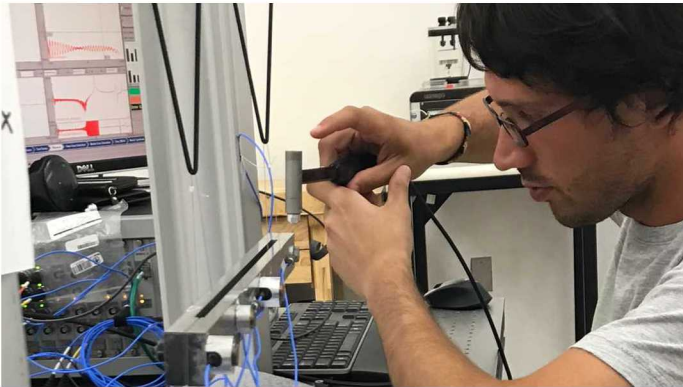
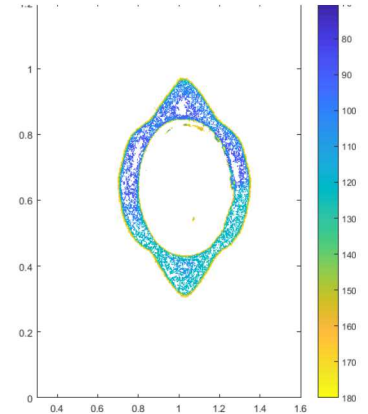
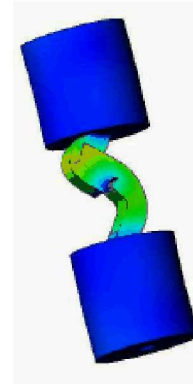


Exceptional service in the national interest



N=O=MAD

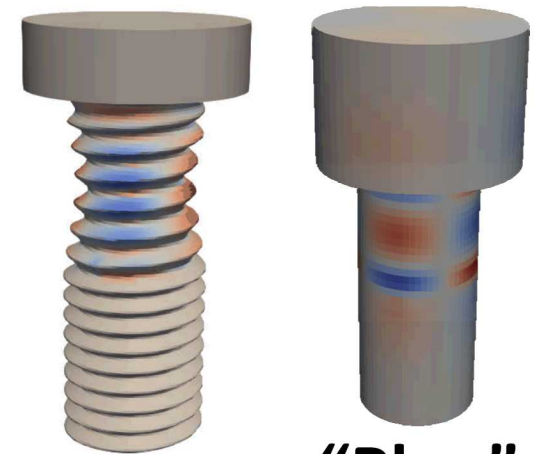
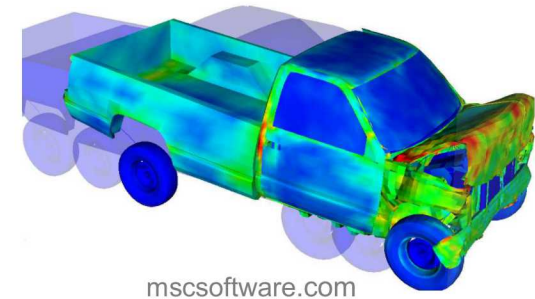
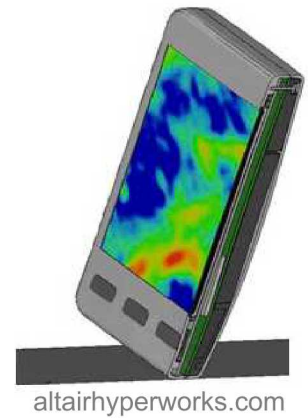


Constructing Optimal Surrogate Models for Bolted Fasteners in Multiaxial Loading

Ernesto Camarena, Anthony Quintana, Victoria Yim

Introduction

- Simulations of structural systems in adverse environments
- Prohibitive computational burden of hundreds of fasteners
- Enormous length scale differences
 - System size, $O(1e3 \text{ mm})$
 - Bolt size, $O(100 \text{ mm})$
 - Thread size, $O(1 \text{ mm})$
- Common fastener modeling
 - So-called “Plug”
 - Analysts rely on pure tension data: no other load angles



“Plug”

Motivation

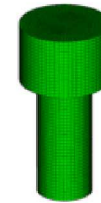
- Research questions:
 - How well do plug models work for an arbitrary loading pull direction?
 - How can plug modeling be modified to improve predictive behavior?
- Solution--Compare plug model to:
 - Experiment data at various load pulls
 - A fully threaded FE model



Methodology: Overview

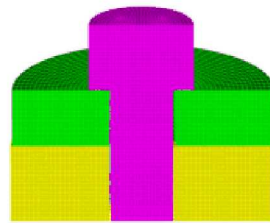
Calibrate Numerical Hardening Curve to Experiments

- Implicit solve, no contact
- 0° load angle (tension only)



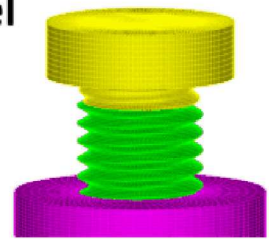
Numerical Plug Model

- Explicit w/ contact
- 0°, 30°, 60°, 90° cases
- Compare w/ experiments @ SNL



Numerical Threaded Model

- Explicit w/ contact
- 0°, 30°, 60°, 90° cases
- Compare w/ experiments @ SNL

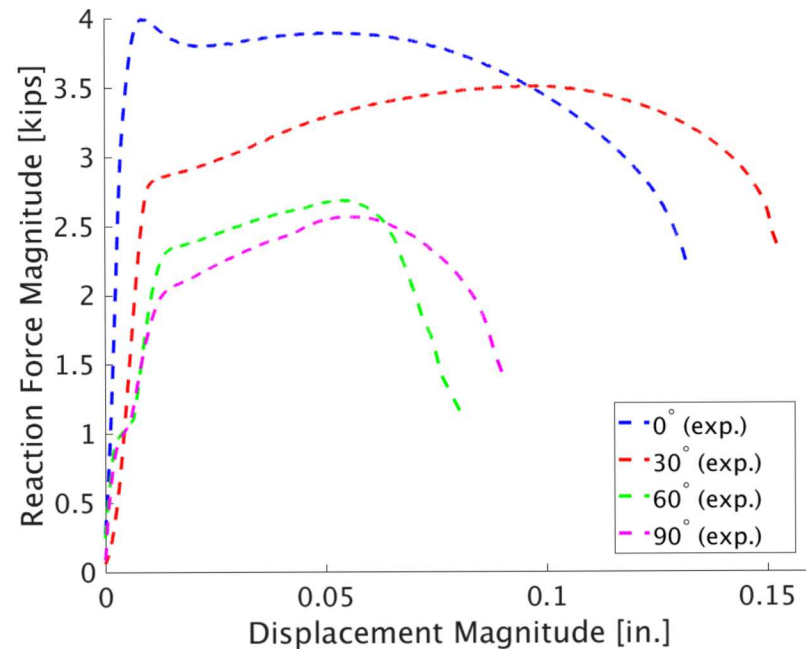
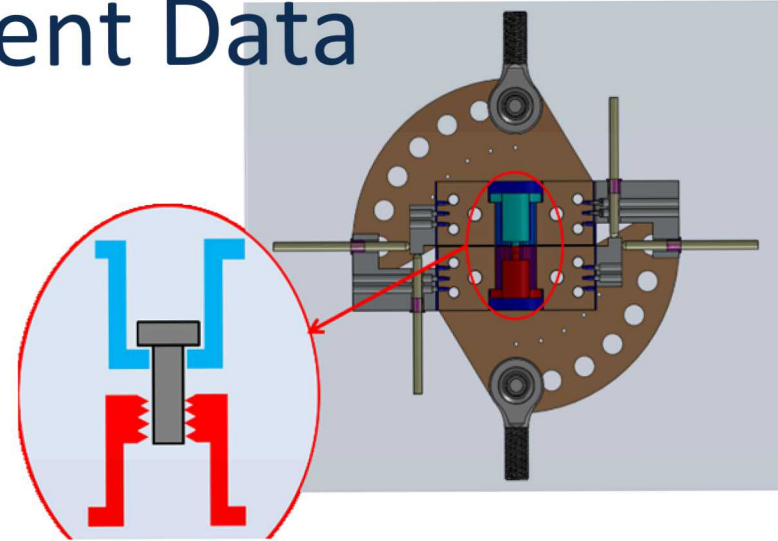
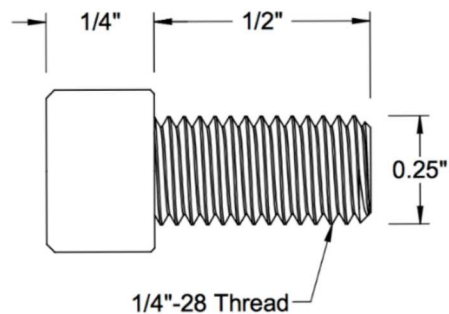


Compare Plug vs. Threaded Model

- 0°, 30°, 60°, 90° cases

Methodology: Experiment Data

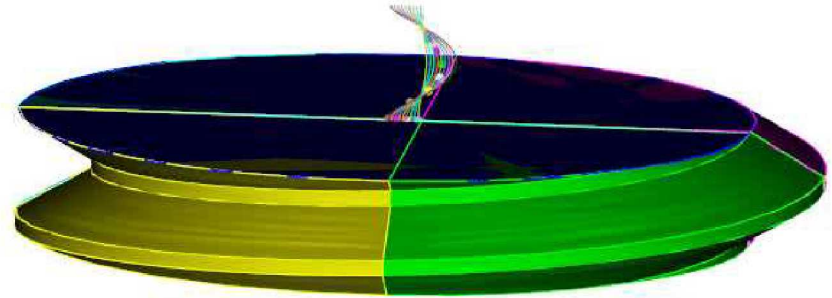
- Multiaxial fastener test setup
 - Setup allows for displacing at various angles
- Fastener details:
 - 18-8 Stainless steel
 - UNF thread type



Methodology: Geometry and Mesh

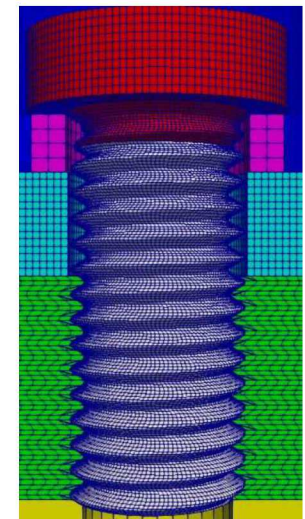
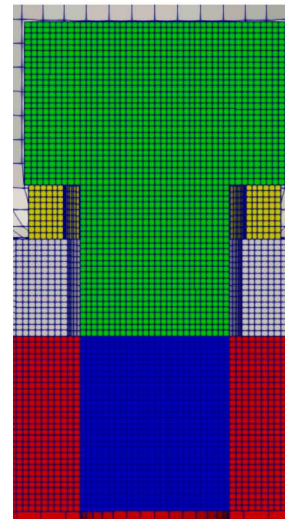
■ Geometry

- Plug uses relatively simple geometry
 - Tensile stress radius
- Threaded model created in slices along helix
 - Fully 3D model



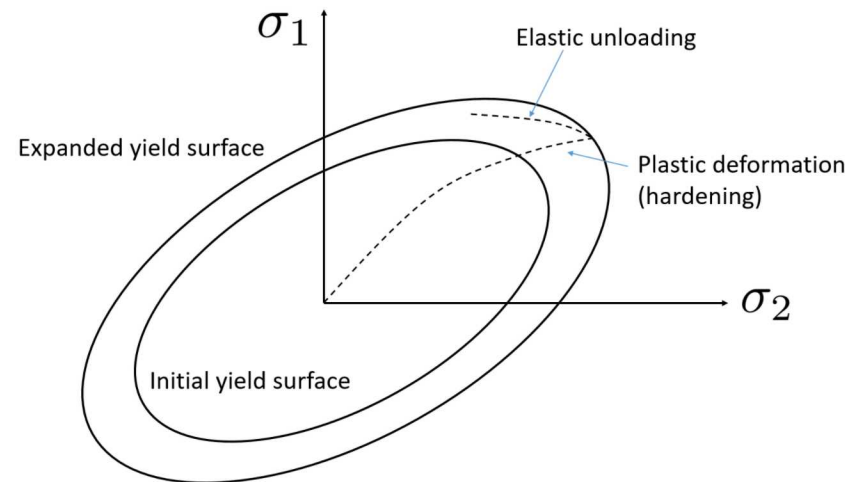
■ Mesh

- Refined regions near fastener
- Coarse mesh for upper and bottom bushing



Methodology: Constitutive Model

- Elasticity: Young's Modulus = $30e6$ psi, Poisson's Ratio = 0.3
- Plasticity
 - Isotropic Hardening
 - Multi-linear elastic-plastic hardening curve
 - Yield stress = $93e3$ psi
 - Yield Surface retains its shape and is symmetric about the origin
 - Increases uniformly as the material deforms plastically
 - Rate independent



Methodology: Failure Criteria

- Hardening Curve Definition: Multi Linear Elastic-Plastic (MLEP)
 - Linear piecewise hardening curve defined with discrete pairs of equivalent plastic strain (EQPS) and yield stress.

$$D_{ij} = D_{ij}^e + D_{ij}^P$$

- Failure Models
 - Element death based on EQPS limit.
 - Ductile Failure Model (ml_ep_fail)
 - Failure in a given element initiates when its tearing parameter (t_p) reaches a critical value. The element stiffness then decreases with increasing crack opening strain (strain in the direction of the max principal stress).

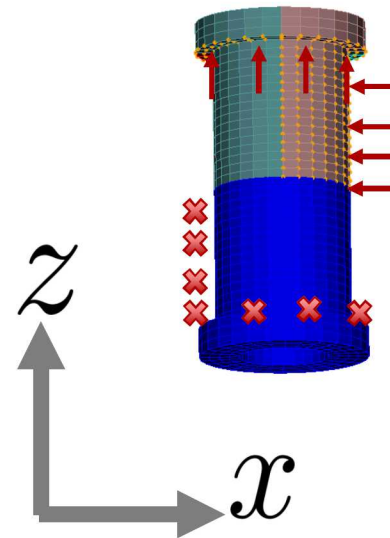
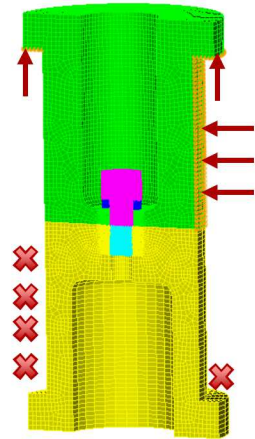
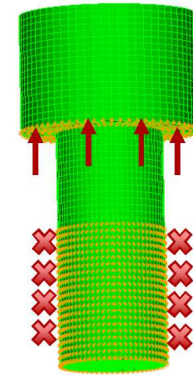
Methodology: Boundary Conditions

- Basic Plug

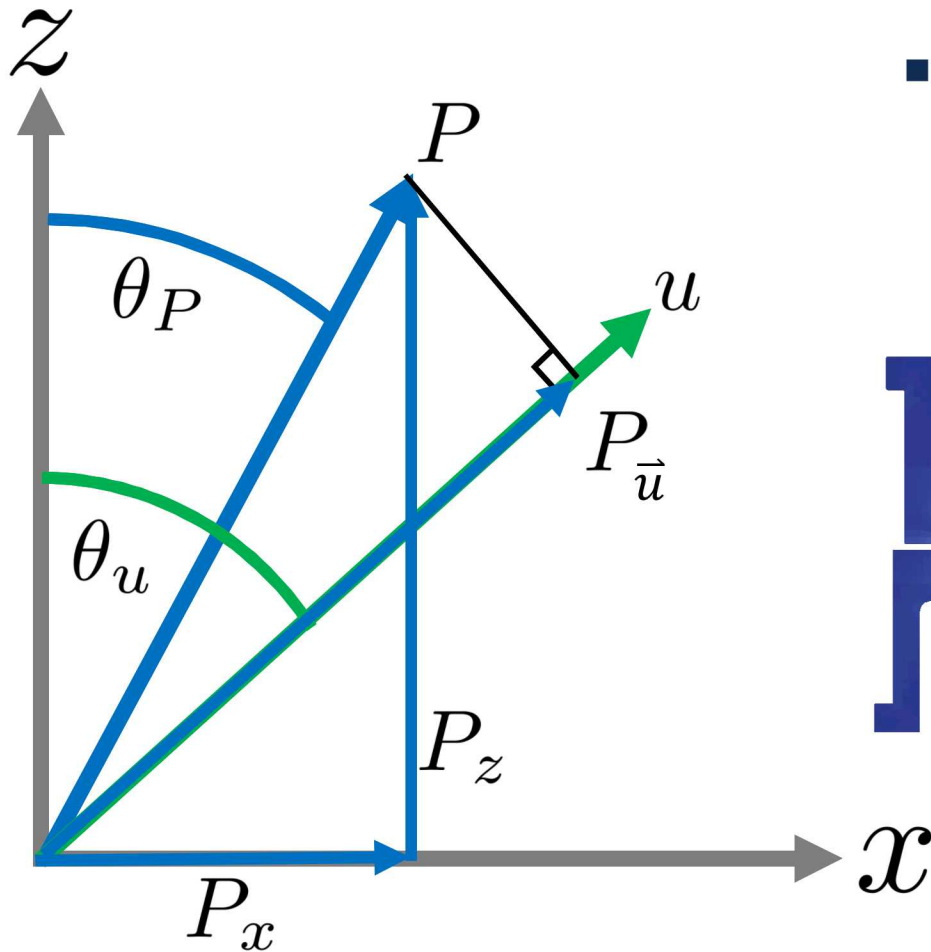
- 0° case: only +z displacement

- Plug with Bushings & Threaded Model

- 0° case:
 - Displace +z face of upper bushing
 - Fixed lower z face of bottom bushing
- 30° , 60° , and 90° case:
 - Displace +x face of upper bushing
 - Displace +z face of upper bushing
 - Fixed lower -x face of bottom bushing
 - Fixed lower z face of bottom bushing

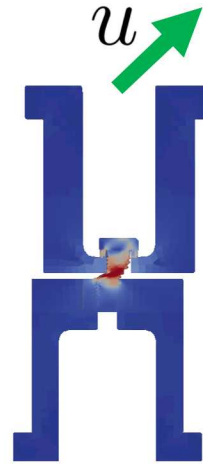


Methodology: Post-Processing



- Load projection

- 30° & 60°

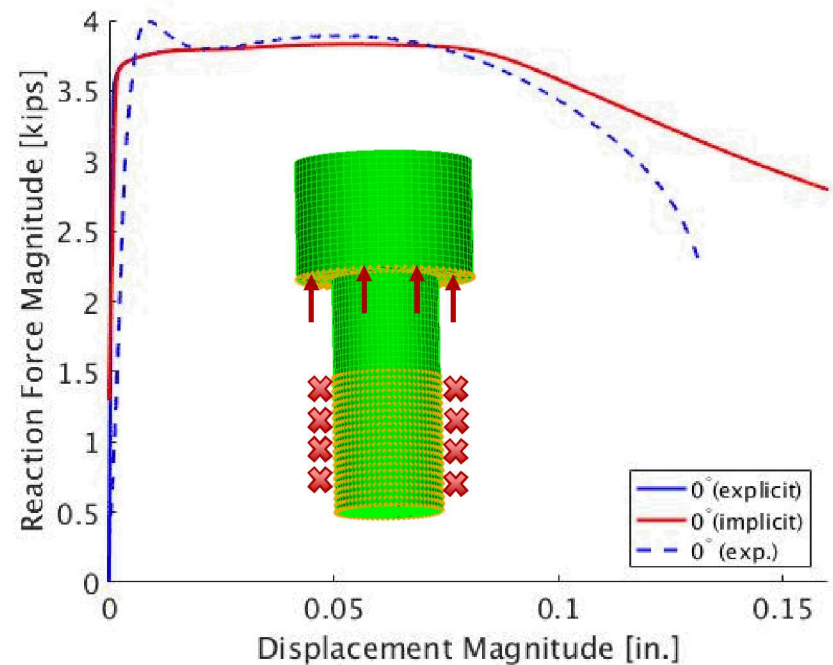


$$\theta_P = \arctan\left(\frac{P_x}{P_z}\right)$$
$$P_{\vec{u}} = P \cos(\theta_u - \theta_P)$$

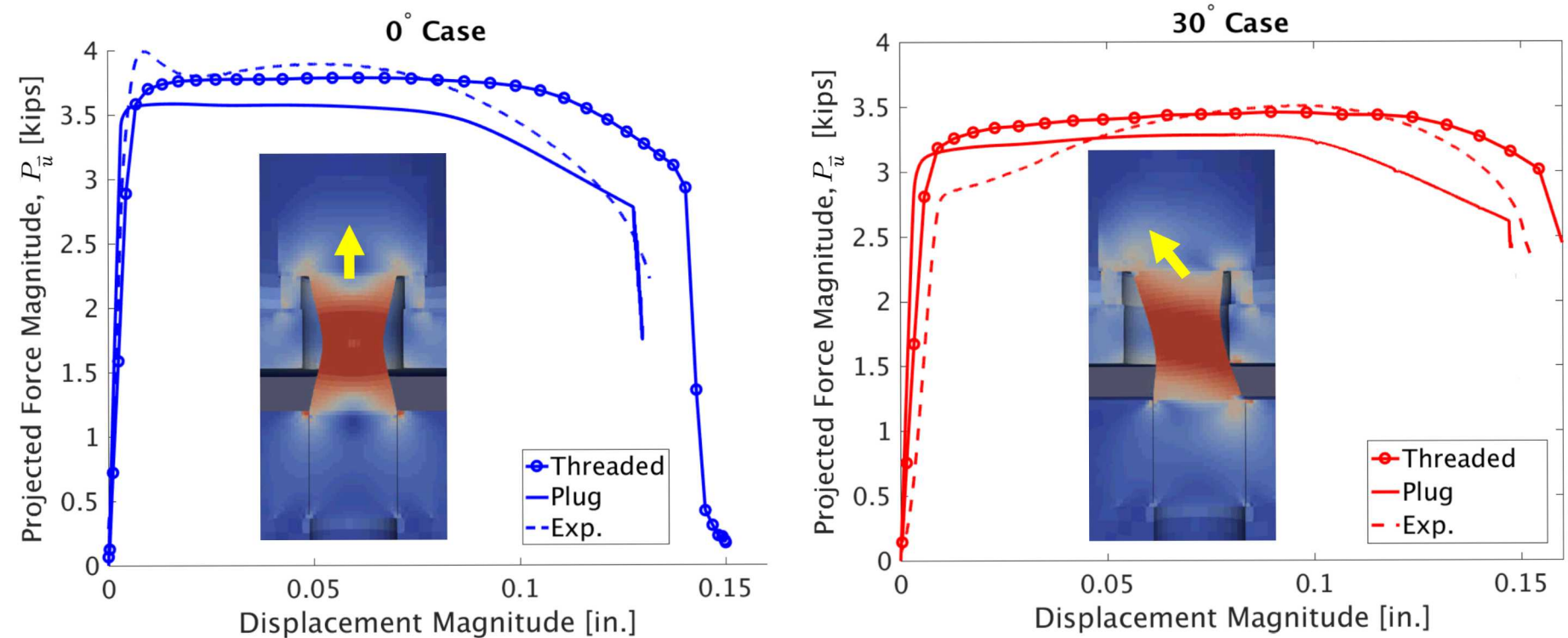
- Smoothing: moving average

Methodology: Numerical Procedures

- Implicit vs. Explicit
 - In order to account for the frictional contact between the plug and bushing an explicit model is required
 - For calibration purposes, the basic plug is analyzed using both implicit and explicit models
 - The hardening curve developed for the plug with bushing and threaded model are based on the this basic plug

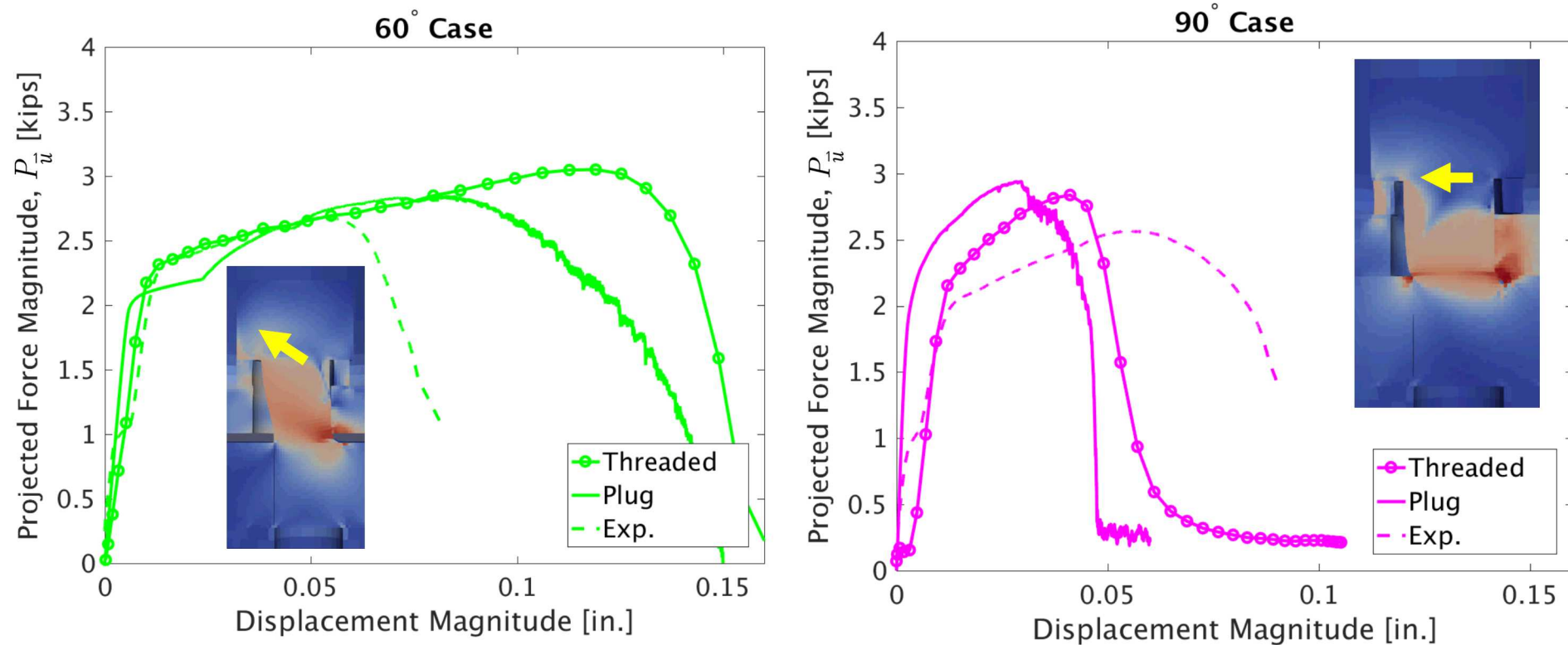


Results: FE vs. Experiments



- Element death on EQPS
- Plug model radius: tensile stress area

Results: FE vs. Experiments



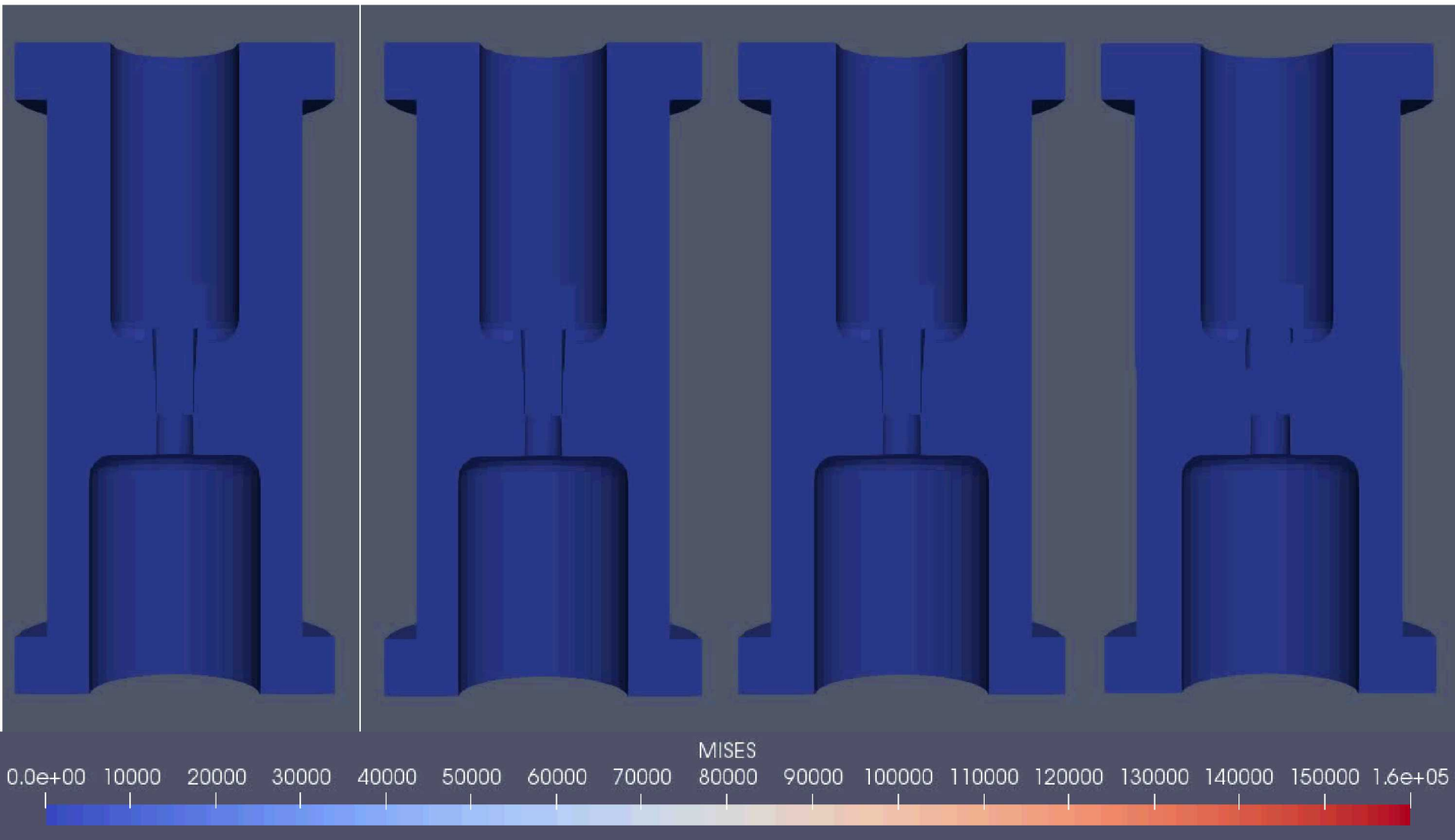
- Element death on EQPS
- Plug model radius: tensile stress area

0°

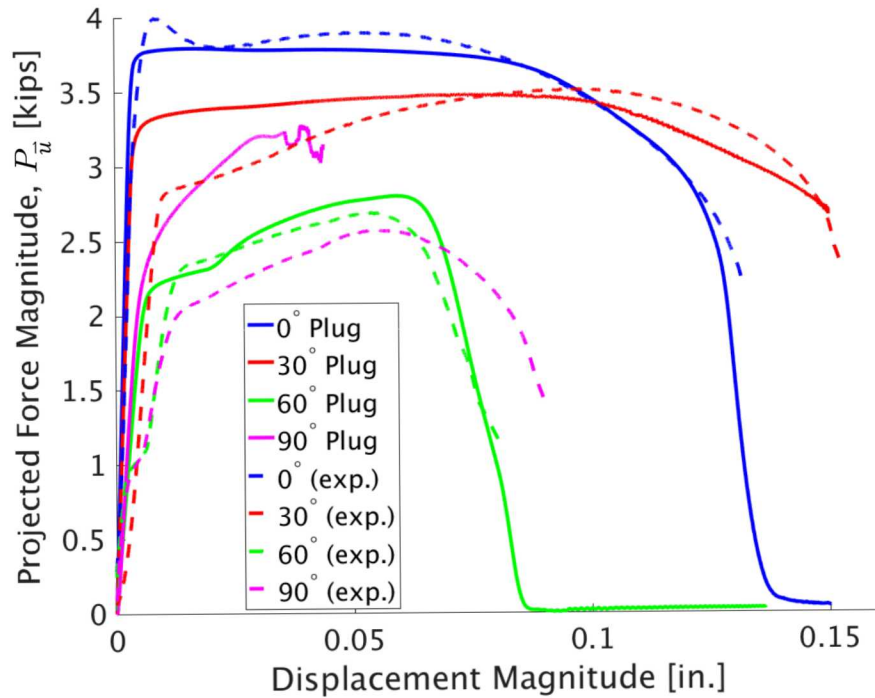
30°

60°

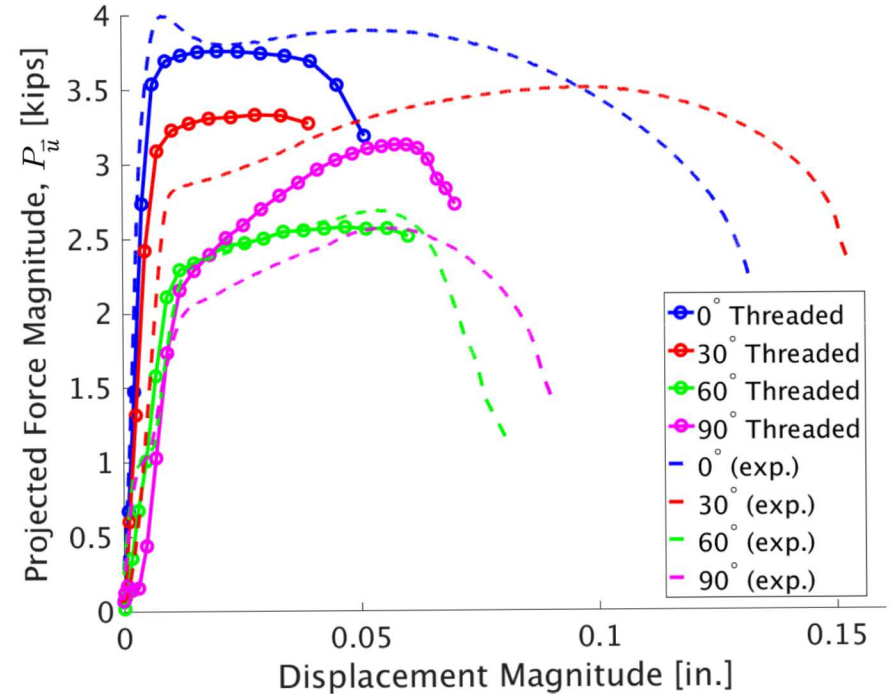
90°



Results: Ductile Damage Failure Model



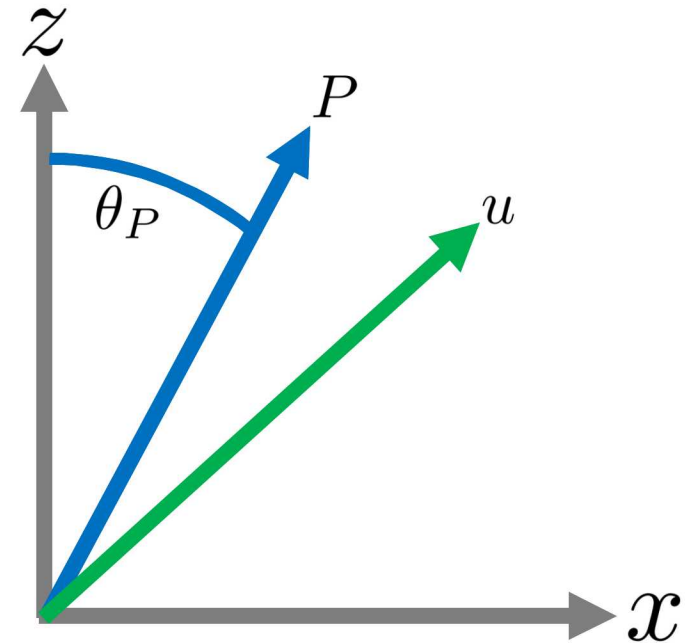
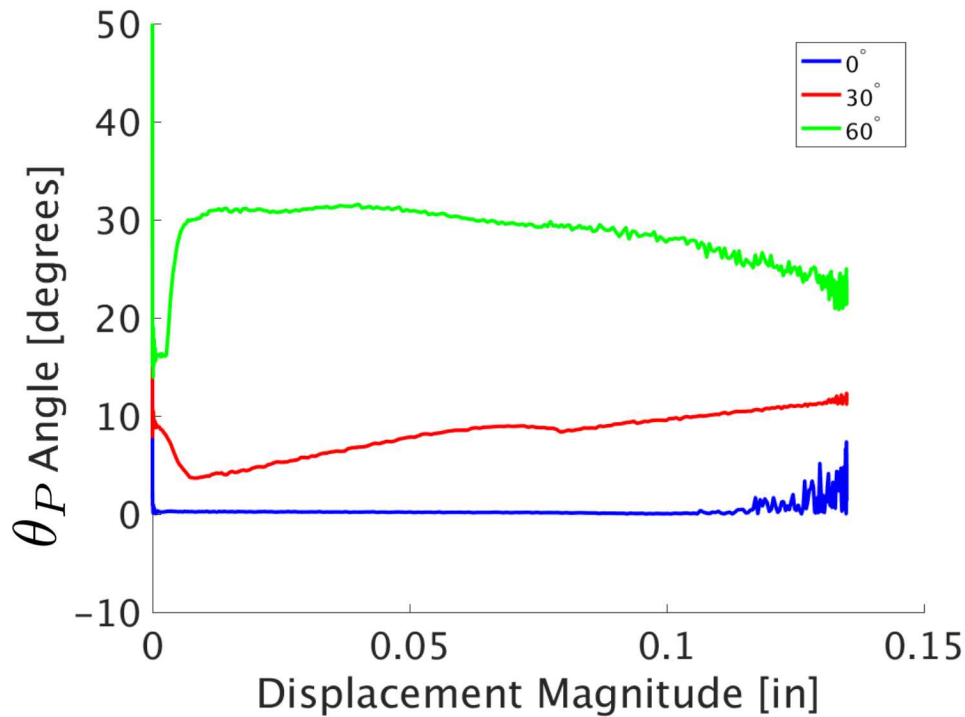
a) Plug Model



b) Threaded Model

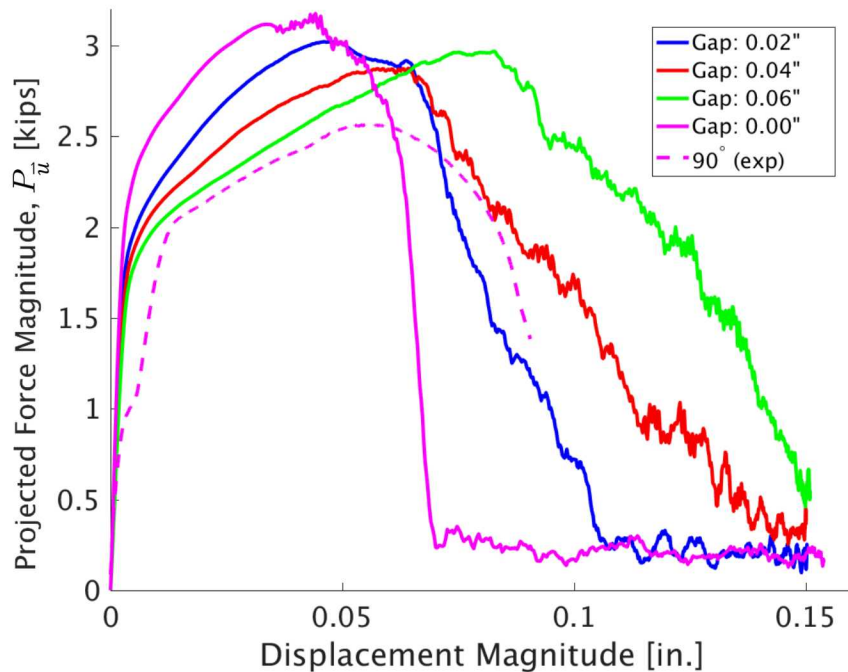
- ml_ep failure shown

Results: Load Angle vs. Displacement

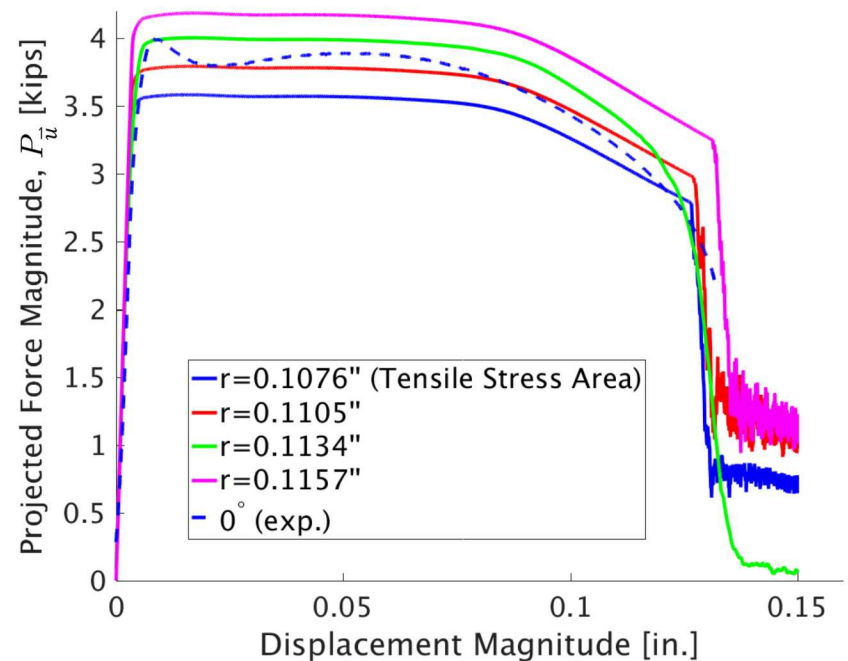


Results: Parameter Studies

- Various studies including: Effect of preload, friction, and yield stress



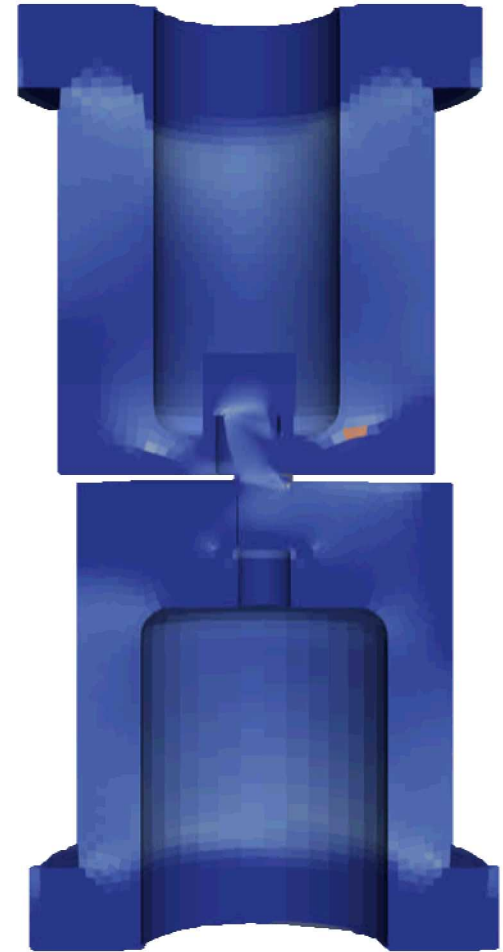
a) Initial bushing gap



b) Plug radius, r

Conclusion

- Plug model comparisons to:
 - Experiment data
 - A fully threaded FE model
- Research answers:
 - Plug models compare favorably for overall load-displacement behavior
 - Agreements to experiments were possible when load projection was considered
 - The failure models considered do not fully capture trends presented in experimental data



Mentor Team

Sandia National Laboratories

Jeffrey Smith

Peter Grimmer

John Mersch

John Emery

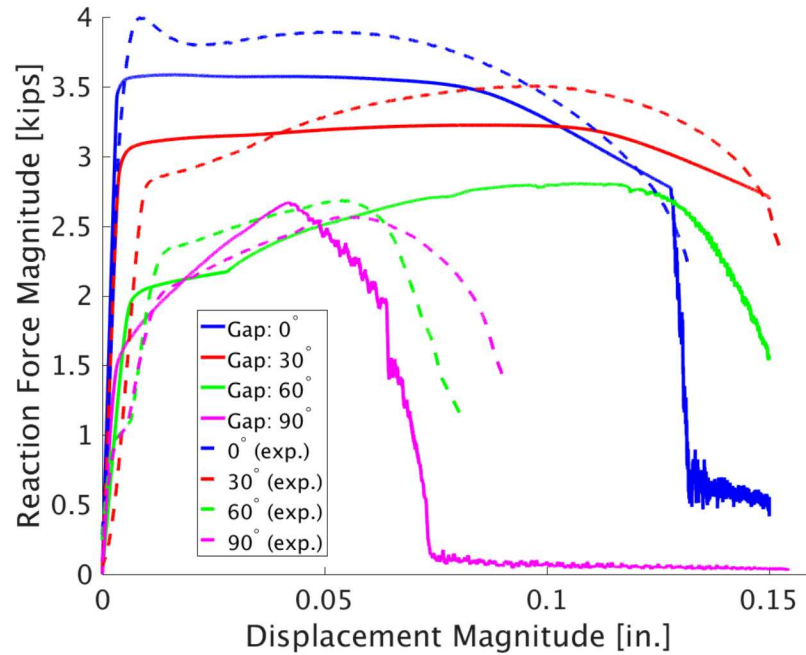
Cranfield University, UK

Gustavo Castelluccio

Acknowledgments

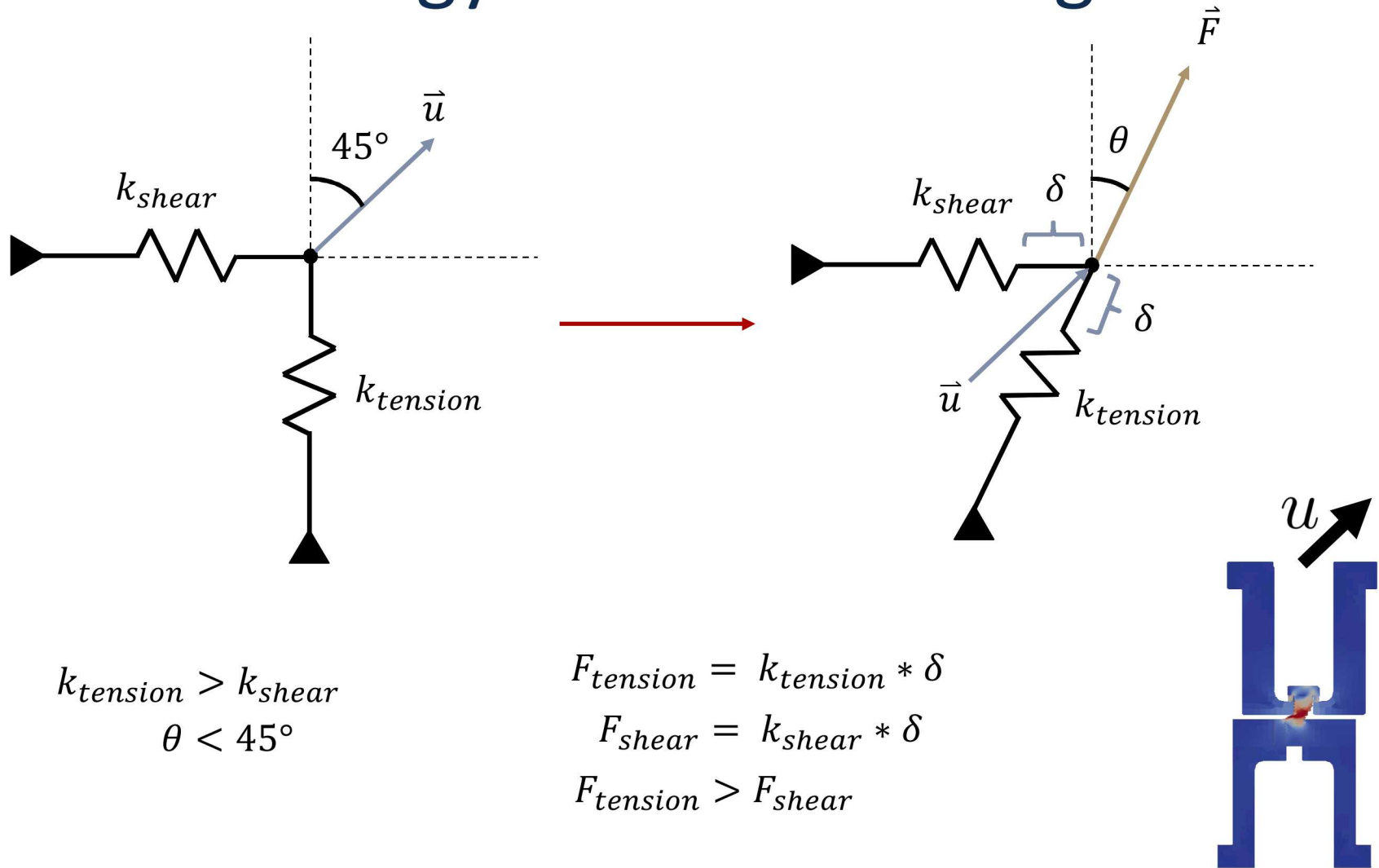
- This research was conducted at the 2018 Nonlinear Mechanics and Dynamics Research Institute hosted by Sandia National Laboratories and the University of New Mexico.
- Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA-0003525.

Backup Slides



a) Plug model with initial gap of 0.04”

Methodology: Post-Processing



Backup Slides

- Von Mises Yield Criterion:

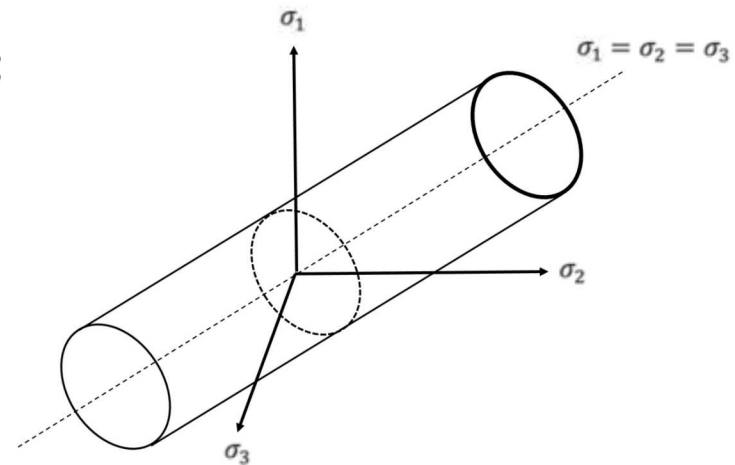
$$\sigma_{vm} = \sqrt{\frac{1}{2}[(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2]}$$

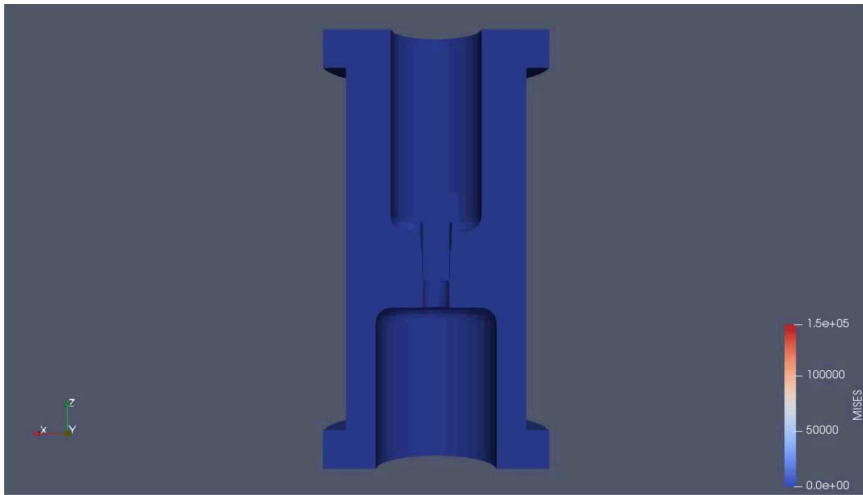
(Where $\sigma_{1,2,3}$ are the principal stresses, respectively)

- This defines a cylindrical 3D yield surface in principal stress space.
 - Axis is along hydrostatic stress states

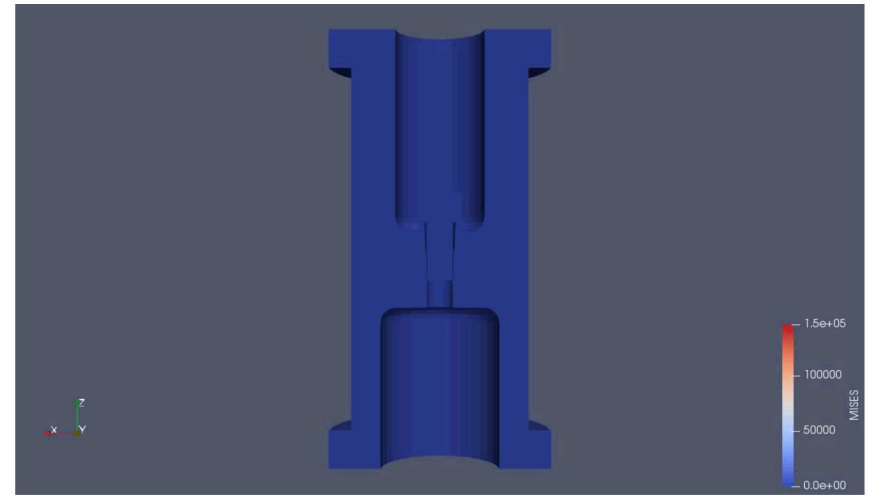
- σ_{vm} comes from deviatoric stress S:

$$\sigma_{ij} = S_{ij} + \frac{1}{3}\sigma_{kk}\delta_{ij}$$
$$J_2 = \frac{1}{2}S_{ij}S_{ij}$$
$$\sigma_{vm} = \sqrt{3J_2}$$

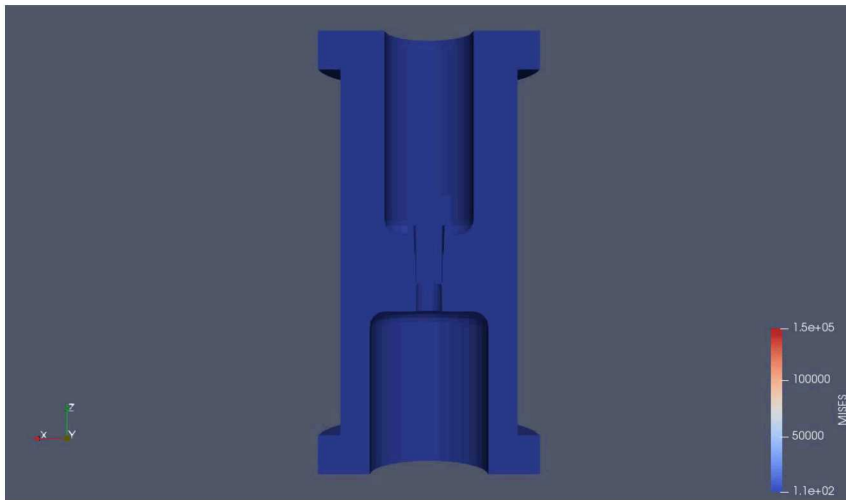




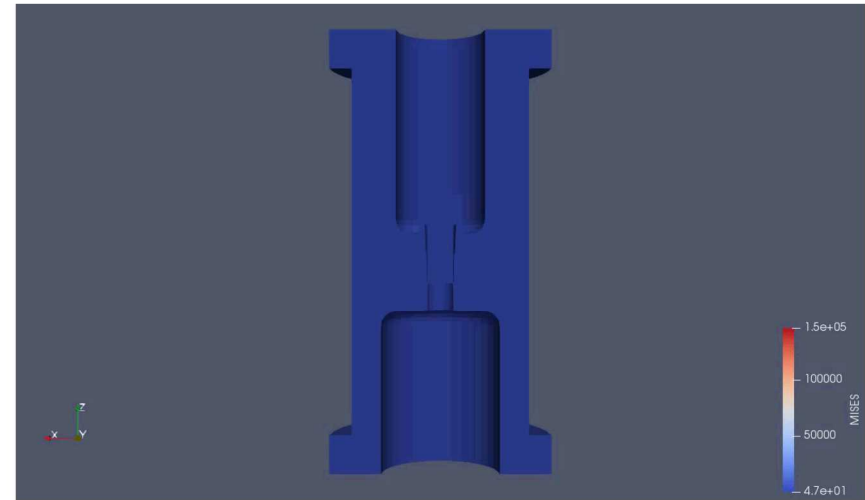
0-deg



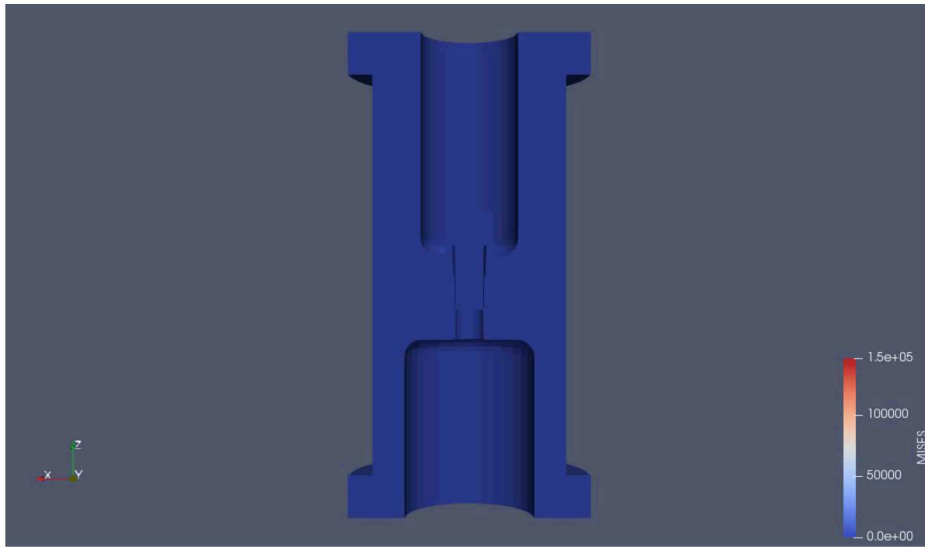
0-deg with tear



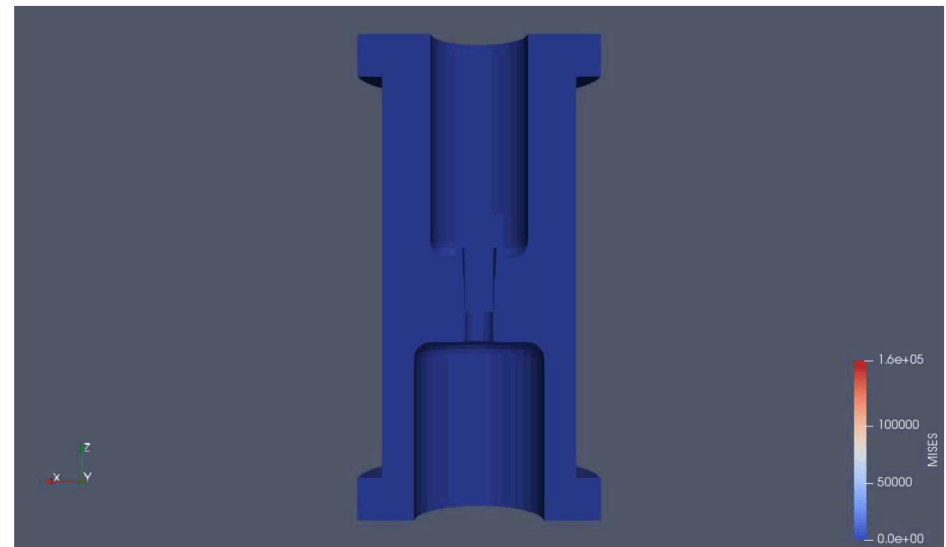
30-deg



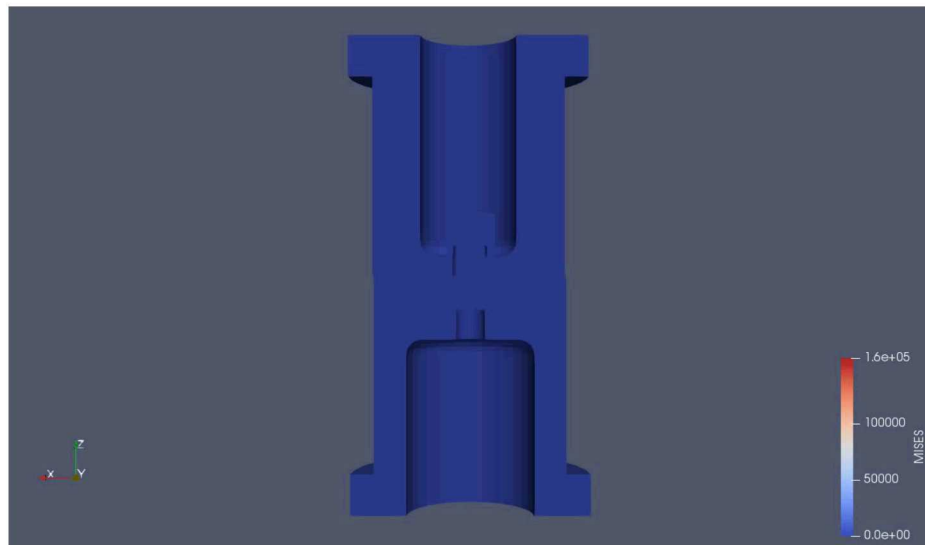
30-deg with tear



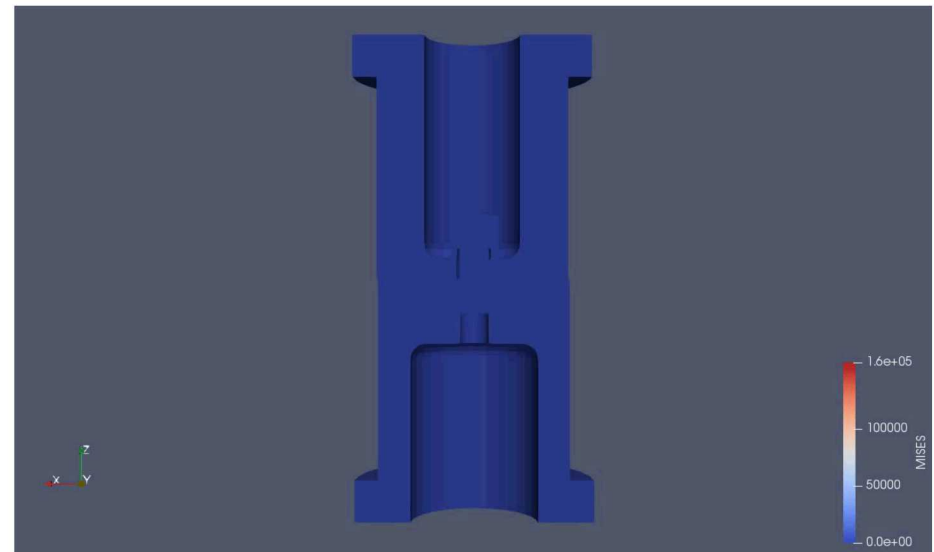
60-deg



60-deg with tear



90-deg



90-deg with tear

0-deg with tear

30-deg with tear

60-deg with tear

90-deg with tear

