

# Recent applications, designs, and sundry improvements in PDV optical probes

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This work was done by National Security Technologies, LLC, under Contract No. DE-AC52-06NA25946 with the U.S. Department of Energy.



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# Acknowledgments

- NSTec: Ed Daykin, Brent Frogget, Morris Kaufman, Brandon La Lone, Bob Malone
- LANL: David Holtkamp, Patrick Younk

# Topics

- Improved performance of Argus NX3b fisheye probe
- New potentials afforded by multicore fiber (MCF)
- An inquiry into back-reflections at the lens-fiber interface in Argus probes
- A possibly ridiculous proposal for a new PDV architecture

# Argus NX3b fisheye probe

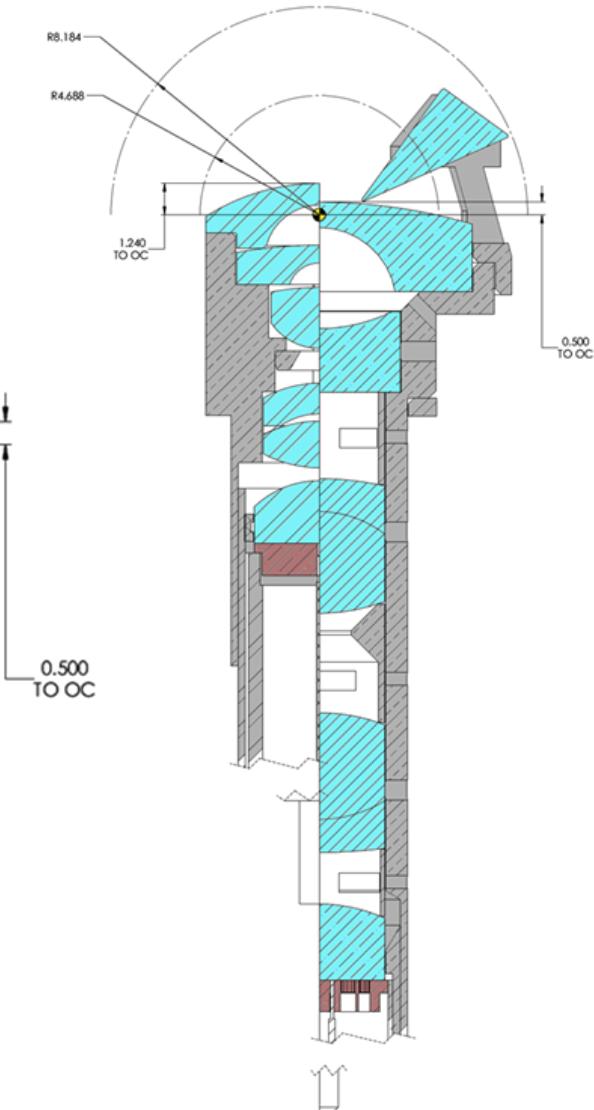
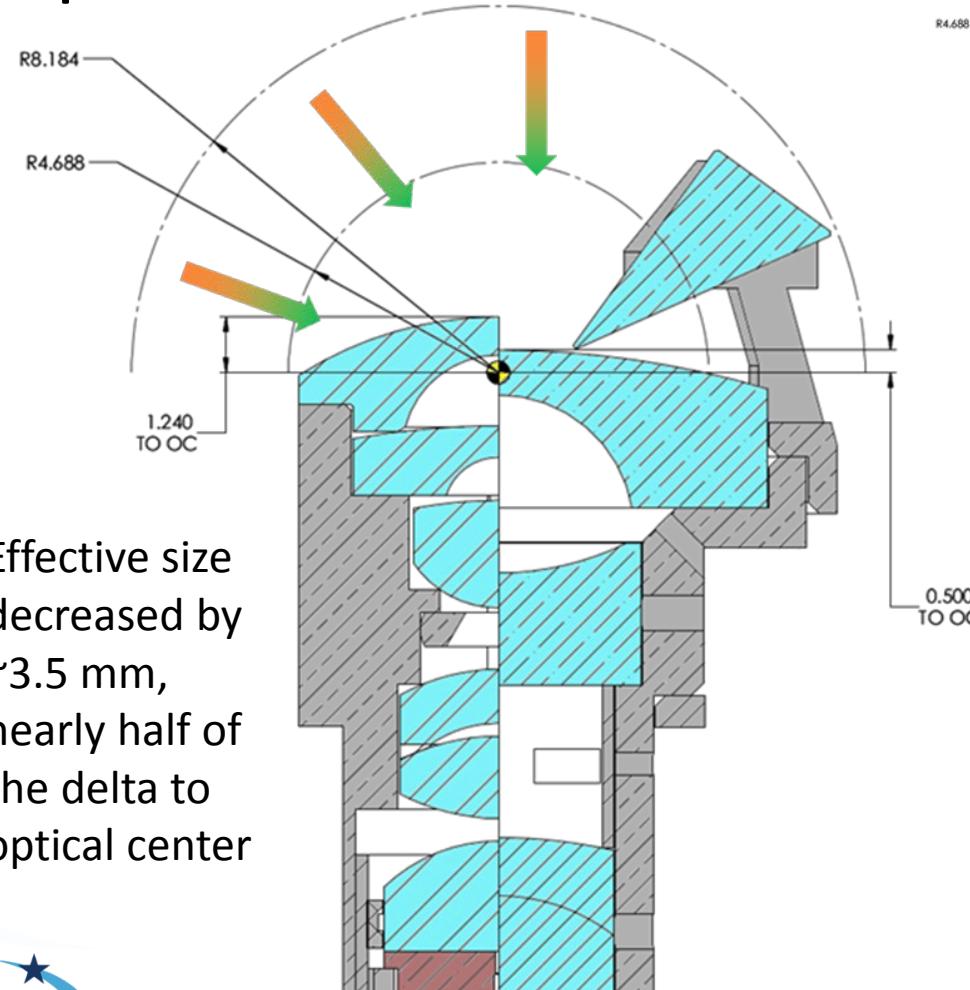
- Envisioned as an improvement over NX1 (the current standard), and as a development and demonstration platform for improved methods and processes
- Improvements over NX1
  - Negligible distortion over full field of view
  - Flat collection efficiency over the field of view
  - No mirrors

# Argus NX3b fisheye probe

- A smaller lens = improved data collection
- Incorporation of multi-core fiber (MCF) enables better angular spacing in any geometry<sup>1</sup>
- Tighter, more sophisticated tolerancing
  - Working with vendors to develop an integrated design, tolerancing, assembly, and qualification process
  - Developing new processes and standards for design and qualification
- Lower back-reflections
  - *Working with Cargille to develop a better-matched coupling fluid<sup>1</sup>*
  - *Developing a new process for optical coupling<sup>1</sup>*

# Argus NX3b fisheye probe

## Comparison to NX1: Size

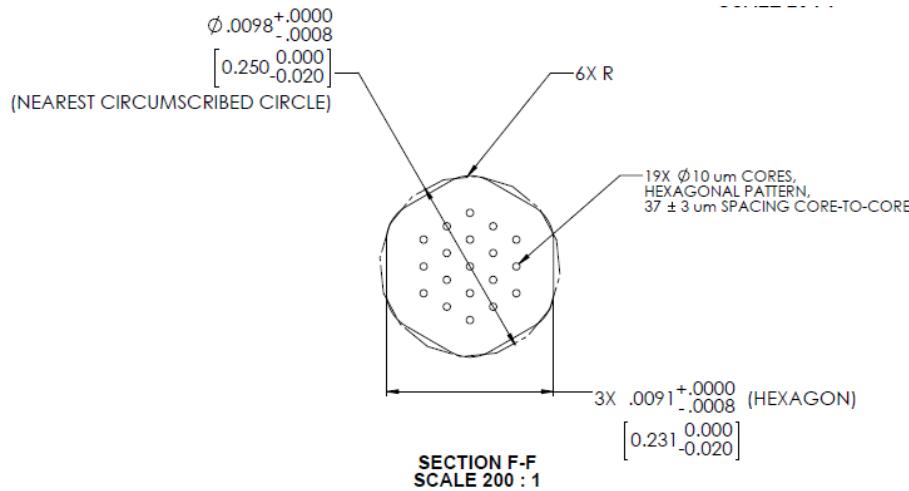


# Incorporation of MCF

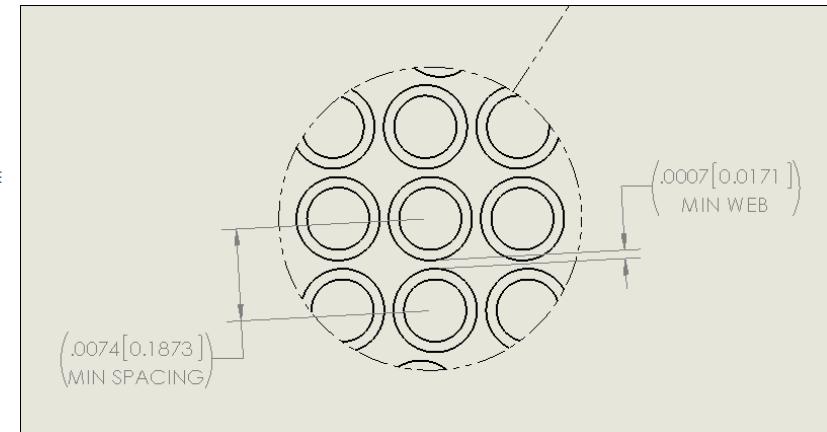
- Chiral Photonics makes customizable PROFA multi-core fiber arrays with smaller fiber-to-fiber spacing than is possible with standard fiber arrays, and greater flexibility than fiber bundles
- One end is a hexagonal array, and the other is broken out into pigtails

# Incorporation of MCF

	PROFA fiber	125-micron fiber	80-micron fiber
Fiber-to-fiber spacing	37 microns	187.3 microns	80 microns (dense pack)



PROFA fiber, 37  $\mu\text{m}$  spacing,  
10  $\mu\text{m}$  core



Minimum spacing for  
individual 125  $\mu\text{m}$  fibers

# Improving back-reflections

- Multiple back-reflections currently limit MPDV optical probe performance. Of these, we decided to look at those at the interface between the fibers in the ferrule and the first lens.
- These are governed by the difference in the two indices of refraction, the index of the material in the gap, and the thickness of the gap

$$R = \frac{(n_0^2 + n_1^2)(n_1^2 + n_2^2) - 4n_0n_1^2n_2 + (n_0^2 - n_1^2)(n_1^2 - n_2^2) \cos 2\delta_1}{(n_0^2 + n_1^2)(n_1^2 + n_2^2) + 4n_0n_1^2n_2 + (n_0^2 - n_1^2)(n_1^2 - n_2^2) \cos 2\delta_1}$$

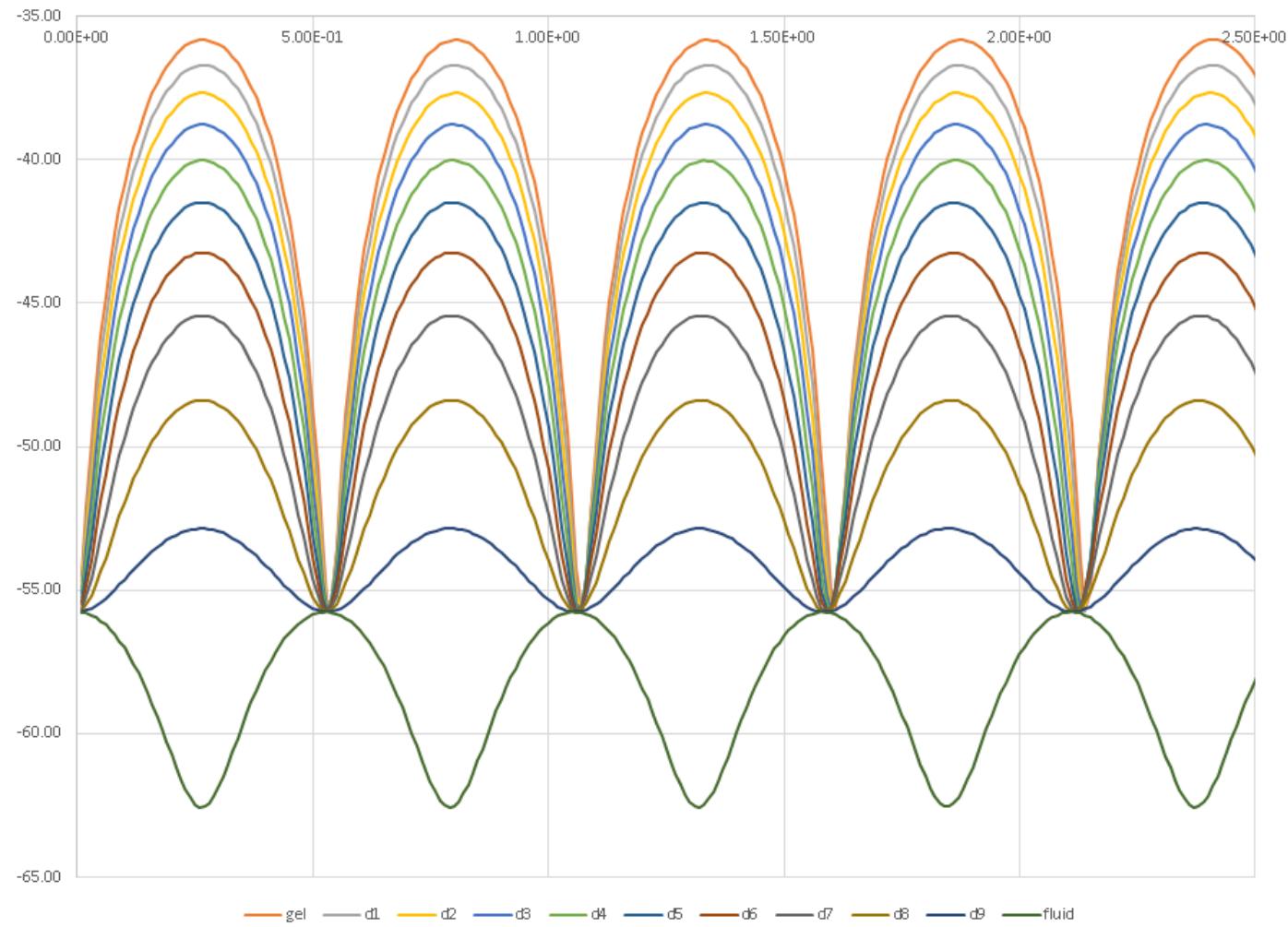
$$\delta_1 = \frac{2\pi}{\lambda} n_1 d_1 \cos \varphi_1$$

# Improving back-reflections

- We know the lens index very accurately
- We know the fiber material index to first order
- We expect to know the optical couplant index to reasonable accuracy
- We don't have any idea what the thickness of the gap is.

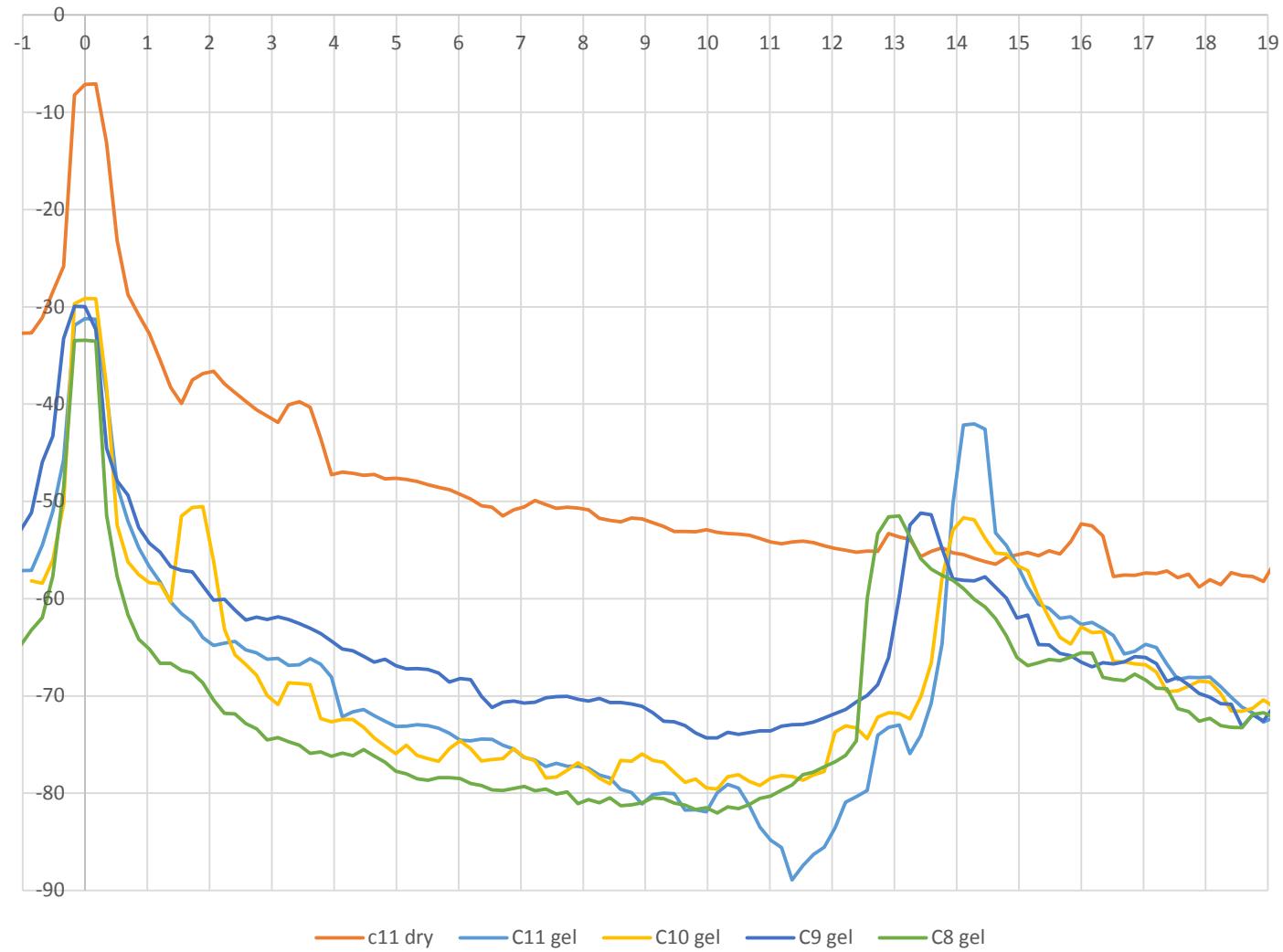
# Improving back-reflections

Regardless of gap size, we expect increasing index to improve back-reflections



# Improving back-reflections

Intra-lens  
reflections  
show up  
as second  
peaks



# Improving back-reflections

## Measurements

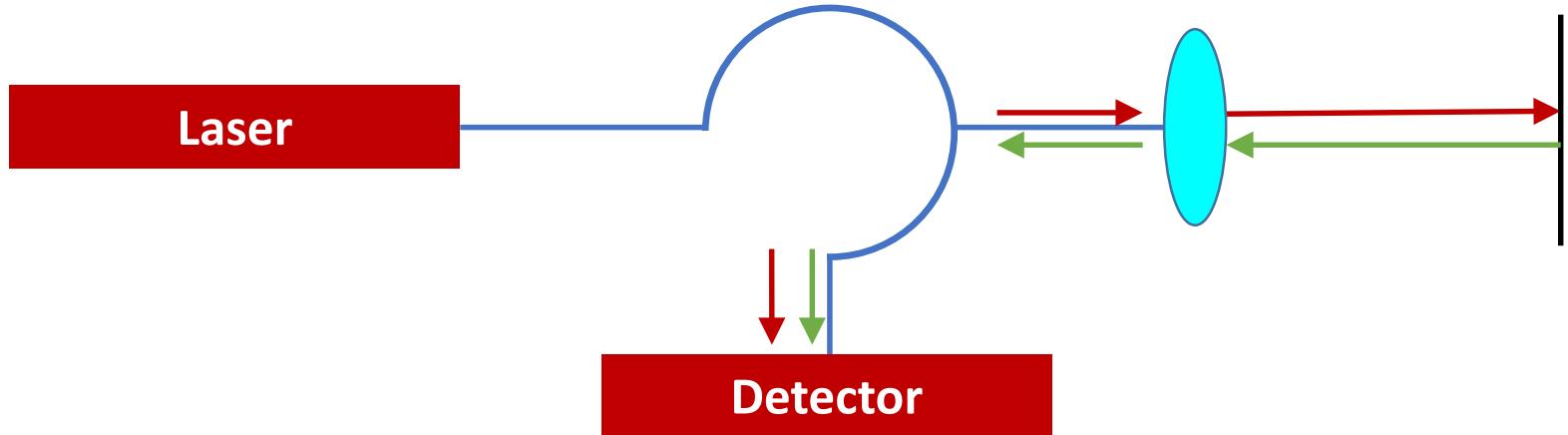
	Index	Back-reflections	
		(average)	(standard deviation)
Air gap	1	−18.276	6.294
Standard gel	1.4470	−41.829	2.366
Custom liquids	1.4690	−44.959	3.291
	1.4695	−44.211	3.152
	1.4700	−45.822	3.745
	1.4710	−46.007	4.424
	1.4720	−45.572	3.332
	1.4730	−45.308	3.497

- Air and gel measurements are consistent with a gap of ~100 nm
- Liquid indices bottom out well above their predicted values
- Intra-lens reflections eliminated via Luna measurements
- Intra-fluid bubbles? Volatility? Measurement technique?

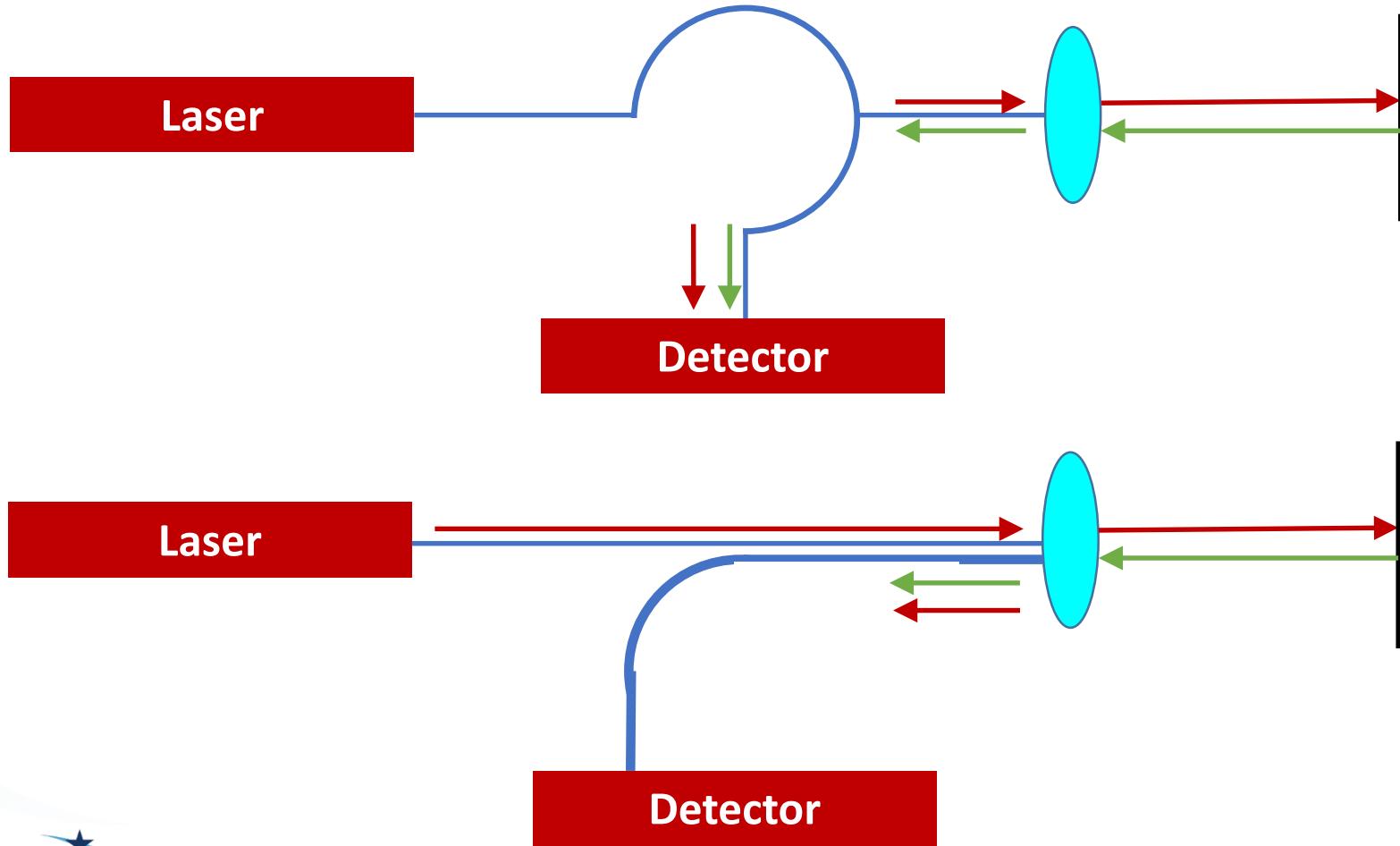
# A proposal for a new architecture

- Recent experiments with separate send and receive paths have shown significant promise for reducing back-reflections
- Some applications require long stand-off distances, longer travel, or greater collection efficiency than possible with the current architecture

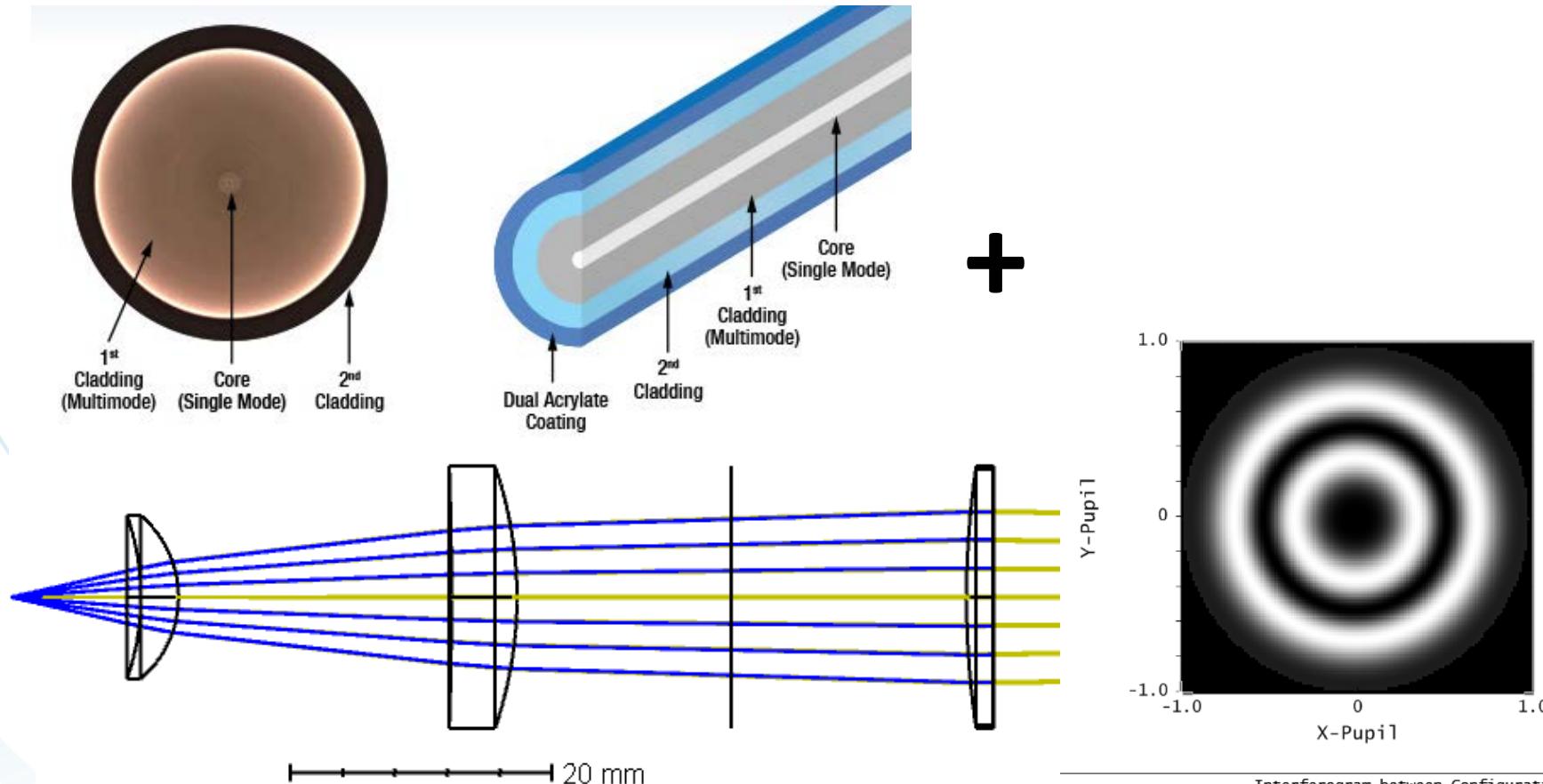
# A proposal for a new architecture



# A proposal for a new architecture

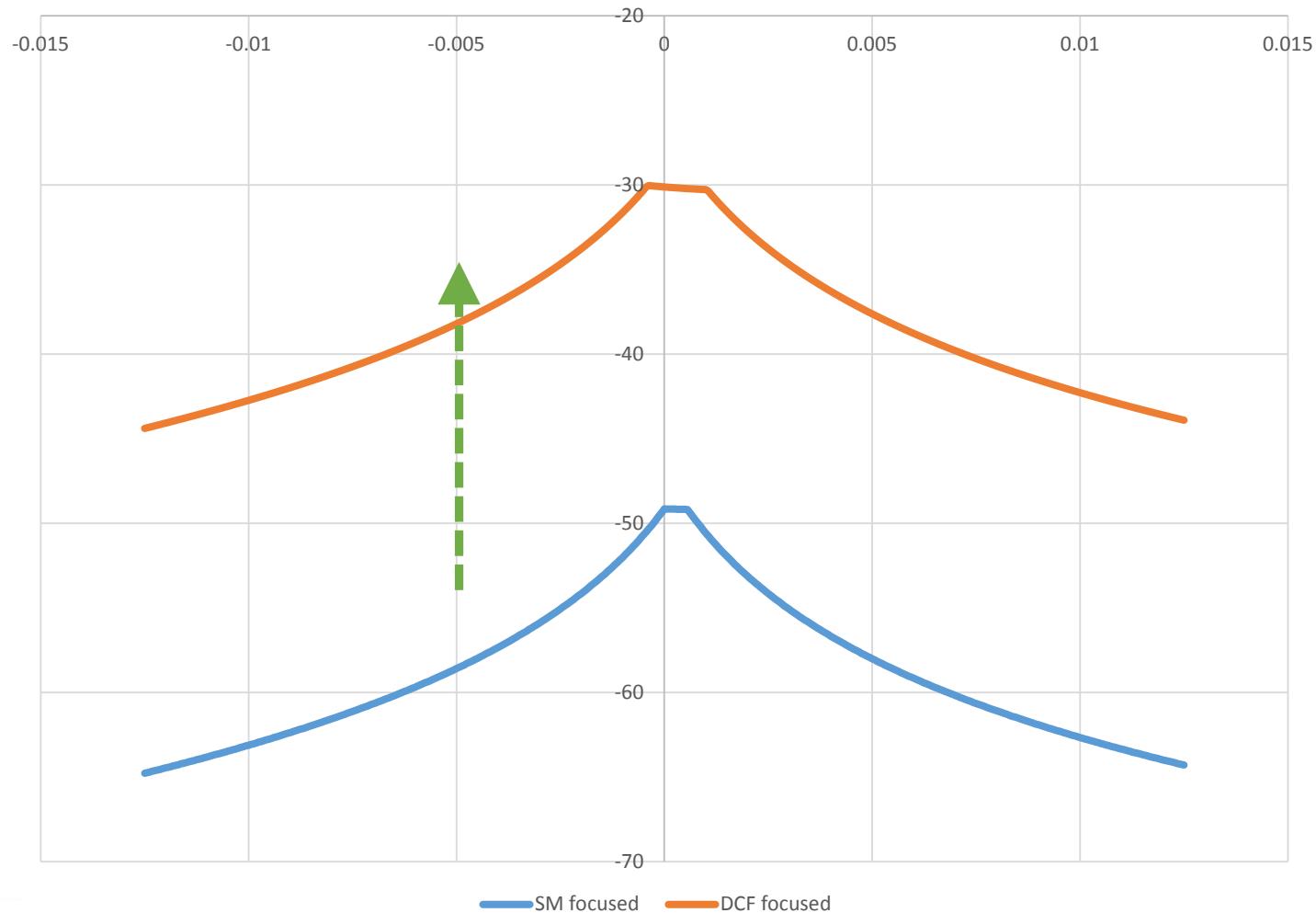


# A proposal for a new architecture



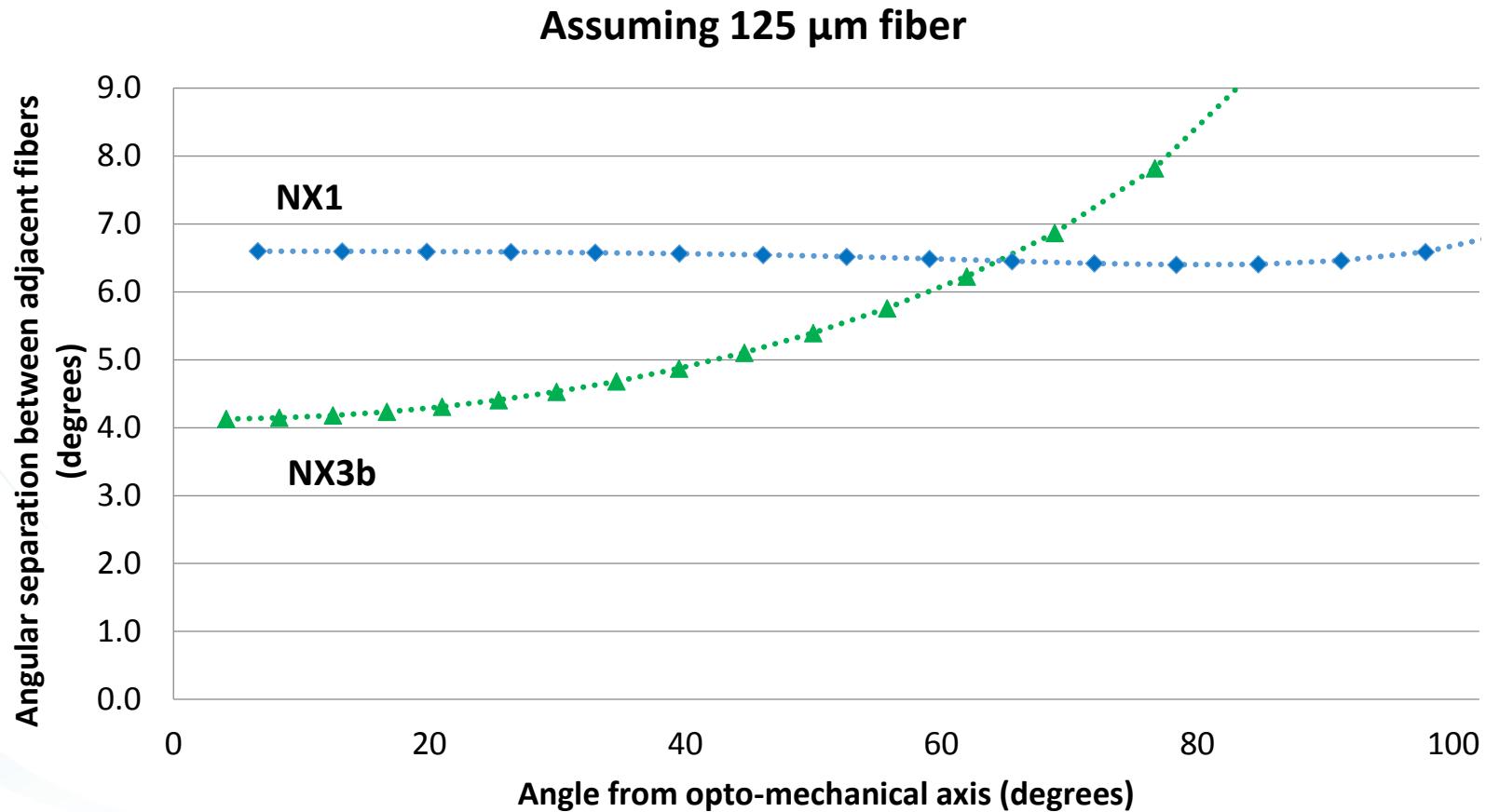
6/6/2016  
1.5500  $\mu\text{m}$  at 0.000 mm.  
Peak to Valley = 1.8920 waves, Fringes/Wave = 1.0000.

# A proposal for a new architecture



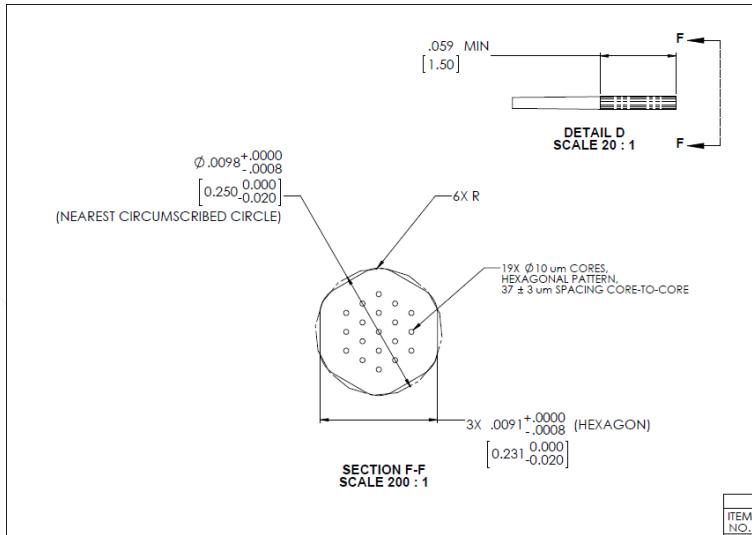
# Argus NX3b fisheye probe

## Comparison to NX1: distortion

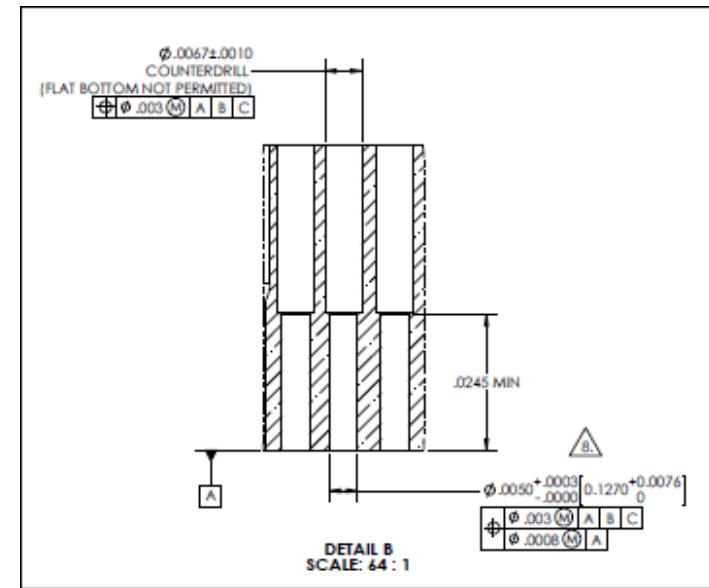


# Incorporation of MCF

- The locational tolerance for individually potted fibers is good because the radial clearance between the fiber and hole will be small: 1 to 5  $\mu\text{m}$
- The radial clearance between a PROFA fiber and its hole is large: 13 to 18  $\mu\text{m}$
- End result: The location of the PROFA fibers is less determinate than that of the potted fibers



PROFA hexagon profile tolerance =  $+0/-20 \mu\text{m}$   
 Hole tolerances for PROFA  $+15 \mu\text{m}/-0$   
 Hole location tolerance:  $\pm 8 \mu\text{m}$



Corning fiber cladding diameter:  
 $125 \mu\text{m} \pm 0.3 \mu\text{m}$   
 Hole dimension:  $127 \mu\text{m} +8/-0$   
 Location tolerance:  $\pm 6 \mu\text{m}$