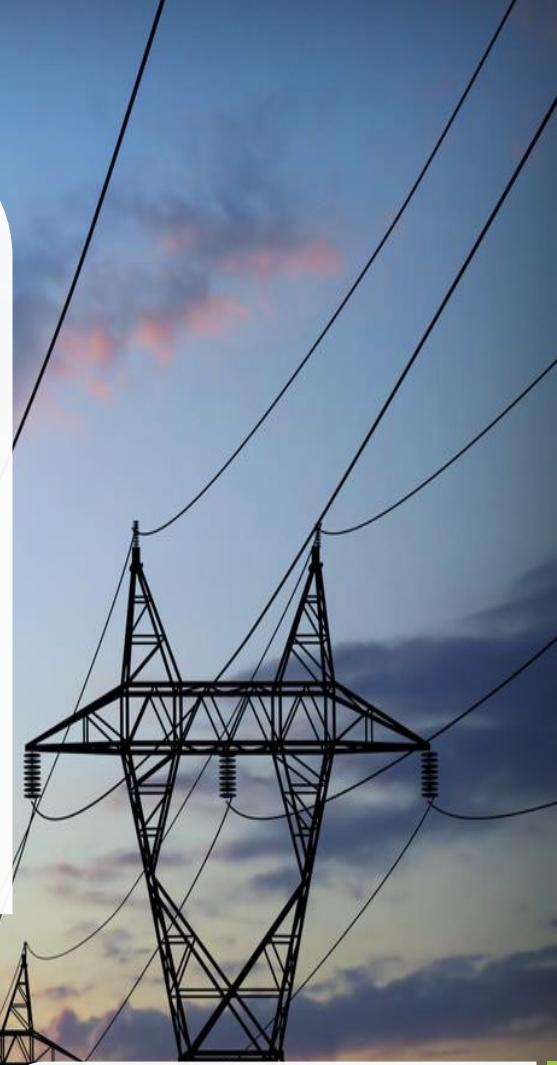


Early stage oxidation of Alloy 617 in CO₂ power cycle environments

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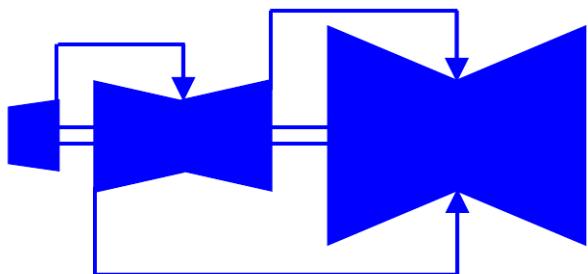
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Why supercritical CO₂ power cycles?

Properties of sCO ₂ Cycles	Impact
No phase change (Brayton Cycle)	Higher efficiency
Recompression near liquid densities	Higher efficiency
High heat recuperation	Higher efficiency
Compact turbo machinery	Lower capital cost
Simple configurations	Lower capital cost
Dry/reduced water cooling	Lower environmental impact
Storage ready CO ₂ in direct cycles	Lower environmental impact

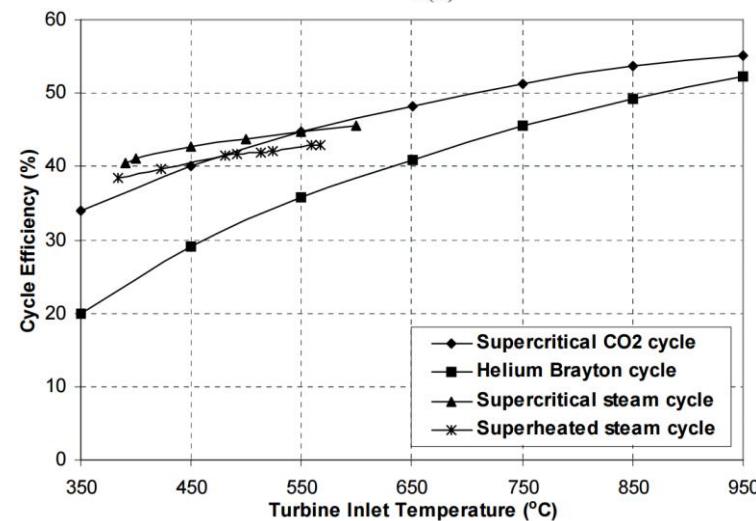
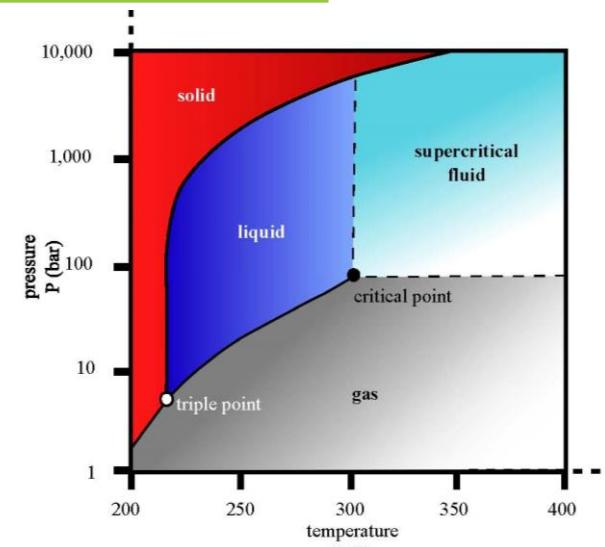


Steam Turbine (250 MWe)



He Turbine
(300 MWe)

1 m S-CO₂ (300 MWe)

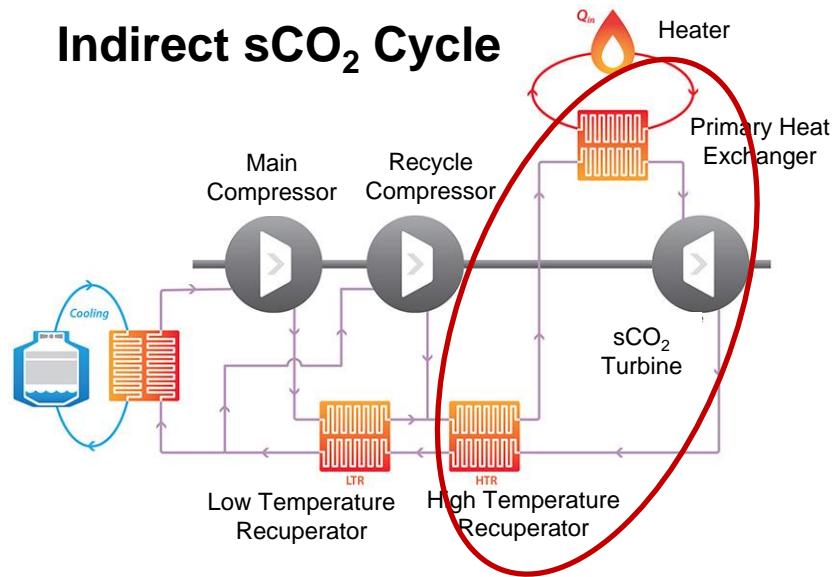


M. J. Driscoll, "Optimized, Competitive Supercritical-CO₂ Cycle GFR for Gen IV Service," MIT-GFR-045, 2008.

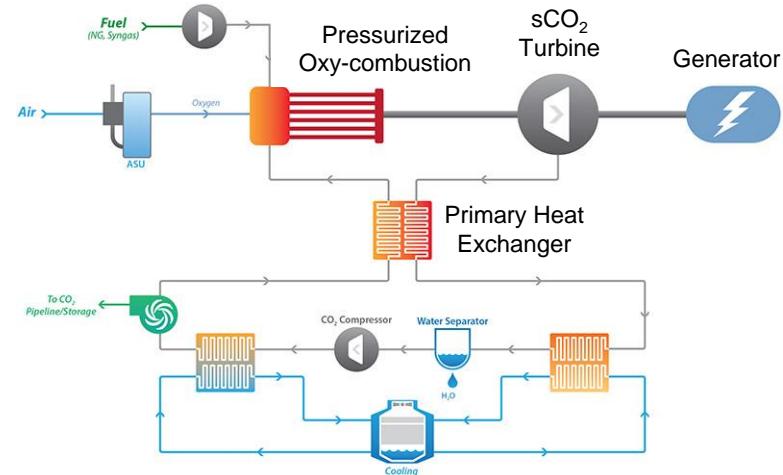
S. A. Wright, "OVERVIEW OF SUPERCRITICAL CO₂ POWER CYCLE DEVELOPMENT AT SANDIA NATIONAL LABORATORIES," in 2011 *University Turbine Systems Research Workshop*, Columbus, Ohio, 2011.

sCO₂ power cycles – materials considerations

Indirect sCO₂ Cycle

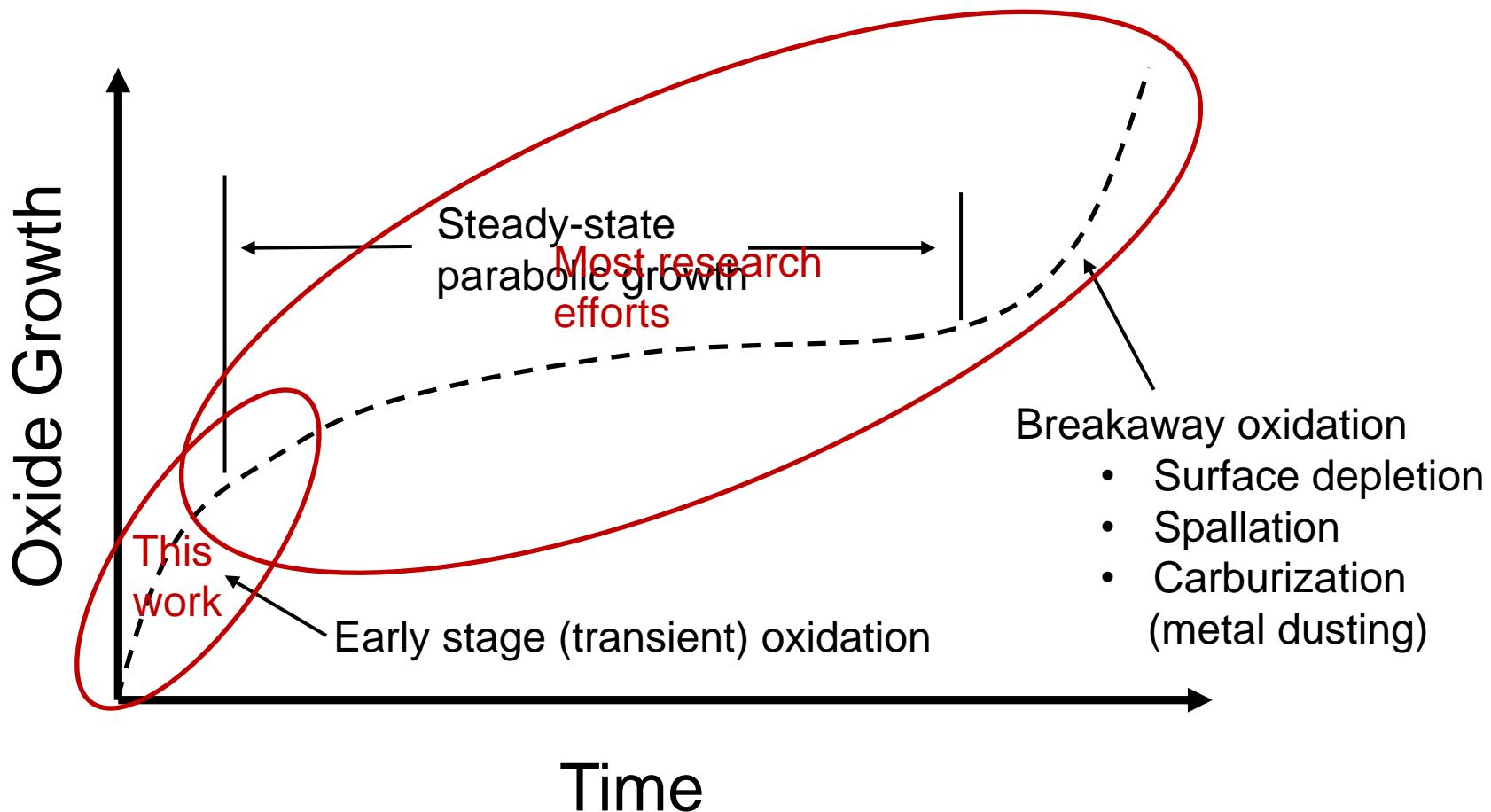


Direct sCO₂ Cycle



Cycle Type	Component	Inlet		Outlet		Fluid components
		T (°C)	P (MPa)	T (°C)	P (MPa)	
Indirect	Heater	450-535	1-10	650-750	1-10	High purity CO ₂
	Turbine	650-750	20-30	550-650	8-10	
	HX	550-650	8-10	100-200	8-10	
Direct	Combustor	750	20-30	1150	20-30	CO ₂ containing H ₂ O, O ₂ , and other impurities
	Turbine	1150	20-30	800	3-8	
	HX	800	3-8	100	3-8	

Typical stages of high-T alloy oxidation



Experimental

Exposure Conditions

- Fluid = 99.999% CO₂
- T = 700 °C
- P = 0.1 MPa (atmospheric) or 20 MPa (supercritical)
- t = 5 min – 500 h

Exposure Apparatus

- High-temperature confocal scanning laser microscope
 - t = 5 min, P = 0.1 MPa
- Tube furnace
 - t = 1 – 500 h, P = 0.1 MPa
- Autoclave
 - t = 500 h, P = 20 MPa

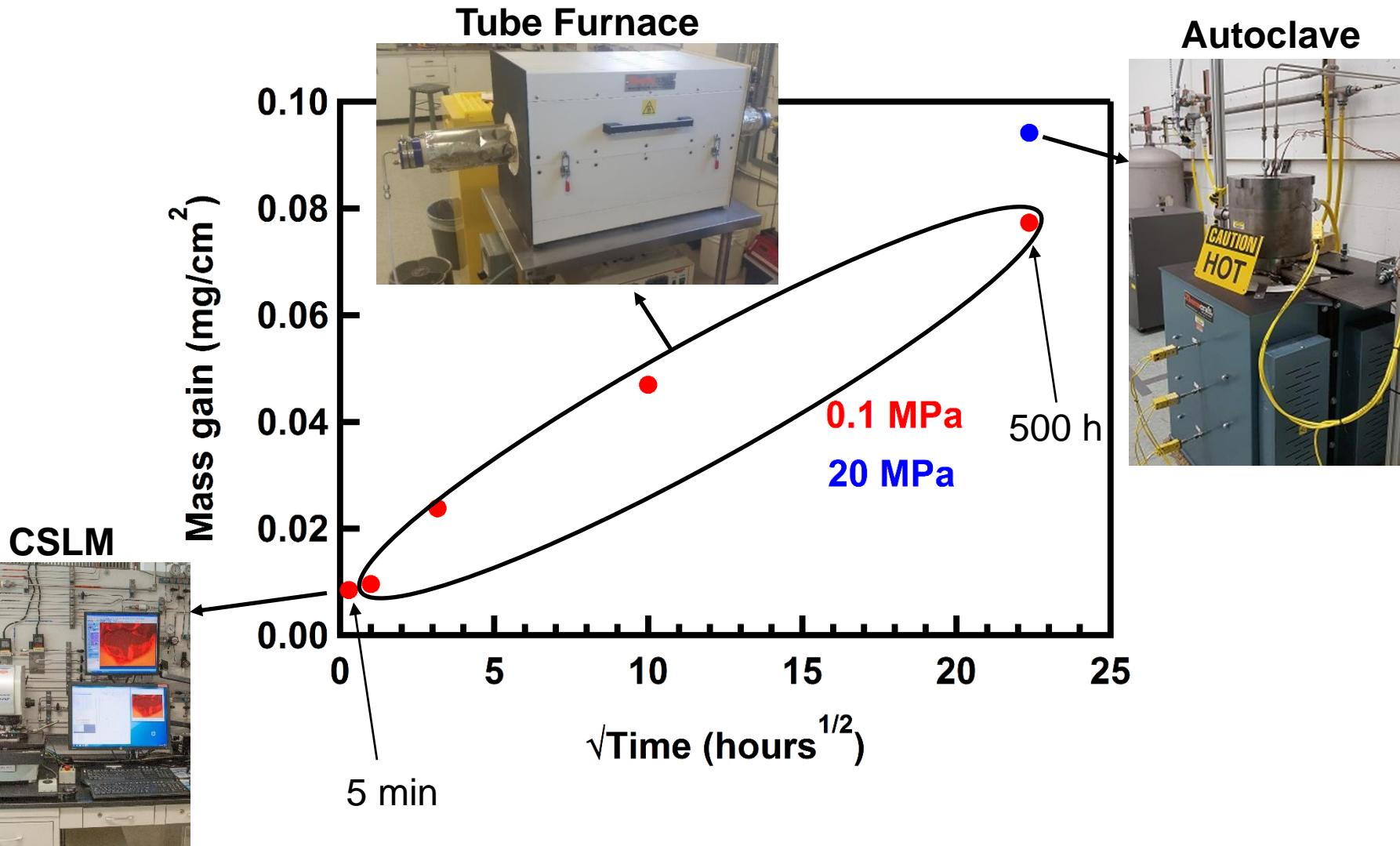
Alloy 617 composition

Element	wt%
Ni	53.3
Cr	22.4
Co	11.5
Mo	9.6
Al	1.1
Fe	1.1
Ti	0.3
C, Si, Mn, Cu	<0.1
B, P, S	<0.01

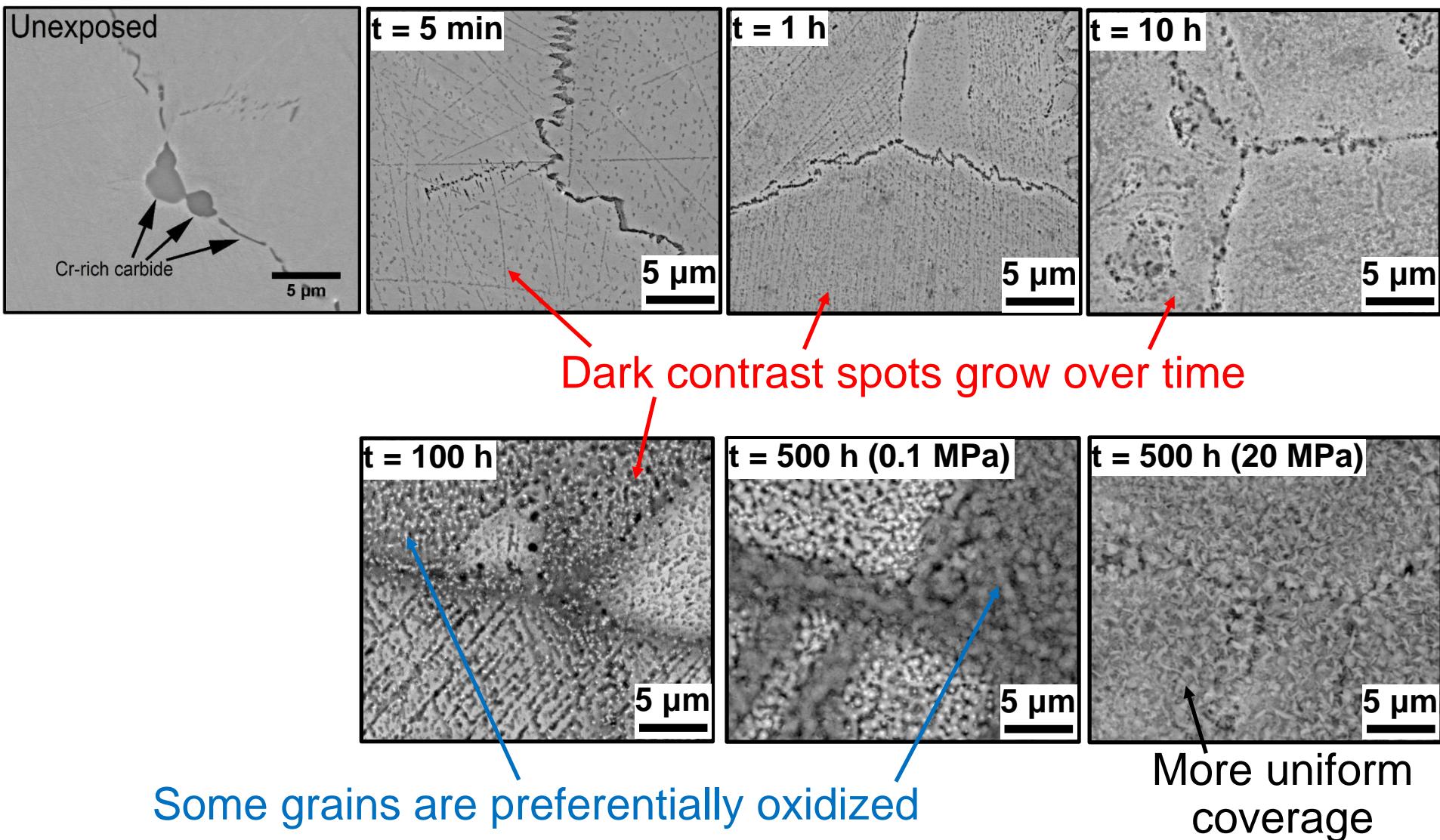
Analysis

- Cross-sectional transmission electron microscopy
- Samples generated using focused ion beam lift-out method

Mass change

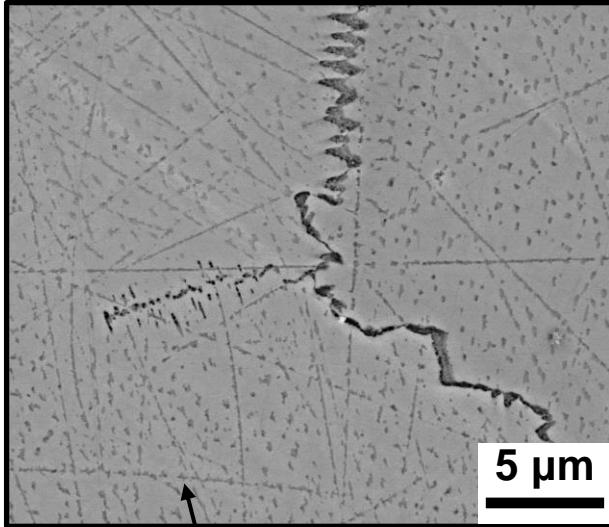


Evolution of surface morphology



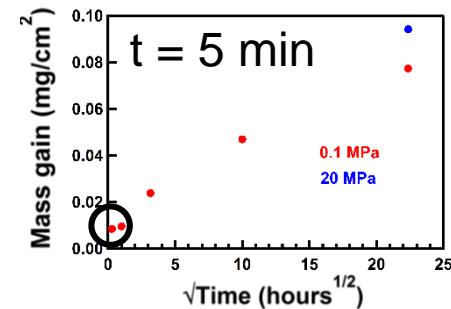
Sub-surface void formation

BSE surface image



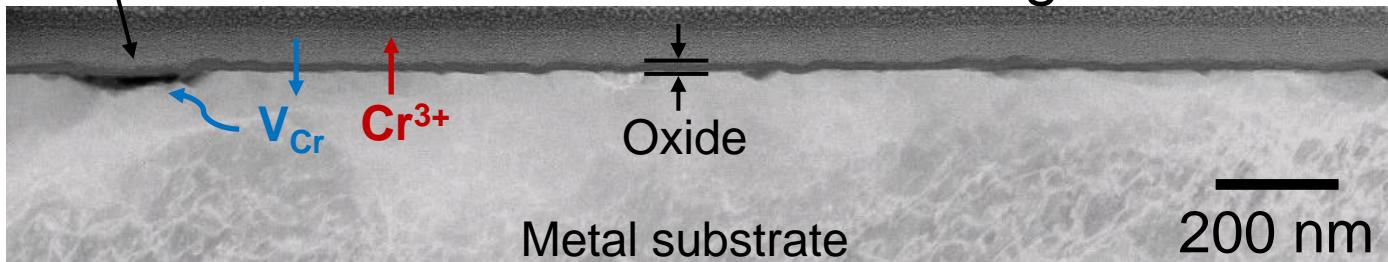
Sub-surface voids

Voids are formed at the oxide/metal interface during the initial stages of oxidation, most likely due to condensation of Cr vacancies.



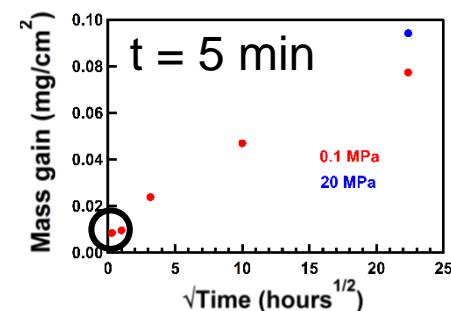
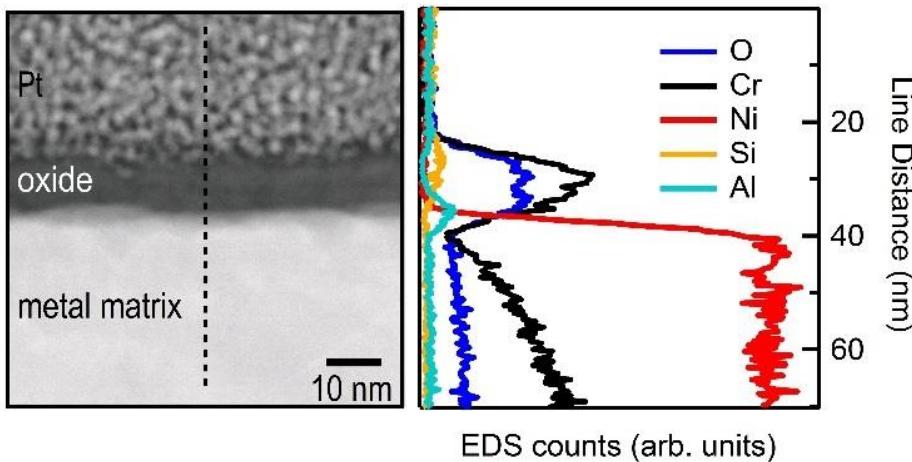
These voids are formed preferentially along micro-scratches and grain boundaries.

Cross-sectional TEM image

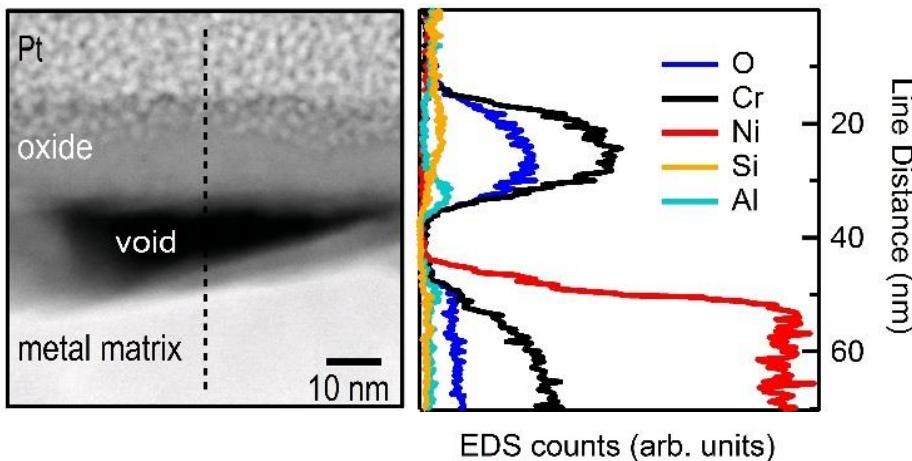


Sub-surface void

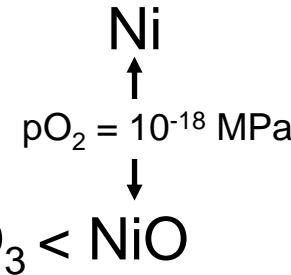
Selective oxidation of Cr



After a short (5 min) exposure the oxide is Cr-rich, containing some Si and Al.

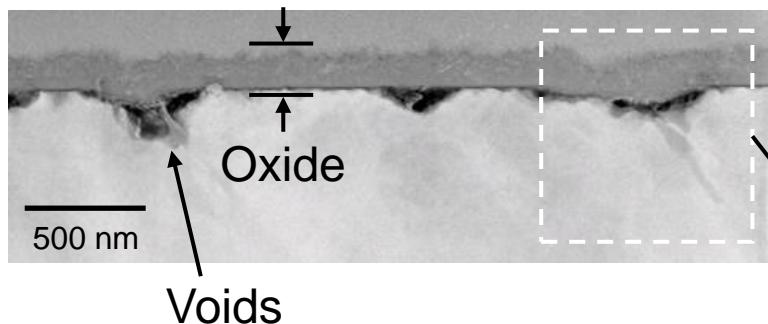


In high purity CO_2 at 0.1 MPa and 700 °C, expected $\text{pO}_2 \approx 10^{-7} - 10^{-6}$ MPa. Yet, no Ni-oxides are formed.



Thermodynamic stability

Continued oxide growth

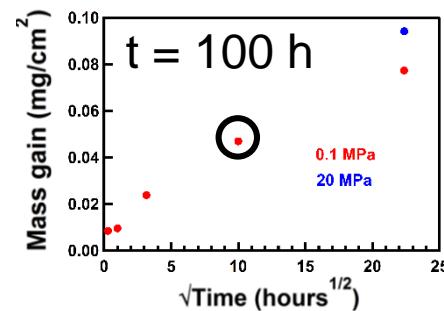
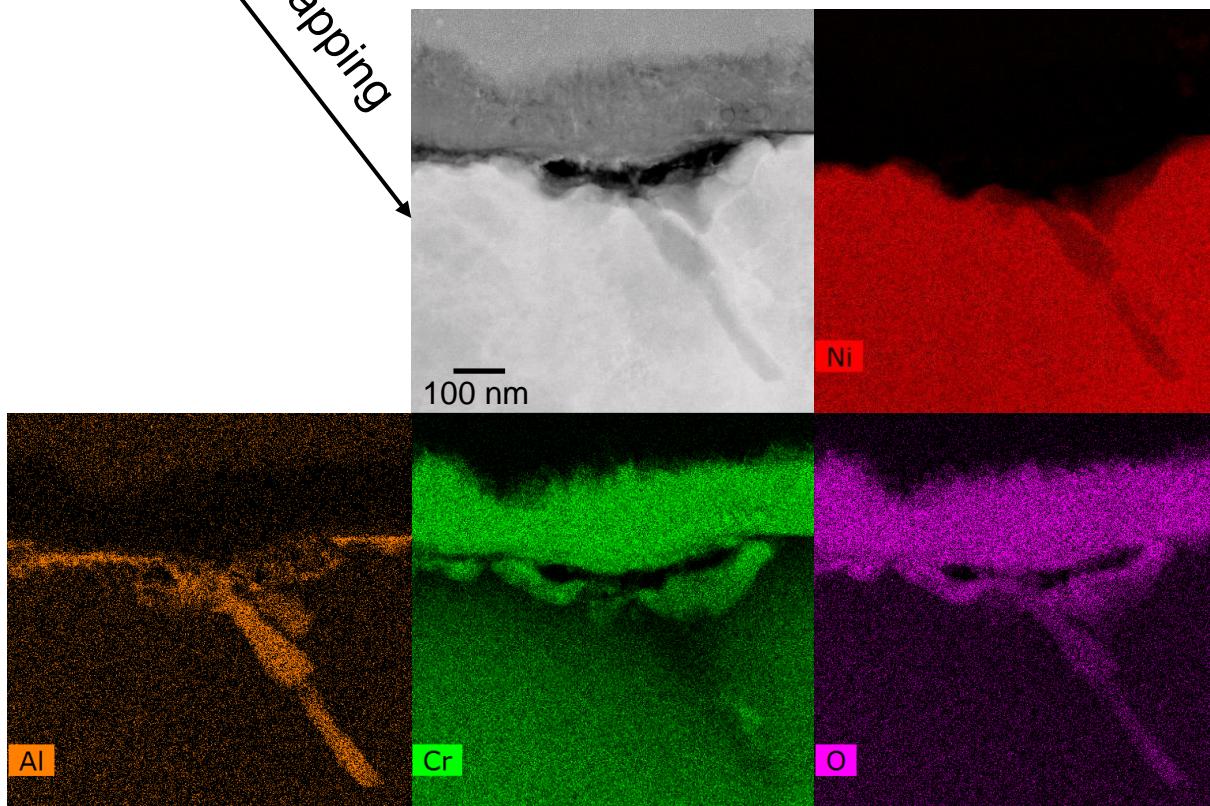


Sub-surface voids continue to grow. Al is oxidized inside and adjacent to the voids.

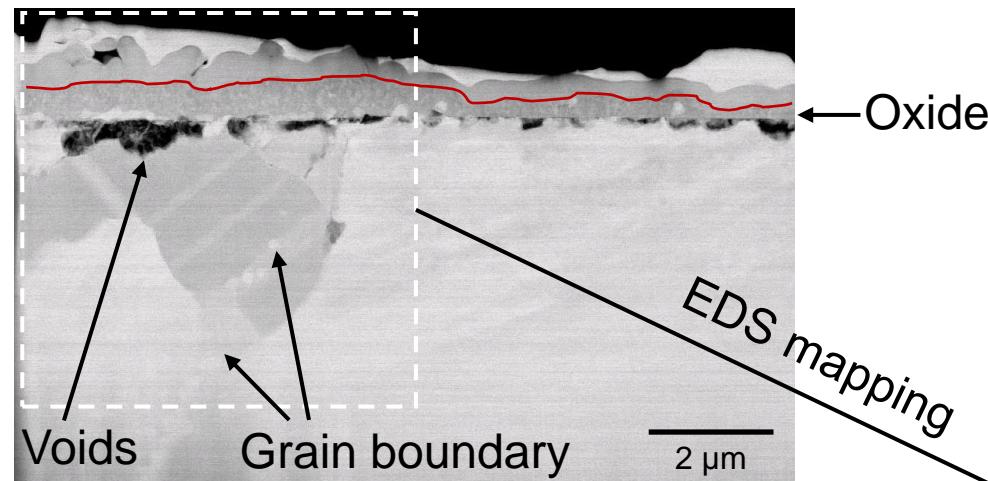
Cr-oxide forms above and below voids.

This suggests that both outward and inward oxide growth has occurred.

EDS mapping



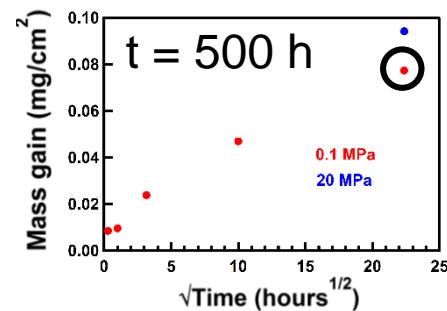
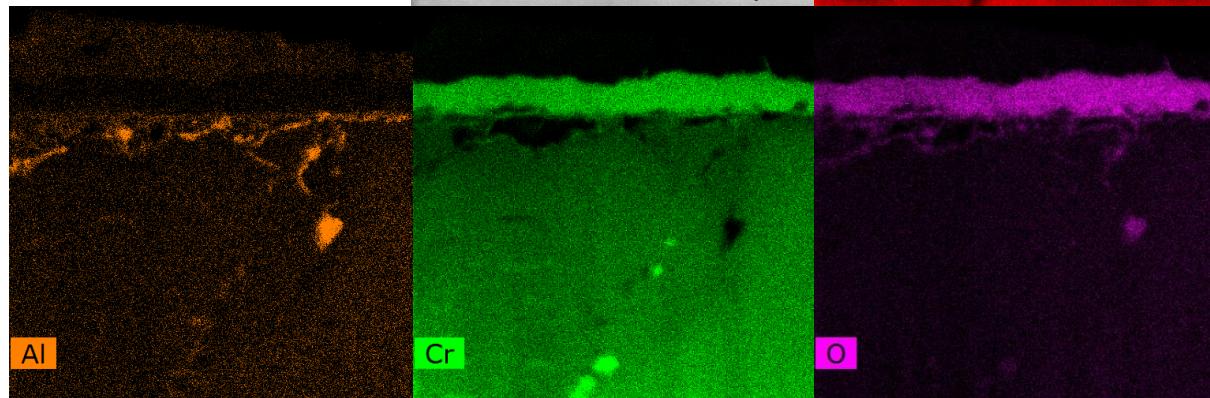
Continued oxide growth



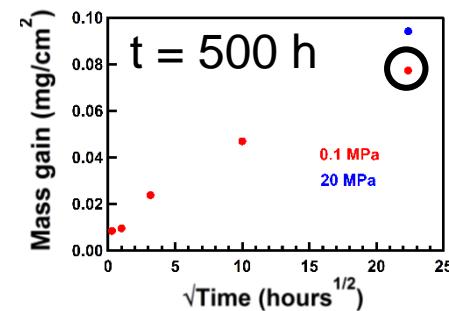
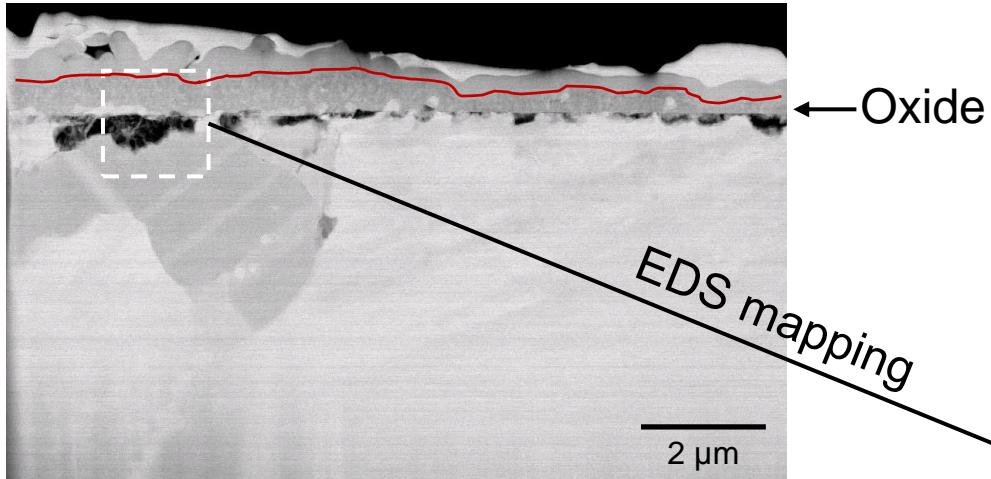
Continued void growth.

Cr-depletion and recrystallization near the alloy surface.

Short-circuit diffusion paths created by voiding and recrystallization lead to further internal oxidation of Al.

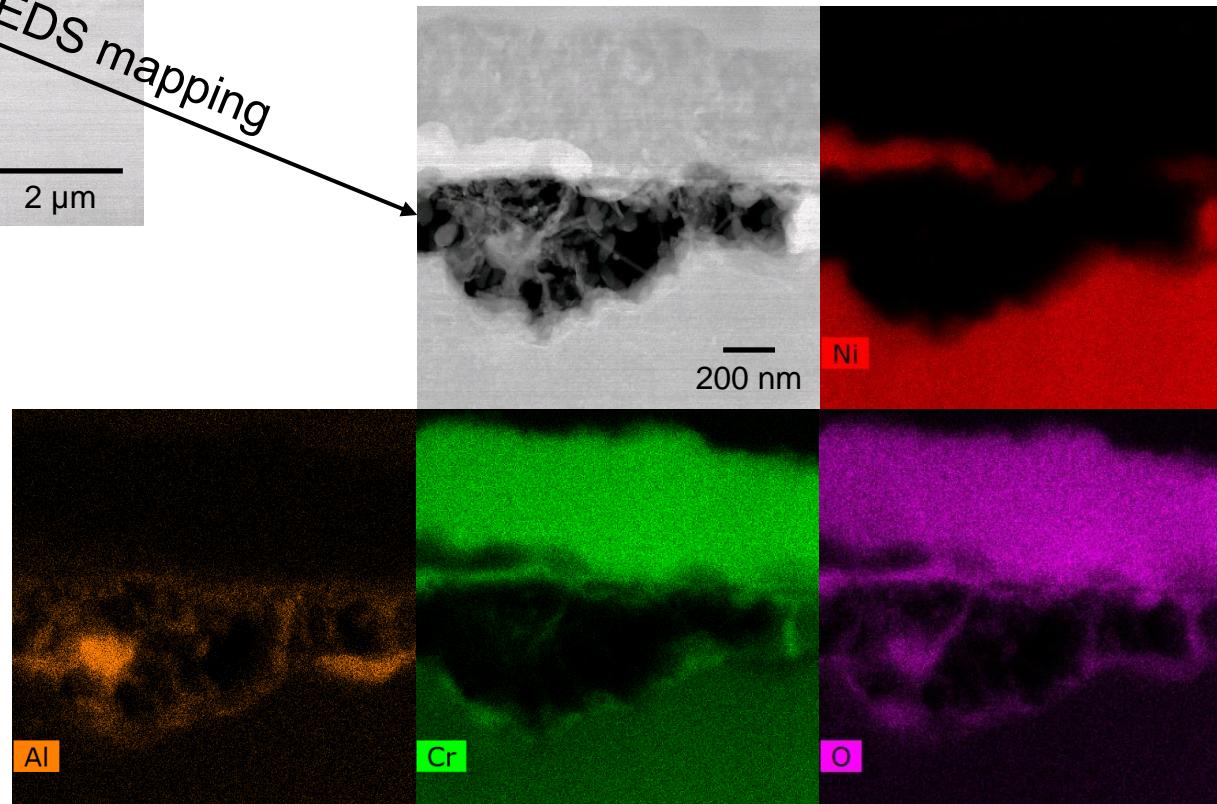


Role of voids during oxidation

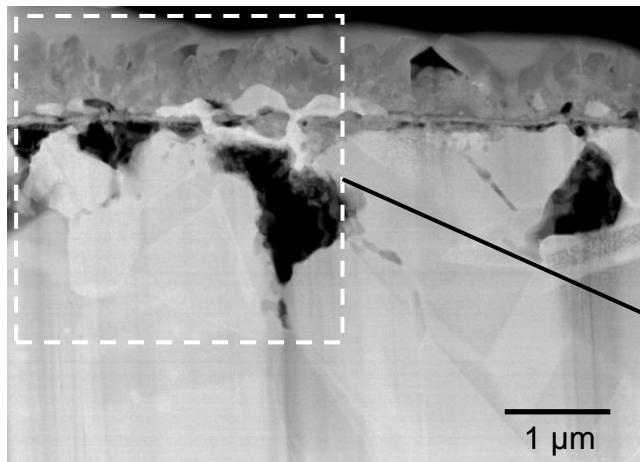


As voids form near the oxide/alloy interface, metal that is depleted of Cr becomes trapped and is incorporated into the scale.

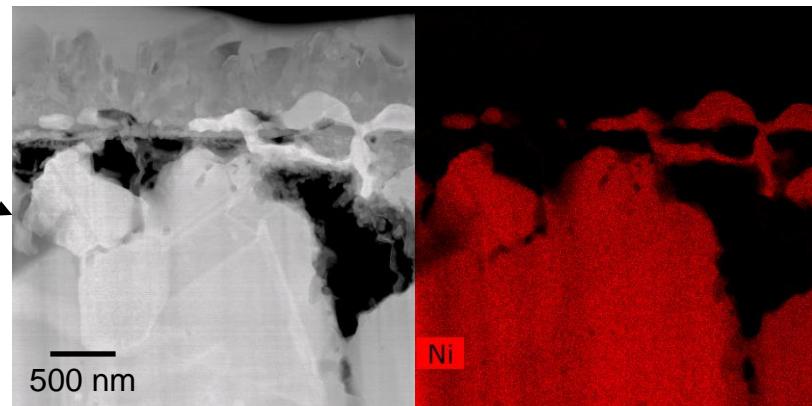
Over time, the voids are filled with Al-oxide.



The effects of pressure

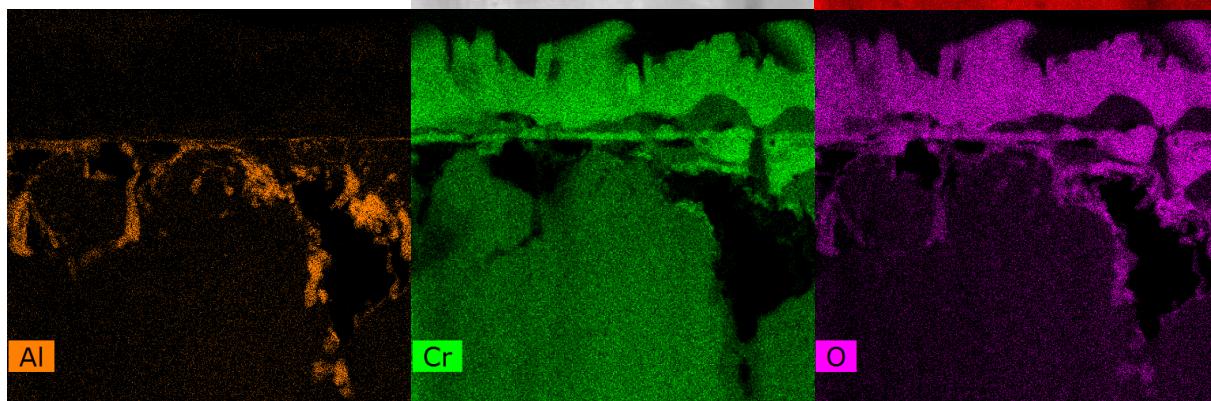


Oxide
Voids
EDS mapping



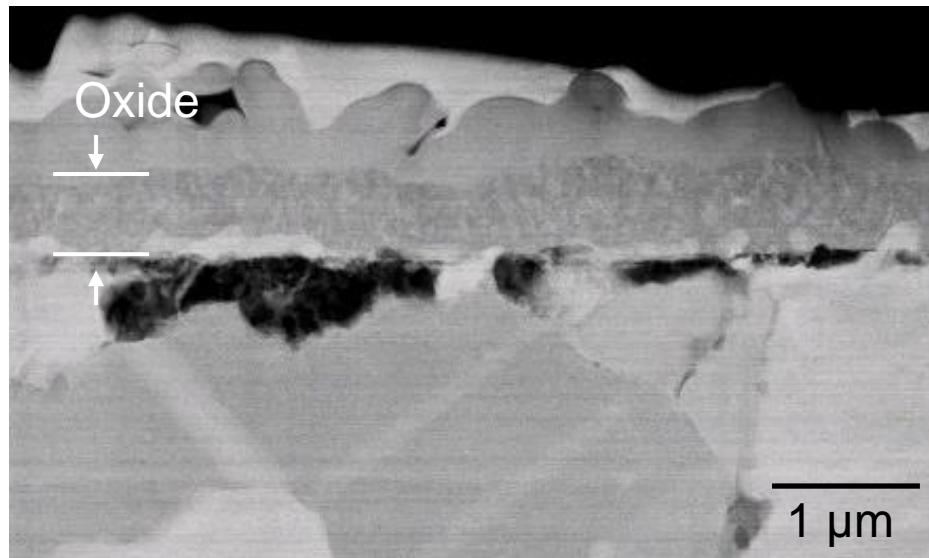
As with the 0.1 MPa exposure, we observe:

- Sub-surface voids
- Recrystallization
- Trapping of Cr-depleted metal
- Oxidation of Al inside and adjacent to voids

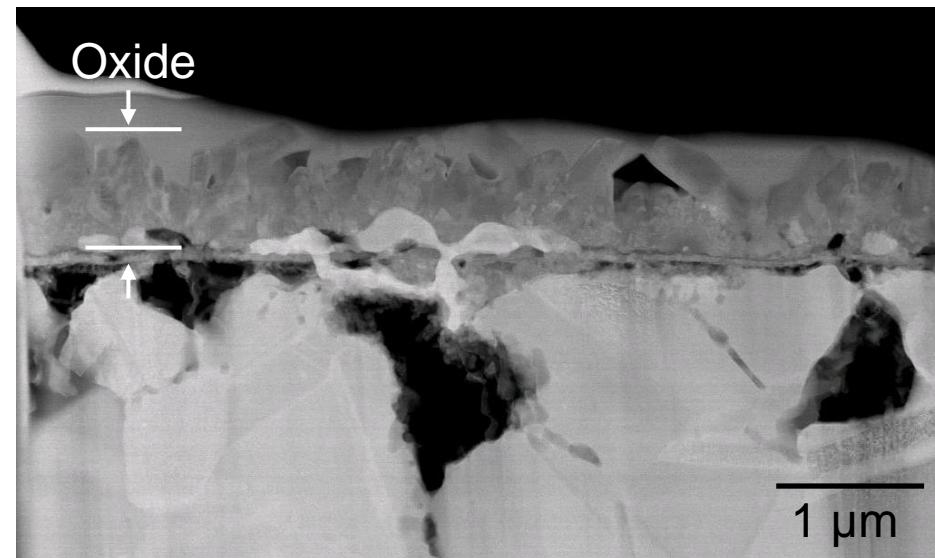


Atmospheric vs. Supercritical exposure

0.1 MPa, 500 h



20 MPa, 500 h



20 MPa exposure is controlled by similar processes as 0.1 MPa, but proceeds to a larger extent.

- 20-30% thicker oxide layer.
- More extensive sub-surface effects including voiding and recrystallization.
- Increased inward oxide growth (note Cr-depleted metal and voids that are incorporated into the oxide layer).

Summary and Conclusions



- Ni-Cr-Al alloy (617) was oxidized in CO_2 at 700 °C for 5 min – 500 hours.
- Good oxidation resistance was observed.
 - Protective Cr_2O_3 -type surface forms in < 5 min.
 - < 0.1 mg/cm² mass gain after 500 h (both 0.1 MPa and 20 MPa).
- Similar oxidation processes were observed in 20 MPa (supercritical) and 0.1 MPa (atmospheric) exposures, however these processes were more extensive in 20 MPa exposure.
- Significant sub-surface voiding associated with surface oxidation.
 - Scale thickens by both outward (leading to void formation) and inward (leading to void filling with oxide) growth mechanisms.
 - Cr-depleted metal is trapped in the scale during voiding.
 - The low concentration, highly stable oxide-former (i.e., Al) is oxidized inside and adjacent to these voids—implications for scale adhesion and long-term stability.

Thank you for listening.

Questions?