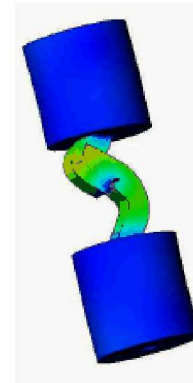


**N=O=MAD**



# Influences of Modal Coupling on Nonlinear Modal Models

# Research Team

**Aabhas Singh**

University of  
Wisconsin – Madison



**Phil Thoenen**

University of Southern California

**Ben Moldenhauer**

University of  
Wisconsin - Madison



# Mentor Team

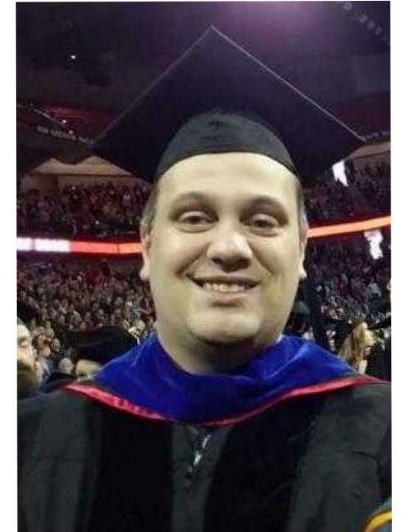
**Matt Allen**

University of  
Wisconsin – Madison



**Dan Roettgen**

Sandia National  
Laboratories



**Rob Kuether**

Sandia National  
Laboratories



**Ben Pacini**

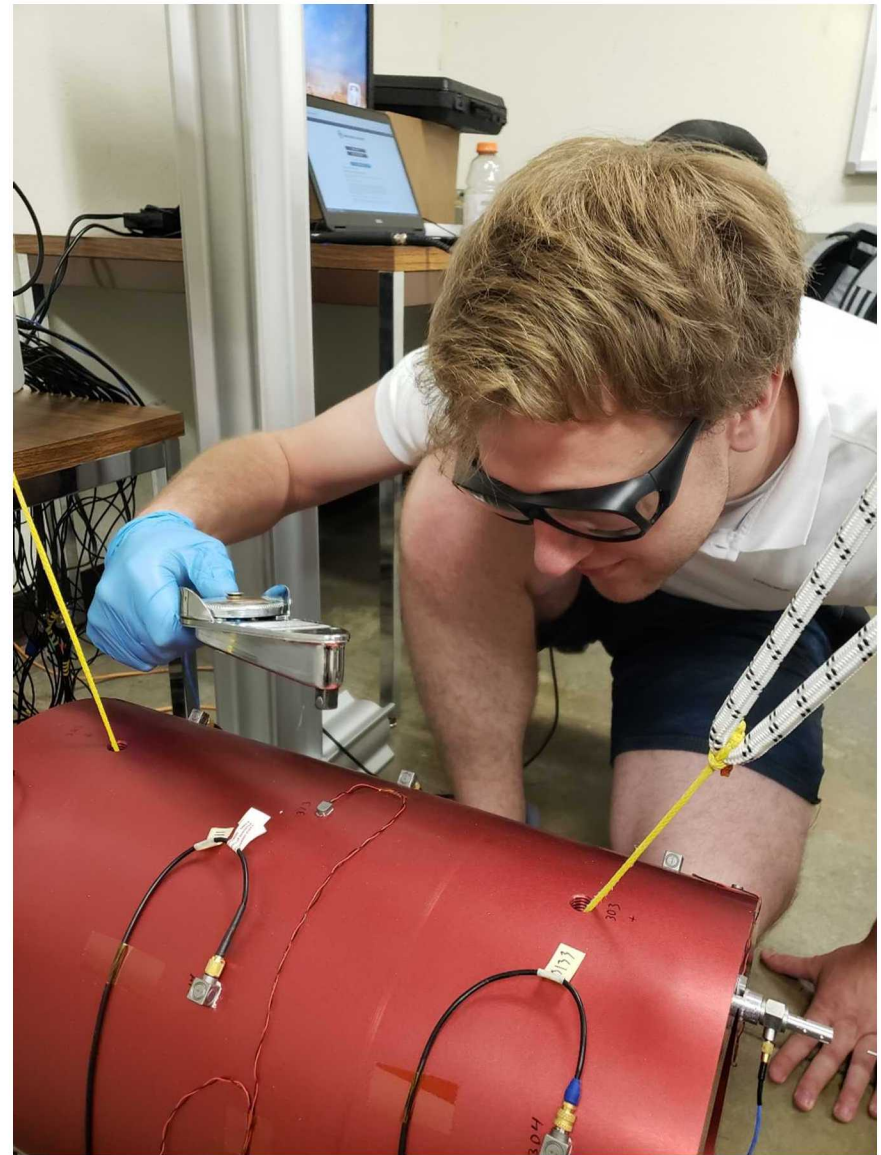
Sandia National  
Laboratories





# Agenda

1. Motivation
2. Test Structure
3. Experimental Process
  - a. Linear Testing
  - b. Nonlinear Testing
4. Nonlinear Coupling Data
5. Closing Remarks



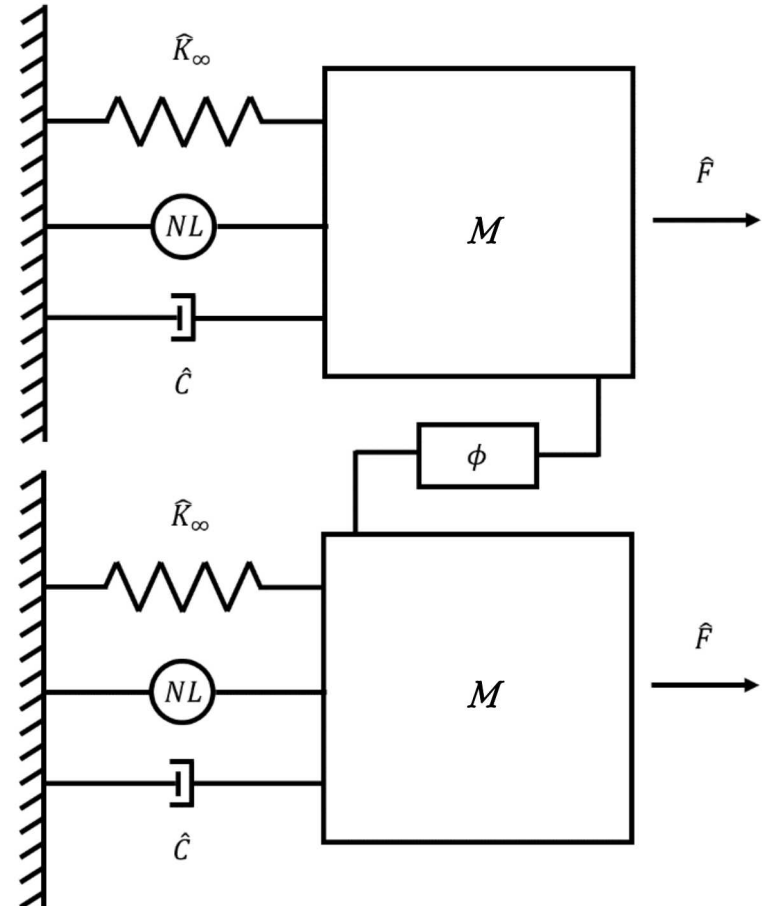
# Linear vs. Nonlinear Systems

- Linear analysis assumes:
  - Small deformations
  - Response is amplitude independent
  - Modal responses can be superimposed
  - $\ddot{q}_r + 2\zeta_r\omega_r\dot{q}_r + \omega_r^2q_r = \Phi^T F_{ext}$
- Pseudo – Nonlinear analysis assumes:
  - Shapes of the linear modes are preserved
  - Linear modes can decouple nonlinear data
  - Coupling between modes is negligible and no energy is transferred between modes
  - $\ddot{q}_r + 2\zeta_r\omega_r\dot{q}_r + \omega_r^2q_r + F_{nl}(q_r, \dot{q}_r) = \Phi^T F_{ext}$

What happens if there is coupling between the modes?

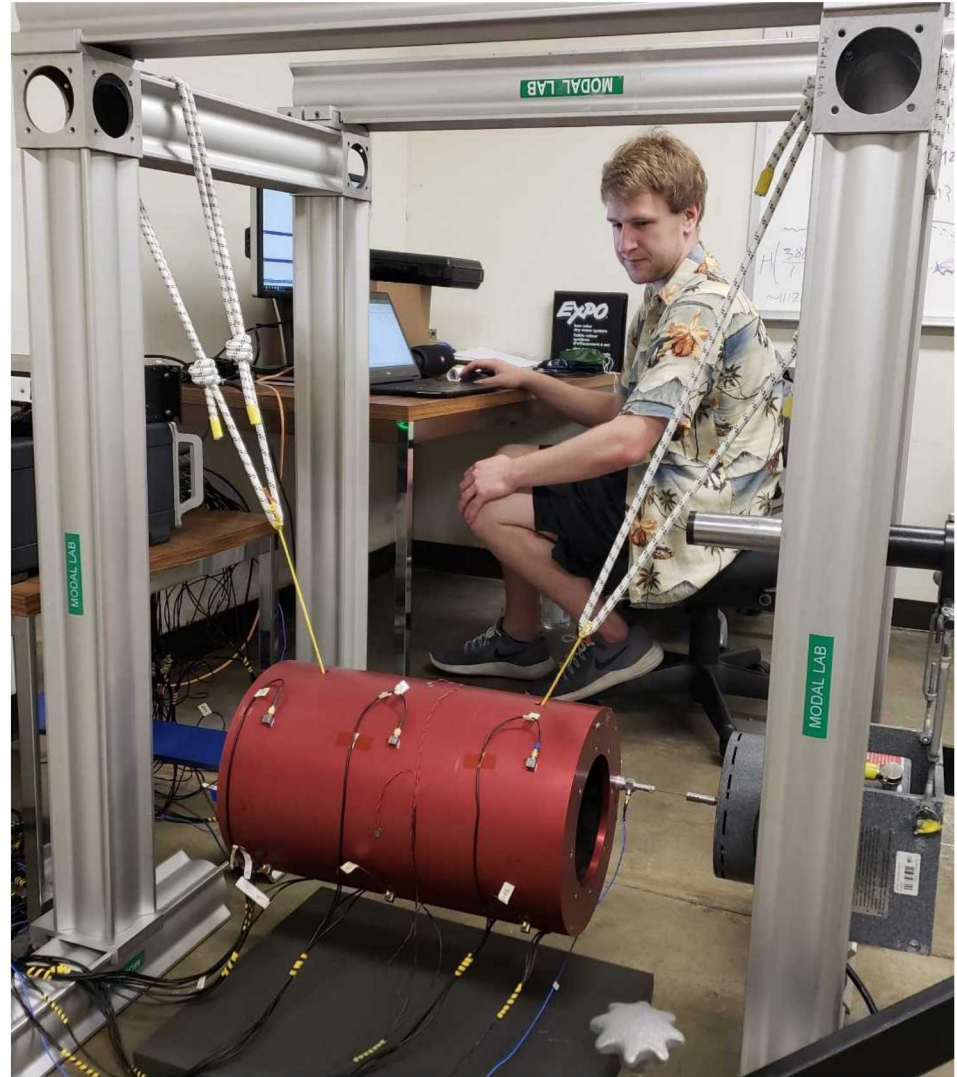
# Modal Coupling

- Excitation of one mode causes a transfer of energy that perturbs another mode
- Usually occurs due to interactions at joints shared by different mode shapes



# Project Objectives

- Excite combinations of modes on a nonlinear structure
- Experimentally identify the presence modal coupling
- Collect data for use in validating computer models of coupling

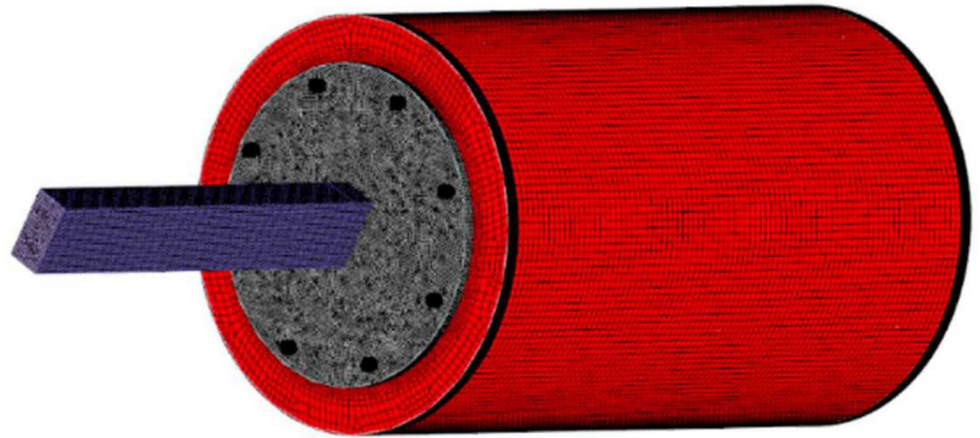




# Test Structure

## Cylinder – Plate – Beam (CPB)

- Plate bolted to cylinder
- Beam bolted and glued to plate

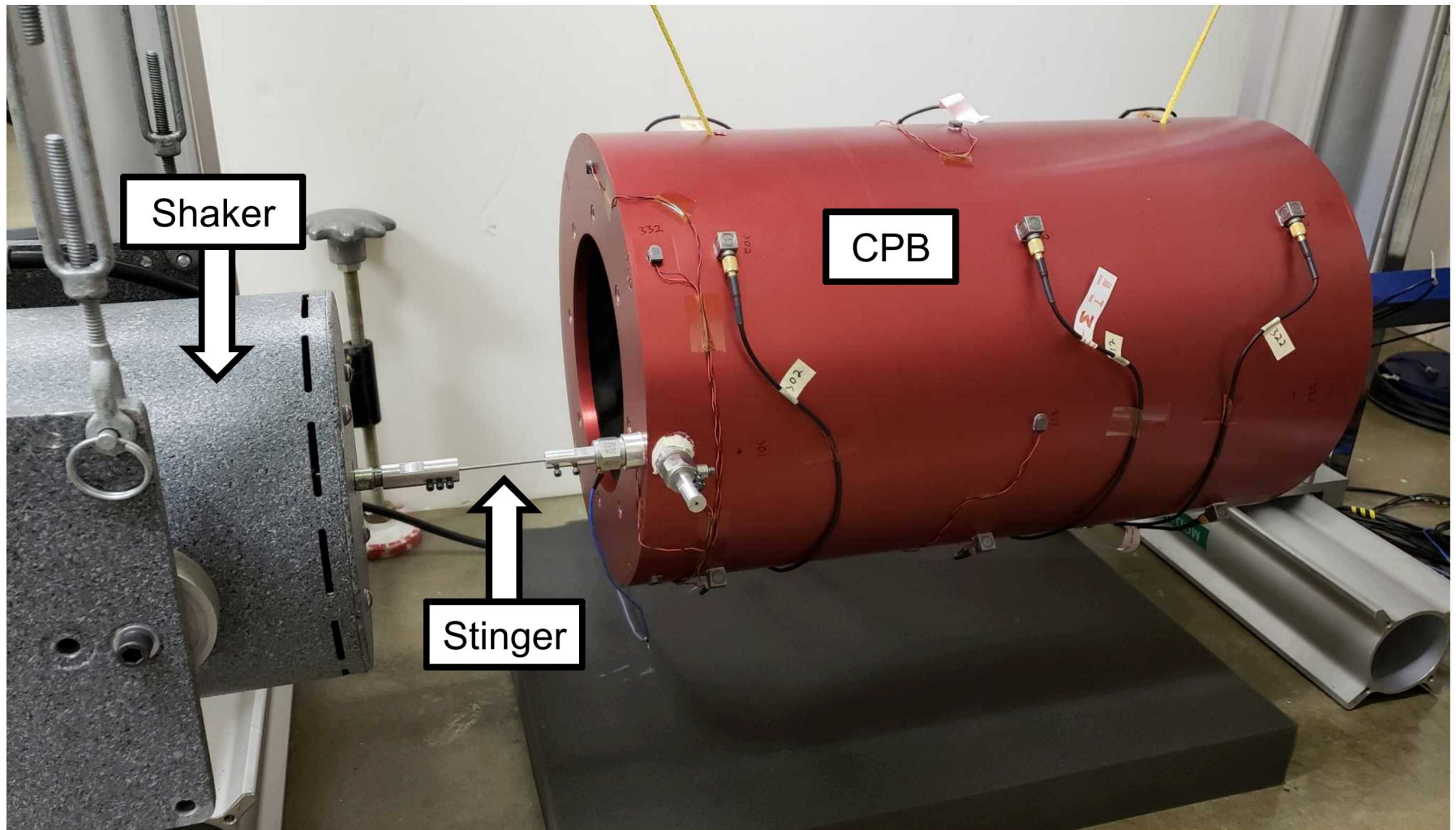


18 triaxial + 8 uniaxial accelerometers

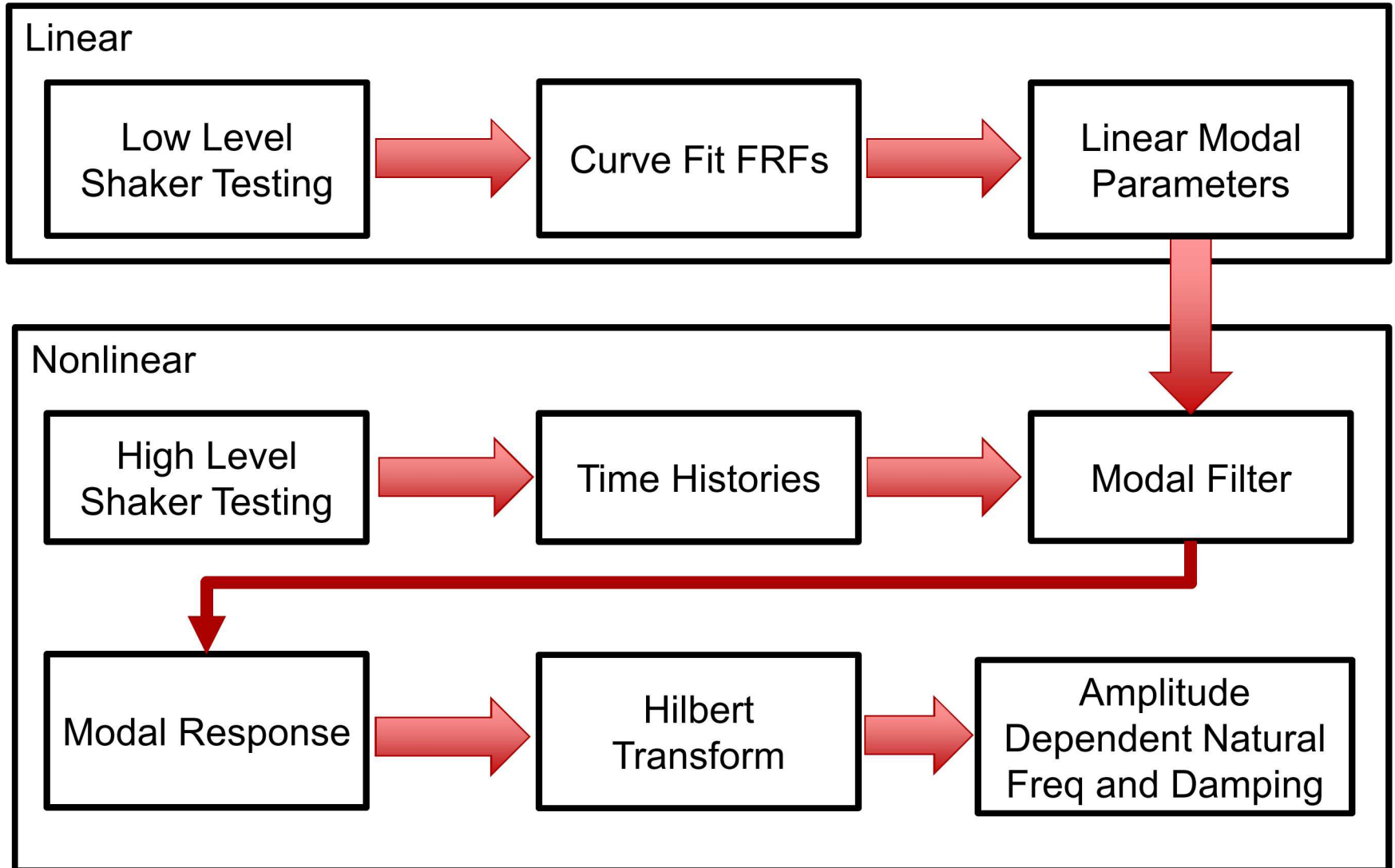




# Experimental Setup

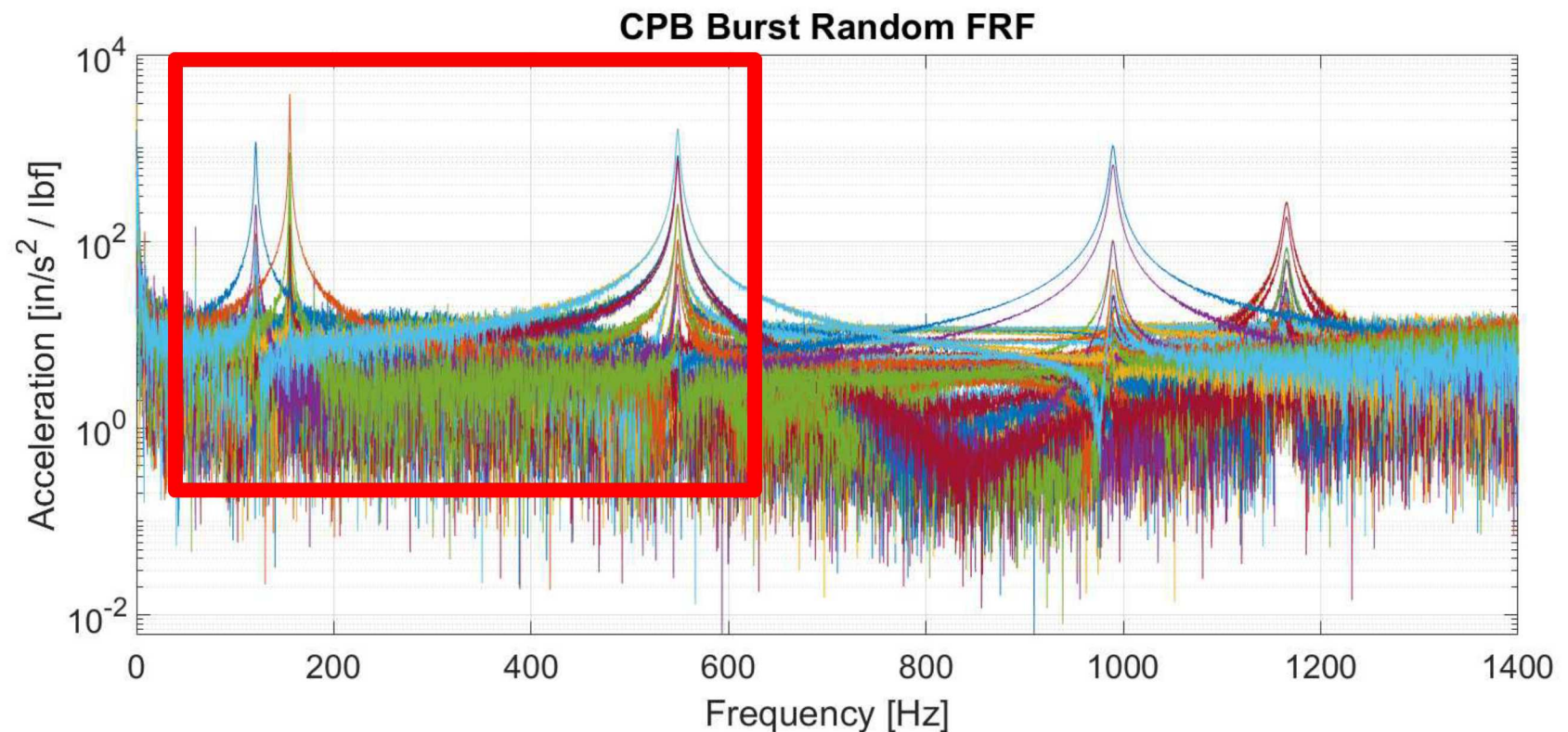


# Experimental Process



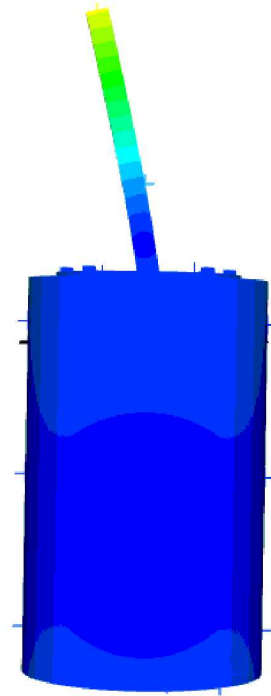
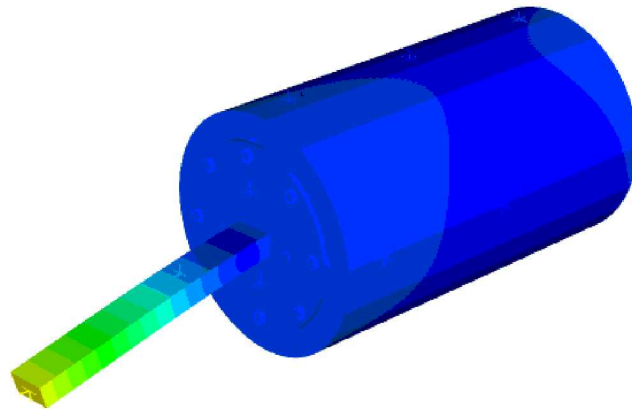
# Linear Experimental Data

- Employed low level burst random excitation from the shaker
  - Curve fit linear FRFs for modeshapes to use as a modal filter



# Mode 1

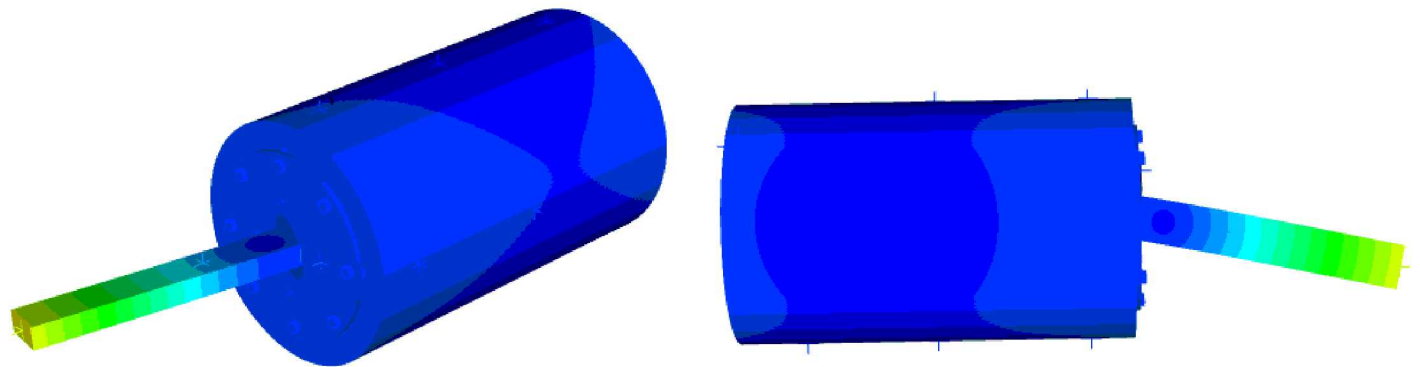
Mode Description	Experimental $\omega_n$ (Hz)
1st Beam Bending X	120.8





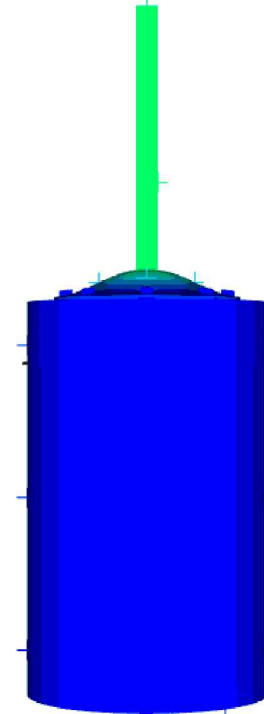
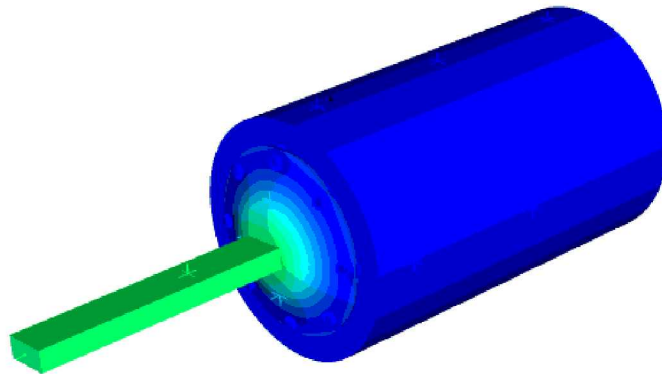
# Mode 2

Mode Description	Experimental $\omega_n$ (Hz)
1st Beam Bending Y	155.3



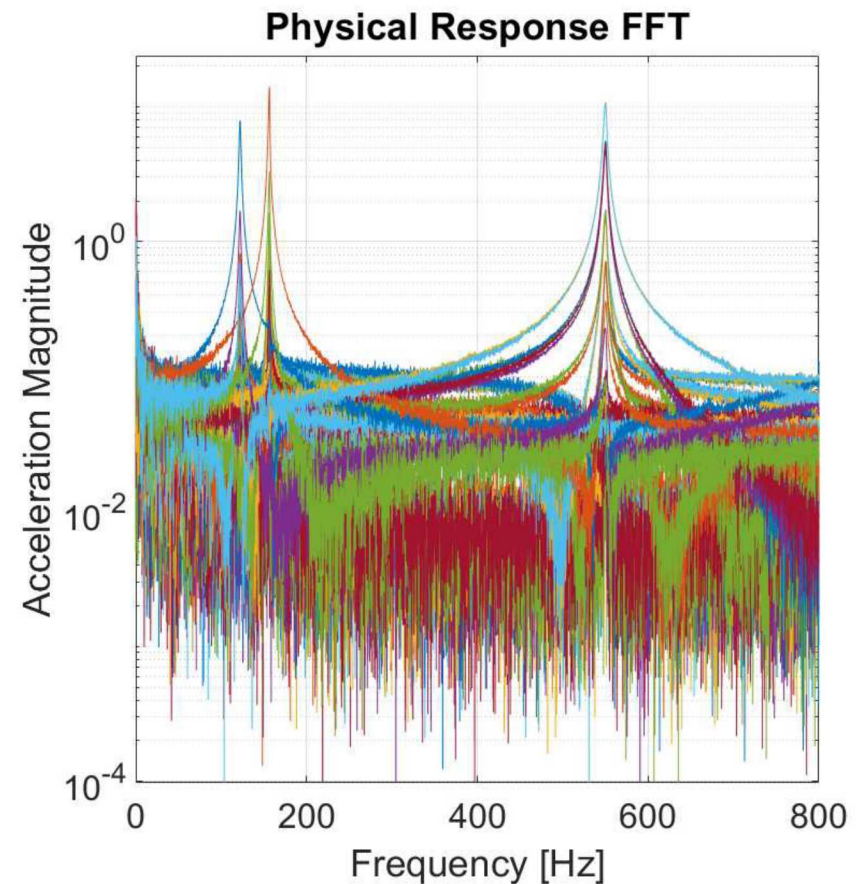
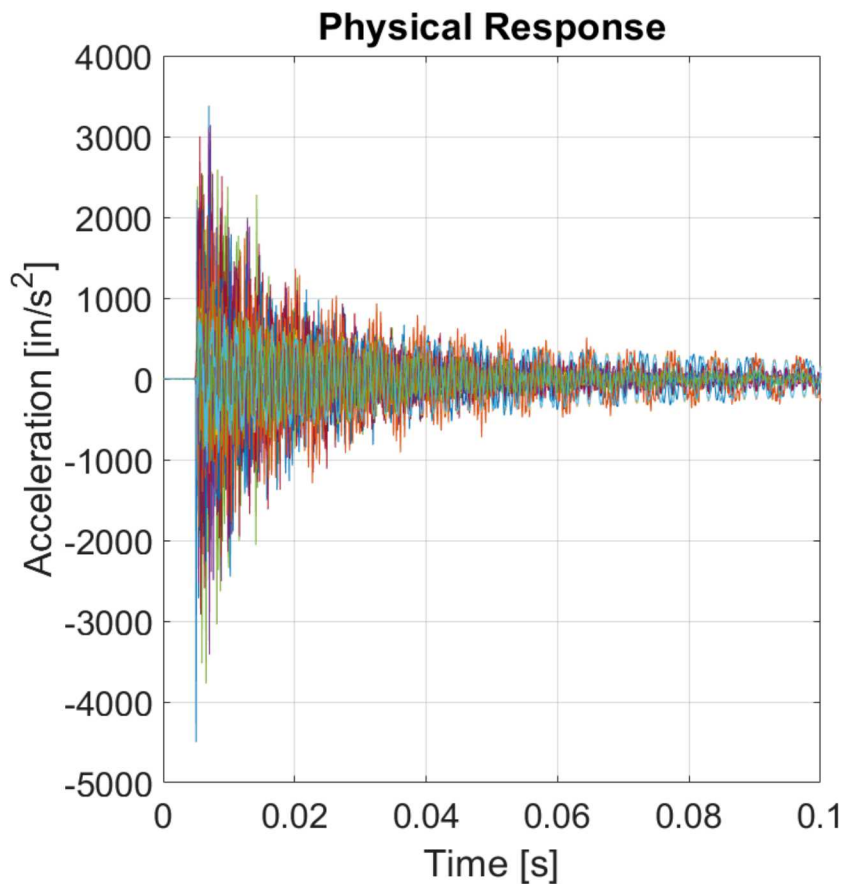
# Mode 3

Mode Description	Experimental $\omega_n$ (Hz)
Plate Drum	548.43



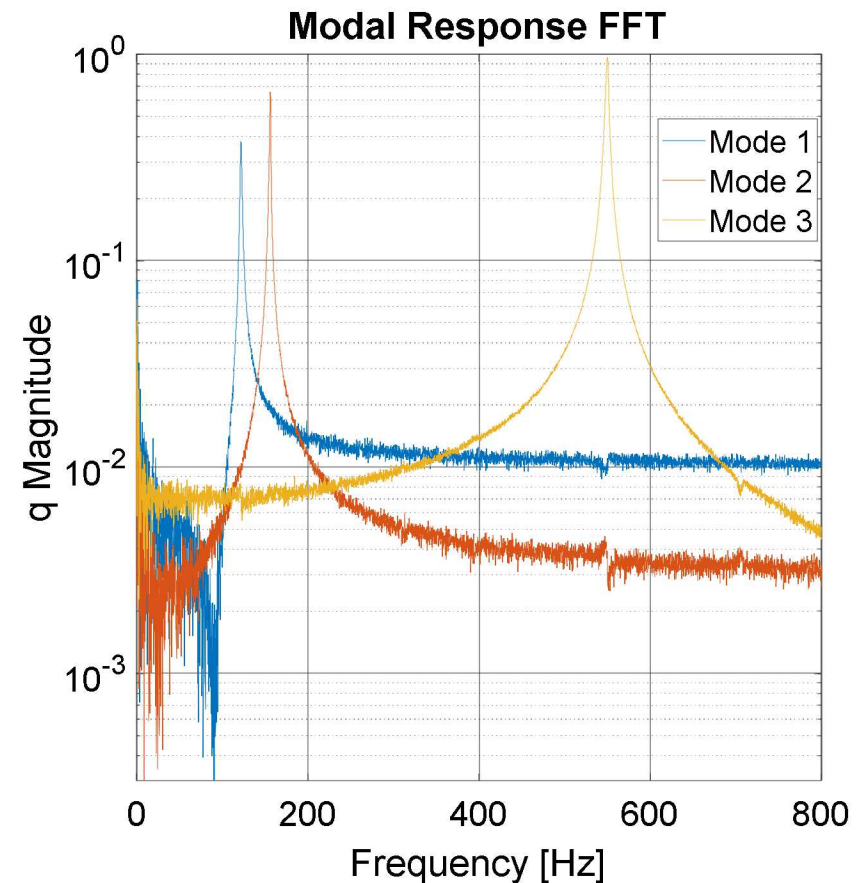
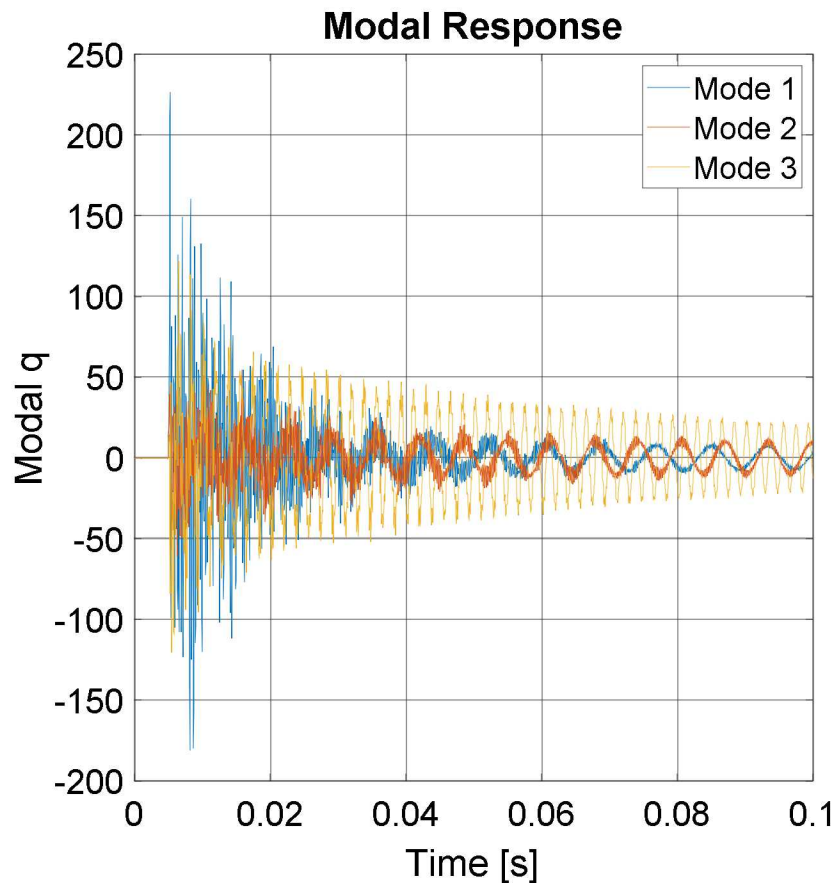
# Modal Filtering

- Linear mode shapes allow for filtering of physical response into modal coordinates



# Modal Filtering

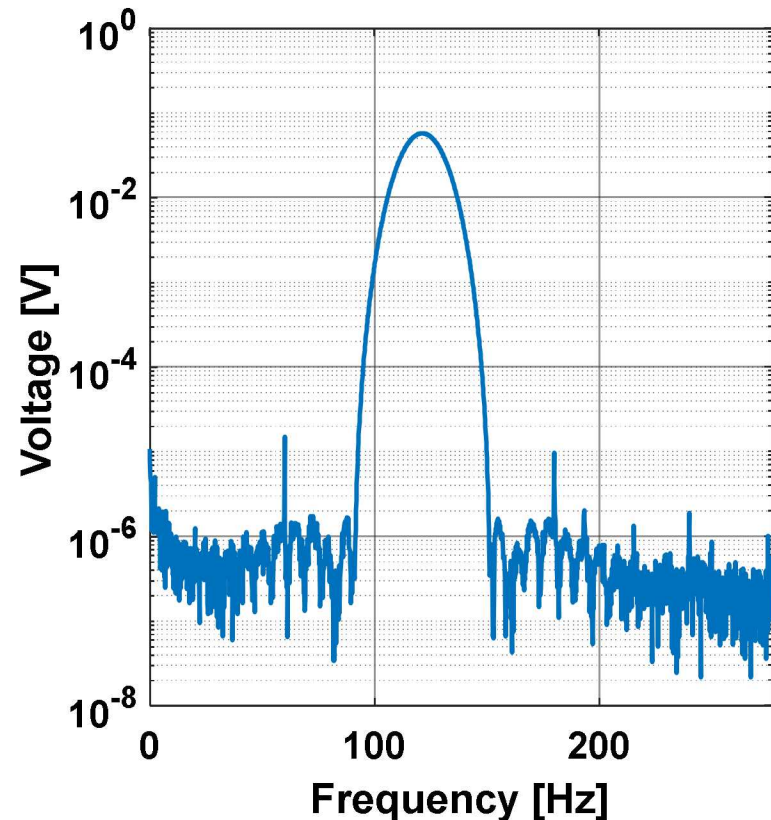
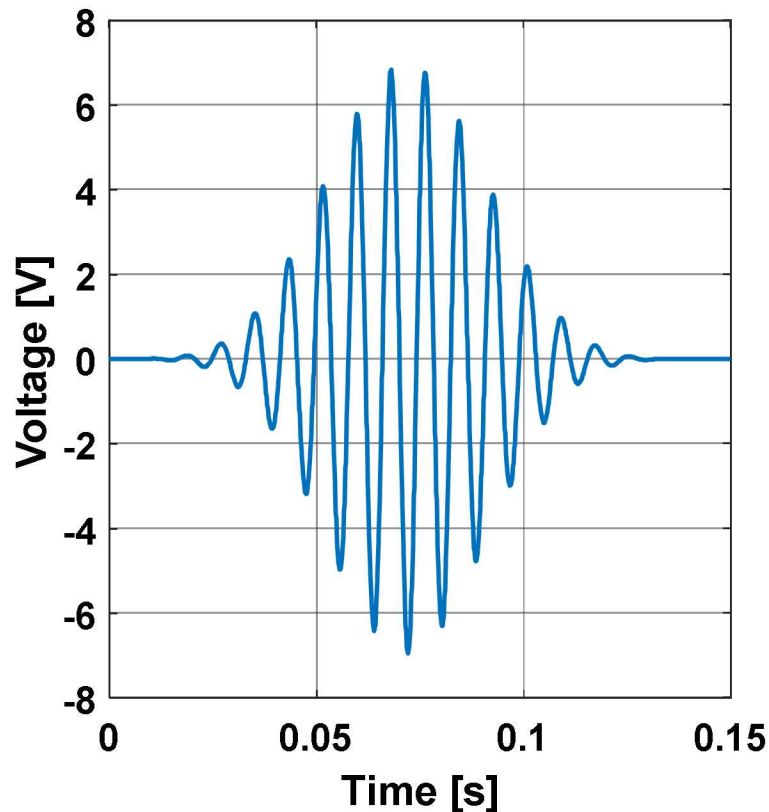
- Linear mode shapes allow for filtering of physical response into modal coordinates





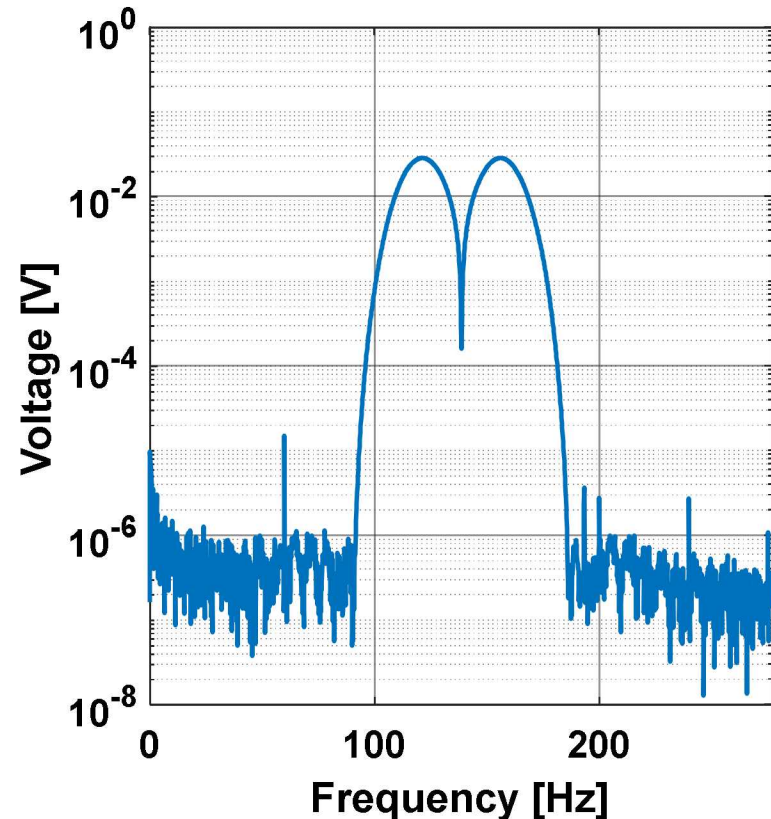
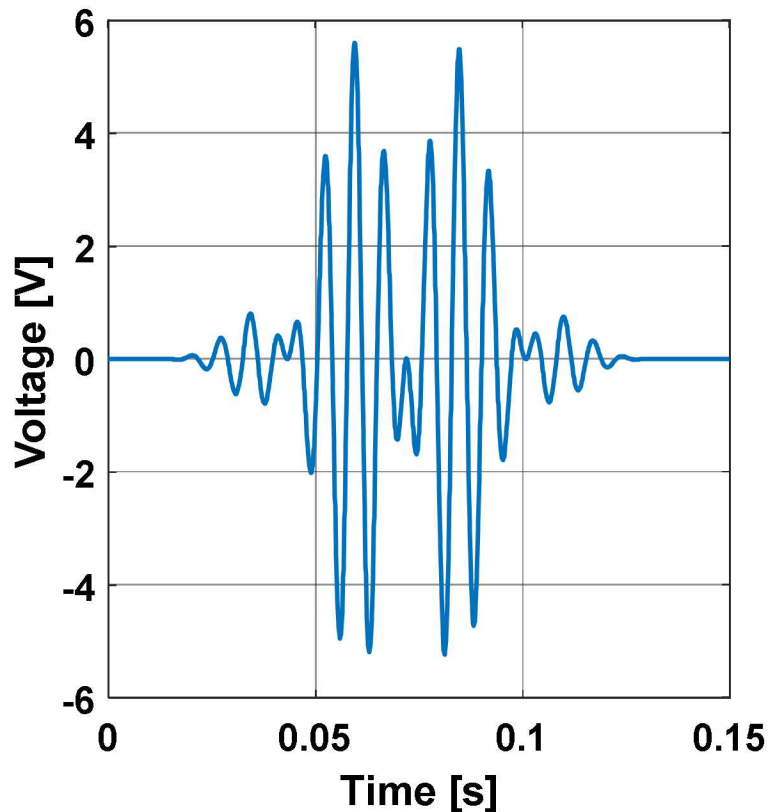
# Nonlinear Data

- Shaker delivers definable force input – able to create a voltage signal with specific frequency content



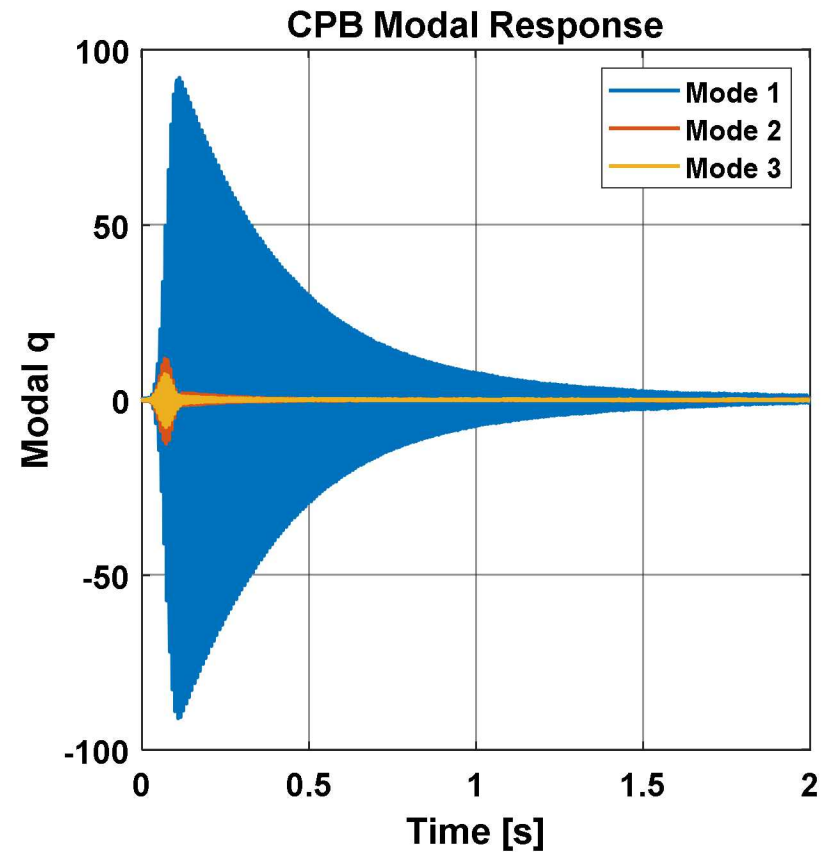
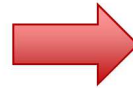
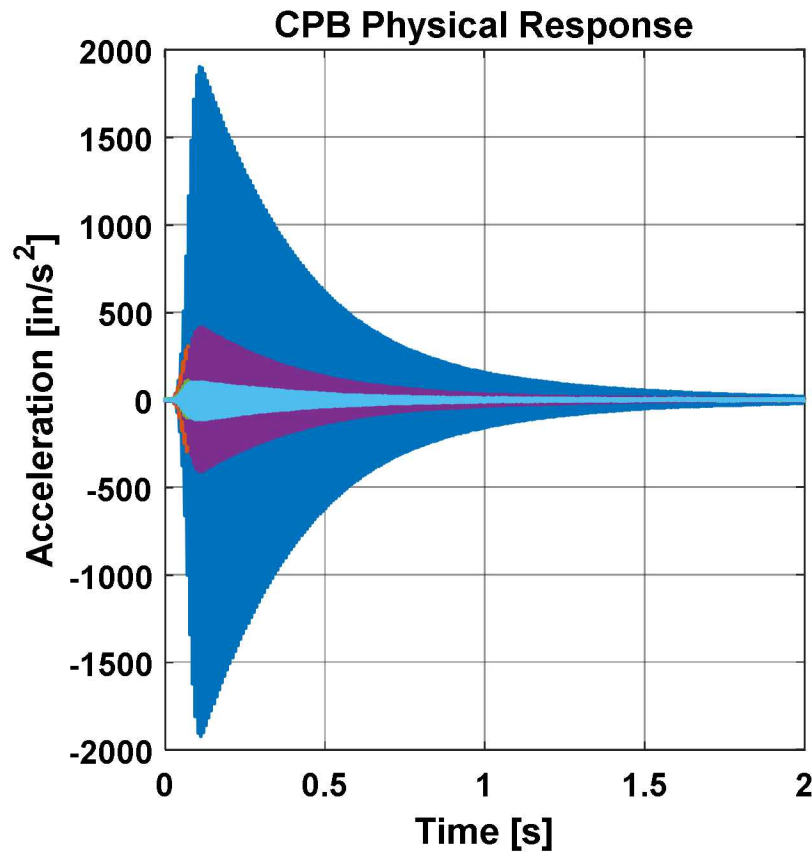
# Nonlinear Data

- Shaker delivers definable force input – able to create a voltage signal with specific frequency content



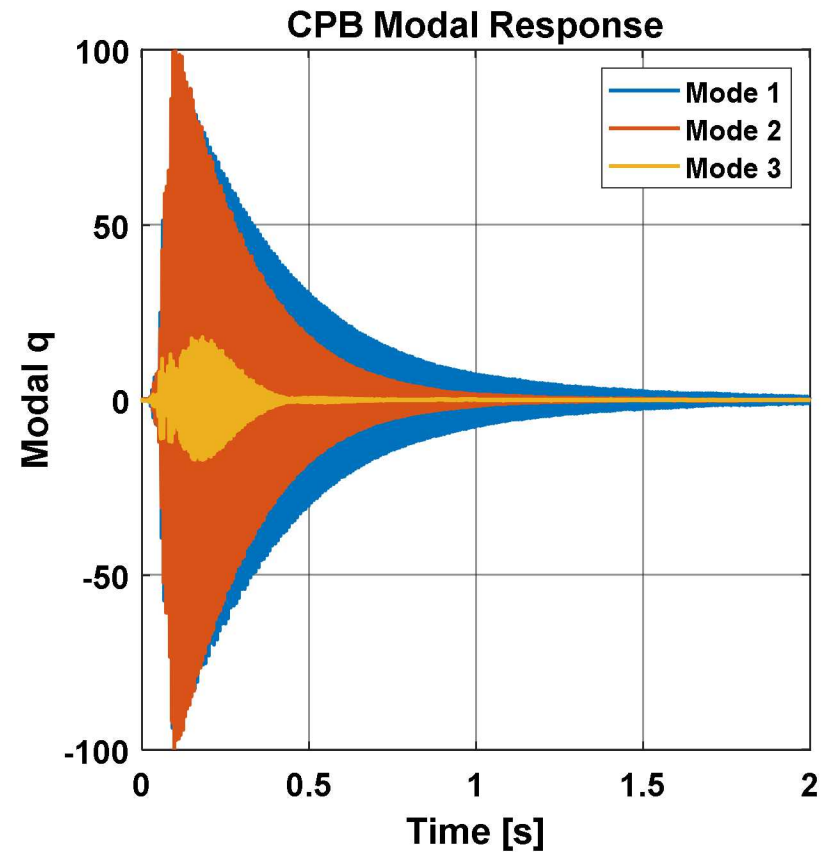
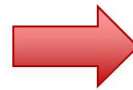
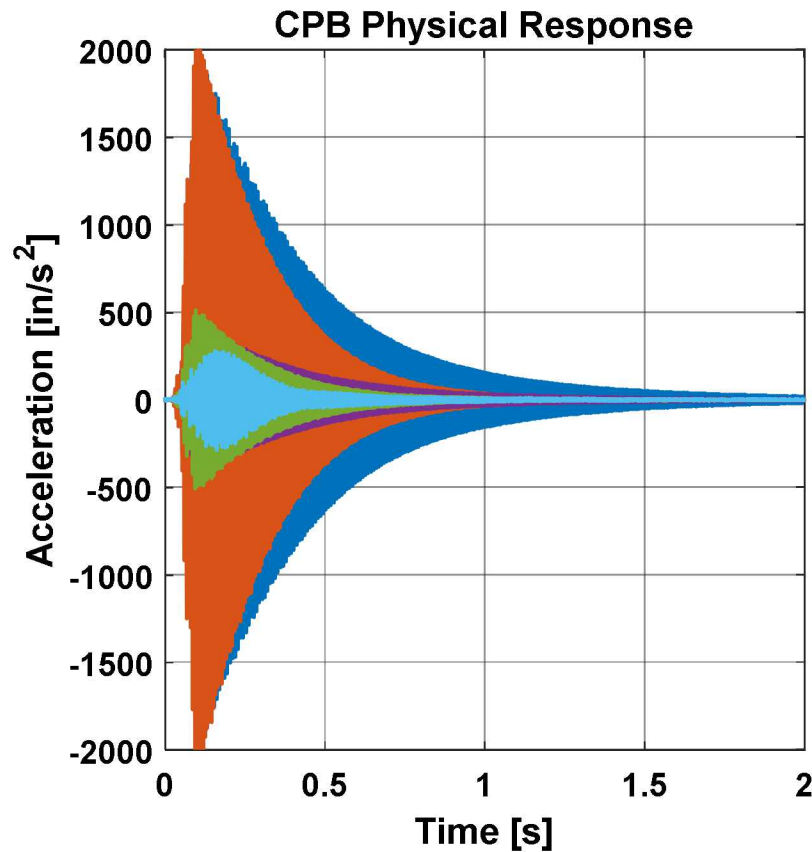
# Nonlinear Data

- Use shaker to excite specific modes



# Nonlinear Data

- Use shaker to excite specific modes

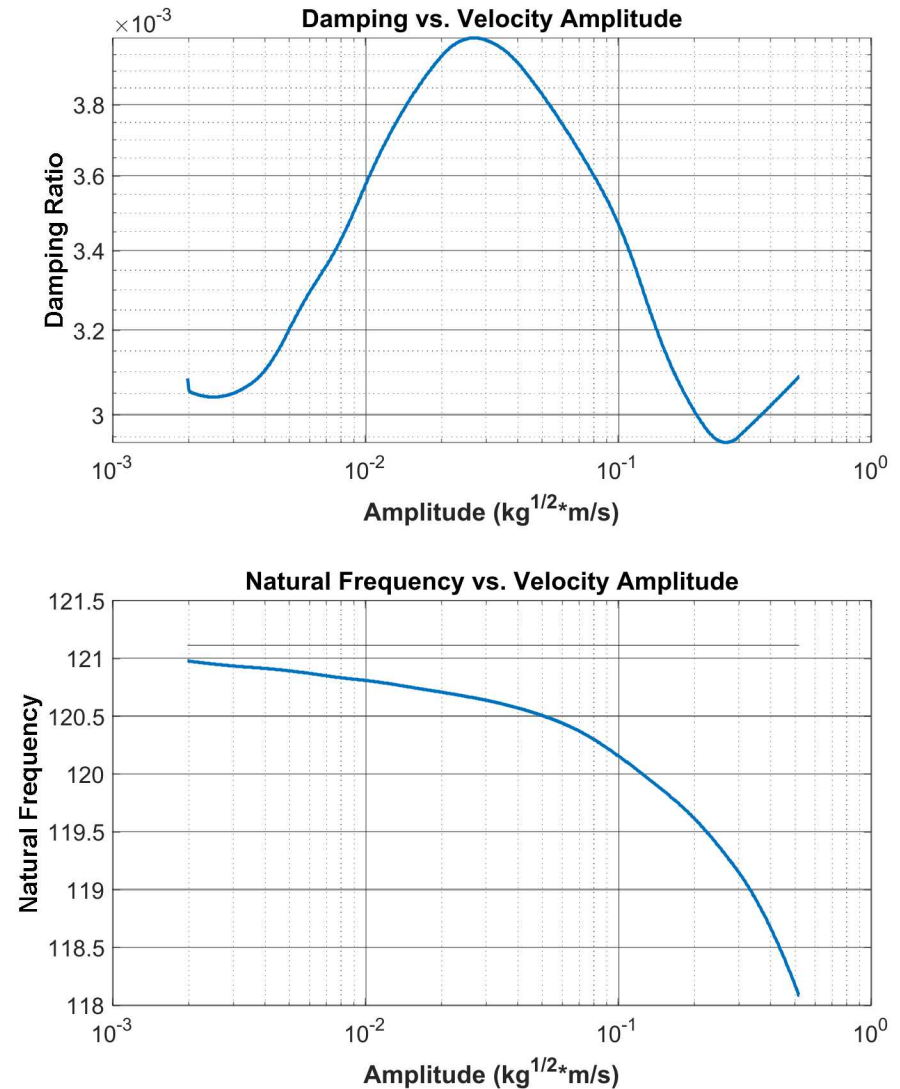
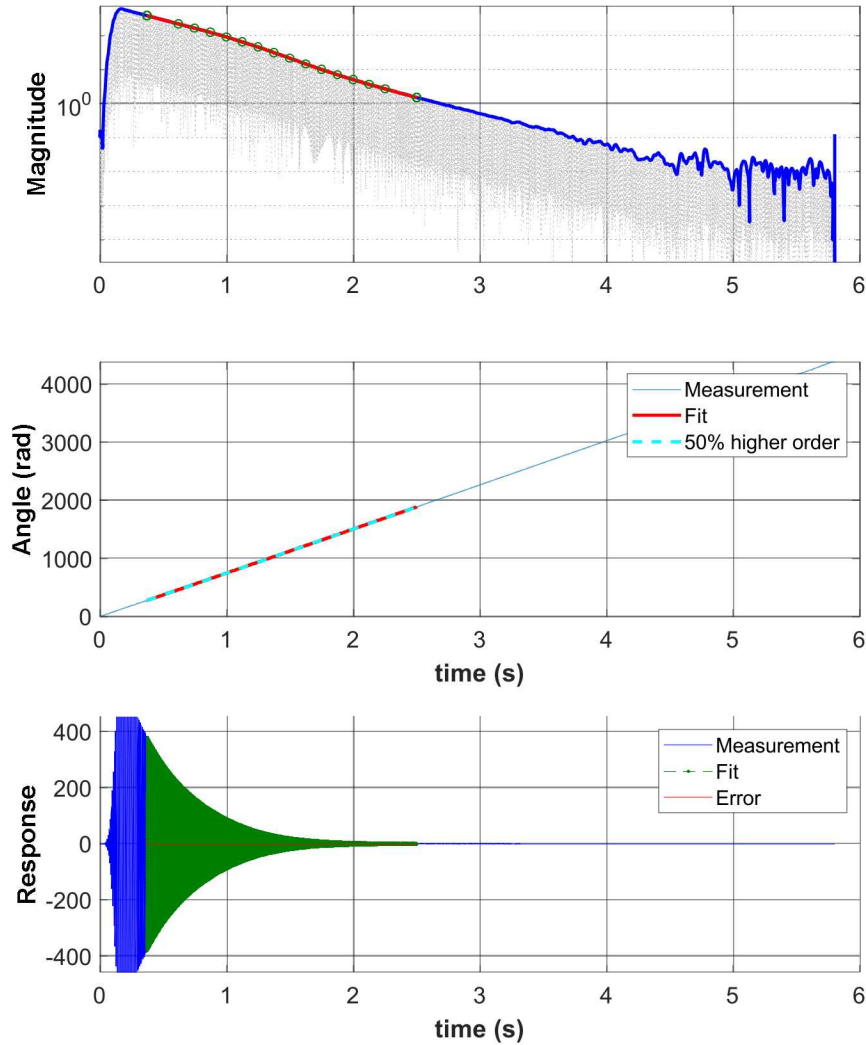


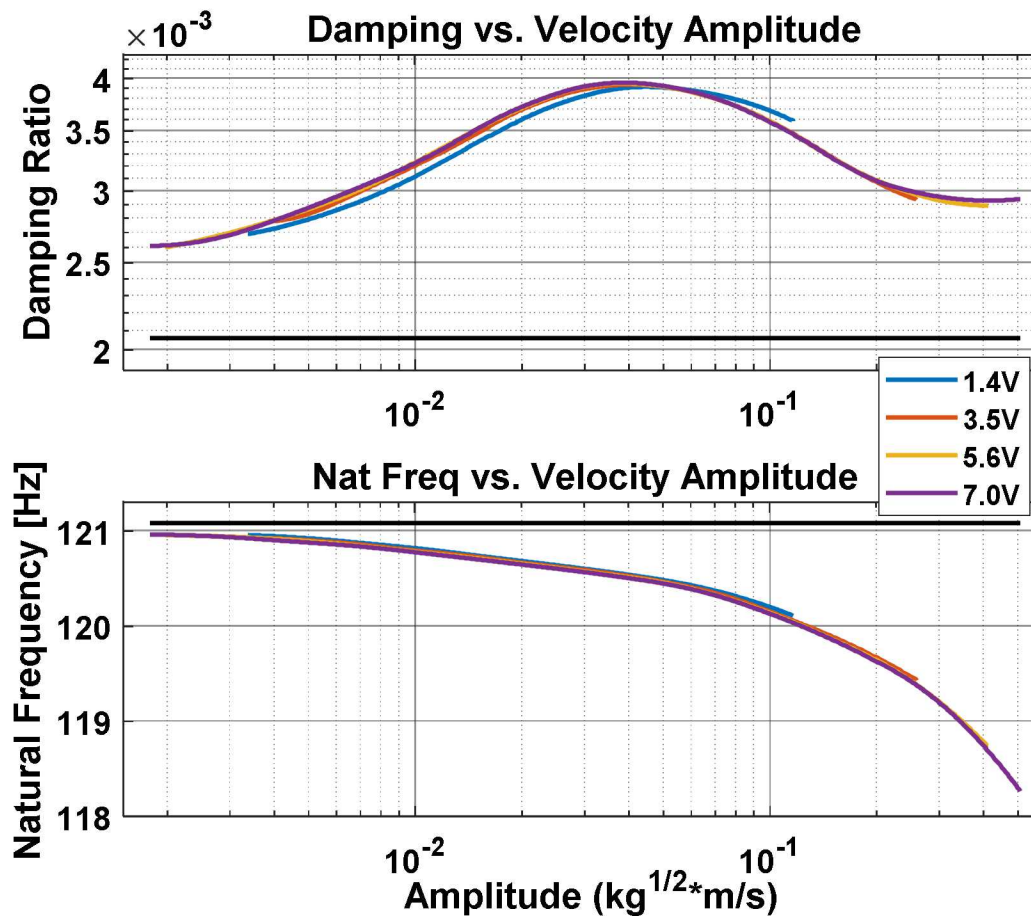


# Hilbert Analysis

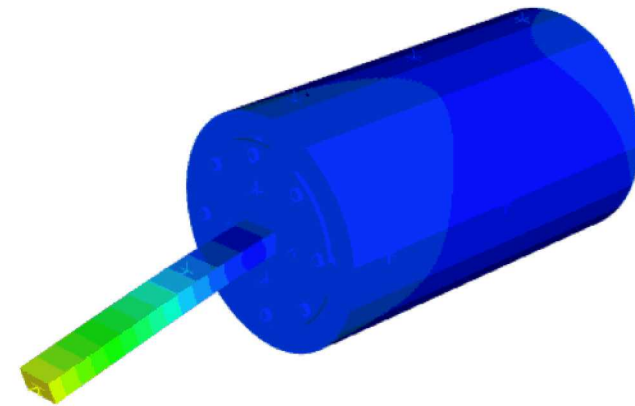
- Requires that each response be uncoupled such that it can be represented by a SDOF system
  - Signal can be represented by a decaying harmonic
  - $\ddot{\eta} = \text{Re}[\exp(\psi_1(t) + i \psi_2(t))]$
- Compute Hilbert Transformation ( $\mathcal{H}(t)$ ) for an amplitude dependent representation of damping and frequency
- $\omega_{d,r} = \frac{d\psi_2}{dt}$
- $\zeta_r \triangleq \frac{d\psi_1}{dt} / \omega_r$

# Hilbert Analysis



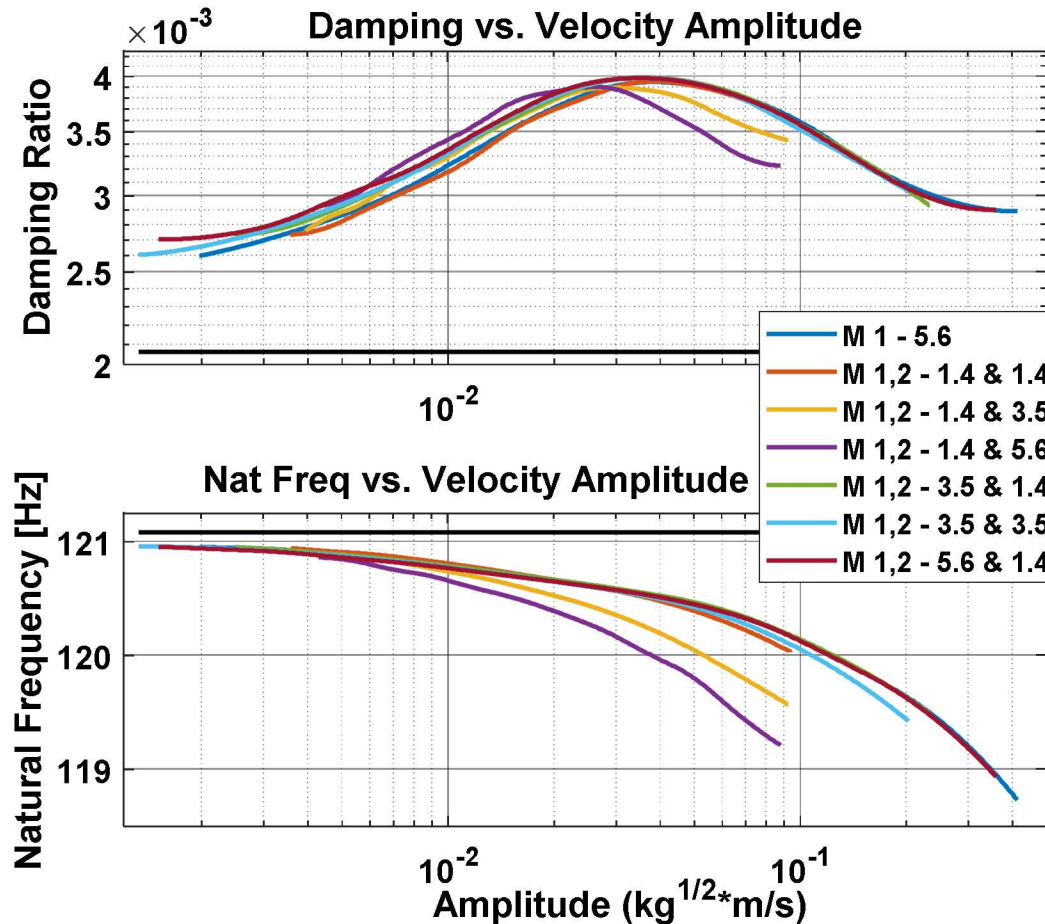
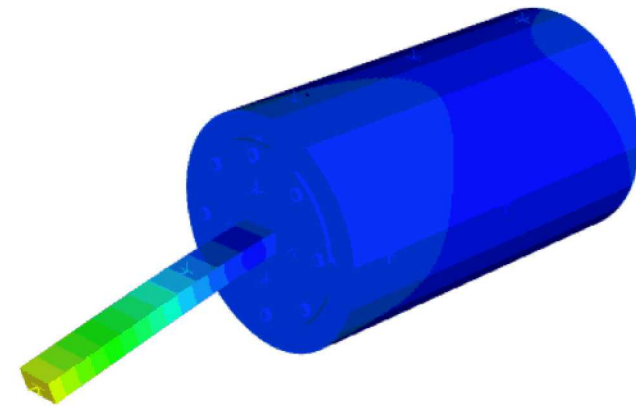


# Mode 1



- When excited alone at various levels, frequency and damping overlay with increasing amplitude

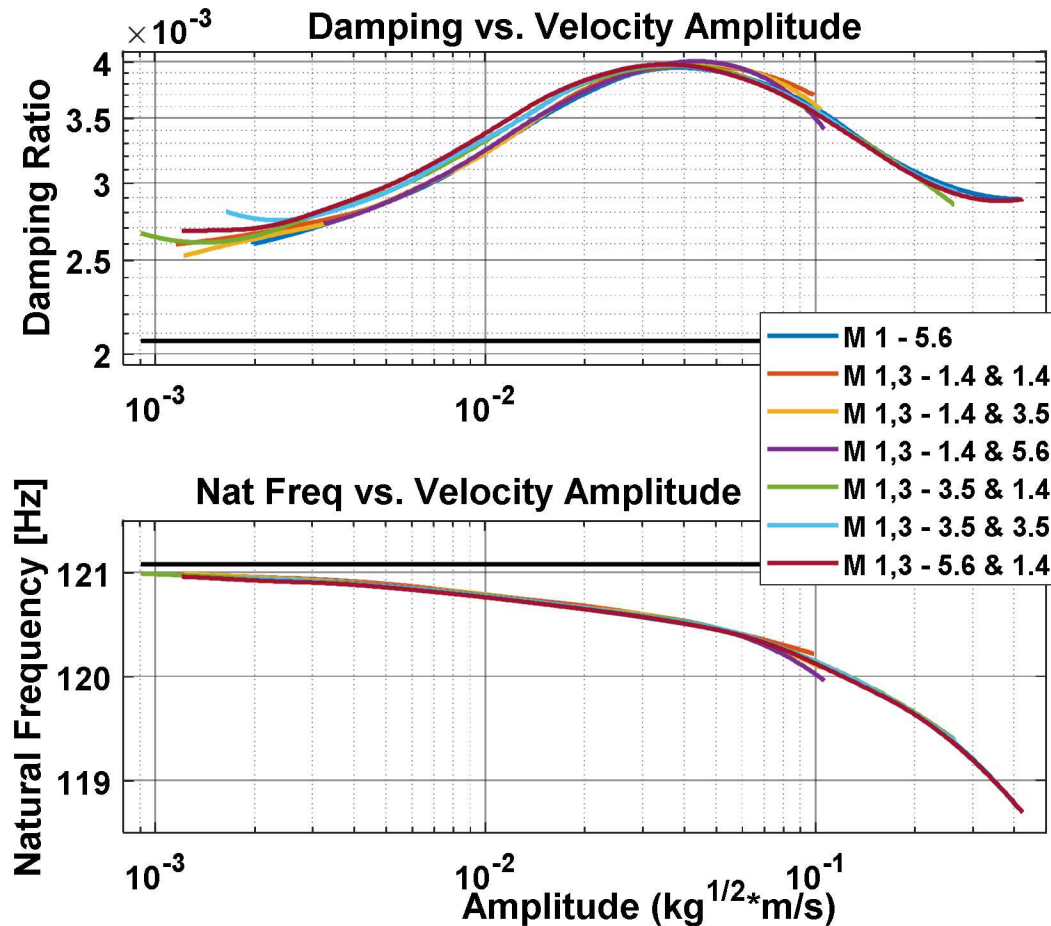
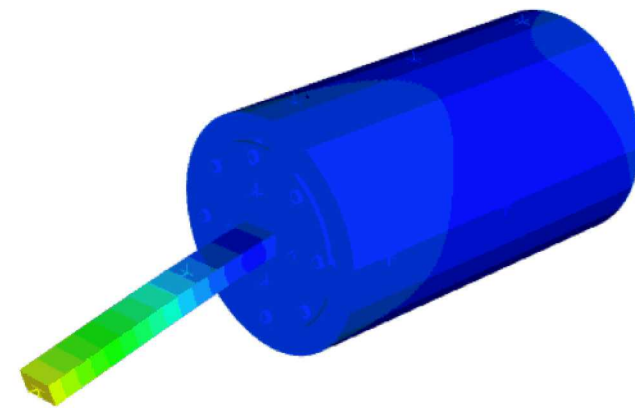
## Mode 1 & 2



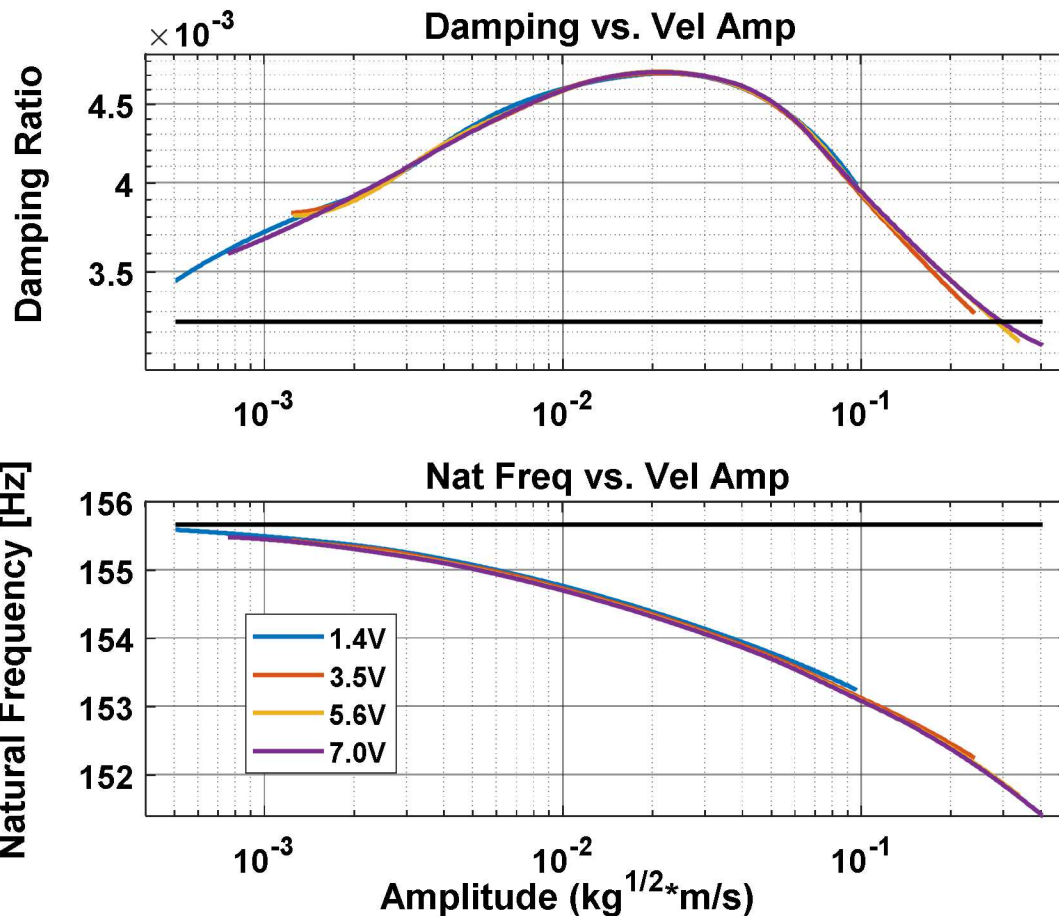
- Coupling visible as a frequency and damping shift when mode 2 is excited to a higher level than mode 1



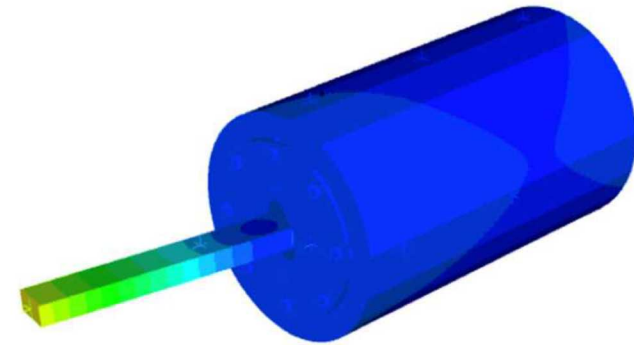
## Mode 1 & 3



- Mode 1 appears to be completely unaffected by mode 3.

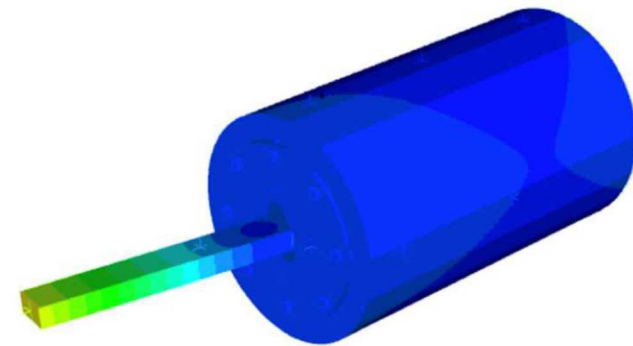
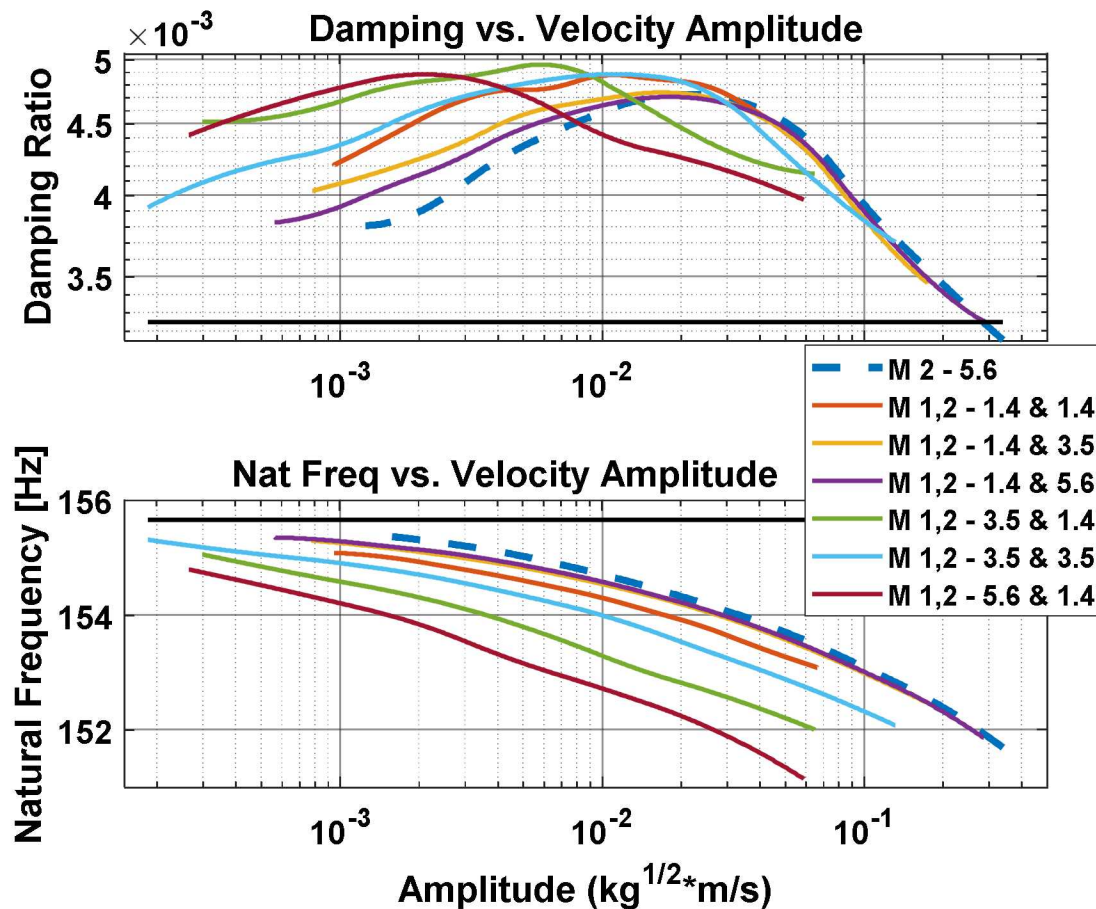


## Mode 2



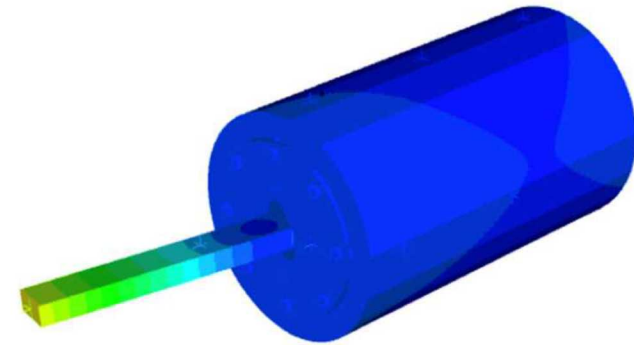
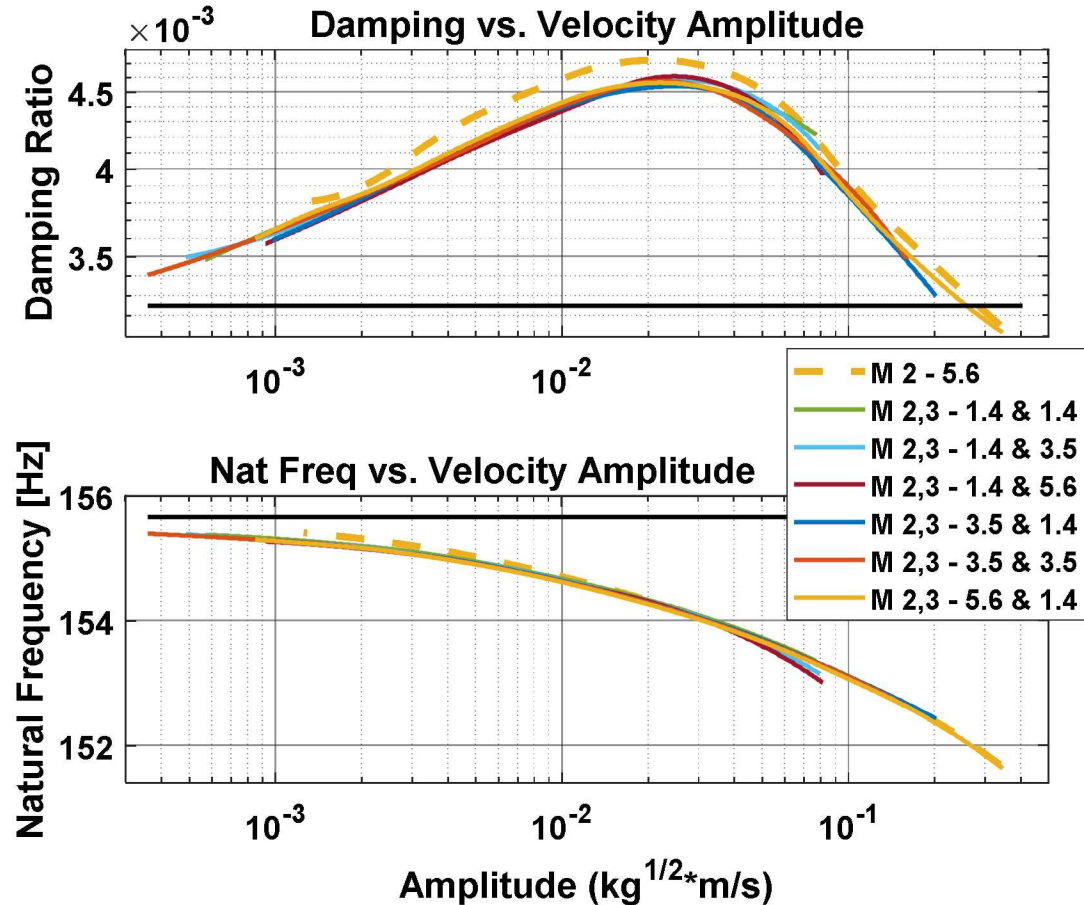
- As with Mode 1, when Mode 2 is excited alone, frequency and damping overlay with increasing amplitude.

## Mode 2 & 1



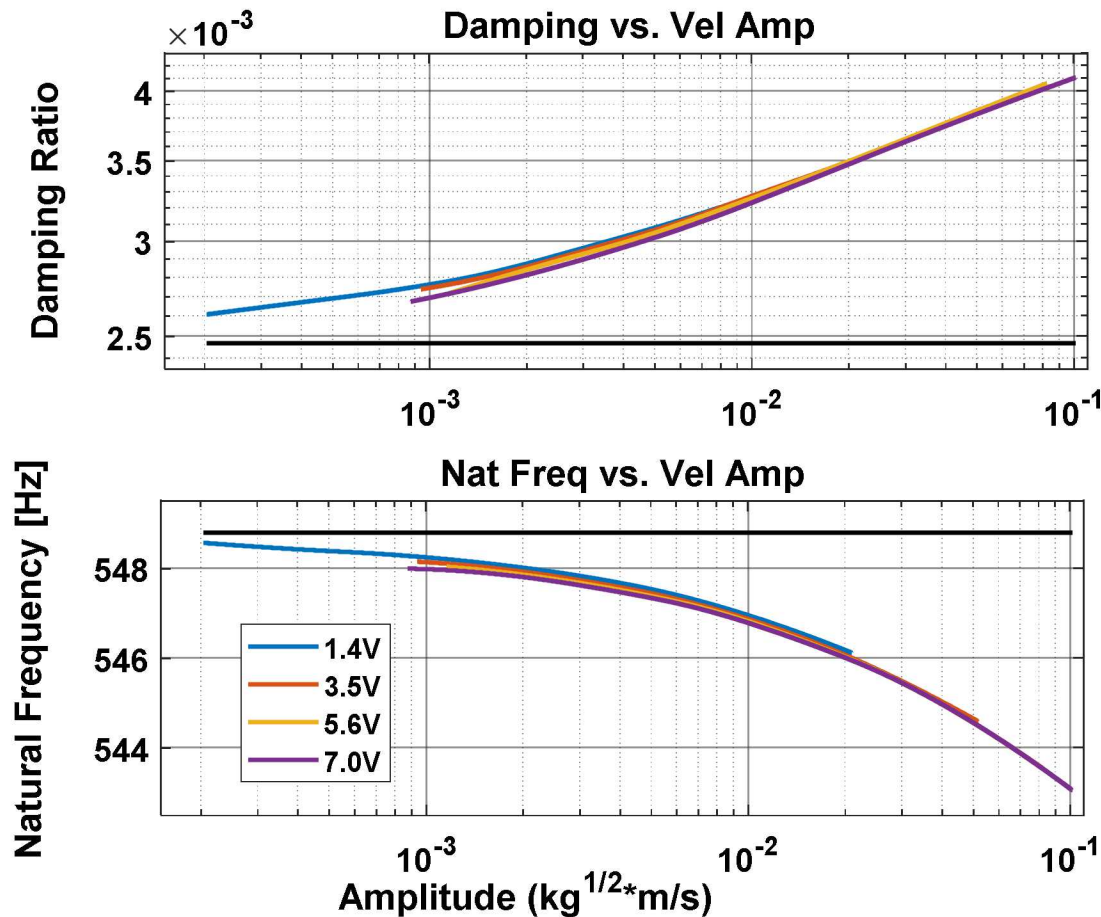
- Observe the same frequency and damping shift, but now to a greater degree in all cases where mode 1 is also excited.

## Mode 2 & 3

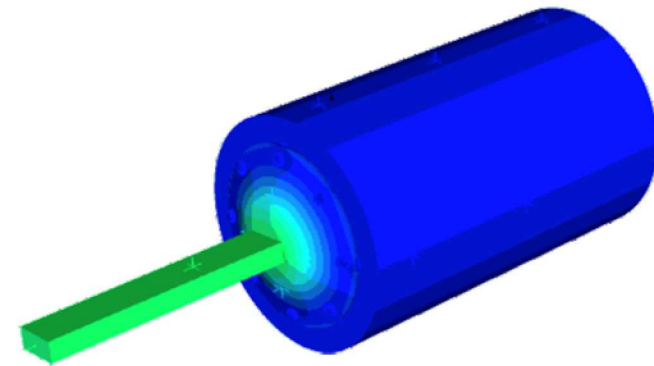


- Mode 2 also appears to be totally indifferent as to the presence of mode 3.

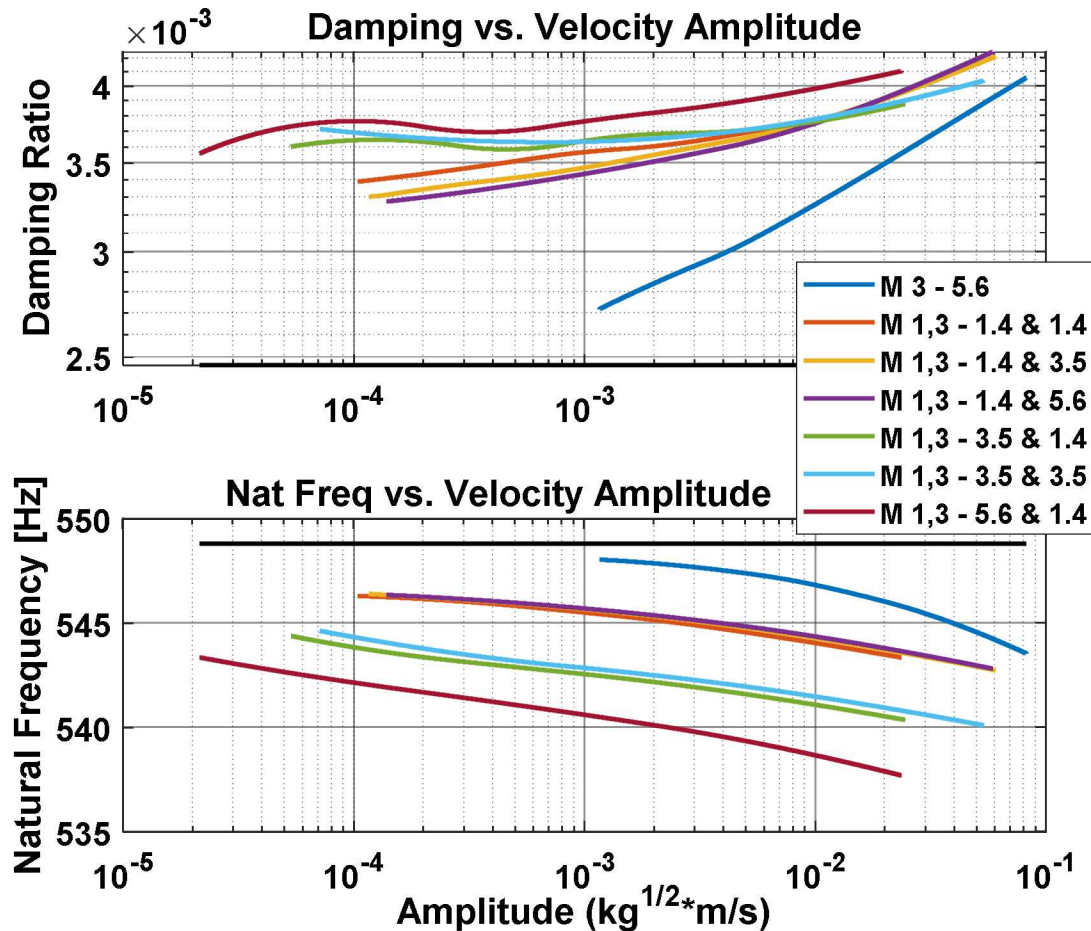




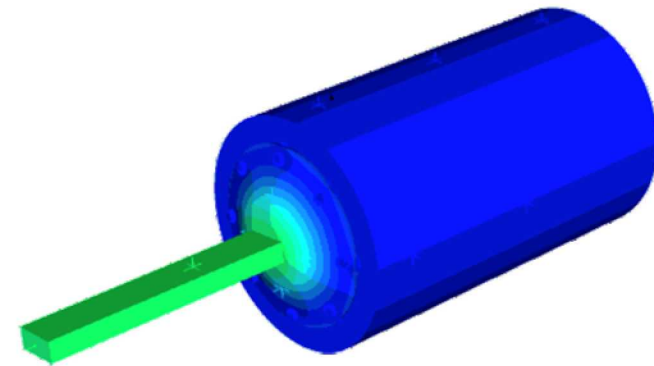
## Mode 3



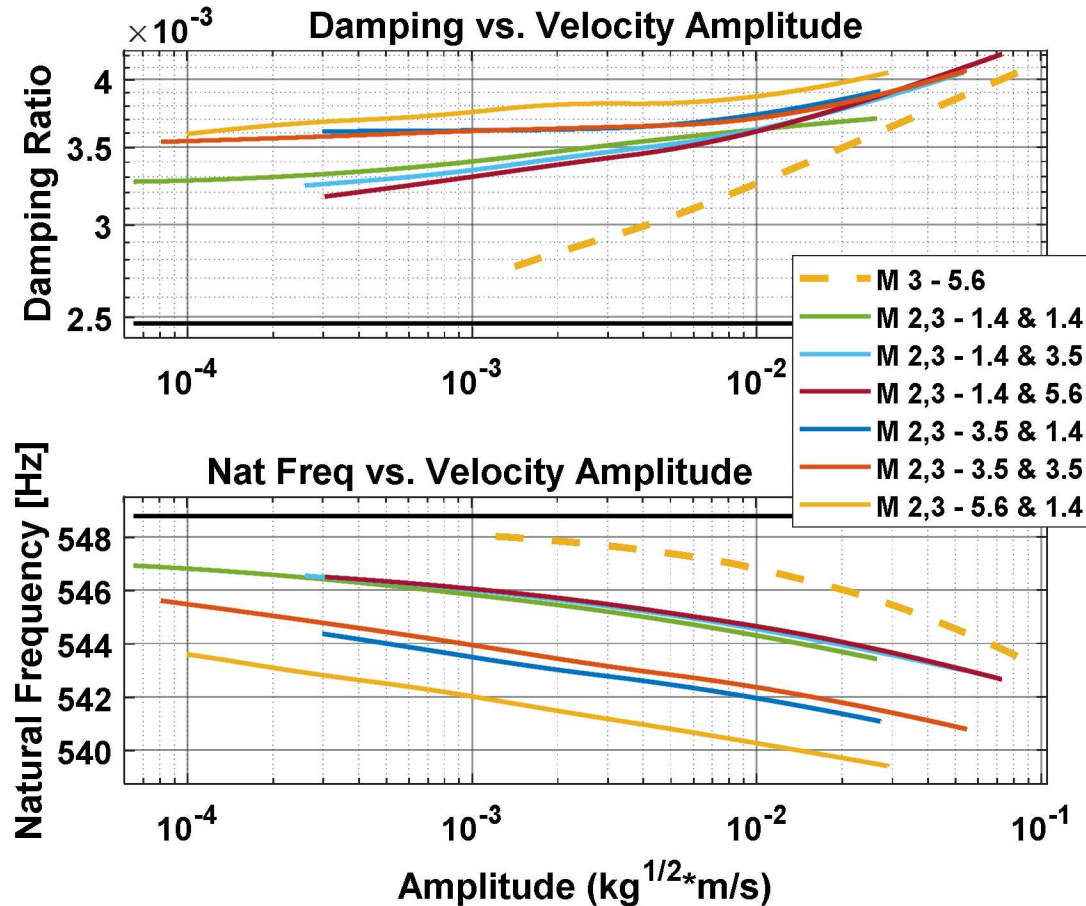
- When excited individually, all modes exhibit consistent frequency and damping shifts with increasing amplitude



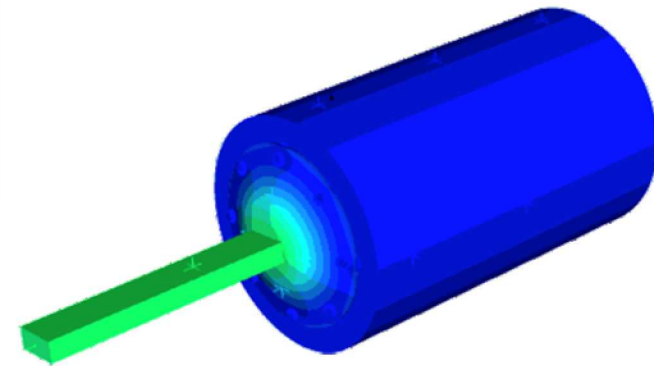
## Mode 3 & 1



- Mode 3 shows significant decreases in frequency and increases in damping when mode 1 is also excited at any level.



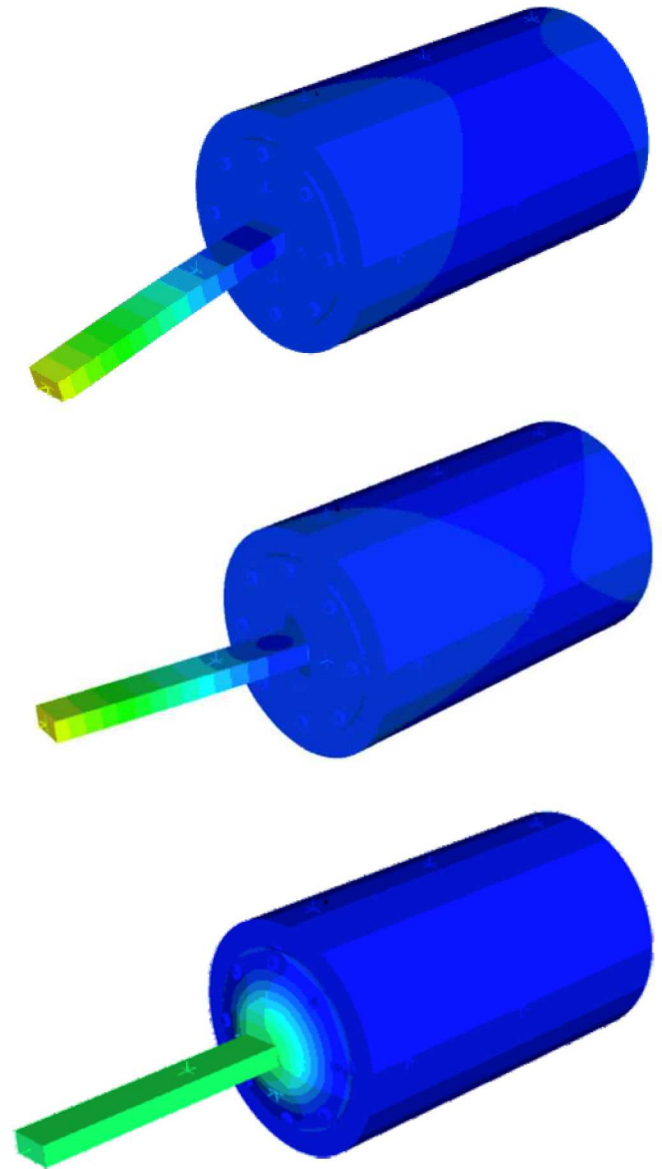
## Mode 3 & 2



- When mode 3 is excited with mode 2, similar drastic shift in frequency and damping are observed.

# Closing Remarks

- When excited alone, all three modes have very consistent frequency and damping responses.
- Mode 1 and 2 show signs of modal coupling when simultaneously excited.
  - Mode 2 appears to be more significantly effected.
- Neither mode 1 or 2 display any indication of modal coupling with mode 3.
- However, mode 3 exhibits very strong coupling with modes 1 and 2.





# Acknowledgments

- This research was conducted at the 2018 Nonlinear Mechanics and Dynamics Research Institute hosted by Sandia National Laboratories and the University of New Mexico.
- Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA-0003525.



