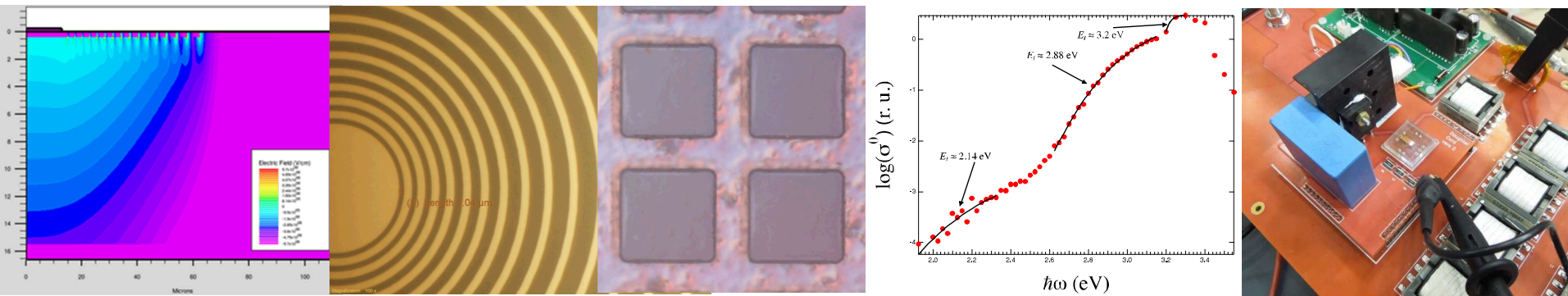


Wide- and Ultra-Wide-Bandgap III-N Semiconductors for Power Electronics



Presented by:

Bob Kaplar

**Principal Member of the Technical Staff
Sandia National Laboratories**

Presented to:

**The Ohio State University
Department of Electrical Engineering**

June 26, 2015

Acknowledgements

I'd like to acknowledge Sandia's entire Ultra-Wide-Bandgap Grand Challenge team (~50 people). Unfortunately not everyone can be listed here; key contributors include:

- **Epitaxy thrust: Andy Allerman**
- **Defect physics thrust: Andy Armstrong**
- **Vertical devices thrust: Jon Wierer**
- **Lateral devices thrust: Albert Baca**
- **Device test thrust: Jason Neely**
- **Management: Jerry Simmons, Rick Schneider, Olga Spahn, Carol Adkins, Vipin Gupta**

I'd also like to thank Prof. Siddharth Rajan for inviting me to give the talk

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- **Introduction and motivation**
 - Introduction to Sandia
 - Motivation for WBG/UWBGs in power electronics
- **Vertical devices**
 - GaN PiN diode design and fabrication
 - Doping and defect physics in GaN drift regions
 - $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ PiN diodes
- **Lateral devices**
 - Al-Rich $\text{Al}_x\text{Ga}_{1-x}\text{N}/\text{Al}_y\text{Ga}_{1-y}\text{N}$ heterostructures

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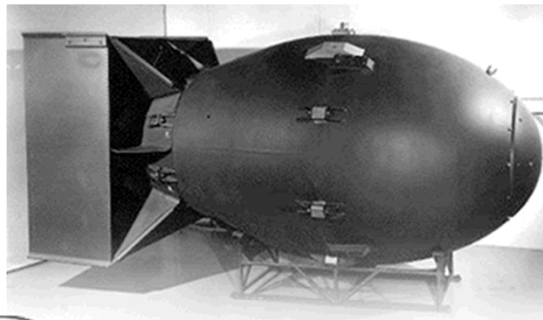
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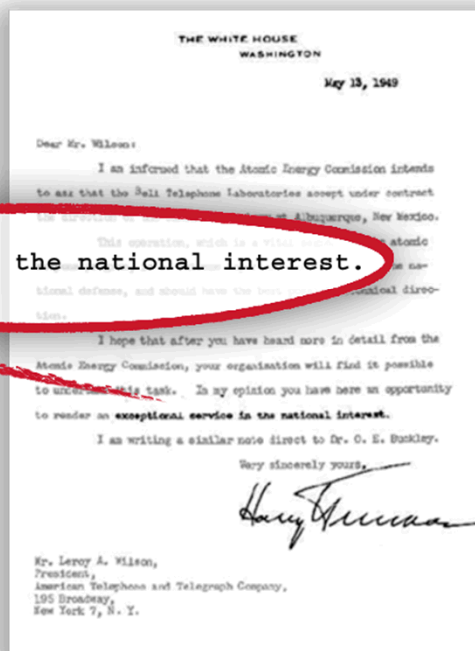
➤ Lateral devices

- Al-Rich $\text{Al}_x\text{Ga}_{1-x}\text{N}/\text{Al}_y\text{Ga}_{1-y}\text{N}$ heterostructures

Sandia's History



exceptional service in the national interest.



Sandia's Sites

**Albuquerque,
New Mexico**



**Livermore,
California**



Tonopah, Nevada



**Waste Isolation Pilot Plant,
Carlsbad, New Mexico**



Pantex, Texas



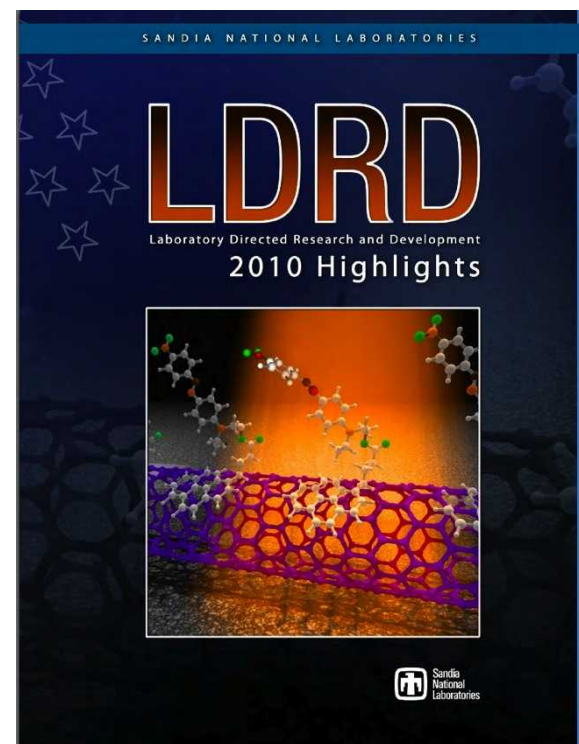
Kauai, Hawaii



Sandia's LDRD Program

➤ *LDRD: Laboratory Directed Research and Development*

- Sandia's sole source of discretionary R&D funds
- Purpose is "to create...the development of a technical expertise within programs deemed by Sandia Management as important to the future of the Laboratories, DOE, and the nation"
- "Grand Challenge" is a special class of LDRD; typically two new starts per year, ~15 full-time equivalent staff



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Power Electronics are Ubiquitous

Satellites



Electric ships



UAVs



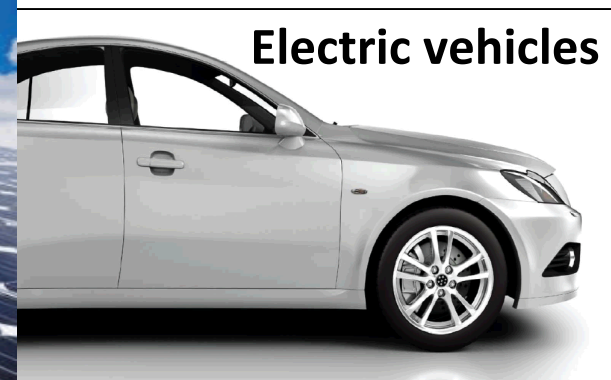
Transmission



Photovoltaics



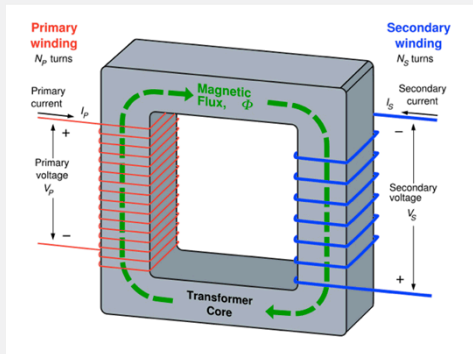
Electric vehicles



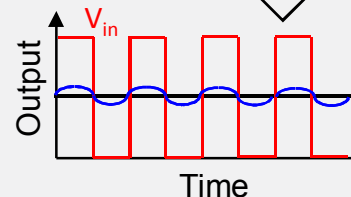
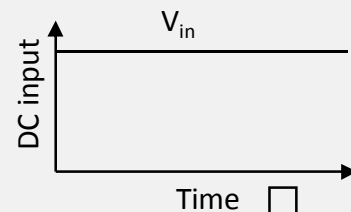
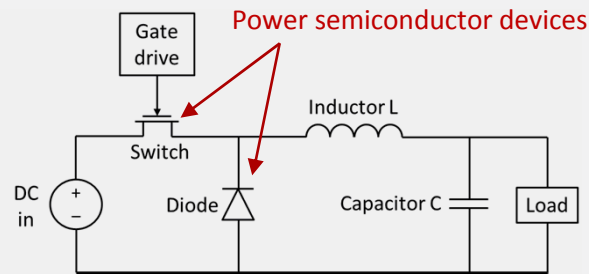
What Are Power Electronics?

- **Power electronics:** Application of solid-state electronics for routing, control, and conversion of electrical power

Passive transformers (dumb)



Power Electronics – Active switching (smart)



- Current power electronics are limited by the properties of silicon semiconductor devices
- New system capabilities are enabled by:

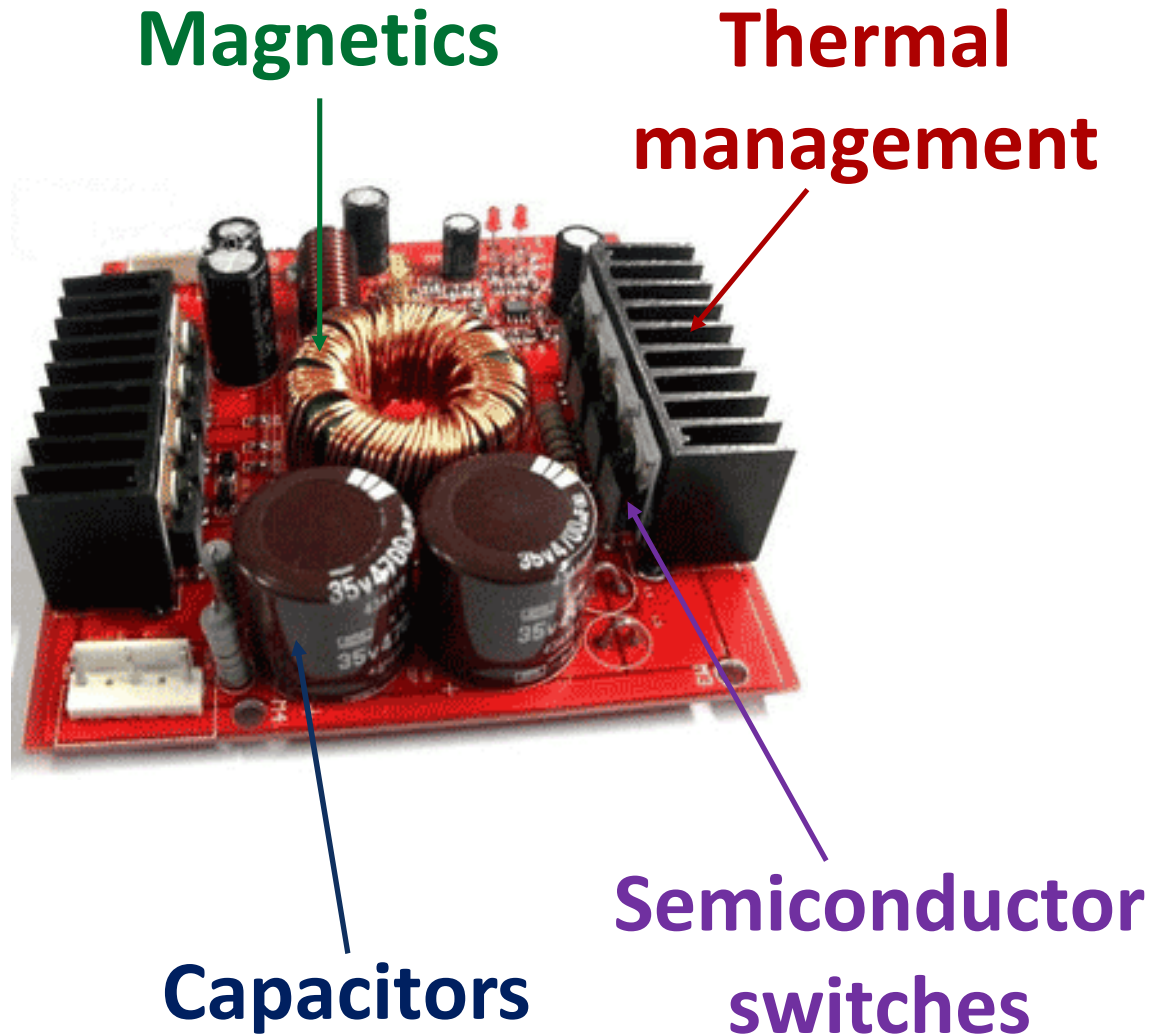
- Higher switching frequency (enables better SWaP)
- Lower power loss
- Higher temperature operation

➤ **Motivation for WBG/UWBG semiconductors**

Semiconductor Devices Dictate System Volume and Weight

Passive elements and thermal management comprise the bulk of the volume and mass of a power converter

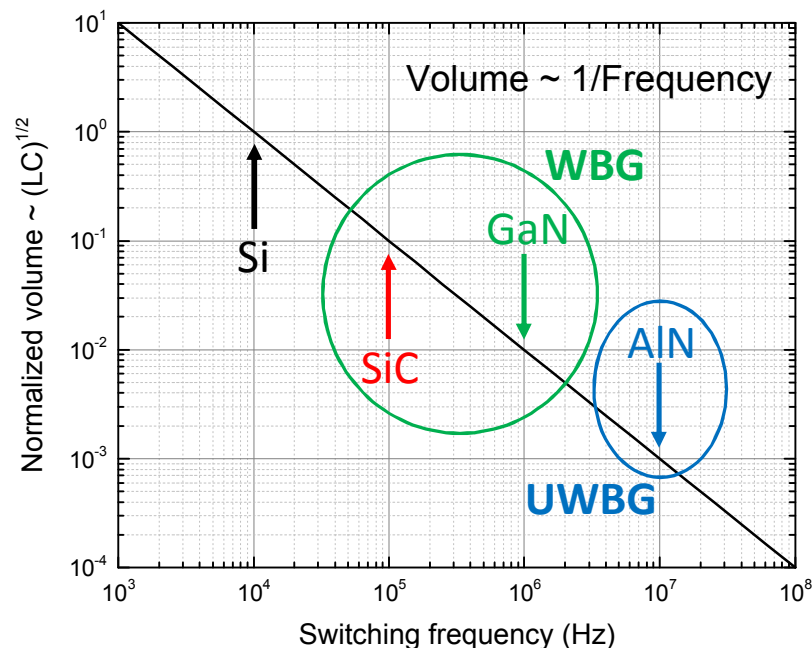
WBG/UWBG materials enable higher switching frequency and better thermal management



Dramatic Reduction in Power Converter Volume with Increasing Bandgap



SiC is 10% the volume and weight of Si for equivalent capability (10 kV, 100 A)



New materials and device architectures are needed to continue the trend towards higher performance PE

III-Nitride Semiconductors Are Ideal WBG and UWBG Materials

Fundamental Materials Capabilities

Property	Conventional		WBG		UWBG
	Si	GaAs	4H-SiC	GaN	AlN
Bandgap (eV)	1.1	1.4	3.3	3.4	6.2
Critical Electric Field (MV/cm)	0.3	0.4	2	3.3	15.9
Saturated electron velocity (10^7 cm/s)	1	1	2	2.5	2
Thermal conductivity (W/cm \cdot K)	1.5	0.5	4.5	4	3.4

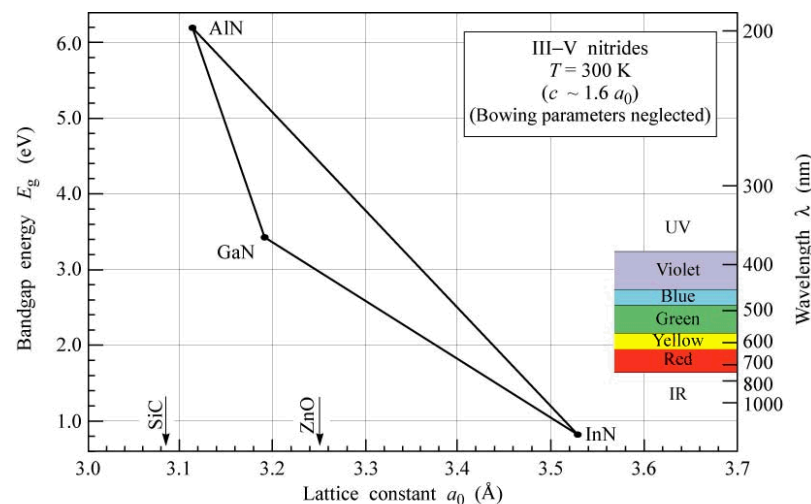
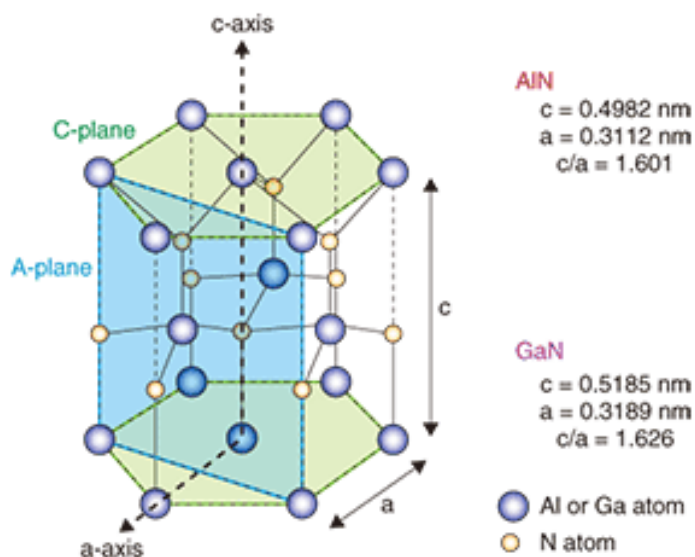
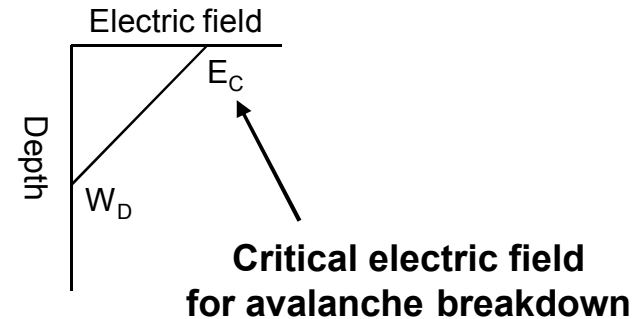
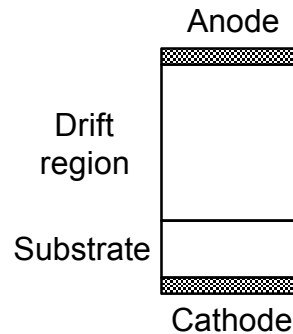
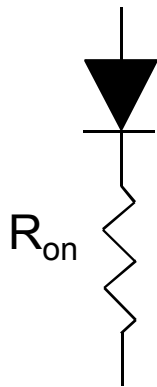


Fig. 12.12. Bandgap energy versus lattice constant of III-V nitride semiconductors at room temperature.

E. F. Schubert
 Light-Emitting Diodes (Cambridge Univ. Press)
www.LightEmittingDiodes.org

Breakdown Voltage and Figure-of-Merit Are Strong Functions of Critical Electric Field



- Off-state: Integrate electric field to get breakdown voltage: $V_B = W_D E_c / 2$ (1)

- Gauss' law: $\epsilon E_c = q N_D W_D$ (2)

- On-state: Current transport due to carrier drift, resistance $R_{on} = W_D / \sigma A$
 Conductivity $\sigma = q \mu_n n = q \mu_n N_D$ assuming complete dopant ionization
 Specific on-resistance $R_{on,sp} = R_{on} A = W_D / \sigma \rightarrow R_{on} A = W_D / q \mu_n N_D$ (3)

- Combining (1) and (2) gives dependence of V_B on N_D and E_c : $V_B = \epsilon E_c^2 / 2 q N_D$

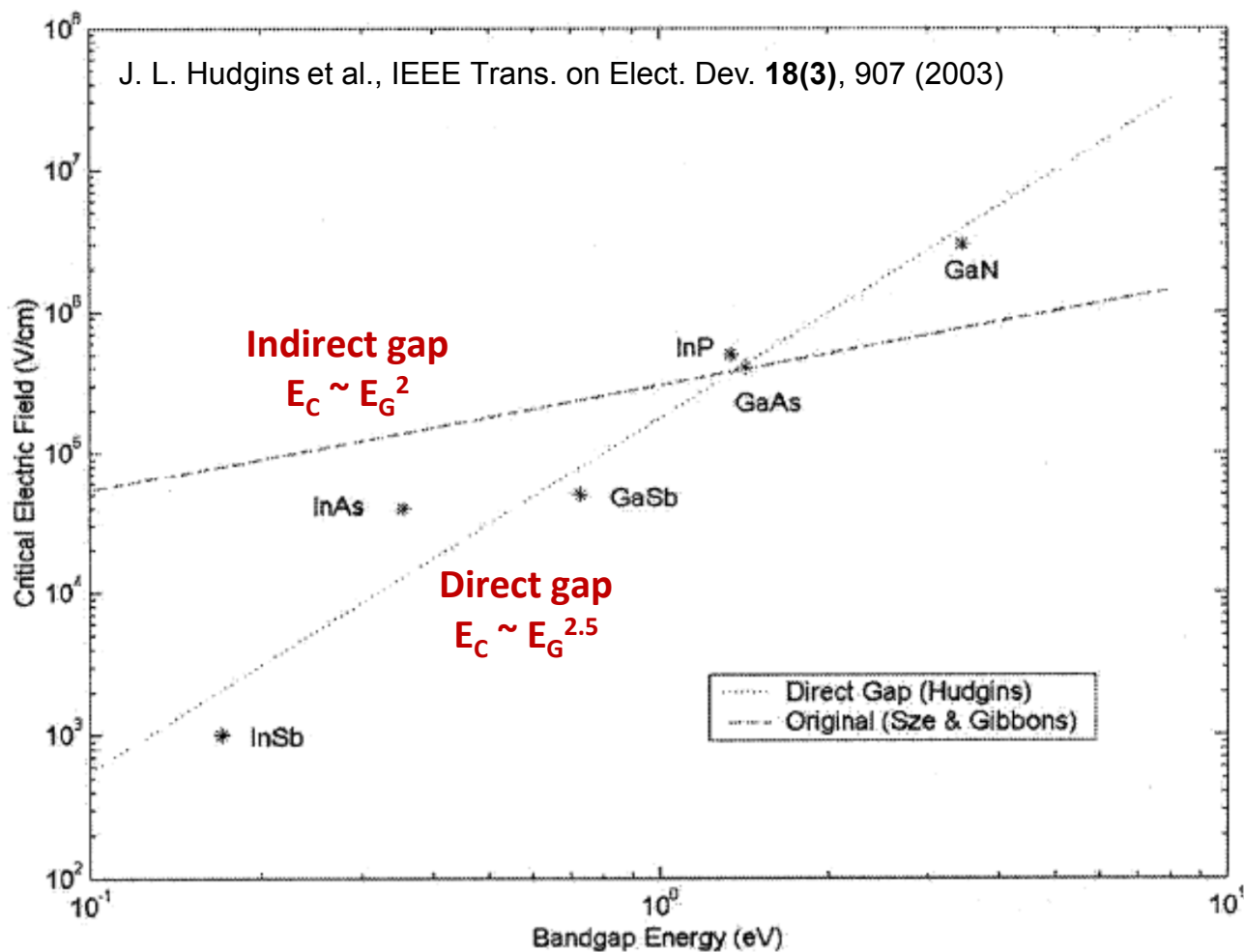
- Combining (1), (2), and (3) one obtains the unipolar "figure-of-merit":

$$R_{on,sp} = 4 V_B^2 / \epsilon \mu_n E_c^3 \rightarrow V_B^2 / R_{on,sp} = \epsilon \mu_n E_c^3 / 4$$

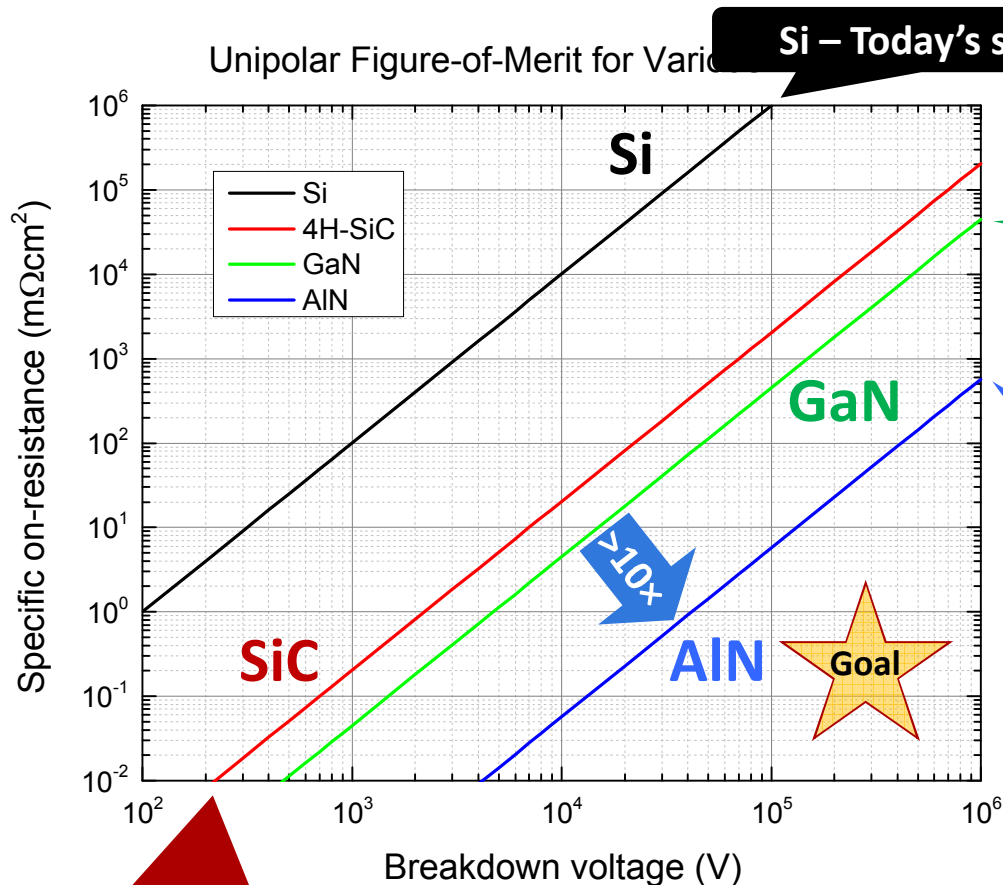
Depends on cube of E_c

Depends on square of E_c

Strong Dependence of Critical Field on Bandgap



This Grand Challenge Is Developing the Next Generation of Materials for Power Electronics



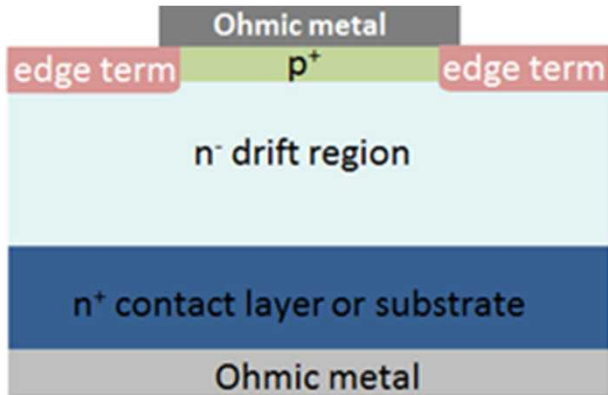
SiC
Many commercial devices
now available

GaN
Lateral devices fairly mature
Vertical devices emerging

AlN
Unexplored space
Unprecedented performance
Numerous challenges!

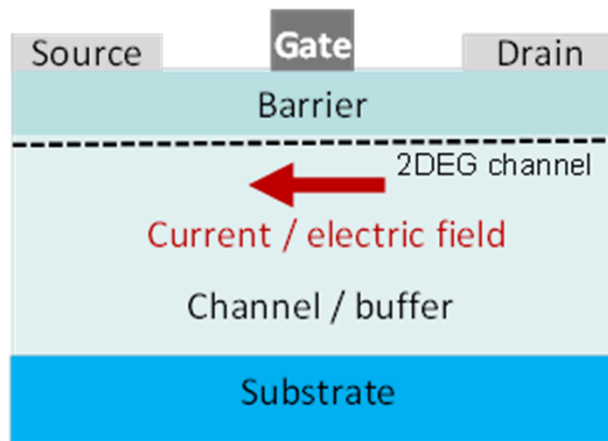
Unique opportunity for SNL and
partners to make a
foundational contribution to a
strategically important field

Two Target Classes of Power Devices



Vertical device (15 kV target)

- Current flow and voltage drop perpendicular to surface
- Architecture is better-suited to high voltage devices
- But native substrates and low doping are challenges



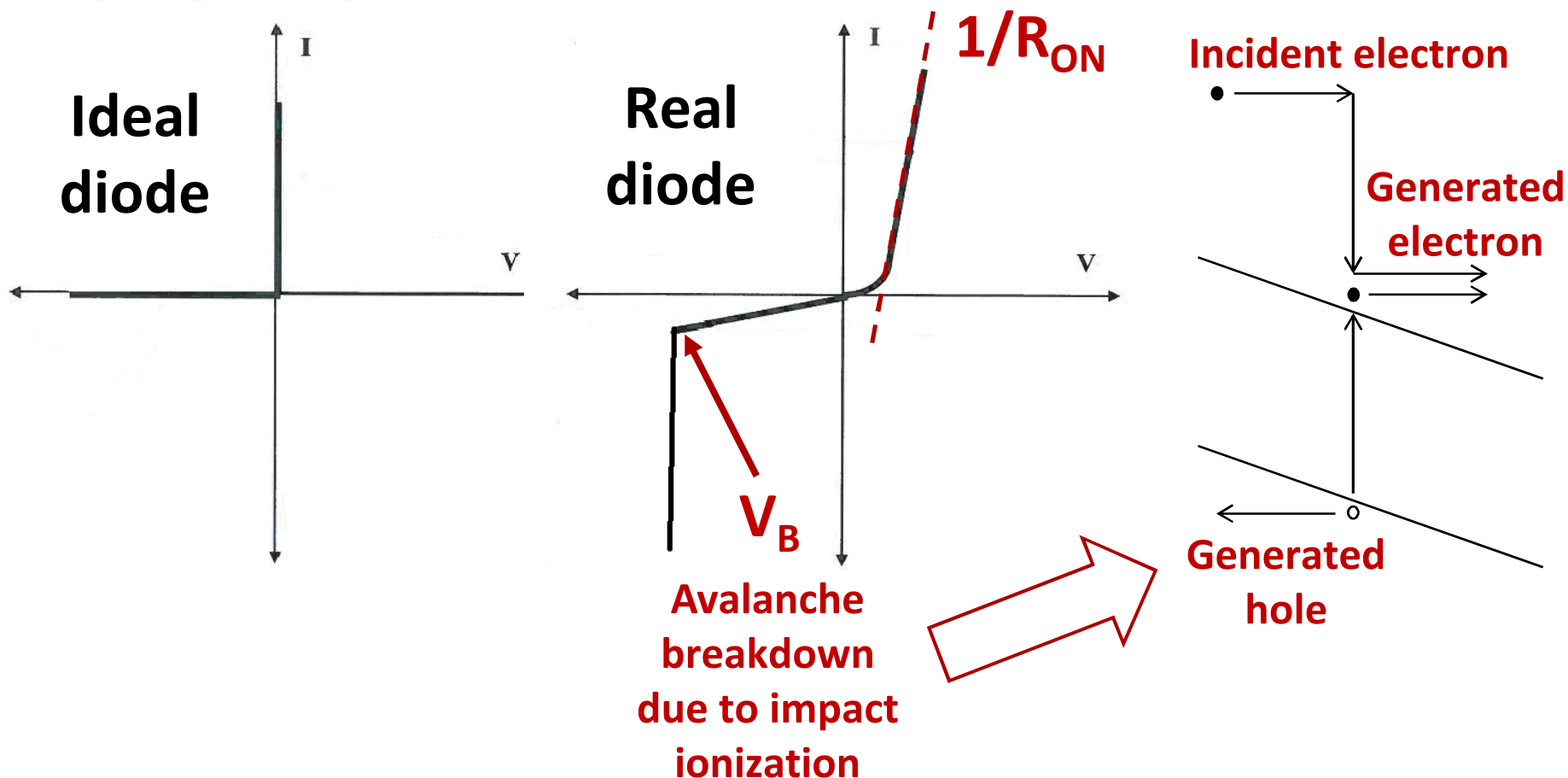
Lateral device (5 kV target)

- Current flow and voltage drop parallel to surface
- Availability of heterostructures and 2DEG is an advantage
- Electric field management is challenging

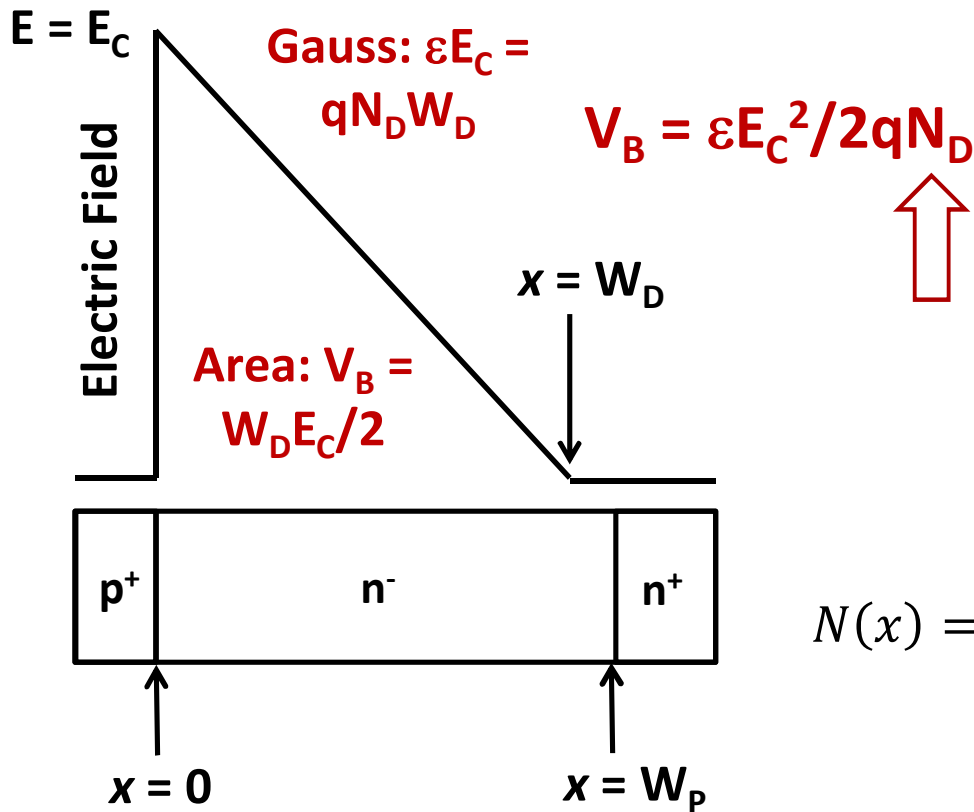
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Basics of Power Diodes



Critical Electric Field



Number $N(x)$ of generated electron-hole pairs obeys

$$\frac{dN}{dx} = (\alpha_p - \alpha_n) N(x)$$

$$\alpha_{n,p} = a_{n,p} \exp \left[- \left(\frac{b_{n,p}}{E} \right) \right]$$

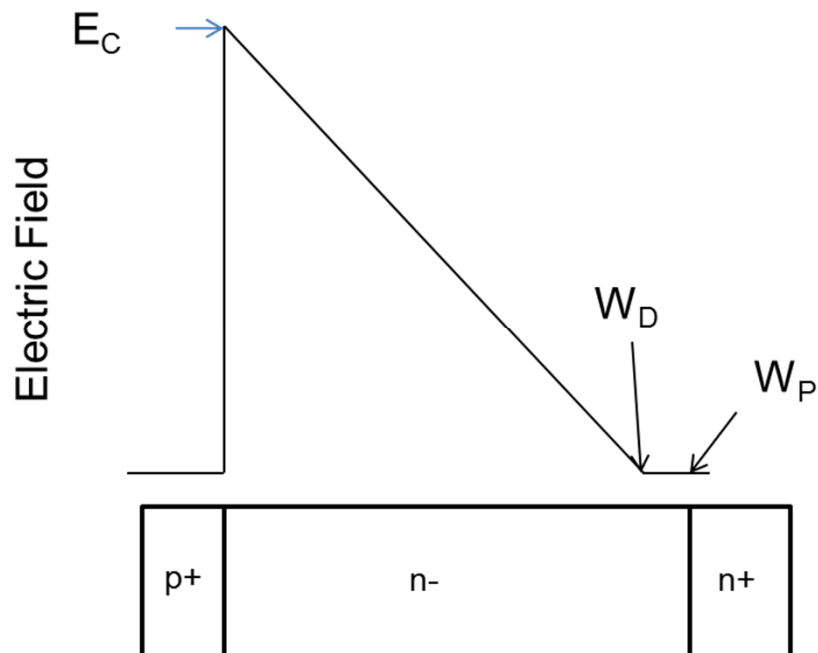
$$N(x) = \frac{\exp \left[\int_0^x (\alpha_p - \alpha_n) dx' \right]}{1 - \int_0^W \alpha_n \exp \left[\int_0^x (\alpha_p - \alpha_n) dx' \right] dx}$$

Avalanche occurs when denominator approaches infinity

The critical field is defined as the maximum electric field that leads to avalanche breakdown in a 1D analytical model

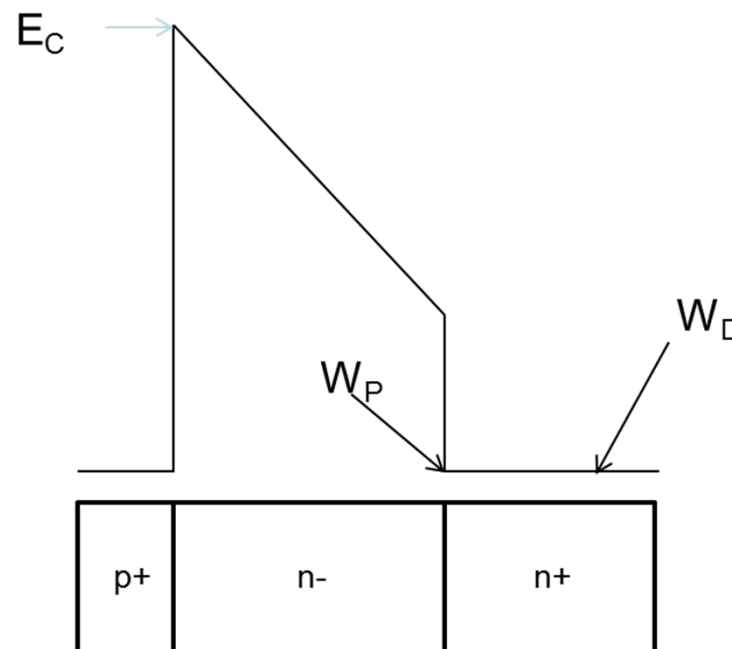
Punch-Through vs. Non-Punch-Through Design

Non-Punch-Through
 $W_P \geq W_D$



$$V_{br} = \frac{\epsilon E_C^2}{2qN_D}$$

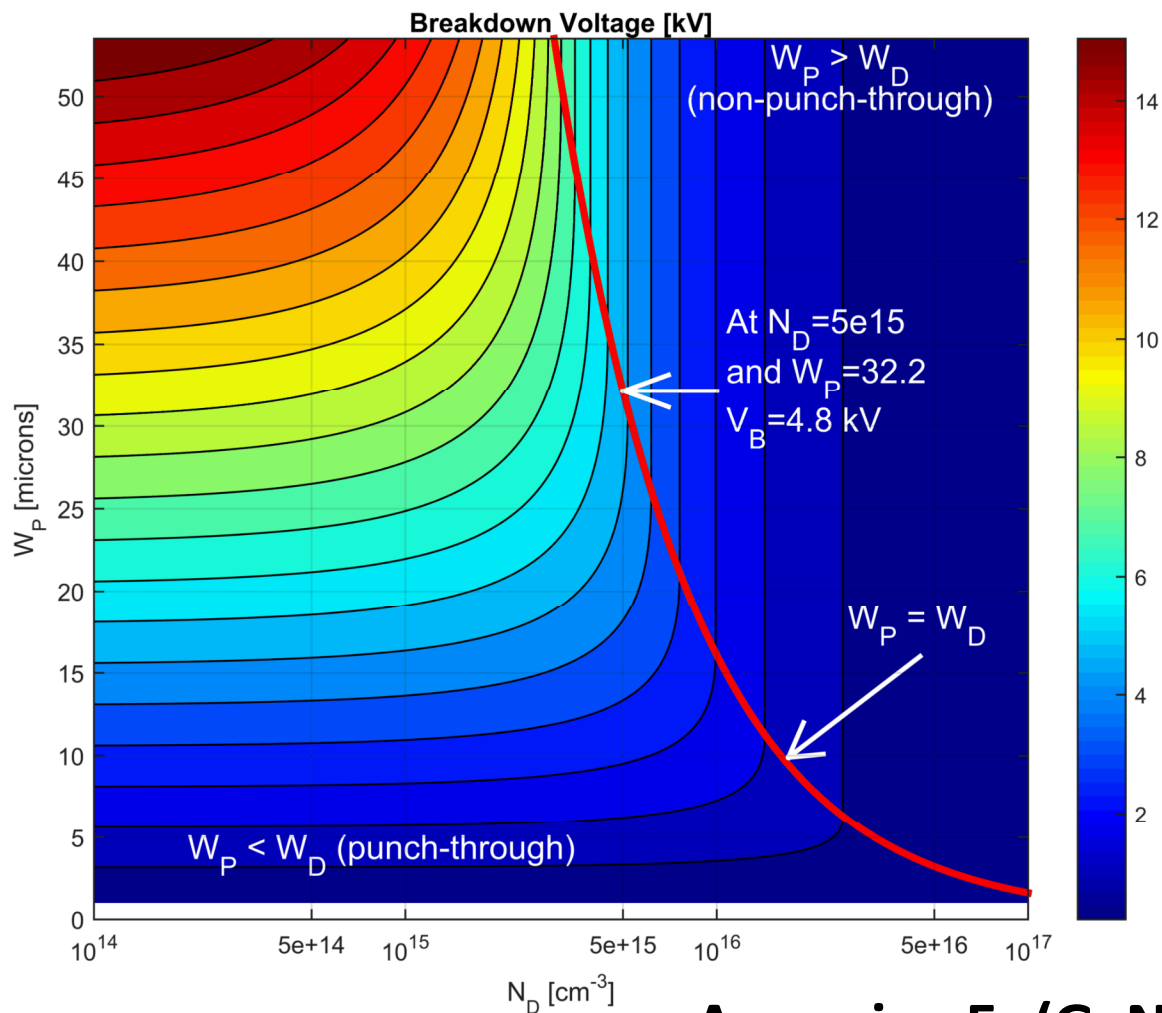
Punch-Through
 $W_P < W_D$



$$V_{br} = E_C W_P - \frac{qN_D W_P^2}{2\epsilon}$$

In both cases, low doping is required for high breakdown voltage

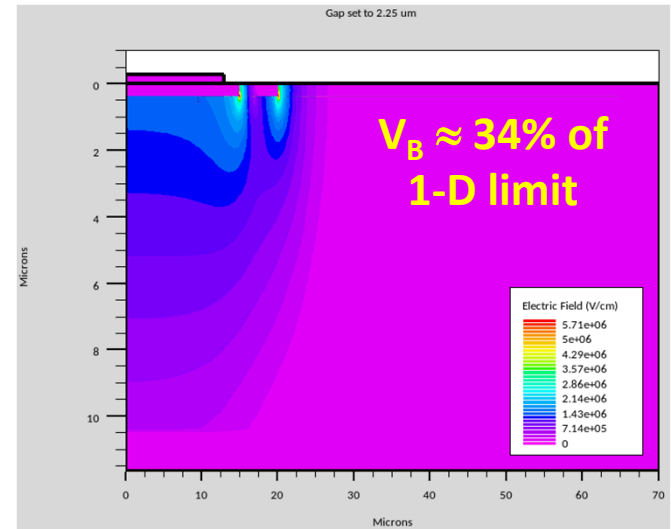
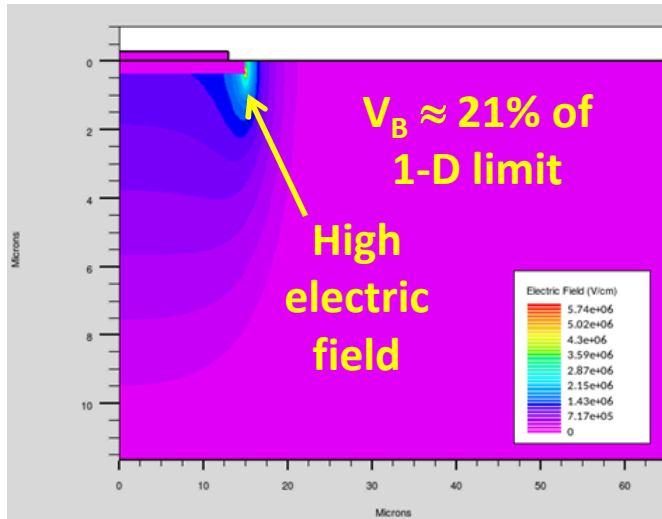
Dependence of V_B on Doping and Layer Thickness



Assuming E_c (GaN) = 3.0 MV/cm

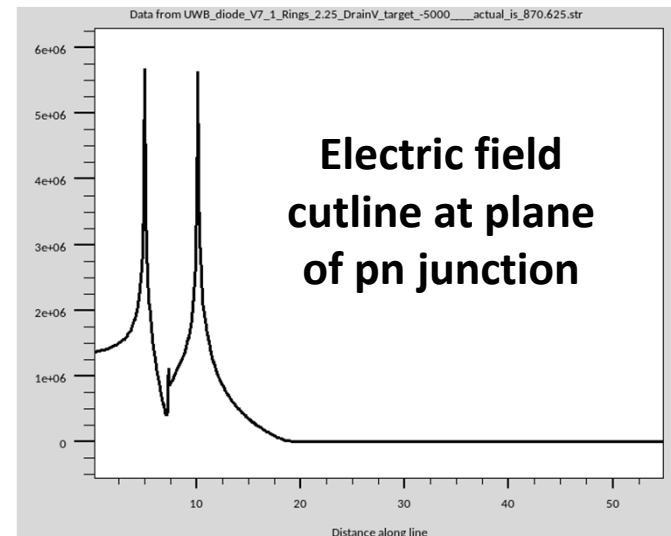
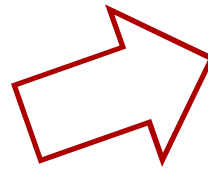
J. Dickerson et al., EMC 2015

Finite Lateral Extent of the Junction Reduces V_B in a Real Device



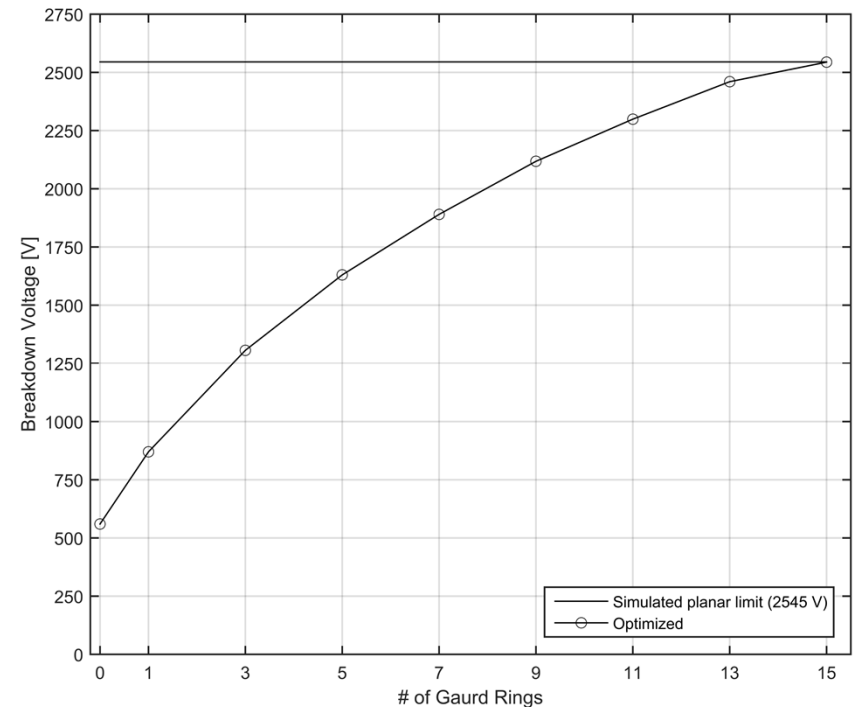
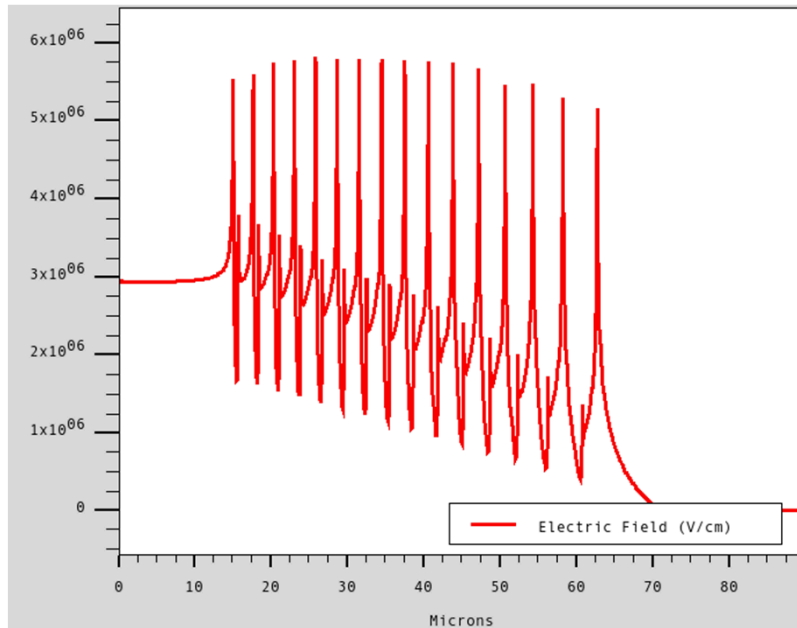
Solution: Implanted guard rings

- N implantation to “deaden” portions of the p^+ epilayer
- Large design space: # of rings, width and spacing of rings, implant dose and depth



J. Dickerson et al., EMC 2015

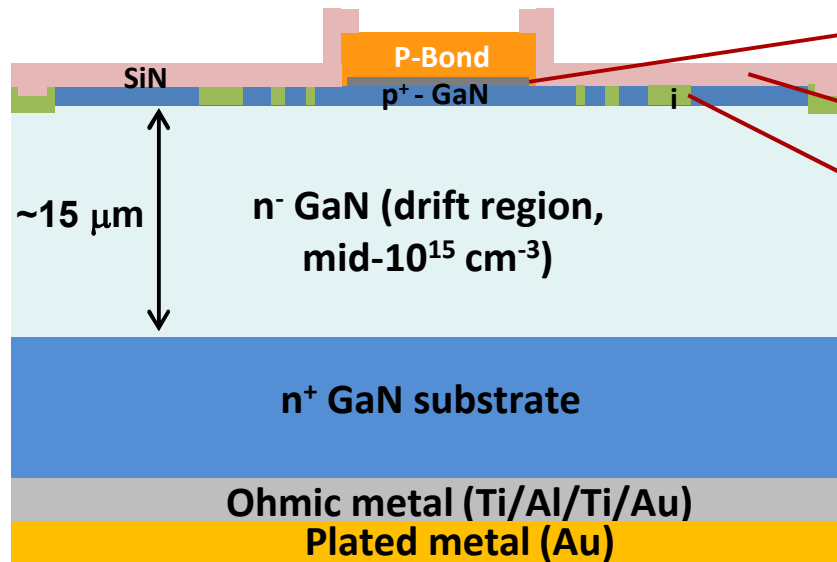
Optimized Guard Ring Designs



V_B saturates at 1-D limit for 15 optimized guard rings

J. Dickerson et al., EMC 2015

GaN PiN Diode Fabrication

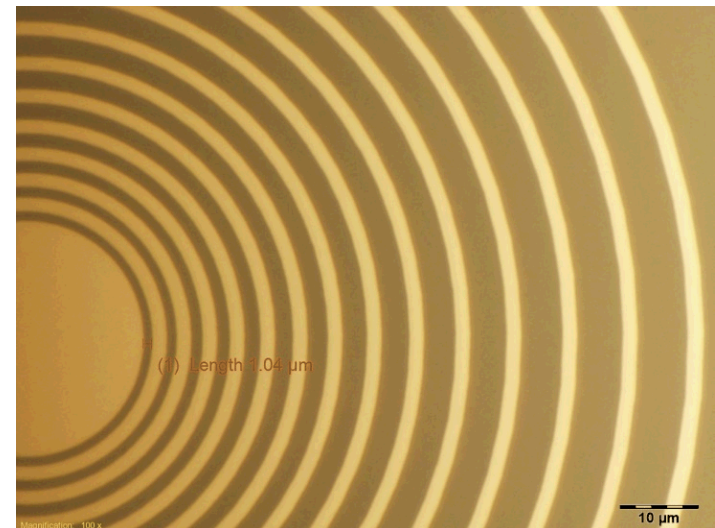


Ohmic p-contact process (Pd/Au)

High breakdown SiN (PECVD, 350°C)

Implantation of guard ring gaps

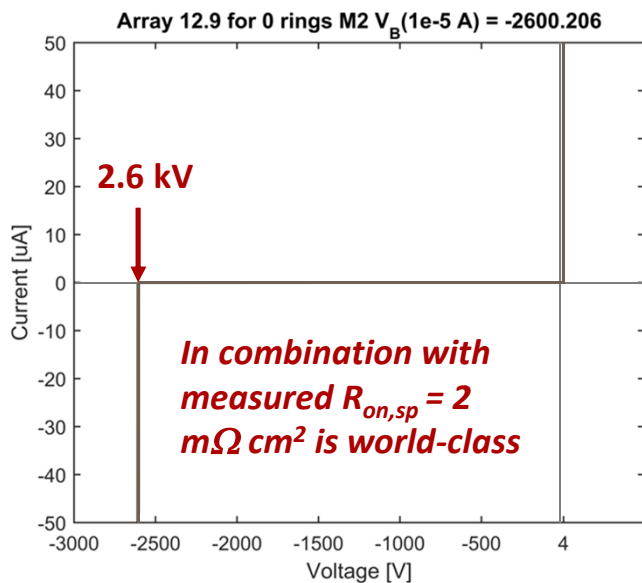
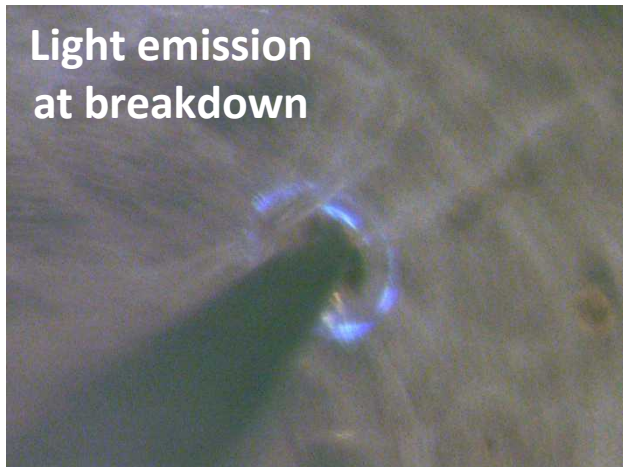
***Homoepitaxial GaN growth
on GaN substrates!***



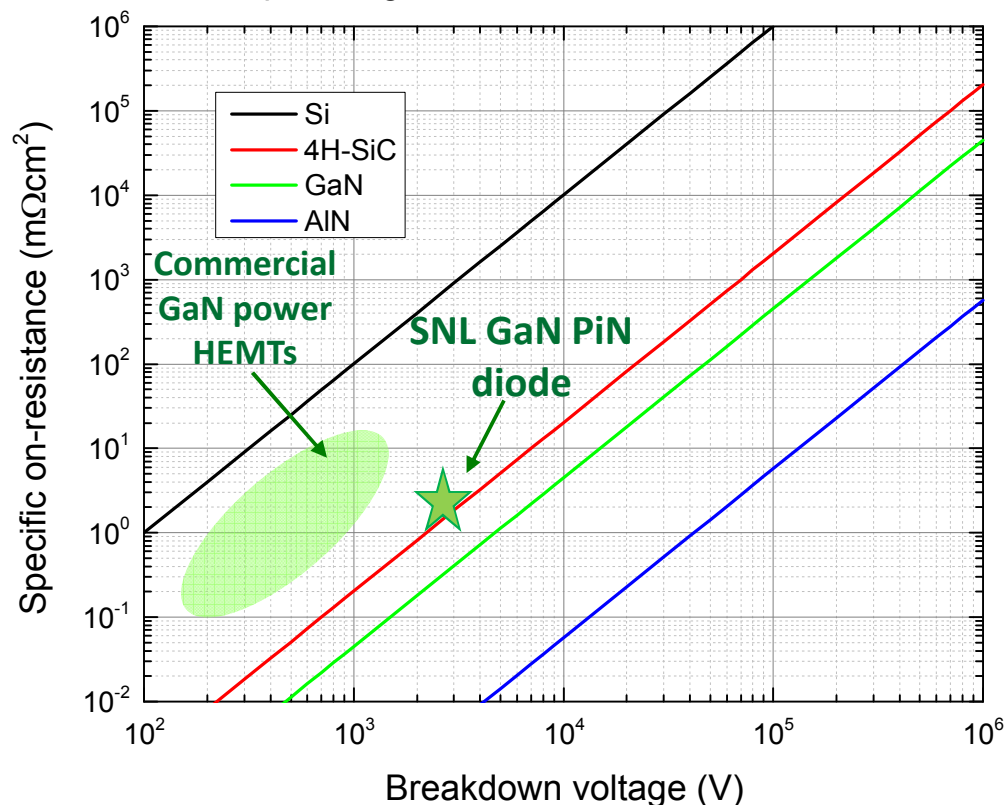
J. Dickerson et al., EMC 2015

GaN PiN Diode Performance

Light emission
at breakdown



Unipolar Figure-of-Merit for Various Materials

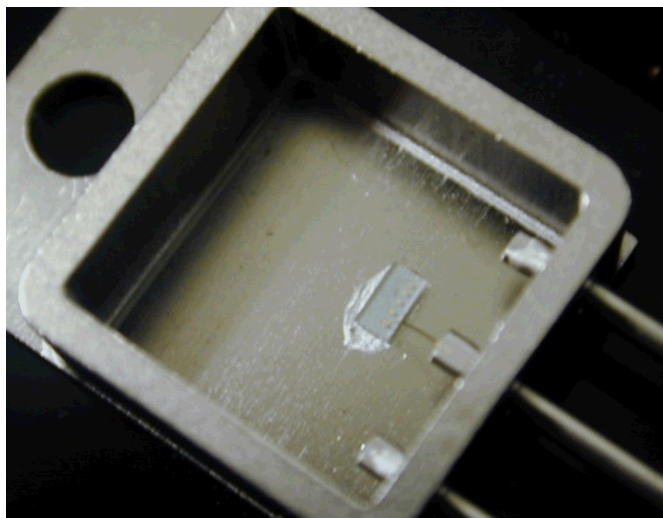


Outstanding results, but dependence of V_B on # of guard rings does not follow theory!

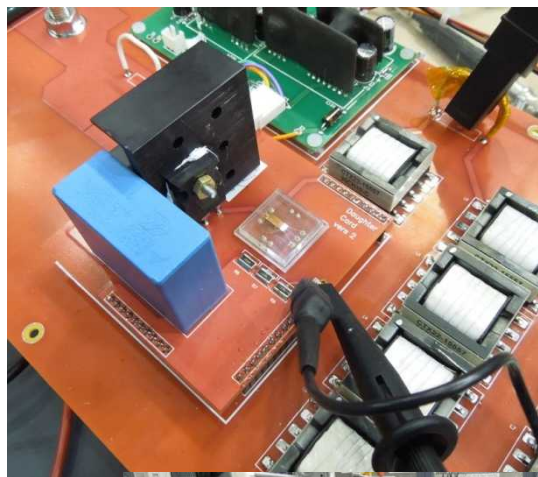
- We have an explanation, is now being verified

J. Dickerson et al., EMC 2015

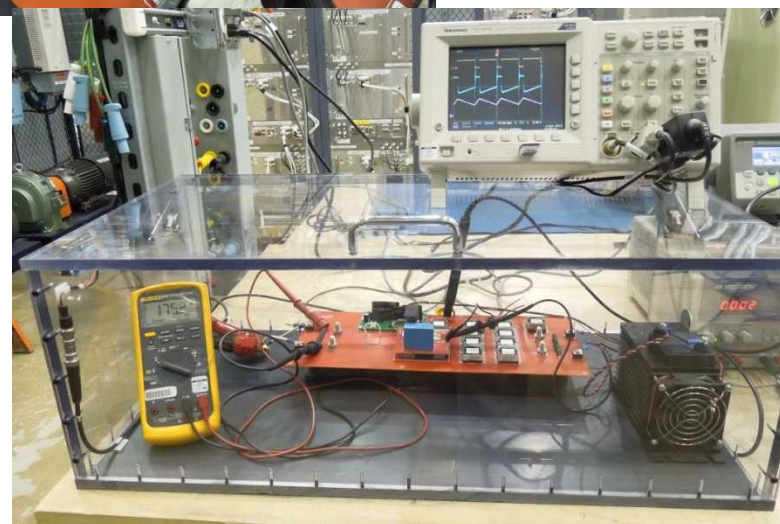
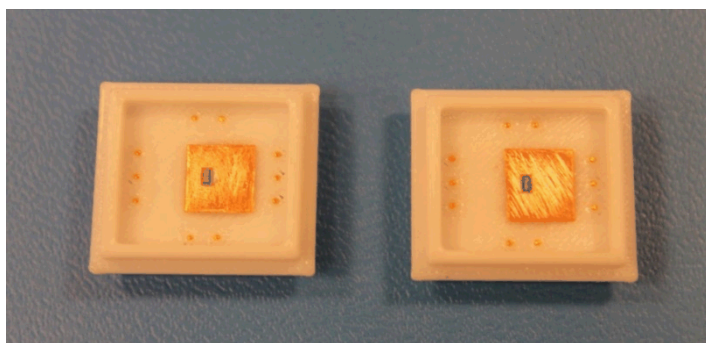
Packaging and Switching Characterization of GaN PiN Diodes



Commercial and custom in-house device packaging



**Switching test
characterization**

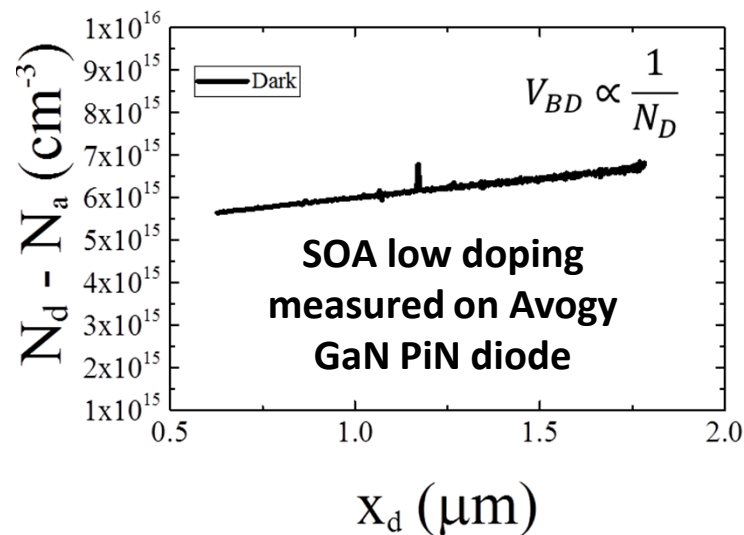
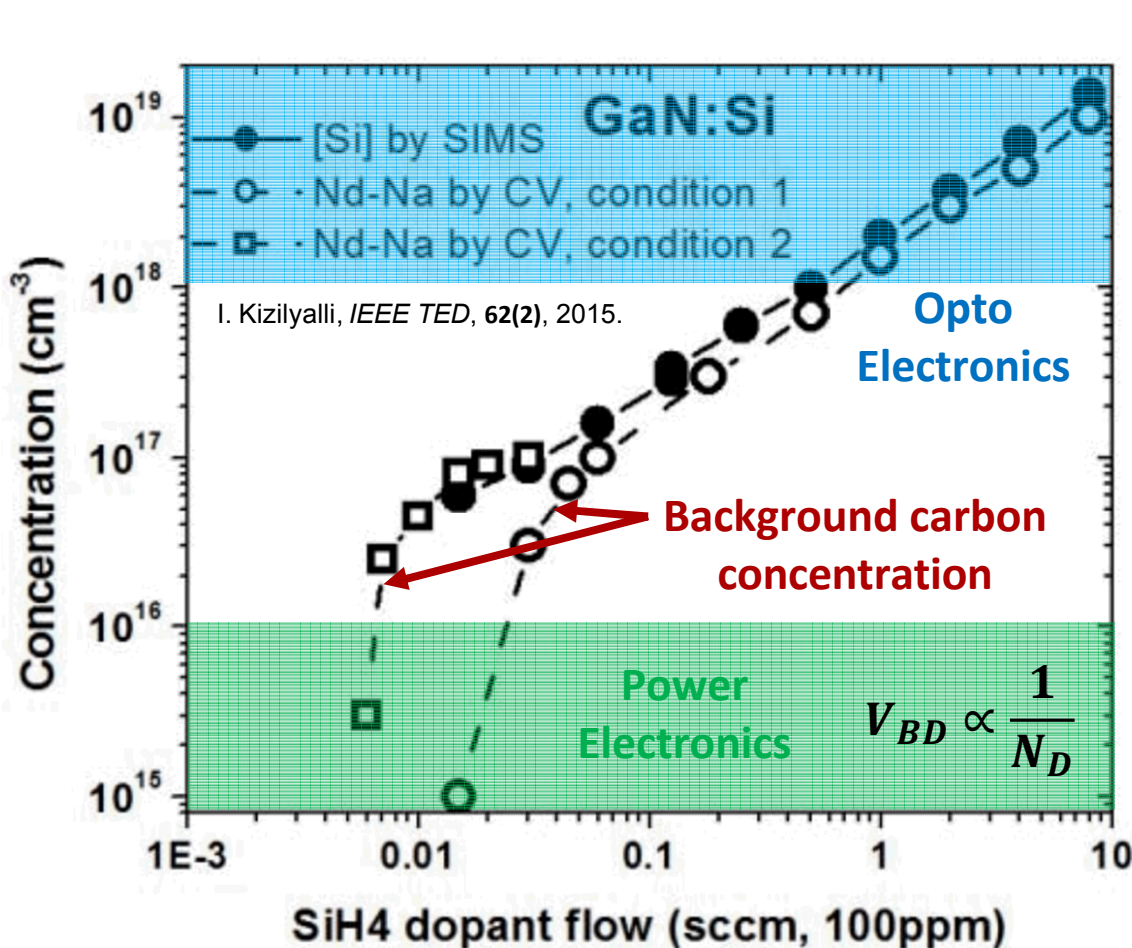


J. Neely

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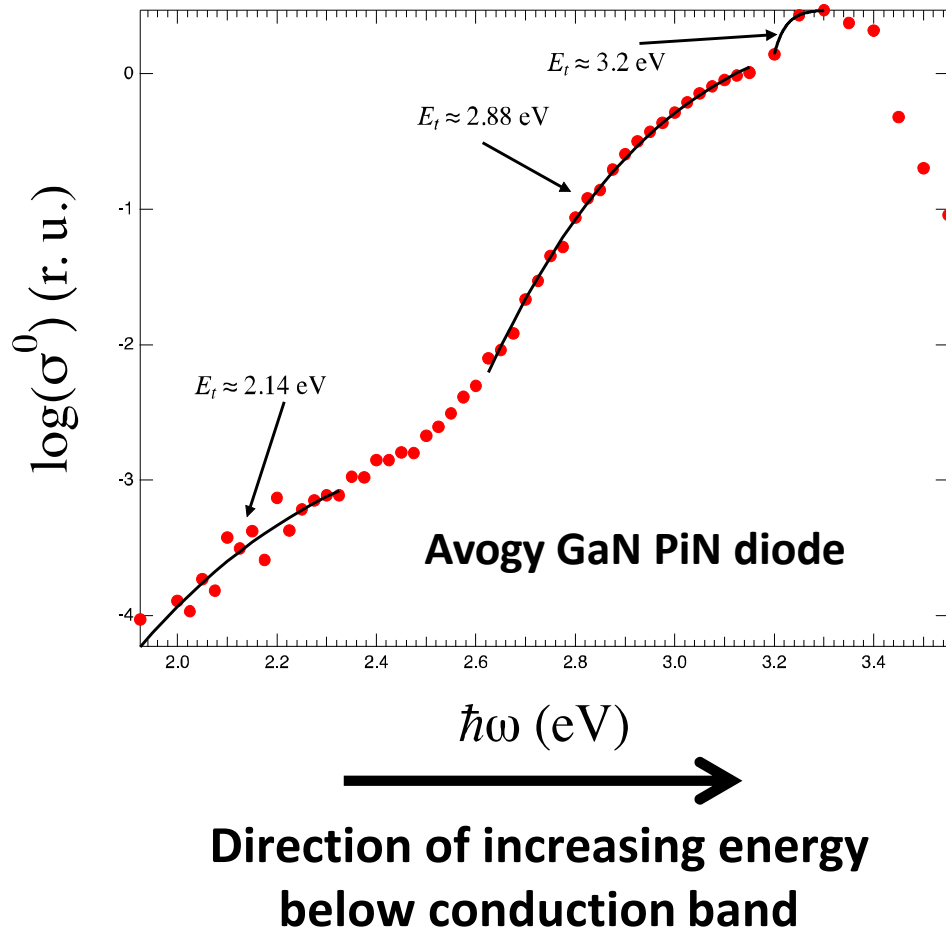
Low Doping in GaN Drift Regions



For GaN drift regions, the background acceptor concentration may be the same order of magnitude as the intentional dopant concentration!

M. P. King et al., EMC 2015

DLOS Spectrum of Homoepitaxial GaN Drift Region

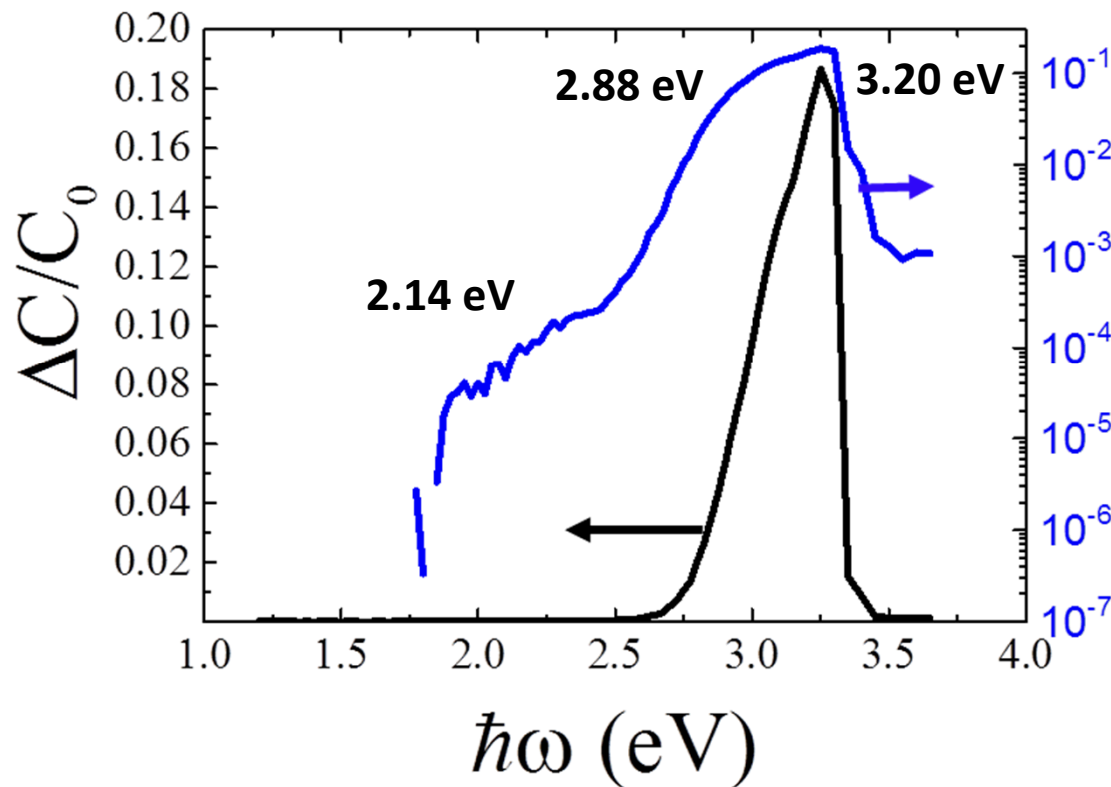


- DLOS studies show three prominent defect levels at:
 - $E_c - 2.14$ eV
 - $E_c - 2.88$ eV
 - $E_c - 3.20$ eV
- States at $E_c - 2.14$ eV and $E_c - 2.88$ eV are broad, indicating strong lattice relaxation following carrier emission

M. P. King et al., EMC 2015

Steady-State Photocapacitance

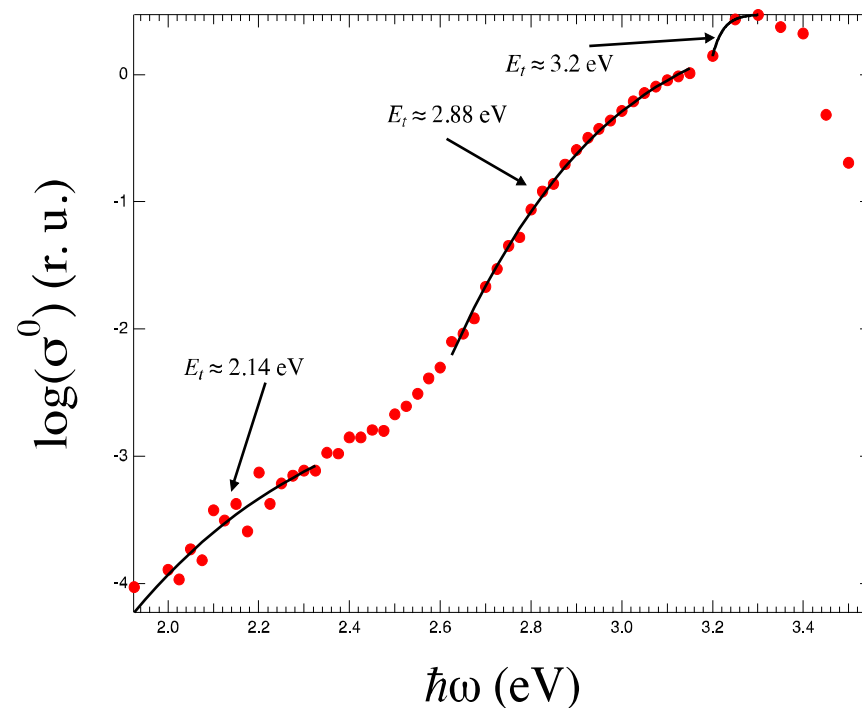
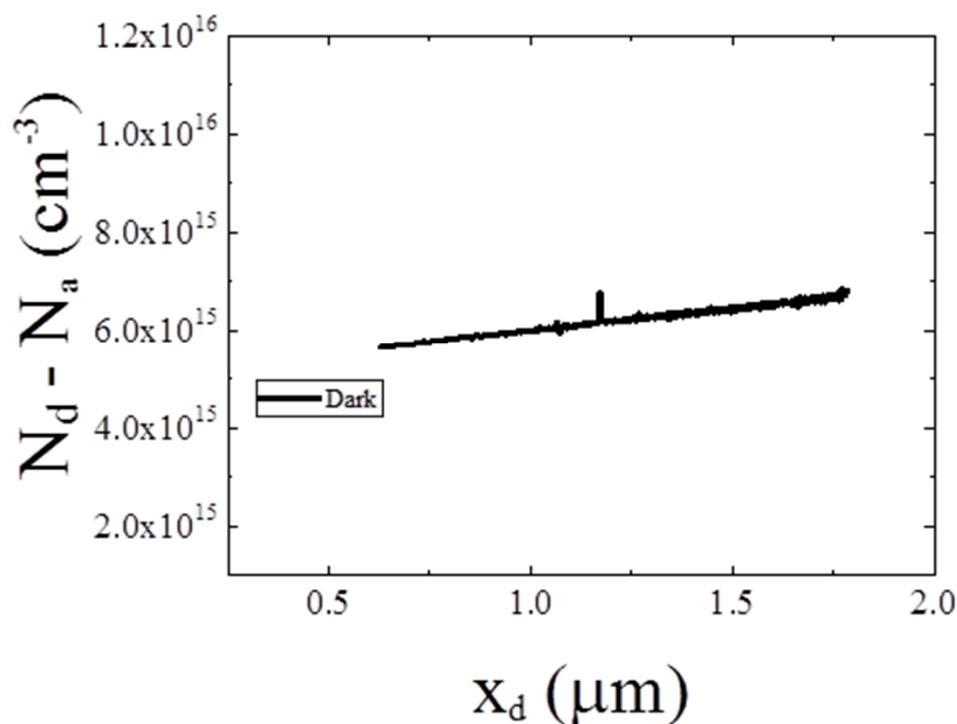
Provides defect density information



- States at $E_c - 2.14$ eV and $E_c - 2.88$ eV are again broad
- Defect level at $E_c - 2.14$ eV shows small impact on response
- Levels at $E_c - 2.88$ eV and $E_c - 3.20$ eV are observed to be large in magnitude and *are likely primary compensating centers*

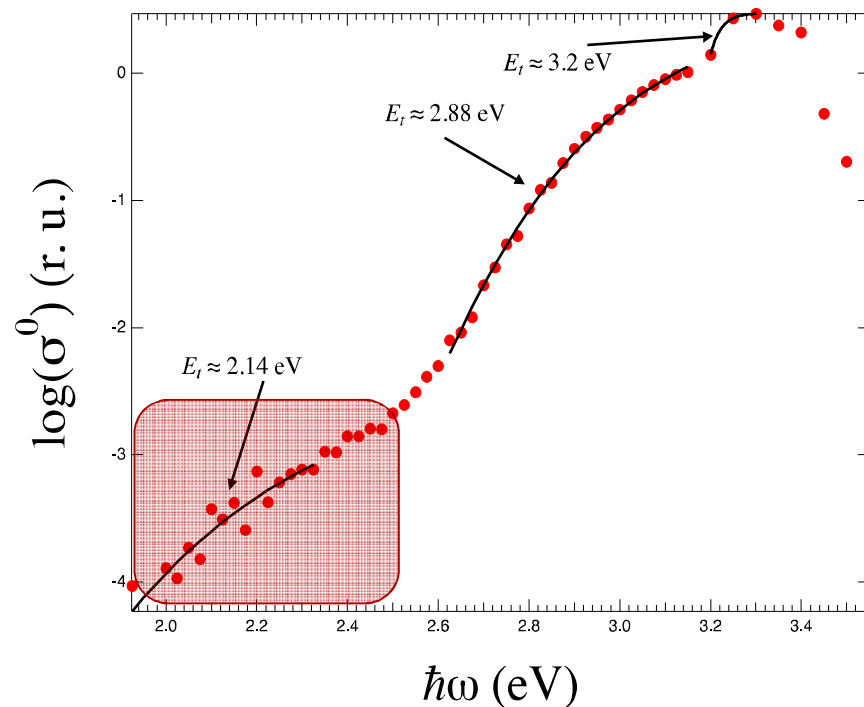
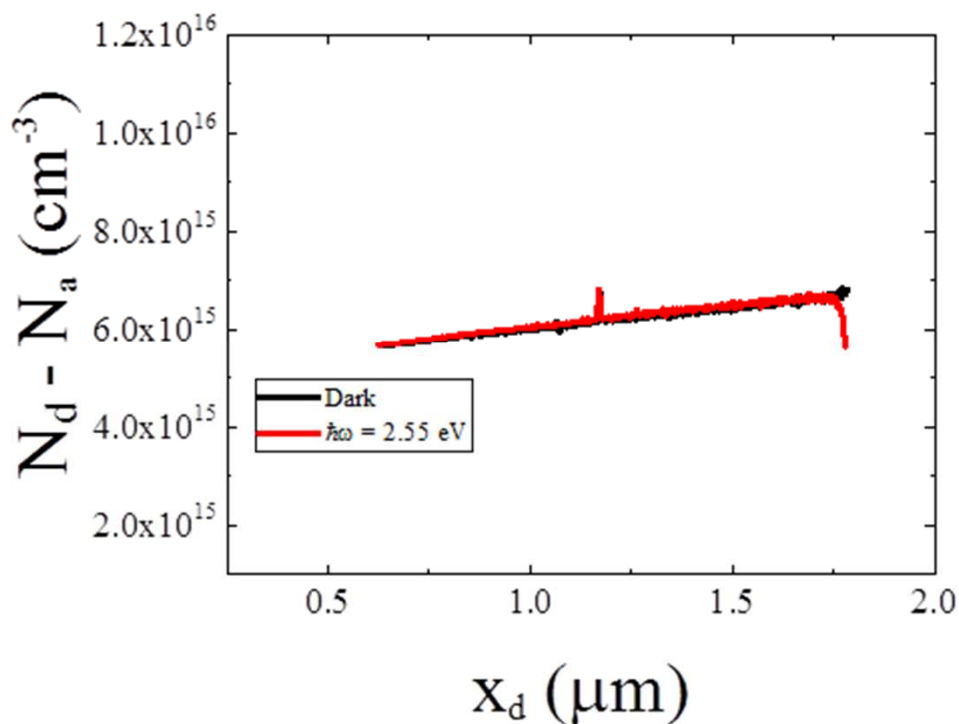
M. P. King et al., EMC 2015

Lighted CV Correlates with DLOS to Determine Compensating Defect Density



M. P. King et al., EMC 2015

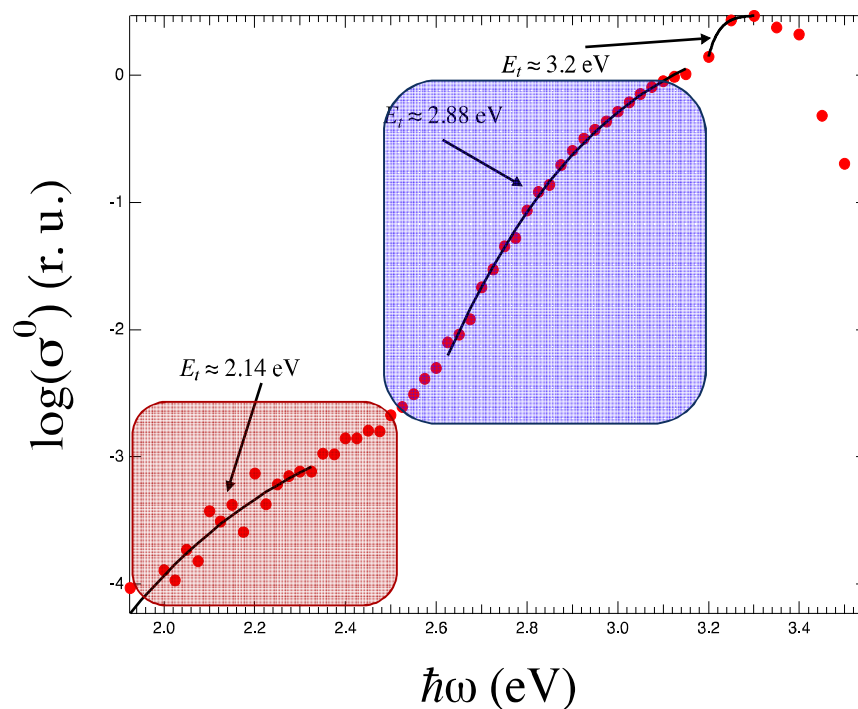
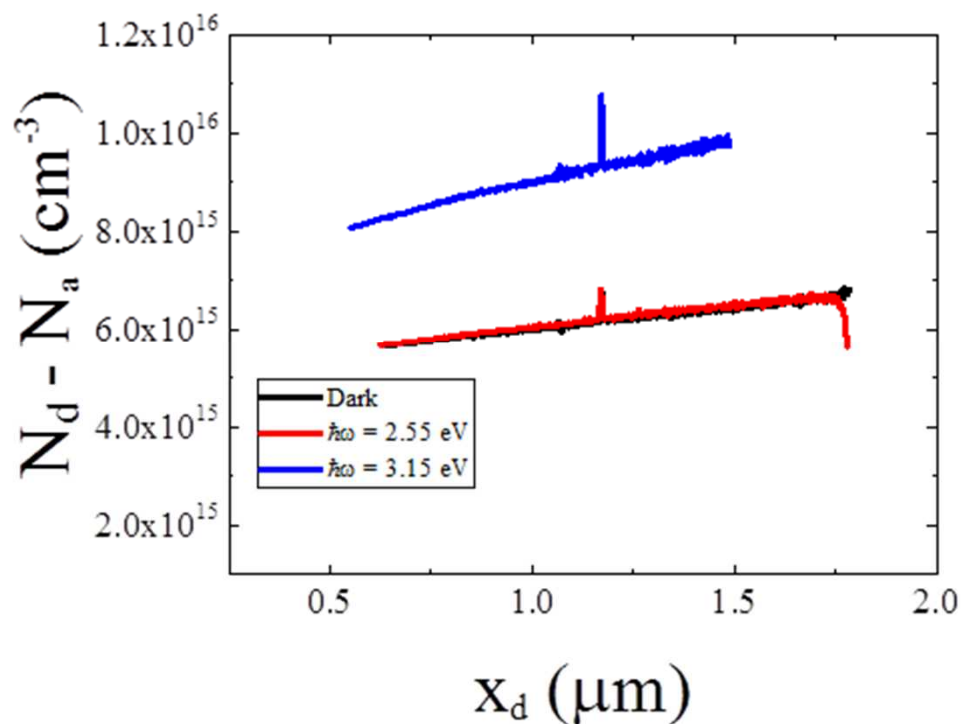
Lighted CV Correlates with DLOS to Determine Compensating Defect Density



- Small response from $E_c - 2.14$ eV level, $N_T \approx 3 \times 10^{13}$ cm⁻³

M. P. King et al., EMC 2015

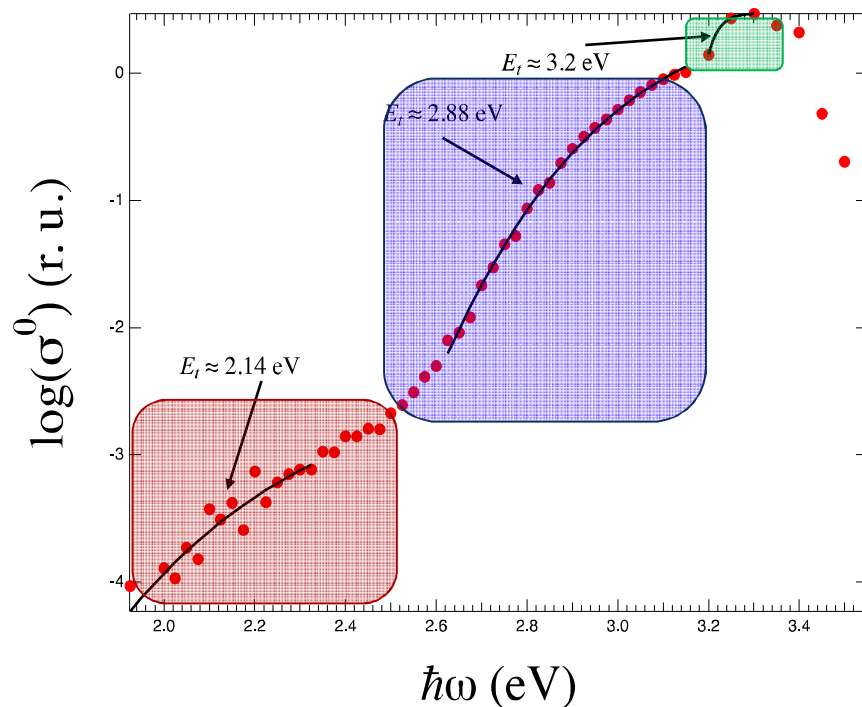
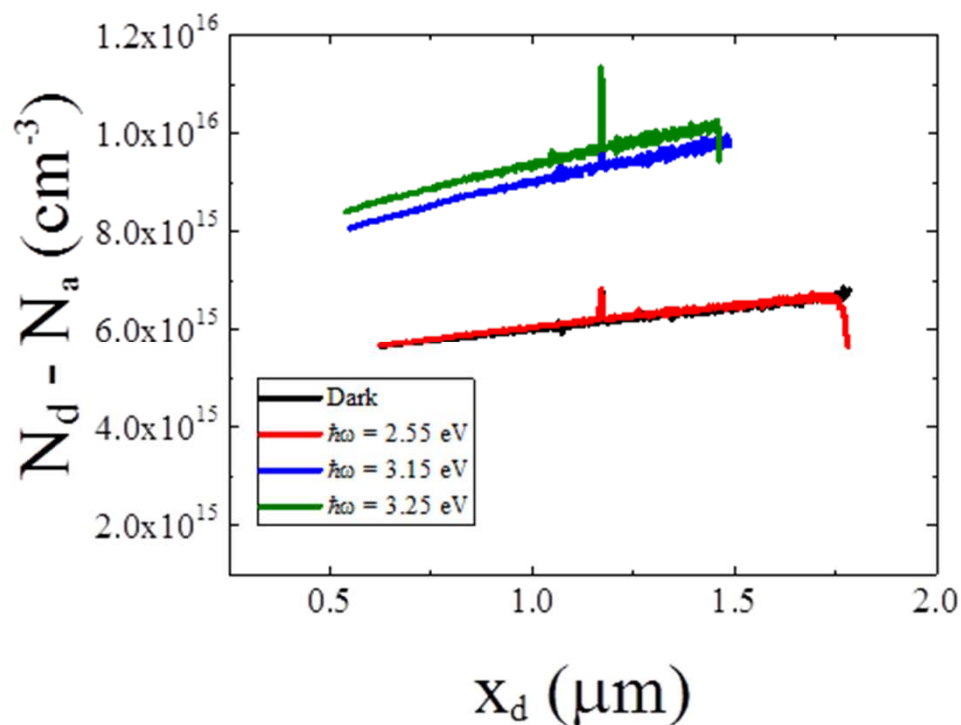
Lighted CV Correlates with DLOS to Determine Compensating Defect Density



- Small response from $E_c - 2.14$ eV level, $N_T \approx 3 \times 10^{13} \text{ cm}^{-3}$
- $E_c - 2.88$ eV level is the primary compensating defect, $N_T \approx 2 \times 10^{15} \text{ cm}^{-3}$

M. P. King et al., EMC 2015

Lighted CV Correlates with DLOS to Determine Compensating Defect Density



- Small response from $E_c - 2.14$ eV level, $N_T \approx 3 \times 10^{13} \text{ cm}^{-3}$
- $E_c - 2.88$ eV level is the primary compensating defect, $N_T \approx 2 \times 10^{15} \text{ cm}^{-3}$
- $E_c - 3.20$ eV level is on order of free carrier concentration, $N_T \approx 2.5 \times 10^{15} \text{ cm}^{-3}$

M. P. King et al., EMC 2015

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Problem: No Lattice-Matched Conducting Substrate!

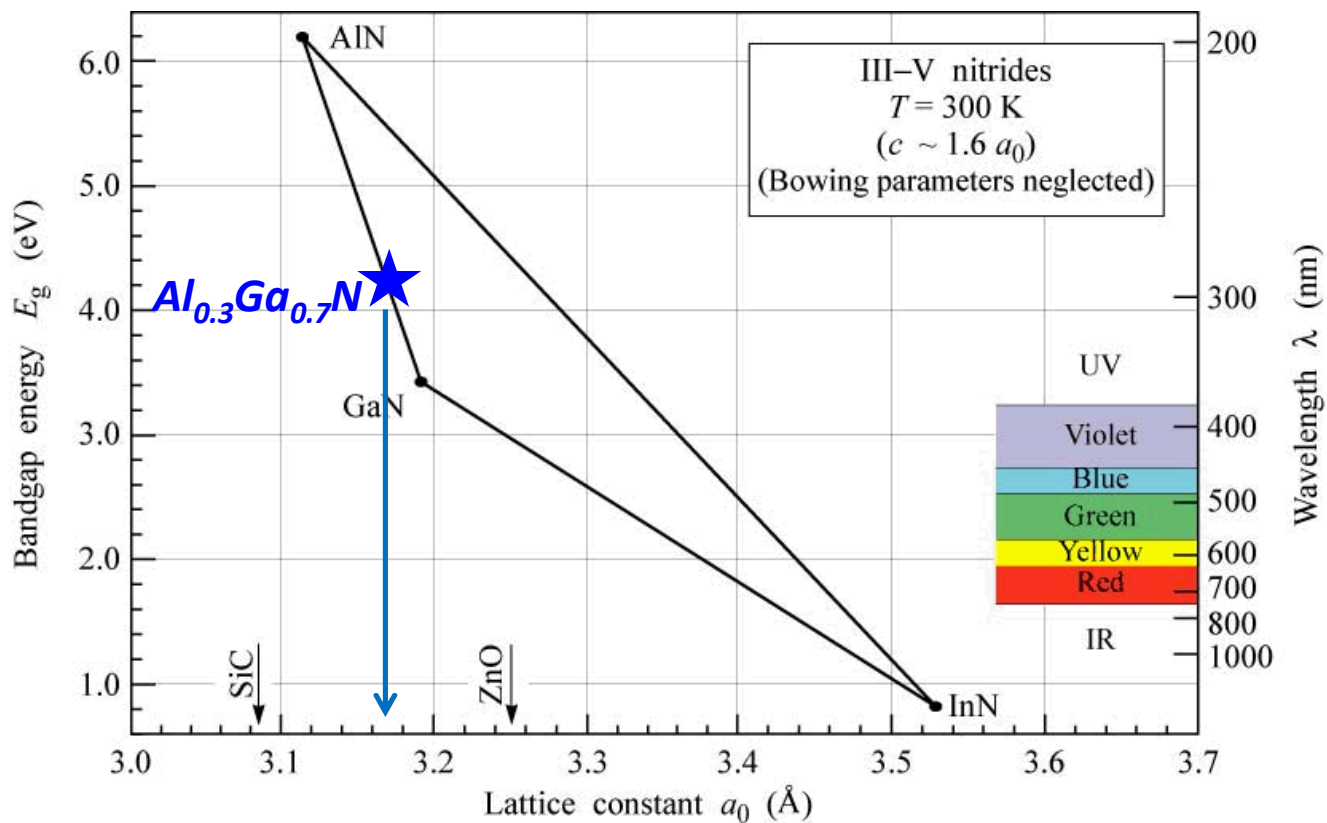


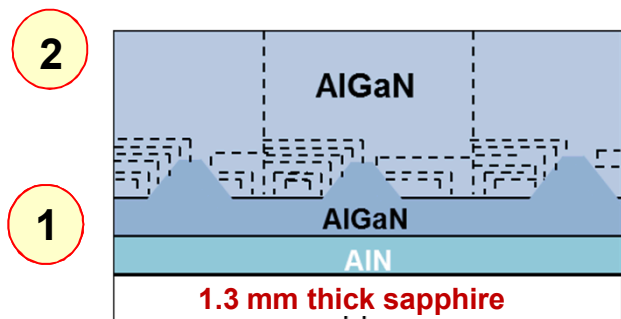
Fig. 12.12. Bandgap energy versus lattice constant of III-V nitride semiconductors at room temperature.

E. F. Schubert
Light-Emitting Diodes (Cambridge Univ. Press)
www.LightEmittingDiodes.org

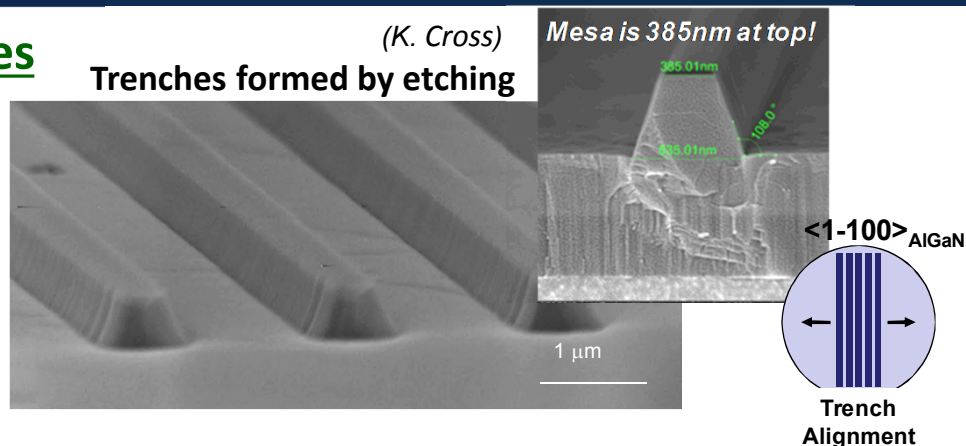
AlGaN Overgrowth of Patterned Templates on Thick Sapphire

AlGaN Growth on Patterned Templates

AlGaN with reduced dislocations

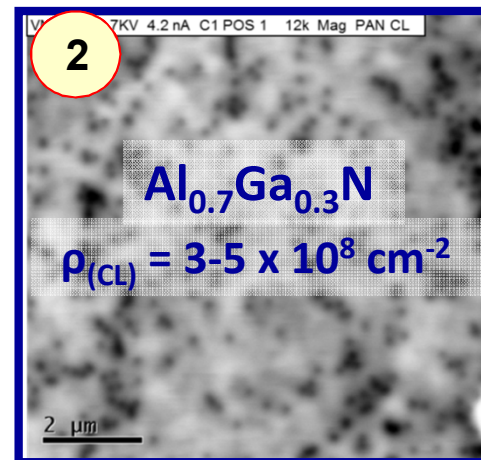
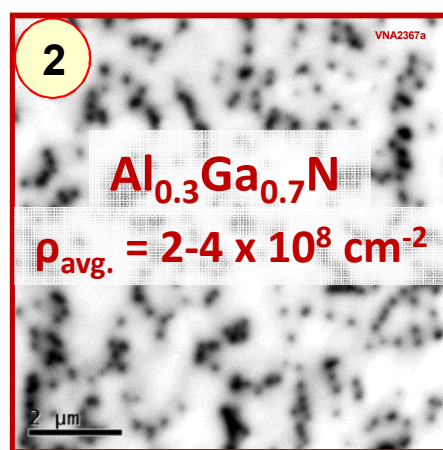
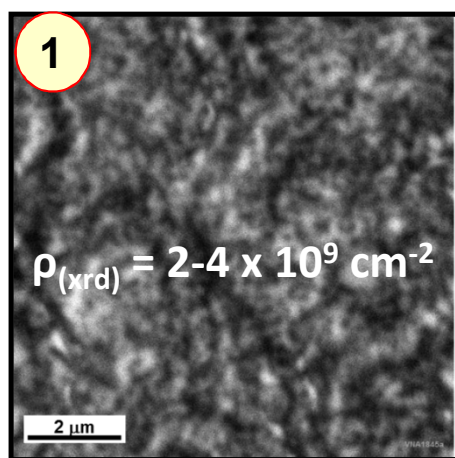


(K. Cross)
Trenches formed by etching



➔ *Sub-micron features are key innovation for uniform reduction of dislocations*

Cathodoluminescence (L. Alessi)

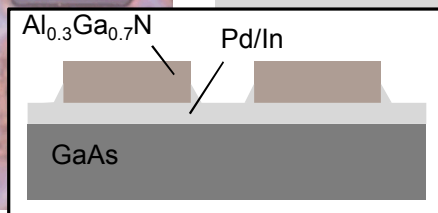
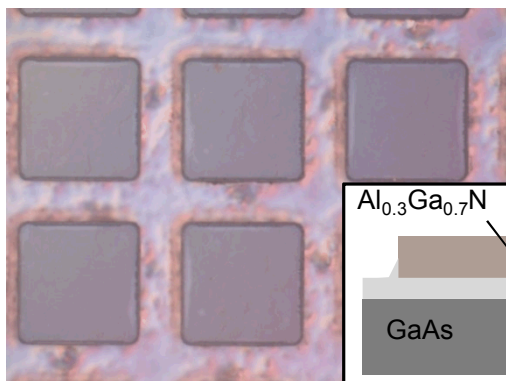
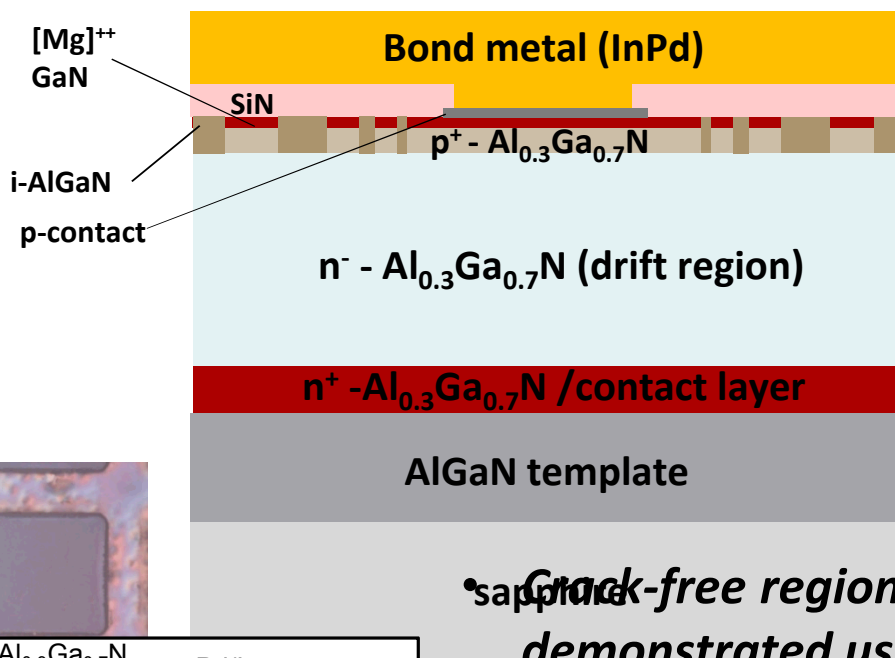
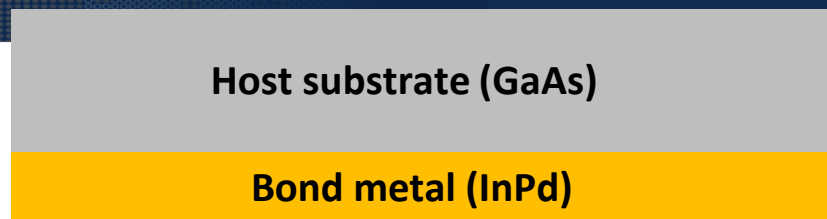


A. Allerman et. al., JCG 2014

10-20x reduction

10-15x reduction

$\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ PiN Diode Processing



Crack-free regions have been demonstrated using laser lift-off of $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ epitaxial layers from AlN/sapphire templates using a pulsed laser (> 1 J/cm²)

J. Wierer

Outline

➤ Introduction and motivation

- Introduction to Sandia
- Motivation for WBG/UWBGs in power electronics

➤ Vertical devices

- GaN PiN diode design and fabrication
- Doping and defect physics in GaN drift regions
- $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ PiN diodes

➤ Lateral devices

- Al-Rich $\text{Al}_x\text{Ga}_{1-x}\text{N}/\text{Al}_y\text{Ga}_{1-y}\text{N}$ heterostructures

Target Metrics for 5 kV UWBG HEMT

$$R_{on,sp} = \frac{1}{q\mu n_s} (L_{sd} + 2\sqrt{q\mu n_s \rho_c})^2$$

$$R_{sh} = 1/q\mu n_s$$

$$V_B = E_{crit} L_{gd}$$

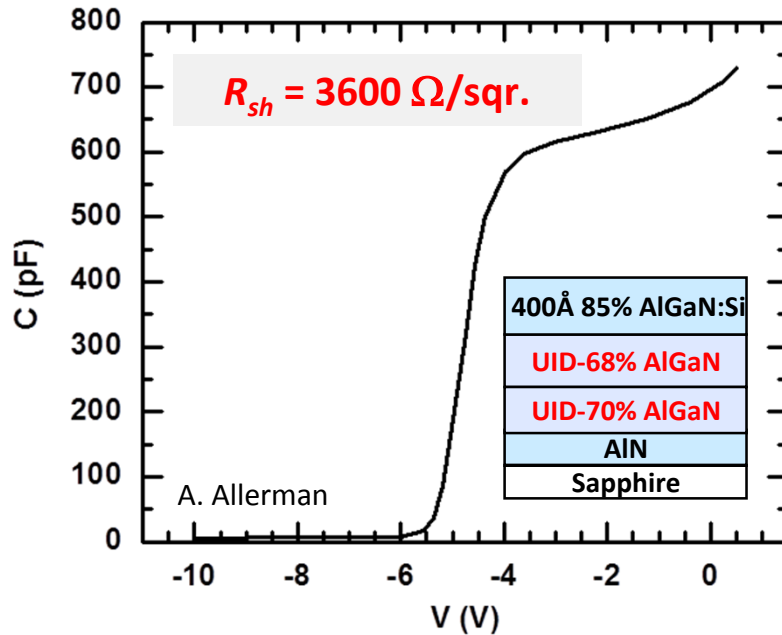
$$V_{th} = \frac{\phi_B}{q} - \frac{\Delta E_c}{q} - \frac{n_s d}{\epsilon}$$

- **AlN/Al_{0.85}Ga_{0.15}N HEMT with $L_{gd} = 12.5 \mu\text{m}$, $L_g = 1 \mu\text{m}$, $L_{sg} = 1 \mu\text{m}$**
- **$R_{on,sp} = 5 \text{ m}\Omega\cdot\text{cm}^2$**
 - **$\mu = 250 \text{ cm}^2/\text{V}\cdot\text{s}$**
 - **$n_s = 10^{13} \text{ cm}^{-2}$**
 - **$\rho_c = 10^{-5} \Omega\cdot\text{cm}^2$**
- **$V_B = 5000 \text{ V}$**
 - **$E_{crit} = 4 \text{ MV/cm}$ (effective value)**
- **$V_T > +3 \text{ V}$**
 - **$\phi_B = 4 \text{ eV}$**

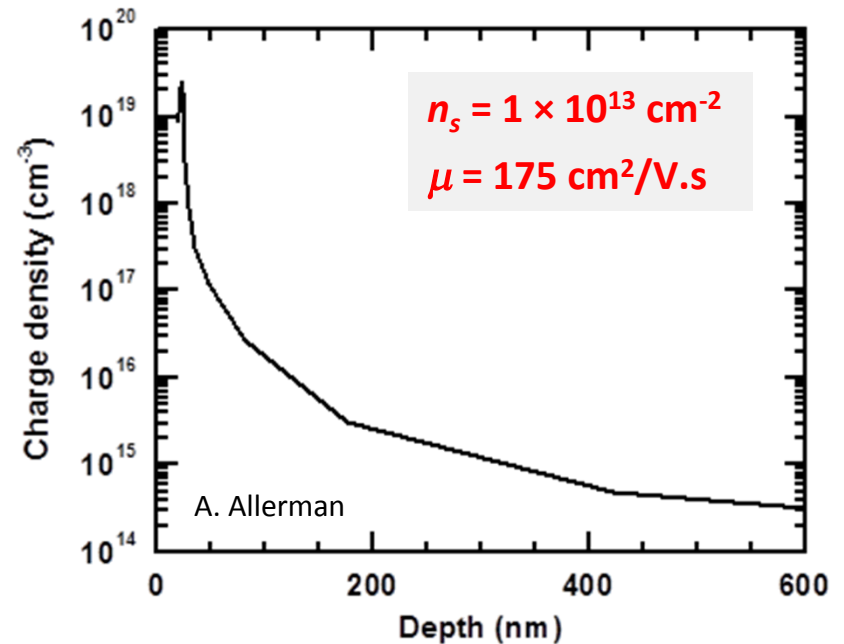
A. Armstrong et al., ICMAT 2015

$\text{Al}_{0.85}\text{Ga}_{0.15}\text{N} / \text{Al}_{0.70}\text{Ga}_{0.30}\text{N}$ Heterostructures

$\text{Al}_{0.85}\text{Ga}_{0.15}\text{N} / \text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ MODFET



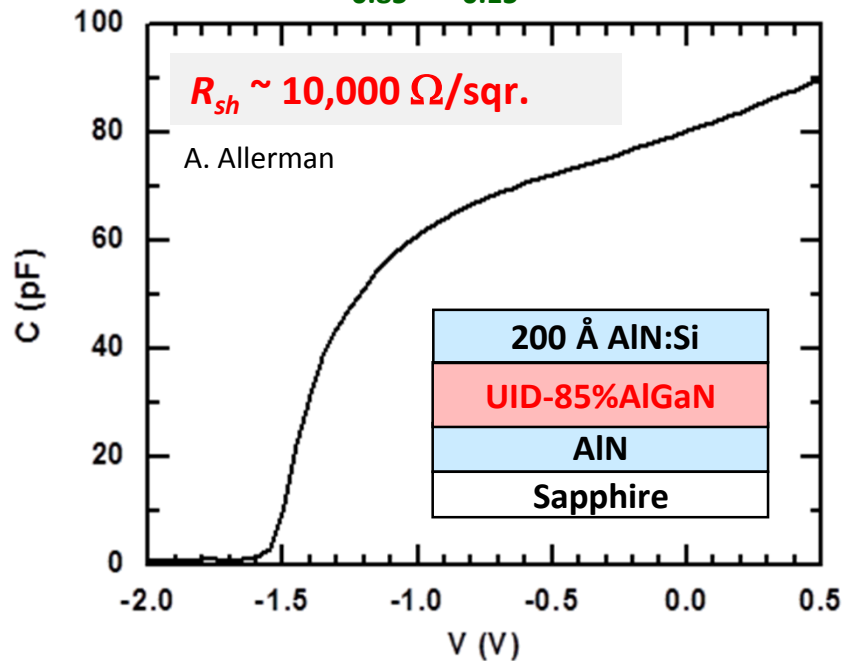
$\text{Al}_{0.85}\text{Ga}_{0.15}\text{N} / \text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ MODFET



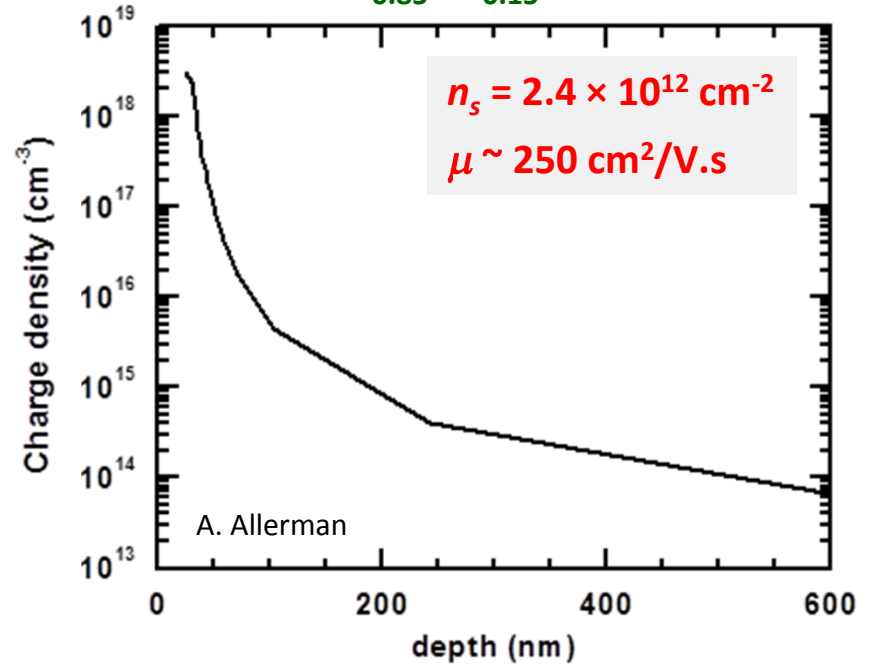
- First demonstration of 2DEG in $\text{Al}_x\text{Ga}_{1-x}\text{N}$ channel for $x > 0.6$
- Achieved $n_s = 1 \times 10^{13} \text{ cm}^{-2}$, $\mu = 175 \text{ cm}^2/\text{V.s}$ in $\text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ channel

AlN / Al_{0.85}Ga_{0.15}N Heterostructures

AlN/Al_{0.85}Ga_{0.15}N MODFET



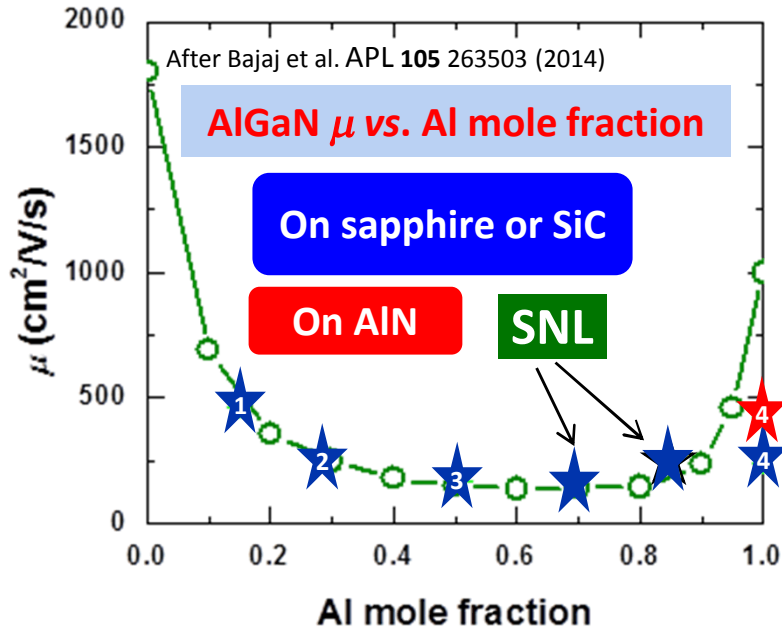
AlN/Al_{0.85}Ga_{0.15}N MODFET



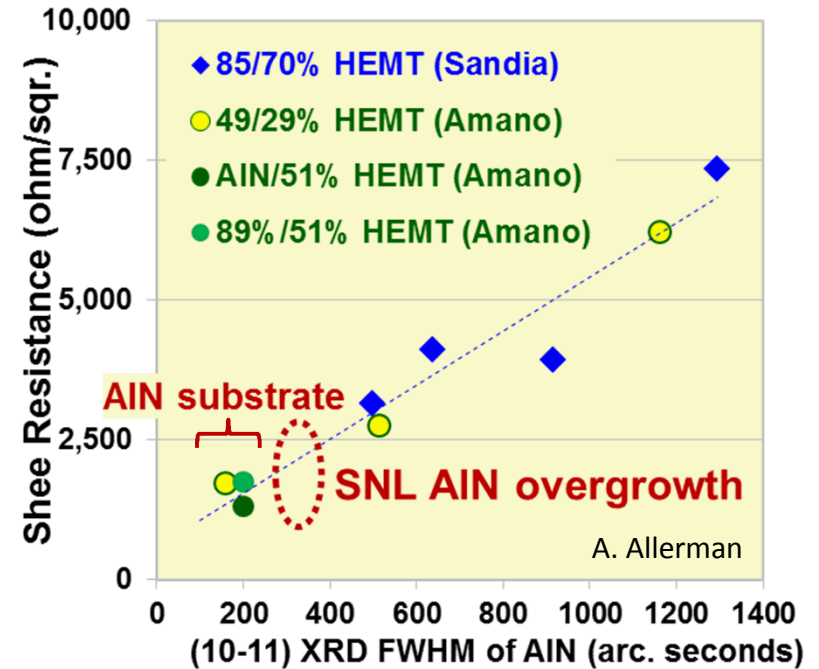
- Achieved $n_s = 2.4 \times 10^{12} \text{ cm}^{-2}$, $\mu \sim 250 \text{ cm}^2/\text{V.s}$ in Al_{0.85}Ga_{0.15}N channel
- Largest Al mole fraction exhibiting 2DEG

A. Armstrong et al., ICMAT 2015

Challenge: Channel Mobility and Sheet Resistance



1. Nanjo et al. IEEE TED **60** 1046 (2013)
2. Hashimoto et al. SEI Tech. Rev. **71** 83 (2010)
3. Hashimoto et al. PSSA **209** 501 (2012)
4. Taniyusa et al. APL **89** 182112 (2006)



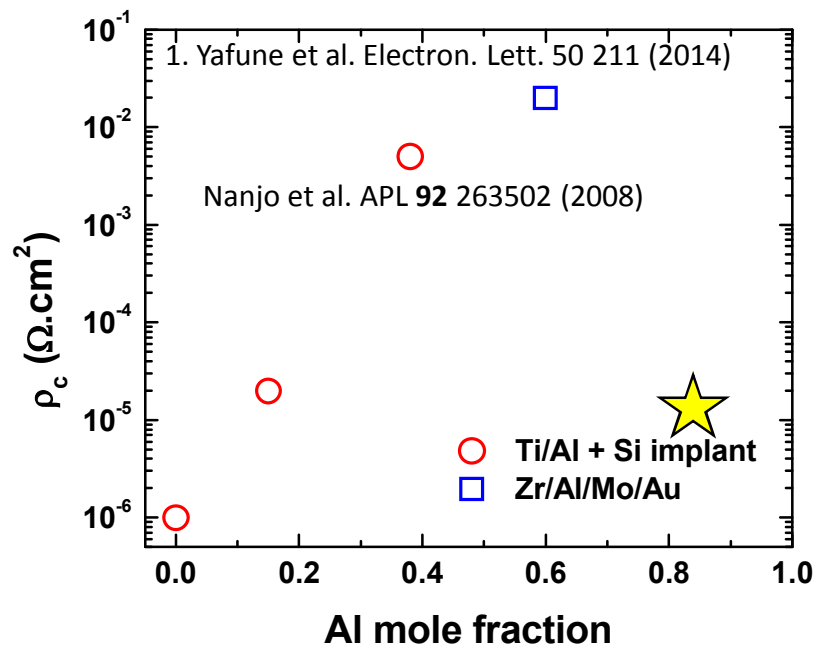
Hashimoto et al. SEI Tech. Rev. 71 83 (2010)
Hashimoto et al. PSSA **209** 501 (2012)

- Sandia AlGaN channel quality tracks with SOA
- $R_{sh} < 2500 \Omega/\text{sqr.}$ achievable with threading dislocation reduction

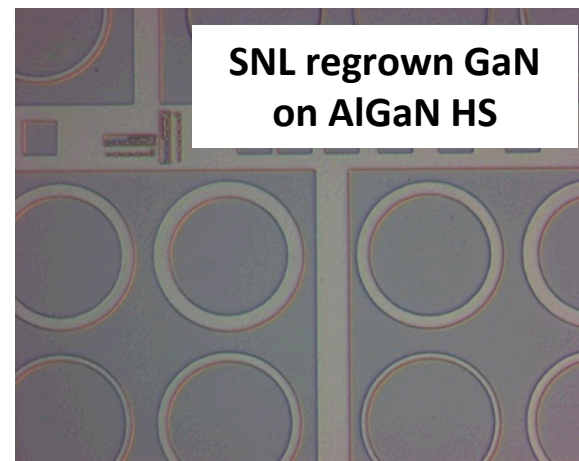
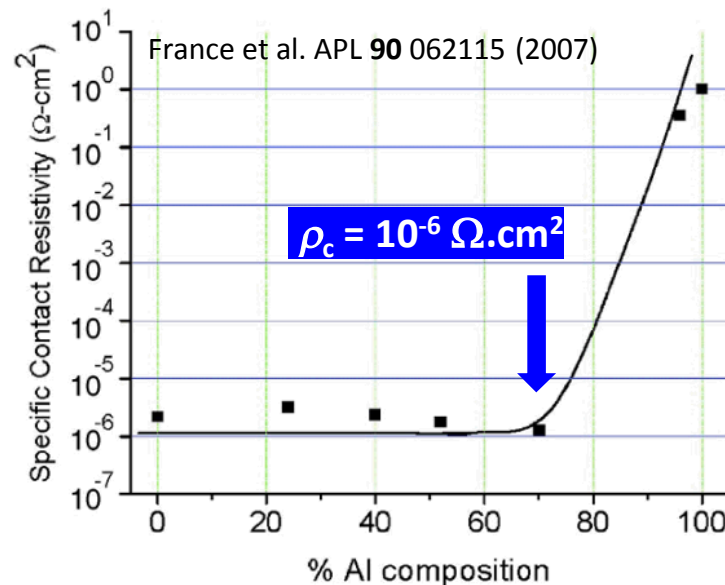
A. Armstrong et al., ICMAT 2015

Challenge: Ohmic Contacts

ρ_c increases rapidly with alloying



- Planar/surface Ohmic contacts are a significant challenge
- Re-grown AlGaN contacts are likely required



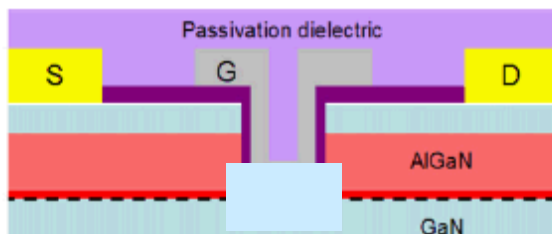
A. Allerman / E. Douglas

A. Armstrong et al., ICMAT 2015

Challenge: Normally-Off Devices

Su et al., SST 28
074012 (2013)

Recessed Gate HEMT



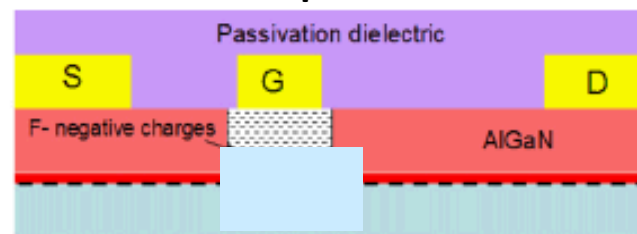
- Gate etch damages channel quality
- Gate leakage concerns
- Low yield across wafer

p-type Gate HEMT



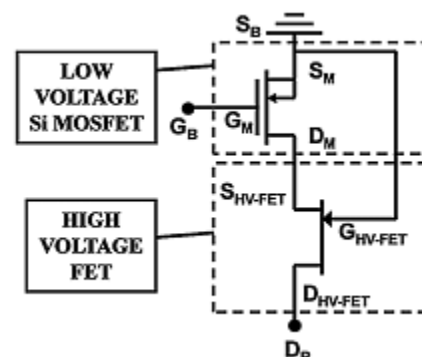
- Highly defective *p*-AlGaN produces dynamic R_{on}
- Mg is undesirable in MOCVD HEMT epi
- Unclear if *p*-type UWBG AlGaN possible

F-implant HEMT



- F- implant damages channel quality
- Long-term stability of F⁻ ions uncertain

Cascode

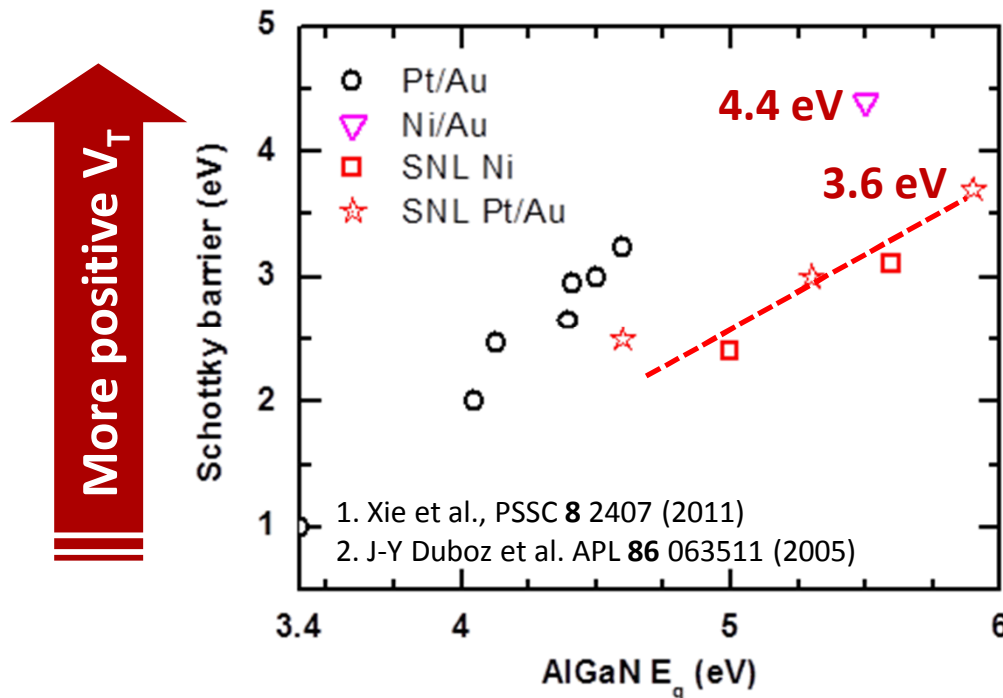


Baliga, SST 28 074011 (2013)

- Lose thermal margin gains
- Lose switching speeds gains

Strategies for E-mode GaN increase cost and degrade reliability/performance

High Schottky Barriers for E-Mode Operation



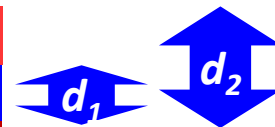
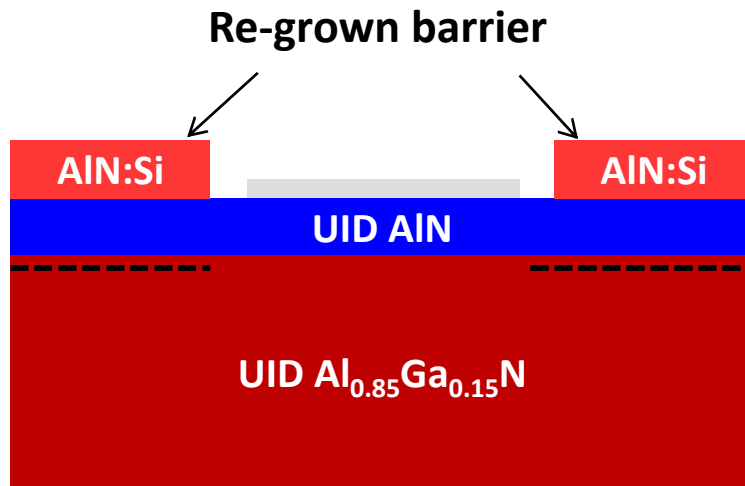
*AlGaIn Schottky
barrier vs. alloying*

$$V_{th} = \frac{\phi_B}{q} - \frac{\Delta E_c}{q} - \frac{qN^+d^2}{2\epsilon}$$

- $\phi_B > 4$ eV for $\text{Al}_{0.8}\text{Ga}_{0.2}\text{N}$
- Sandia achieved $\phi_B = 3.6$ eV for $\text{Al}_{0.9}\text{Ga}_{0.1}\text{N}$
- $> +3$ V gain in V_T for $\text{AlN}/\text{Al}_{0.85}\text{Ga}_{0.15}\text{N}$ compared to GaN HEMTs

A. Armstrong et al., ICMAT 2015

Combine High Schottky Barrier with Regrown Access Region



$$V_T = \frac{\phi_B}{q} - \frac{\Delta E_c}{q} - \frac{qN^+d_1^2}{2\epsilon}$$

$$n_s = \frac{N^+(d_2^2 - d_1^2)}{2d_2} + \frac{\Delta E_c \epsilon}{d_2} - \frac{\phi_s \epsilon}{d_2}$$

- Non-planar device decouples V_T and $R_{on,sp}$
- Re-grown barrier instead of recess etch to preserve channel quality
- Large AlGaN ϕ_B is critical to preserve sufficient barrier thickness

A. Armstrong et al., ICMAT 2015

Questions?

Contact information:

Bob Kaplar

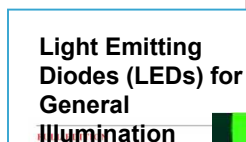
Sandia National Labs

505-844-8285

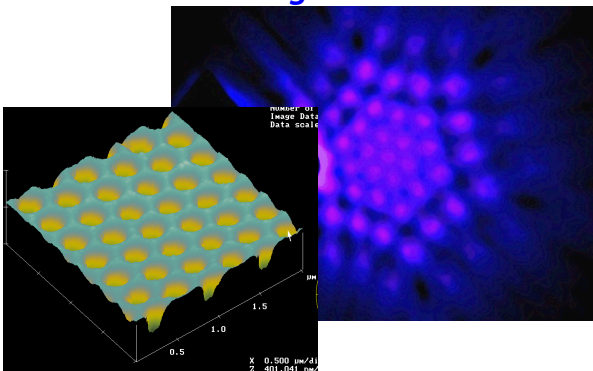
rjkapla@sandia.gov

Backups

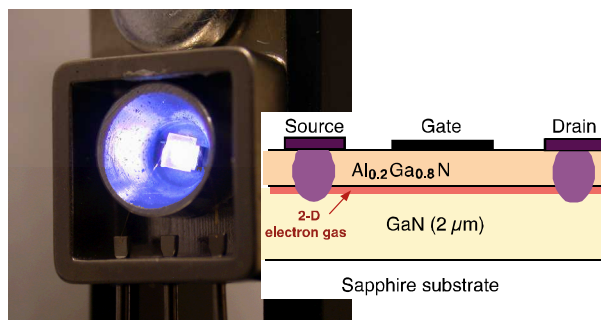
**1999-2006:
Comprehensive US
Technology Roadmaps**



2000-2004: Grand Challenge LDRD

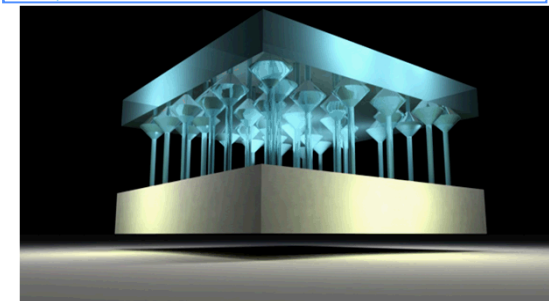


2003-2007: high power amplifiers, UV emitters



**2006-2008: DOE /EERE
National Center for SSL**

2009-2014: DOE EFRC for SSL Science



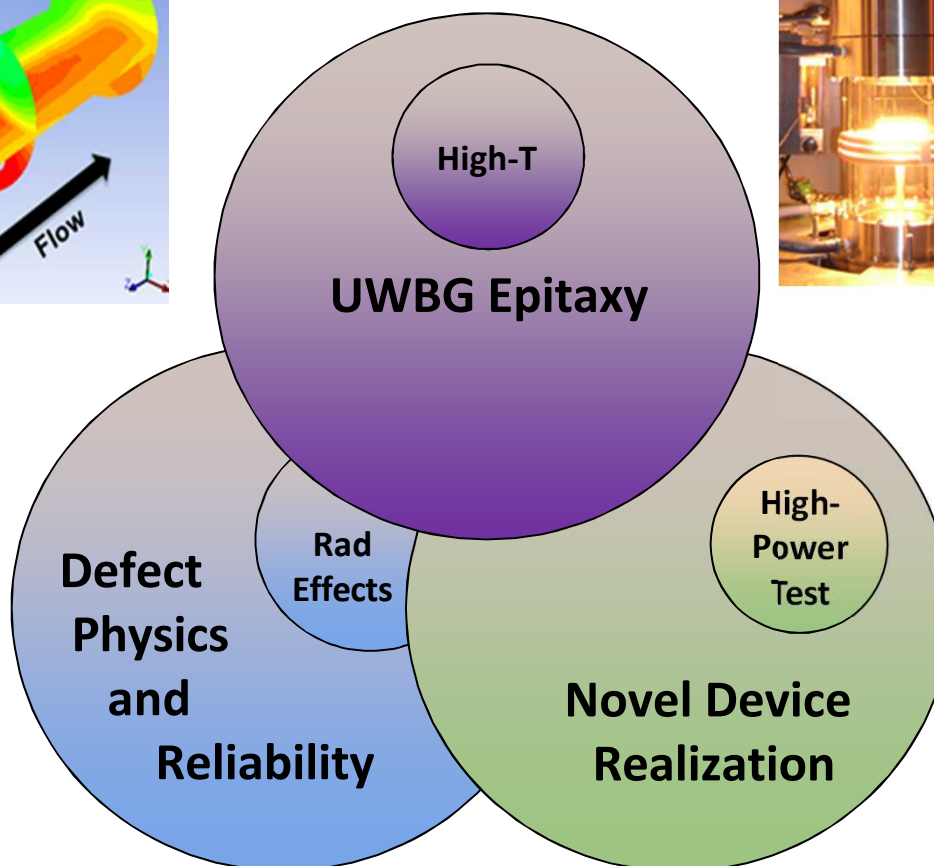
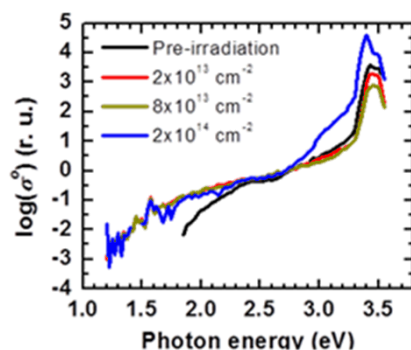
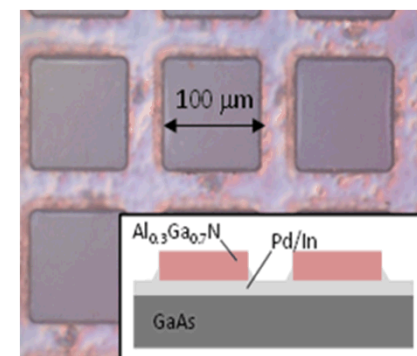
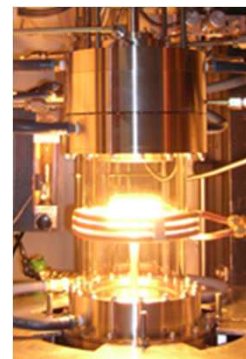
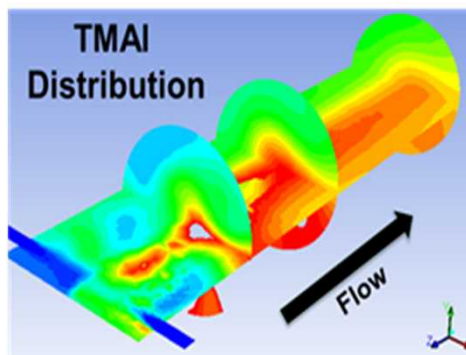
**2003-2012: DOE-Funded
Collaborations with industry**



GeneSiC SiC Thyristors



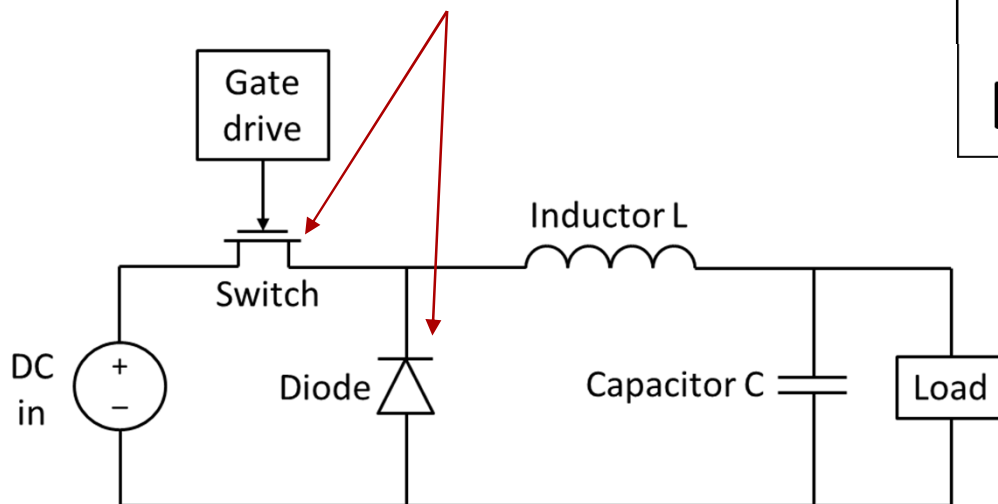
UWBG Project Team Structure



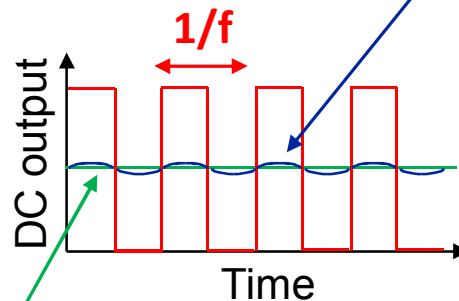
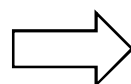
Higher Switching Frequency Enables Reduction in Passive Element Volume and Weight

Power semiconductor devices

Step-Down (Buck) DC-to-DC Converter



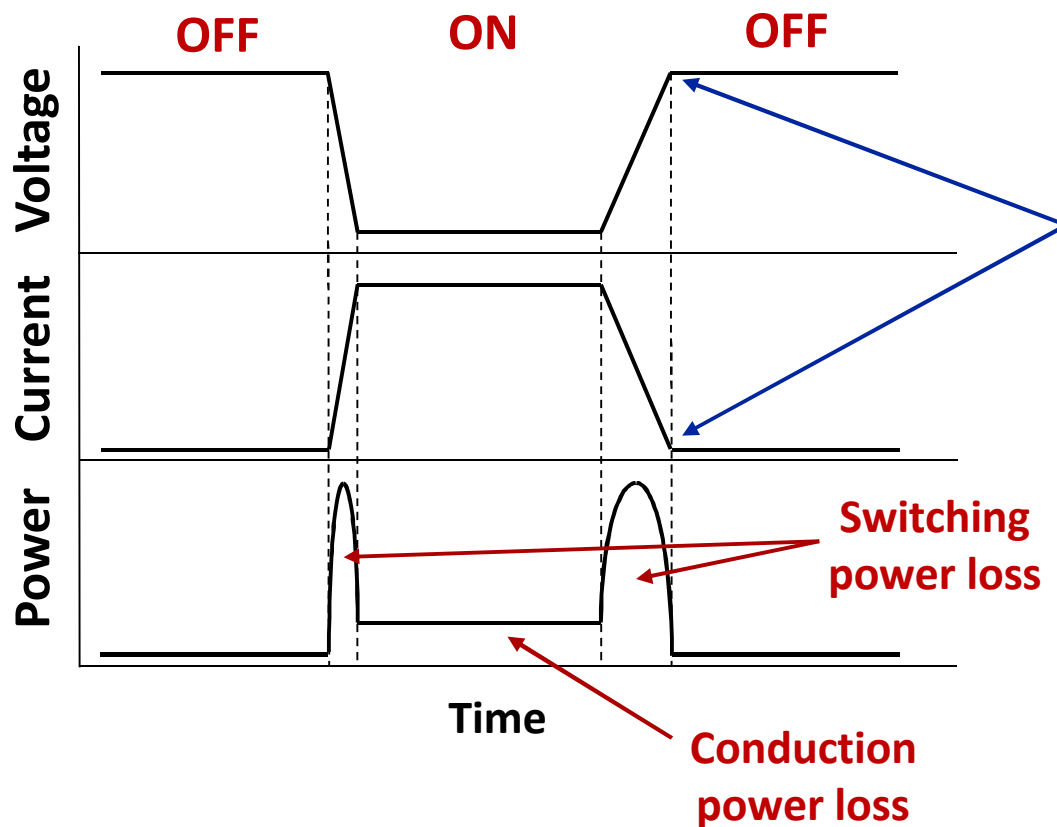
$$\frac{V_{ripple}}{V_{out}} = \frac{1-D}{8LCf^2}$$



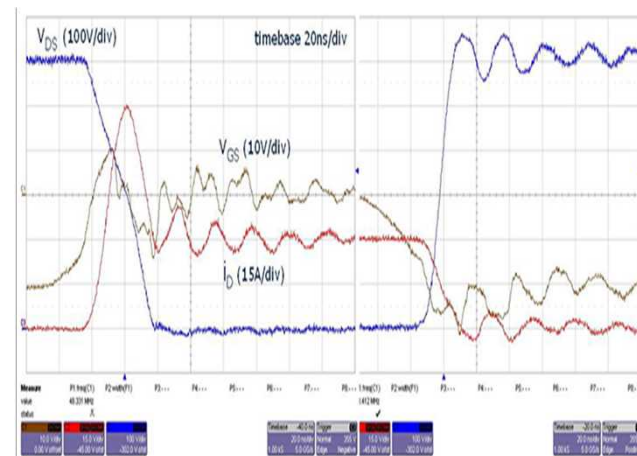
$$V_{out} = DV_{in}$$

Increasing f allows one to reduce L and C while keeping the ripple constant

Heat Generation from Semiconductor Conduction and Switching Losses

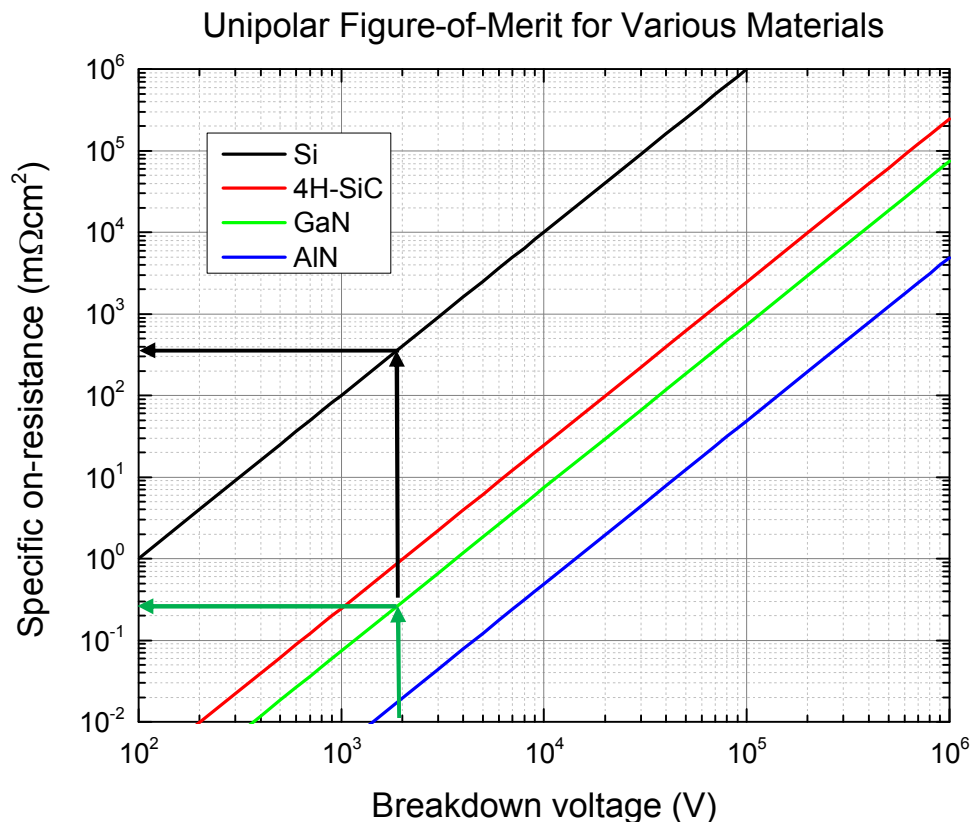


A real circuit will have voltage and current overshoot and oscillations that must be minimized



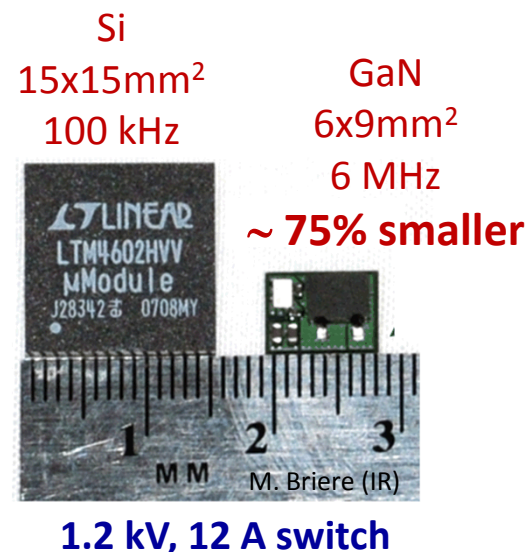
Minimum ON-state loss: *Need low R_{on}*
Minimum switching loss: *Need fast switching transients*

How Do WBGs and UWBGs Lead to Higher Switching Frequency and Lower Loss?

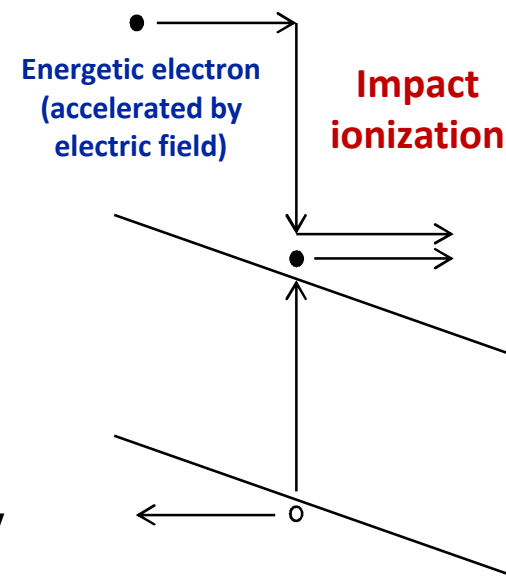
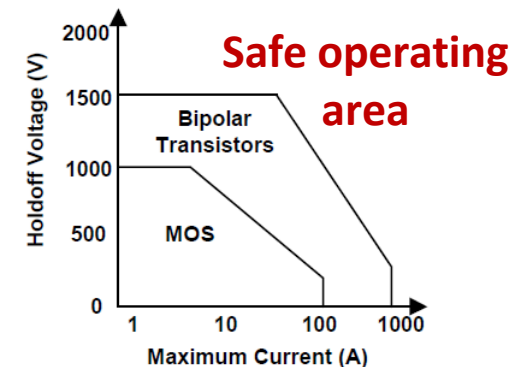
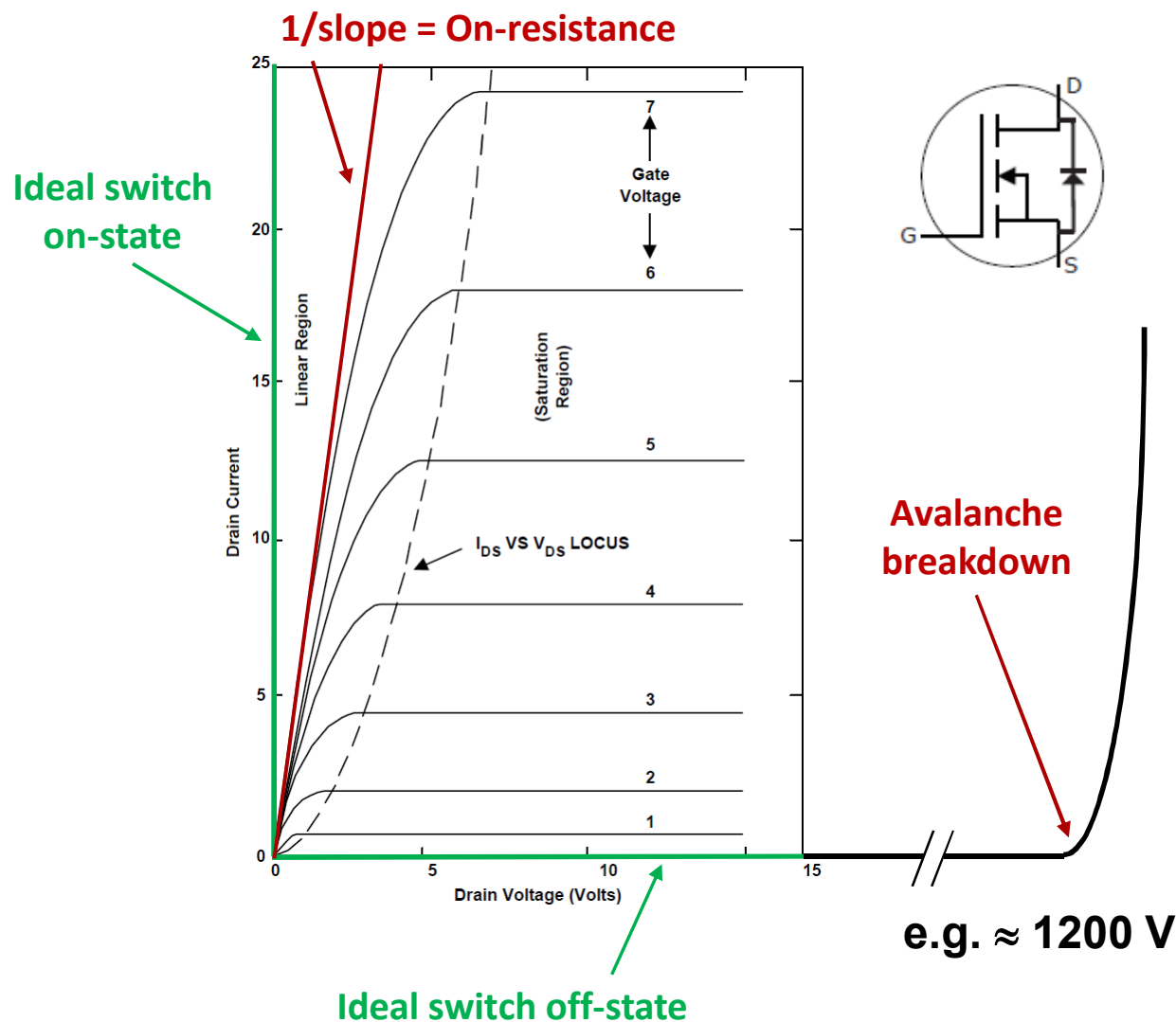


- For equivalent breakdown voltage, get lower $R_{on}A$ for WBG device
 - For same R_{on} , WBG device can have *smaller area*
 - Smaller area results in *less capacitance*
 - Gives a *faster switching transient* and *lower loss per switching cycle*

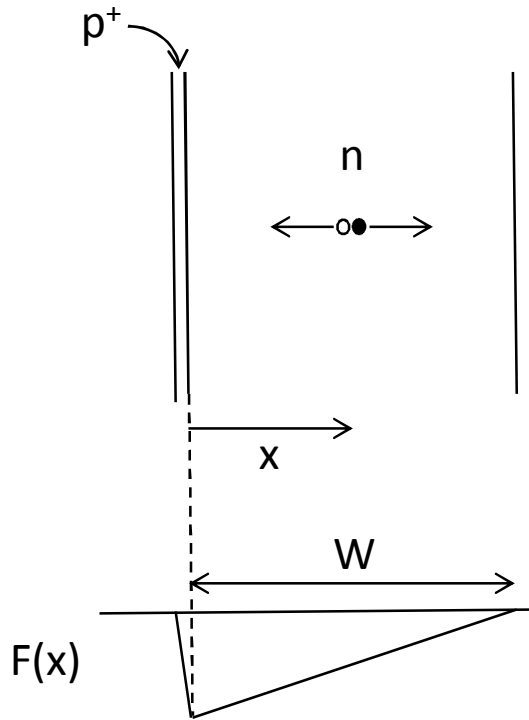
The scaling that results from the properties of WBG and UWBG materials can be utilized to optimize for switching frequency, conduction loss, and switching loss



Semiconductor Devices Are *NOT* Ideal Switches



Impact Ionization in a Depletion Region



Impact ionization coefficient for electrons, holes = α_n, α_p = # of ehps generated per cm by an incident hot electron, hole; may be defined in terms of generation rate:

$$G_{ii} = \alpha_n J_n + \alpha_p J_p$$

Suppose that an electron-hole pair is generated at position x . Then the number of ehps $N(x)$ generated at position x is (1):

$$N(x) = 1 + \int_0^x \alpha_p N(x') dx' + \int_x^W \alpha_n N(x') dx'$$

This can be differentiated to give:

$$\frac{dN}{dx} = (\alpha_p - \alpha_n) N(x)$$

The solution of the differential equation is:

$$N(x) = N(0) \exp \left[\int_0^x (\alpha_p - \alpha_n) dx' \right]$$

(1) R. J. McIntyre, "Multiplication Noise in Uniform Avalanche Diodes," IEEE Trans. Elec. Dev. **13**(1), 164 (1966).

Criterion for Avalanche Breakdown

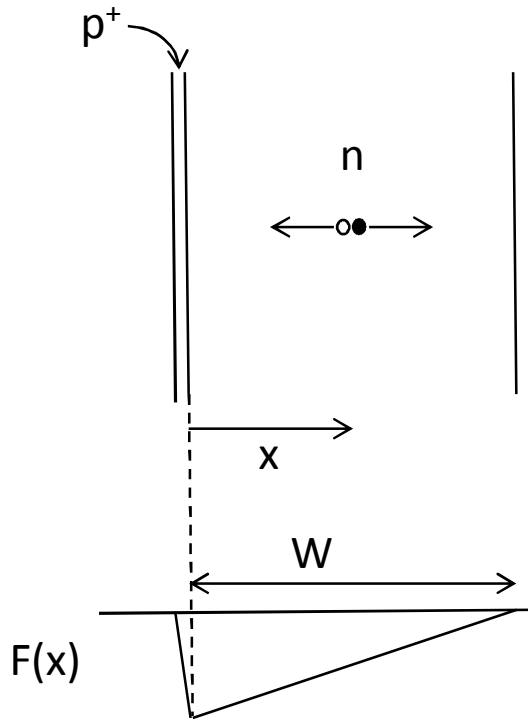
The equations may be combined to give (after some algebra):

$$N(x) = \frac{\exp\left[\int_0^x (\alpha_p - \alpha_n) dx'\right]}{1 - \int_0^W \alpha_n \exp\left[\int_0^x (\alpha_p - \alpha_n) dx'\right] dx}$$

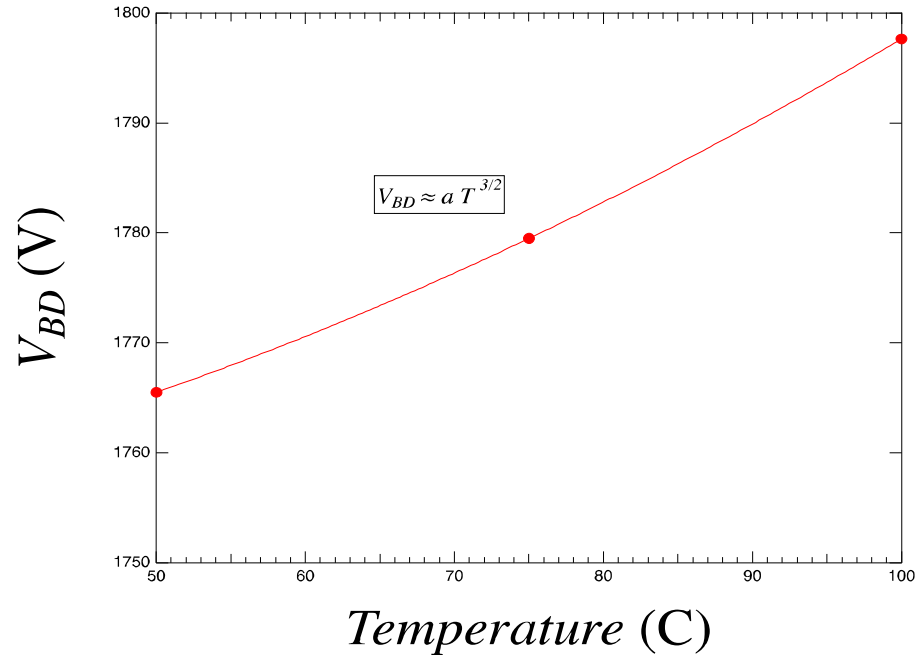
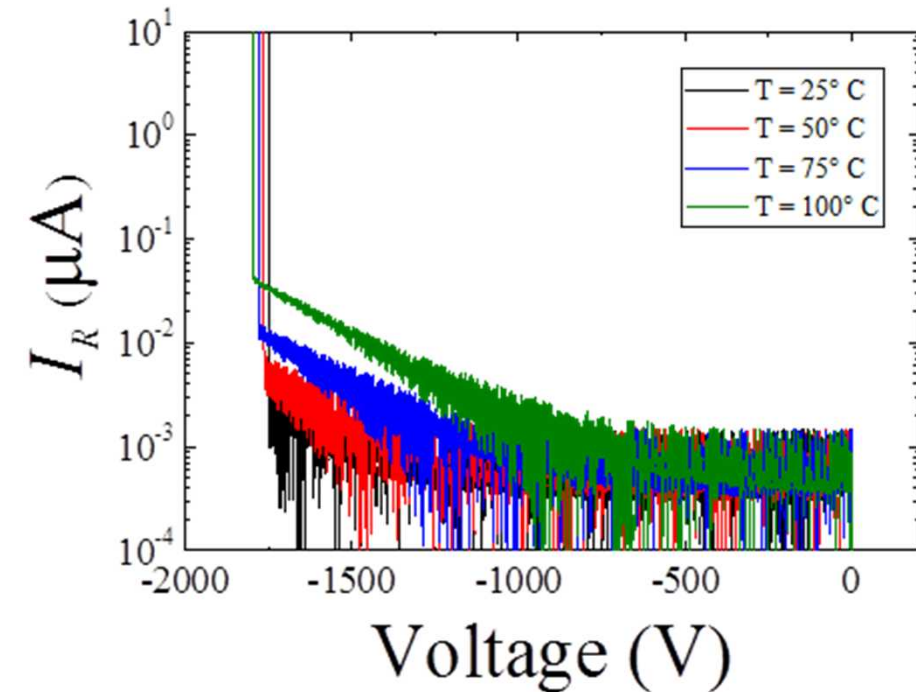
Avalanche breakdown occurs when the number of generated ehps tends to infinity, i.e. when the denominator goes to zero:

$$\int_0^W \alpha_n \exp\left[\int_0^x (\alpha_p - \alpha_n) dx'\right] dx = 1$$

Since α_n and α_p are such strong functions of electric field, in practice this always occurs near the location of peak field, and the majority of the contribution to the integral is from a small volume near this point (i.e. at the junction).

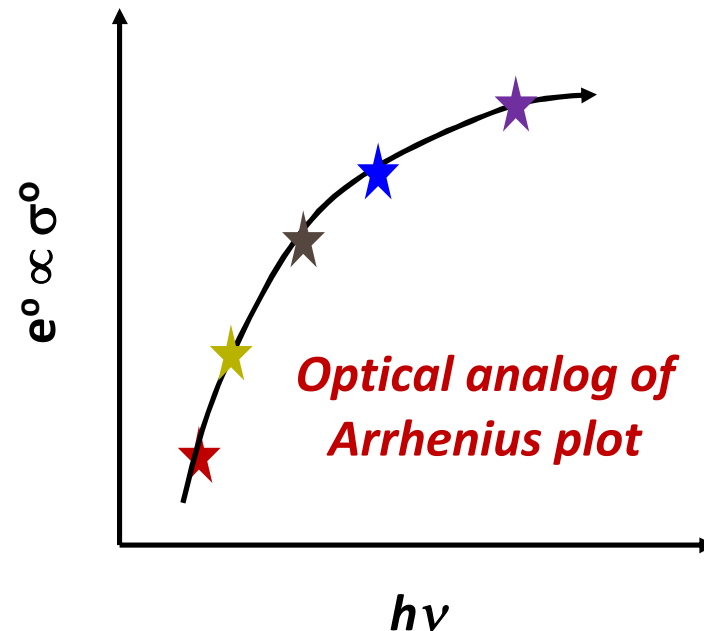
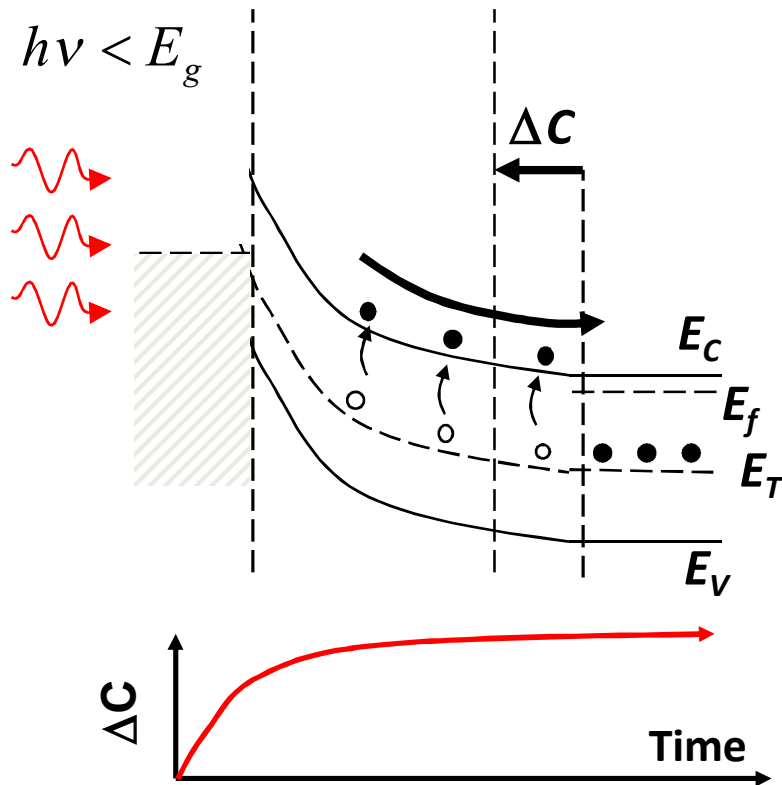


Reverse Breakdown vs. Temperature



- Increasing temperature leads to increased leakage current (possibly generation current)
- V_B vs T exhibits $T^{3/2}$ dependence, consistent with avalanche processes impeded by phonon scattering

Deep Level Optical Spectroscopy



DLOS is able to probe the entire bandgap of GaN

Electrical measurement of optical absorption by deep level defects

- Photocapacitance technique
- Sub-bandgap optical stimulation to photoionize defect levels
- Determine deep level energy E_o from lineshape of $\sigma^o(h\nu)$