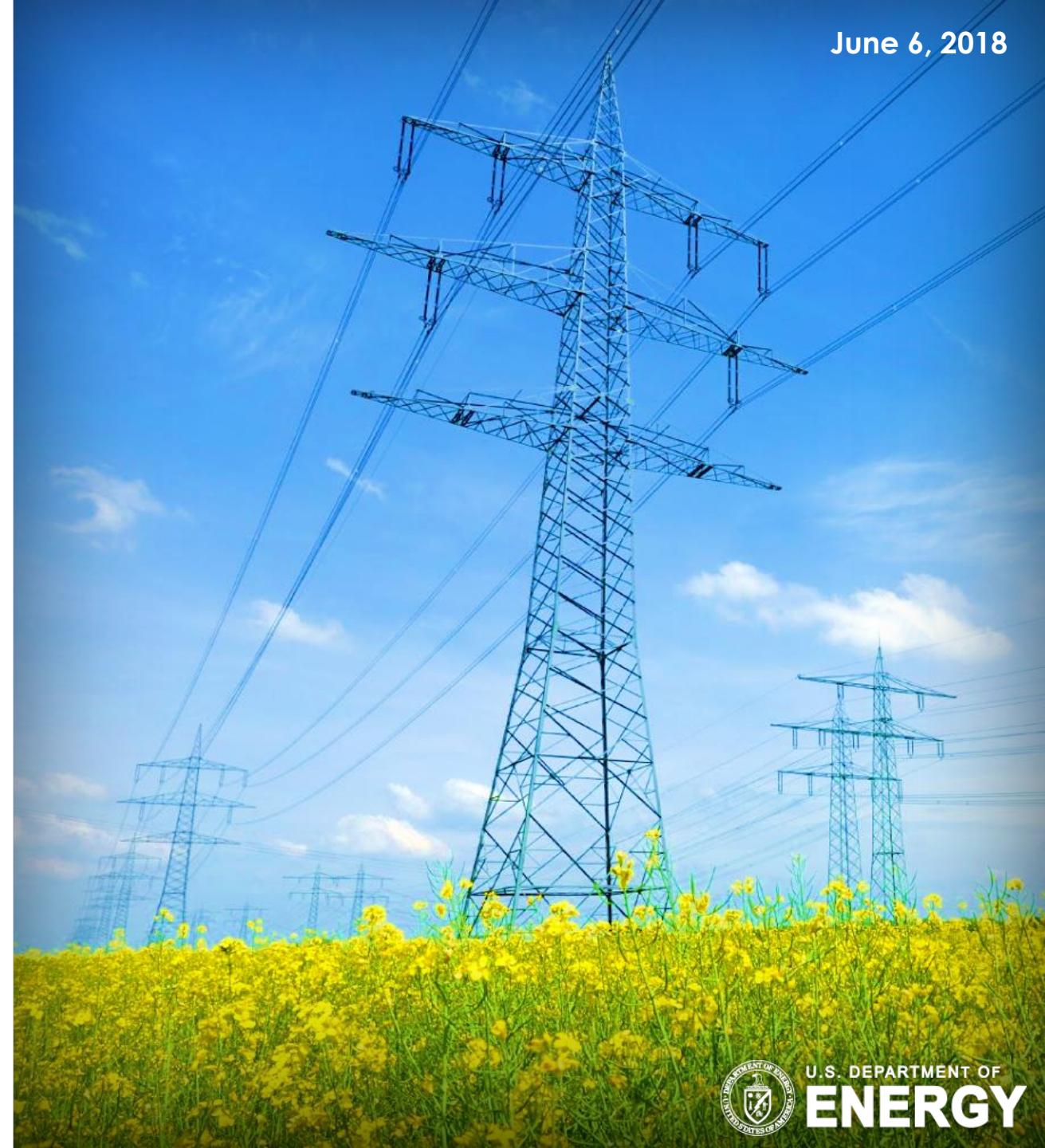


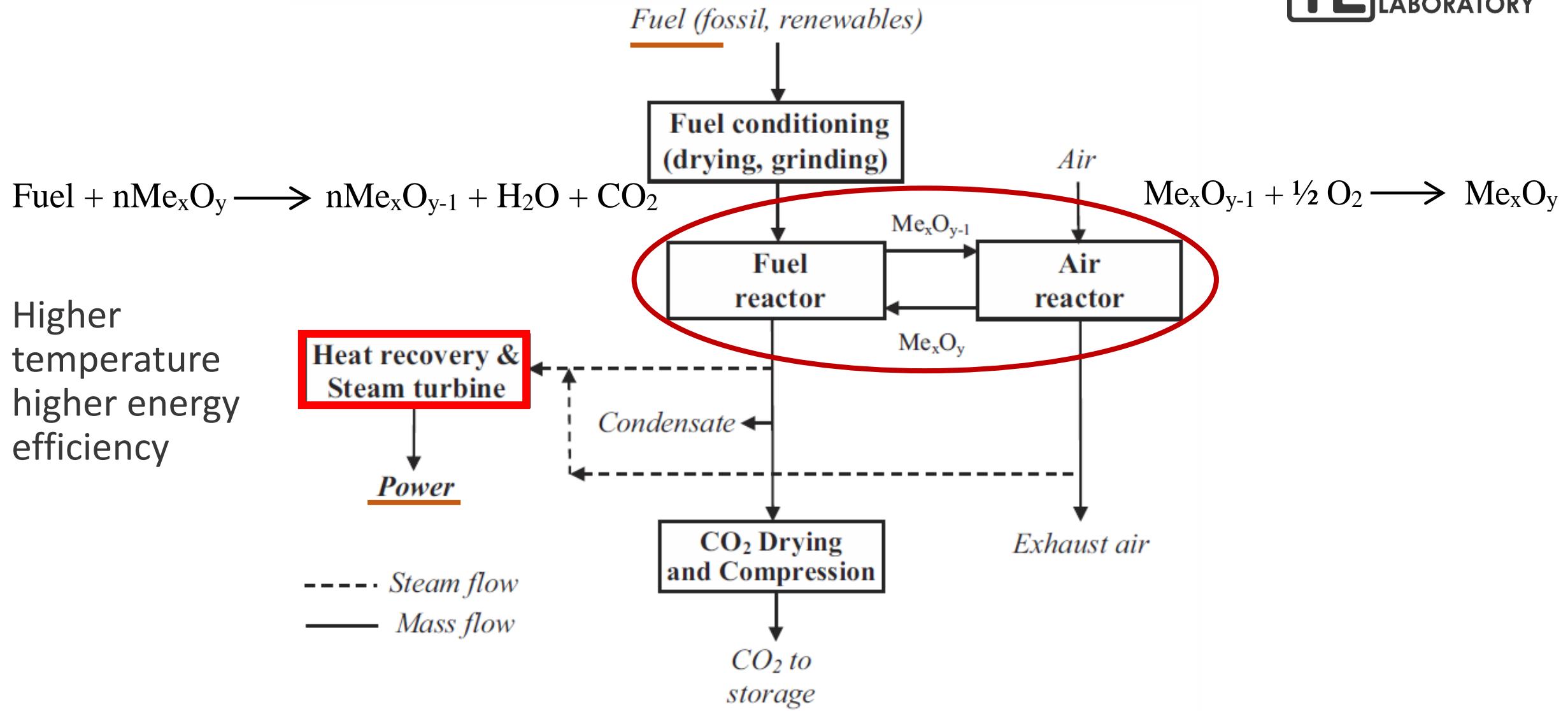
# Development of Bimetallic Cu-Fe Oxygen Carriers for Coal Chemical-Looping Combustion

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# CLC Power Generation with Carbon Capture



## Concept development and lab testing (1-1000kW<sub>th</sub>)



## Scale-up and industrial validation

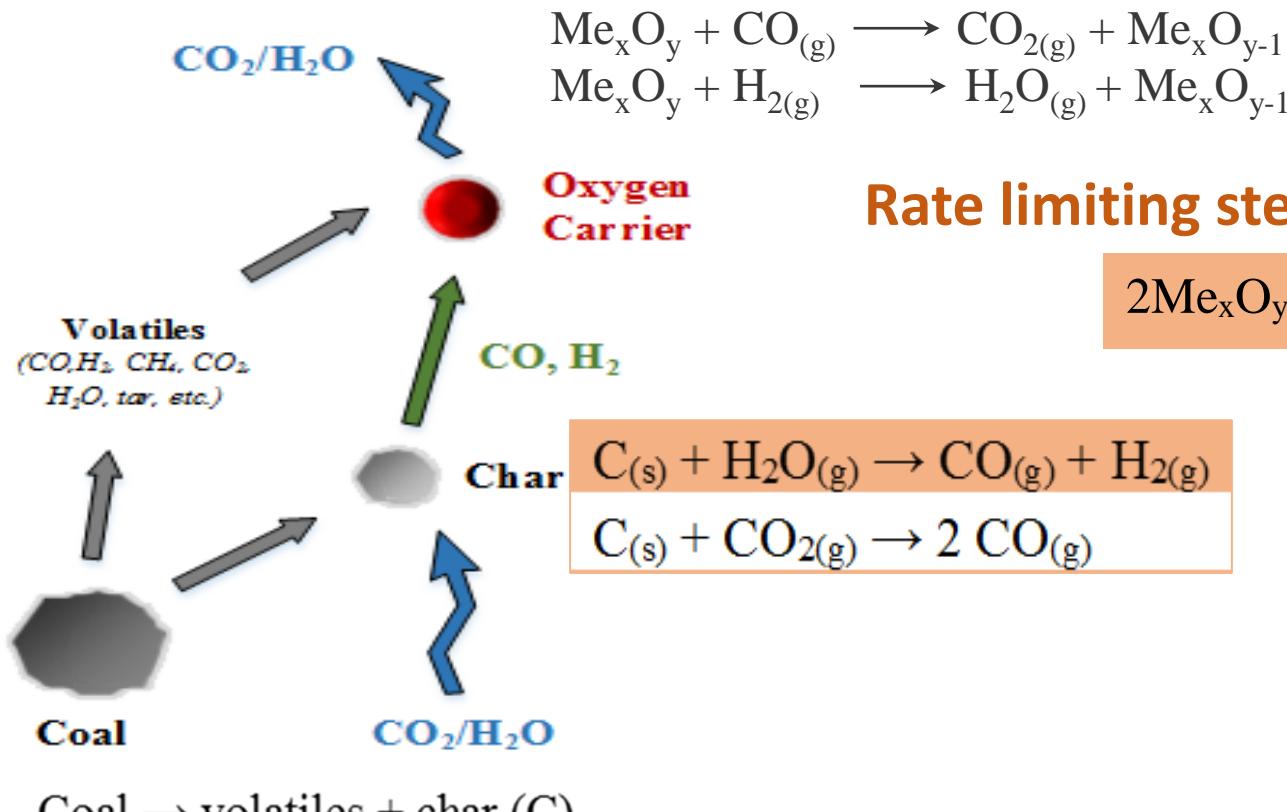
- Important OC properties
  - High reactivity and oxygen transfer capacity
  - High attrition resistance
- Upscaling of OC manufacture
  - Produce at multi-ton scale and competitive price
  - Waste disposal, health and safety
  - Upscaling reactor system
  - Optimize the OC and the system for fuels

# Main Reactions in Fuel Reactor for Direct Coal CLC



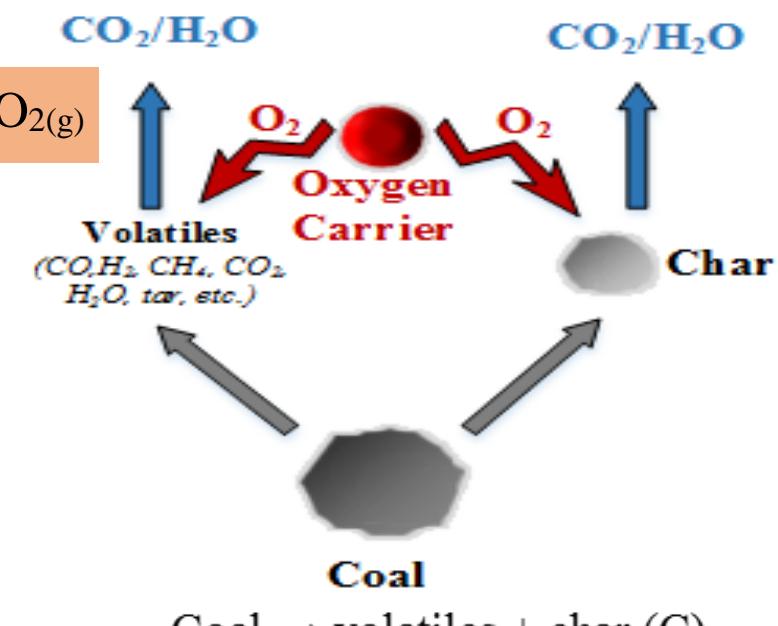
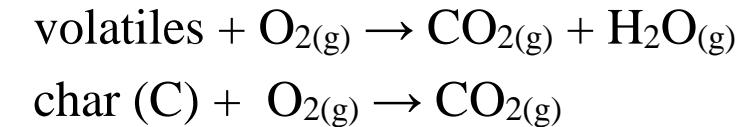
IG-CLC (In-situ gasification chemical-looping combustion)

OC:  $\text{Fe}_2\text{O}_3$ ,  $\text{NiO}$ ,  $\text{CuO}$



CLOU (Chemical-looping with oxygen uncoupling)

OC:  $\text{CuO}$ ,  $\text{Mn}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$



# Cu-Fe Oxygen Carriers for Coal IG-CLC and CLOU



IG-CLC

OC:  $\text{Fe}_2\text{O}_3$

Disadvantage:

- Low oxygen transport capability

$\text{Fe}_2\text{O}_3$ - $\text{Fe}_3\text{O}_4$ - $\text{FeO}$ - $\text{Fe}$

$\text{Fe}_2\text{O}_3/\text{Fe}_3\text{O}_4$ :0.033

$\text{CuO}/\text{Cu}_2\text{O}$ :0.1

Combined Cu-Fe OC

- Keep the parent metal oxide advantages and overcome the parent metal oxide disadvantages
- Cu-Fe-Si is attractive based on its availability from naturally occurring materials with low cost

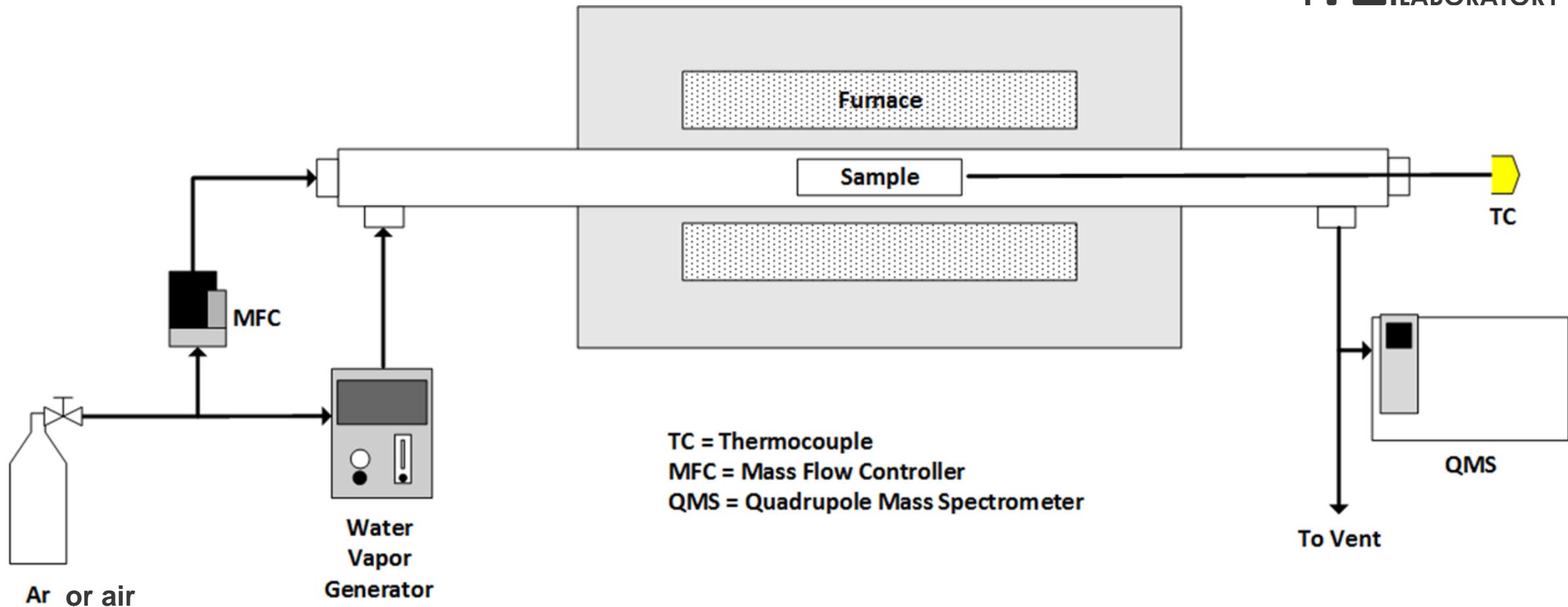
# Objectives

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- To prepare Cu-Fe-Si OC for iG-CLC and CLOU
- To study reactivity and  $\text{CO}_2$  capture efficiencies of Cu-Fe-Si OC with coal char at high temperature (up to  $1100^\circ\text{C}$ ) in iG-CLC and CLOU at different ratios of OC to coal char (by weight  $\varphi$ )
- To discuss main reactions taking place in iG-CLC and CLOU

# Experiment Set-up



On-line quantitative measurement of the product gas constituents: Ar, CO, CO<sub>2</sub>, CH<sub>4</sub>, and H<sub>2</sub>  
X-ray diffraction (XRD) analysis of the phase composition of fresh OC and reacted OC

# Data Analysis



- **Oxygen uncoupling**

$$\text{Oxygen uncoupling } X_o, X_o = \frac{n_o}{n_{\max}}$$

Oxygen uncoupling rate  $R$ ,  $R = dX_o/dt$

- **Carbon conversion**

Carbon conversion efficiency  $X_c$ , mainly consider  $\text{CO}_2$  and  $\text{CO}$  from combustion (full or partial) or gasification

$$X_c = \frac{n_c}{n_0} = \frac{\sum_{t=0}^t F(y_{\text{CO}_2} + y_{\text{CO}})}{n_0}$$

Carbon conversion rate  $R$ ,  $R = dX_c/dt$

- **$\text{CO}_2$  capture efficiency**

$$\eta_{\text{CO}_2} = \frac{n_{\text{CO}_2}}{n_0}$$

# Coal and Char Properties



Coal char: pyrolysis of PRB sub-bituminous coal with particle size from 106 to 180  $\mu\text{m}$  at 1000°C

Proximate analysis (% day basis)			
	Volatile	Fixed carbon	Ash
Powder River Basin (PRB) Sub-bituminous coal char	1.98	85.6	12.42
PRB coal	45.08	47.66	7.26

	Ultimate analysis (% dry basis)									
	C	H	N	S	O (diff)					
PRB coal	67.24	4.23	1.53	0.38	17.79					
Ash mineral analysis (oxides and ignited % wt.)										
	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	TiO <sub>2</sub>	CaO	P <sub>2</sub> O <sub>5</sub>	MgO	Na <sub>2</sub> O	K <sub>2</sub> O	SO <sub>3</sub>
PRB	38.71	16.00	5.52	1.08	19.24	0.96	4.68	1.22	0.75	10.69

# Bimetallic Cu-Fe-Si OC Preparation



- Pelletizing by pressure

Paste, pellet, calcine at 1000 and 1100°C, grind and sieve (<180µm)

- IG-CLC

Fe40 OC: 40% $\text{Fe}_2\text{O}_3$ +20% $\text{CuO}$ +40% $\text{SiO}_2$  by weight

Fe40 OC phase mainly  $\text{CuFe}_2\text{O}_4$  and  $\text{SiO}_2$



- CLOU

Cu40 OC: 40% $\text{CuO}$ +20% $\text{Fe}_2\text{O}_3$ +40% $\text{SiO}_2$  by weight

Cu40 OC phase mainly  $\text{CuO}$ ,  $\text{CuFe}_2\text{O}_4$  and  $\text{SiO}_2$

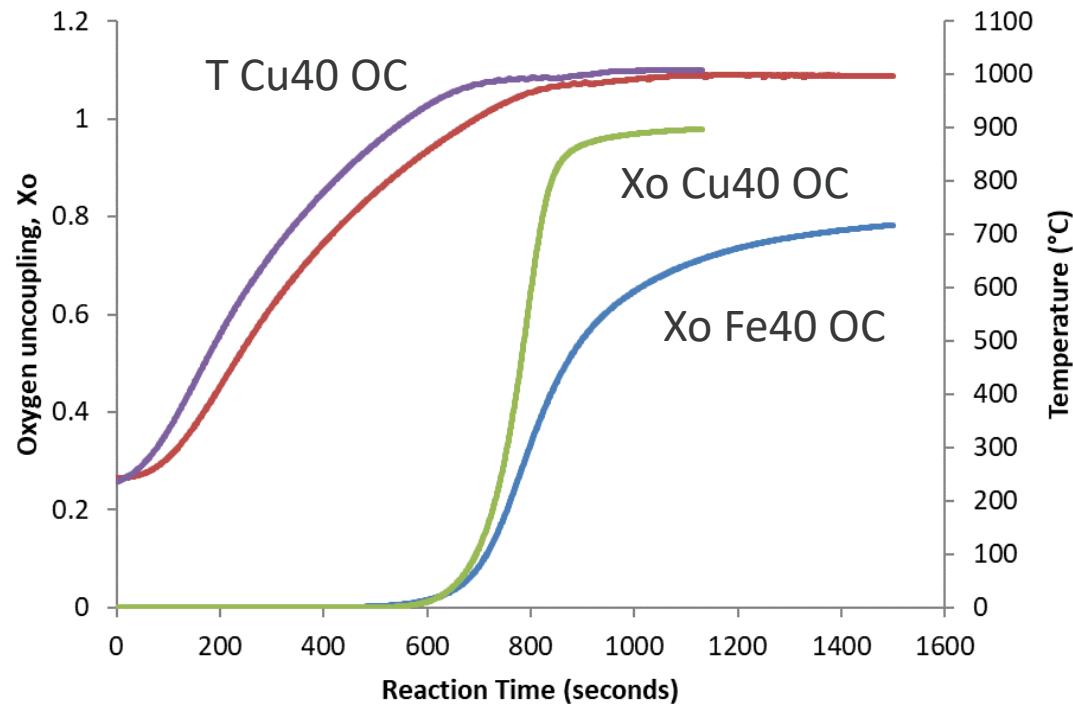
CuO wt.%	Calcination temp. (°C)	
	1000	1100
20	✓	✓
40	✓	✗
50	✗	✗
60	✗	✗

# Oxygen Uncoupling of Fe40 OC and Cu40 OC

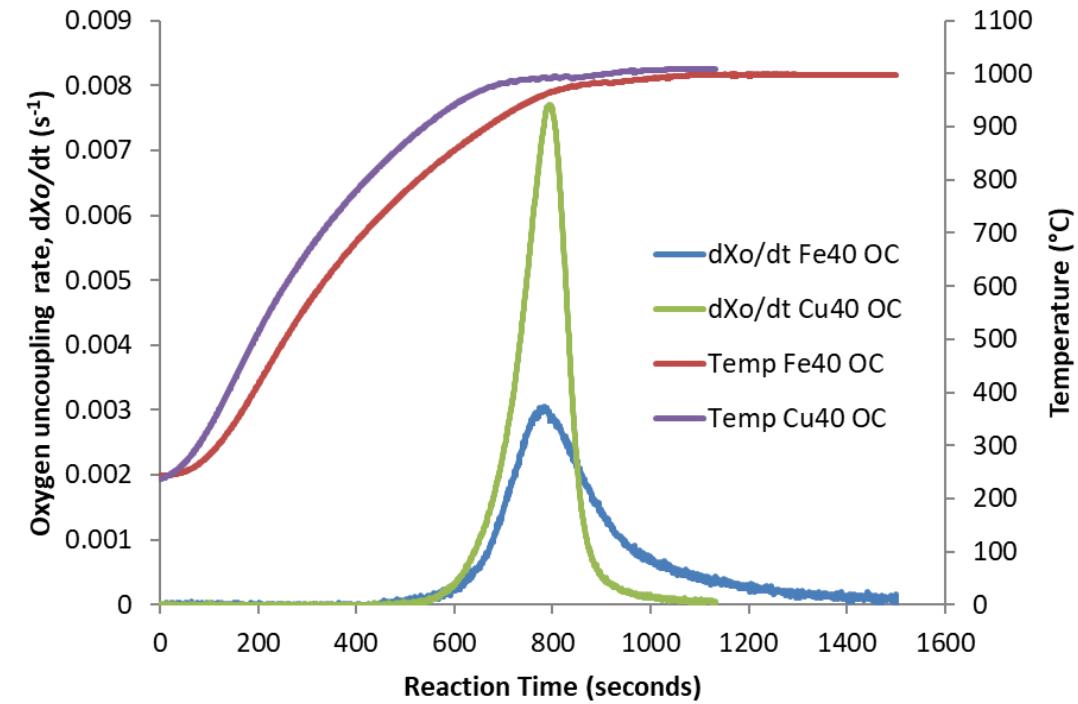
- Test in Ar at 1000°C
- Oxygen uncoupling(CuO to Cu<sub>2</sub>O)  $X_o$

Fe40 OC: maximum  $X_o=0.78$ ,  $dX_o/dt=0.003\text{ s}^{-1}$ ,  $T_{max}=960^\circ\text{C}$

Cu40 OC: maximum  $X_o=0.98$ ,  $dX_o/dt=0.008\text{ s}^{-1}$ ,  $T_{max}=975^\circ\text{C}$



Fe40 OC and Cu40 OC oxygen uncoupling ( $X_o$ )



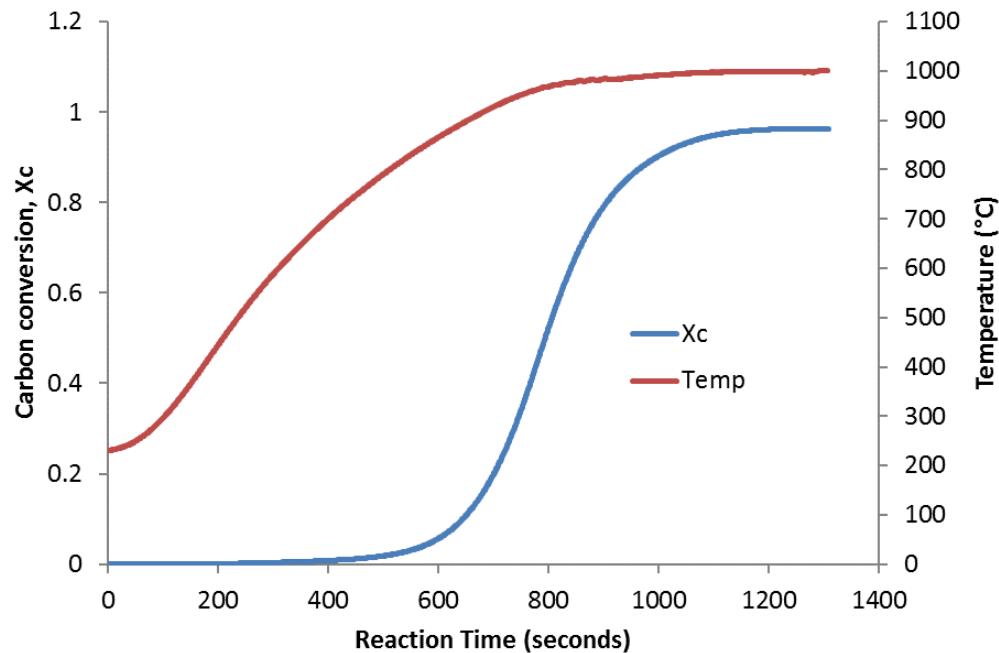
Fe40 OC and Cu40 OC oxygen uncoupling rate ( $dX_o/dt$ )

Fe 40 OC mainly phase change:  
 $\text{CuFe}_2\text{O}_4/\text{CuFeO}_2$  ( $\text{Cu}_2\text{OFe}_2\text{O}_3$ )  
Cu 40 OC mainly phase change:  
 $\text{CuO}/\text{Cu}_2\text{O}$ ,  $\text{CuFe}_2\text{O}_4/\text{CuFeO}_2$

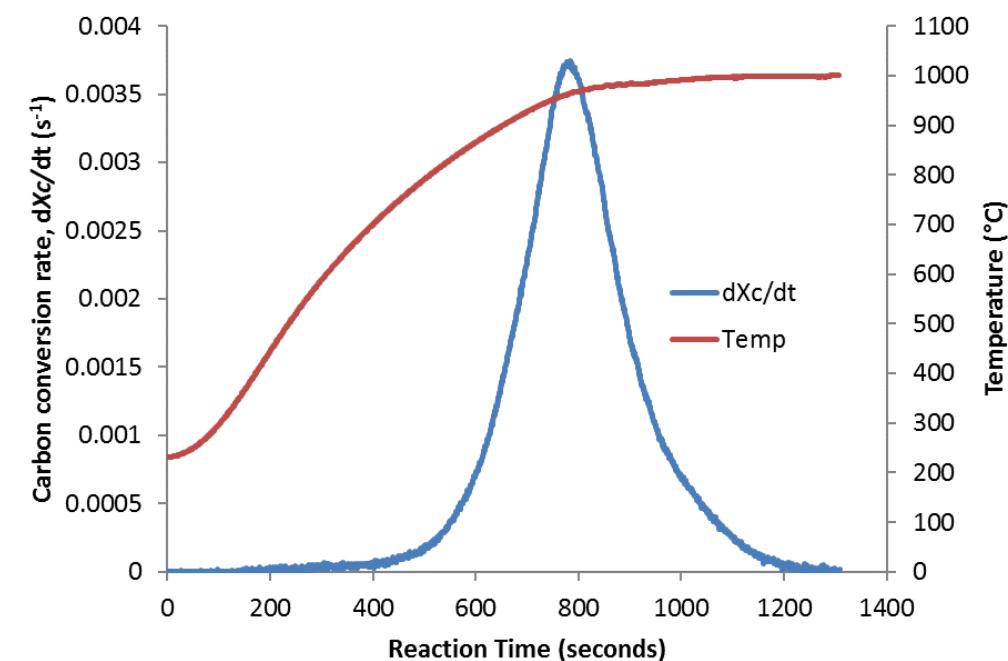
# Fe40 OC with Coal Char in IG-CLC

## Reactivity of Fe40 OC and char with $\varphi$ 80 at 1000°C

- Select  $\varphi=80$  considering  $\text{CuO}/\text{Cu}_2\text{O}$  and  $\text{Fe}_2\text{O}_3/\text{Fe}_3\text{O}_4$
- $X_c= 0.96$ , Theoretical  $X_c= 1$
- Maximum  $dX_c/dt=0.0037 \text{ s}^{-1}$  at  $T_{\text{max}}=956^\circ\text{C}$



Carbon conversion efficiency  $X_c$

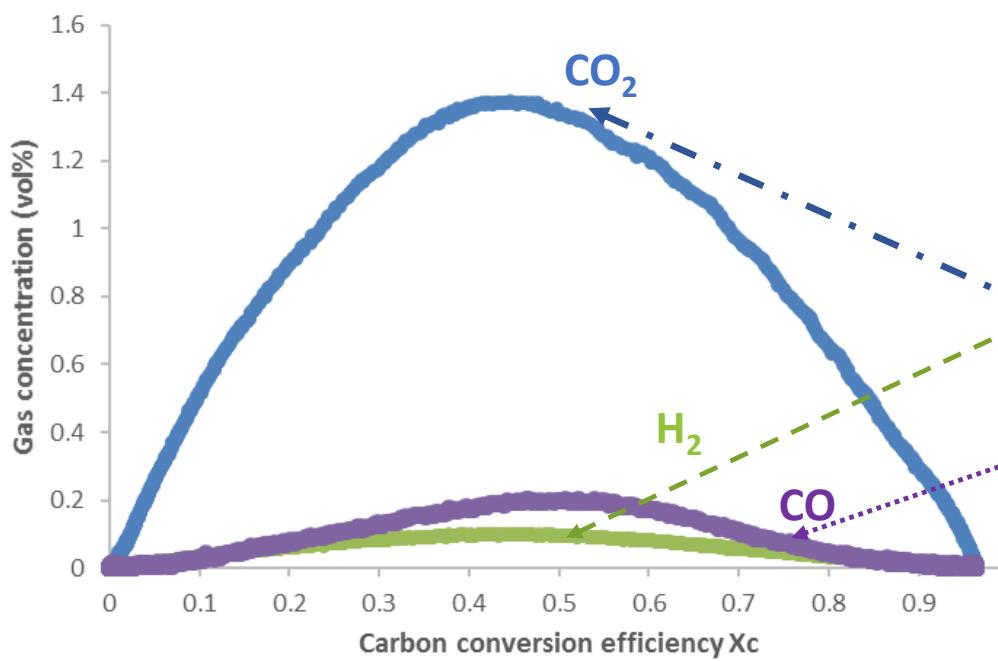


Carbon conversion rate  $dX_c/dt$

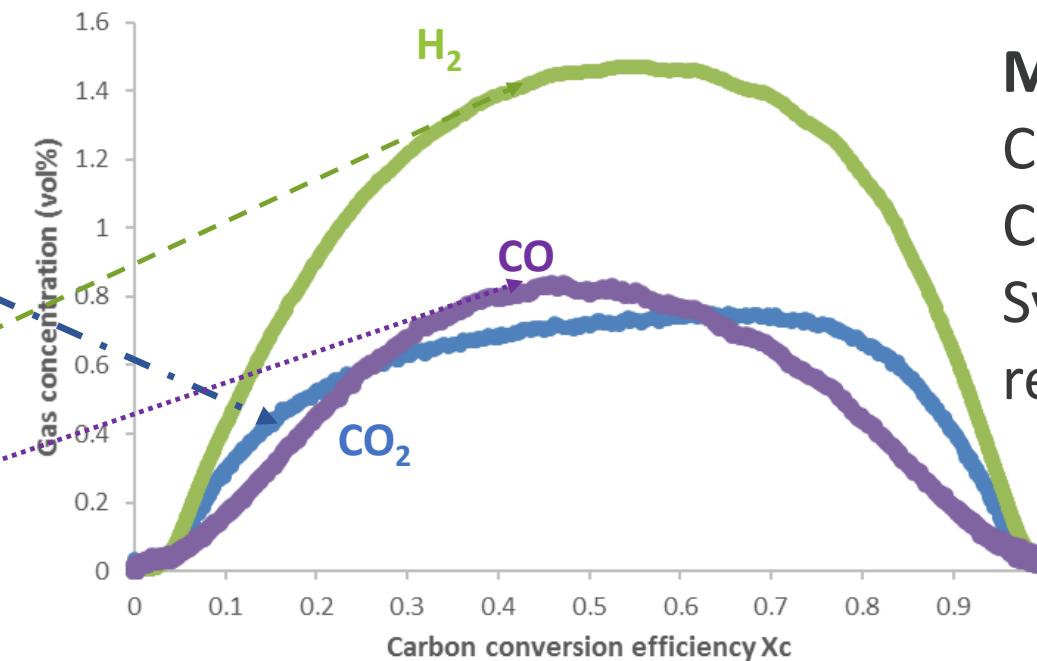
# Fe40 OC with Coal Char in IG-CLC

## CO<sub>2</sub> capture efficiency

- Mainly generated CO<sub>2</sub> at temperatures above 650°C
- Also produced CO + H<sub>2</sub> above 850°C
- Carbon capture efficiency  $\eta_{CO_2} = 0.88 > \eta_{CO_2} = 0.76$  single Fe<sub>2</sub>O<sub>3</sub> OC



Gas Concentrations of CO<sub>2</sub>, CO and H<sub>2</sub> vs Xc  
in Fe40 OC and char reaction



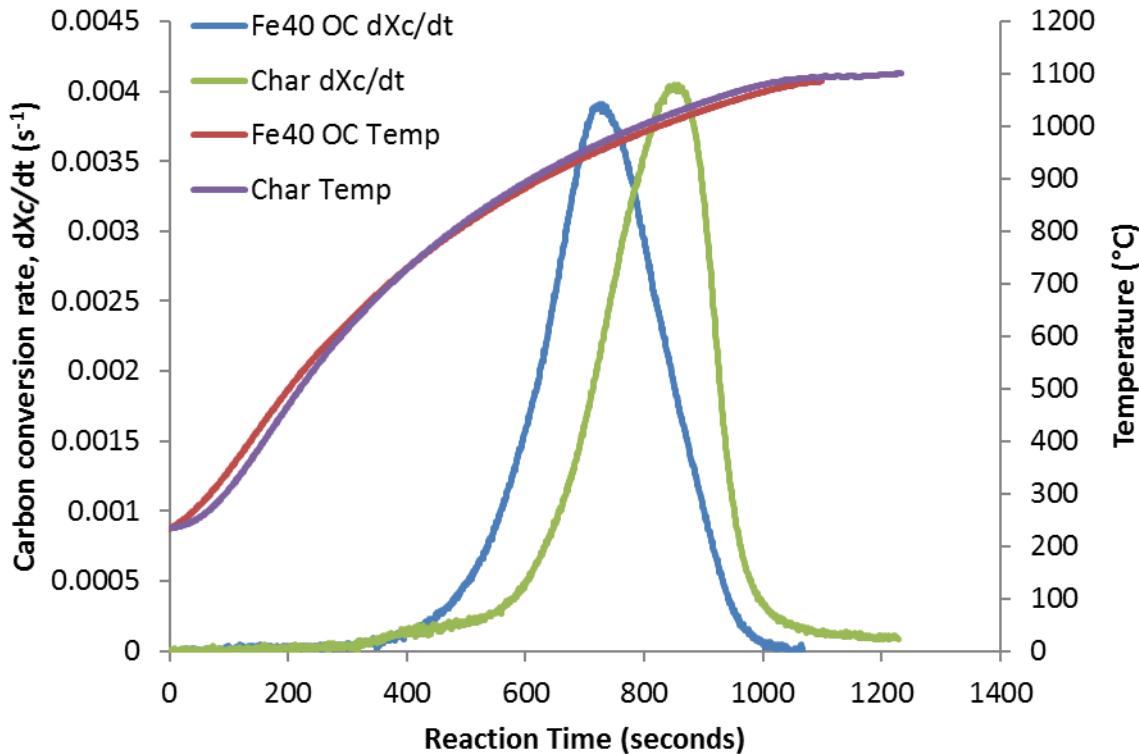
Gas Concentrations of CO<sub>2</sub>, CO and H<sub>2</sub> vs Xc  
in char gasification

**Main reactions**  
C combustion,  
C gasification,  
Syngas  
reduction

# Fe40 OC with Coal Char in IG-CLC

## Impact of reaction temperatures on the reactivity at $\varphi 80$

- Reaction rate increased as temperatures increased
- Reaction rate similar as temperature increased from 1000 to 1100°C



Carbon conversion rate  $dX_c/dt$  of Fe40 OC with char and char gasification at 1100°C

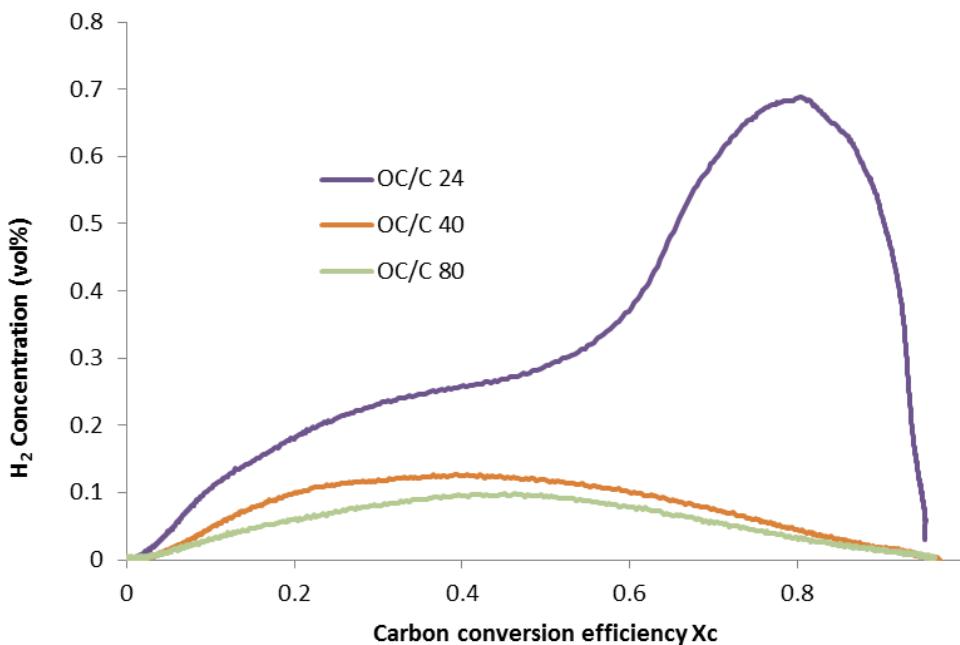
The maximum conversion rates and temperatures for Fe40 OC reactions with char and char gasification

Samples	Temp. (°C)	Rmax ( $s^{-1}$ )	Tmax (°C)
Fe40 OC/char	950	0.0026	938
	1000	0.0037	966
	1100	0.0039	972
Char	950	0.0025	950
	1000	0.0036	988
	1100	0.0040	1026

# Fe40 OC with Coal Char in IG-CLC

## Impact ratios of OC to char on $\eta_{CO_2}$ and OC phase changes

- Carbon capture efficiencies reduced as ratios of OC to char decreased due to increasing amount of CO and  $H_2$
- $Cu^{2+}Fe^{3+}_2O_4 \xrightarrow{O_2} Cu^+Fe^{3+}O_2 \rightarrow Cu_xFe_{3-x}O_4 (X=0.67 \text{ or } 0.86) + Cu$



$\varphi$	$\eta_{CO_2}$	OC phase changes		
80	0.88	$Cu^+Fe^{3+}O_2$ (major)	$Cu_xFe_{3-x}O_4^*$ (major)	Cu (trace)
40	0.80	$Cu^+Fe^{3+}O_2$ (minor)	$Cu_xFe_{3-x}O_4$ (major)	Cu (minor)
24	0.76	NA	$Cu_xFe_{3-x}O_4$ (major)	Cu (minor)

\*  $X=0.67 \text{ or } 0.86$

## Main reactions

C combustion, C gasification, Syngas reduction

# Cu40 OC and Coal Char in CLOU

## Reactivity of Cu40 OC and char with $\phi$ 67 at 1000°C in Ar

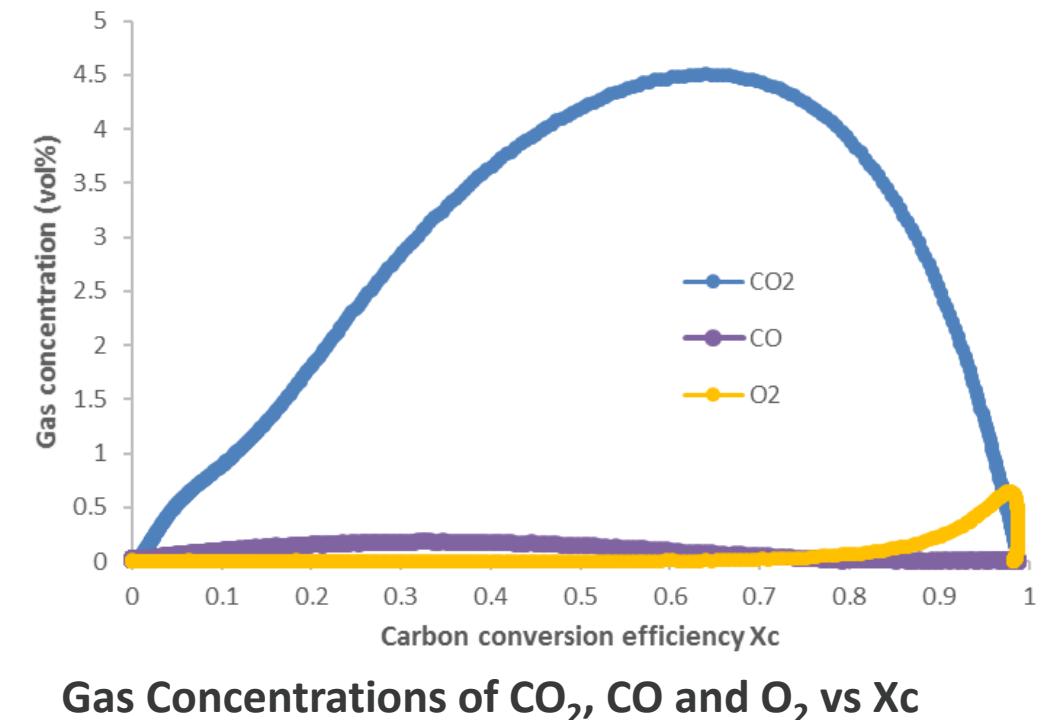
- Select  $\phi$  67 considering CuO/Cu<sub>2</sub>O
- X<sub>c</sub>= 0.99, Theoretical X<sub>c</sub>= 1
- Maximum dX<sub>c</sub>/dt=0.0077 s<sup>-1</sup> at T<sub>max</sub>=942°C
- Mainly generated CO<sub>2</sub> at temperatures above 650°C
- Carbon capture efficiency  $\eta_{CO_2}$ =0.96

### Cu 40 OC phase changes

- CuO/Cu<sub>2</sub>O
- CuFe<sub>2</sub>O<sub>4</sub>/CuFeO<sub>2</sub> (Cu<sub>2</sub>OF<sub>2</sub>O<sub>3</sub>)

### Main reactions

C combustion, C partial combustion

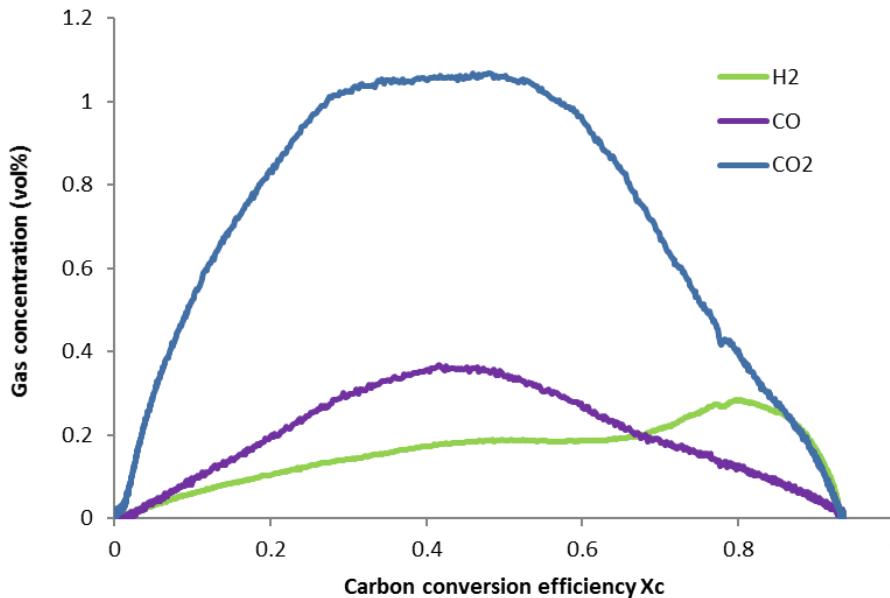


# Cu40 OC and Coal Char Reactions in Ar+H<sub>2</sub>O



## Impact ratios of OC to char on reactivity and OC phase changes

- Test results at  $\varphi$  67 in Ar+H<sub>2</sub>O are similar with ones at the same  $\varphi$  in Ar (CLOU)
- Test results at  $\varphi$  18 are similar with the test of Fe40 OC and char at  $\varphi$  24 in Ar+H<sub>2</sub>O (IG-CLC)
- $\text{Cu}^{2+}\text{O} \rightarrow \text{Cu}^{+}\text{O}_2 \rightarrow \text{Cu}$
- $\text{Cu}^{2+}\text{Fe}^{3+}\text{O}_4 \rightarrow \text{Cu}^{+}\text{Fe}^{3+}\text{O}_2 \rightarrow \text{Cu}_x\text{Fe}_{3-x}\text{O}_4$  ( $X=0.67$  or  $0.86$ ) + Cu



Gas Concentrations of CO<sub>2</sub>, CO and H<sub>2</sub> vs X<sub>c</sub>

$\varphi$	$dX_c/dt_{\max}$ (s <sup>-1</sup> )	$\eta_{\text{CO}_2}$	OC phase changes			
67	0.0074 (CLOU)	0.94	Cu <sub>2</sub> O major	Cu <sup>+</sup> Fe <sup>3+</sup> O <sub>2</sub> major	Cu <sub>x</sub> Fe <sub>3-x</sub> O <sub>4</sub> * trace	Cu NA
18	0.0031 (IG-CLC)	0.68	NA	NA	Cu <sub>x</sub> Fe <sub>3-x</sub> O <sub>4</sub> major	Cu major

# Summary

- Prepared Cu-Fe-Si OC for coal iG-CLC and CLOU formed  $\text{CuFe}_2\text{O}_4$  and released gaseous  $\text{O}_2$
- Ratios of oxygen carrier to char impact reactivity,  $\text{CO}_2$  capture efficiency, and OC phases
- For coal iG-CLC using  $40\%\text{Fe}_2\text{O}_3+20\%\text{CuO}+40\%\text{SiO}_2$  (by weight) oxygen carrier (Fe40 OC) at  $1000^\circ\text{C}$ , char was fully converted with maximum carbon conversion rate  $dX_c/dt=0.0037 \text{ s}^{-1}$  at  $T_{\text{max}}=956^\circ\text{C}$  and carbon capture efficiency  $\eta_{\text{CO}_2}=0.88$  with CO and  $\text{H}_2$
- For coal CLOU using  $40\%\text{CuO}+20\%\text{Fe}_2\text{O}_3+40\%\text{SiO}_2$  (by weight) oxygen carrier (Cu40 OC) at  $1000^\circ\text{C}$ , char was fully converted with maximum carbon conversion rate  $dX_c/dt=0.0077 \text{ s}^{-1}$  at  $T_{\text{max}}=942^\circ\text{C}$  and carbon capture efficiency  $\eta_{\text{CO}_2}=0.96$  with CO and  $\text{O}_2$

# Thank You

- Questions?
- Please contact Ping Wang
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