



U-slot Patch Antenna Theory and Design



PRESENTED BY

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Outline

Review patch antennas

The U-slot patch antenna historically

Intro CMT & CMA

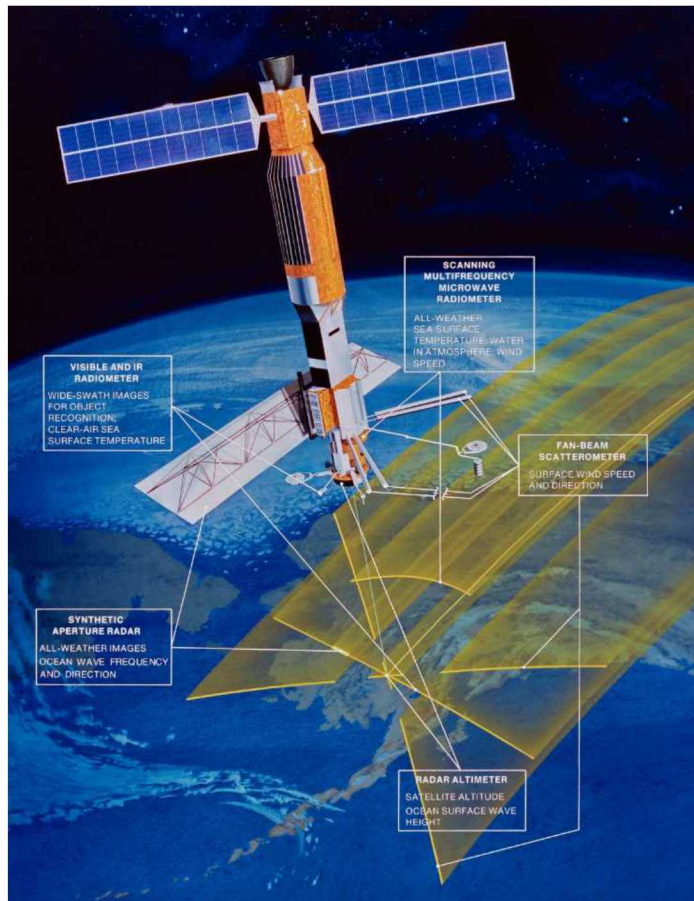
CMA of the U-slot patch > show CMT is relevant

Design methodology

Patch antennas

Attributed to Deschamps in the 50's...

Byron, Howell, Munson developed in the 70's...



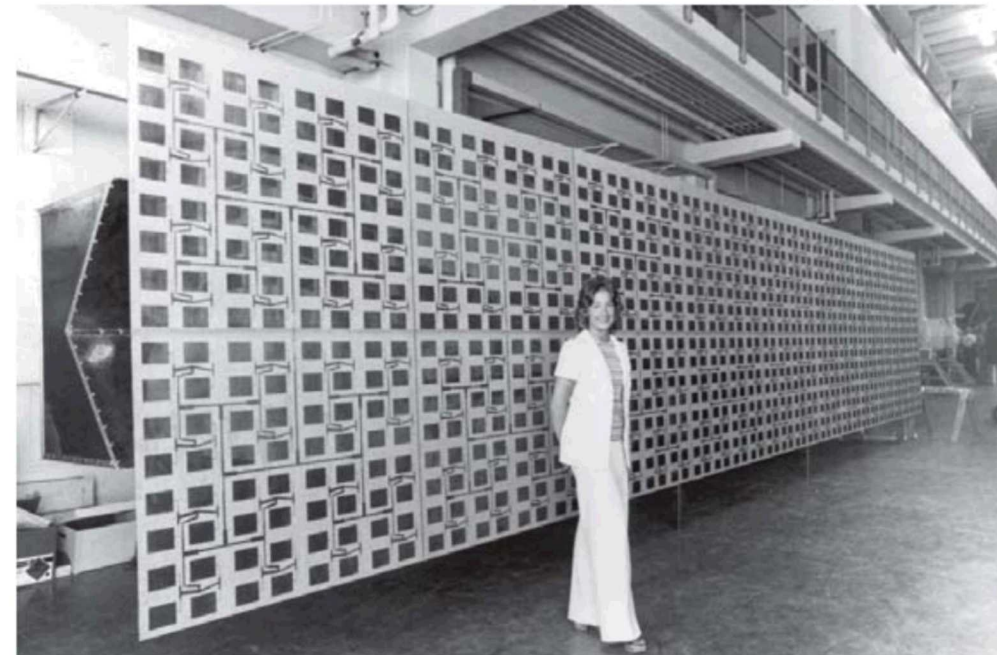
A COMMEMORATION OF DESCHAMPS' AND SICHAK'S "MICROSTRIP MICROWAVE ANTENNAS": 50 YEARS OF DEVELOPMENT, DIVERGENCE, AND NEW DIRECTIONS

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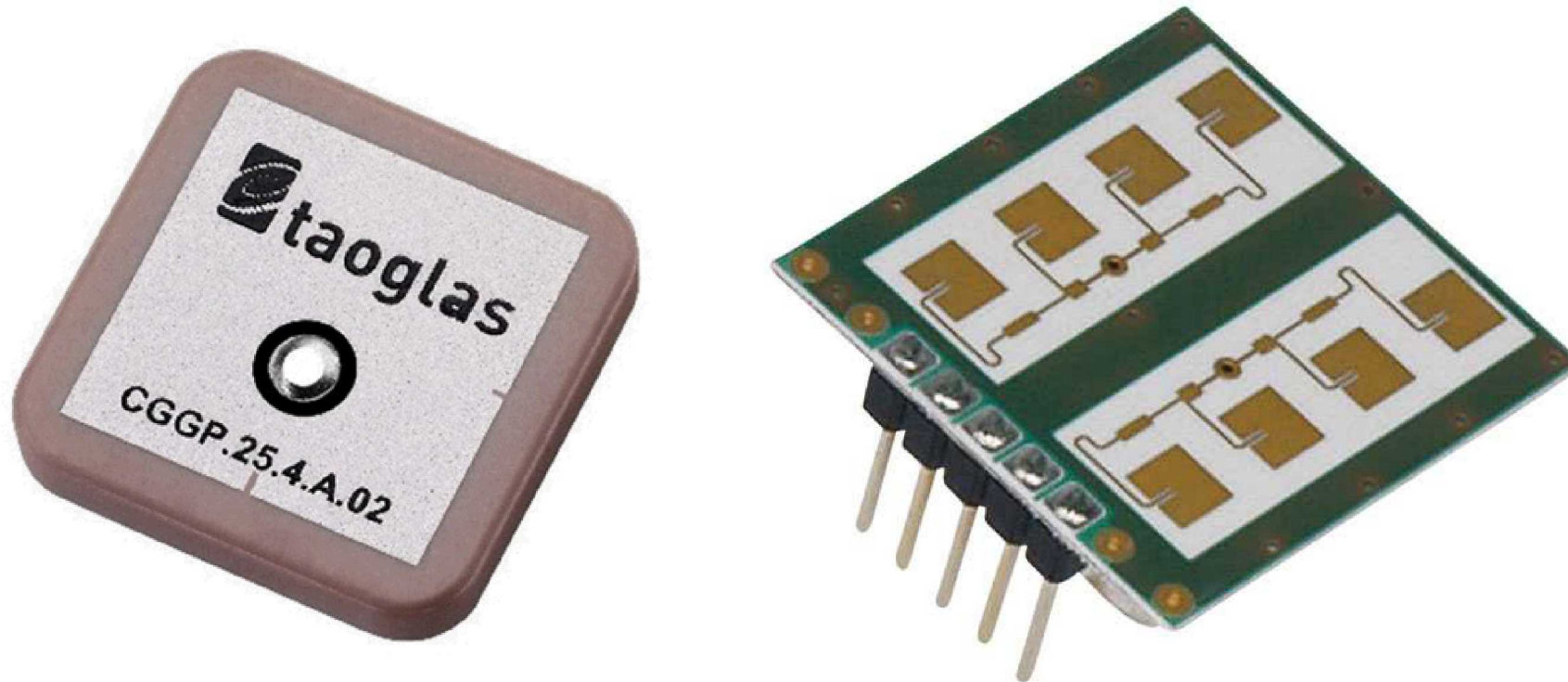
Patch antennas

Pros: Low profile, robust, can potentially be integrated w/ RF/microwave circuitry at low cost

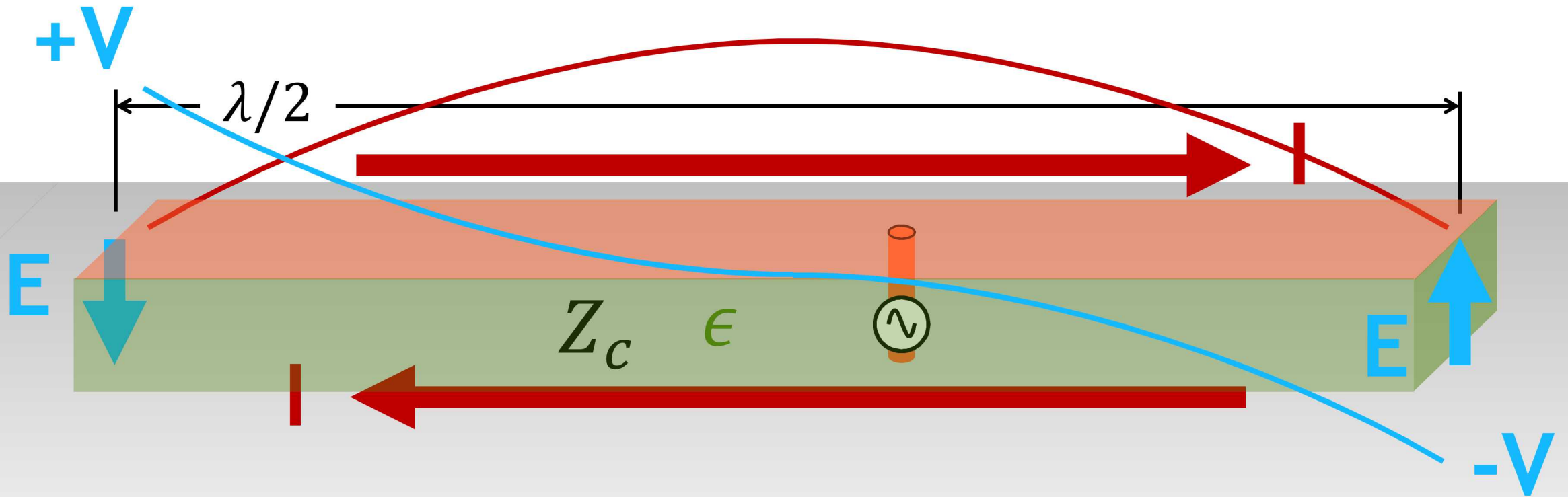
Cons: Limited power handling, narrow impedance bandwidth

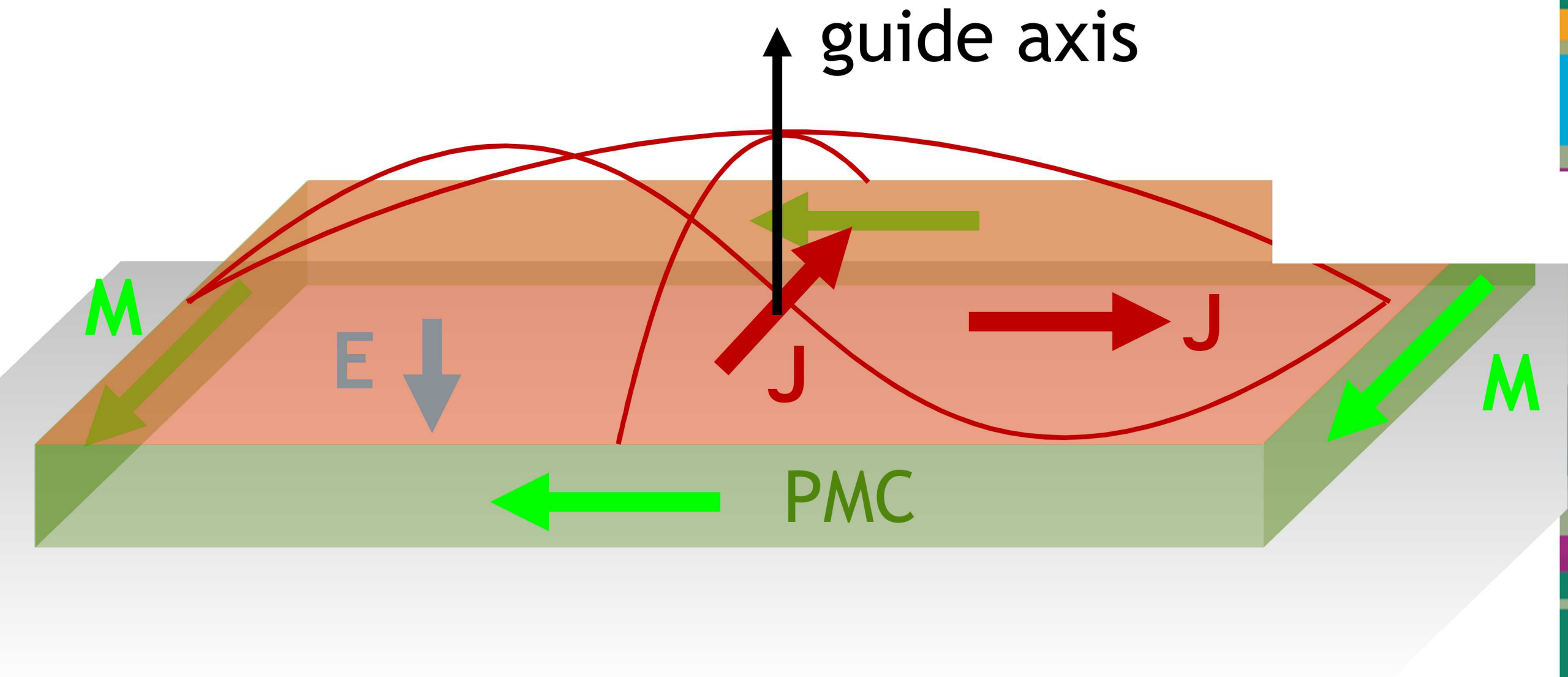
Thicker patch: lower radiation Q (good!) $\Rightarrow$ wider bandwidth, higher radiation efficiency

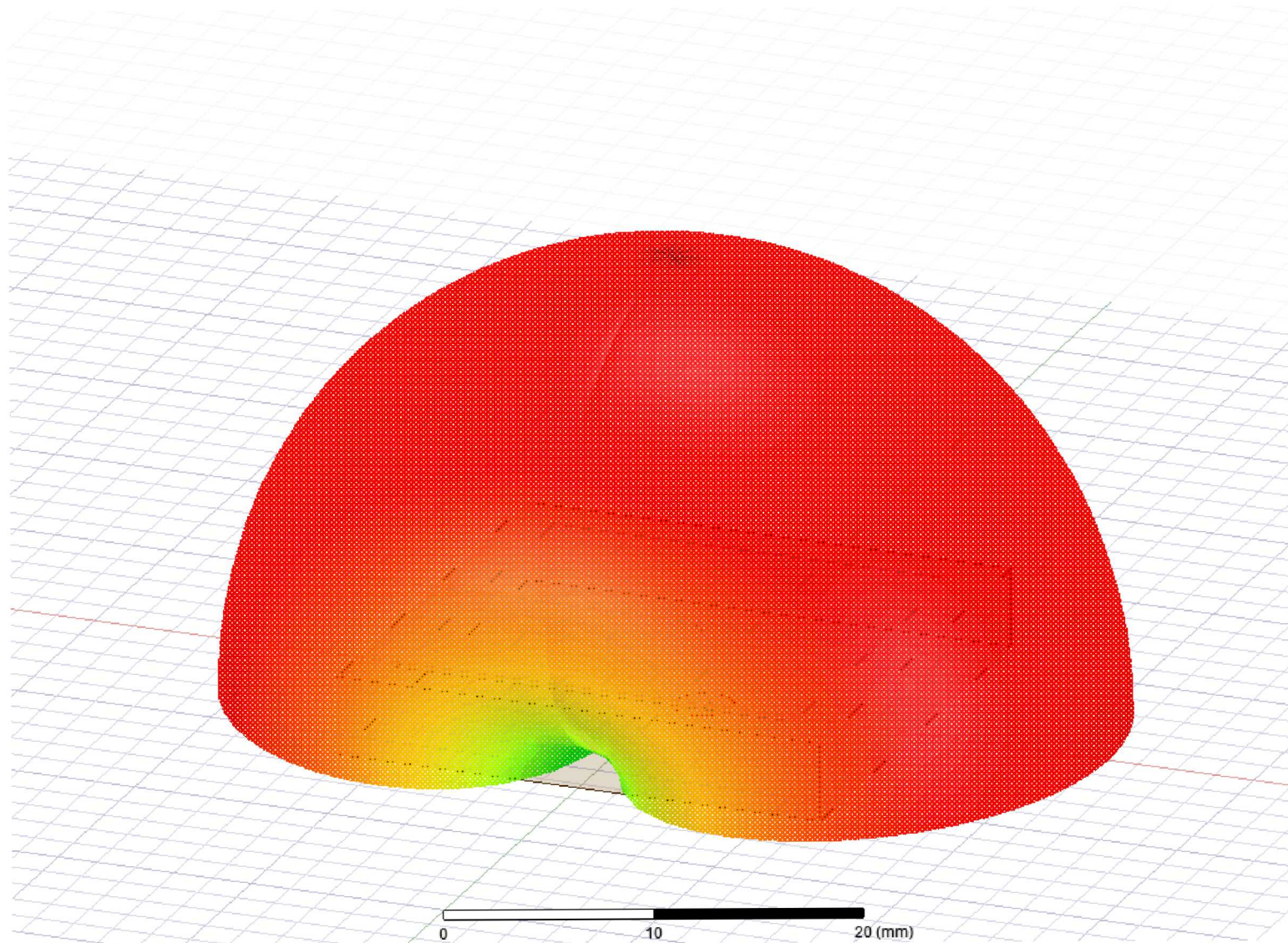
Larger substrate Dk: physically/electrically smaller patch $\Rightarrow$ higher radiation Q (bad!)



5 Patch antennas: t-line model



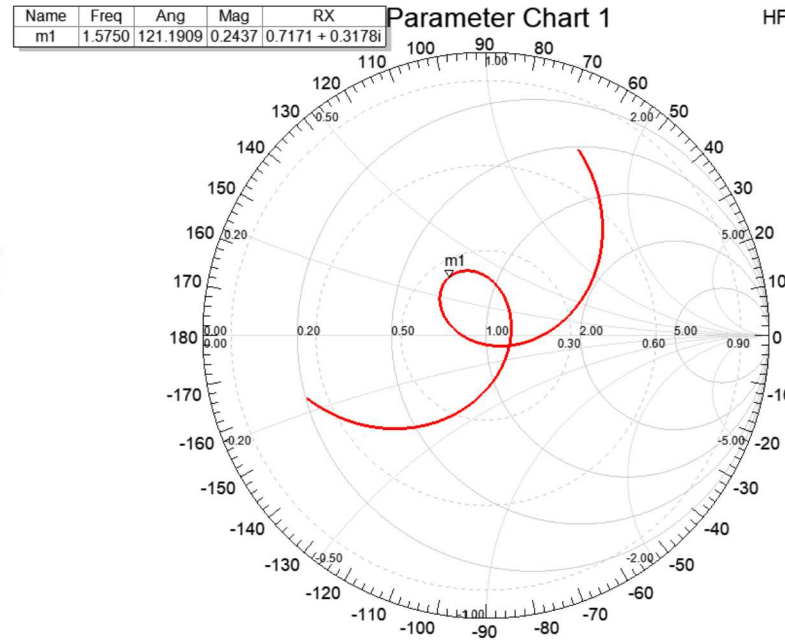




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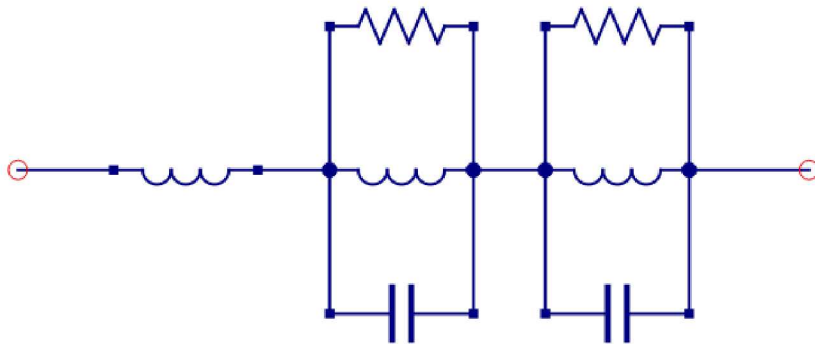
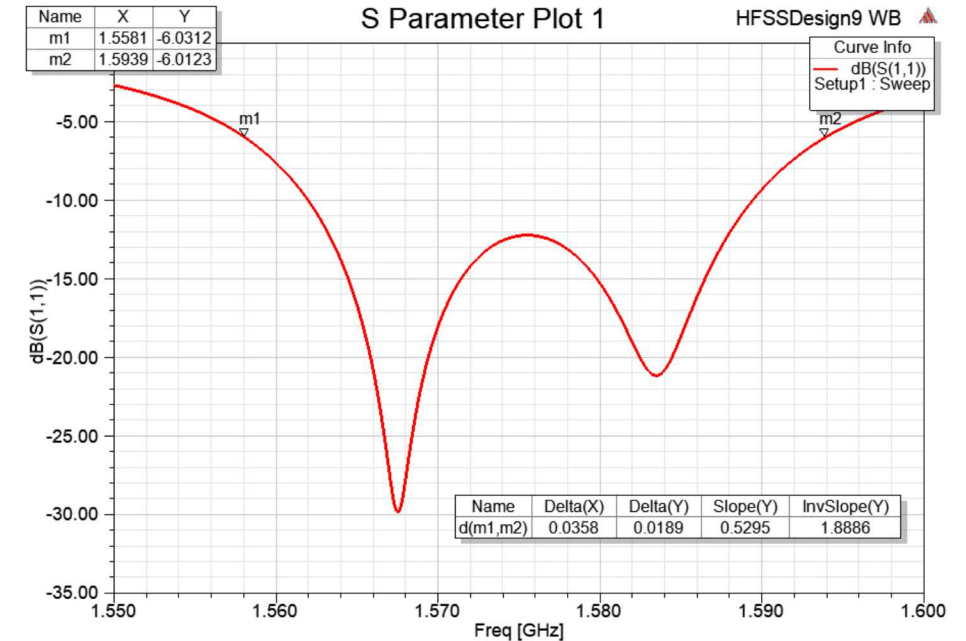
Patch antenna: impedance bandwidth and multi-moding

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$



HFSSDesign9 WB

Curve Info
— S(1,1)
Setup1: Sweep



$$Y \sim G(1 + j2Q \Delta\omega/\omega_0)$$

Multi-mode patches

Stacked patches

Coplanar parasitic patches

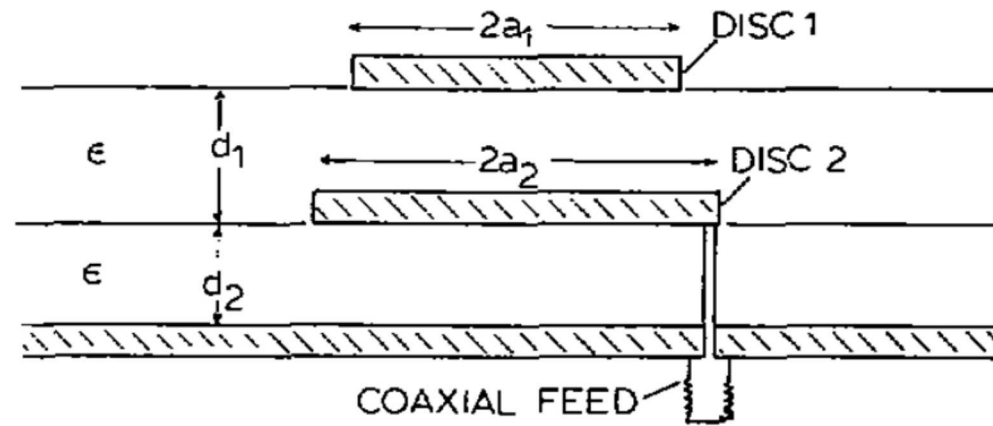
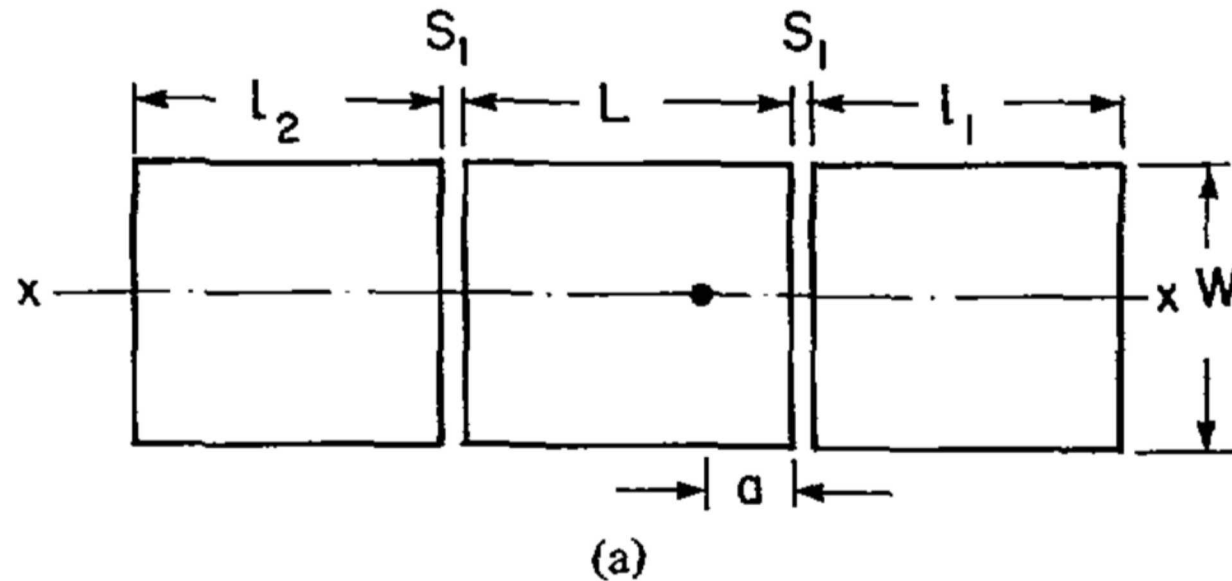


Fig. 1. Stacked circular-disc antenna structure.



10 U-slot patches historically

Huynh and Lee, 1995

BW about 30%

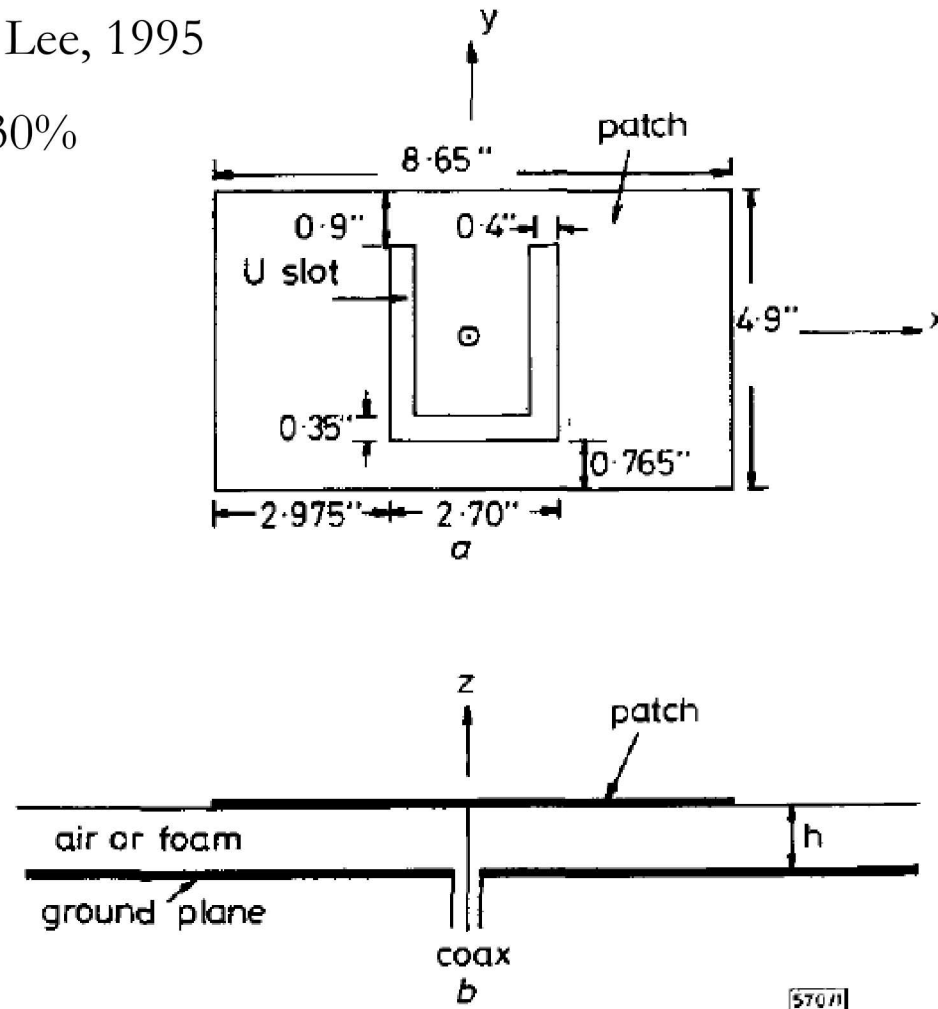


Fig. 1 Geometry of coaxially-fed rectangular patch with U shaped slot

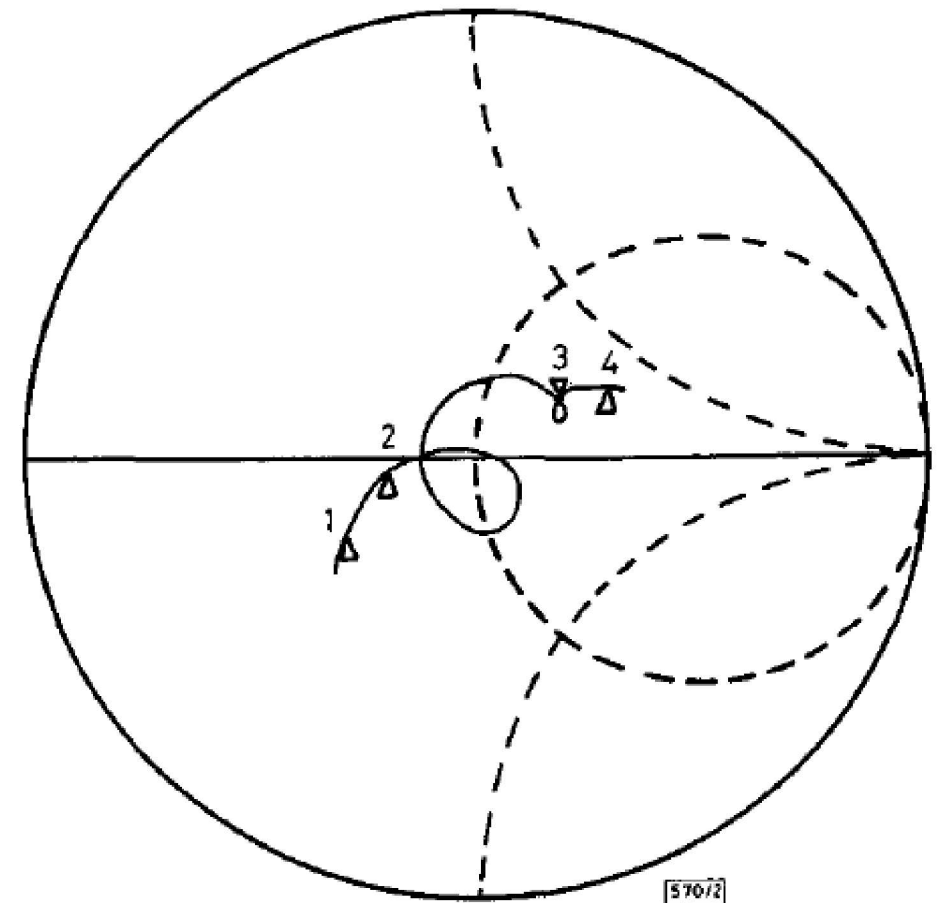
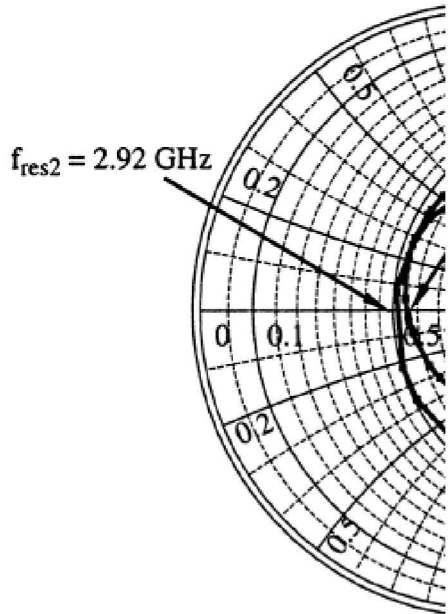


Fig. 2 Measured impedance loci for h = 1.06" (≈0.08λ at 900 MHz)



ϵ_r	
1.0	8
2.33	4
4.0	3
9.8	2
2.33	5

Table 10.7. Design parameters for 2 GHz U-slot patches. (All dimensions in mm.)

ϵ_r	W	L	W_s	L_s	b	$c_x = c_y$	F	h	d_p	Bandwidth
2.33	55.85	40.36	21.71	27.92	6.21	3.11	20.18	12.43	1.53	27.13%
4.0	41.84	30.22	16.26	20.94	4.63	2.34	15.13	10.81	0.76	25.18%
9.8	25.85	18.64	10.04	12.92	2.88	1.44	11.12	9.00	0.36	16.07%

IAL PARAMETERS

Offset	+
0	
0	
+	
-	
0	
+	
-	
-	
-	
v	
+	
-	
-	
v	
-	
+	

Table 10.8. Design parameters for 3 GHz U-slot patches. (All dimensions in mm.)

ϵ_r	W	L	W_s	L_s	b	$c_x = c_y$	F	h	d_p	Bandwidth
2.33	37.23	26.90	14.47	18.61	4.14	2.07	13.45	13.45	1.02	27.13%
4.0	27.89	20.15	10.84	13.96	3.09	1.56	9.06	8.2	0.51	20.77%
9.8	17.23	12.43	6.69	8.61	1.92	0.96	7.34	6.00	0.12	15.95%

Table 10.9. Design parameters for 4 GHz U-slot patches. (All dimensions in mm.)

ϵ_r	W	L	W_s	L_s	b	$c_x = c_y$	F	h	d_p	Bandwidth
2.33	27.93	20.18	3.11	13.96	3.11	1.55	10.09	6.21	0.76	26%
4.0	20.92	15.11	8.13	10.47	2.31	1.17	6.79	5.5	0.38	24.4%
9.8	12.92	9.32	5.02	6.46	1.44	0.72	5.56	4.5	0.09	15.77%

S. Weigand, G. H. Huff, K. H. Pan and J. T. Bernhard, "Analysis and design of broad-band single-layer rectangular U-slot microstrip patch antennas," in IEEE TAP, vol. 51, no. 3, March 2003.

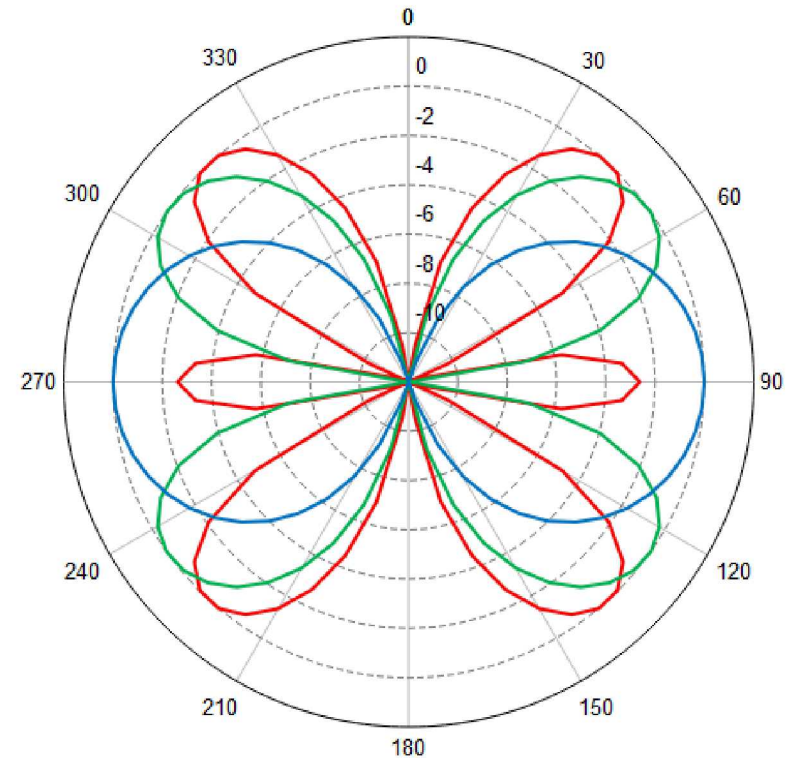
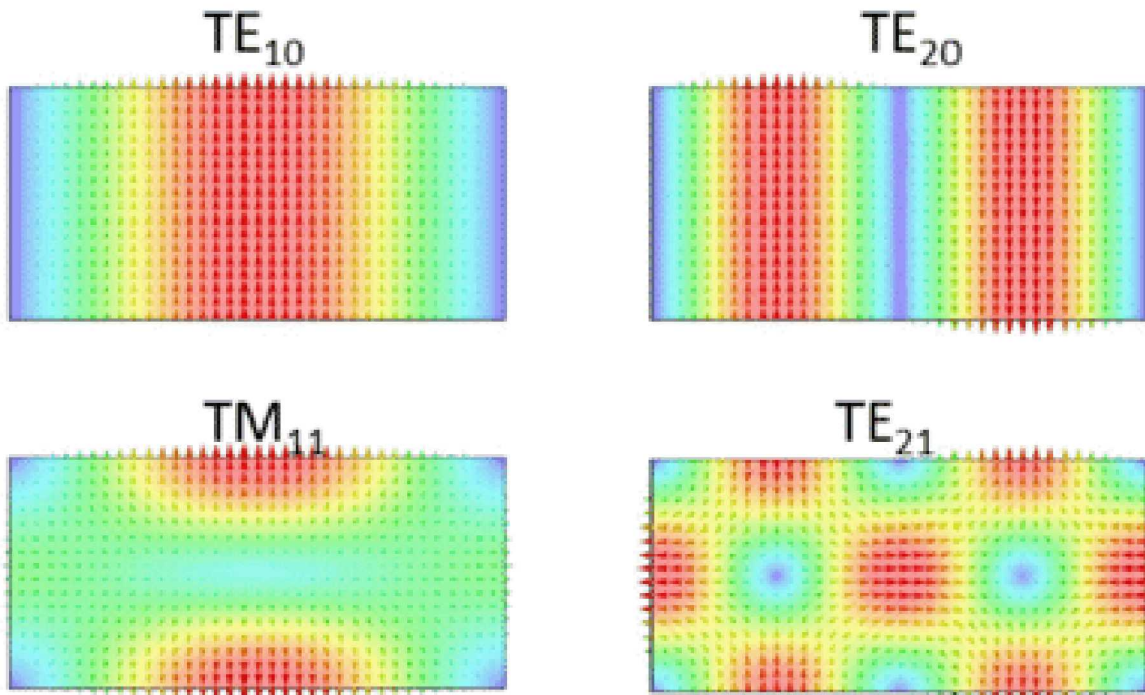
V. Natarajan and D. Chatterjee, "An Empirical Approach for Design of Wideband, Probe-Fed, U-Slot Microstrip Patch Antennas on Single-layer, Infinite, Grounded Substrates," ACES Journal, vol. 18, no. 3, Nov 2003.

K.F. Lee, K. M. Luk and H. W. Lai, "Broadbanding Techniques II --- The U-slot Patch Antenna" in Microstrip patch antennas, 2nd ed., Singapore: World Scientific, 2018, ch. 10.

Intro to Characteristic Mode Analysis (CMA)

Characteristic modes are sets of currents/fields on a structure that satisfy the boundary conditions...

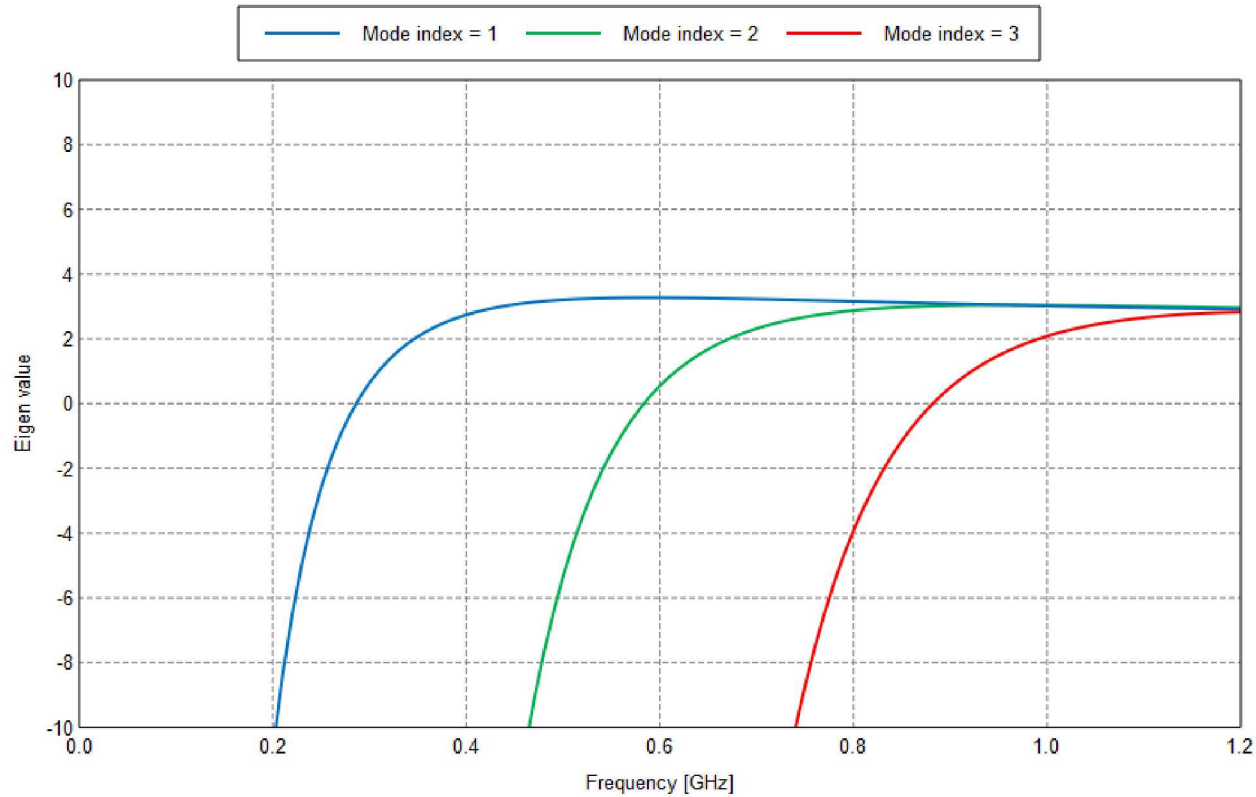
Similar in concept to waveguide modes, but are suited to radiation/scattering problems



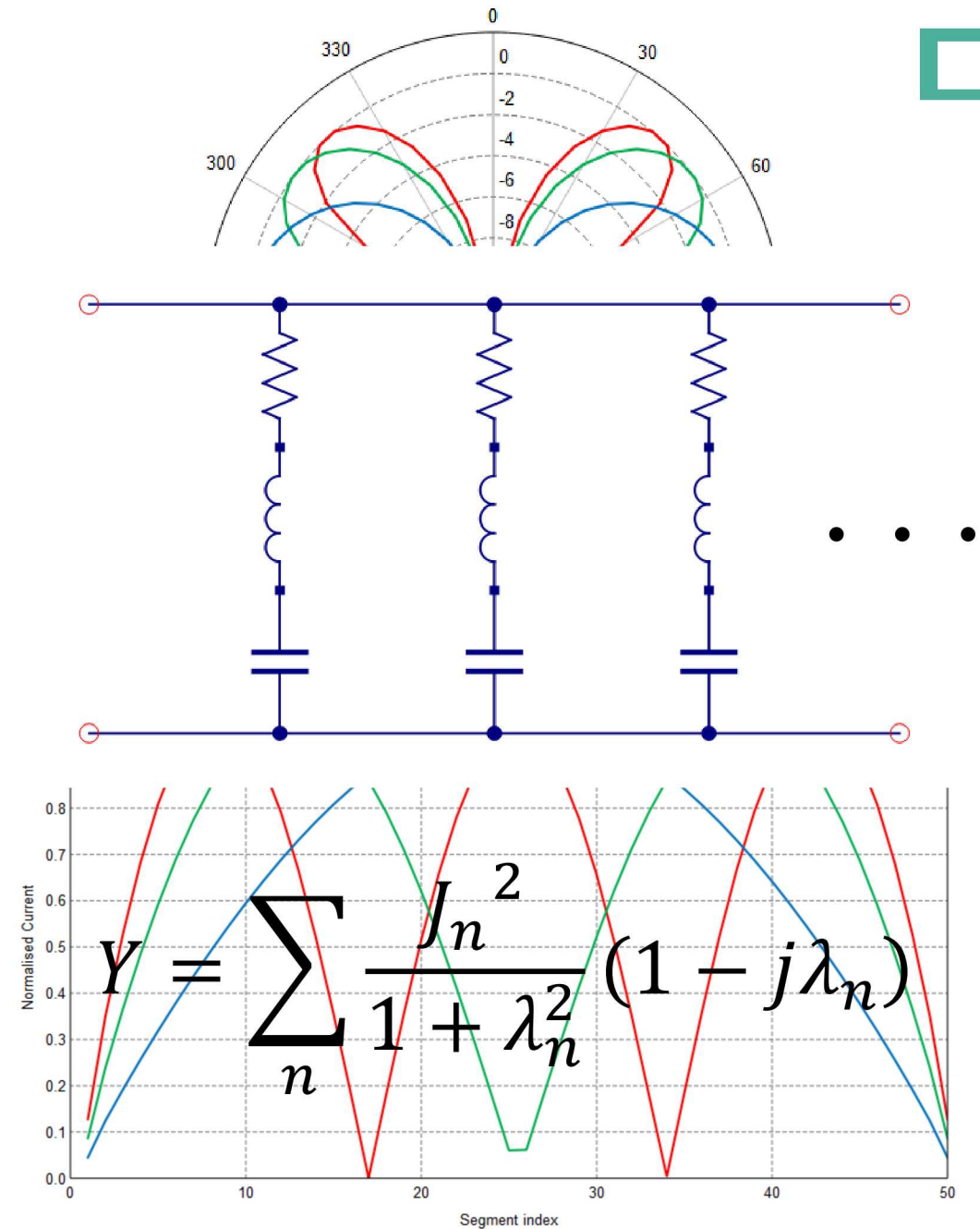
$$\nabla_t^2 e + \beta^2 e = 0$$

$$[X] J_n = \lambda_n [R] J_n$$

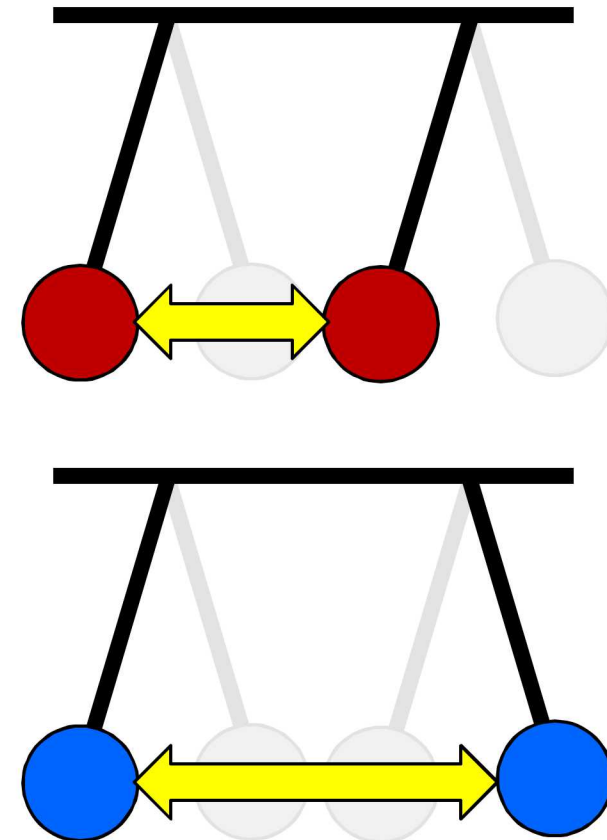
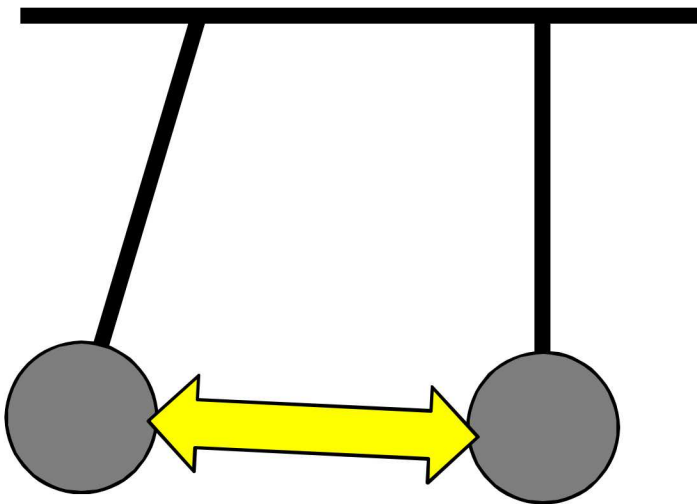
CMA example: 0.5 meter wire dipole



$$\omega (W_m - W_e) = \lambda_n$$



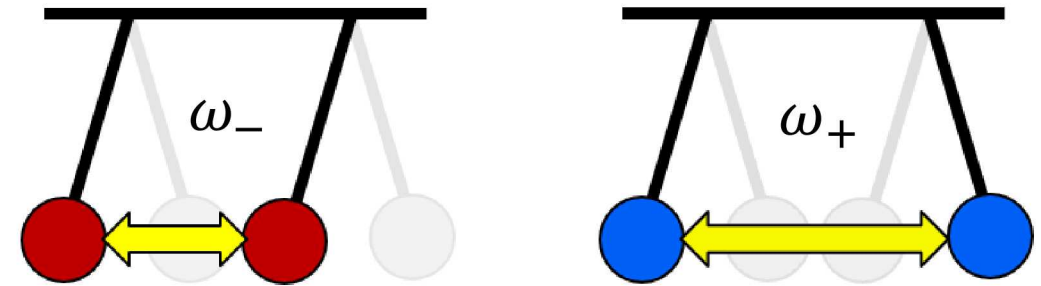
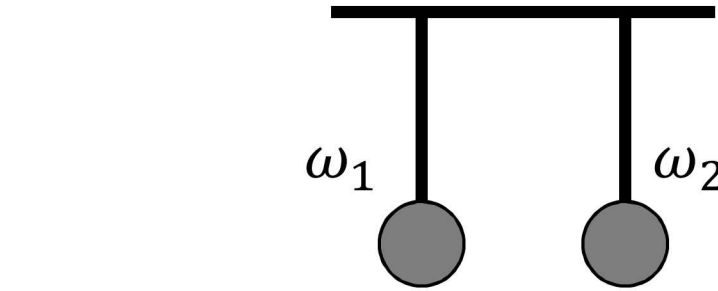
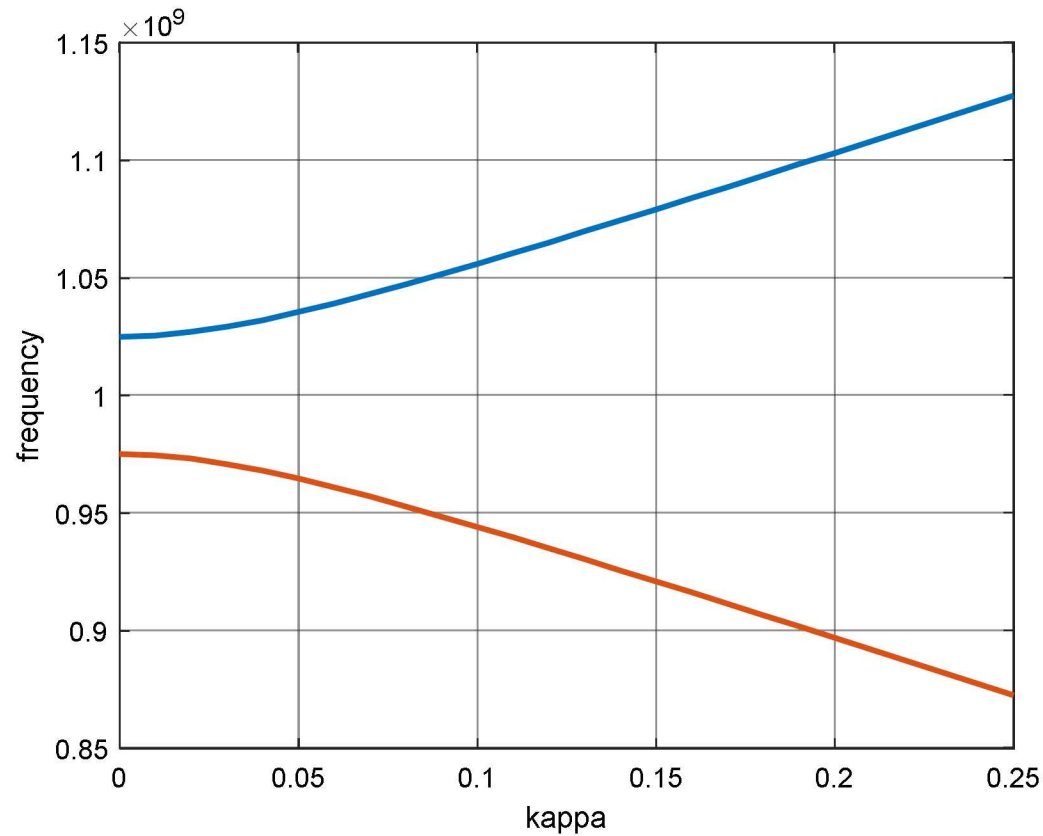
CMT analyses the motion of a system of two coupled resonators as the combination of in-phase and anti-phase modes of motion





<https://www.youtube.com/watch?v=gbJYK7q5ejY>

Coupled mode frequency splitting

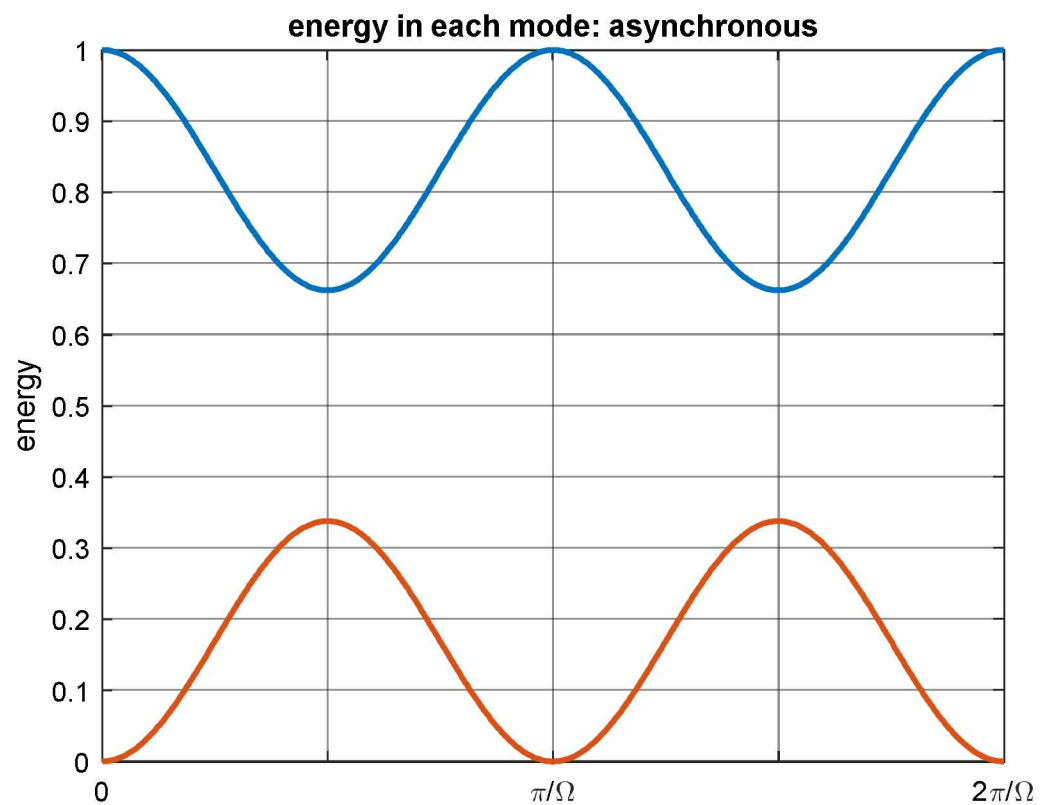


$$\omega_{\pm} = \left(\frac{\omega_2 + \omega_1}{2} \right) \pm \sqrt{\left(\frac{\omega_2 - \omega_1}{2} \right)^2 + |K|^2}$$

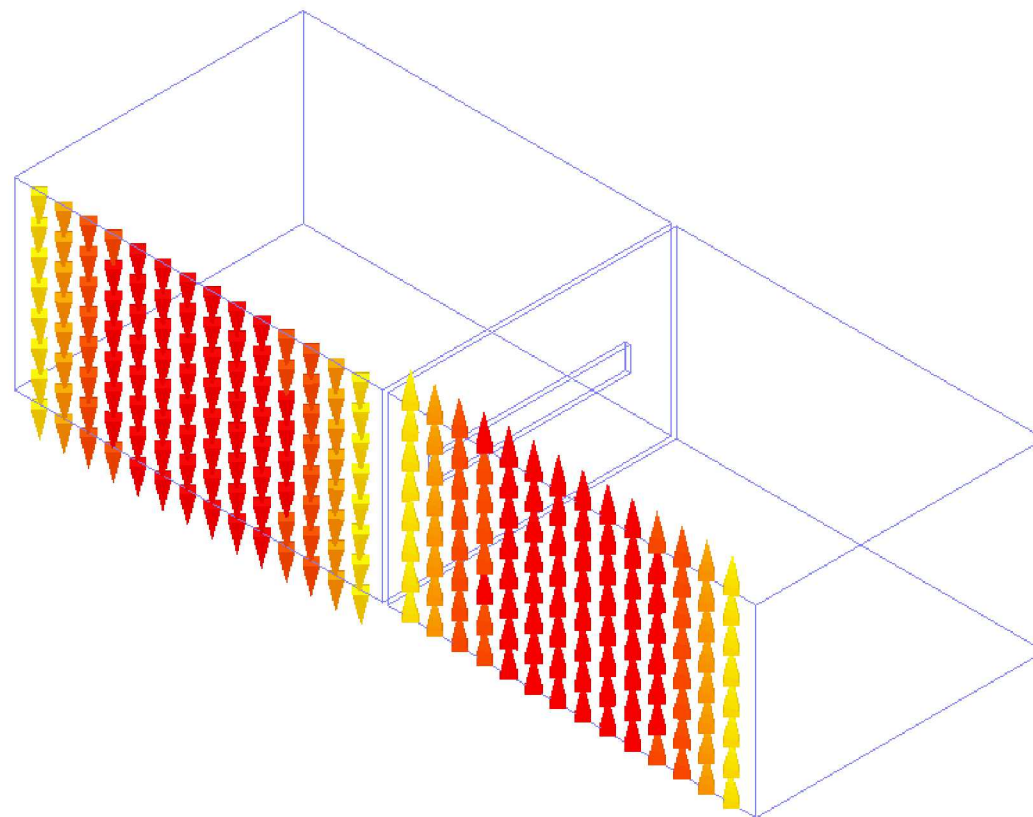
$$\kappa = \frac{\omega_+^2 - \omega_-^2}{\omega_+^2 + \omega_-^2}$$

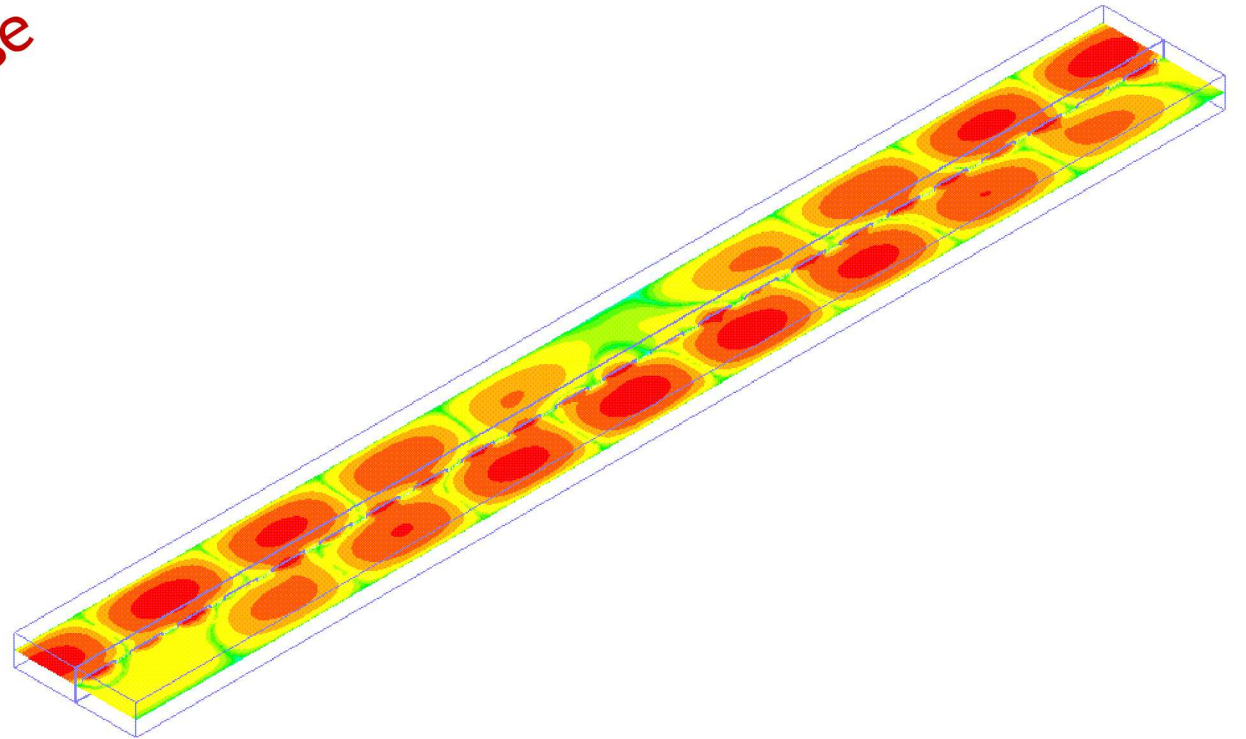
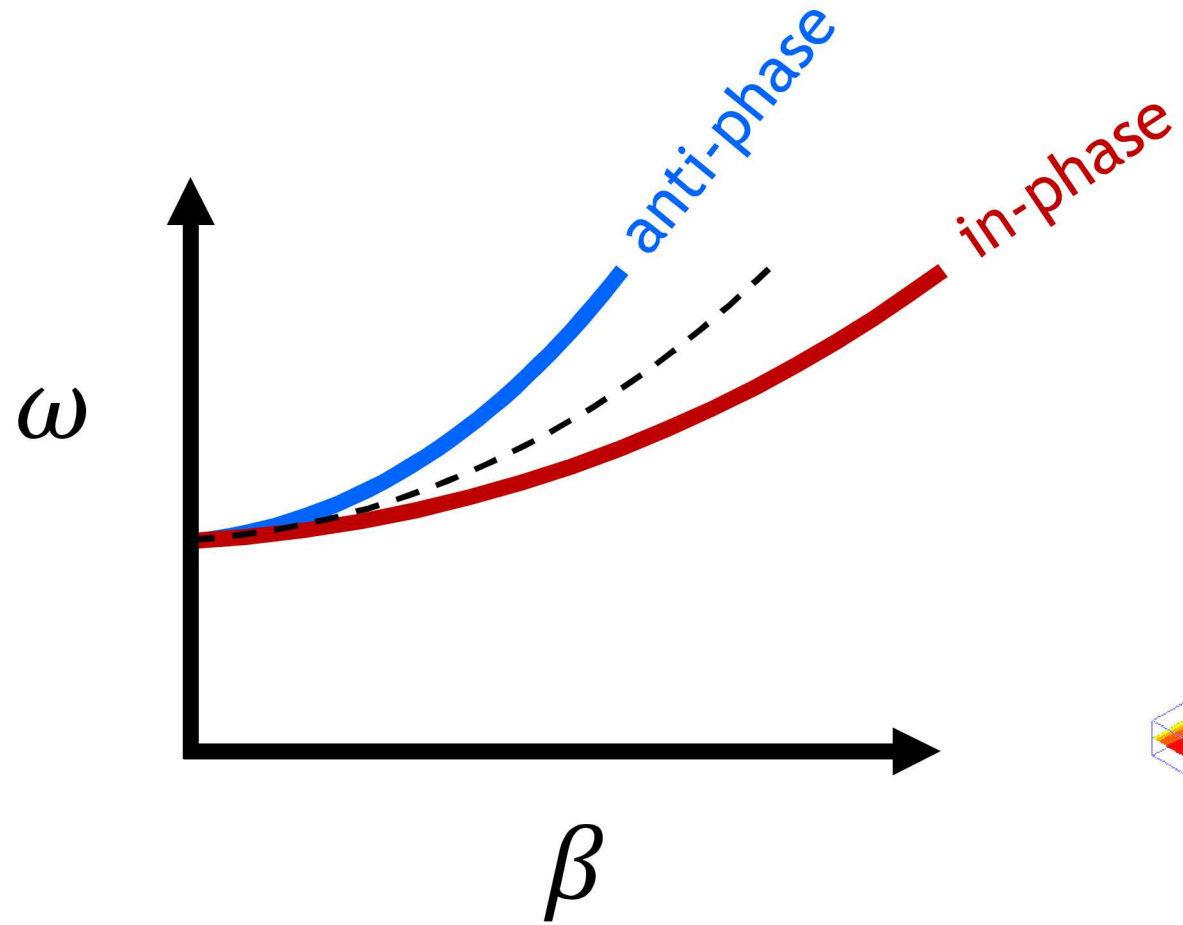
$$\kappa \sim \omega_0 K / 2$$

Coupled mode energy exchange

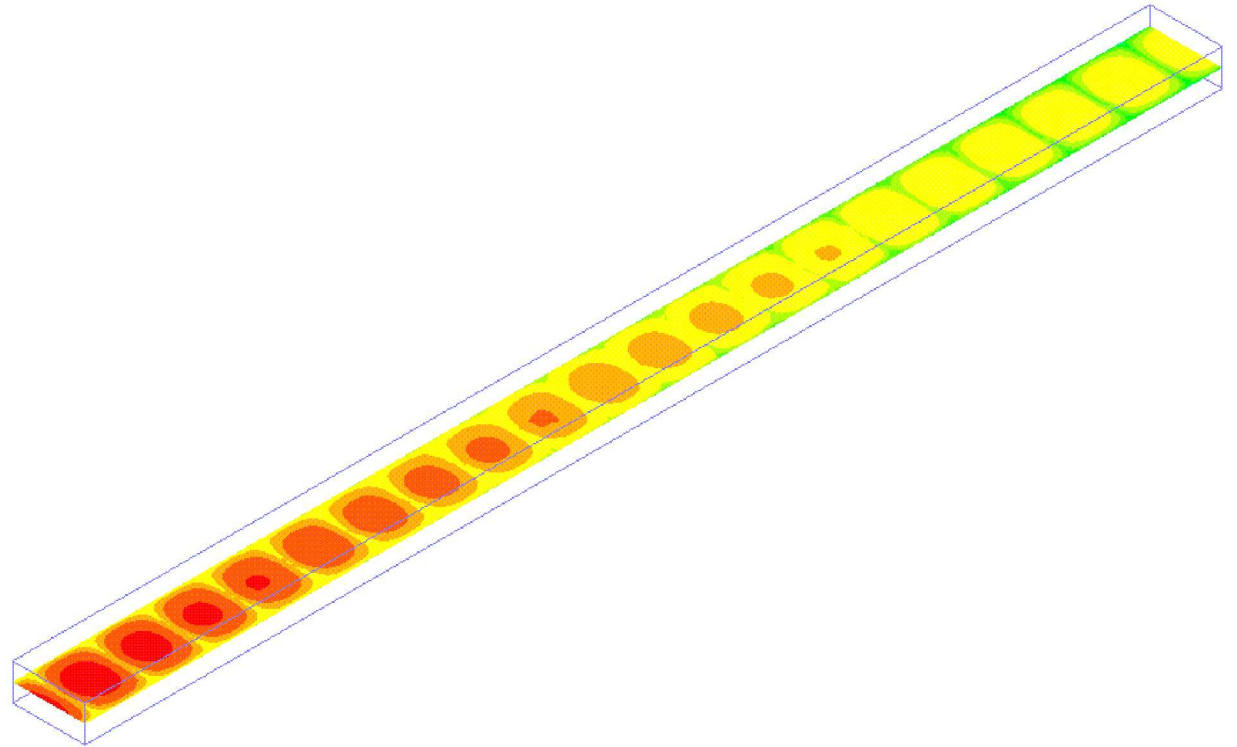
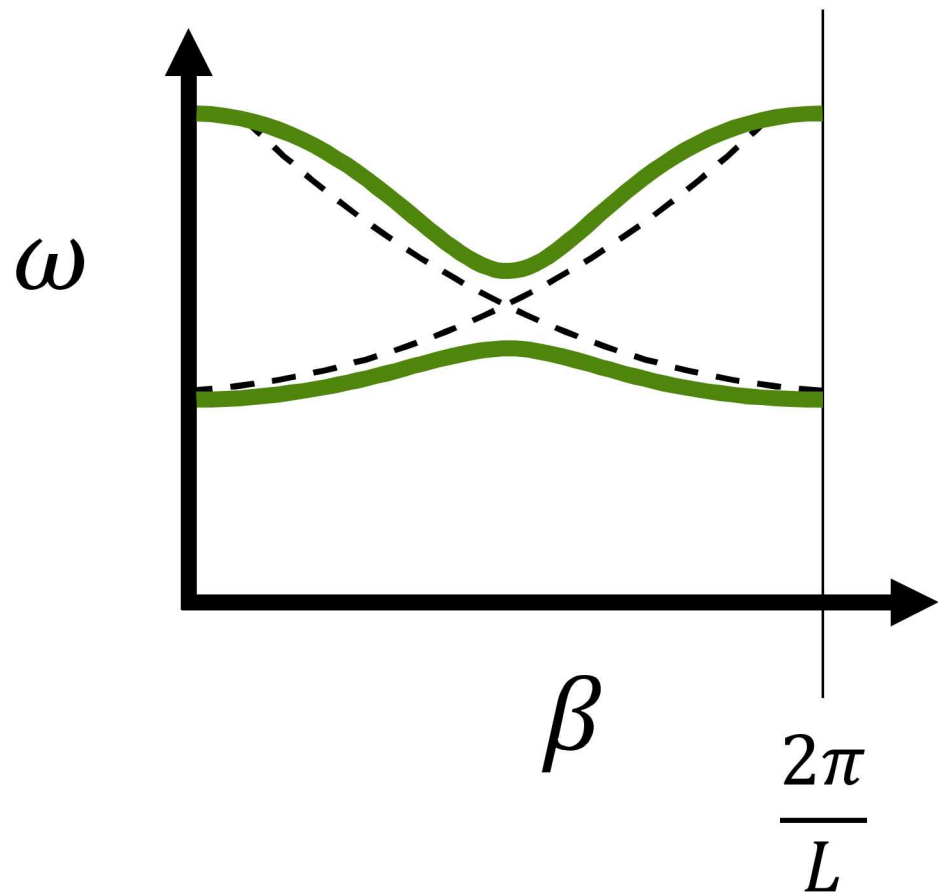


time $\longrightarrow$
space $\longrightarrow$

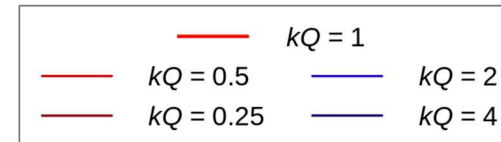
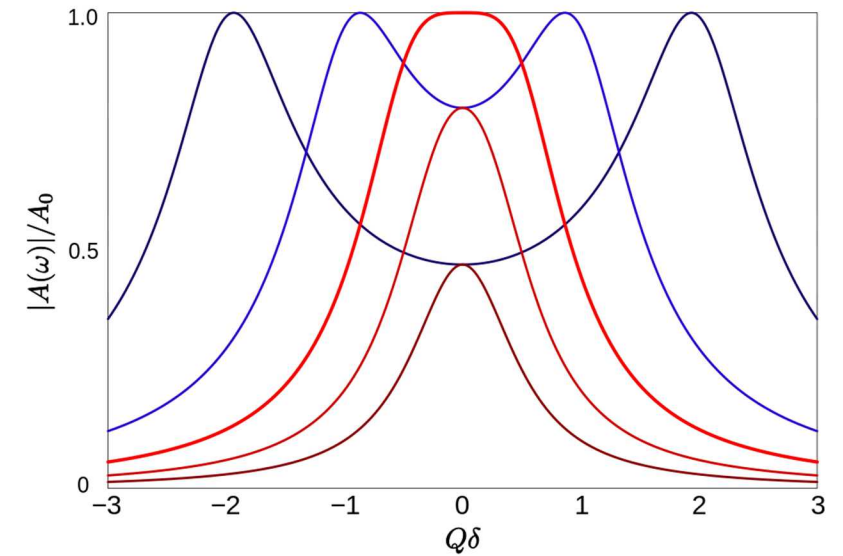
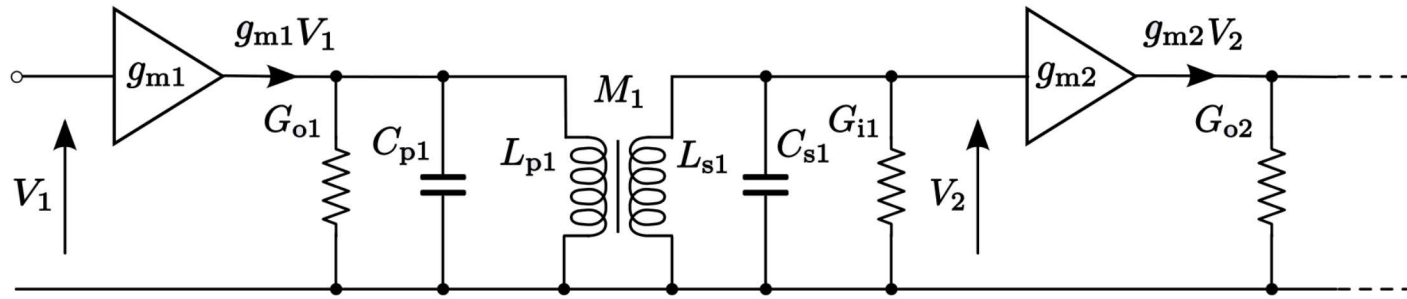




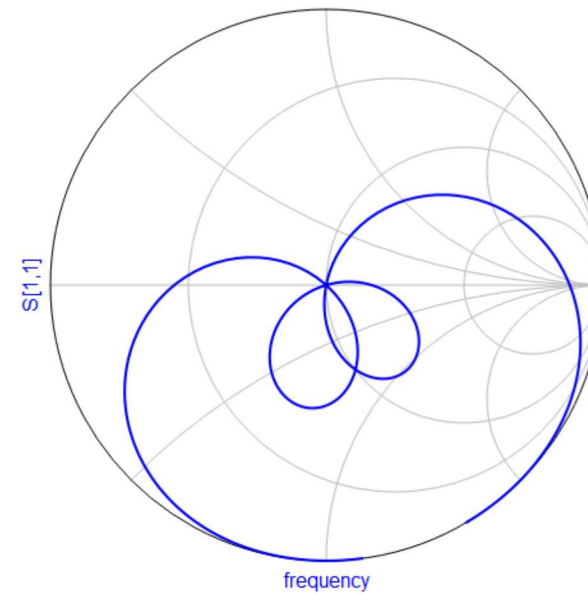
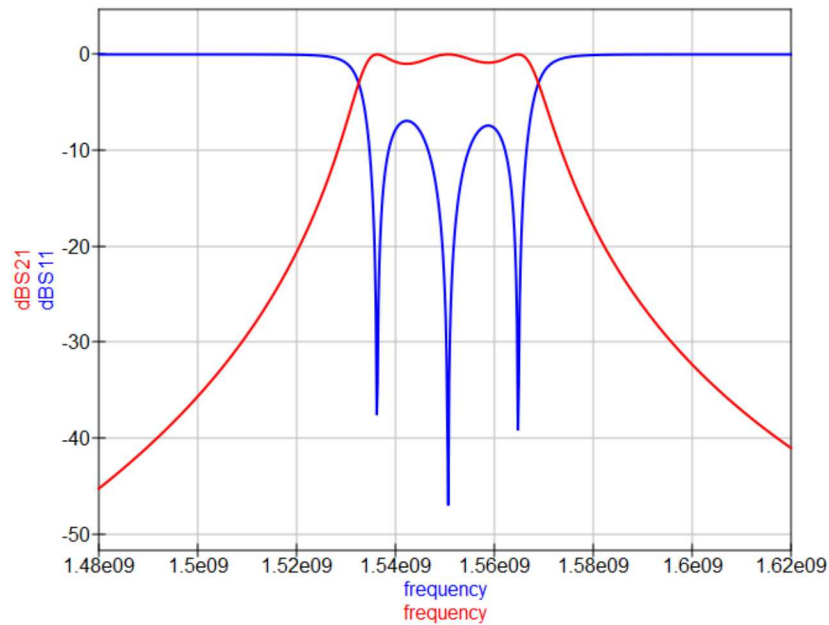
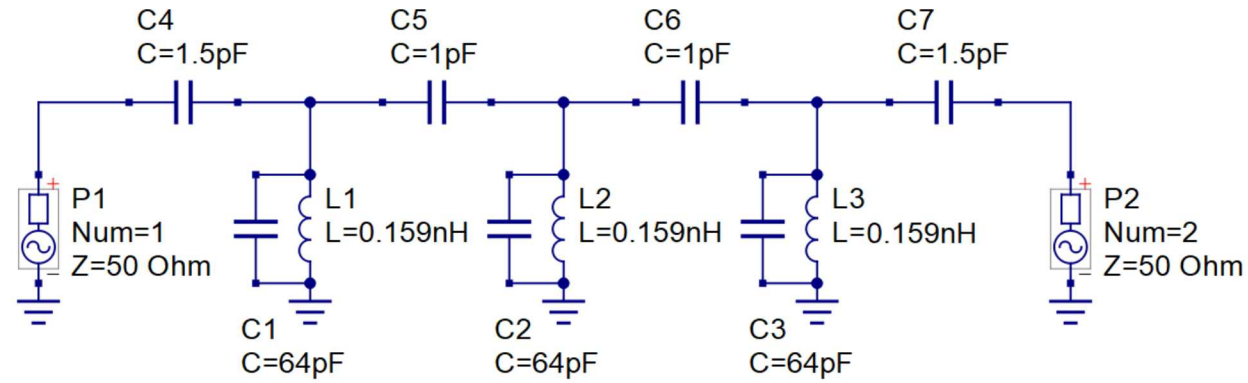
Coupling contra-directional modes in space



Coupled modes: time coupling in the frequency domain



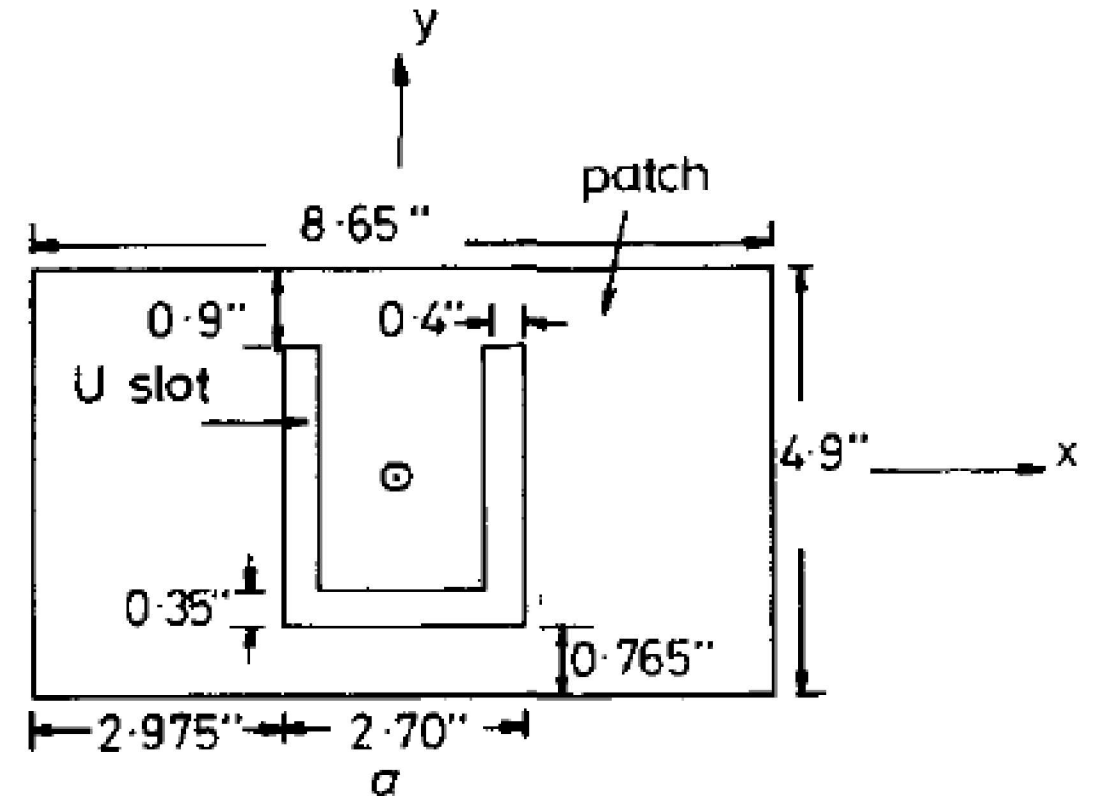
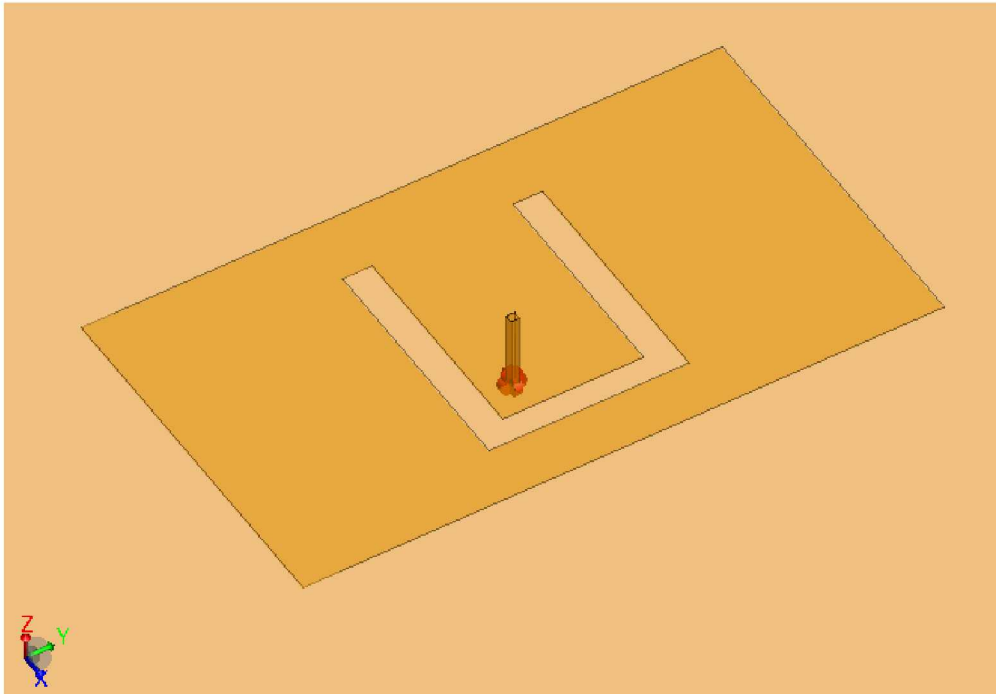
Coupled modes: time coupling in the frequency domain



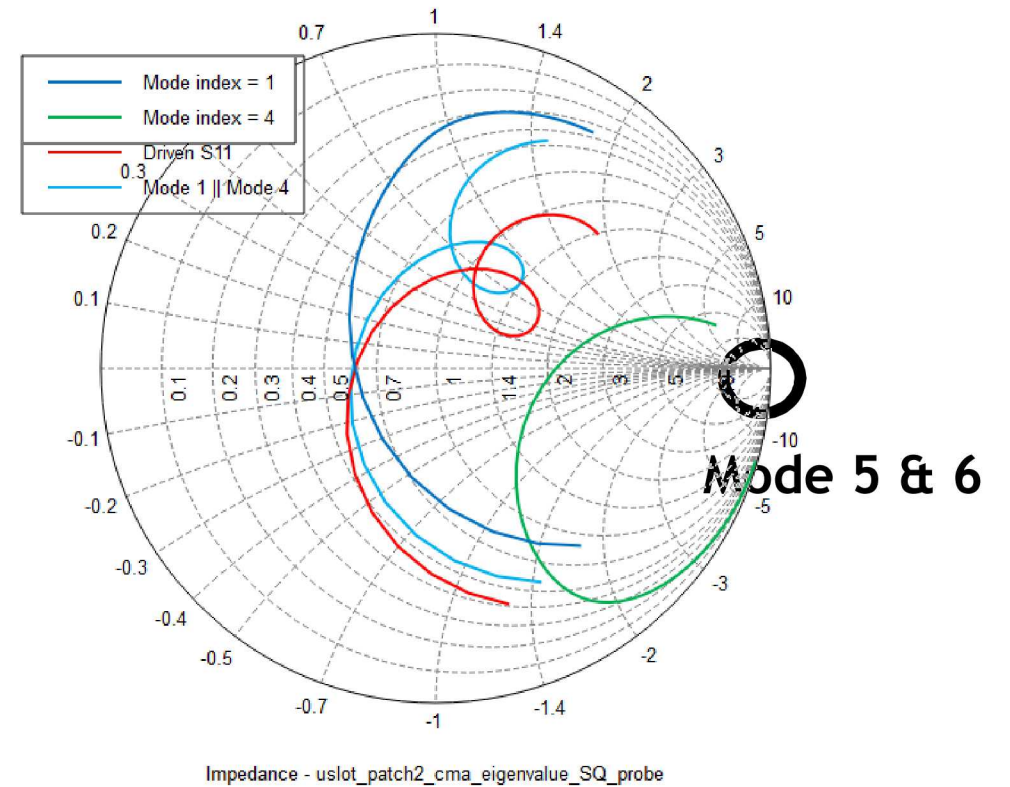
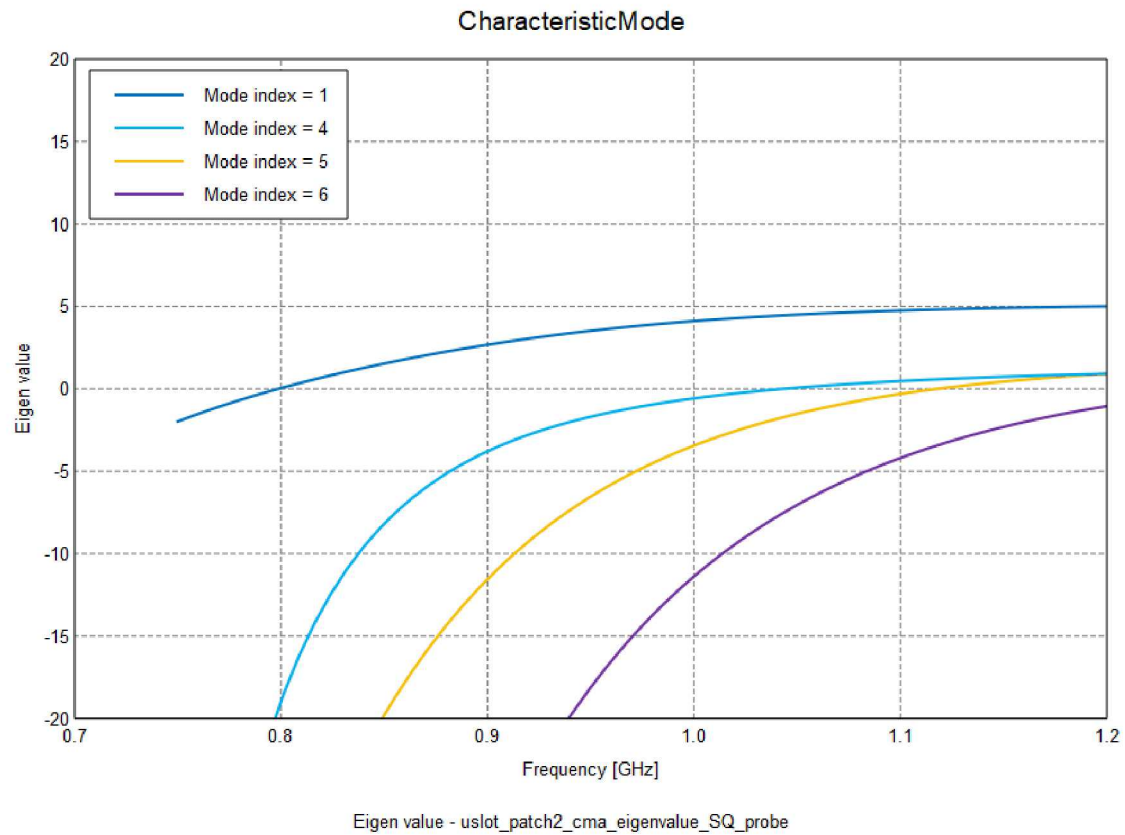
22 CMA of the U-slot patch

Using Feko (commercial MoM code)

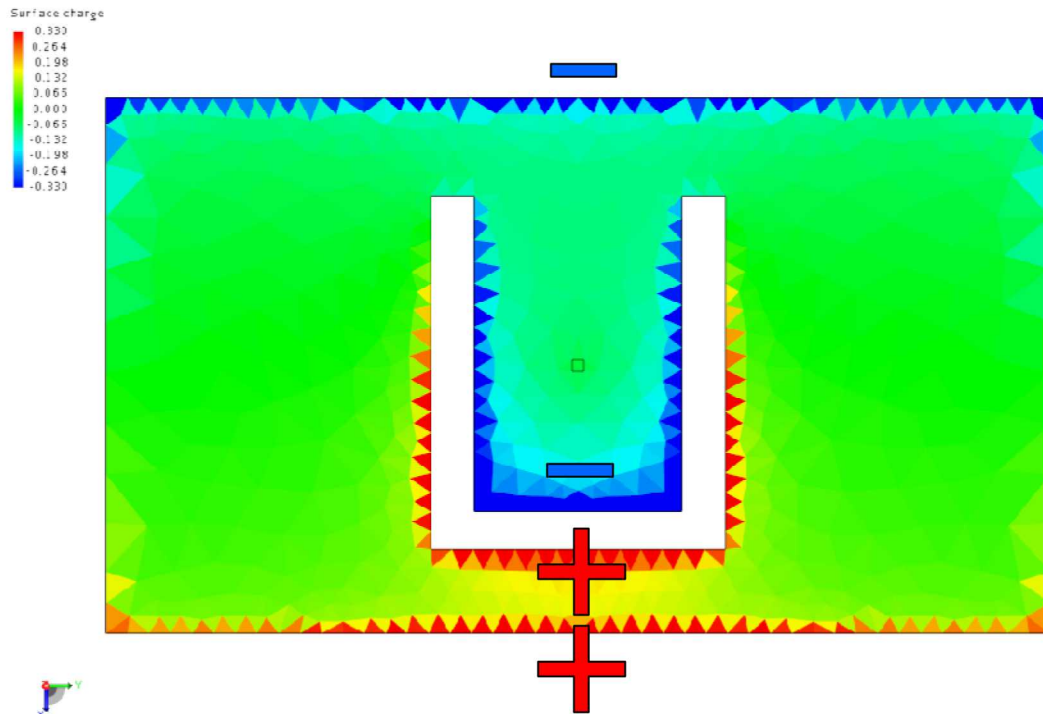
Model the Huynh & Lee geometry but model round probe as cuboid rather than cylinder



Which modes?

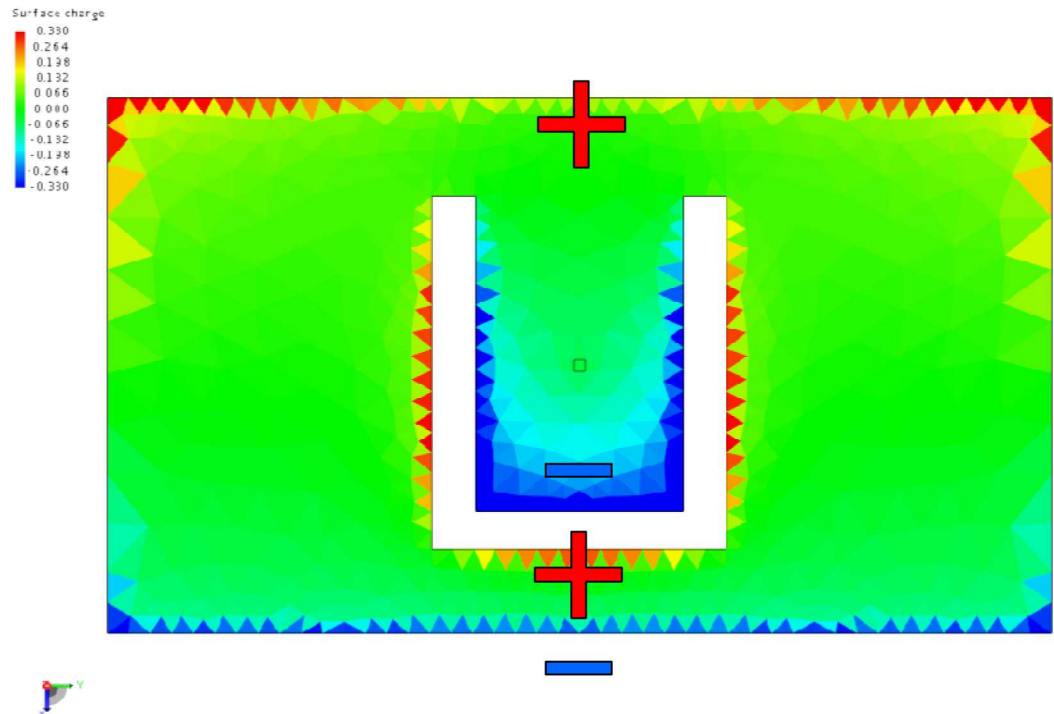


Mode 1



in-phase

Mode 4

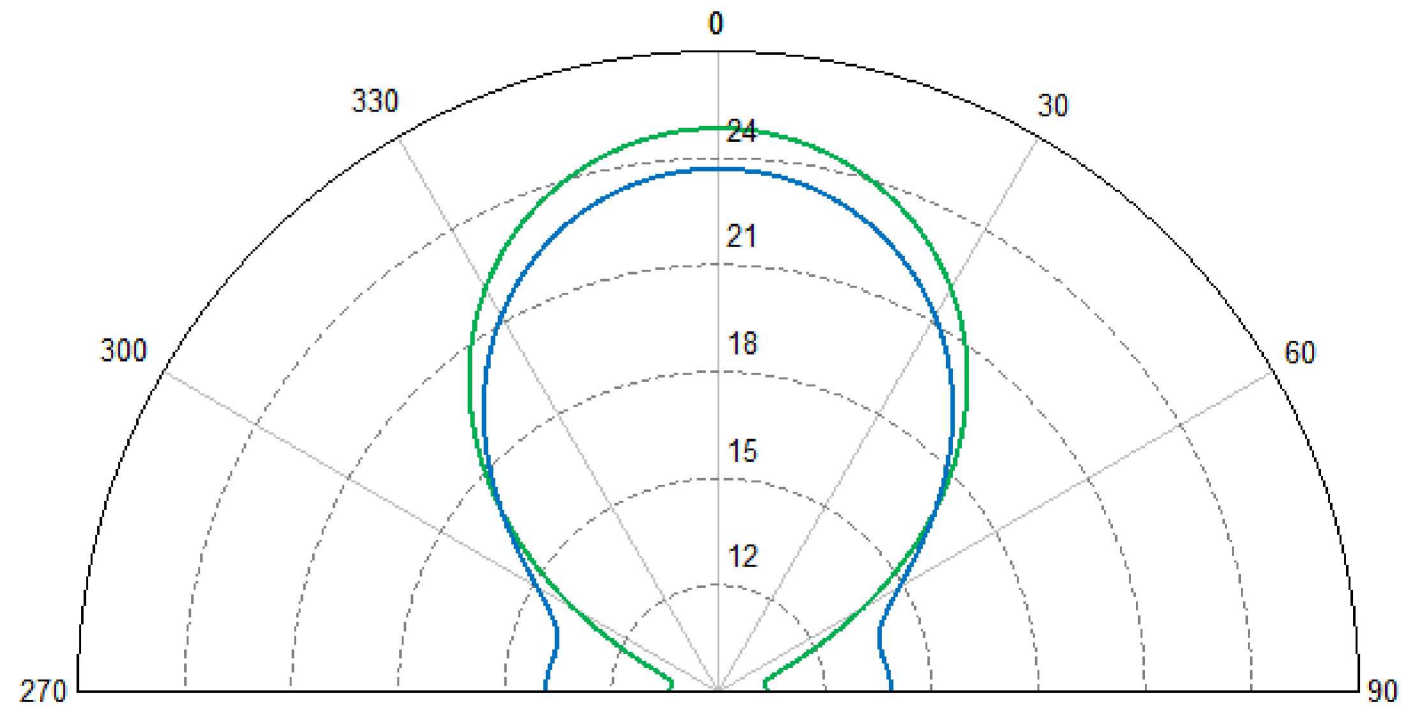


anti-phase

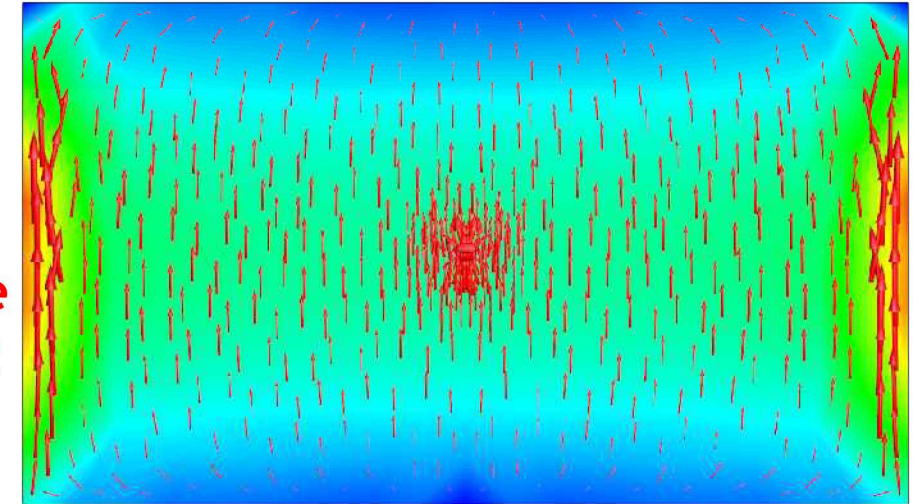
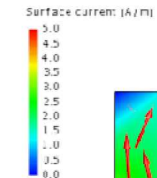
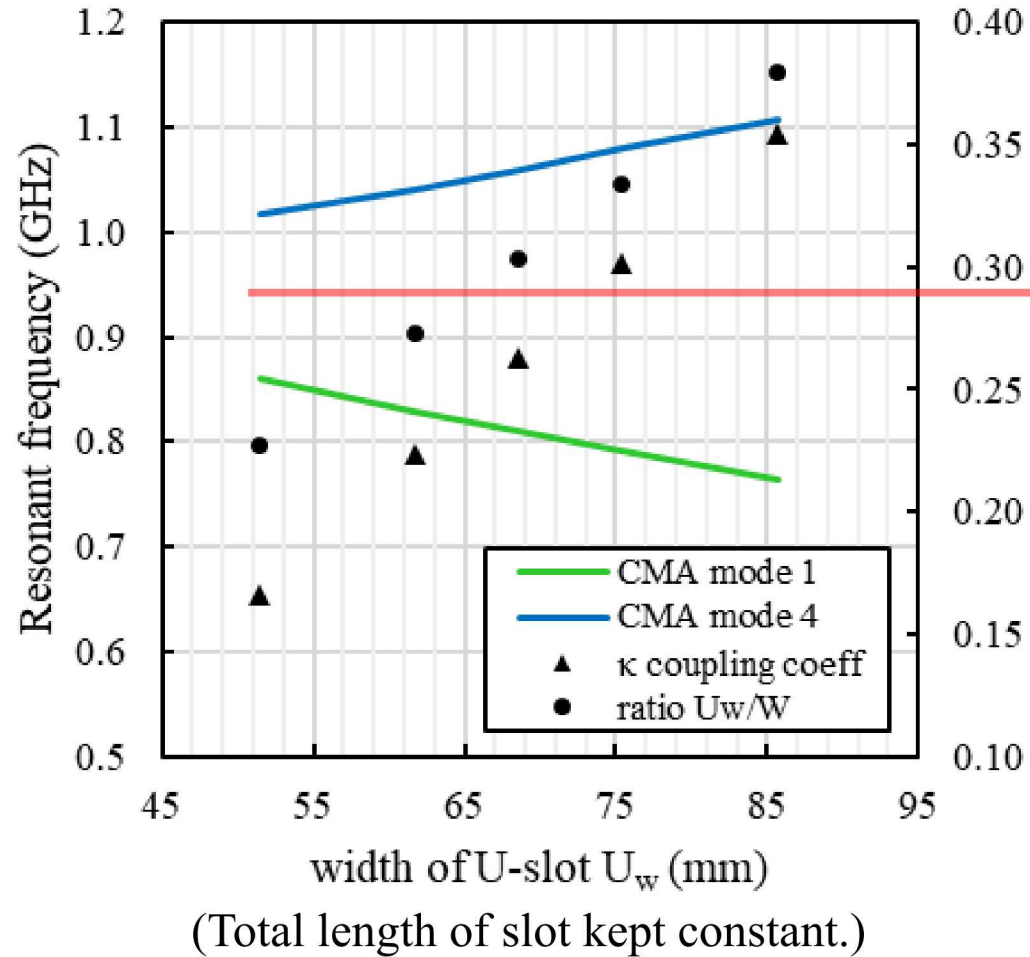
More about the modes

Similar broadside radiation patterns, co-polarized

Radiation from slot is likely relatively small

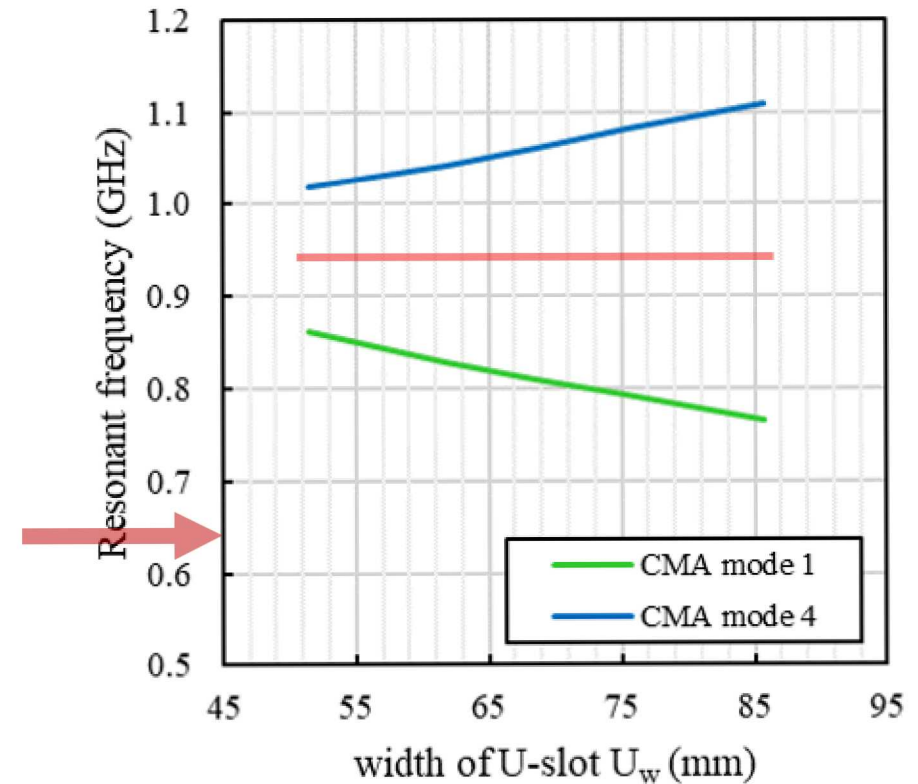
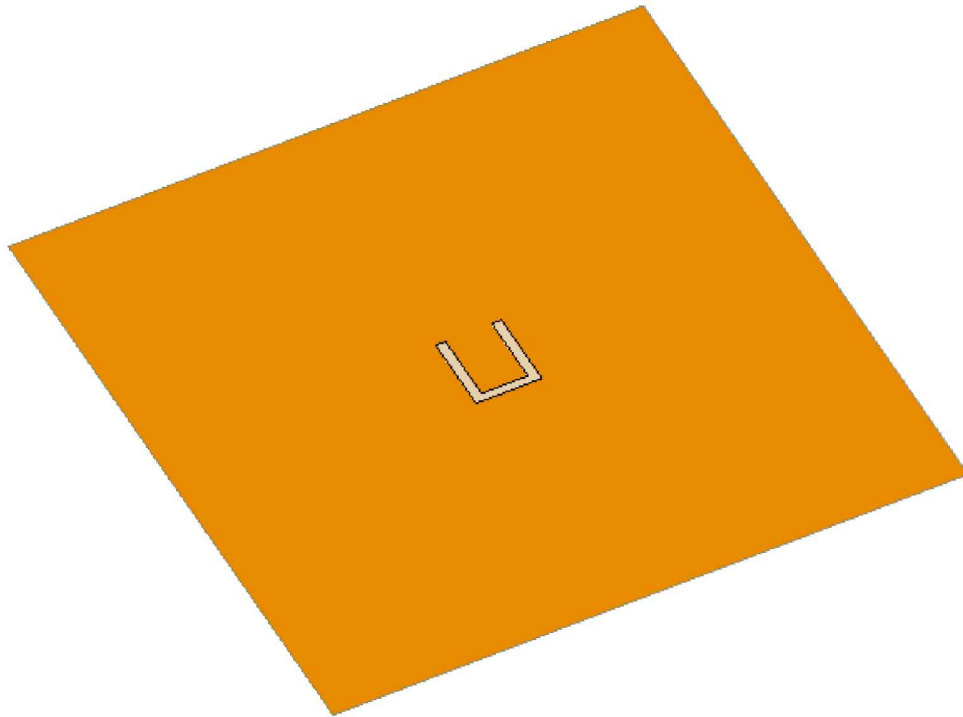


Are they really coupled modes?



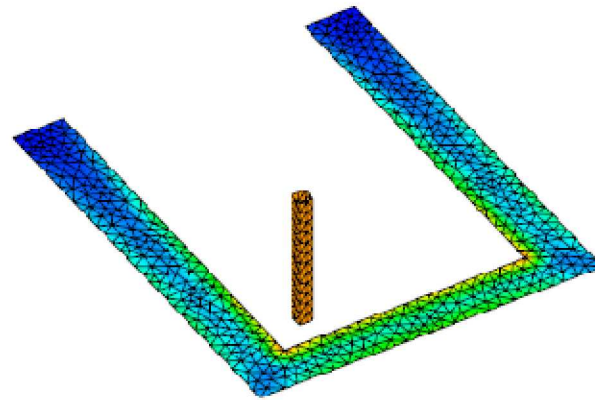
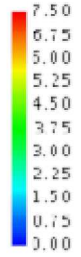
If it's synchronous coupling, then what is the other resonator?

Total length of slot is $\sim 9''$ (23cm); gives CM resonance at $\sim 640\text{MHz}$ (where slot is $\sim \lambda/2$)...



Uncoupled slot resonator, resonant at ~912MHz

Magnetic current [cV/m]

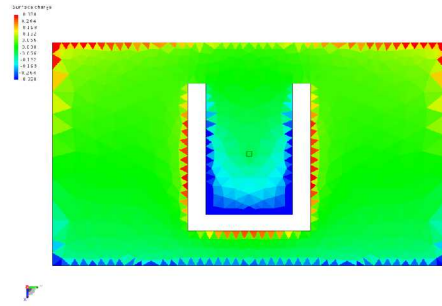
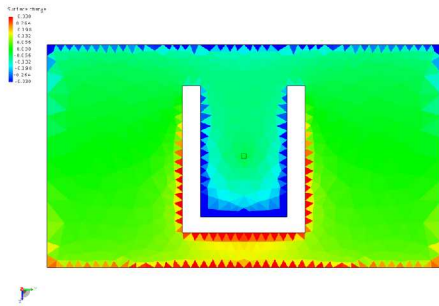
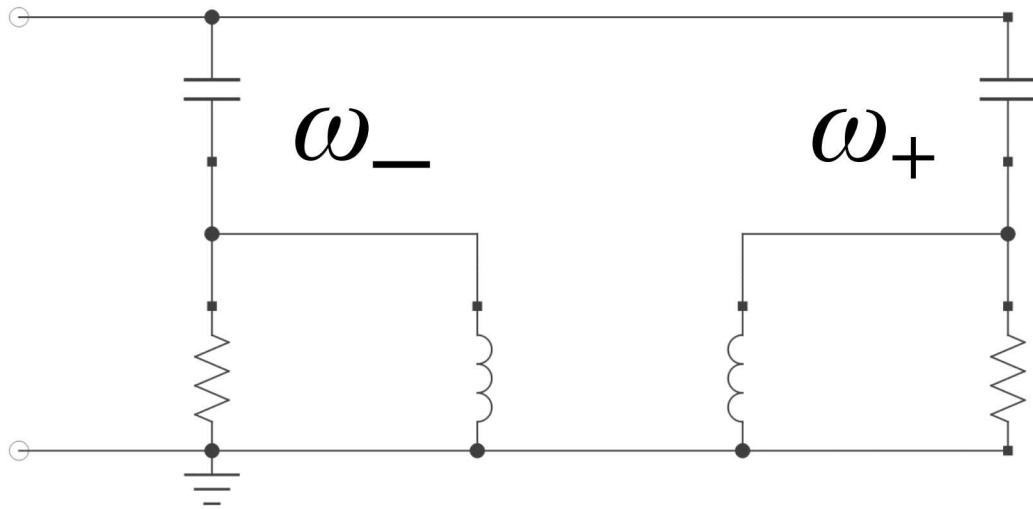


M @ phase = 90



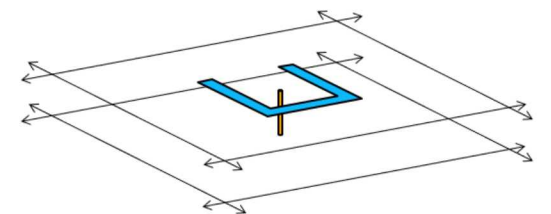
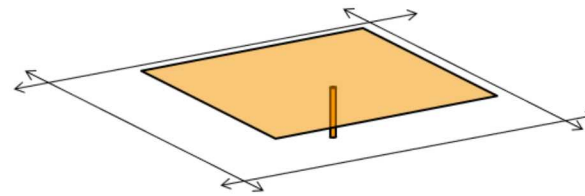
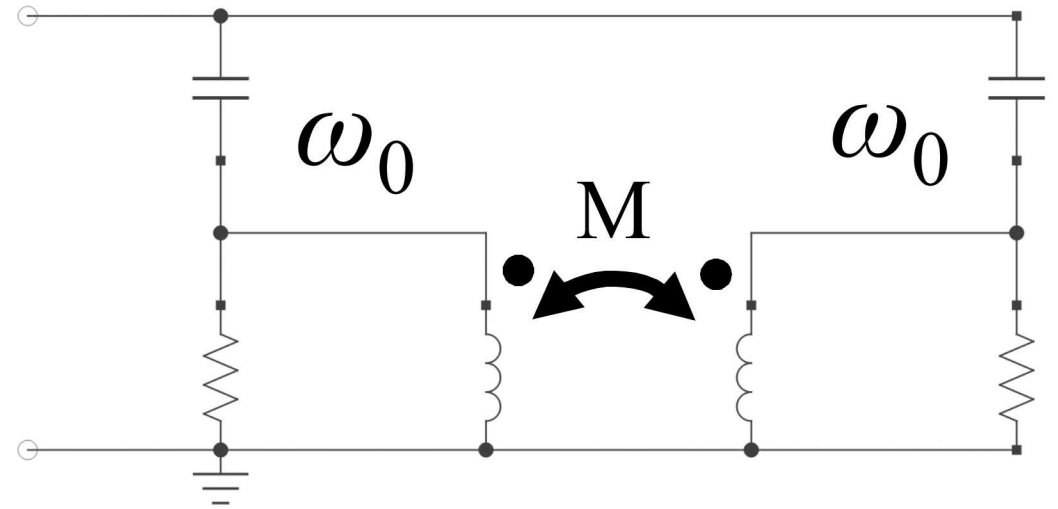
in-phase

anti-phase

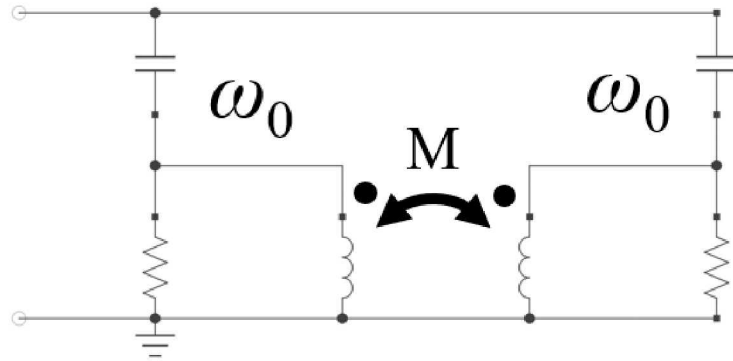


patch

slot



30 Equivalent circuit modeling



$$Y_c = G_0/Q'$$

$$C = Y_c/\omega_0$$

$$R_{hp} = G_0/Y_c^2$$

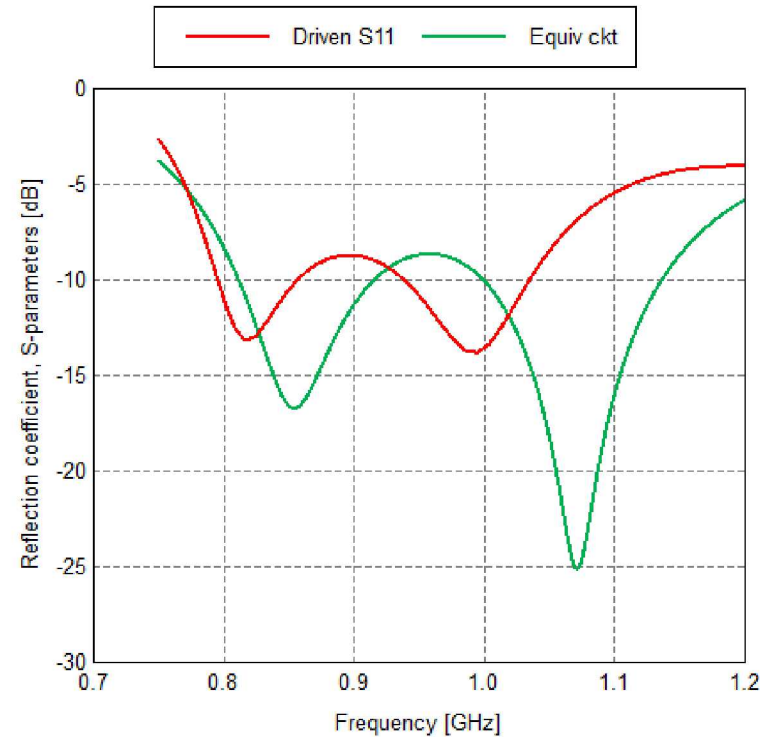
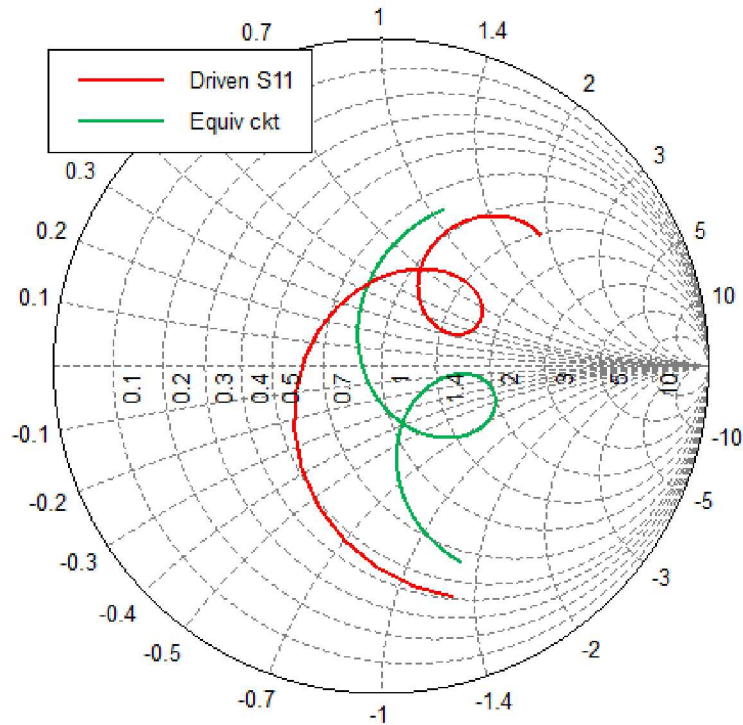
$$L = 1/(Y_c \omega_0)$$

Patch resonator

$\omega_0/2\pi$	946 MHz
G_0	1 μ S
Q	4.5
Q'	6.3
$R_{hp,patch}$	40 M Ω
L_{patch}	1.06 mF
C_{patch}	0.0266 fF

Slot resonator

$\omega_0/2\pi$	912 MHz
G_0	34 mS
Q	8.9
Q'	6.3
$R_{hp,slot}$	1.18 k Ω
L_{slot}	32.5 nH
C_{slot}	0.938 pF



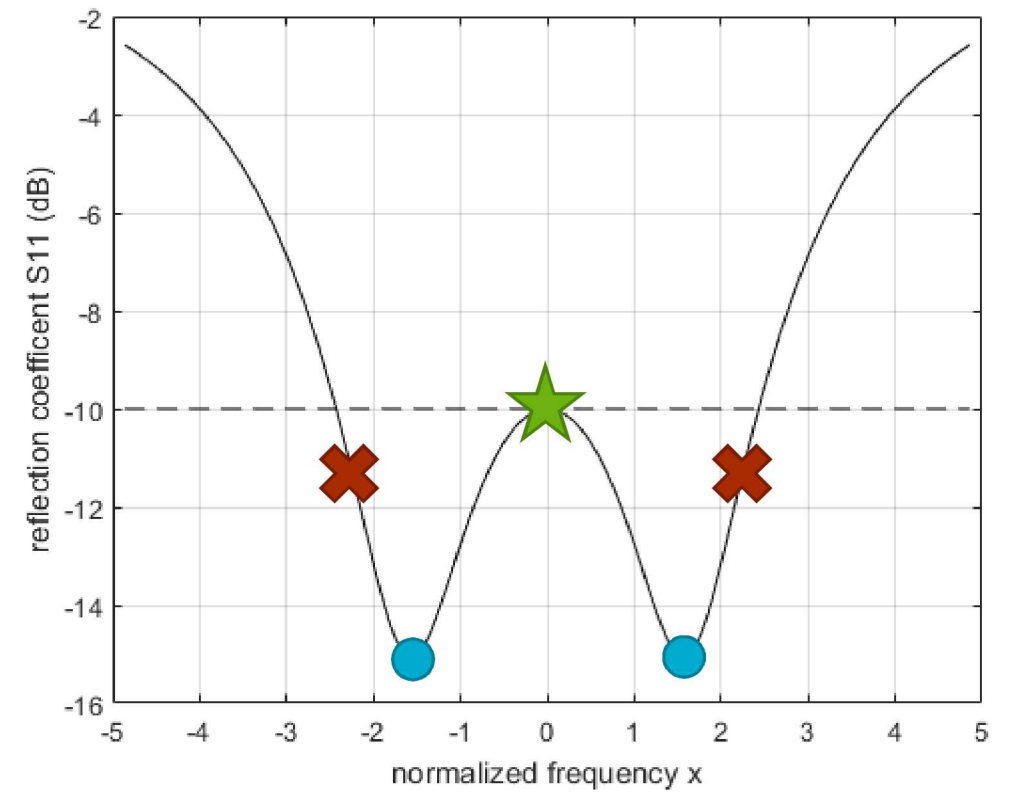
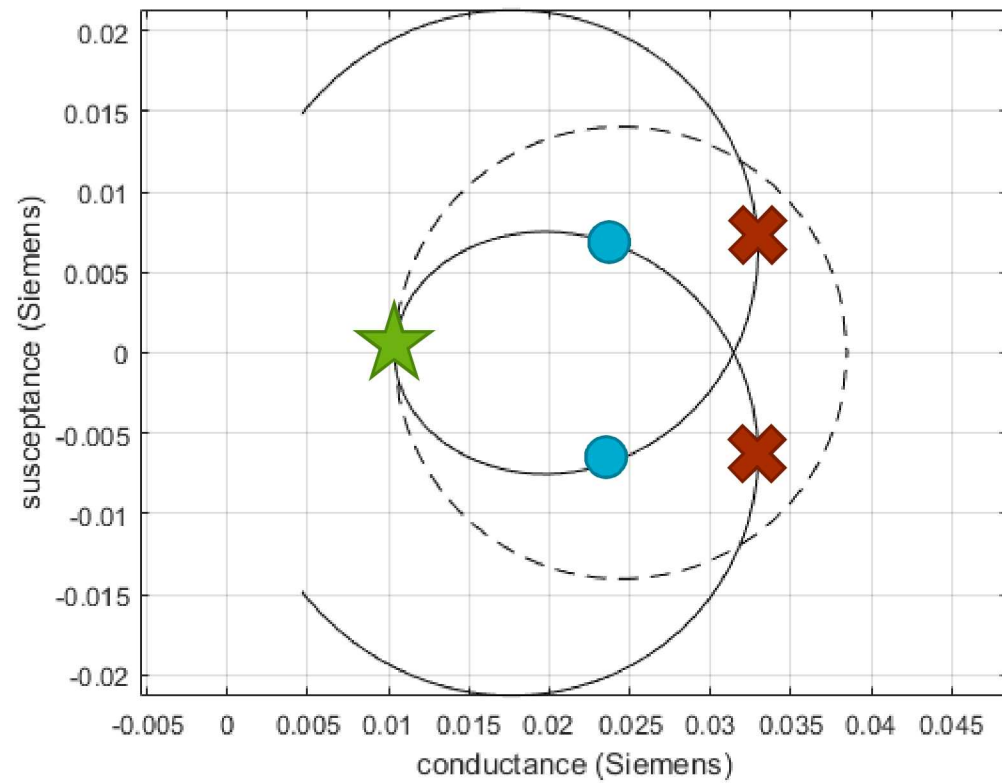
Place resonances

Design uncoupled patch and slot resonators with equal frequency & correct coupling

Combine patch and slot resonators into single structure, simulate & refine

$$\frac{BW}{f_0} \sim \kappa \quad \kappa = \frac{\omega_+^2 - \omega_-^2}{\omega_+^2 + \omega_-^2}$$

Placing resonances



Designing the uncoupled patch

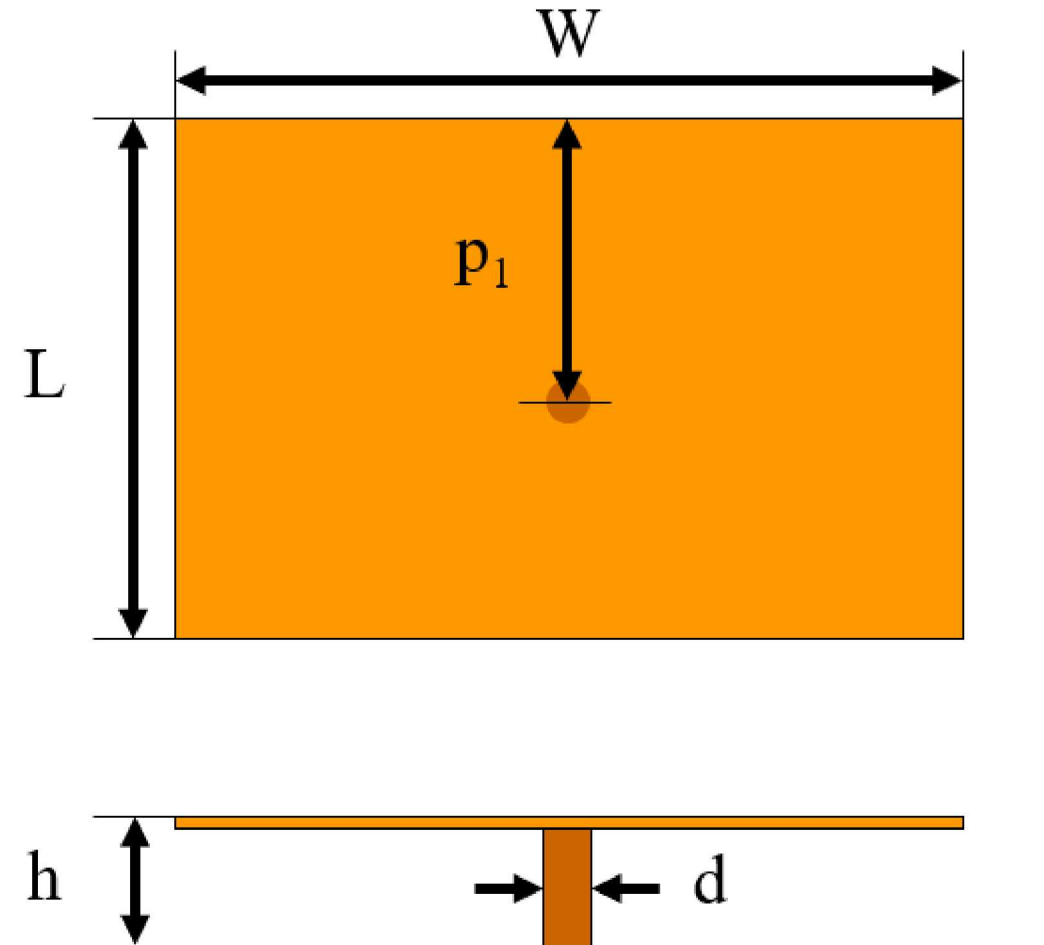
$$Q \sim 2.25 \frac{f_0}{BW} \sim 2.25 \kappa$$

Minimum Q sets constraints on patch height and substrate Dk

Set L to obtain resonant frequency at band center: $L \sim \lambda/2$

Start with $W \sim L/2$ and $p_1 \sim L/2$

Probe has no effect at this point, resonant conductance is very small

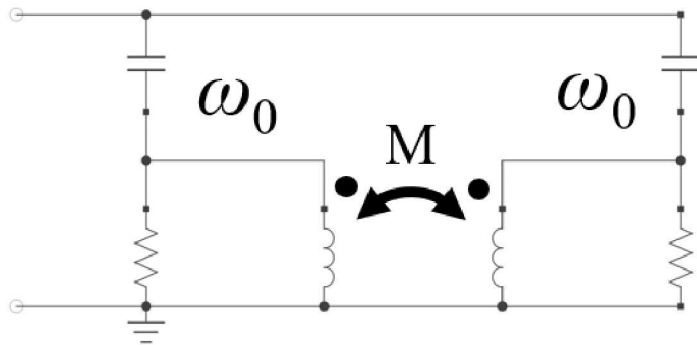


Designing the uncoupled slot

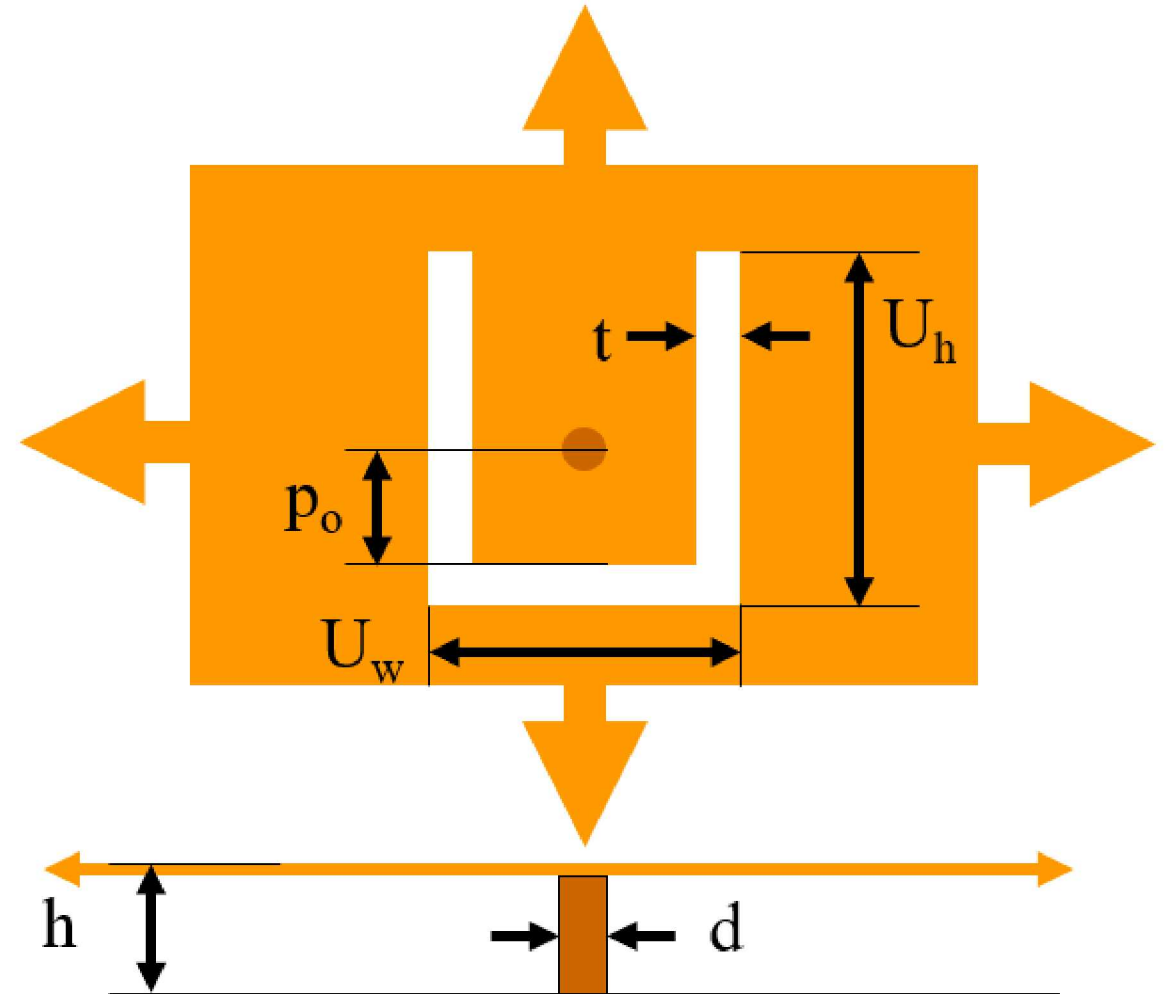
Total length of slot has largest effect on resonant frequency

Start with $U_w \sim \kappa W$

Study of the equivalent circuit shows that proper resonant conductance is about 40-50mS.



There are several guidelines to obtaining resonant frequency and conductance; some parameters affect these more than others.

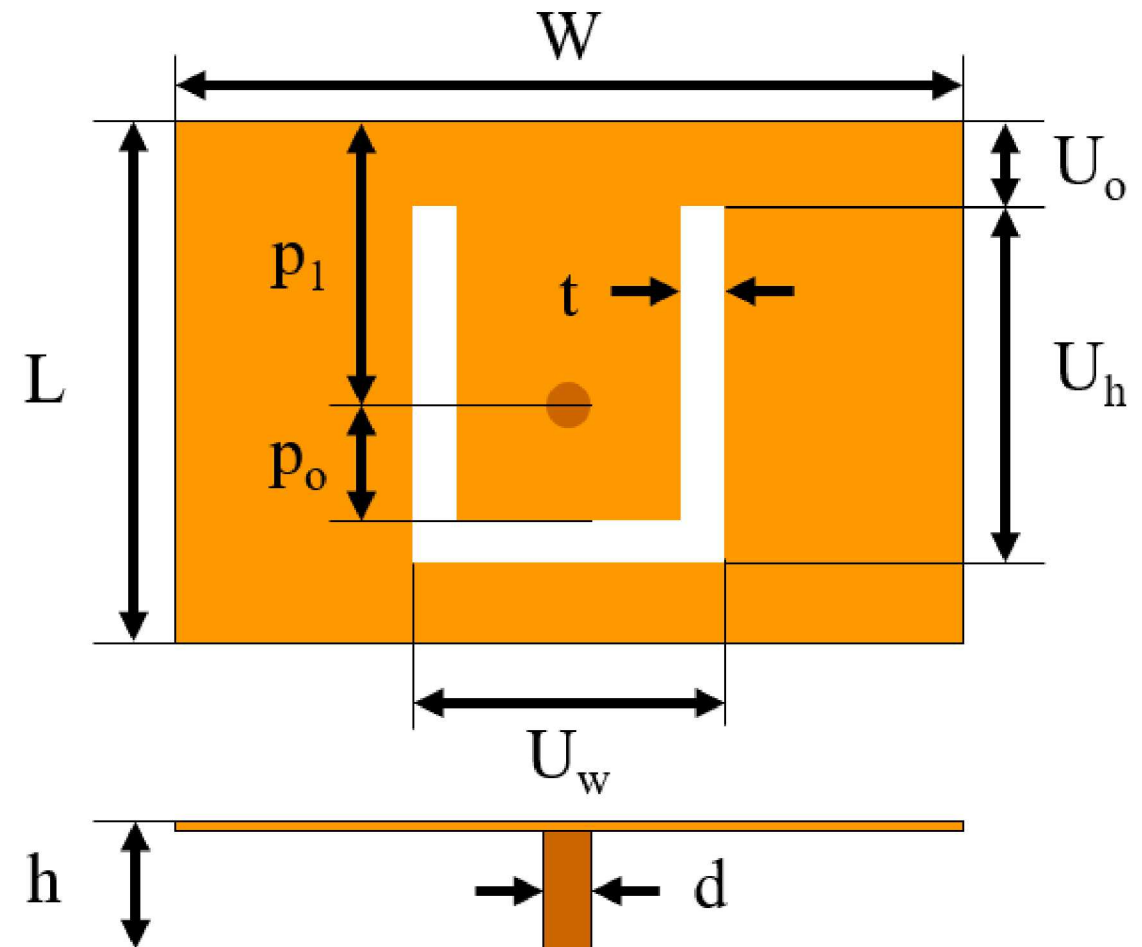


Combine uncoupled resonators & refine

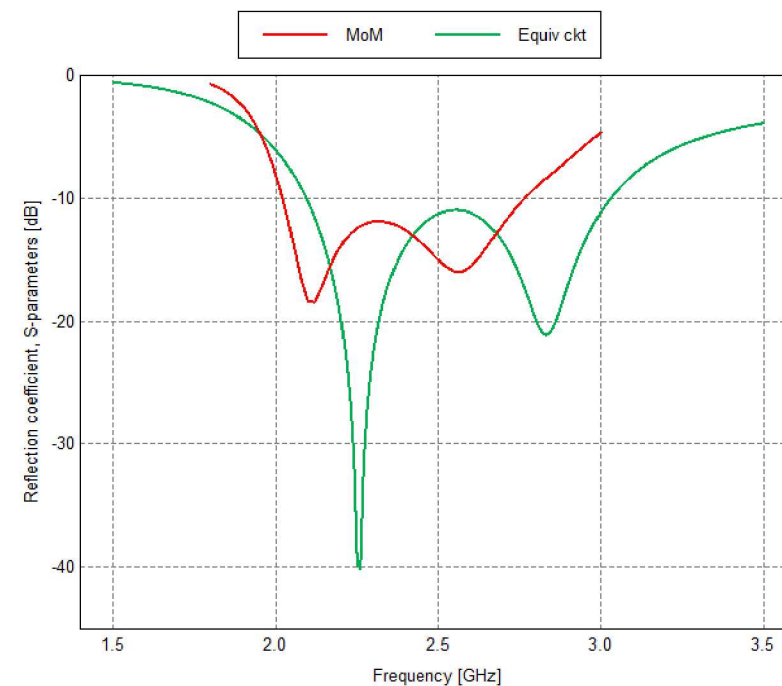
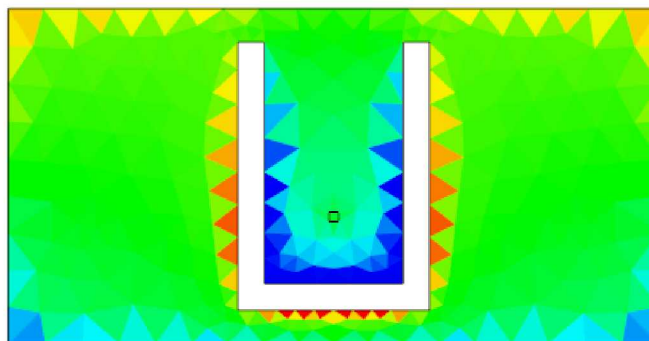
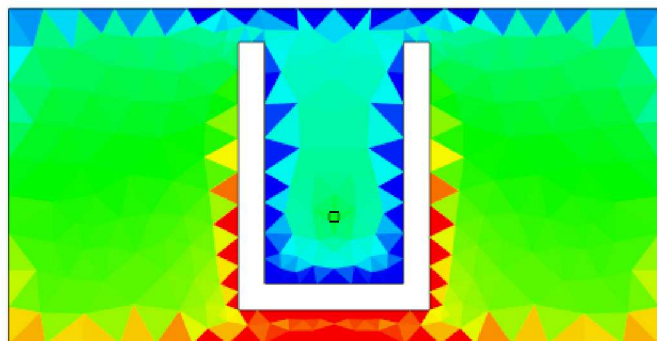
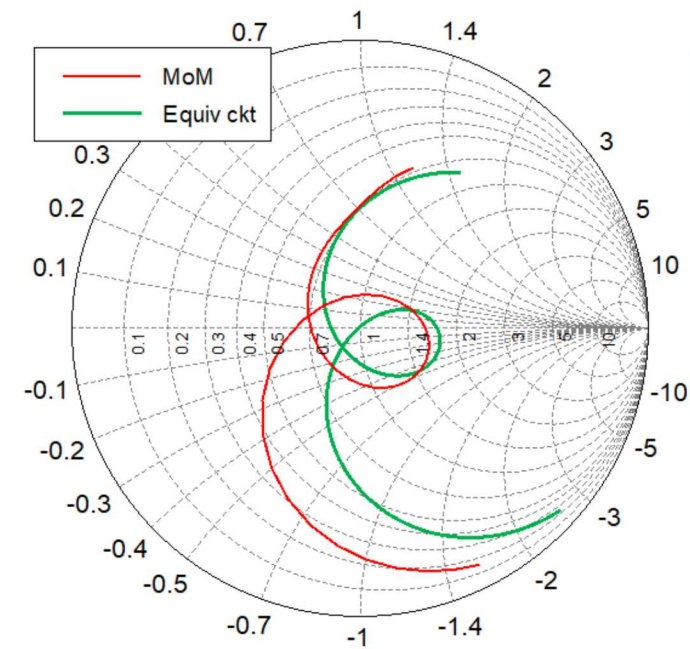
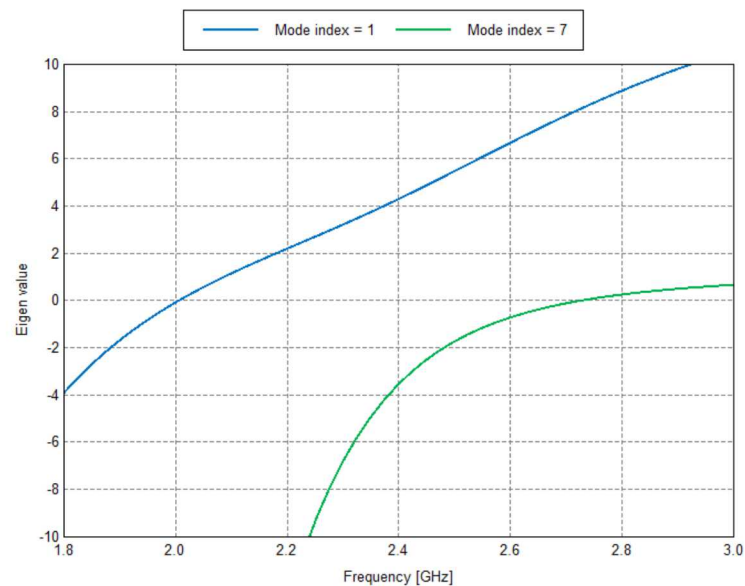
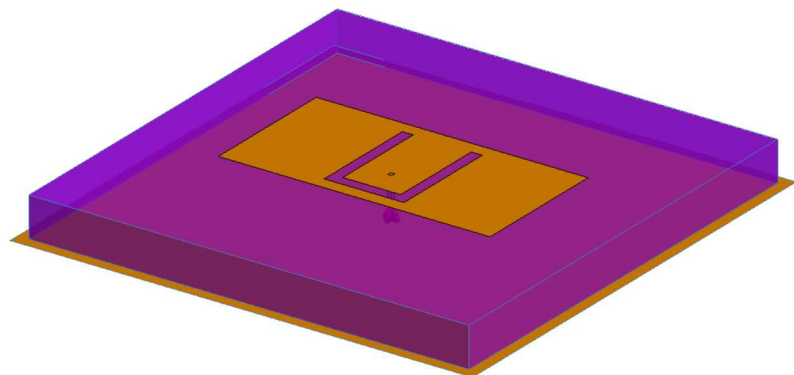
Drop uncoupled U-slot geometry onto patch such that the “U” is centered on the patch; maintain probe offset p_0

Run driven sim; impedance locus will have a loop in the Smith chart

Small adjustments (e.g., to U_0 , t , d) can be made such that loop optimally resides within VSWR circle on Smith chart



Example design



The U-slot patch operates with **coupled** modes; the patch and slot modes are equally important over the entire impedance bandwidth

The patch provides the majority of the radiation; the slot comparatively less

Due to the probe location, the patch mode is not well matched to 50Ω but the lumped LC “slot” resonator causes a good match

Coupled mode theory is **everywhere** in electrical engineering

Characteristic mode analysis is a modal decomposition method that can provide insight into EM/antenna designs

After a bit of modal deconstruction, sensible guidelines for designing the U-slot patch antenna can be developed