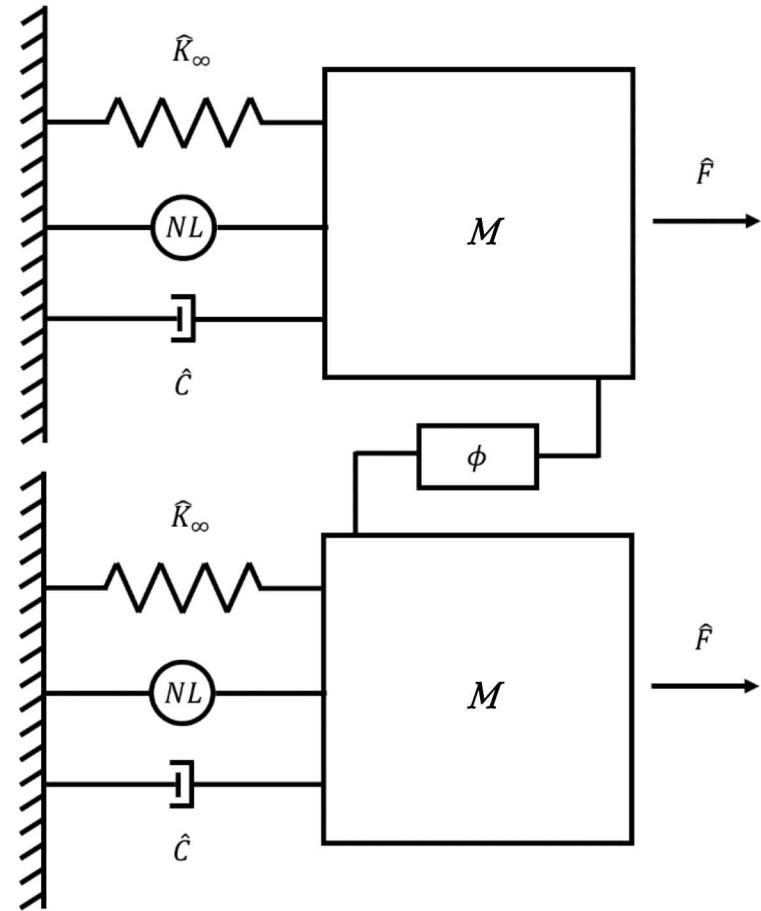
Linear vs. Nonlinear Systems

- Linear analysis assumes:
 - Small deformations
 - Response is amplitude independent
 - Modal responses can be superimposed
 - $\ddot{q}_r + 2\zeta_r\omega_r\dot{q}_r + \omega_r^2 q_r = \Phi^T F_{ext}$
- Pseudo – Nonlinear analysis assumes:
 - Shapes of the linear modes are preserved
 - Linear modes can decouple nonlinear data
 - Coupling between modes is negligible and no energy is transferred between modes
 - $\ddot{q}_r + 2\zeta_r\omega_r\dot{q}_r + \omega_r^2 q_r + F_{nl}(q_r, \dot{q}_r) = \Phi^T F_{ext}$

What happens if there is coupling between the modes?

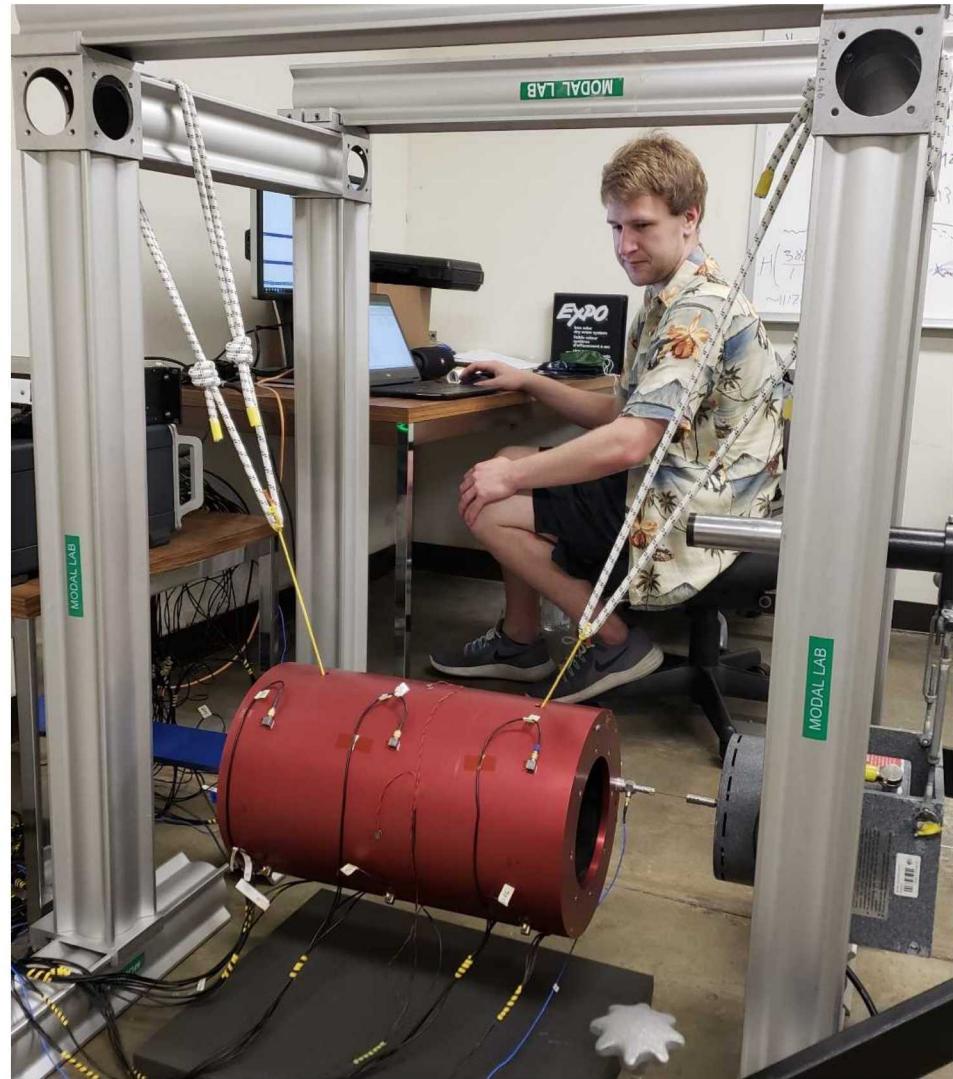
Modal Coupling

- Excitation of one mode causes a transfer of energy that perturbs another mode
- Usually occurs due to interactions at joints shared by different mode shapes



Project Objectives

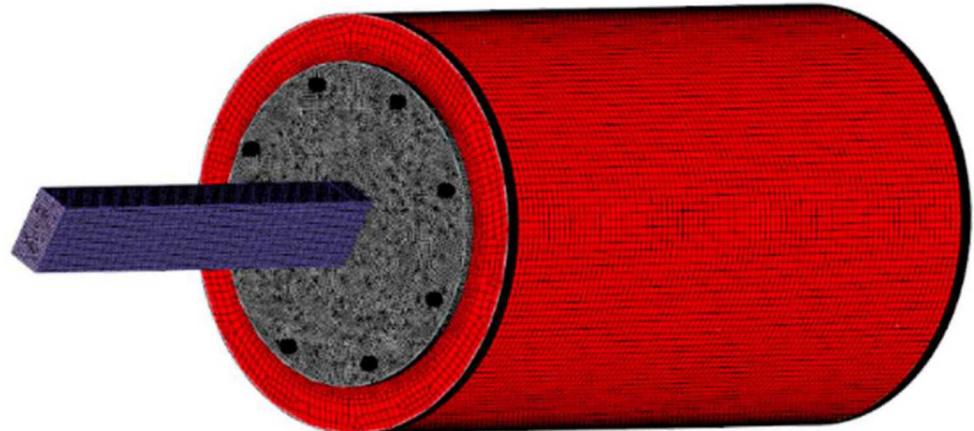
- Excite combinations of modes on a nonlinear structure
- Experimentally identify the presence modal coupling
- Collect data for use in validating computer models of coupling



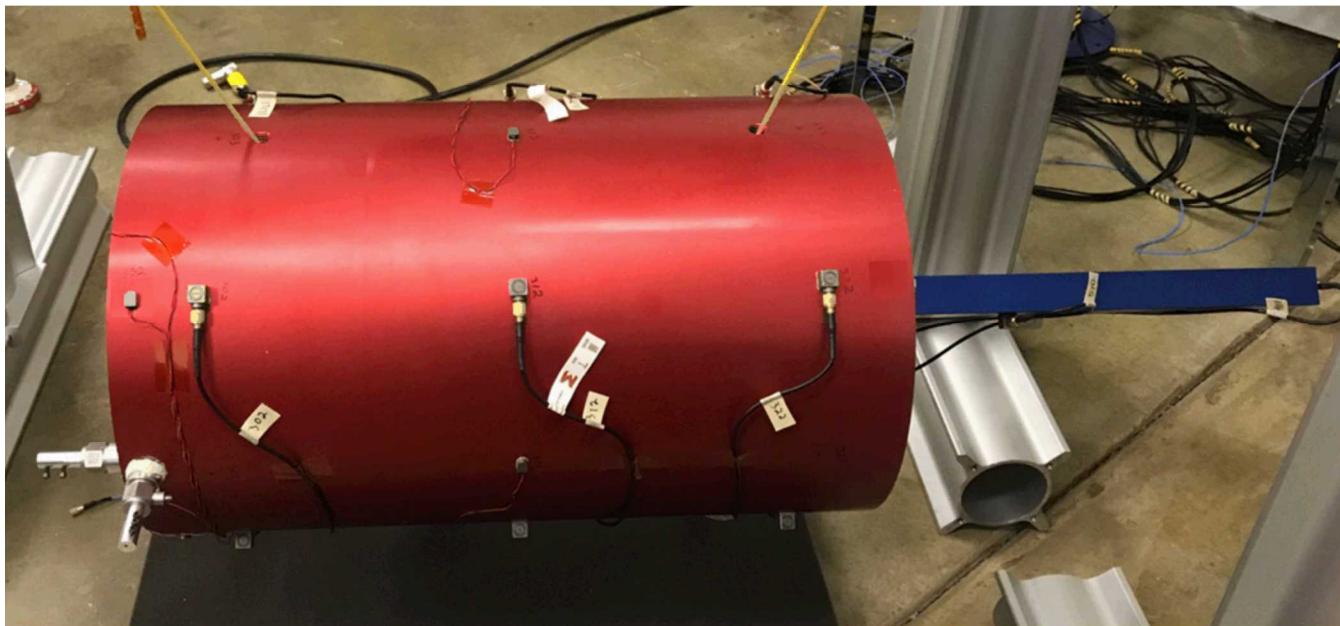
Test Structure

Cylinder – Plate – Beam (CPB)

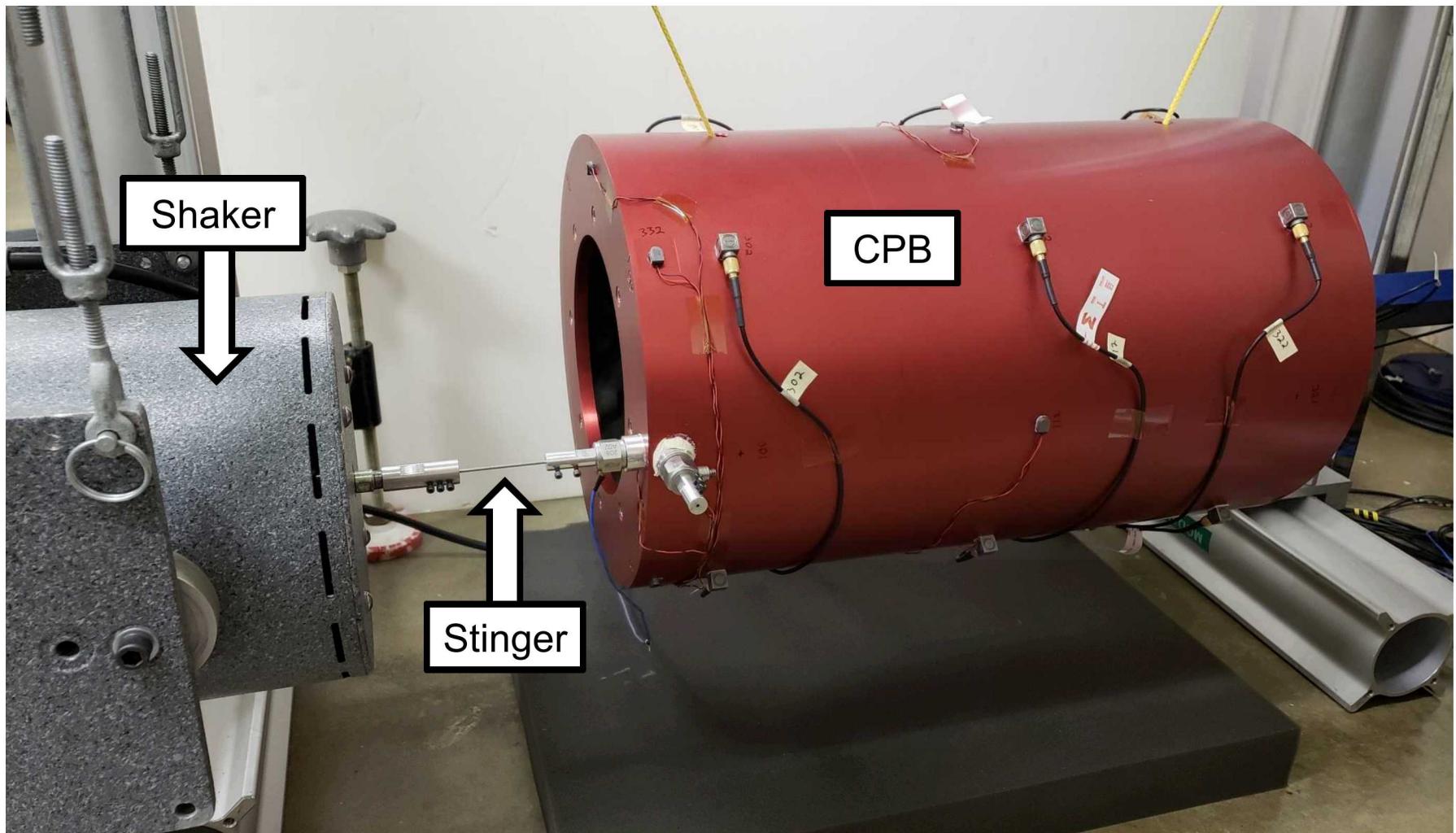
- Plate bolted to cylinder
- Beam bolted and glued to plate



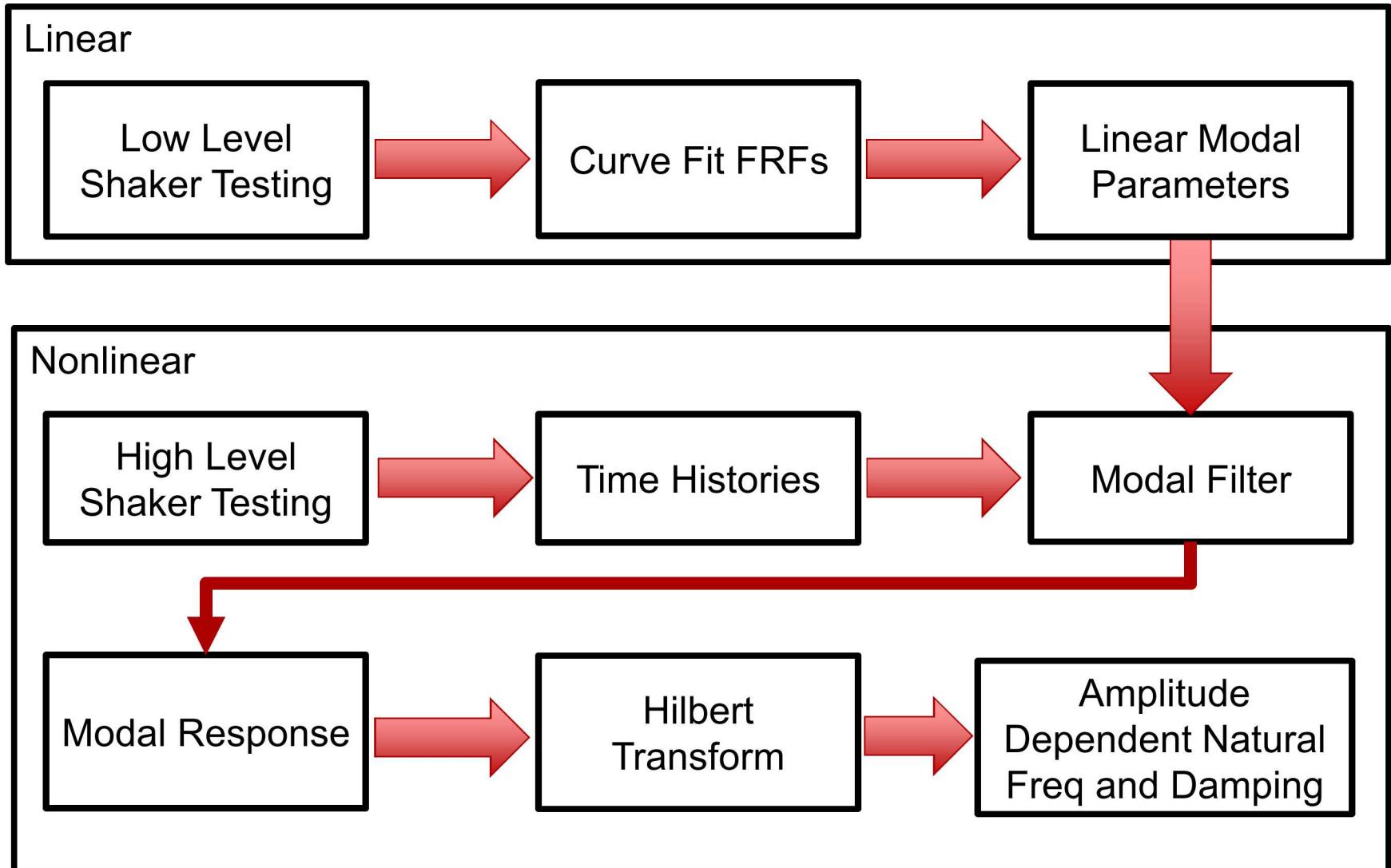
18 triaxial + 8 uniaxial accelerometers



Experimental Setup

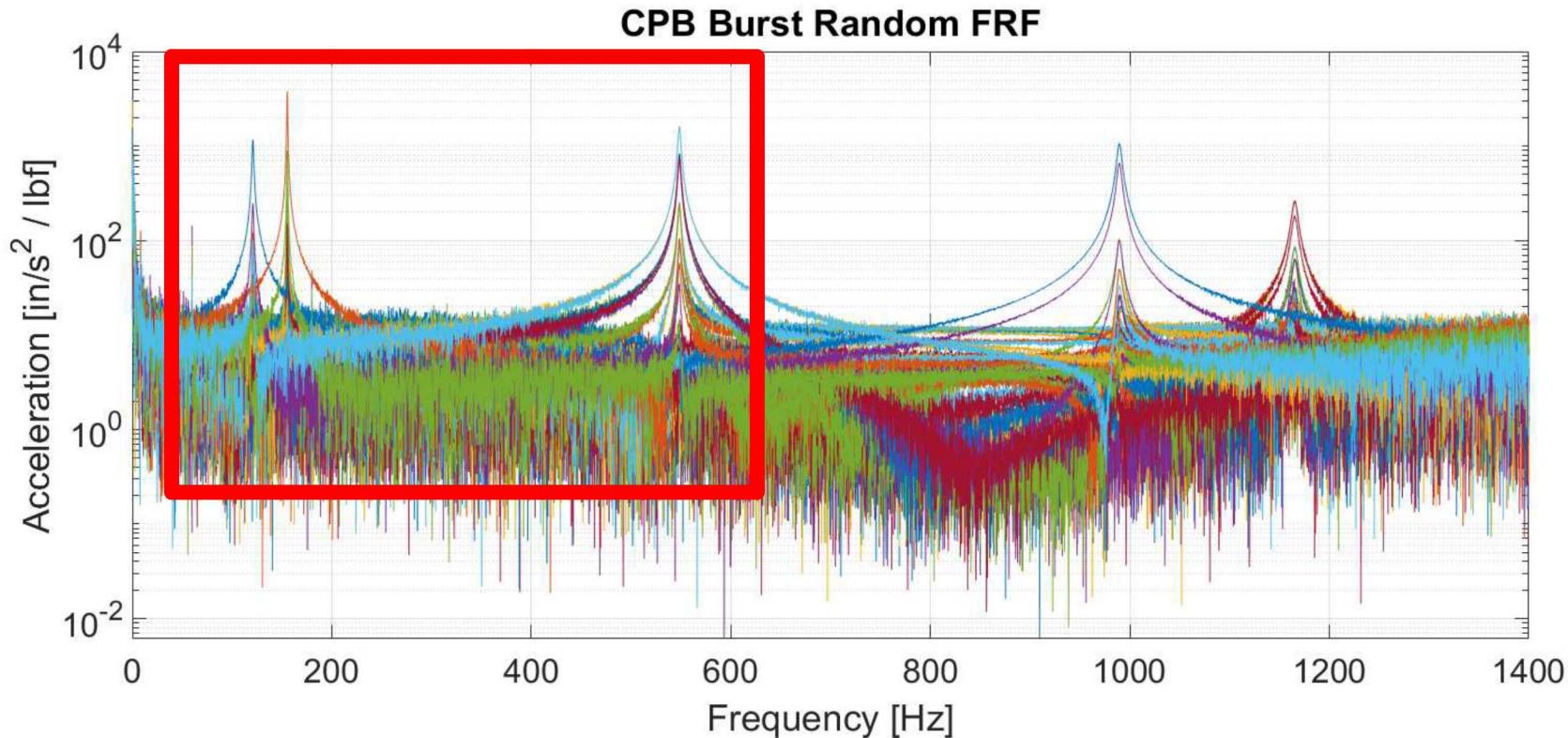


Experimental Process



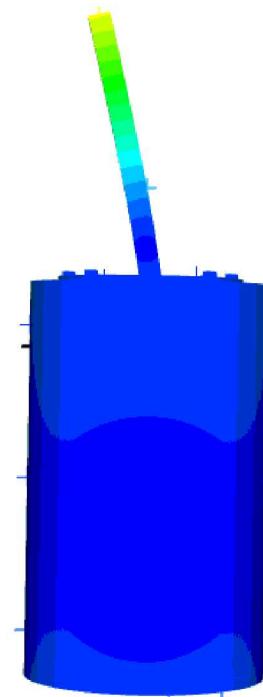
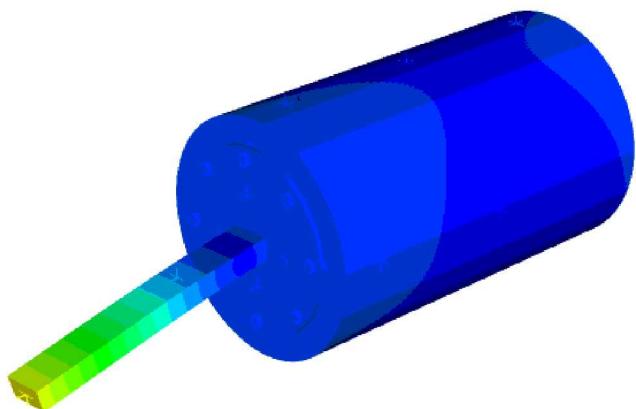
Linear Experimental Data

- Employed low level burst random excitation from the shaker
 - Curve fit linear FRFs for modeshapes to use as a modal filter



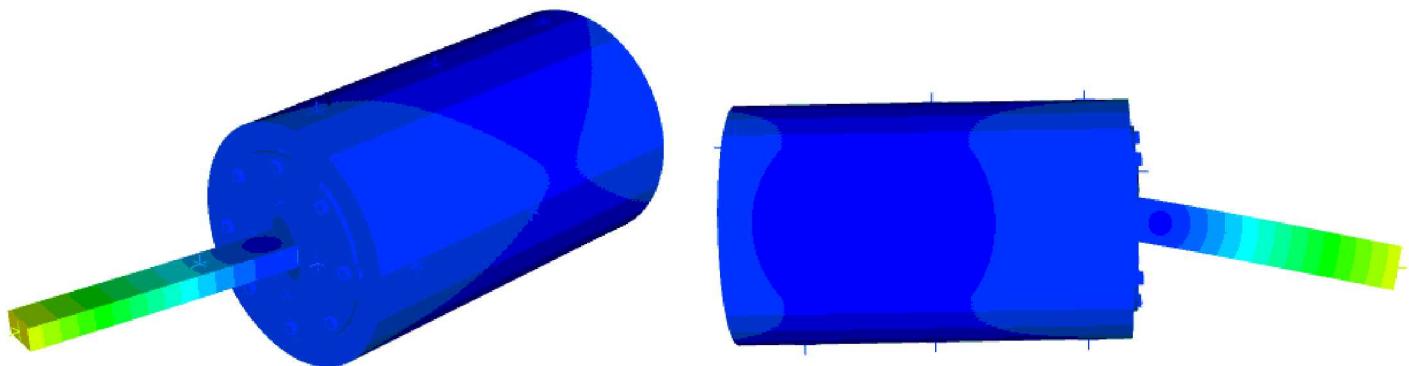
Mode 1

Mode Description	Experimental ω_n (Hz)
1st Beam Bending X	120.8



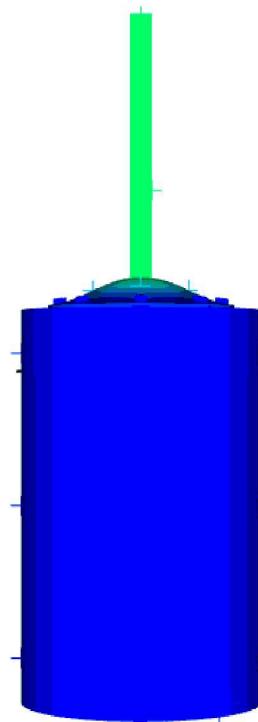
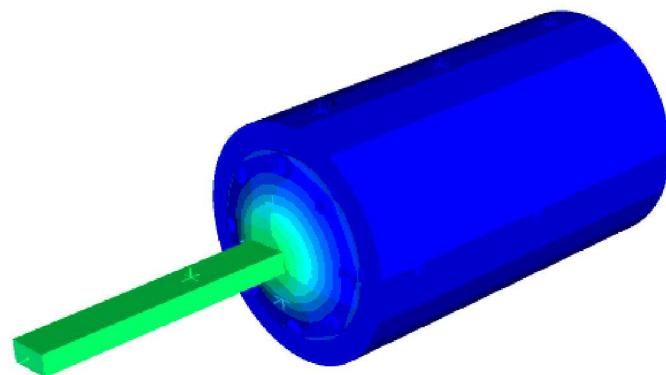
Mode 2

Mode Description	Experimental ω_n (Hz)
1st Beam Bending Y	155.3



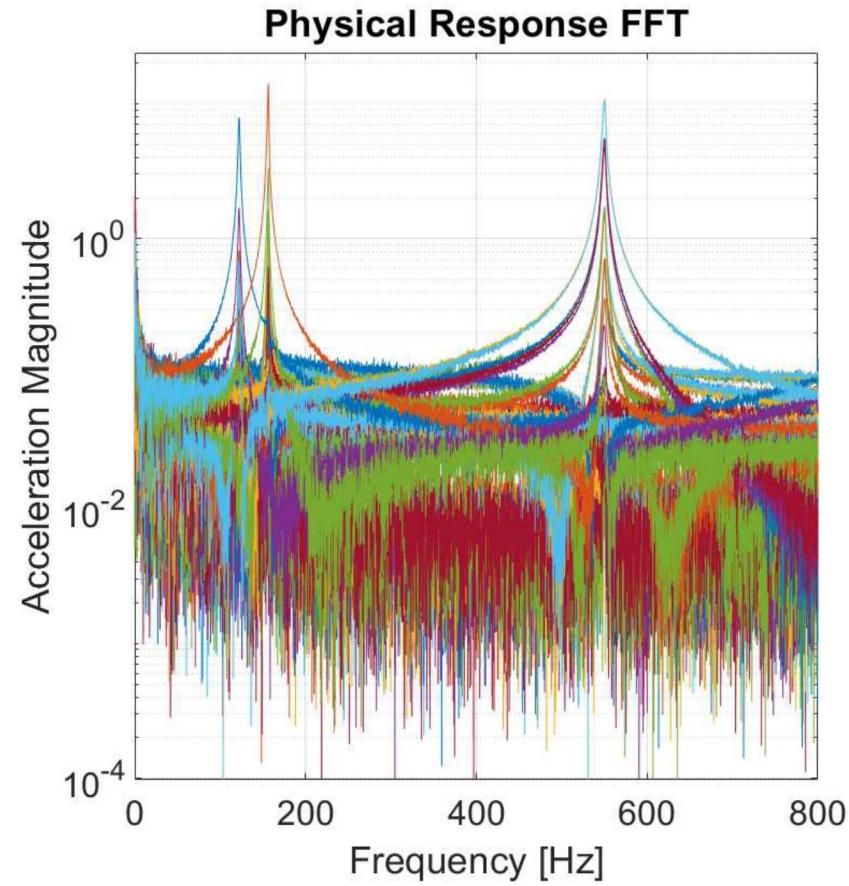
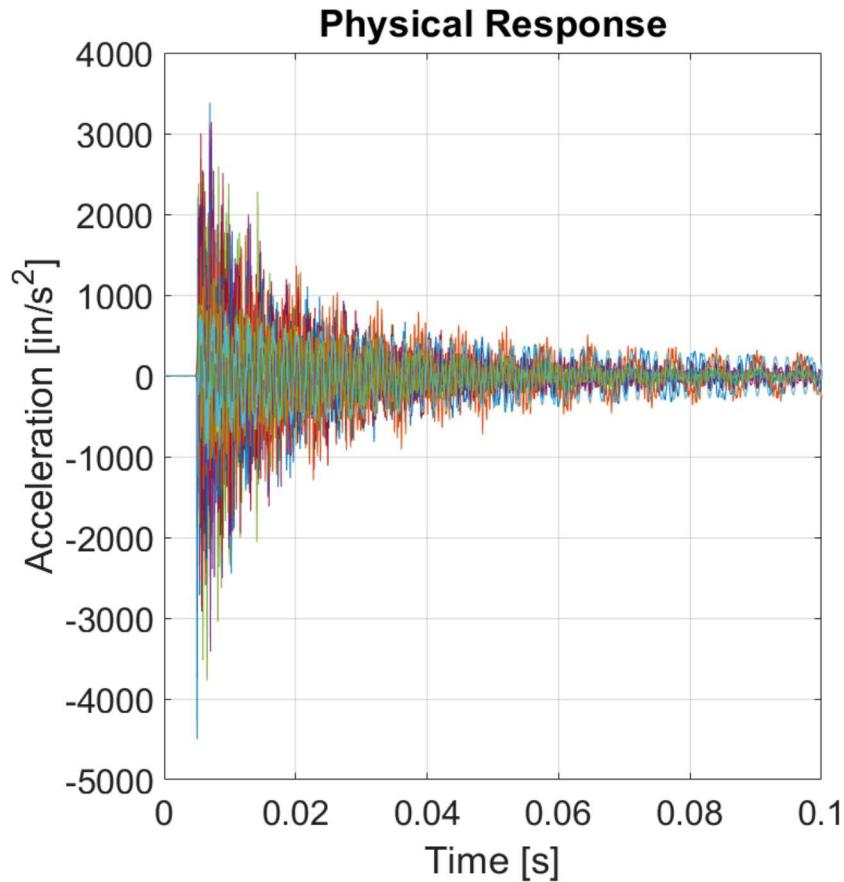
Mode 3

Mode Description	Experimental ω_n (Hz)
Plate Drum	548.43



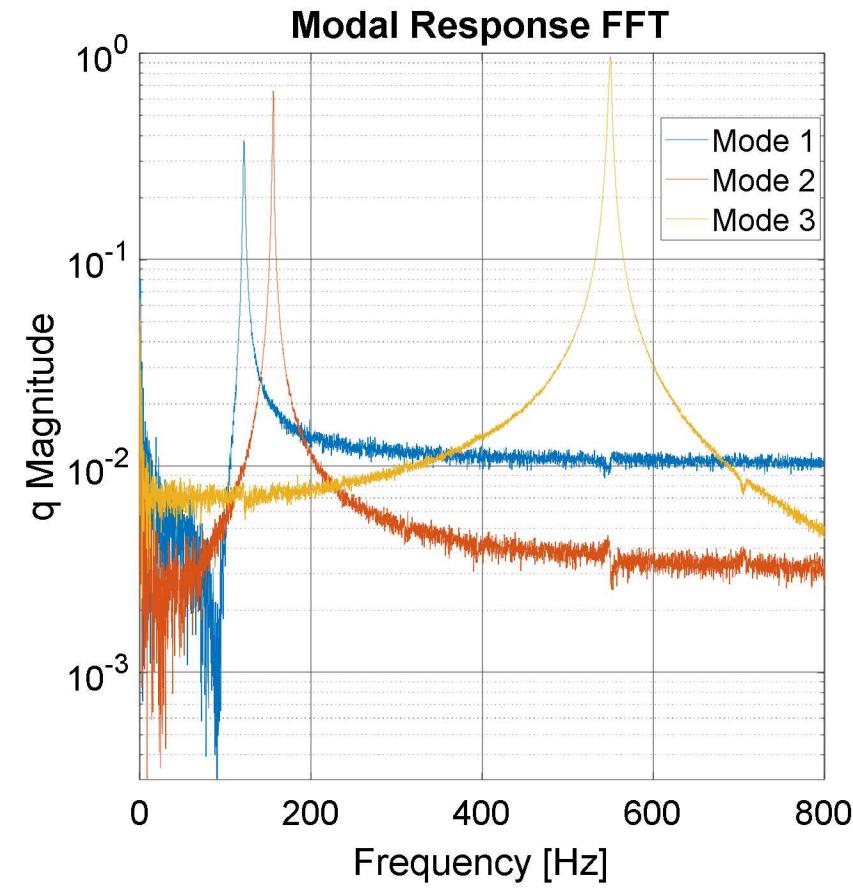
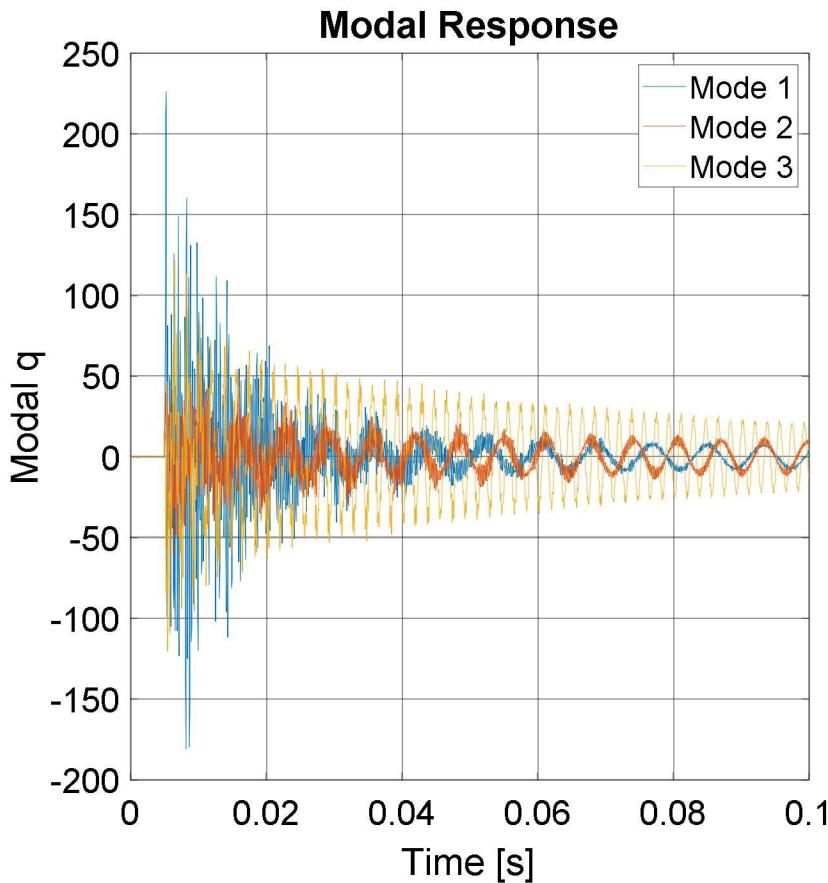
Modal Filtering

- Linear mode shapes allow for filtering of physical response into modal coordinates



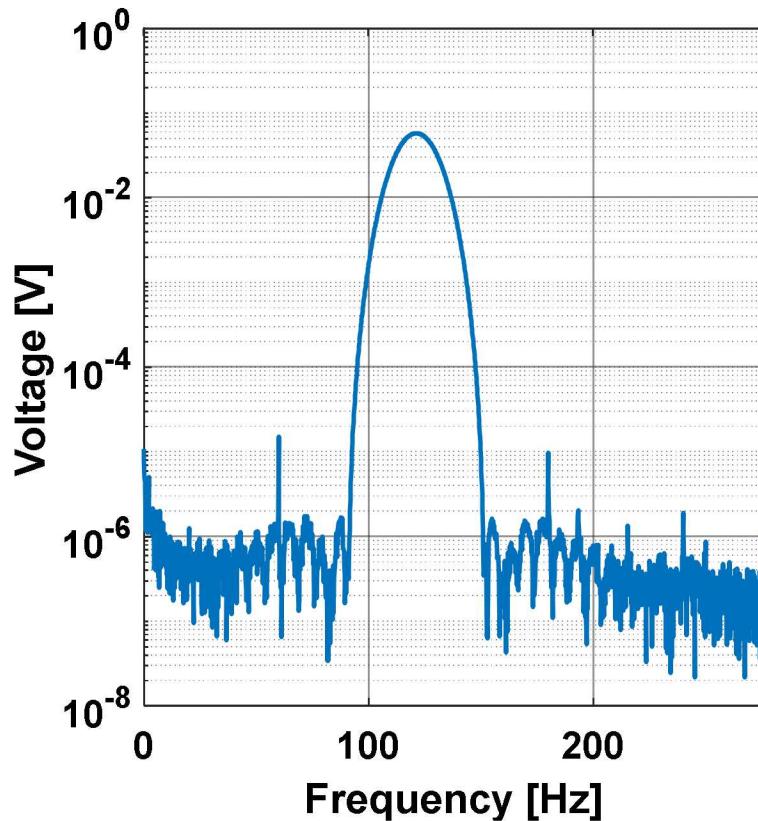
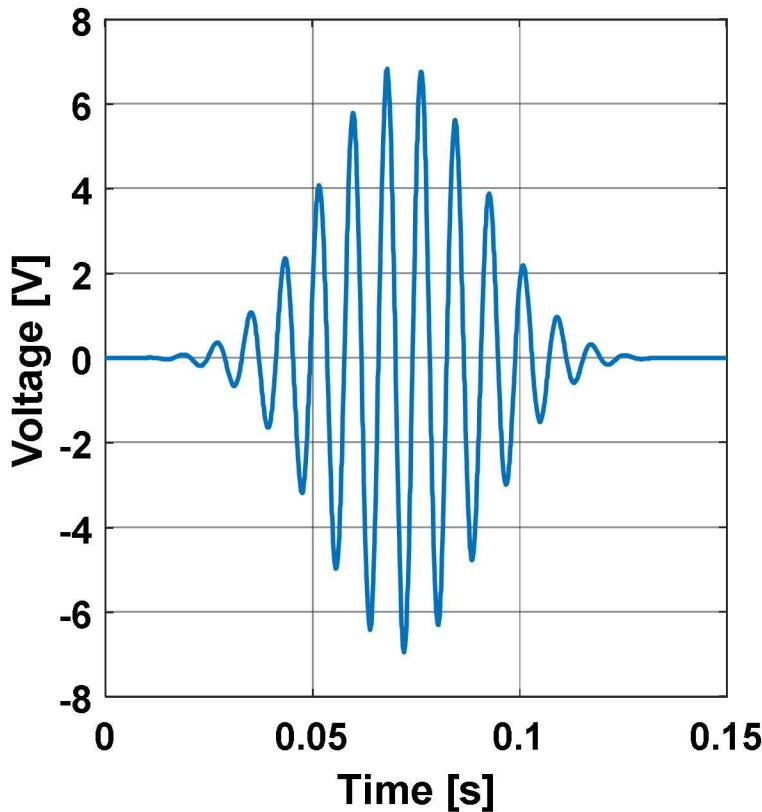
Modal Filtering

- Linear mode shapes allow for filtering of physical response into modal coordinates



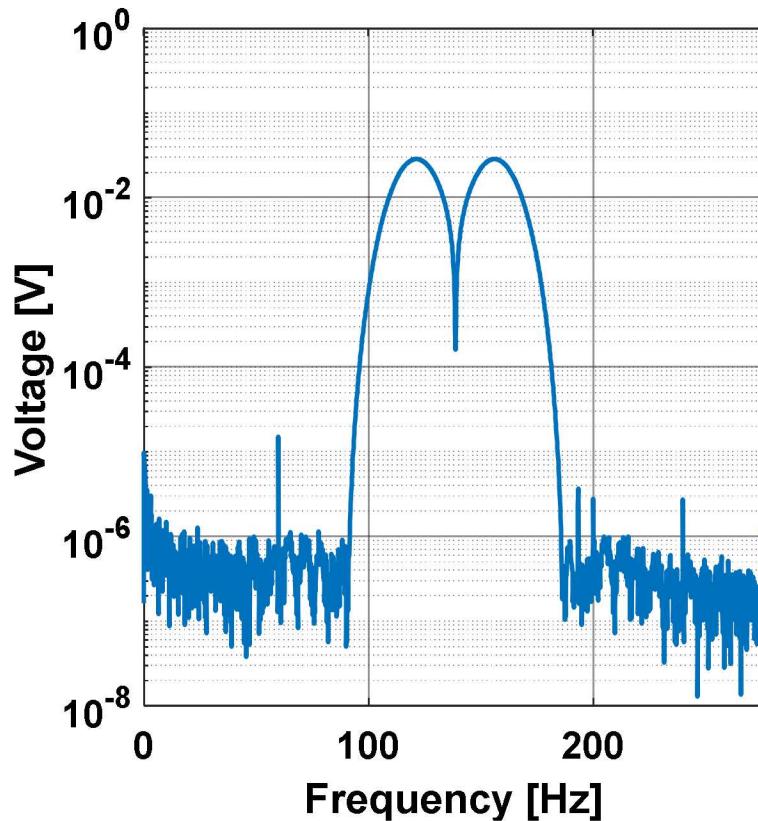
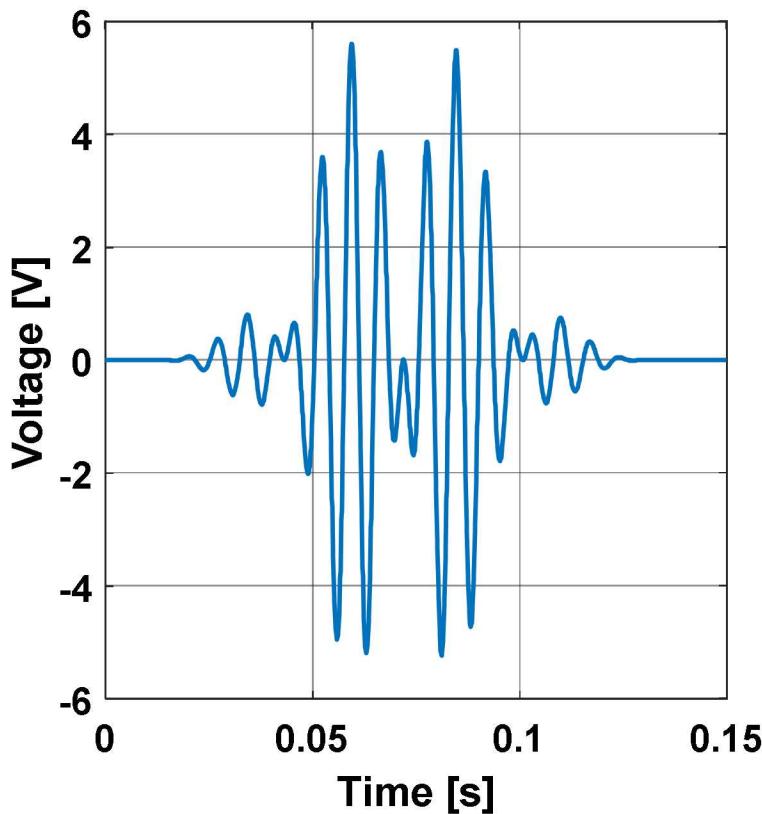
Nonlinear Data

- Shaker delivers definable force input – able to create a voltage signal with specific frequency content



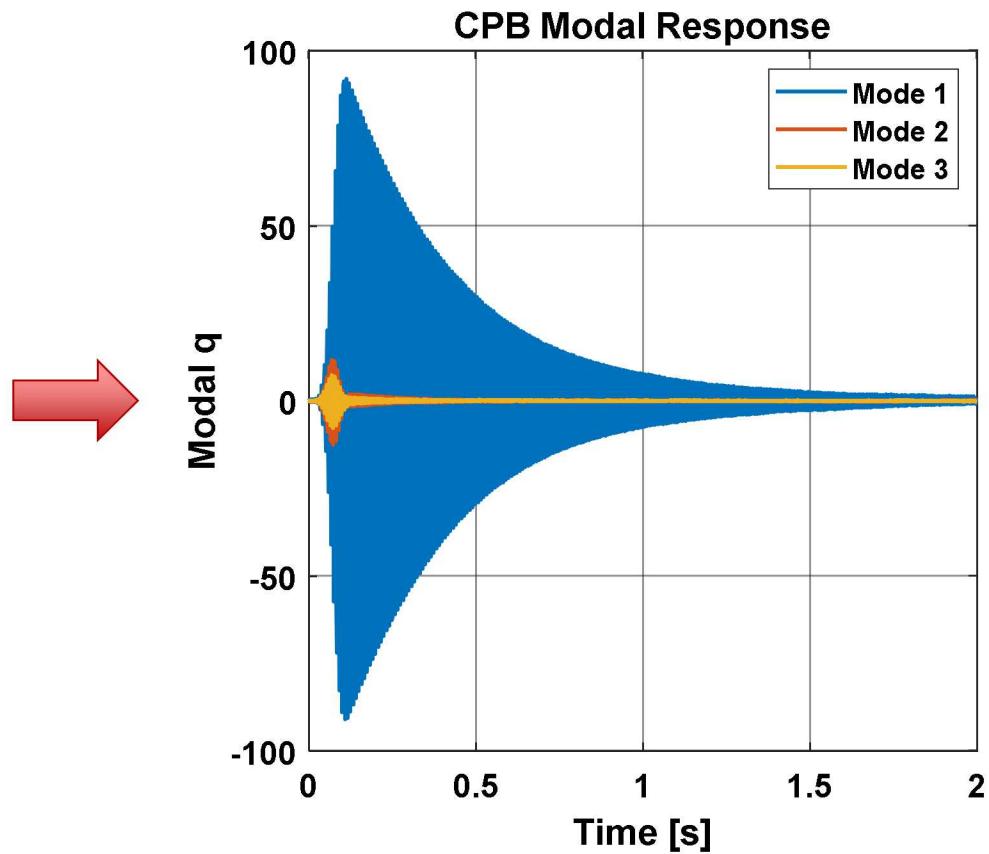
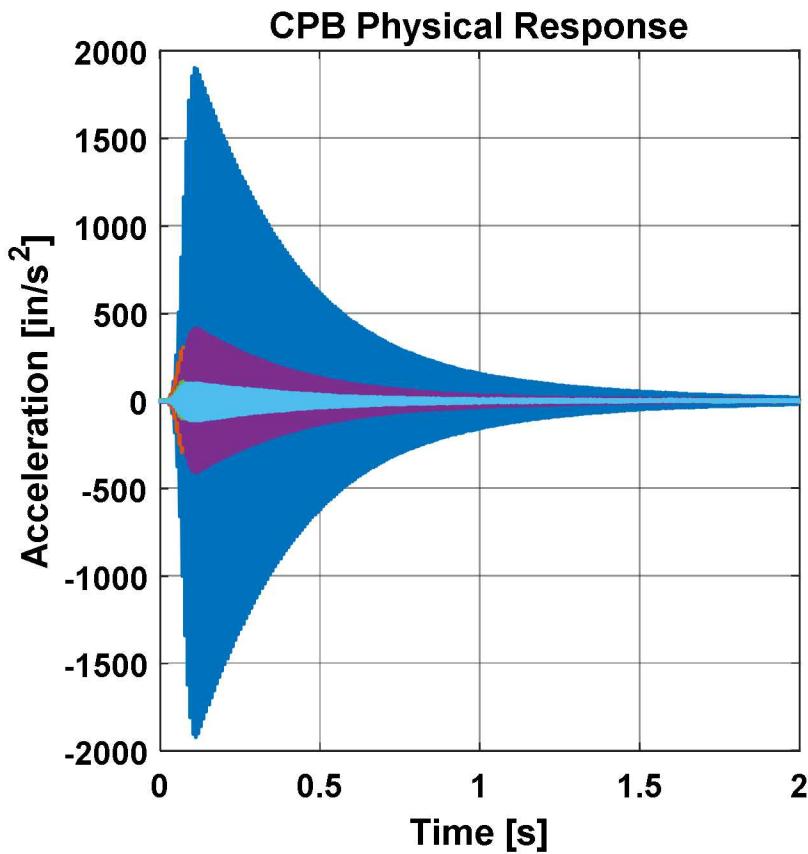
Nonlinear Data

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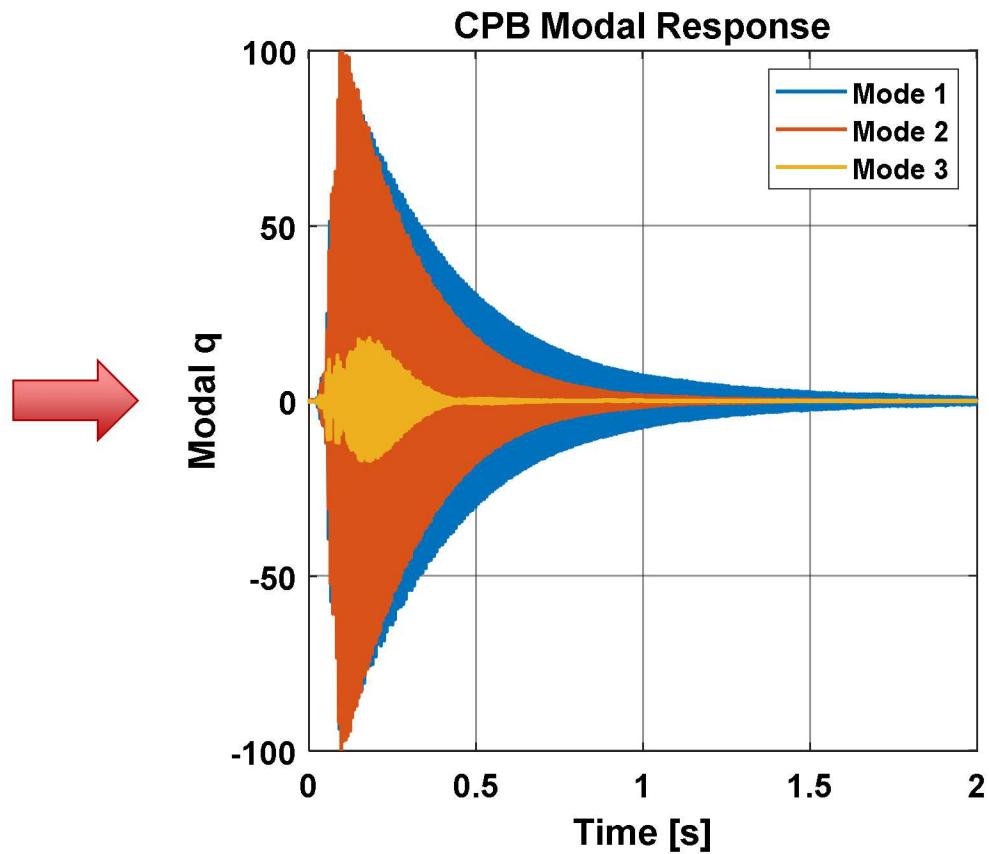
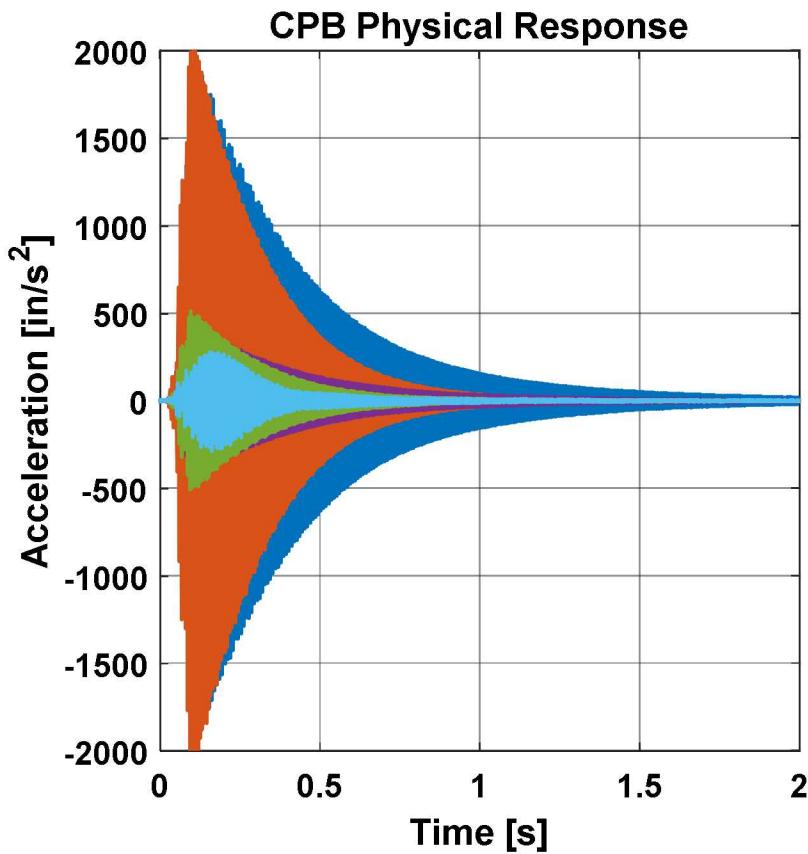
Nonlinear Data

- Use shaker to excite specific modes



Nonlinear Data

- Use shaker to excite specific modes

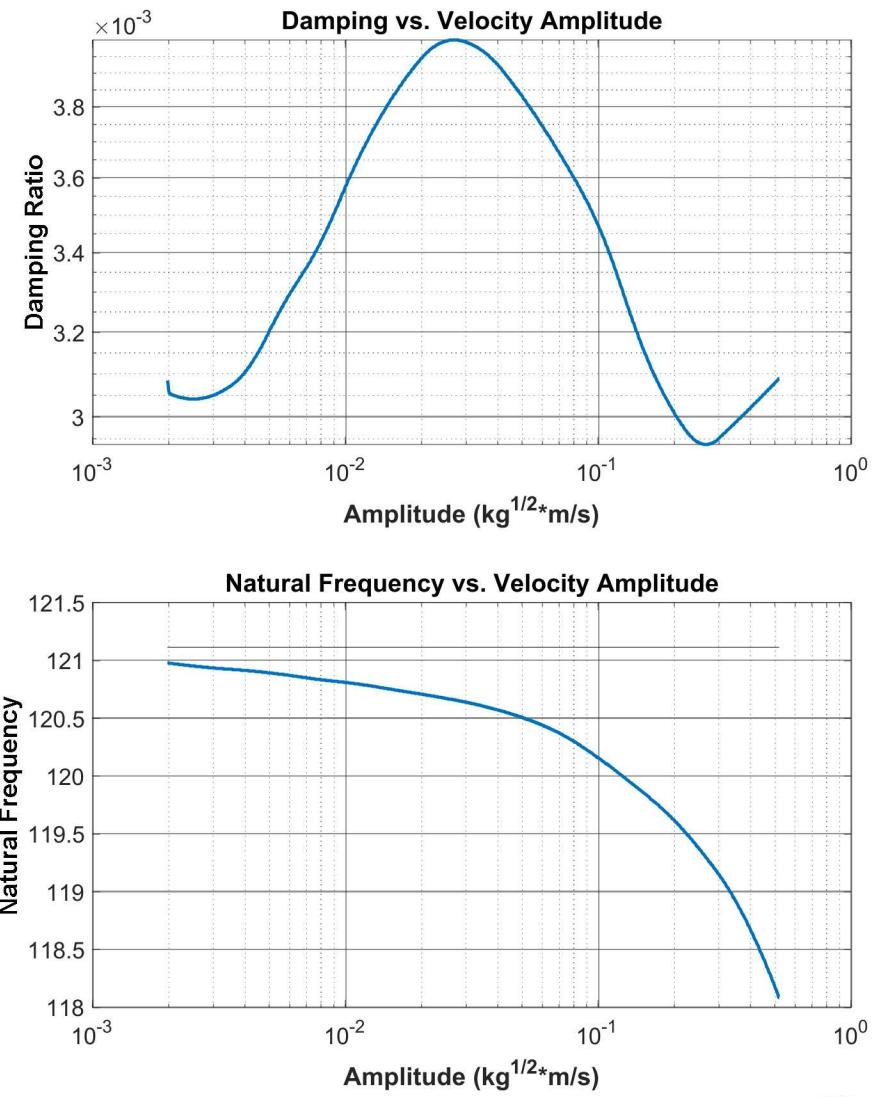
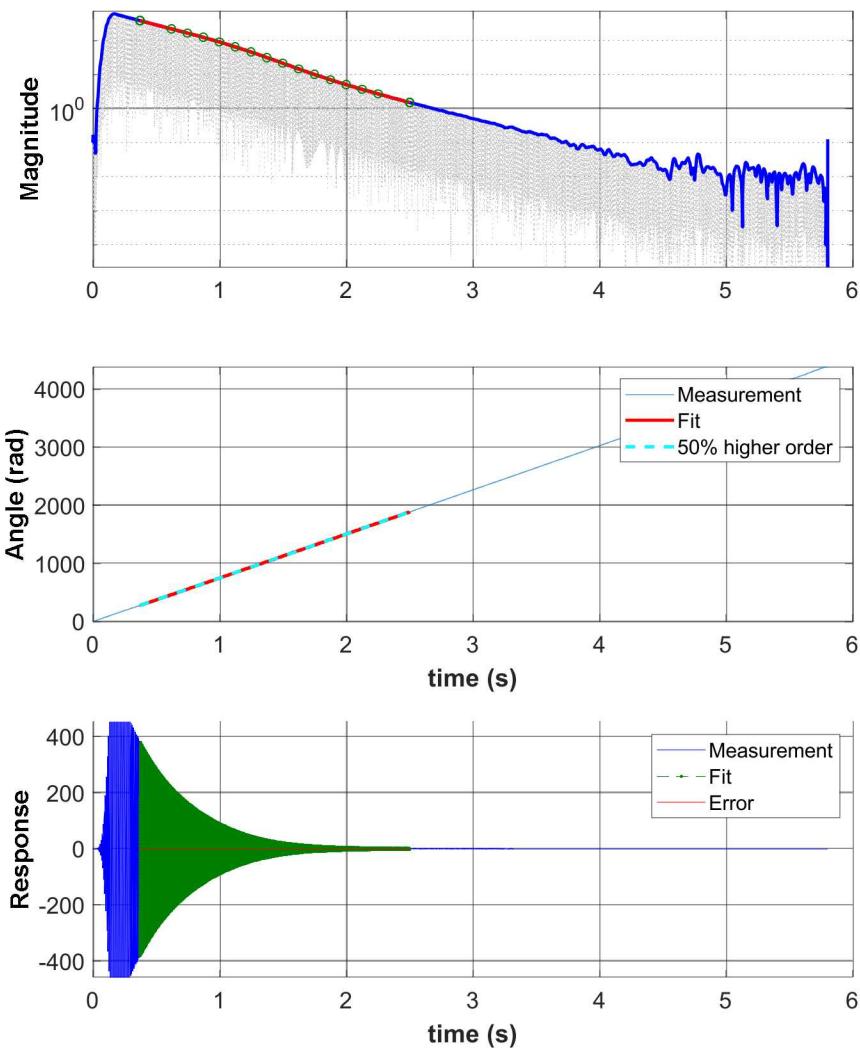


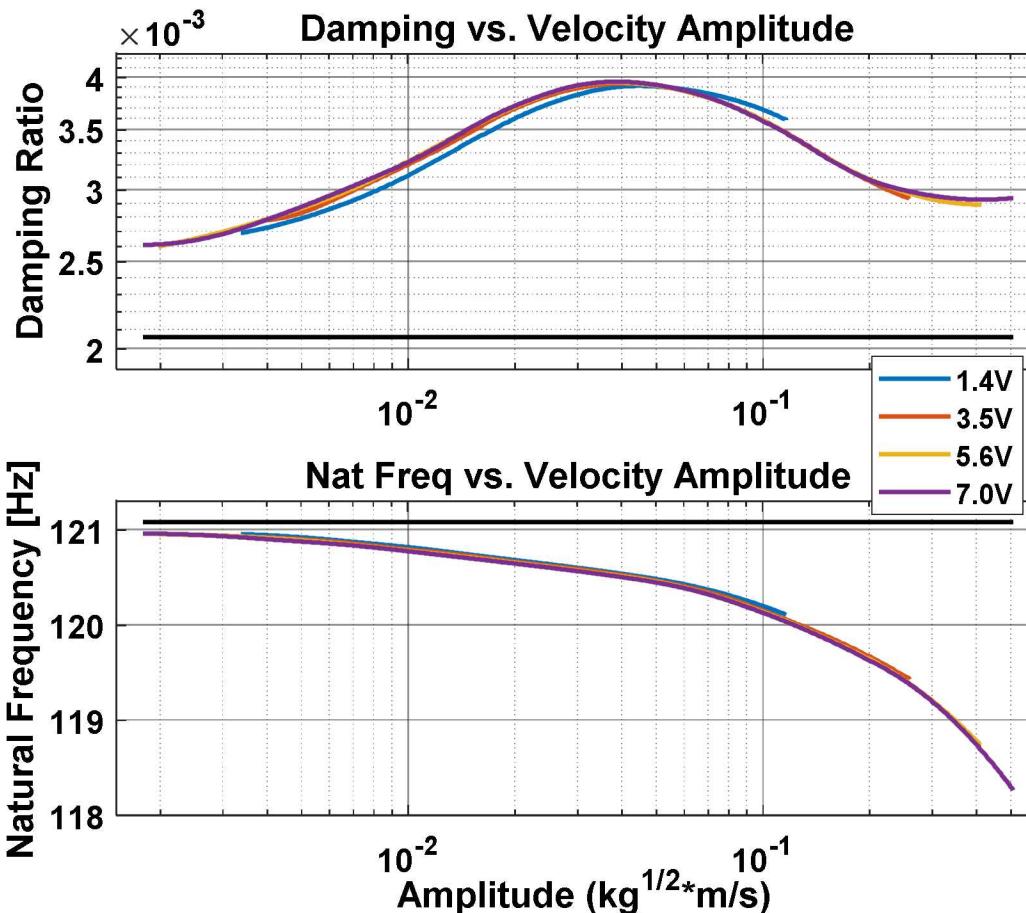
Hilbert Analysis

- Requires that each response be uncoupled such that it can be represented by a SDOF system
 - Signal can be represented by a decaying harmonic
 - $\ddot{\eta} = \operatorname{Re}[\exp(\psi_1(t) + i \psi_2(t))]$
- Compute Hilbert Transformation ($\mathcal{H}(t)$) for an amplitude dependent representation of damping and frequency
 - $\omega_{d,r} = \frac{d\psi_2}{dt}$
 - $\zeta_r \triangleq \frac{d\psi_1}{dt} / \omega_r$

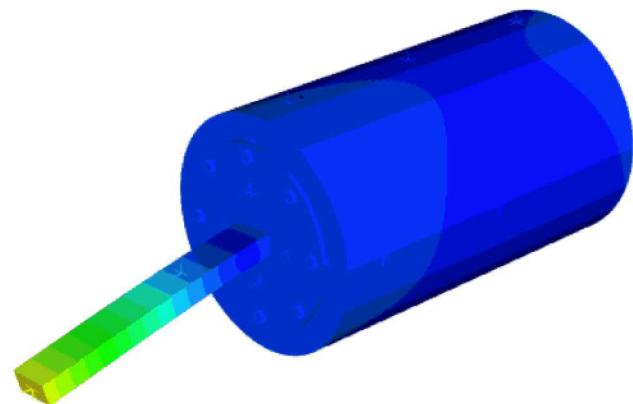


Hilbert Analysis

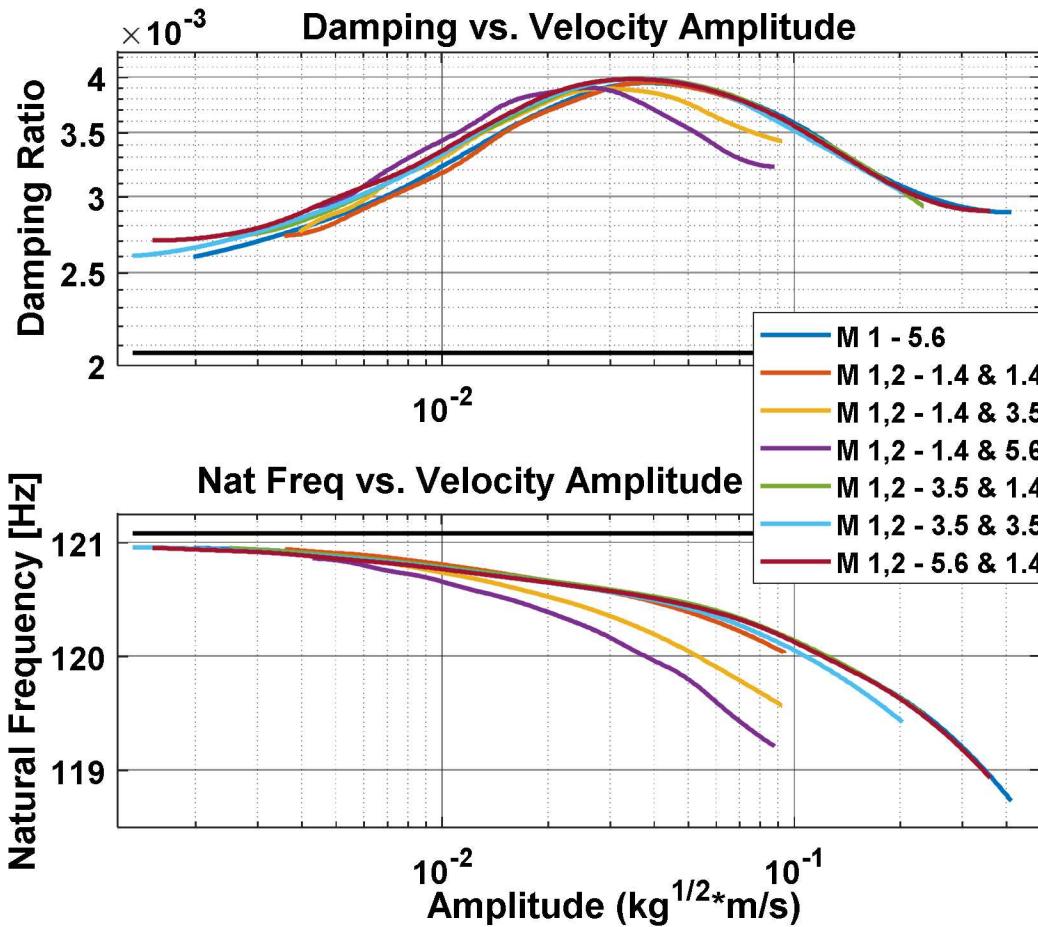




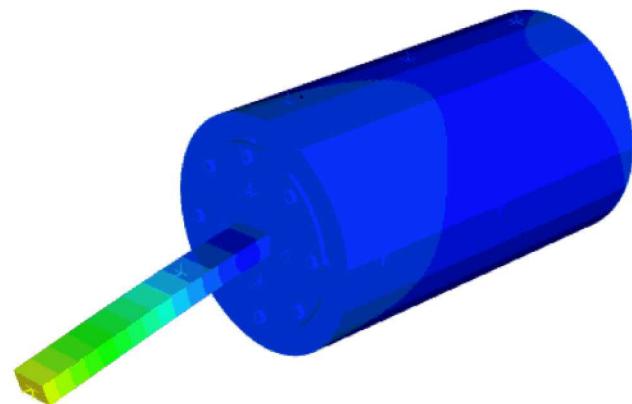
Mode 1



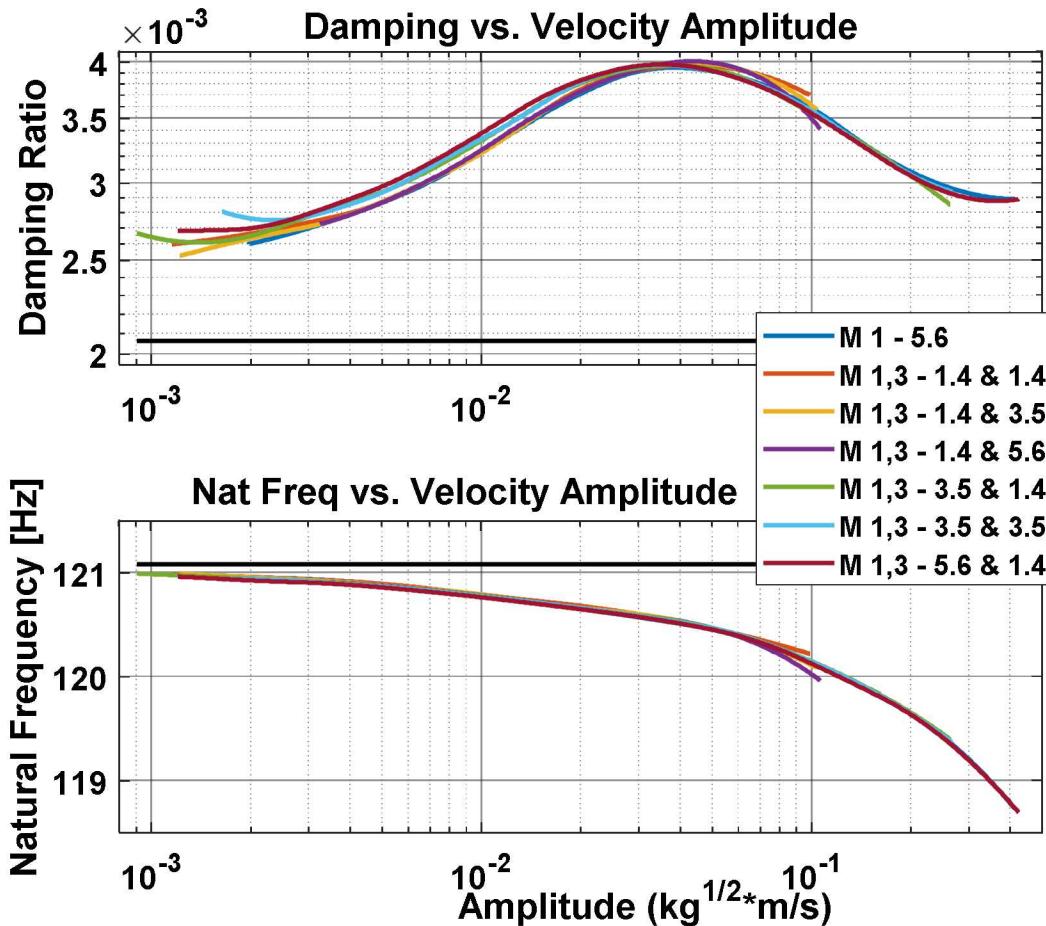
- When excited alone at various levels, frequency and damping overlay with increasing amplitude



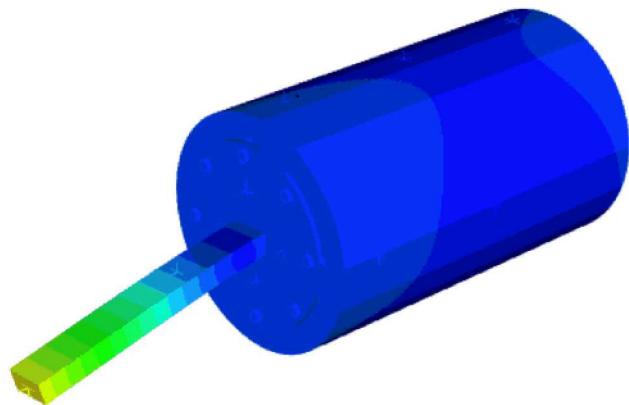
Mode 1 & 2



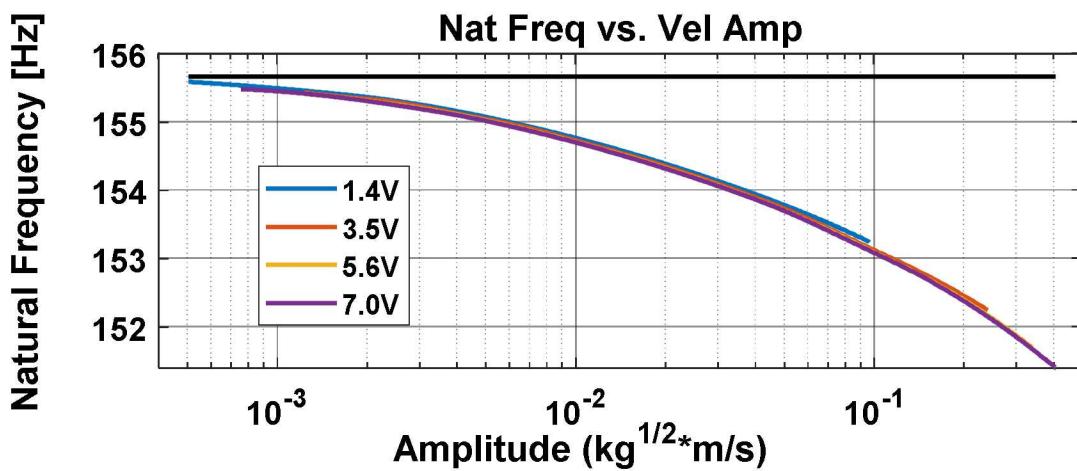
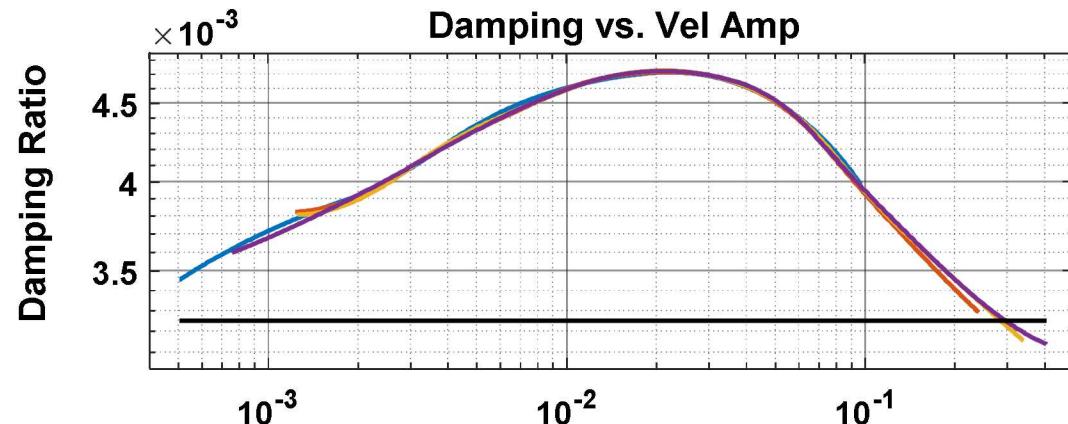
- Coupling visible as a frequency and damping shift when mode 2 is excited to a higher level than mode 1



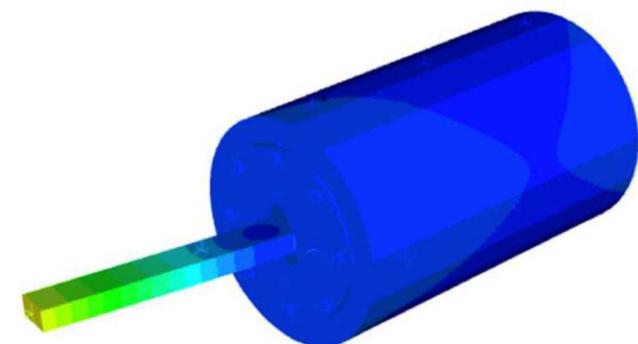
Mode 1 & 3



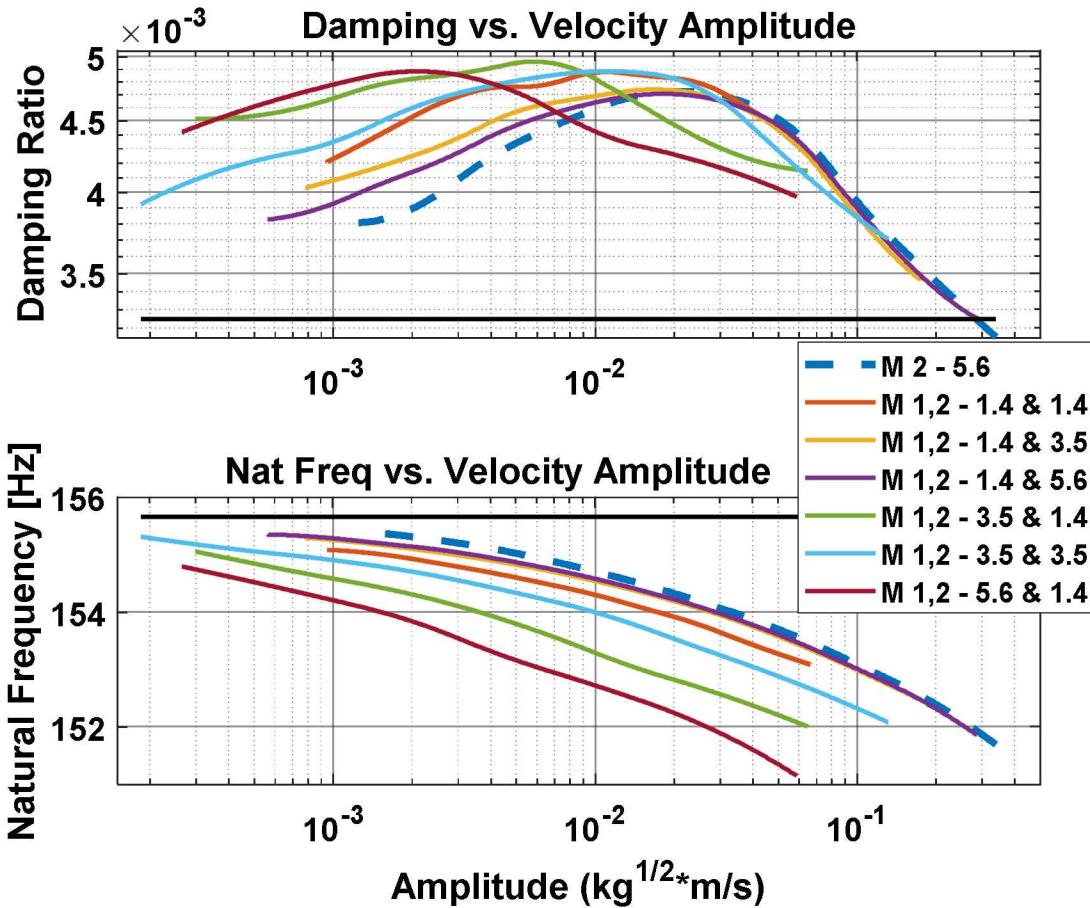
- Mode 1 appears to be completely unaffected by mode 3.



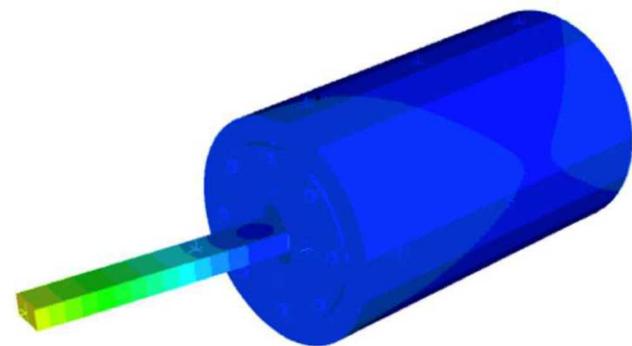
Mode 2



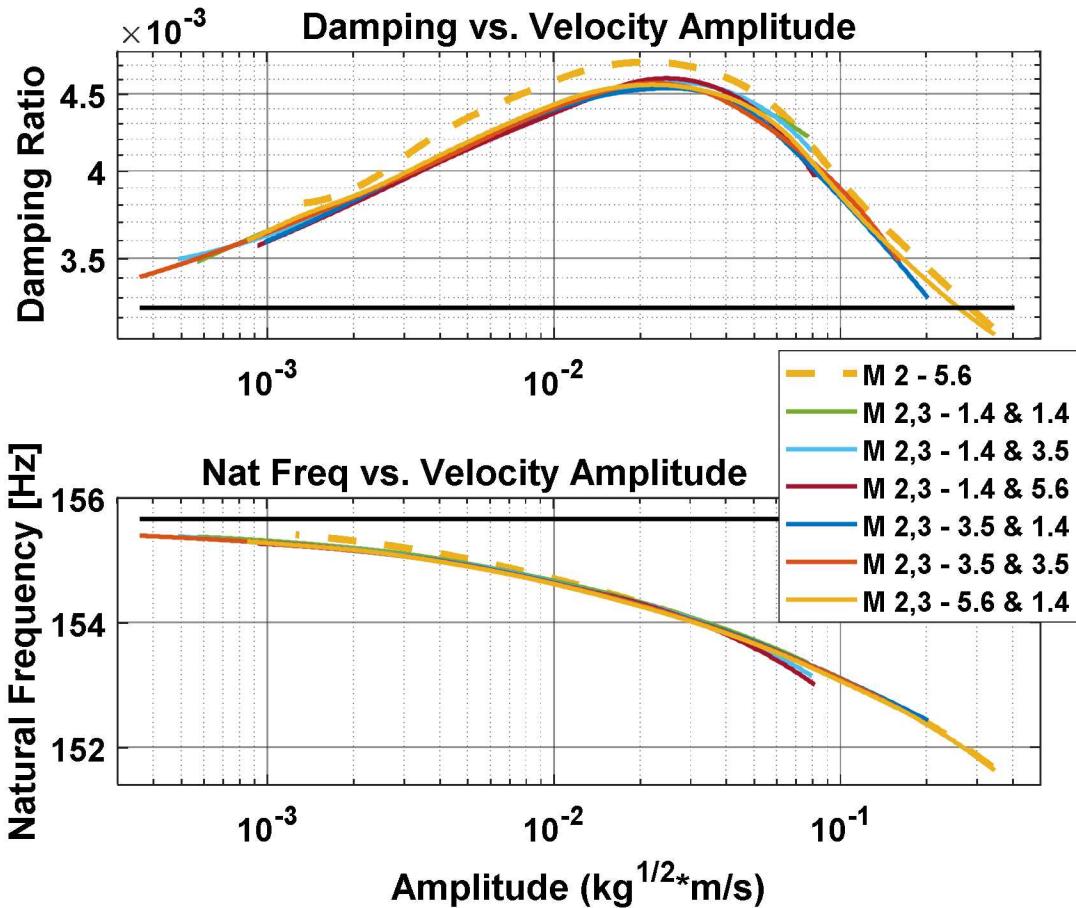
- As with Mode 1, when Mode 2 is excited alone, frequency and damping overlay with increasing amplitude.



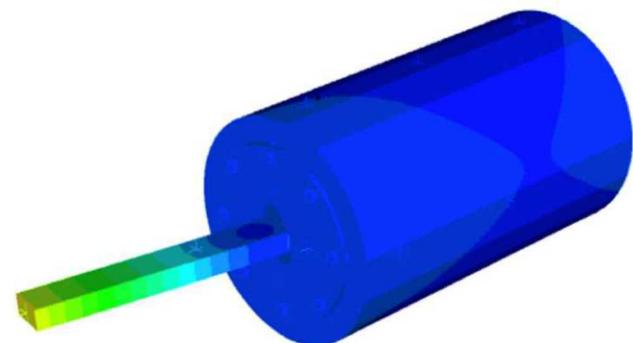
Mode 2 & 1



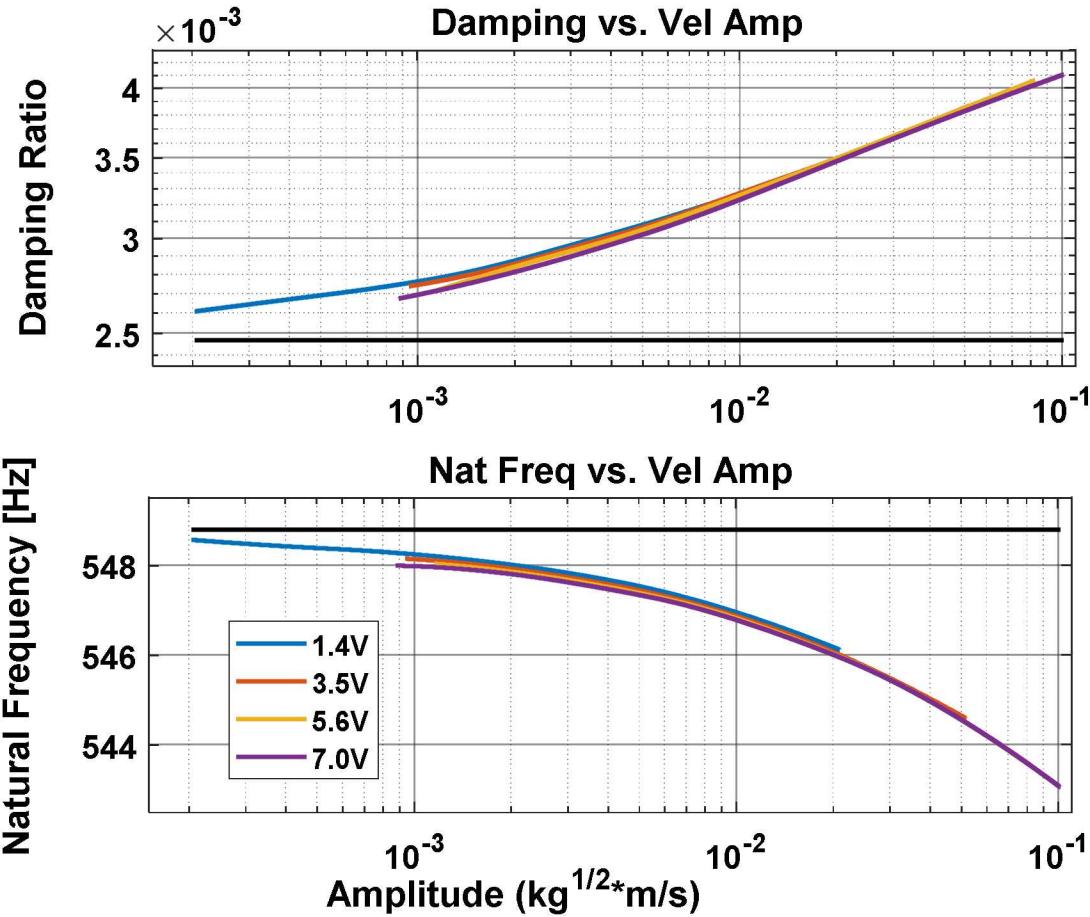
- Observe the same frequency and damping shift, but now to a greater degree in all cases where mode 1 is also excited.



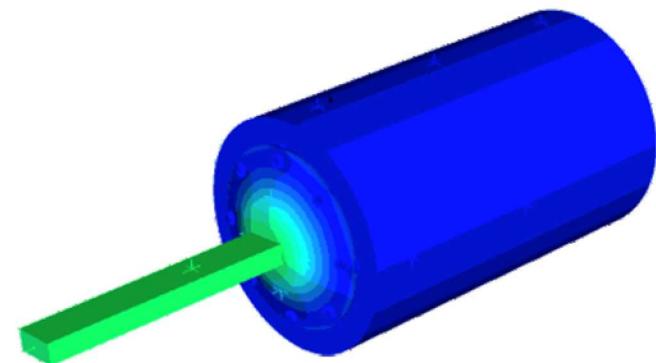
Mode 2 & 3



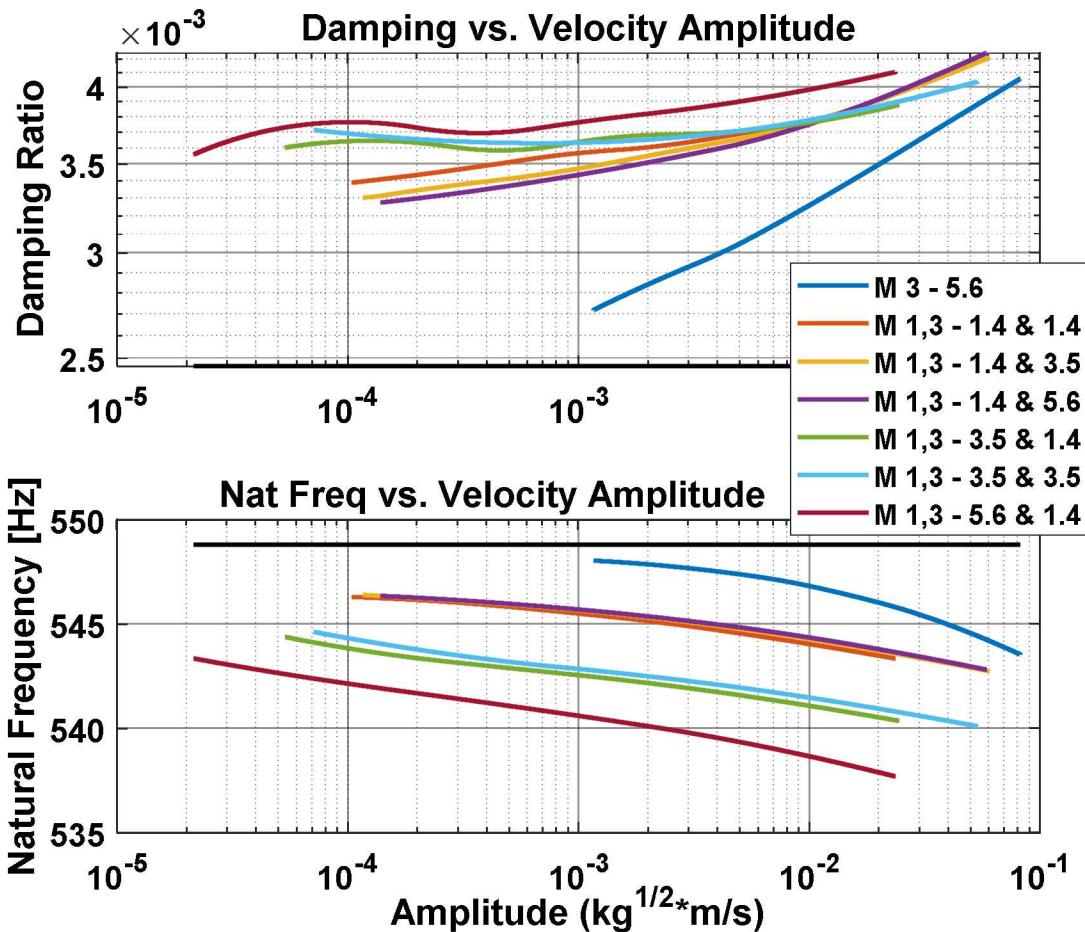
- Mode 2 also appears to be totally indifferent as to the presence of mode 3.



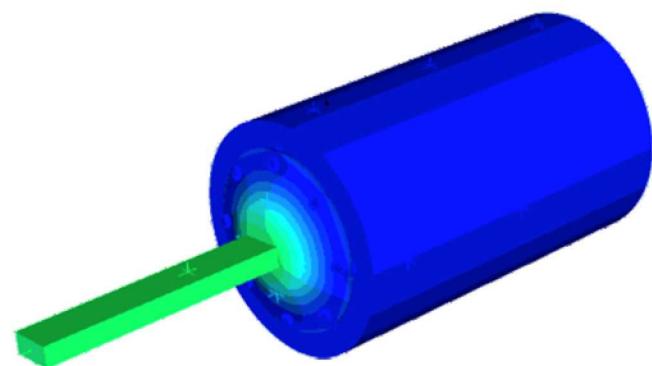
Mode 3



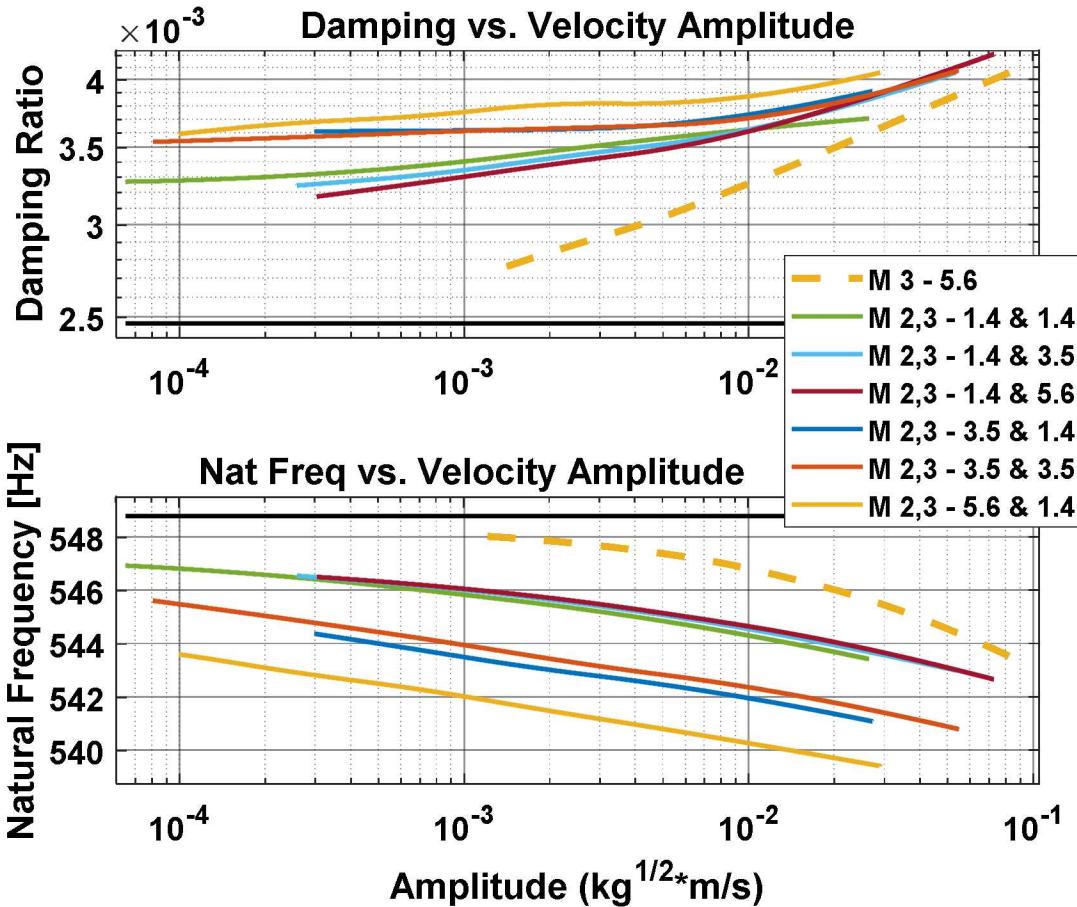
- When excited individually, all modes exhibit consistent frequency and damping shifts with increasing amplitude



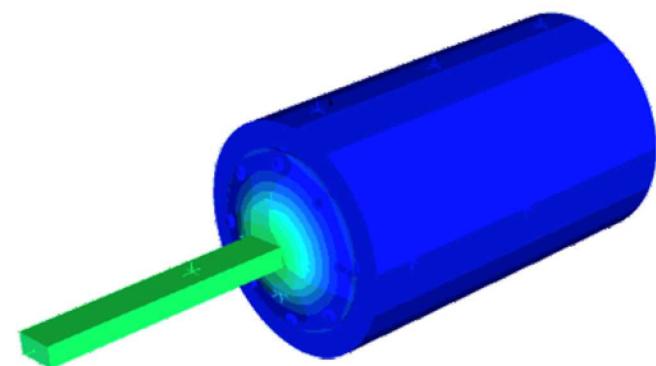
Mode 3 & 1



- Mode 3 shows significant decreases in frequency and increases in damping when mode 1 is also excited at any level.



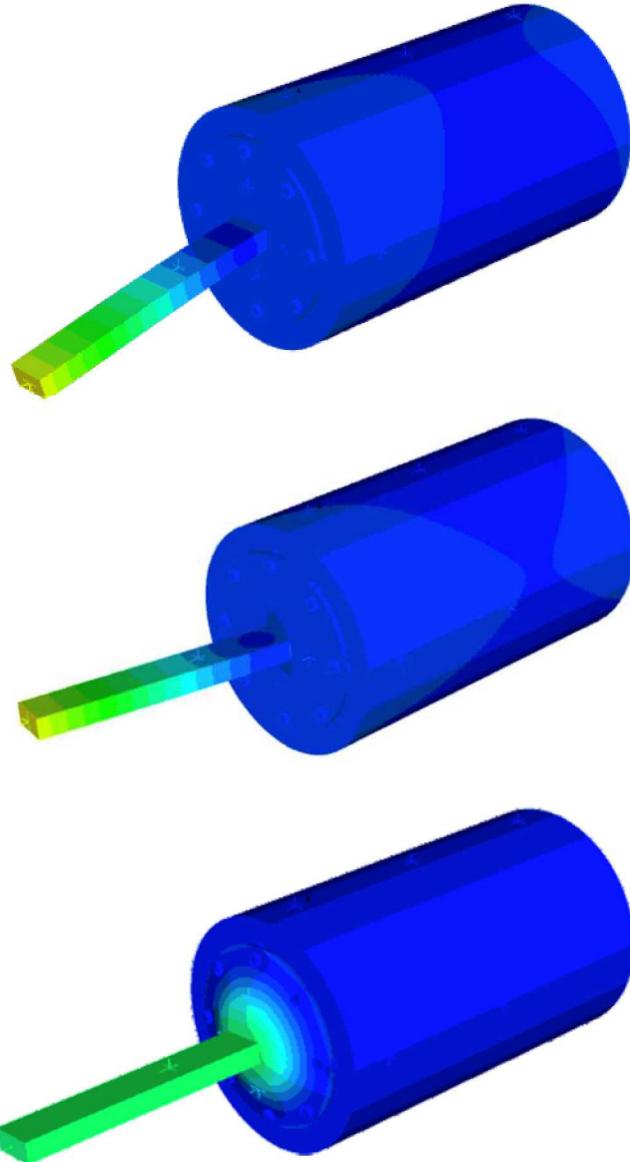
Mode 3 & 2



- When mode 3 is excited with mode 2, similar drastic shift in frequency and damping are observed.

Closing Remarks

- When excited alone, all three modes have very consistent frequency and damping responses.
- Mode 1 and 2 show signs of modal coupling when simultaneously excited.
 - Mode 2 appears to be more significantly effected.
- Neither mode 1 or 2 display any indication of modal coupling with mode 3.
- However, mode 3 exhibits very strong coupling with modes 1 and 2.



Acknowledgments

- This research was conducted at the 2018 Nonlinear Mechanics and Dynamics Research Institute hosted by Sandia National Laboratories and the University of New Mexico.
- Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA-0003525.

