

Magneto-inertial fusion: Relaxing the requirements for efficient fusion on the Z machine

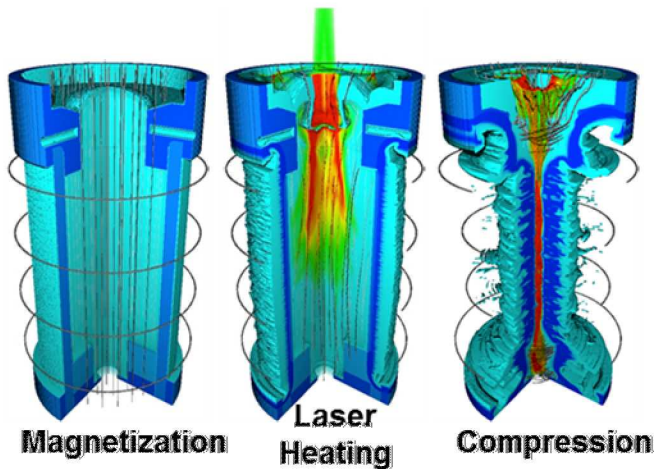
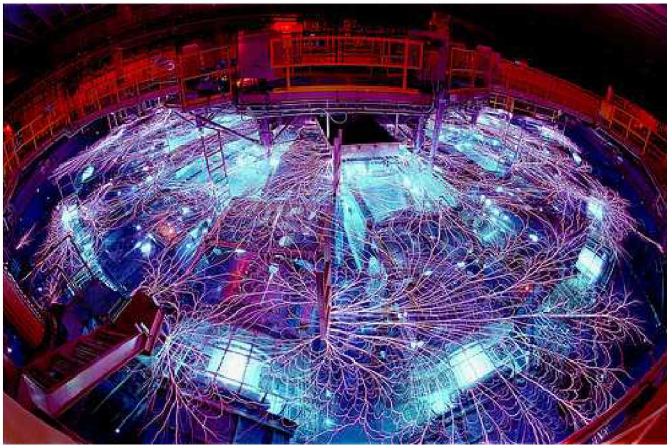
Matthew R. Gomez

for the MagLIF team

Sandia National Laboratories

HEDP Seminar at General Atomics

October 3, 2018



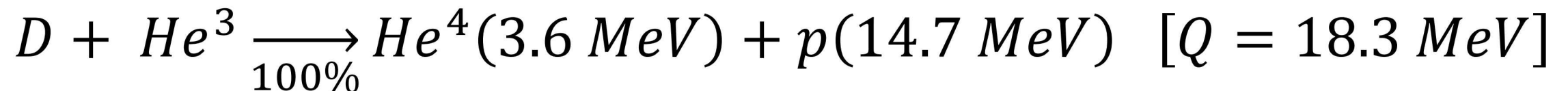
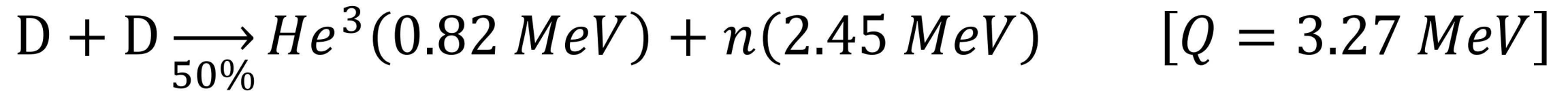
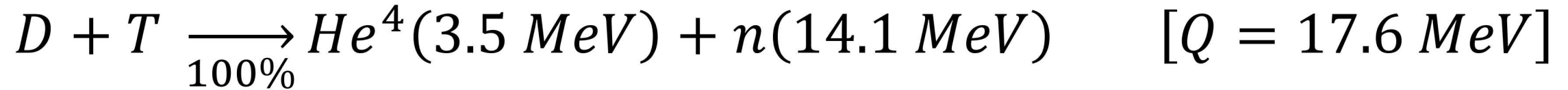
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Outline

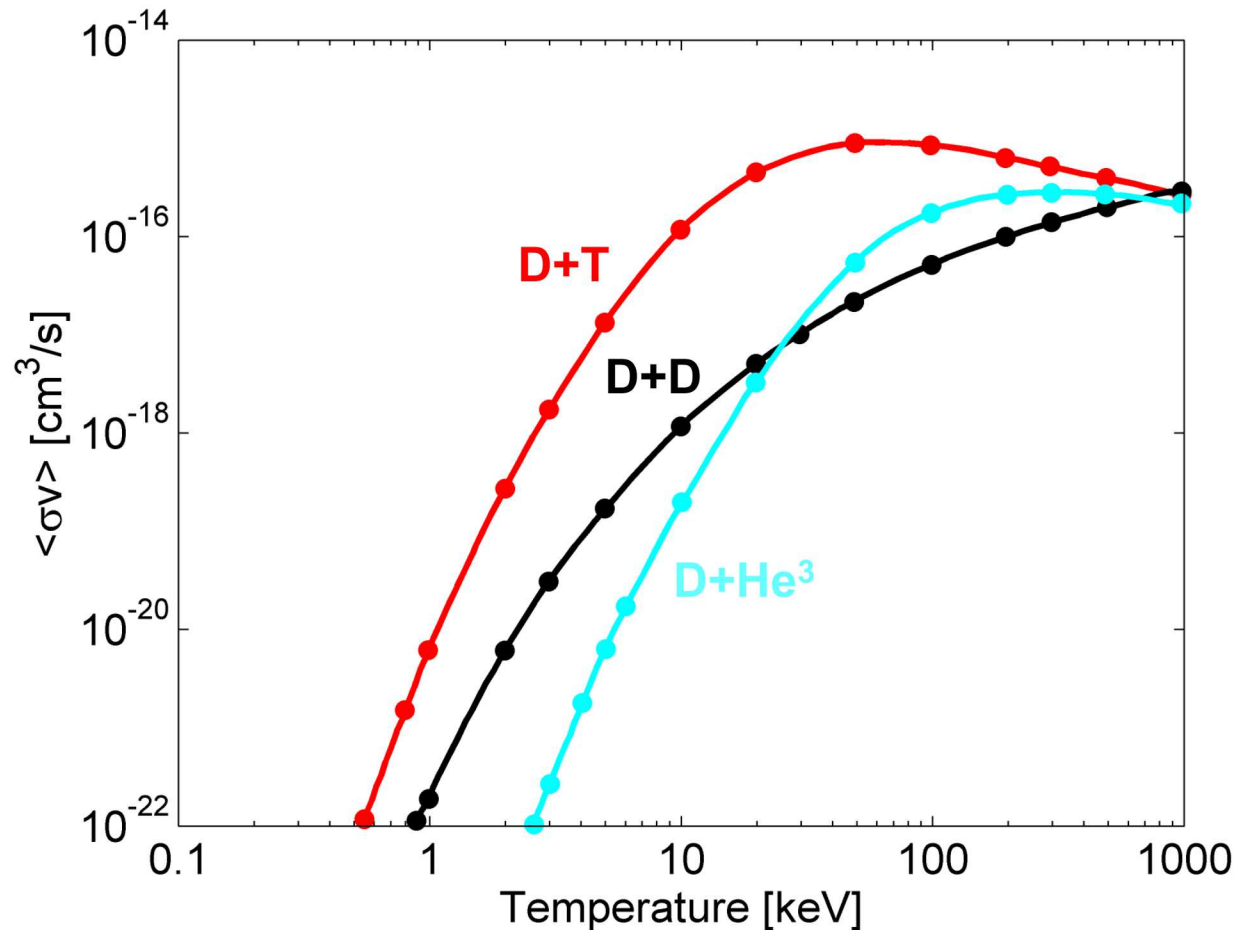
- **Introduction to magneto-inertial fusion**
 - Intro to Magnetized Liner Inertial Fusion (MagLIF)
- MagLIF experiments
 - Demonstration of the efficacy of magneto-inertial fusion
 - Improving target behavior
 - Identifying scaling trends
- Next generation experiments
 - Architecture of a next-generation pulsed power driver
 - Scaling to future drivers

Nuclear fusion reactions can release a significant amount of energy



All of these reactions are between two positively charged nuclei, so we need to overcome the coulomb repulsion between the reactants to get them close enough to fuse

Fusion reactions require extreme temperatures



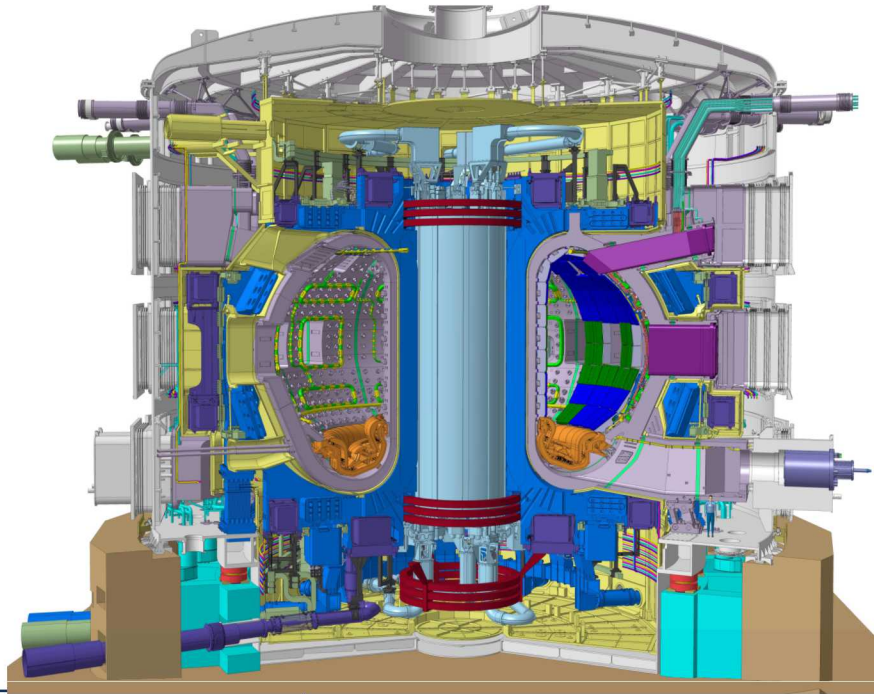
- All reaction rates drop precipitously at low temperatures
- D+T fusion has the highest rate across reasonable temperatures
- D+D fusion does not require tritium
- D+He³ fusion does not produce neutrons

At these temperatures, confinement is an issue

The two main schemes being pursued are magnetic and inertial confinement

Magnetic confinement fusion holds a large volume at low density for a long duration

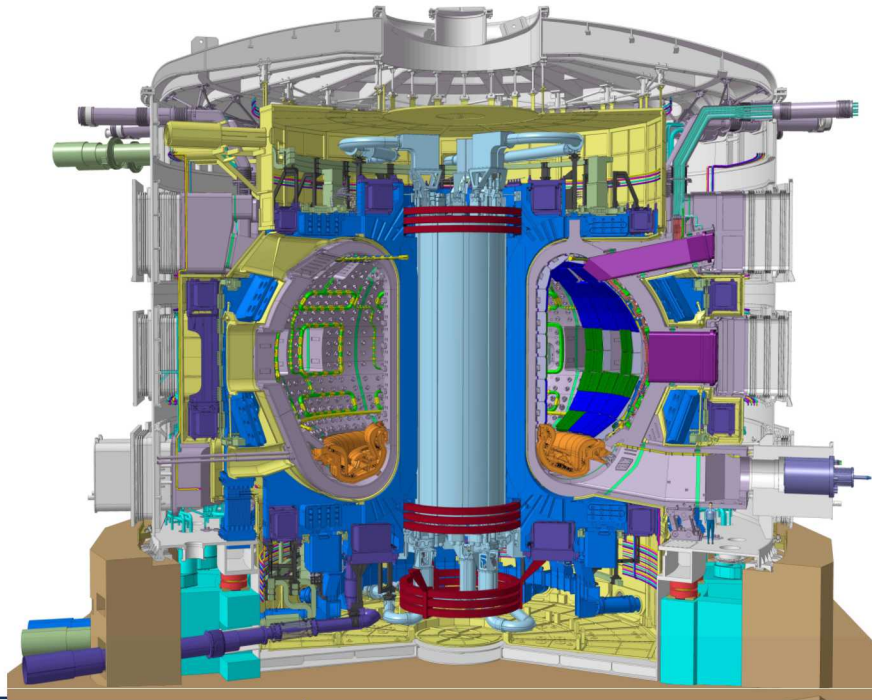
ITER



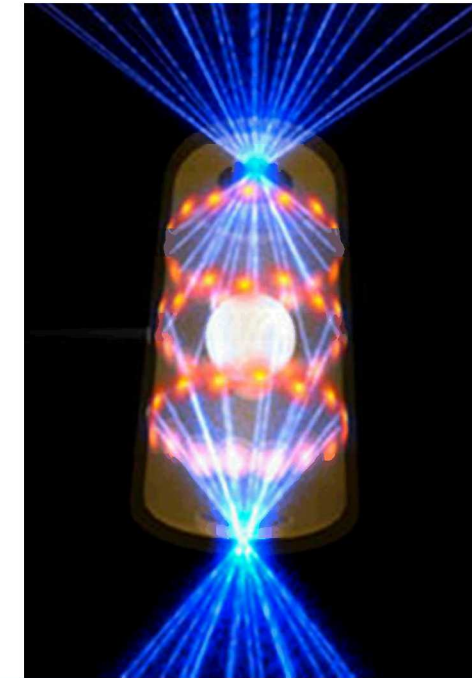
Density	$1 \times 10^{14} \text{ cm}^{-3}$		
Volume	$8 \times 10^8 \text{ cm}^3$		
Duration	300-500 s		
Magnetic field	100 kG		

Inertial confinement fusion creates a high density over small volume and short duration

ITER



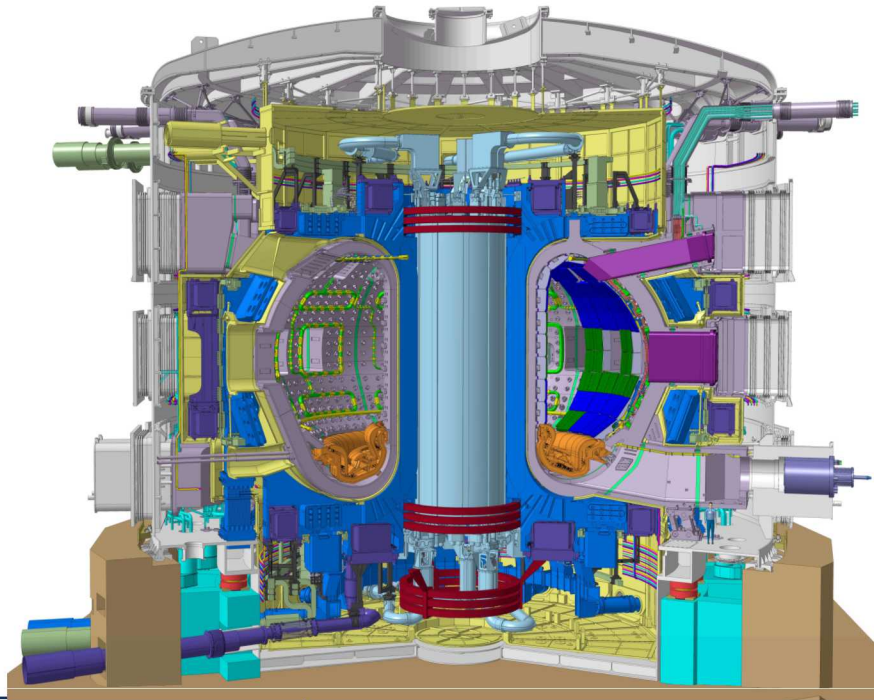
NIF hohlraum



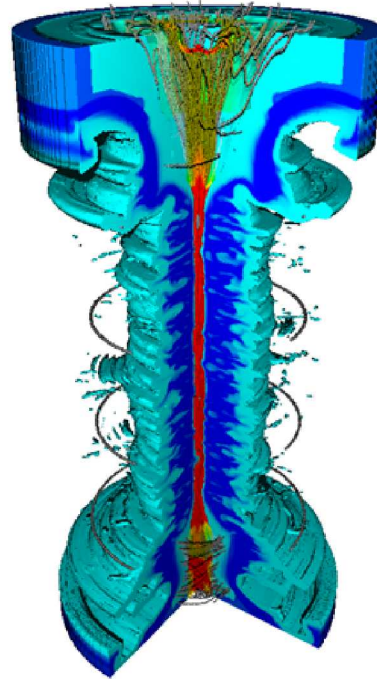
Density	$1 \times 10^{14} \text{ cm}^{-3}$		$2\text{-}20 \times 10^{25} \text{ cm}^{-3}$
Volume	$8 \times 10^8 \text{ cm}^3$		$6 \times 10^{-8} \text{ cm}^3$
Duration	300-500 s		$5\text{-}10 \times 10^{-11} \text{ s}$
Magnetic field	100 kG		0 kG

Magneto-inertial fusion sits in the space between the two

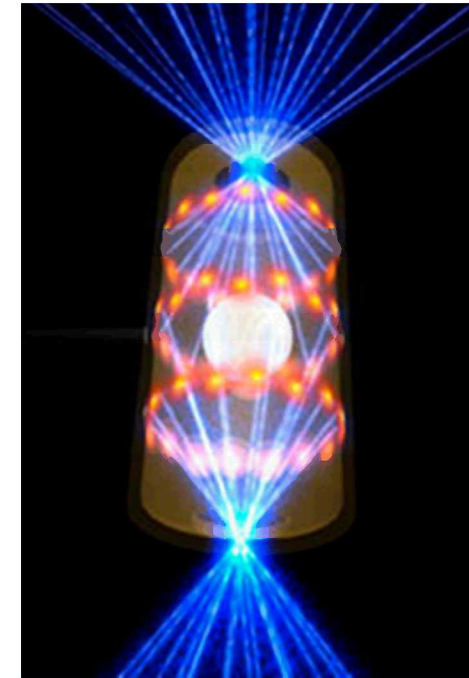
ITER



MagLIF stagnation

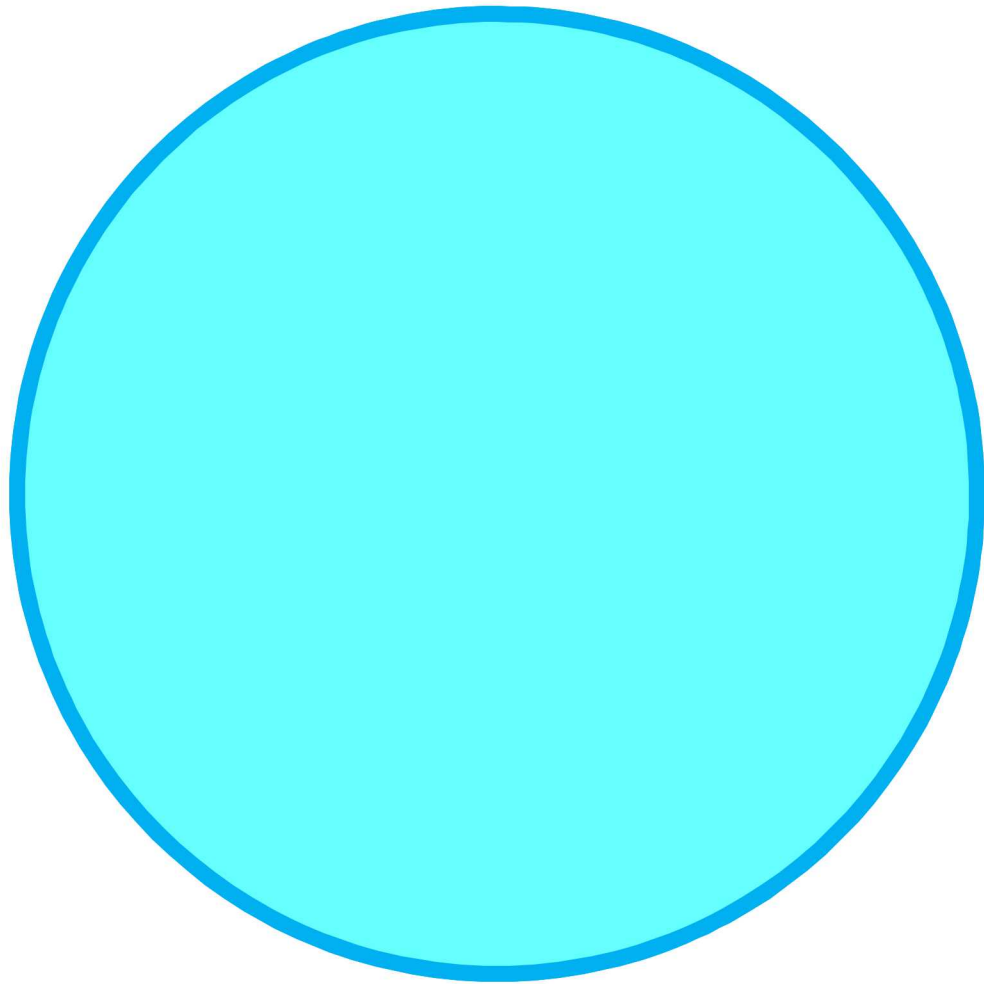


NIF hohlraum



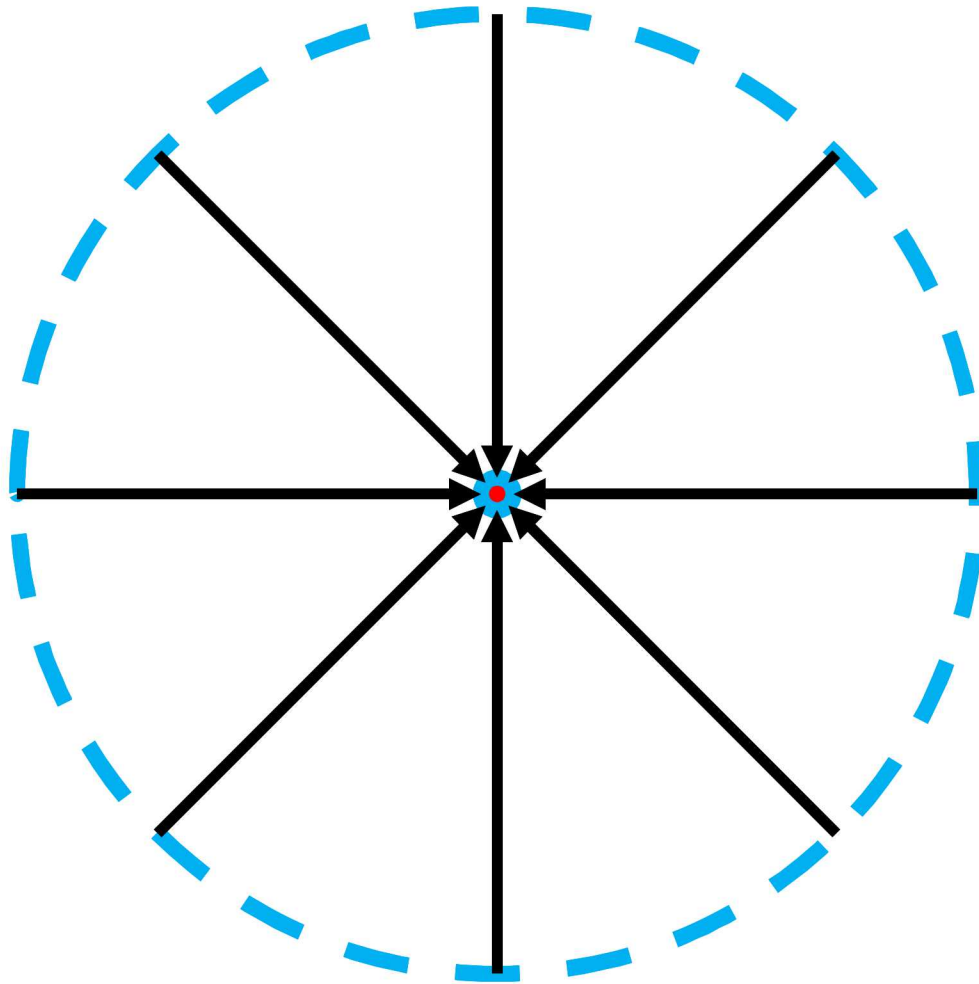
Density	$1 \times 10^{14} \text{ cm}^{-3}$	$1 \times 10^{23} \text{ cm}^{-3}$	$2\text{-}20 \times 10^{25} \text{ cm}^{-3}$
Volume	$8 \times 10^8 \text{ cm}^3$	$8 \times 10^{-5} \text{ cm}^3$	$6 \times 10^{-8} \text{ cm}^3$
Duration	300-500 s	$1\text{-}2 \times 10^{-9} \text{ s}$	$5\text{-}10 \times 10^{-11} \text{ s}$
Magnetic field	100 kG	50-100 MG	0 kG

Since we are building from ICF, let's quickly review traditional ICF



- Start with a sphere containing DT

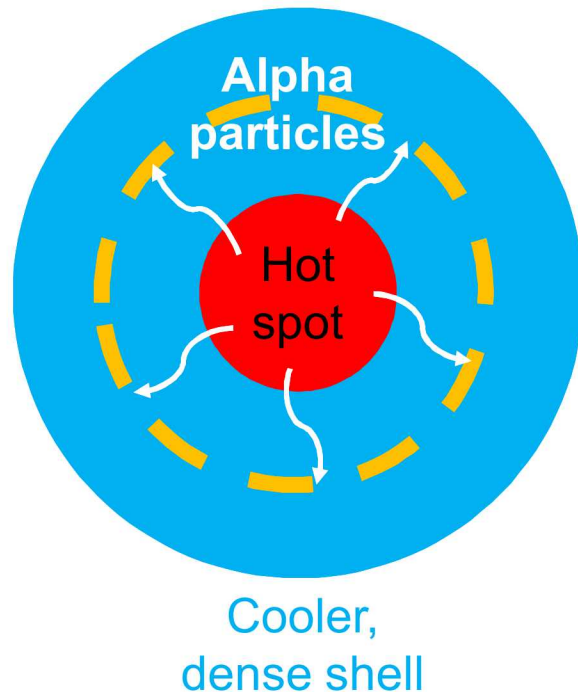
Since we are building from ICF, let's quickly review traditional ICF



- Start with a sphere containing DT
- Implode the sphere
 - Compress radius by ~ 30
(volume decreases by $\sim 27,000$)
 - Series of shocks heat the center
(hot spot)

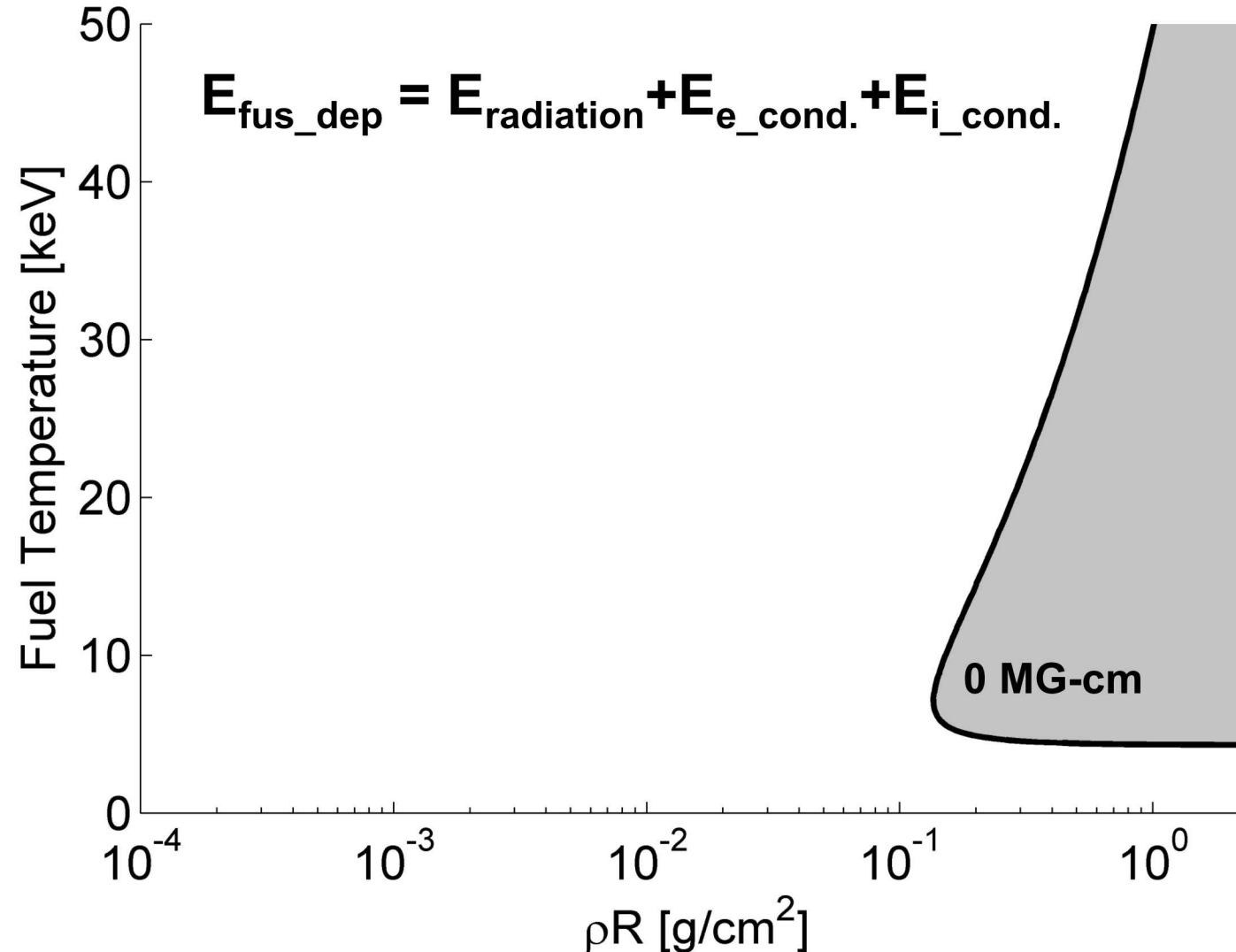
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Zooming in



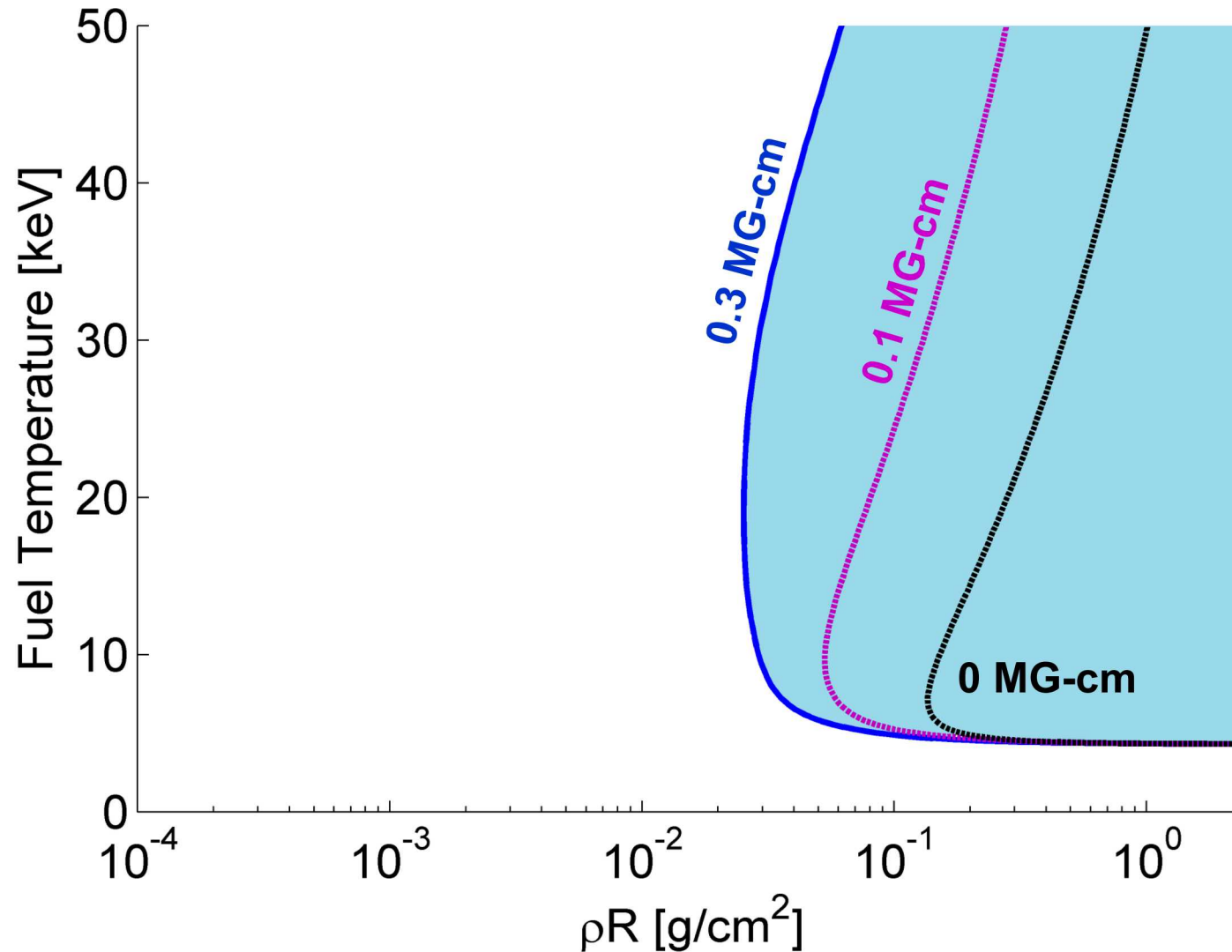
- Start with a sphere containing DT
- Implode the sphere
 - Compress radius by 30 (volume by 27,000)
 - Series of shocks heat the center (hot spot)
- Fuel in hot spot undergoes fusion
 - Fusion products heat surrounding dense fuel
- With a favorable power balance, a chain reaction occurs

ICF has requirements on stagnation conditions to propagate a burn wave



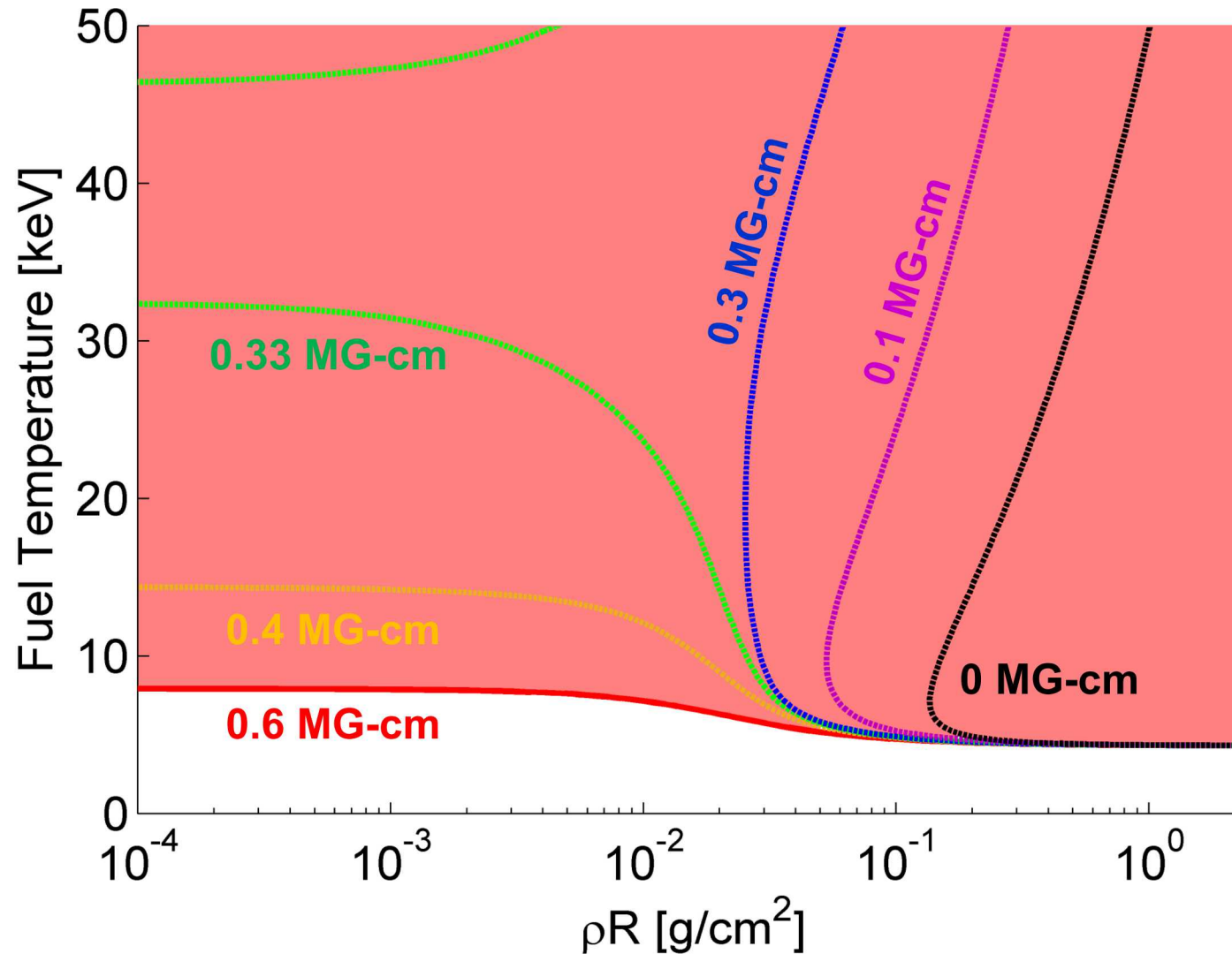
- There is a minimum fuel temperature of about 4.5 keV
 - This is where fusion heating outpaces radiation losses
- The minimum fuel areal density is around 0.2 g/cm²
- Traditional ICF concepts attempt to operate in this minimum

Magneto-inertial fusion utilizes magnetic fields to relax the stagnation requirements of ICF



- Applying a magnetic field opens up a larger region of parameter space
- The minimum temperature does not change because it is driven by radiation losses
- At 0.3 MG-cm, the Larmor radius of fusion alphas is approximately the radius of the fuel

Magneto-inertial fusion utilizes magnetic fields to relax the stagnation requirements of ICF

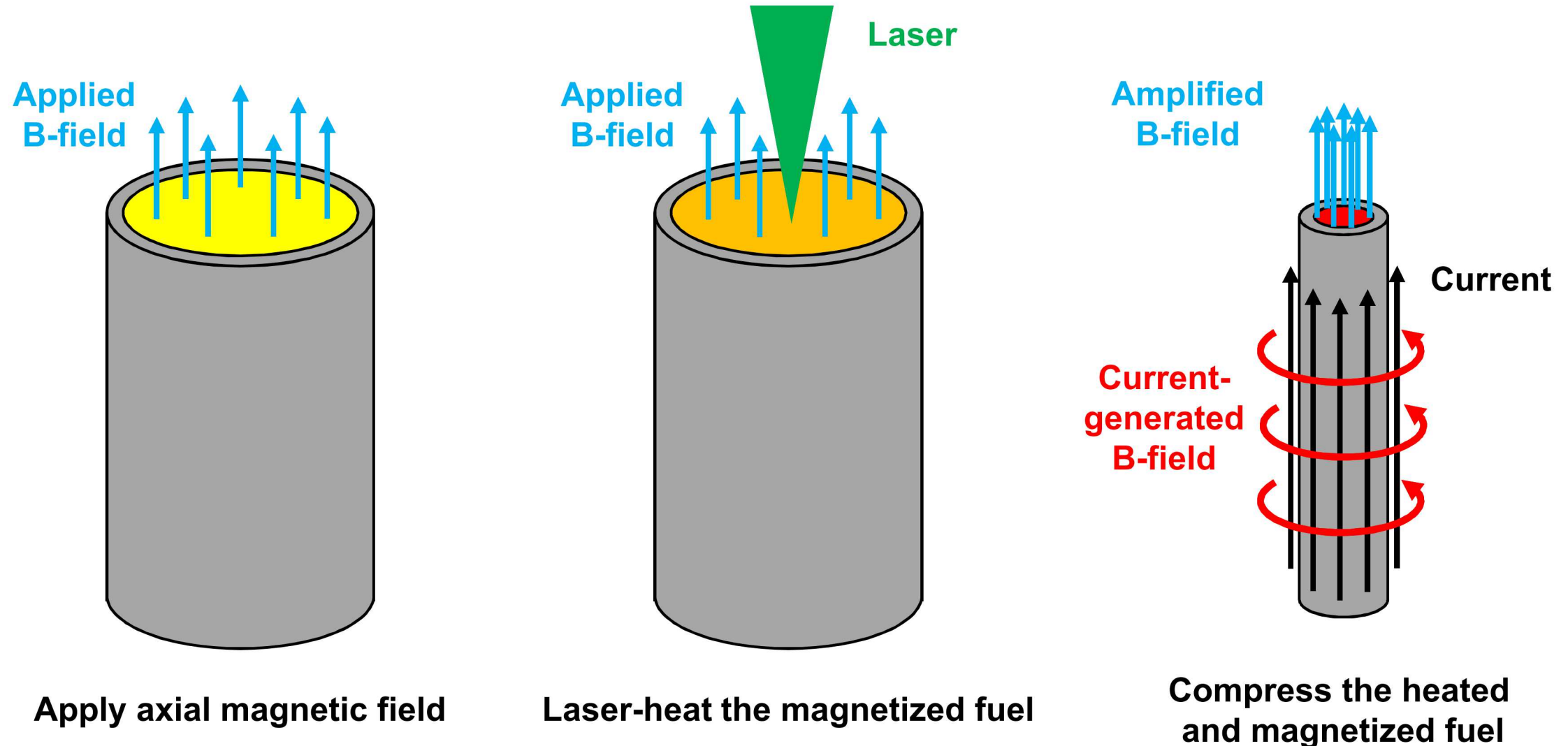


- With a high enough magnetic-field-radius product, most charged fusion products become trapped
- This relaxes the areal density requirement of the fuel
- Good performance is possible over a much larger region of parameter space

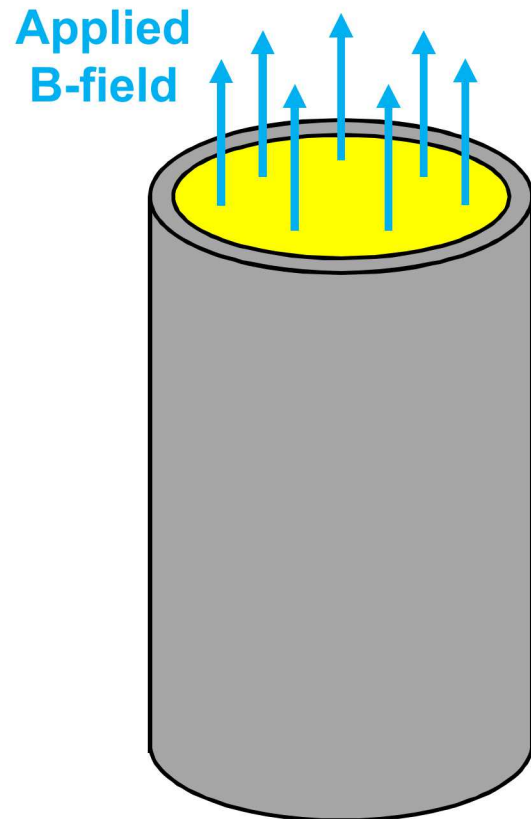
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Magnetized Liner Inertial Fusion relies on three stages to produce fusion relevant conditions



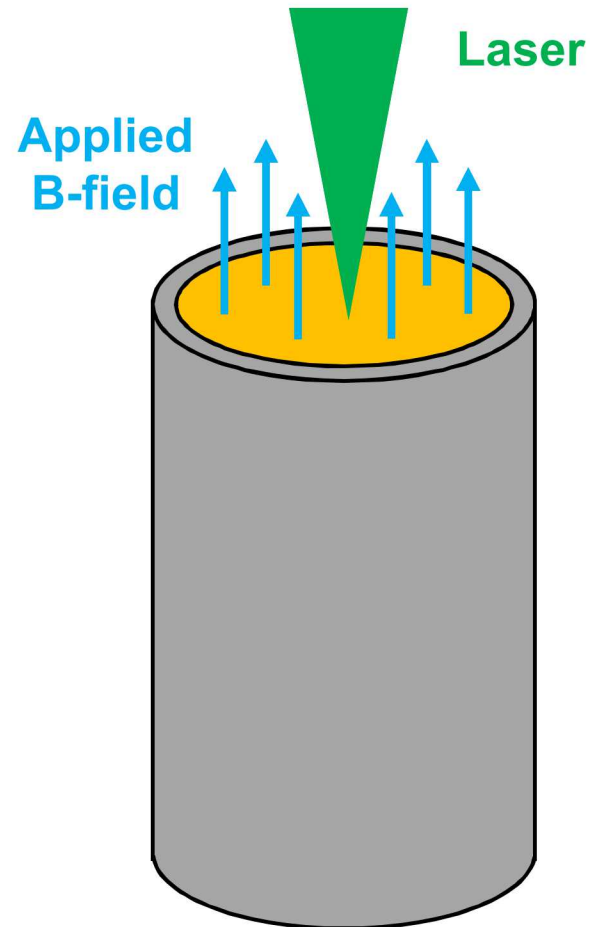
We start with a metal cylinder containing fusion fuel



Apply axial magnetic field

- The metal cylinder (also called a liner or target) is 10 mm tall, about 5 mm in diameter, and has a wall thickness of about 0.5 mm
 - The fuel is about 1 mg/cc of deuterium gas
- Helmholtz-like coils apply 10s of T
 - few ms risetime to allow field to diffuse through conductors
 - The field will limit thermal transport in the radial direction when the fuel has been converted to a plasma

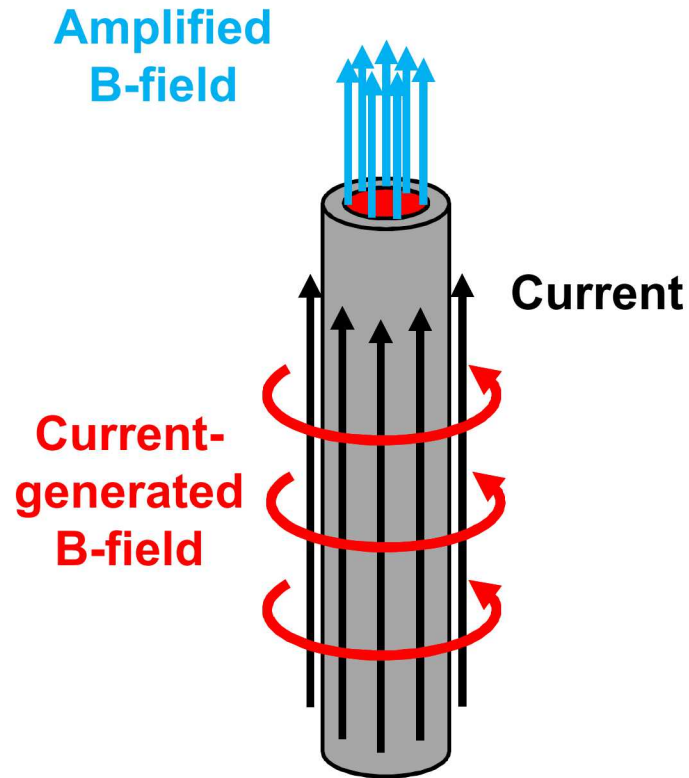
A laser is used to heat the fuel at the start of the implosion



Laser-heat the magnetized fuel

- A green (527 nm) laser is used to heat the fuel in a few ns with a few kJ of energy
- Laser must pass through 1-3 μm thick plastic window
 - Can lose many hundreds of joules to absorption in and scattering off of the plastic
- Fuel is heated to hundreds of eV
 - Recall the axial magnetic field limits thermal conduction in the radial direction

The current from the Z machine is used to implode the target



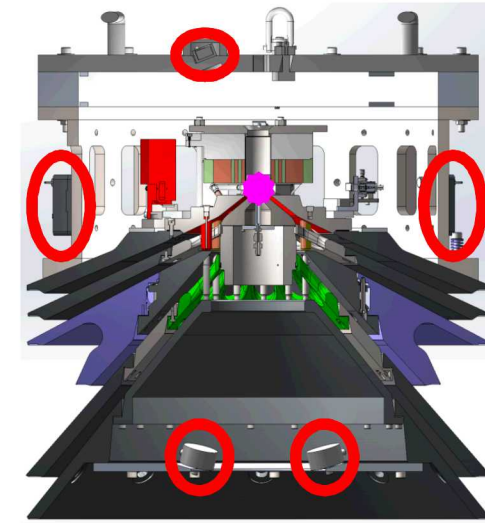
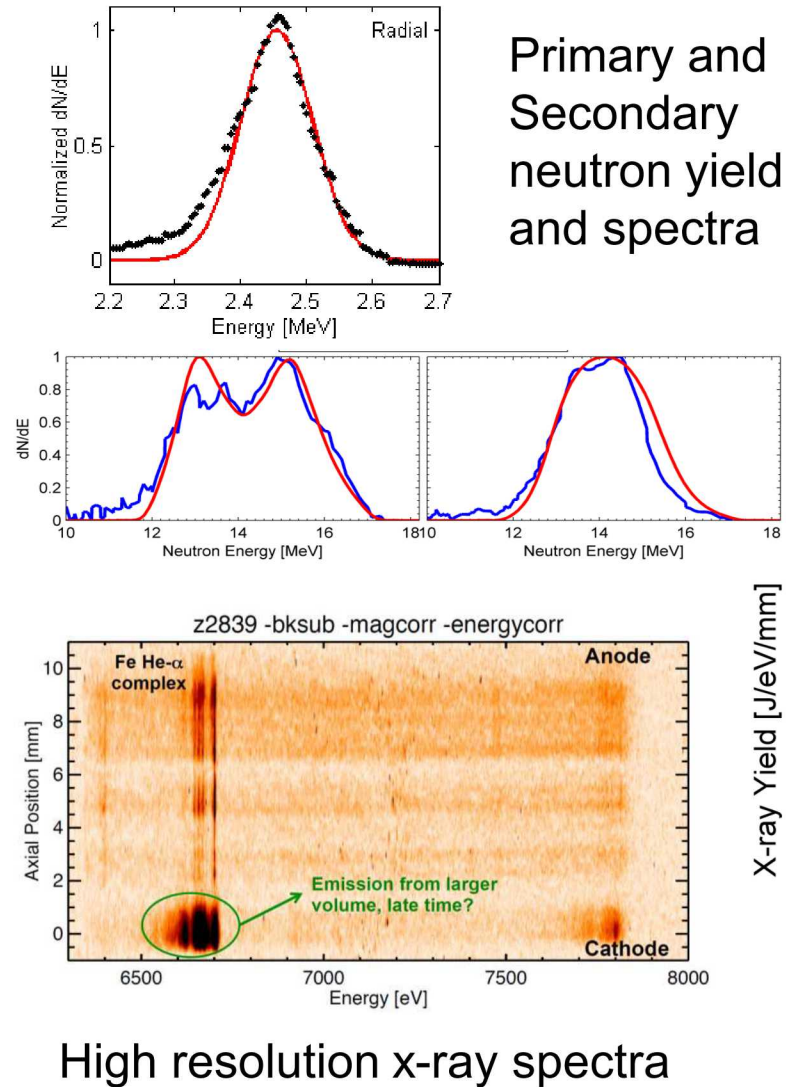
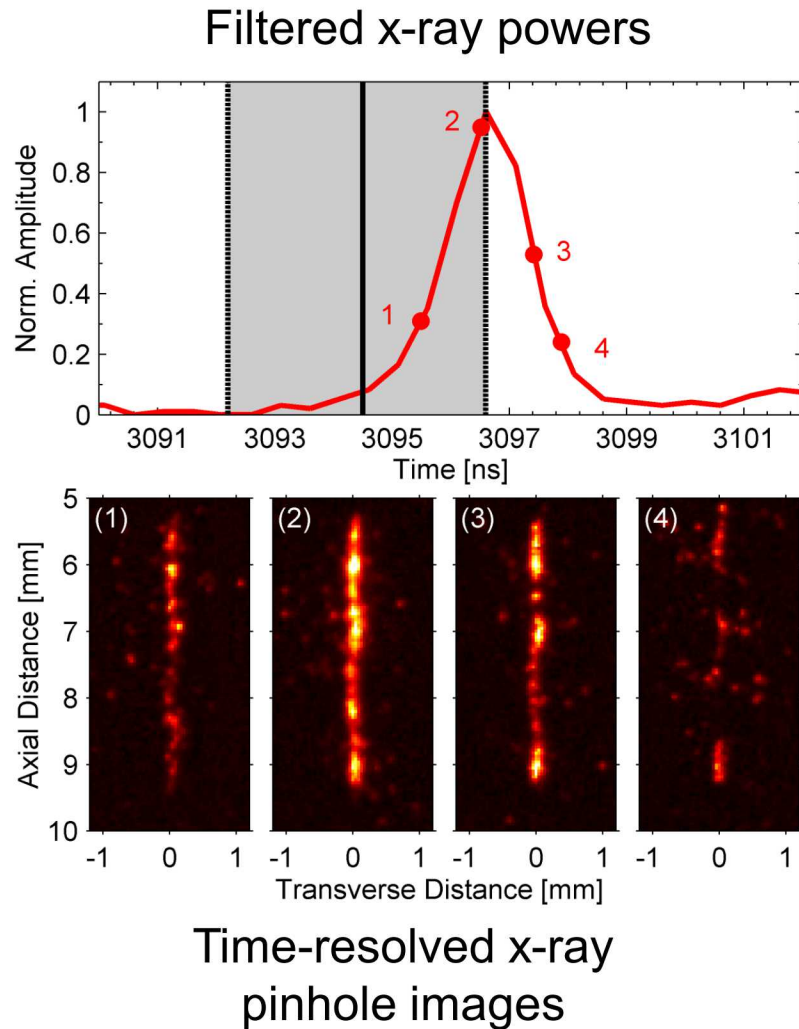
Compress the heated
and magnetized fuel

- Axial current is 15-20 MA, risetime is 100 ns
 - Generates ~ 3 kT azimuthal B-field
 - Metal cylinder implodes at ~ 70 km/s
- Fuel is nearly adiabatically compressed, which further heats the fuel to keV temperatures
- Axial magnetic field is increased to 1-10 kT through flux compression

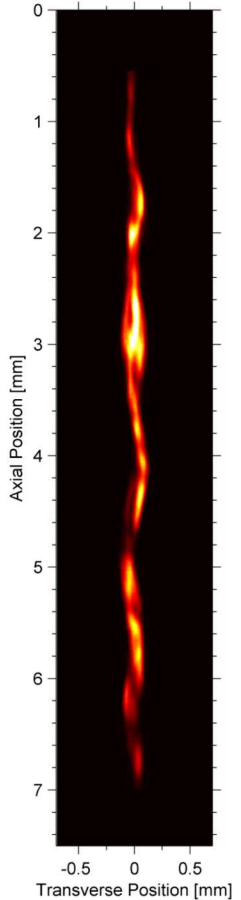
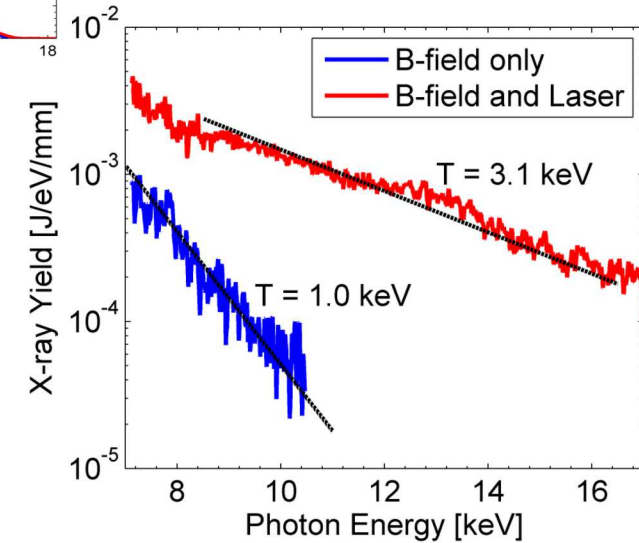
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We collect a wide range of data to assess stagnation



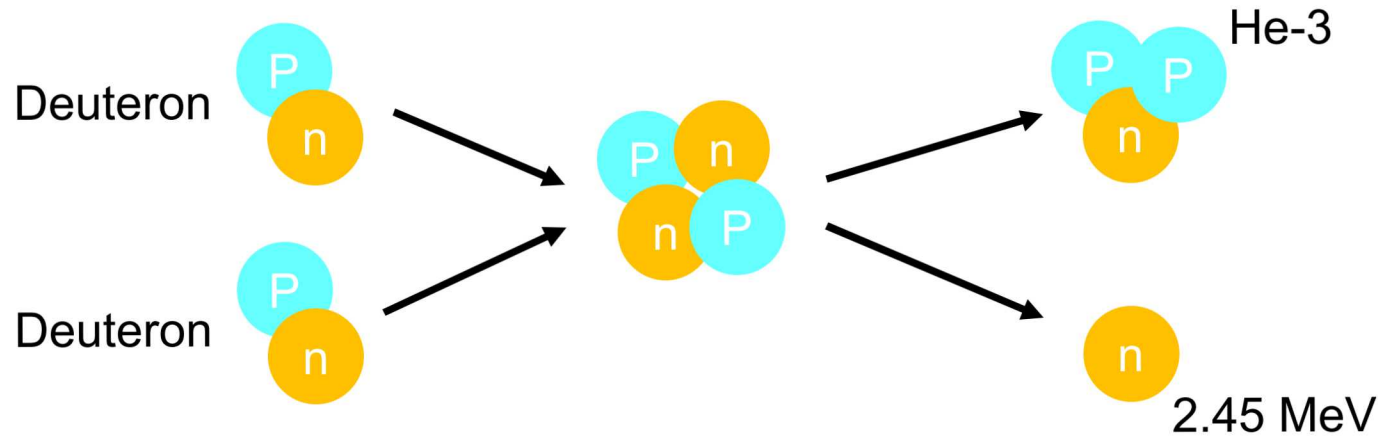
Time-integrated high resolution images



High energy x-ray spectra

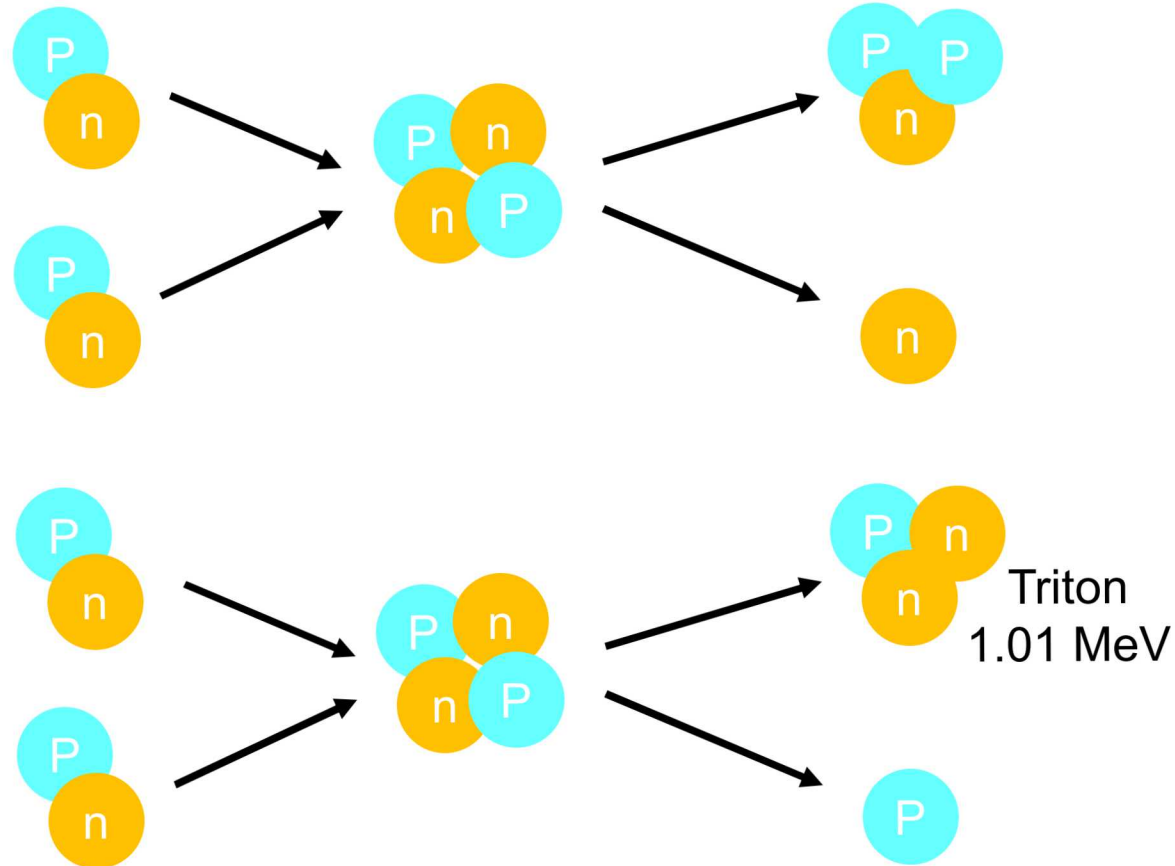
The fuel in these experiments is deuterium gas: one branch produces a neutron...

Primary Reactions



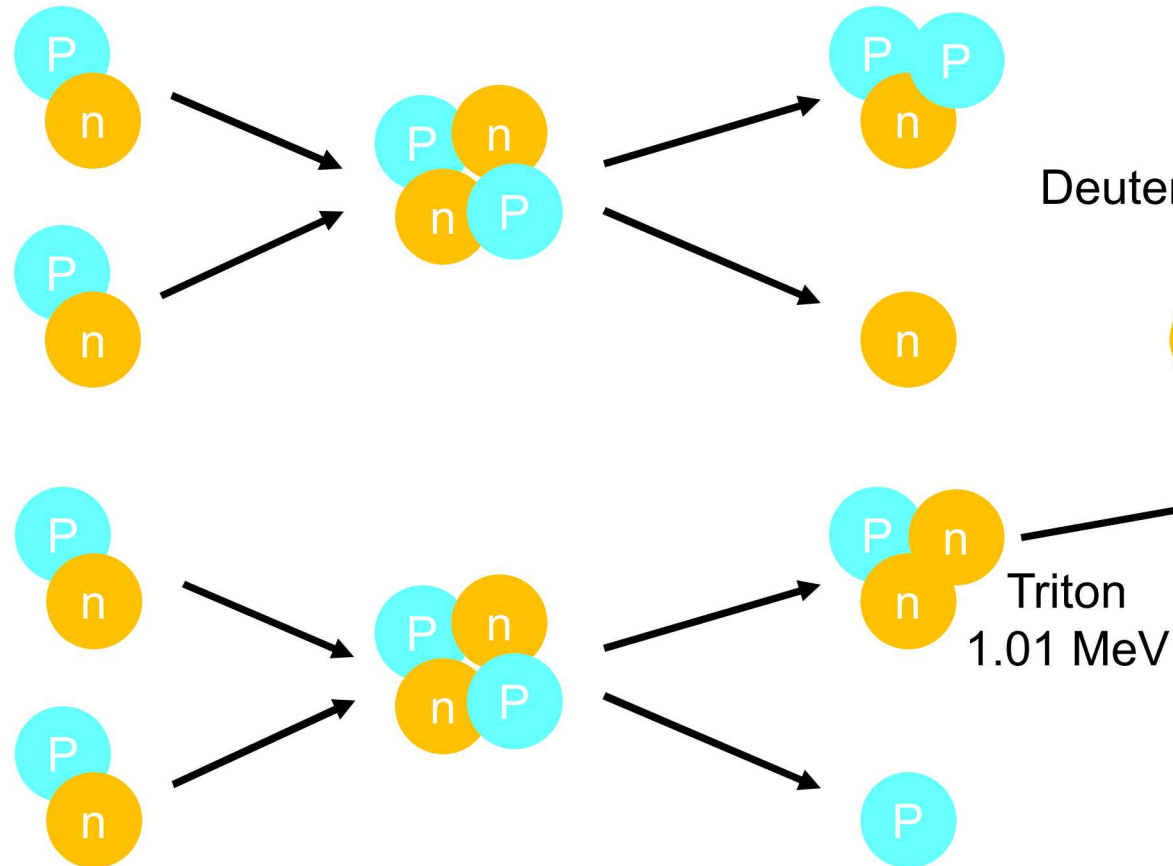
...and the other branch produces a triton...

Primary Reactions



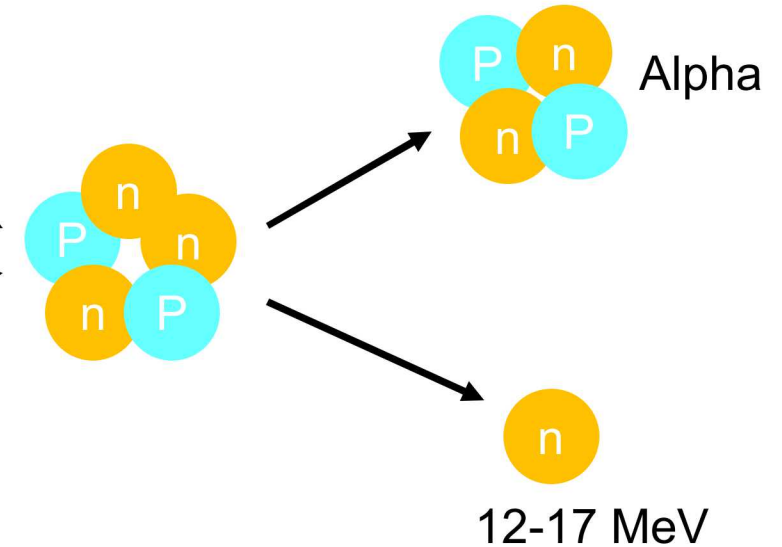
...which can fuse with a deuteron to produce a higher energy neutron

Primary Reactions

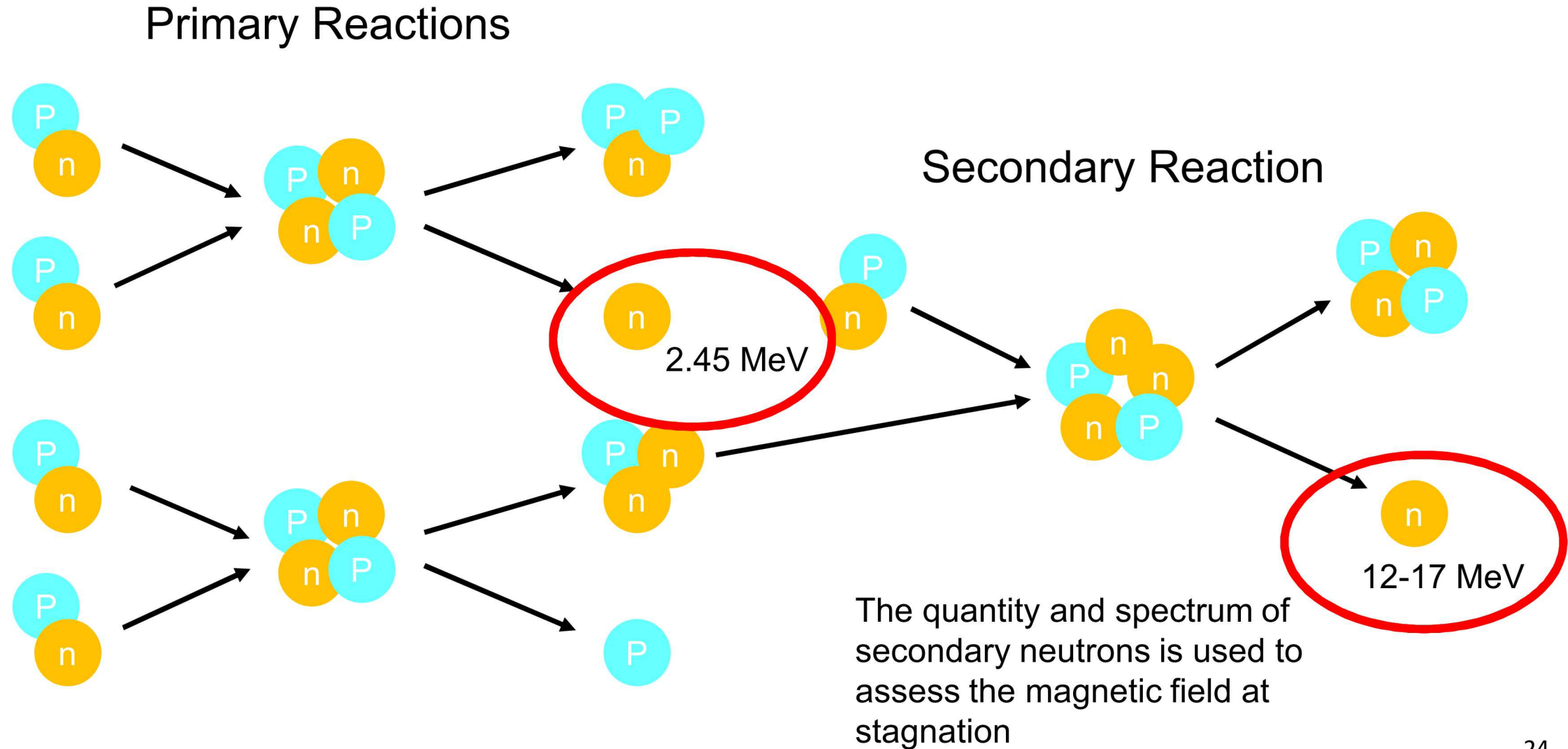


Secondary Reaction

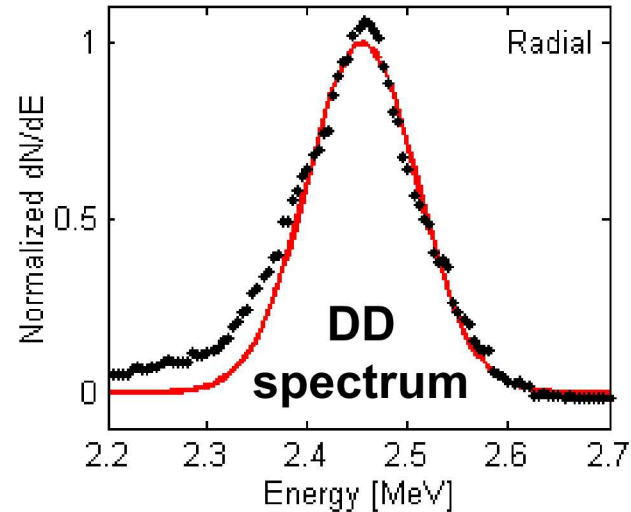
Deuteron



We measure both the primary and secondary neutrons

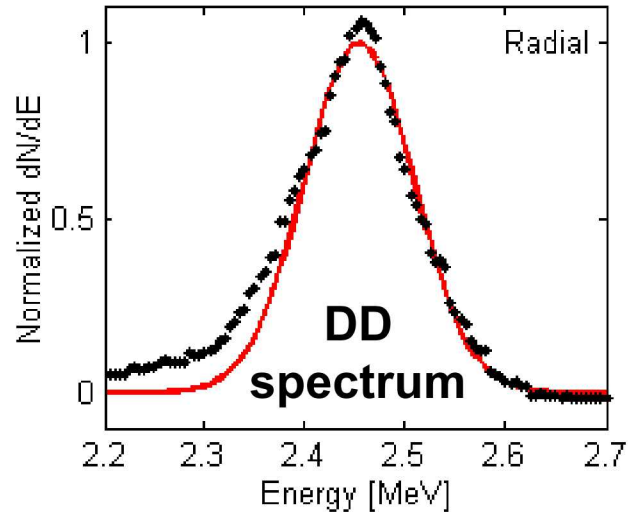


The first round of experiments demonstrated the fundamental requirements for MIF



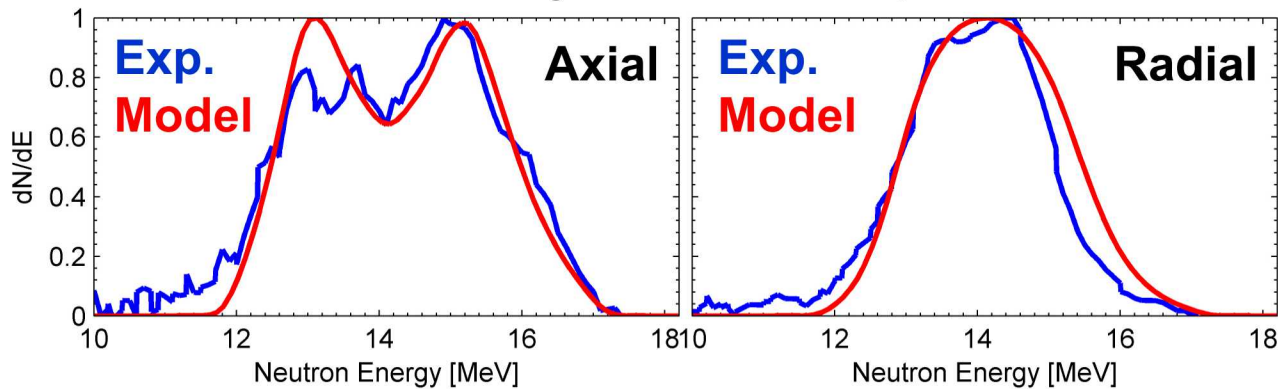
Thermonuclear neutron
generation with
fusion-relevant ion
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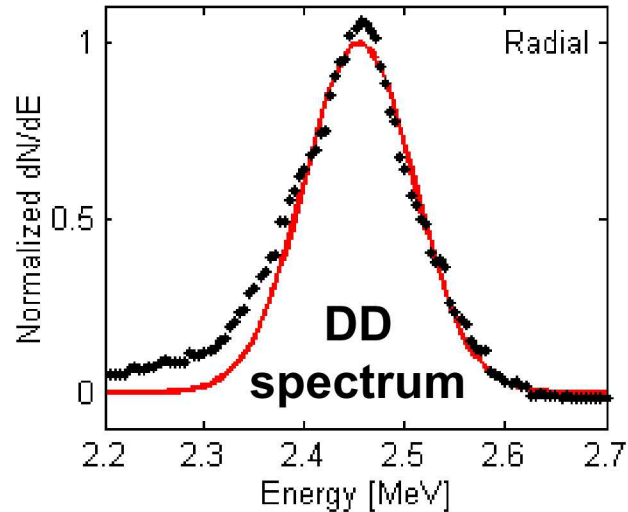
Thermonuclear neutron generation with fusion-relevant ion temperatures (2-3 keV)

Secondary DT Neutron Spectra



Highly magnetized fuel at stagnation (>0.3 MG-cm)

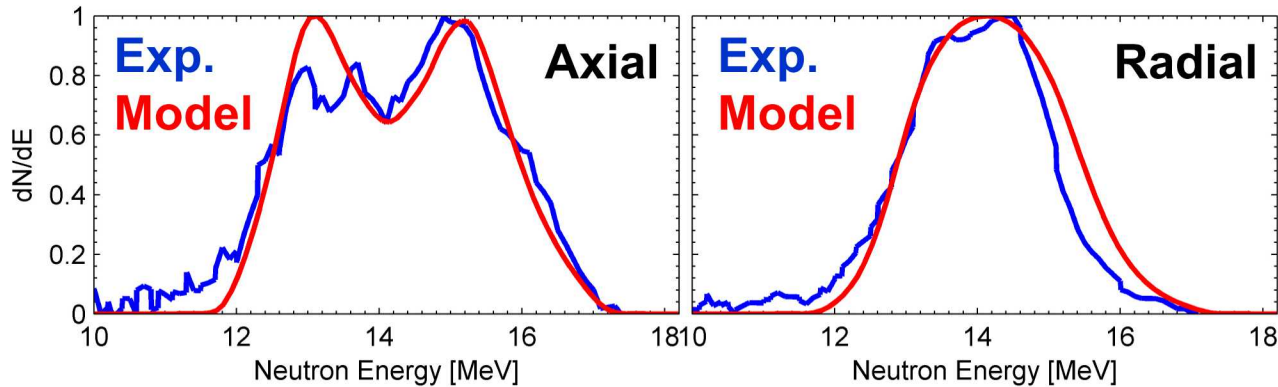
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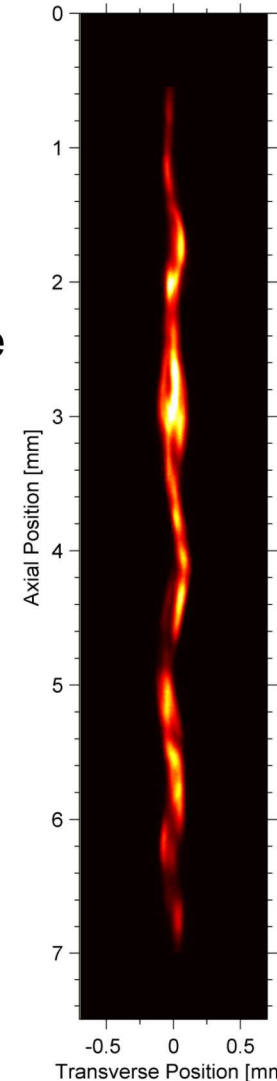
Thermonuclear neutron generation with fusion-relevant ion temperatures (2-3 keV)

Relatively stable fuel column at $CR > 30$

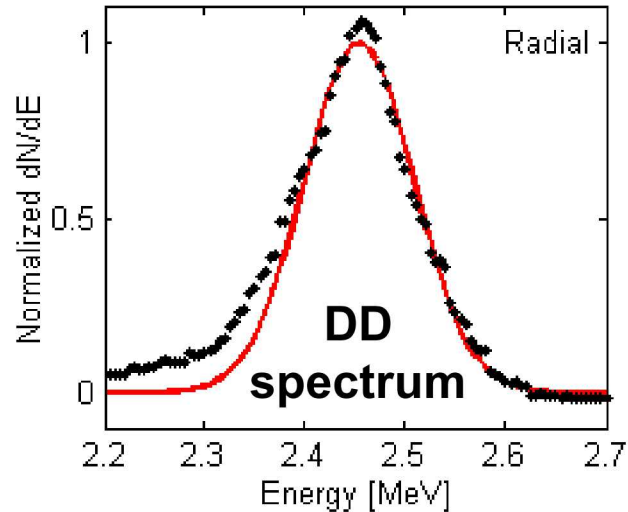
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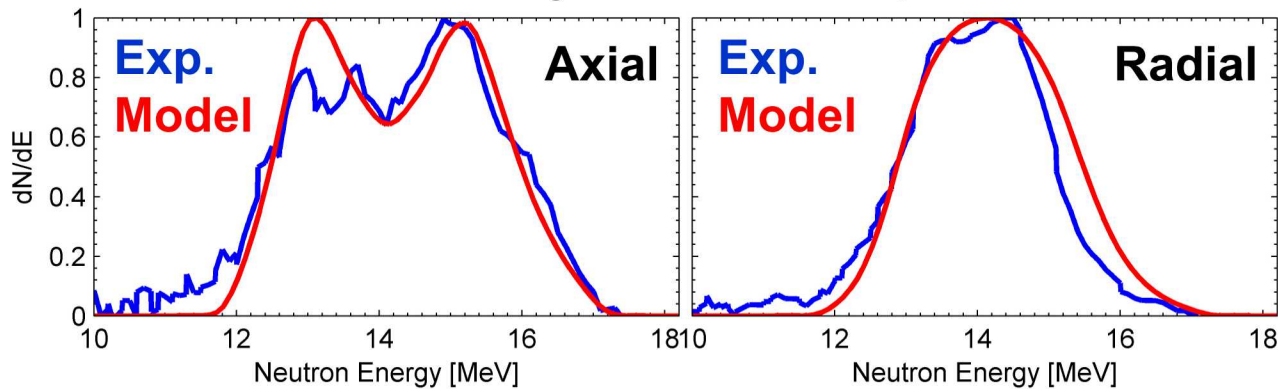
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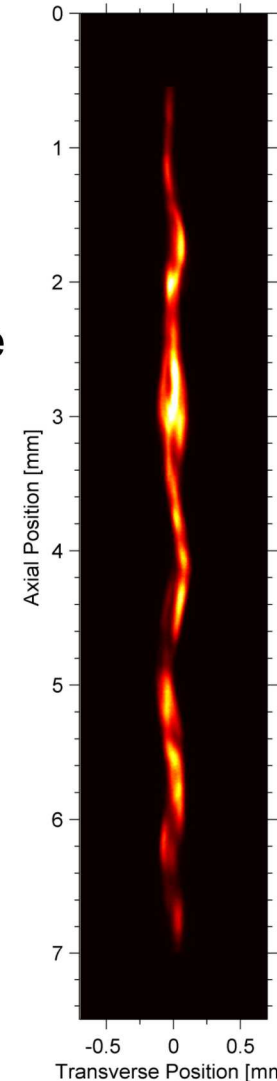
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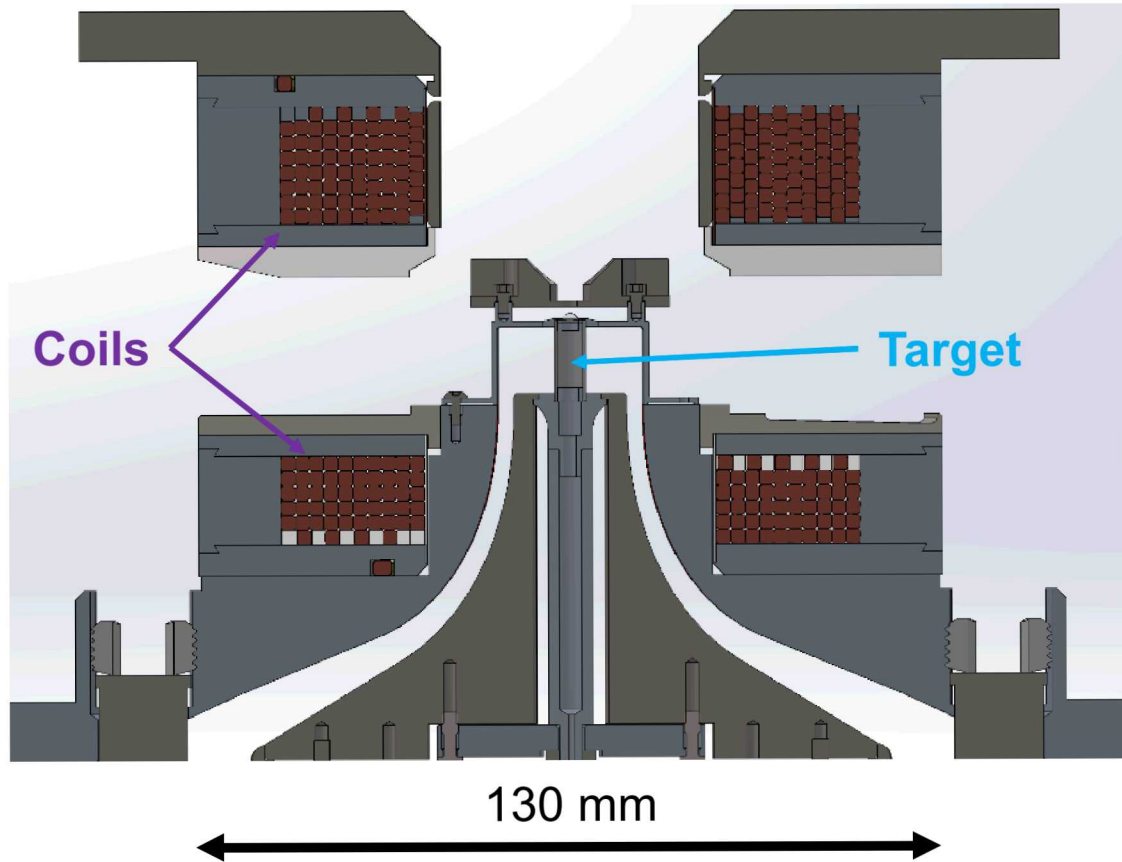
	No B-field	B-field
No Laser	3e9	1e10
Laser	4e10	2e12

Highly diagnosable primary DD neutron yield **only when using B-field and preheat** ($\sim 10^{12}$)

Outline

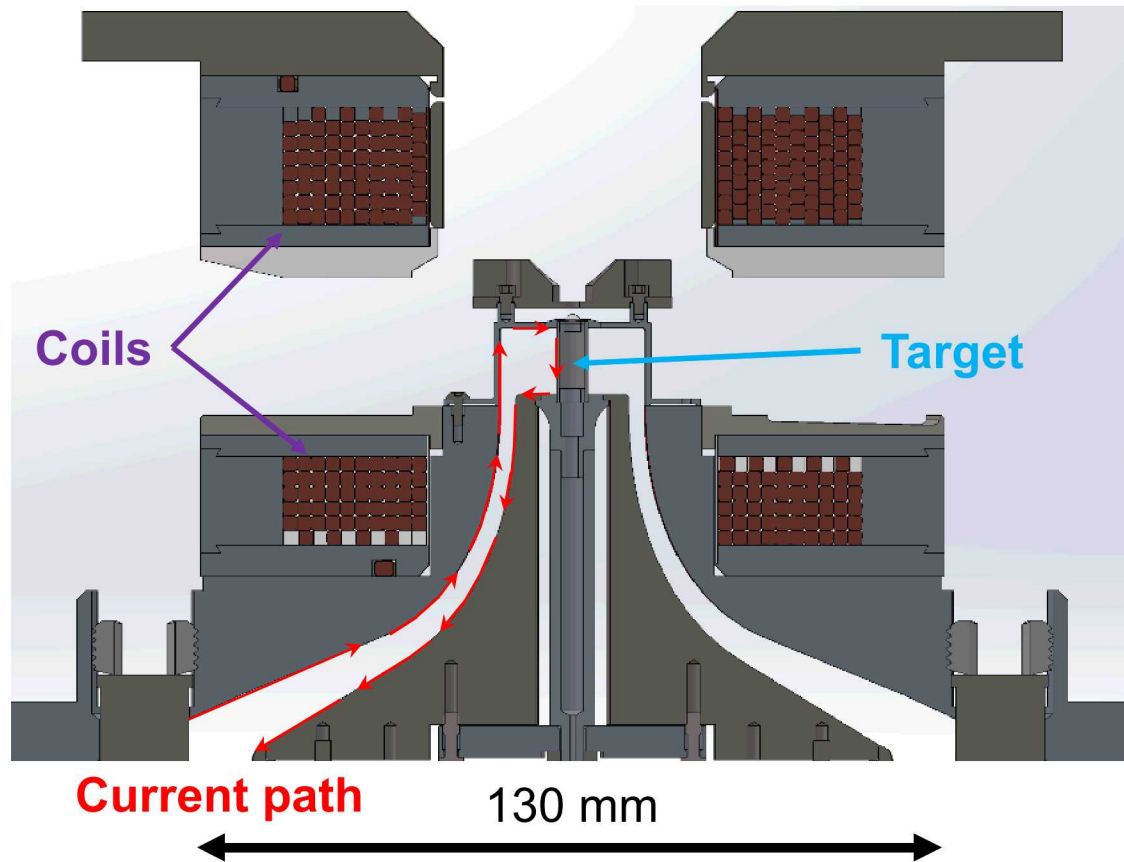
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With our initial experiments, we targeted 2 kJ, 10 T, and 18 MA



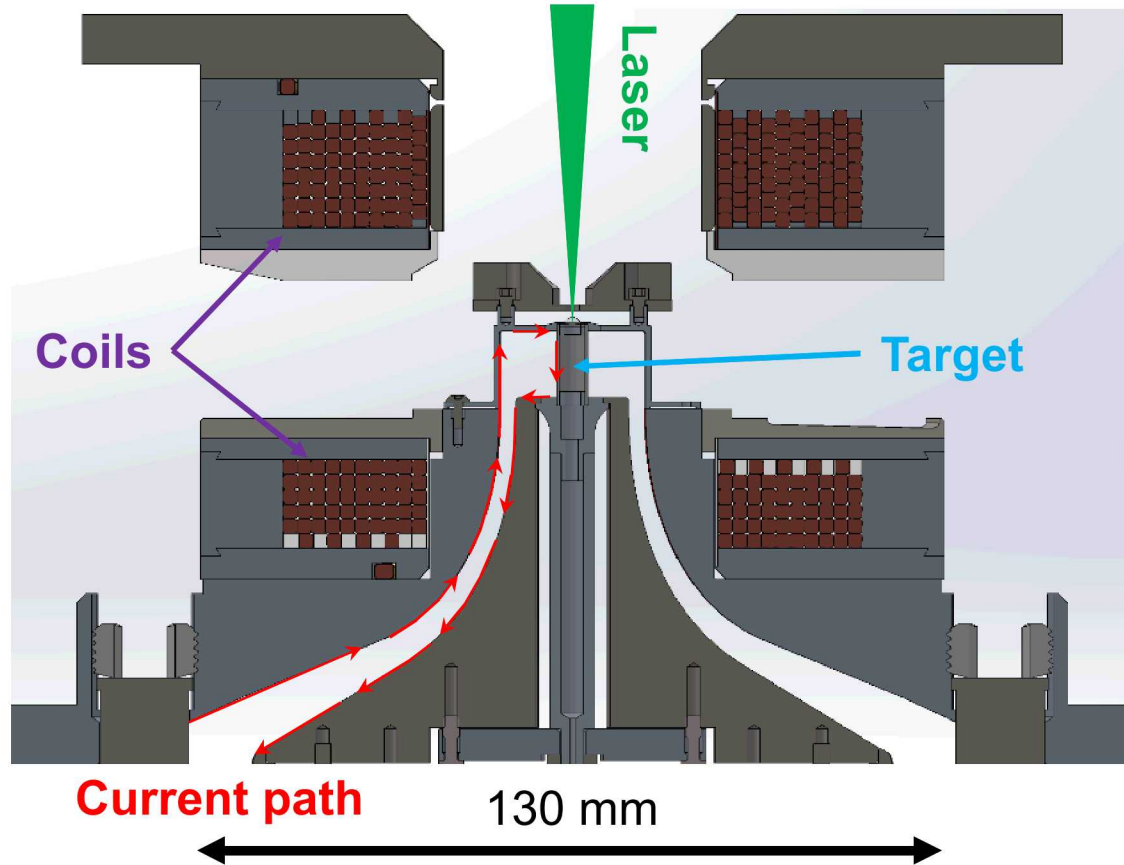
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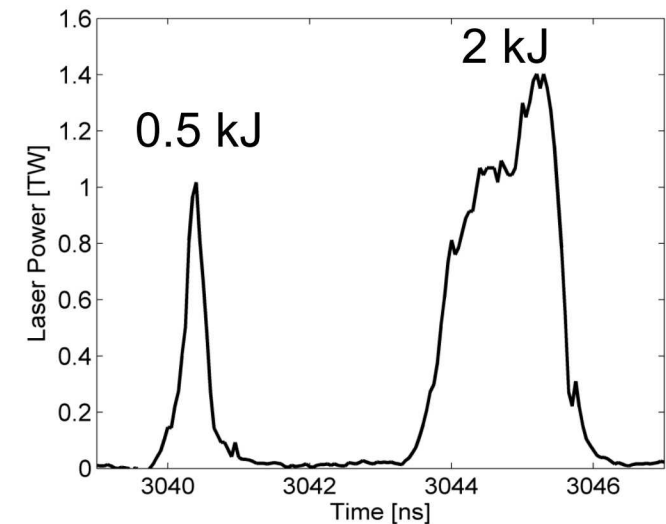


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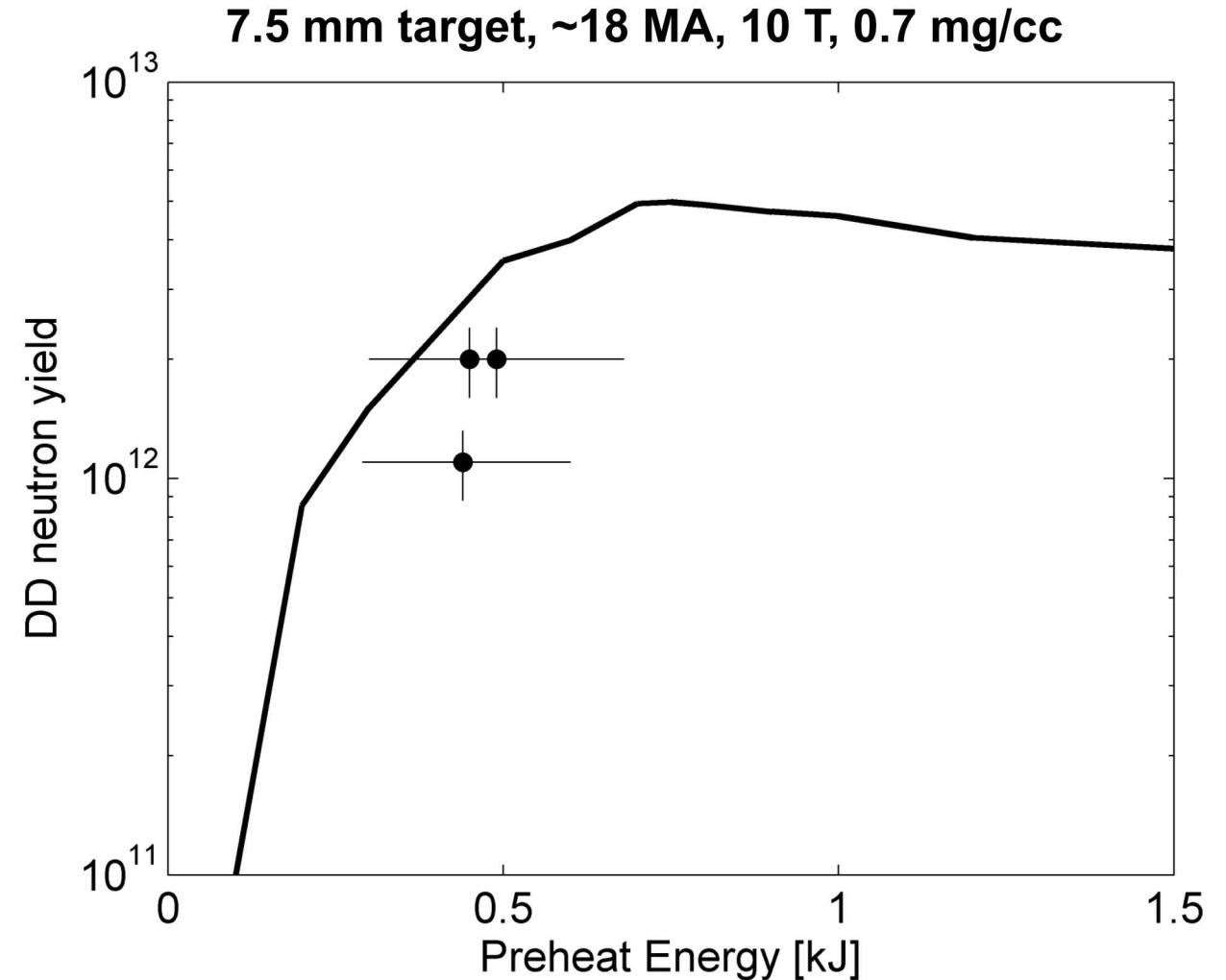
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- Only expected about 18 MA due to the high inductance inner-MITL extension required by the coils
- We believed our laser pre-pulse would disassemble the window, enabling the majority of the main pulse to be absorbed in the fuel



This configuration was predicted to produce more than 5×10^{12} DD neutrons (~ 1 kJ DT)

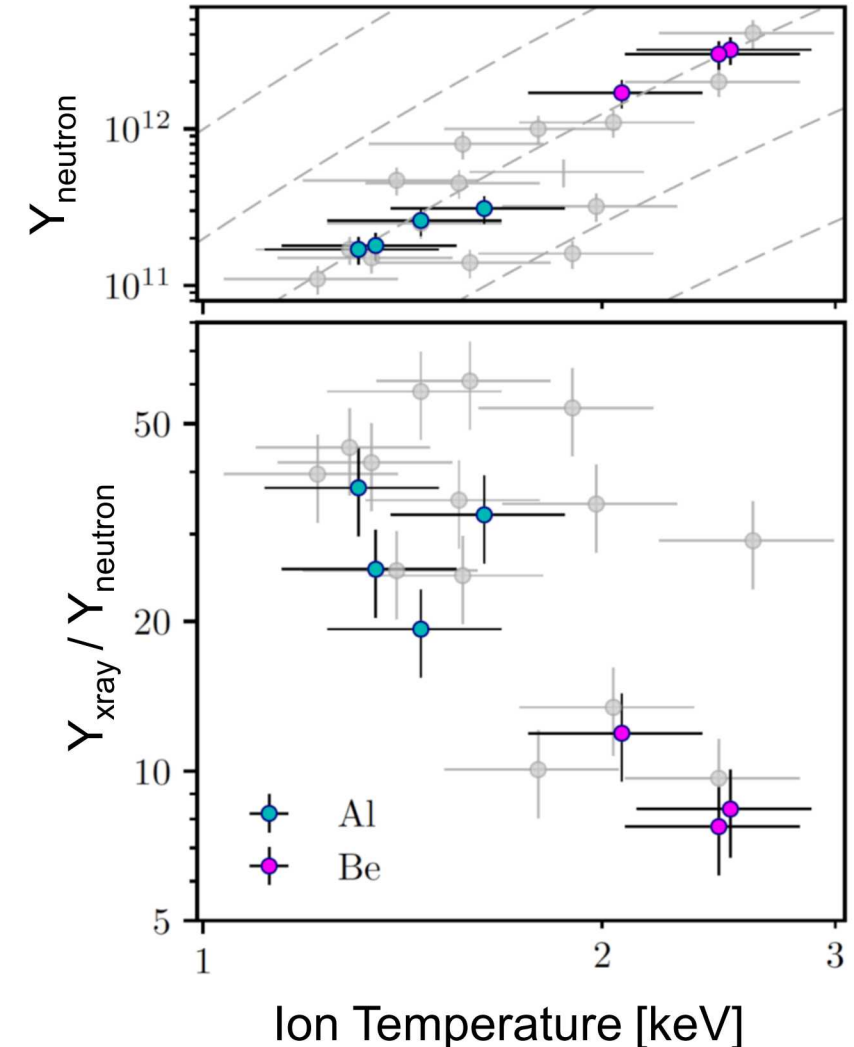
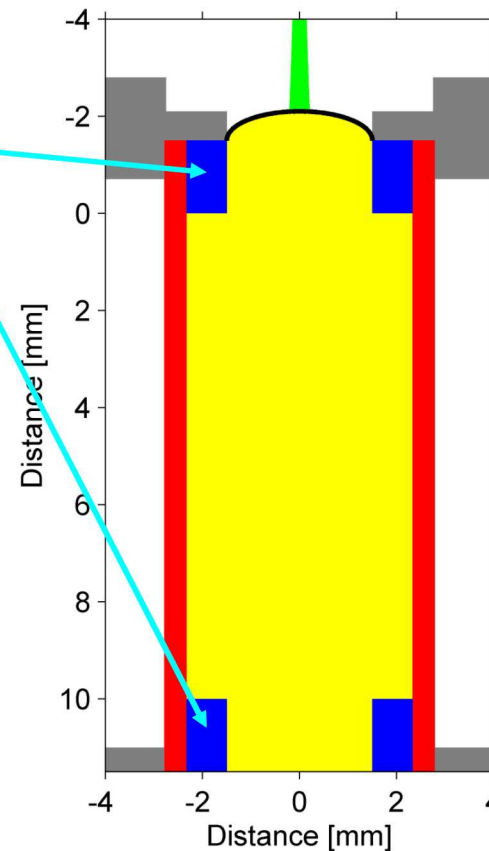
The neutron yields in the initial experiments were lower than expected

- Pre-shot neutron yield predictions were $\sim 5e12$
 - Performance is highly dependent on preheat energy
- Experimental neutron yields were about 2-4x lower than predicted
 - Consistent with low preheat energy according to simulations
 - Subsequent analysis indicates the laser energy coupled was significantly below 2 kJ, likely around 0.5 kJ
- Some of the degradation was due to low laser energy, the rest was likely due to mix and 3D effects



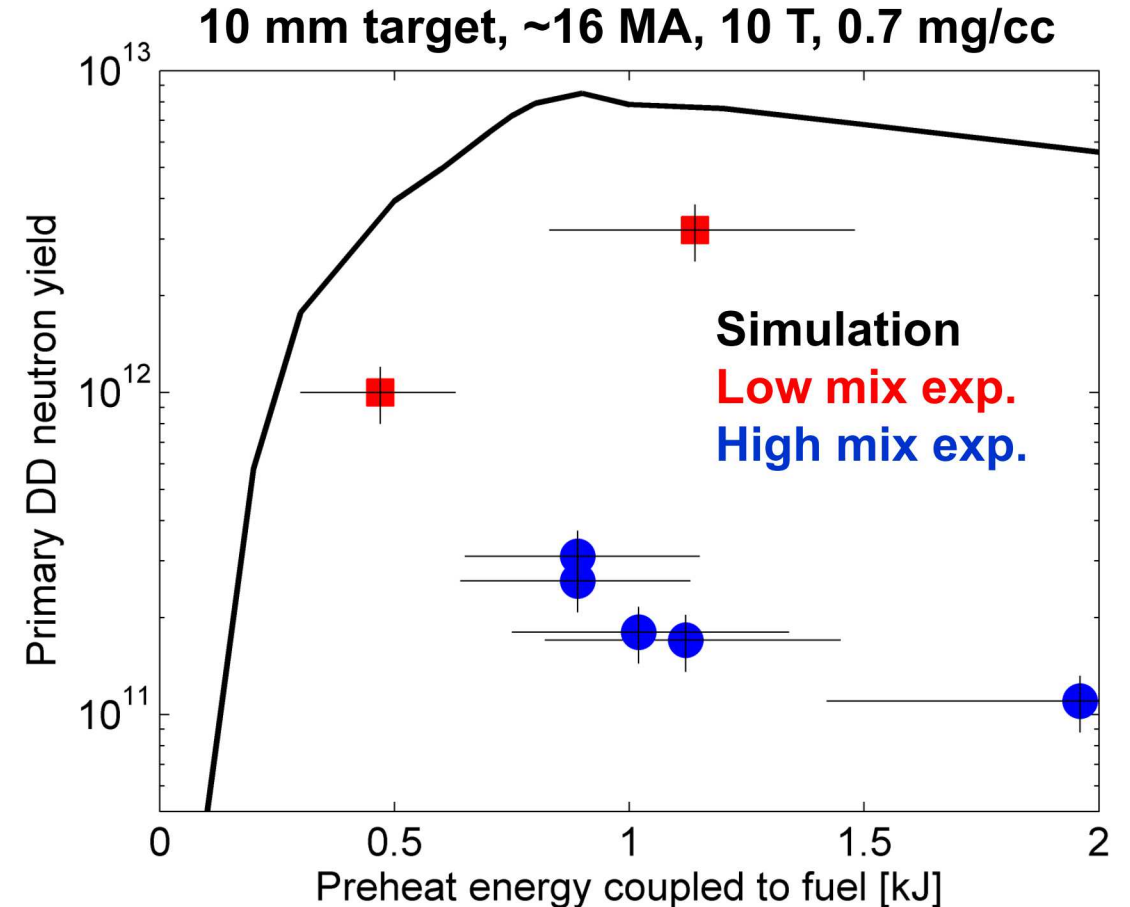
We replaced plasma-facing Al components with Be and observed record performance

- There is a significant difference between Al and Be endcaps with ~1 kJ of preheat energy
 - Neutron yield increased by an order of magnitude
 - Ratio of x-ray to neutron yield decreased by a factor of several
 - Similar mix levels, but lower Z with Be

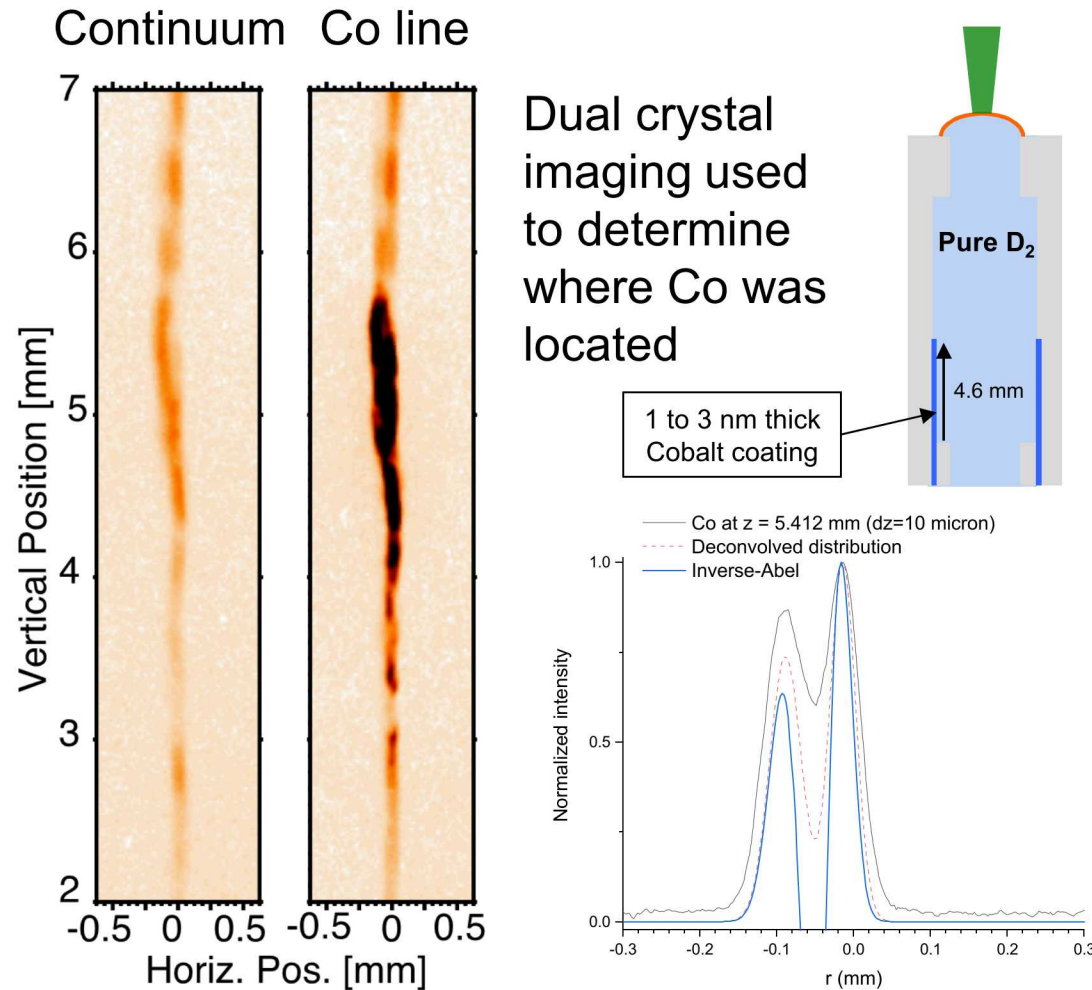


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 - Neutron yield increased by an order of magnitude
 - Ratio of x-ray to neutron yield decreased by a factor of several
 - Similar mix levels, but lower Z with Be
- We also looked at ~0.5 kJ vs ~1 kJ deposited with beryllium endcaps
 - Neutron yield increased by a factor of 2-3, similar to in clean 2D simulations
- Low mix experimental points are consistently about 50% of simulations
 - Mix and 3D effects could account for this difference



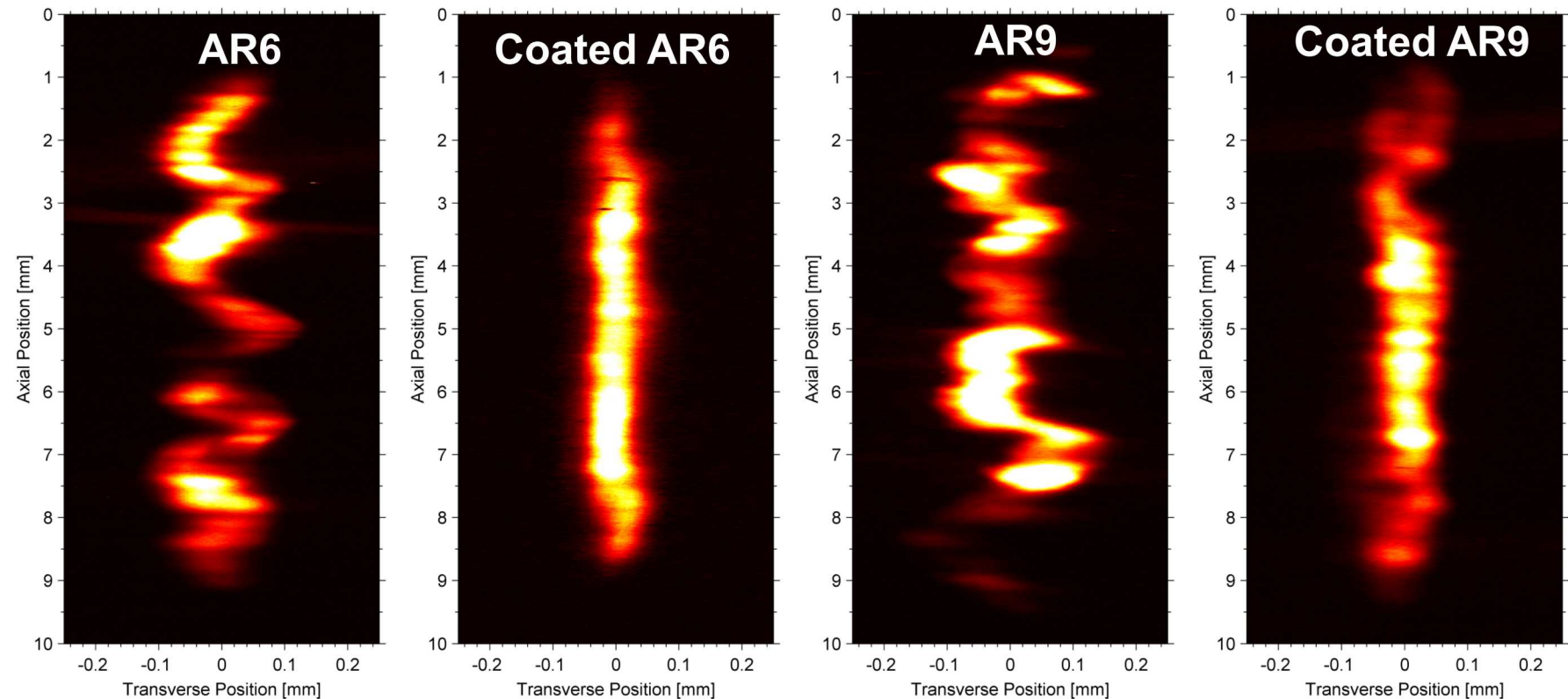
Cobalt coatings on target components were used to assess the importance of mix



- A Co coating on the top endcap resulted in Co spectral lines observed at stagnation, indicating top endcap material was mixed into the fuel
- A Co coating on the bottom endcap resulted in significantly reduced neutron yield, indicating mix from the bottom endcap is also important
- A Co coating on a portion of the inner surface of the liner resulted in axially localized mix, indicating liner mix occurs late in time, likely during the deceleration phase just before stagnation

A thick dielectric coating on the liner exterior significantly improved stagnation morphology

- Density perturbations from the electro-thermal instability seed the magneto-Rayleigh-Taylor instability
- The dielectric coating tamps the density modulations, reducing the impact of ETI
- With a dielectric coating, the helical structure at stagnation as well as the axial modulations were significantly reduced

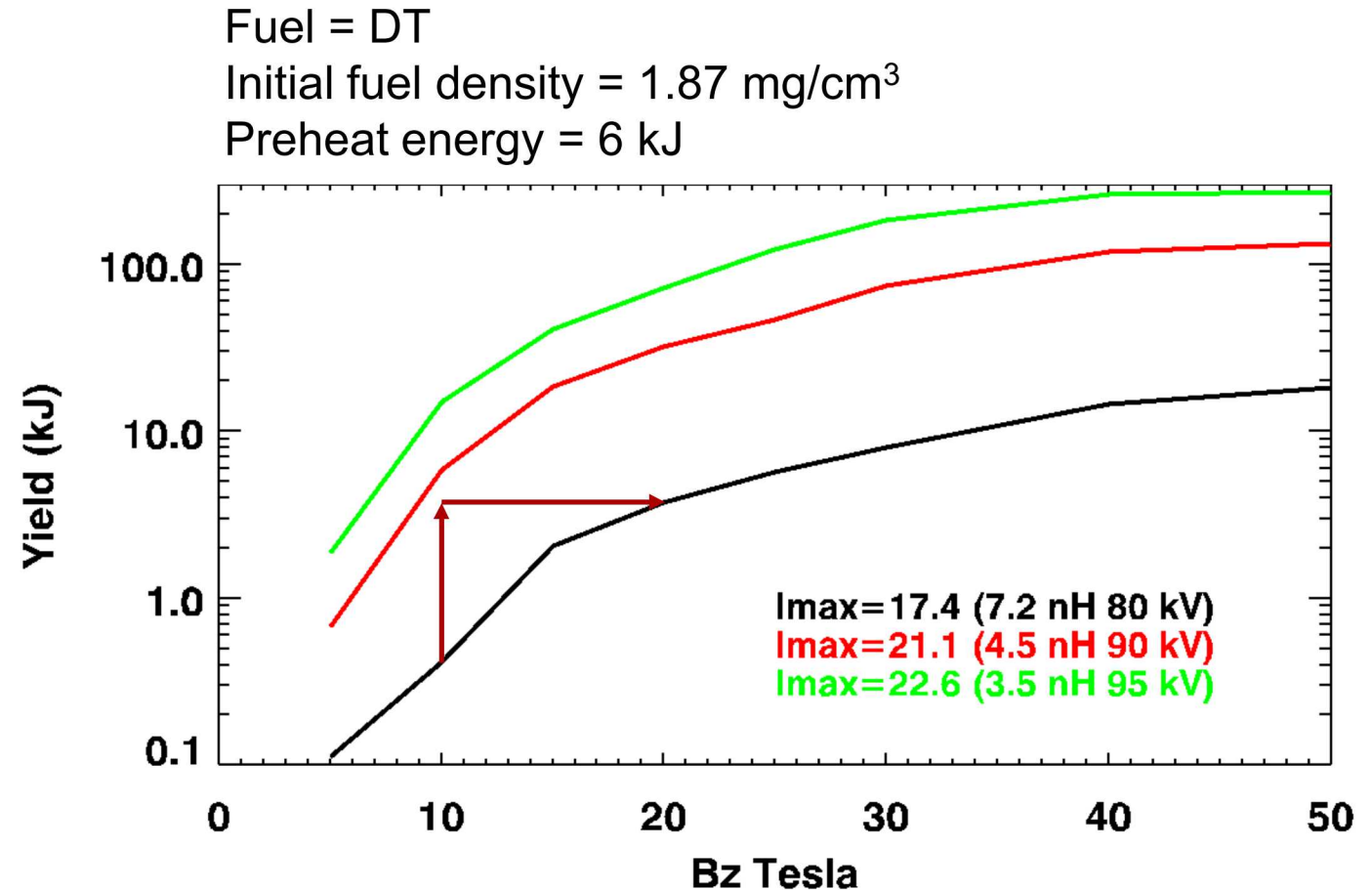


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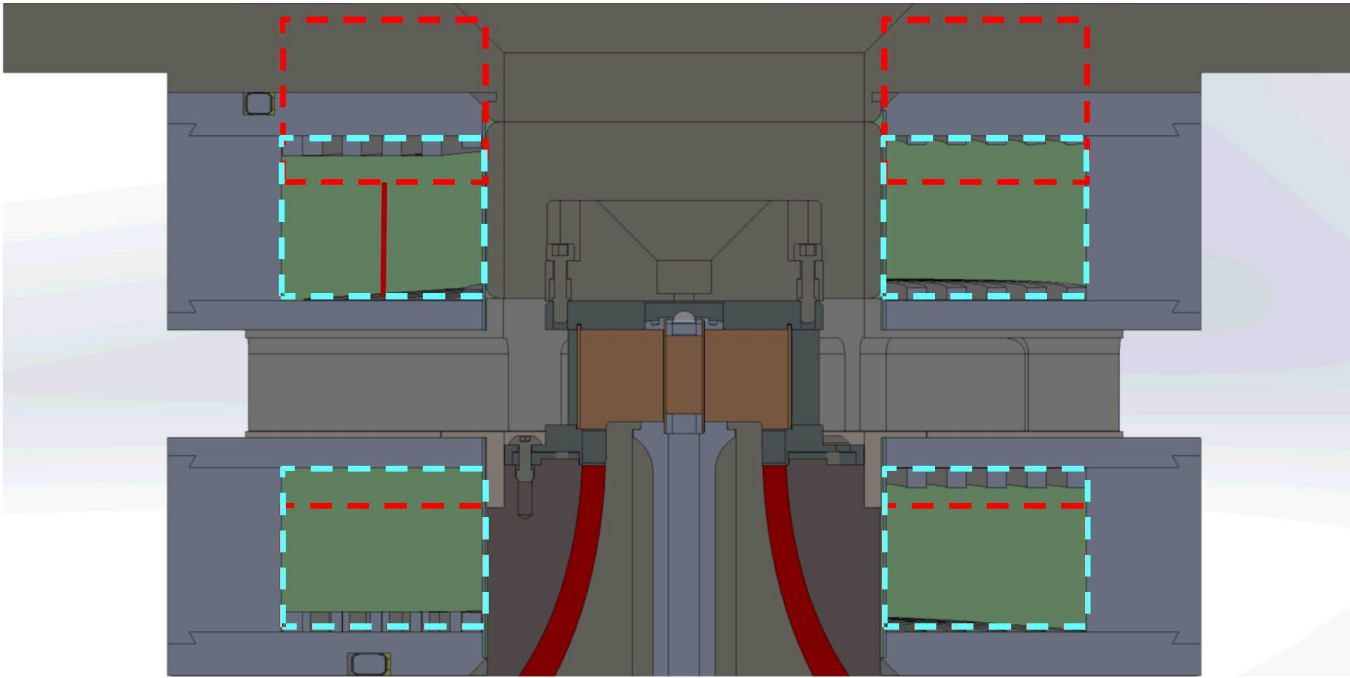
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Simulations predict the amplitude of the initial B-field has a strong impact on target performance

- Without any other changes, doubling the B-field to 20 T was expected to increase yield by about a factor of 2
- Simulations with greater laser energy deposition show an even stronger dependence
 - Nearly an order of magnitude increase in yield with 6 kJ of laser energy and 1.87 mg/cm^3 DT



The B-field was increased with modest change in coil configuration resulting in record performance

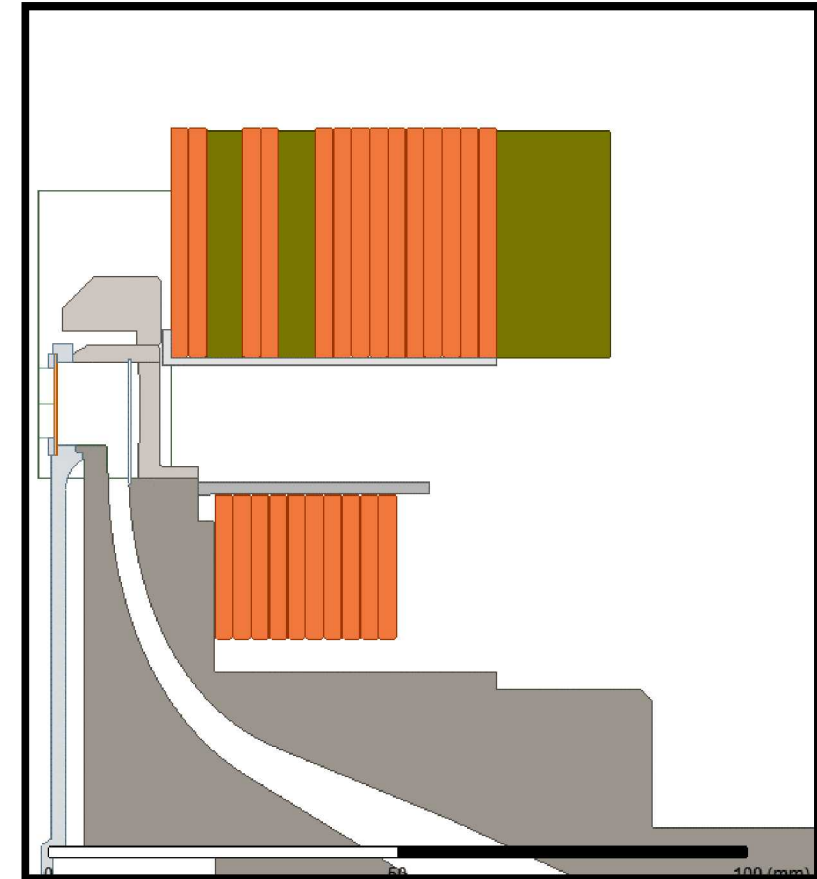


- Bottom coils increased from 60 turns to 80 turns
- Top coils lowered by 15 mm, eliminating 12 degree x-ray diagnostic access

- Applied B-field was increased from 10 to 15 T
- Simulations predicted an increase in primary neutron yield of about 1.5x
- **Experimental yield increased by 1.7x from 3.1e12 to 5.5e12**
- DD/DT yield ratio decreased to ~50, which is an indication of increased magnetization at stagnation

New coil and target designs could allow 25 T operation without giving up diagnostic access

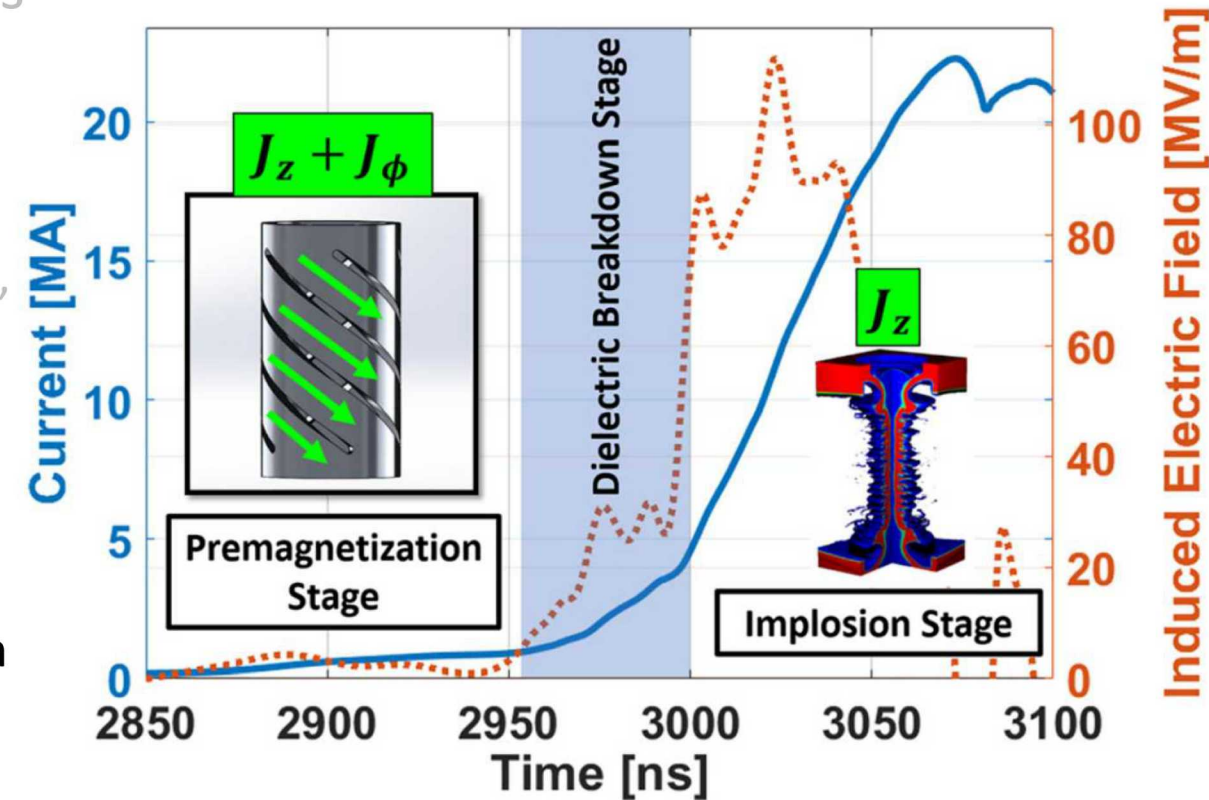
- Exceeding 15 T requires developing new coil configurations or giving up diagnostic access
 - A larger top coil, which enables 20 T with diagnostic access, was developed during 2017 and tested earlier this year
 - A new bottom coil could further increase B-field, but this MITL configuration is not compatible with >20 MA, so we have not pursued this
- Auto-Mag is an alternative path to high magnetic fields
 - Helical conducting paths in the liner generate an axial B-field in the target using Z's current
 - >50 T was demonstrated on Z in early 2018
 - Implosion stability is still under investigation



80-turn Coil + Low-L Coil
20 – 22T avg. field in Standard Feed
(~17 MA drive current)

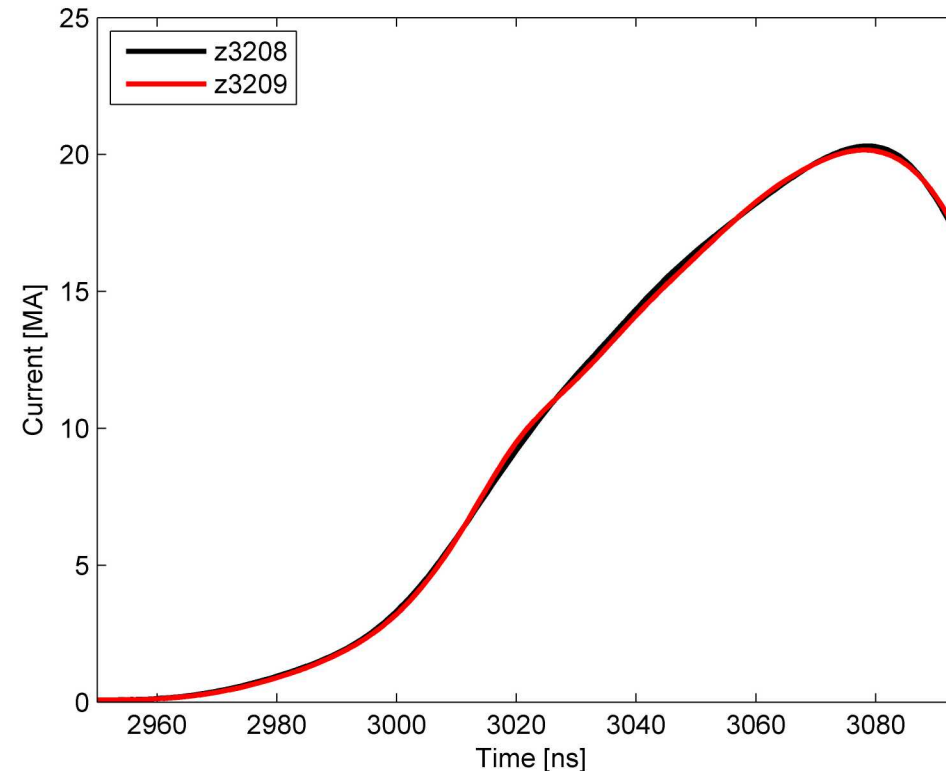
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 - A new bottom coil could further increase B-field, but this MITL configuration is not compatible with >20 MA, so we have not pursued this
- Auto-Mag is an alternative path to high magnetic fields
 - Helical conducting paths in the liner generate an axial B-field in the target using Z's current
 - >50 T was demonstrated on Z in early 2018
 - Implosion stability is still under investigation



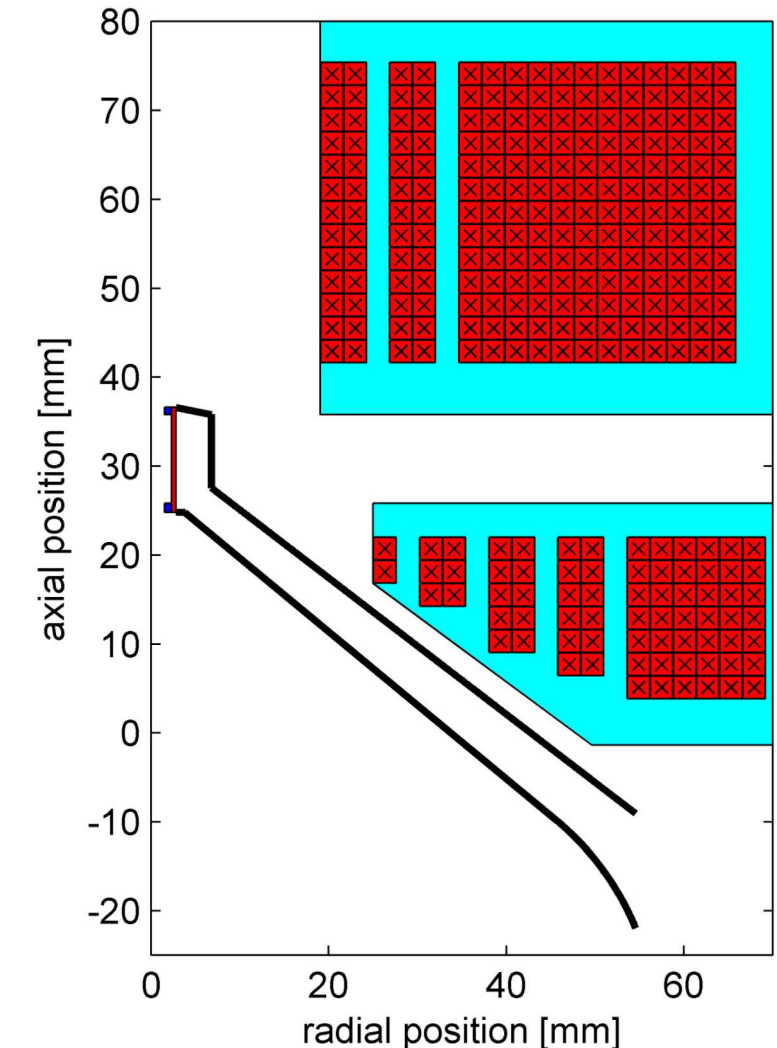
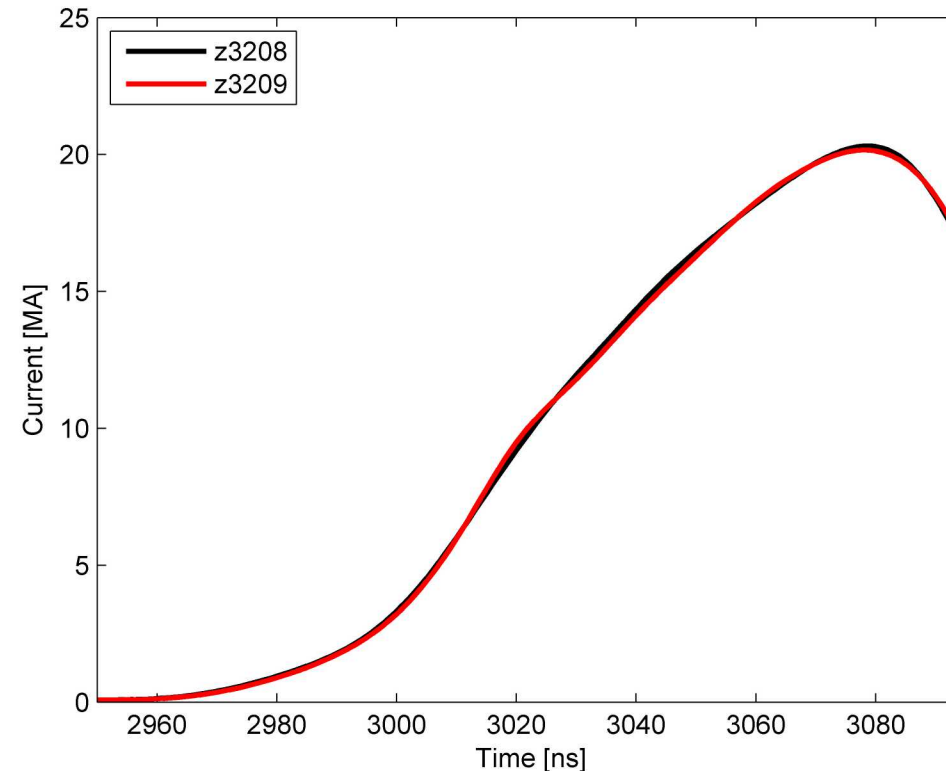
A reduction of the load inductance led to a new record load current

- 20 MA has been demonstrated
- 22 MA seems plausible with small modifications

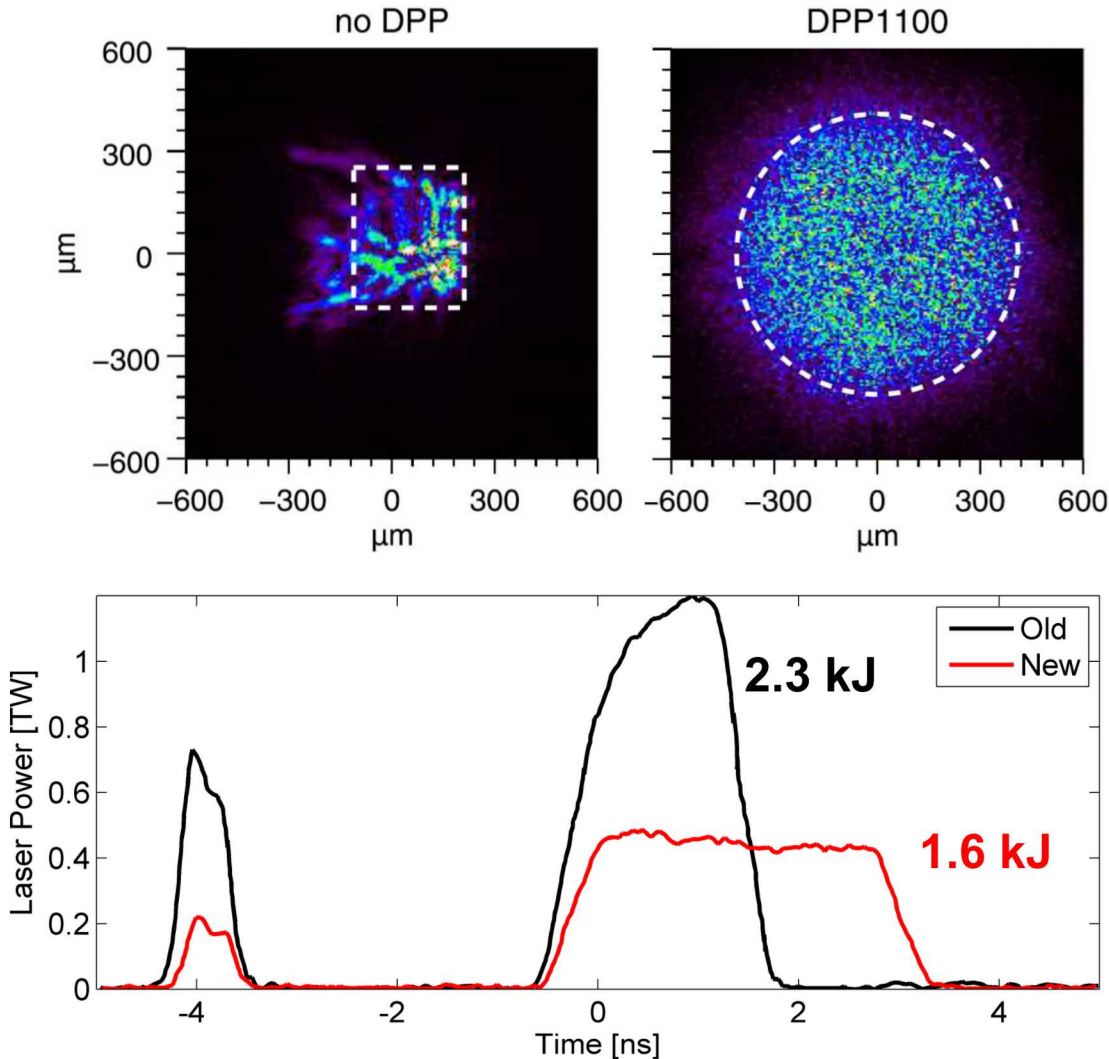


A reduction of the load inductance led to a new record load current

- 20 MA has been demonstrated
- 22 MA seems plausible with small modifications
- This configuration is also compatible with >20 T operation
 - Requires new bottom coil development

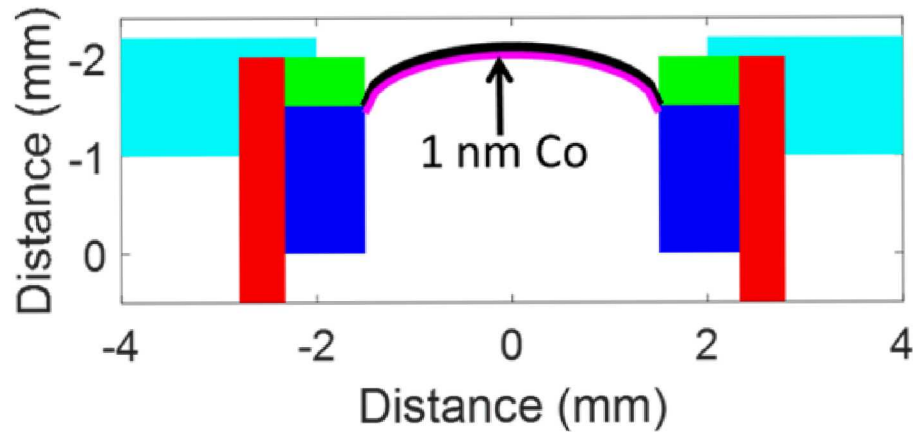


Laser coupling was improved using a new pulse shape and a phase plate to smooth the beam



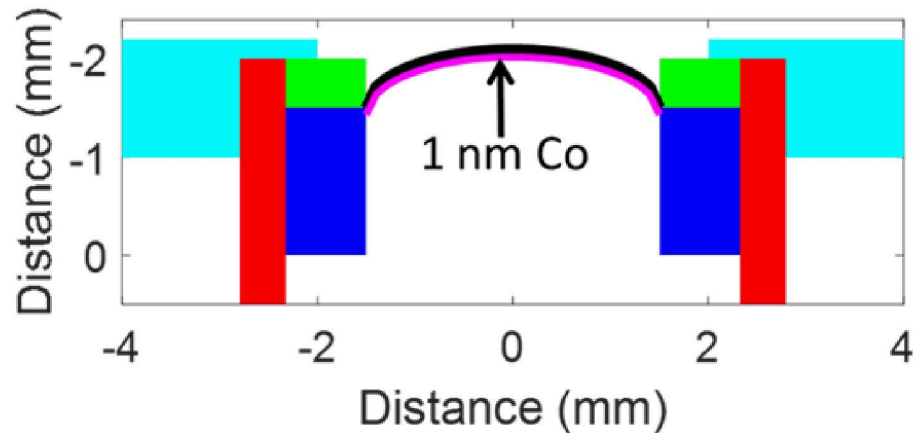
- Decreased laser power and larger spot size significantly decreased the laser intensity and laser plasma instability losses
- Goal was to couple a similar amount of energy in a more efficient, reliable way
 - Minimal change in energy coupled to fuel but efficiency improved significantly
- Observed an increase in yield from $3e12$ to $4e12$ but also observed an increase in mix
- Suspected that window mix was important so we developed a technique to measure window mix spectroscopically

A cobalt tracer on the LEH window was used to track the depth of window mix

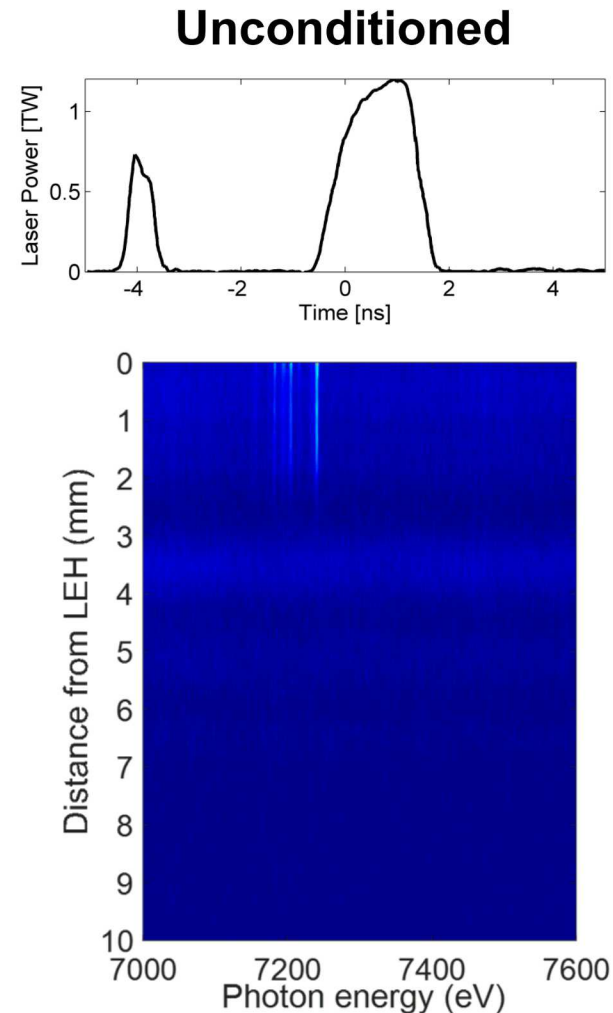


- Looking for Co K-shell emission at stagnation

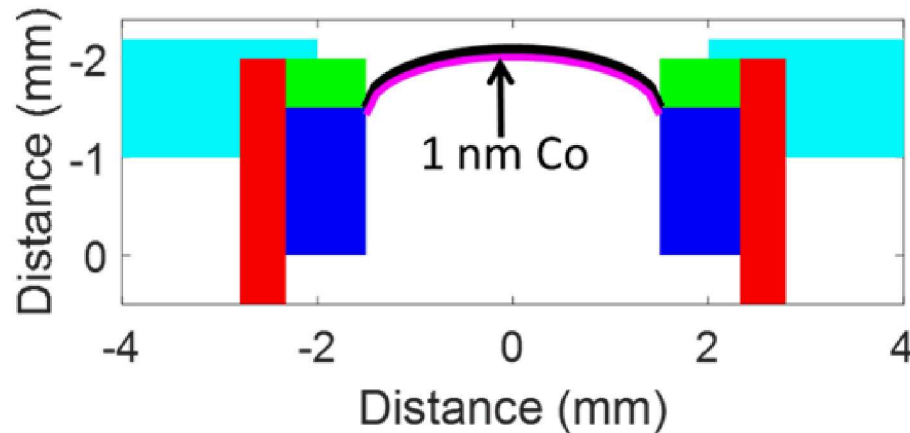
A cobalt tracer on the LEH window was used to track the depth of window mix



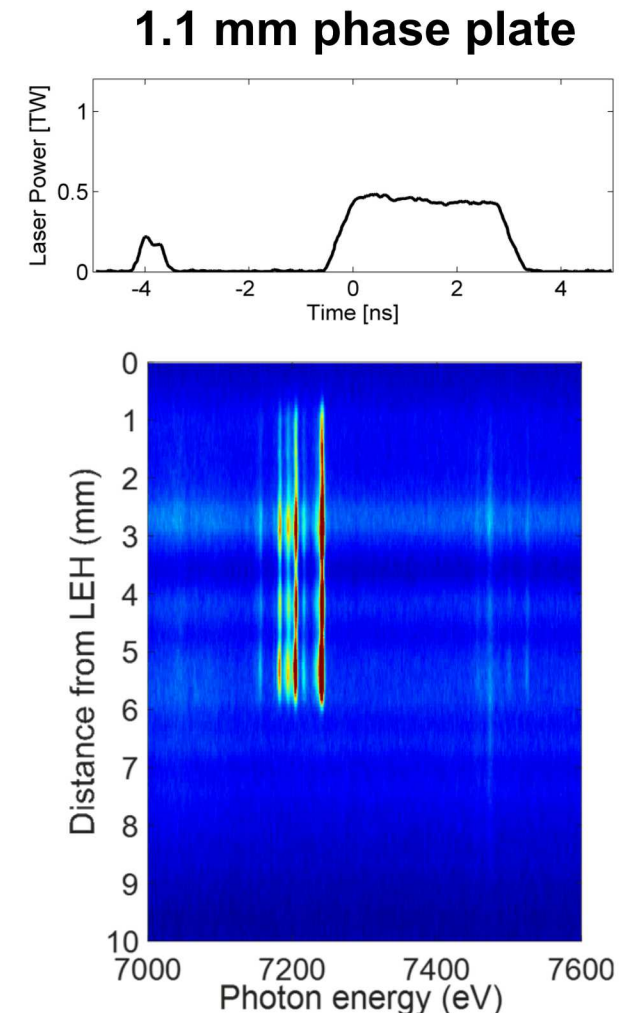
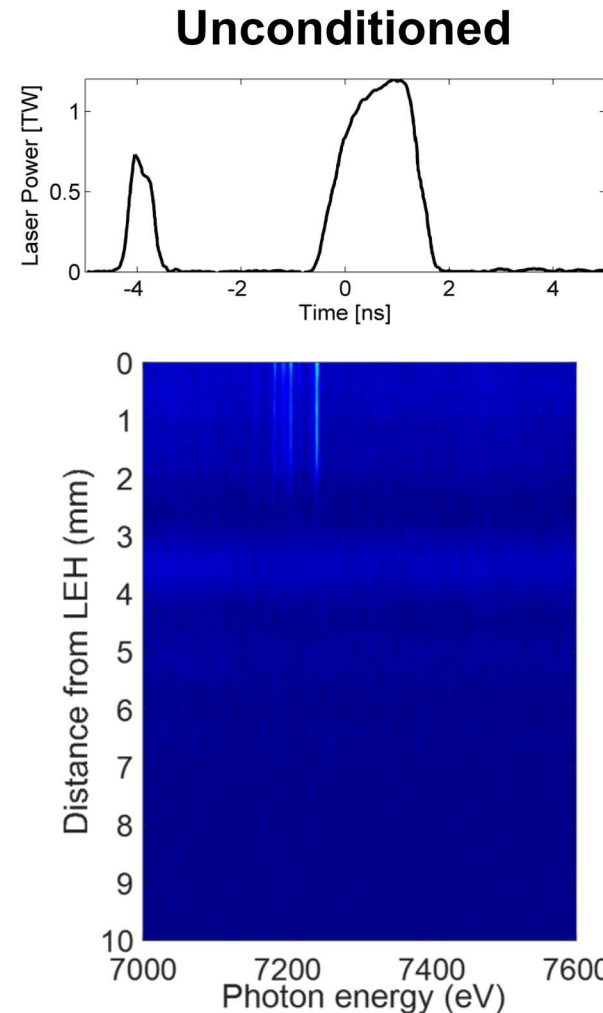
- Looking for Co K-shell emission at stagnation
- Window mix was observed in the top 3 mm of the target with the old laser configuration



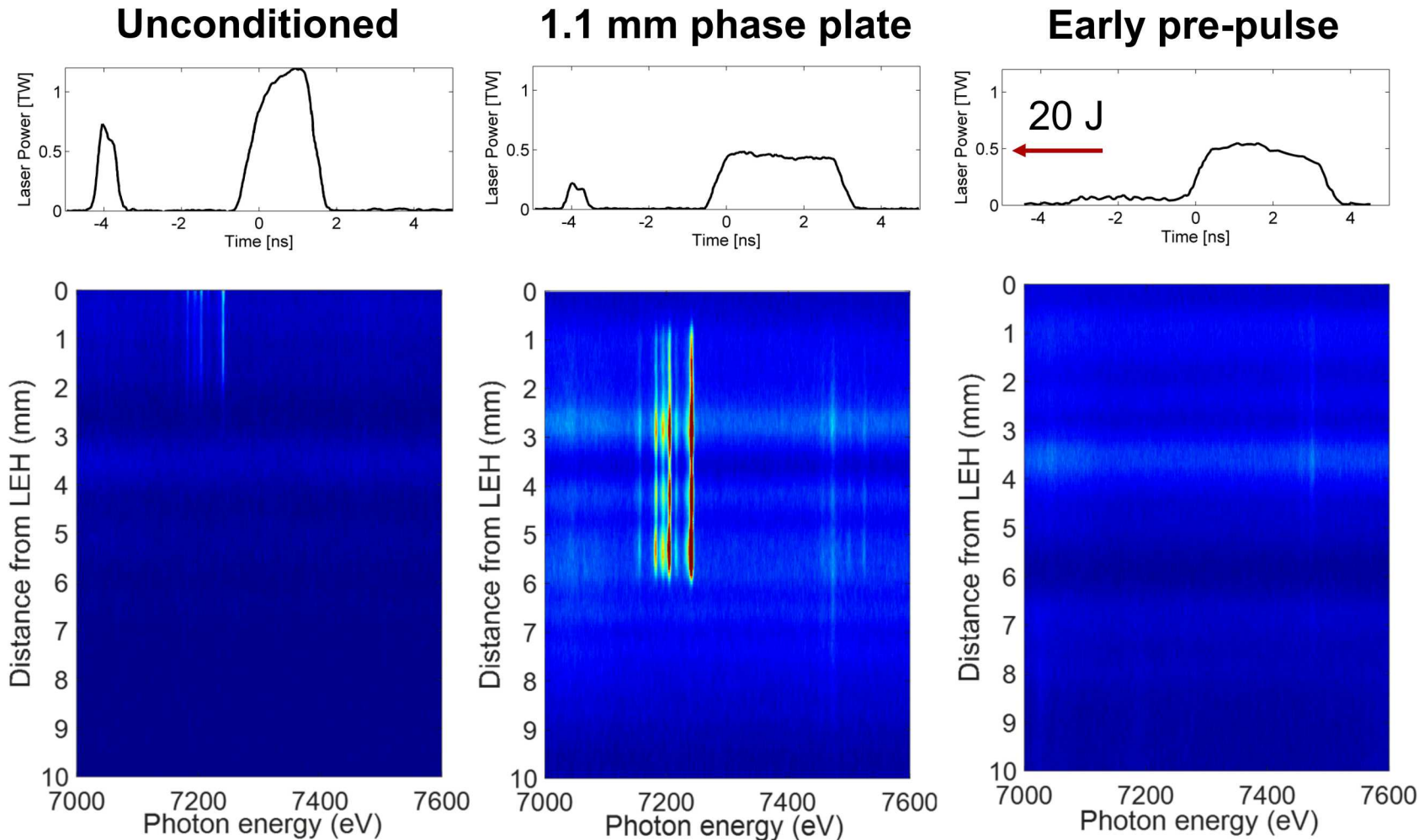
A cobalt tracer on the LEH window was used to track the depth of window mix



- Looking for Co K-shell emission at stagnation
- Window mix was observed in the top 3 mm of the target with the old laser configuration
- The new laser configuration with the 1.1 mm DPP injected window mix into the top 6 mm of the target!



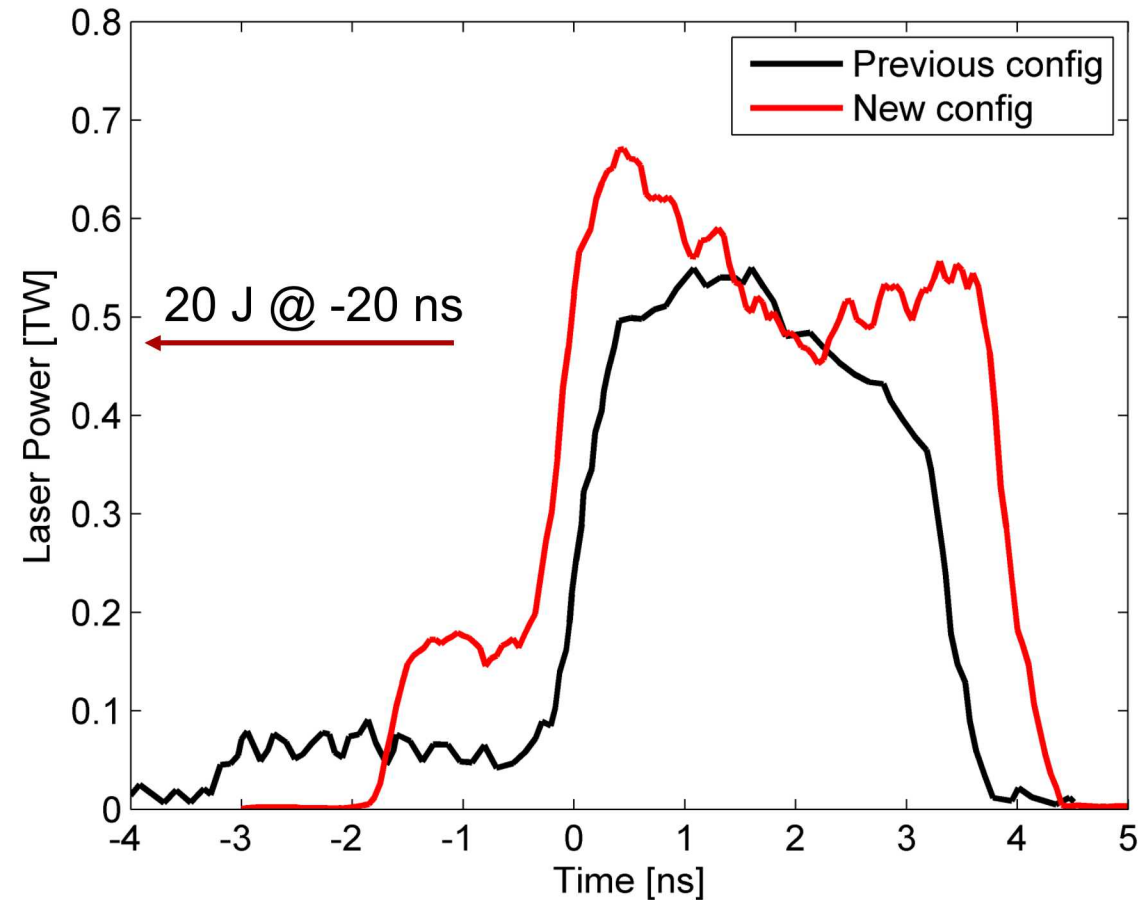
Simulations predicted a small change in laser pulse shape would greatly reduce window mix



- Early pre-pulse configuration utilizes a 20 J pre-pulse approximately 20 ns early and a low intensity foot
 - 1.1 mm phase plate used
- Couples ~1 kJ to the fuel out of 1.8 kJ
- Slight increase in laser energy coupled to fuel with substantially less mix

A higher energy version of this new laser configuration produced record performance

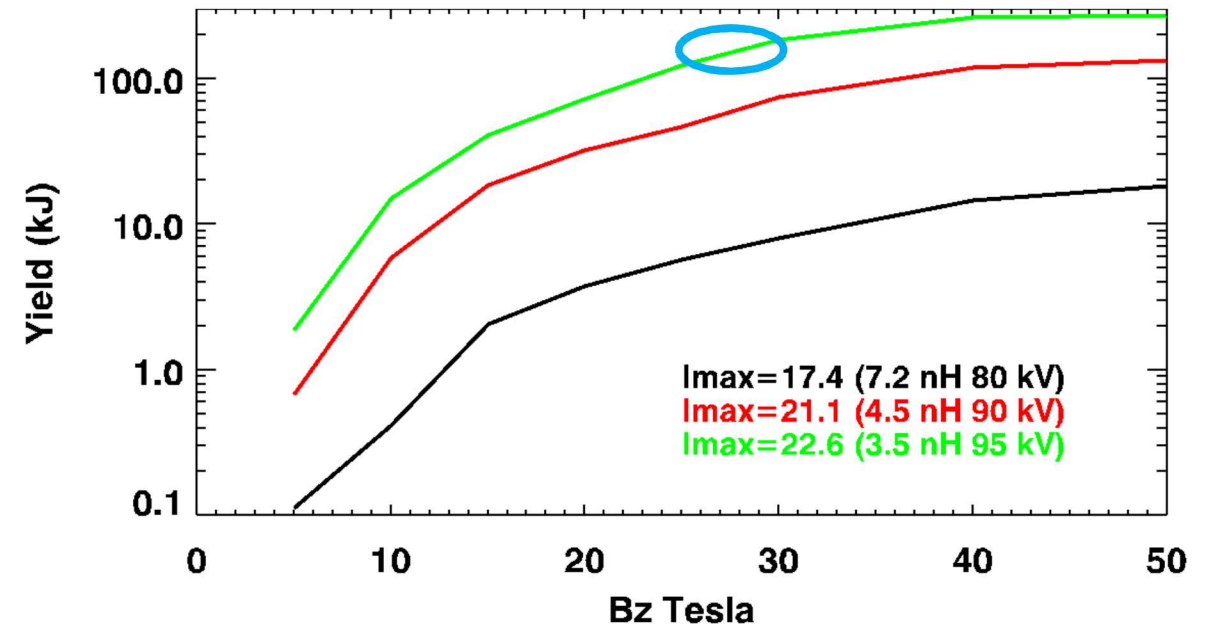
- Used the same low energy, very early pre-pulse to convert the window to plasma
- Shorter, higher intensity foot allowed more energy in the main pulse
 - 2500 J total energy
 - 1200-1400 J coupled
- **New record DD neutron yield of $1.1e13$**
 - About 3x increase from $3.3e12$
 - Minimal increase in mix from window
 - Used coated-AR9 target configuration



Our goal on Z is to produce a fusion yield of ~100 kJ DT-equivalent

- 2D simulations indicate an experiment with 22 MA, 25-30 T, and 6 kJ of laser heating could produce >100 kJ
- Presently we cannot produce these inputs simultaneously
- We are making progress in demonstrating scaling

Preheat Energy = 6 kJ into 1.87 mg/cc DT



Date	Liner	Fill (D2)	Current	B-field	Preheat	Yield (DT-eq.)
2014	AR=6	0.7 mg/cm ³	17-18 MA	10 T	0.2-0.6 kJ	0.2-0.4 kJ
Aug. 2018	AR=6	1.1 mg/cm ³	19-20 MA	15 T	1-1.4 kJ	~2.4 kJ
2020 Goal	TBD	~1.5 mg/cm ³	20-22 MA	20-30 T	2-4 kJ	~10 kJ
Z Goal	TBD	1.5 mg/cm ³	22 MA	25-30 T	6 kJ	100 kJ

Outline

- Introduction to magneto-inertial fusion
 - Intro to Magnetized Liner Inertial Fusion (MagLIF)
- MagLIF experiments
 - Demonstration of the efficacy of magneto-inertial fusion
 - Improving target behavior
 - Identifying scaling trends
- **Next generation experiments**
 - **Architecture of a next-generation pulsed power driver**
 - **Scaling to future drivers**

We are exploring a modular architecture that is twice as electrically efficient as the Z machine

Brick – “quantum” of next generation driver designs

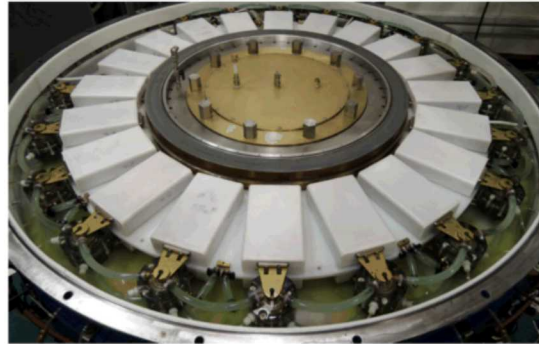


5.2 GW/800 J per brick

Brick design is similar to what was used in early LTD designs

The overall inductance was lowered with a new switch design, and the capacitance was increased

Cavity – multiple bricks connected in parallel

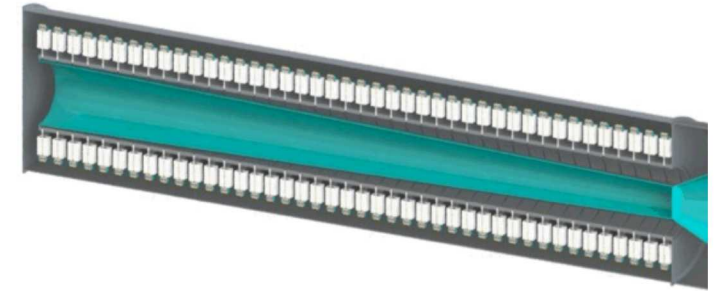


>100 GW/1.6 kJ per cavity

Each brick delivers 50 kA to a matched load

The full cavity delivers 1 MA at 100 kV to a matched load (assuming 20 bricks)

Module – multiple cavities connected in series



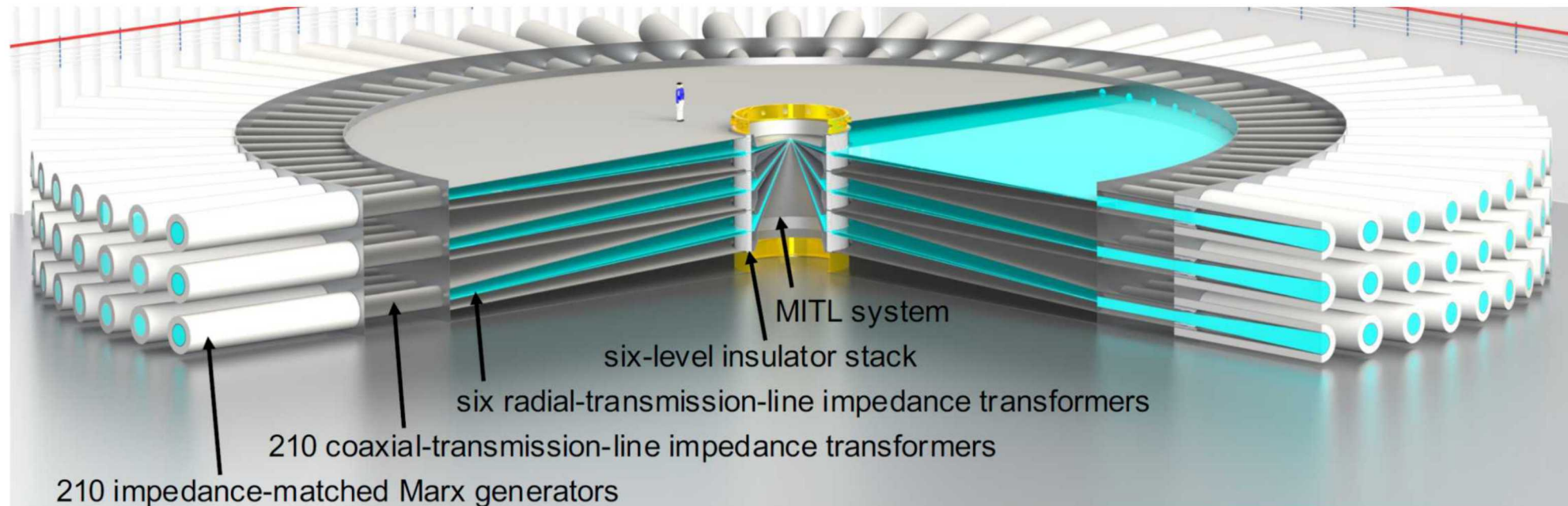
>4 TW/>0.67 MJ per module

Voltage is increased by stacking cavities in series

A full module delivers 1 MA at 4.2 MV to a matched load (assuming 42 cavities)

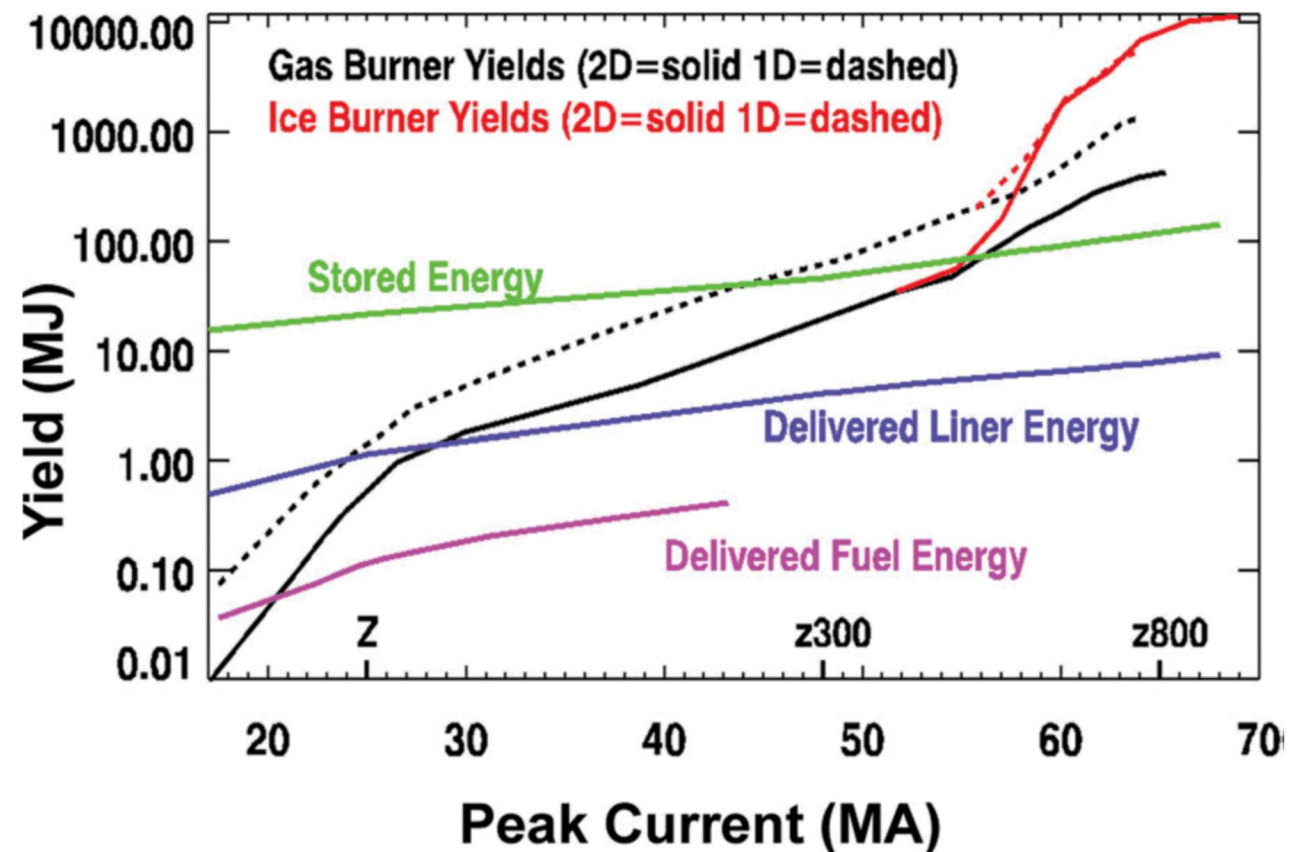
Conceptual designs for a 960 TW next-gen. pulsed power driver are being developed

- 210 modules, each consisting of 42 cavities, which contain 20 bricks
- Total of over 350,000 capacitors and 175,000 switches
- This design utilizes impedance-matched Marx generators as opposed to LTDs
- The generator diameter would be 72 m (over twice that of Z)
- Energy stored: 141 MJ
- Nominal rise-time: 100 ns
- Pulse-shaping possible



MagLIF scaling calculations were conducted to assess performance on a next-generation driver

- Between 50 and 60 MA the predicted yield in 2D exceeds 100 MJ
 - The fusion energy also exceeds the stored energy of the driver in this range
- These calculations were conducted assuming negligible current loss, so the points for next generation 300 TW and 800 TW drivers should be shifted to lower currents
- At 60 MA, the ideal B-field reduces to about 15 T but the ideal laser heating energy is ~60 kJ with an initial fuel density around 10 mg/cm^3



We are pursuing a path to enable the generation of multi-MJ fusion yields in the laboratory

- Our goals for the next 5 years:
 - Demonstrate understanding of the MagLIF concept
 - Expand our capabilities and continue to investigate scaling with applied B-field, laser energy coupling, and load current
 - Begin development of a full module for a next-generation pulsed power driver
 - ~40 cavities – ~1 MA at >4 MV
 - Develop next-generation simulation tools to better predict power flow delivery to the target as well as improve target simulations
 - High resolution, 3D, beyond MHD physics

Thank you for your attention

Questions?