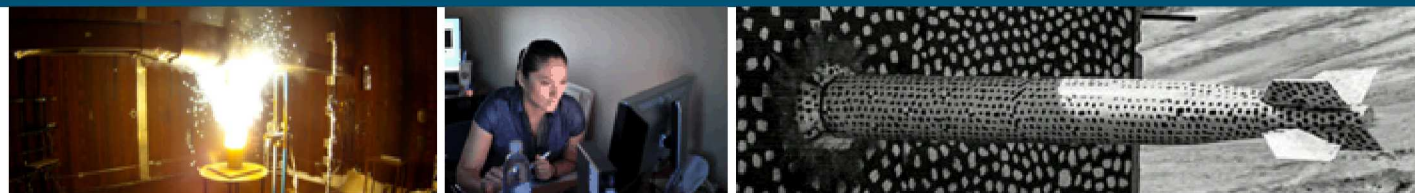


MEC/MHK Load Characterization and Measurements



PRESENTED BY

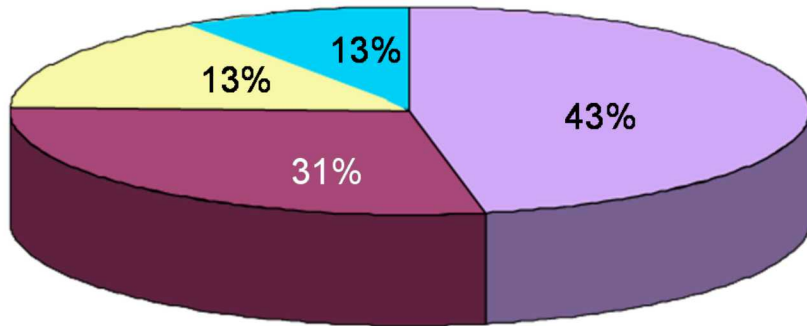
Budi Gunawan

bgunawa@sandia.gov



Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia LLC, a wholly owned subsidiary of Honeywell International Inc. for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

Sandia National Labs



- Nuclear Weapons
- Defense Systems & Assessments
- Energy, Climate, & Infrastructure Security
- International, Homeland, and Nuclear Security



- Federally funded research and development center
- On-site workforce: 12,001 (10,715 NM, 1,286 CA)
- FY16 Budget: \$3 Billion
- Renewable Energy Programs: Solar, Wind, Water, Geothermal, Biomass

Motivations:

1. MEC/MHK design load

- Provide characteristic/design loads for material performance studies

2. Industry needs for structural and mechanical load measurements

- Ability to measure loads on device, as a short-term need (MHK Composites Workshop 2015)
- “In the current IEC TC 114 Strategic Business Plan, Load measurement and verification is identified as the highest priority standard for development based on input and agreement from the National Committees”
- ...immediate need of the MHK industry for inexpensive and reliable means of accurately measuring structural loads in real time during ocean trials of WEC and TEC devices (Resolute)
- Load data during field operation to validate structural and hydrodynamic models, provide confidence in system reliability (ORPC)

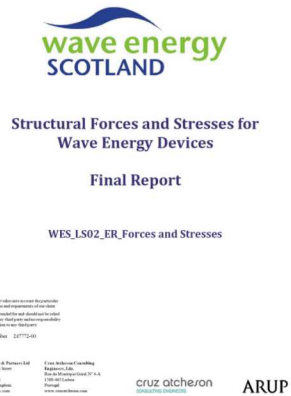
Objectives:

1. Provide design/realistic load for material performance testing
2. Advance the scientific understanding of load measurements and sensor response on composite materials

4 Load design requirements

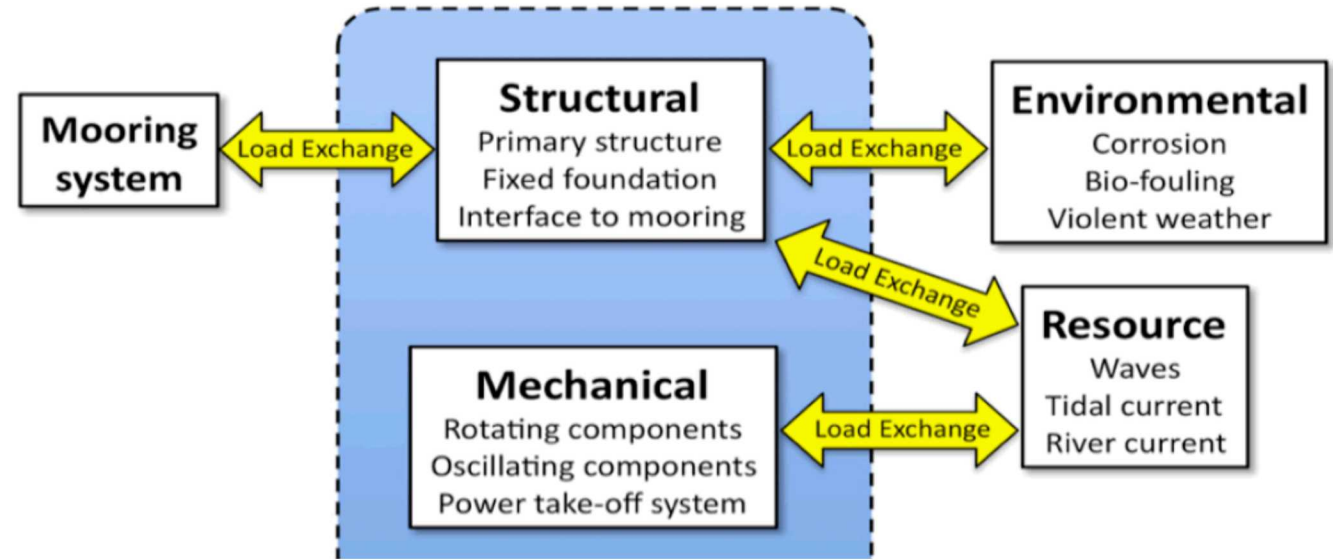


IEC TS 62600 -2 ED2 (2018) Marine energy - Wave, tidal and other water current converters - Part 2: Design requirements for marine energy systems



Structural forces and stresses for wave energy devices. Wave Energy Scotland Report (2016)

Load exchanges on structural and mechanical components

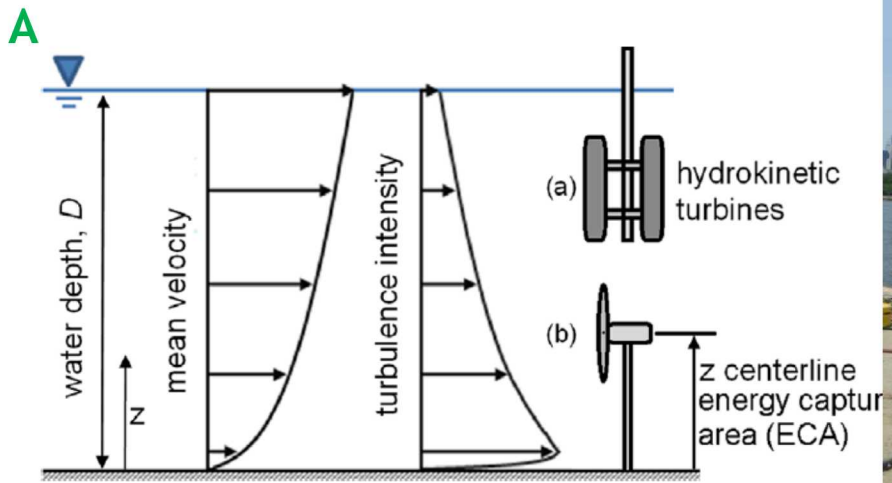


IEC TS 62600 -2 ED2 (2018)

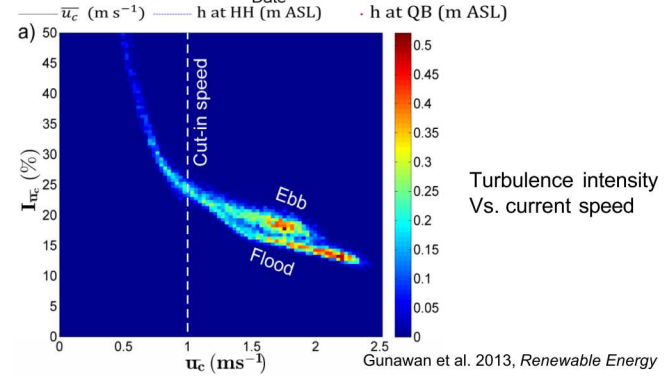
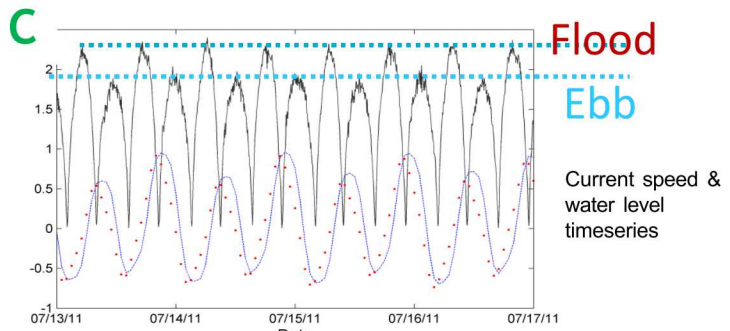
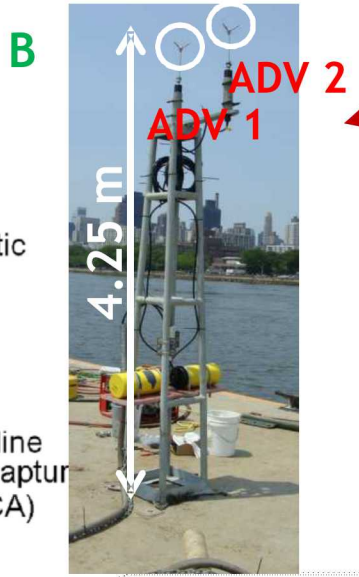
<h3 style="margin: 0;">Design load</h3> $F_d = \gamma_f F_k$ <p>where:</p> <ul style="list-style-type: none"> F_d is the design value for loads acting on the MEC for the given design load case γ_f is the partial safety factor for loads F_k is the characteristic value for the load 	<p style="font-size: 2em;"><</p>	<h3 style="margin: 0;">Material's strength</h3> $f_d = \frac{f_k}{\gamma_m}$ <p>where:</p> <ul style="list-style-type: none"> f_d is the design values for materials γ_m is the partial safety factors for materials f_k is the characteristic values of material properties
---	-------------------------------------	---

Ensure material's strength exceed design loads

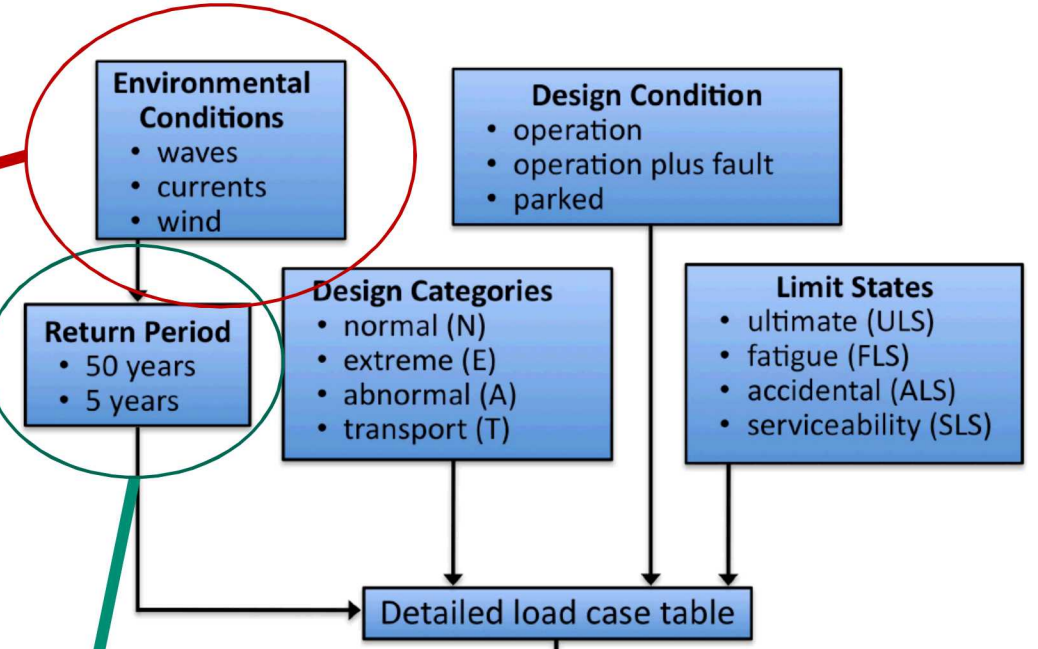
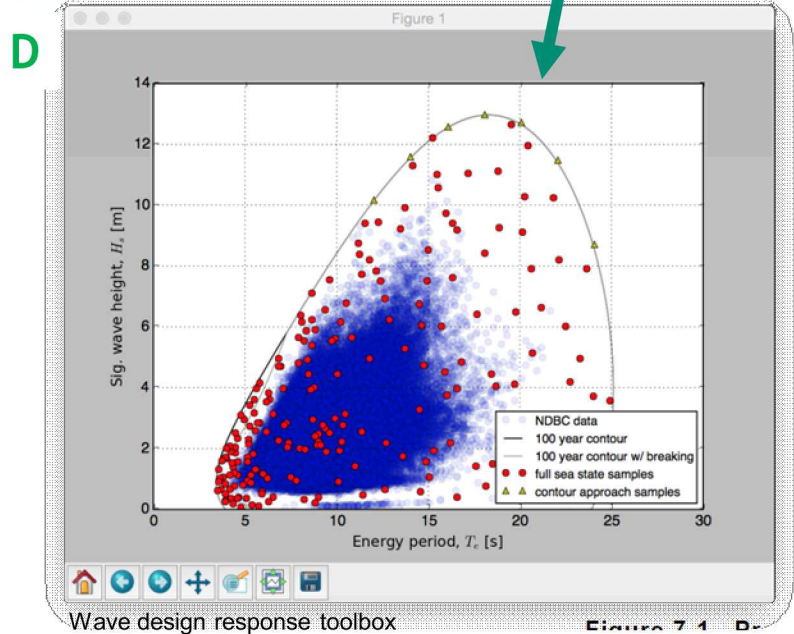
5 IEC design load



Neary et al. 2013, *Renewable and Sustainable Energy Reviews*



Gunawan et al. 2013, *Renewable Energy*



s for determining design loads via load cases

IEC design load

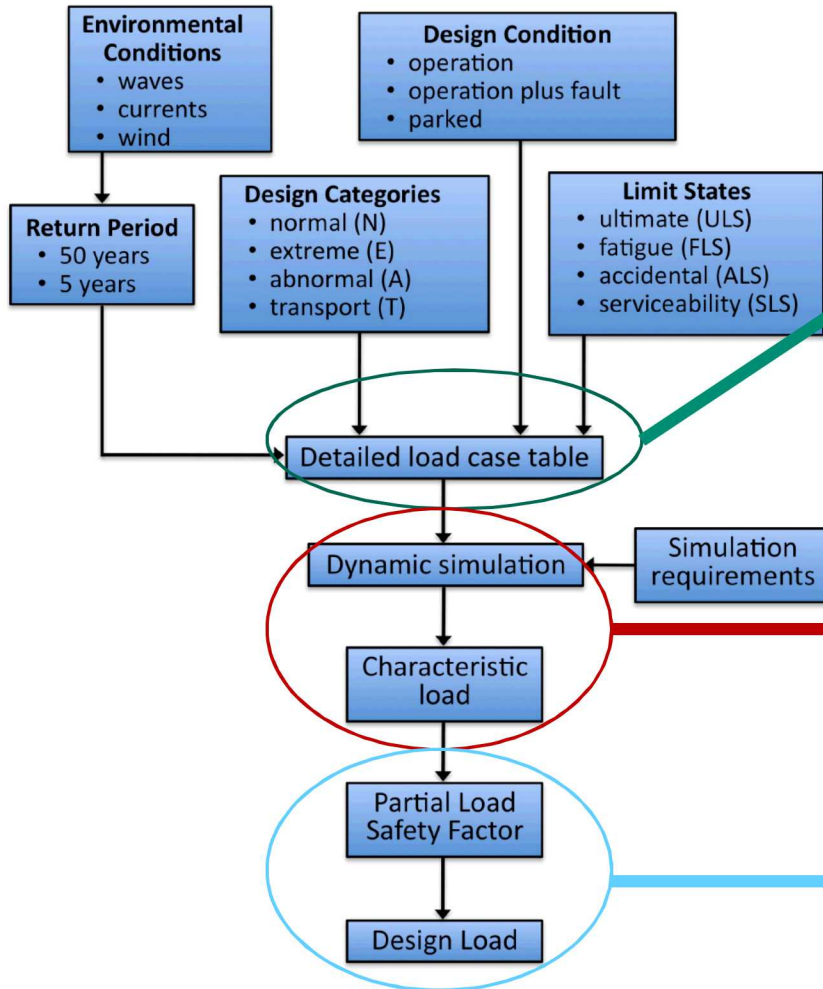
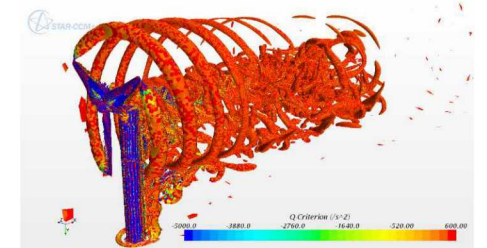
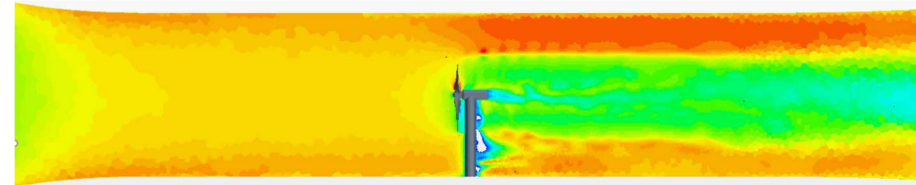


Table 7-5. Design load cases for WEC

Design condition	DLC	Partial safety factor (limit state)	Wave conditions	Current conditions	Water level	Other conditions	Design category
1) Normal operation	1.1	1,35 (ULS) 1,00 (FLS) 1,00 (SLS)	NSS $H_{s,in} \leq H_s \leq H_{s,out}$	NCM $U = U_1$	NWLR		
	Ice	1,35 (ULS) 1,00 (FLS)	No waves	NCM $U_{in} \leq U \leq U_{out}$	NWLR	Ice	
6) Parked/survival conditions	6.1	1,35(ULS) 1,00 (SLS)	ESS $H_s = H_{s50}$	ECM $U = U_5$	EWLR	Wind: EWM ($V = V_5$)	

ECM extreme current model (see 6.2.2.5) NCM normal steady current model (see 6.2.2.4)
 ESS extreme stochastic sea state (see 6.2.1.3) NSS normal stochastic sea state (see 6.2.2.1)



Design load

$$F_d = \gamma_f F_k$$

< Material's strength

$$f_d = \frac{f_k}{\gamma_m}$$

Figure 7-1. Process for determining design loads via load cases

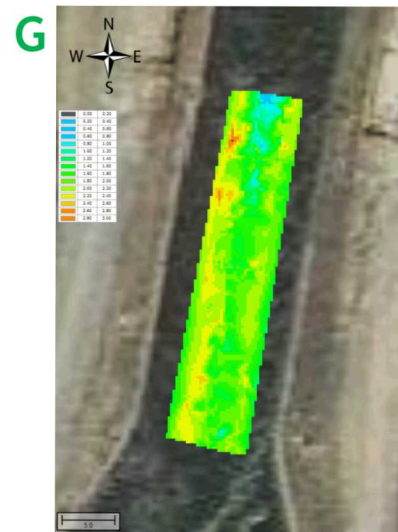
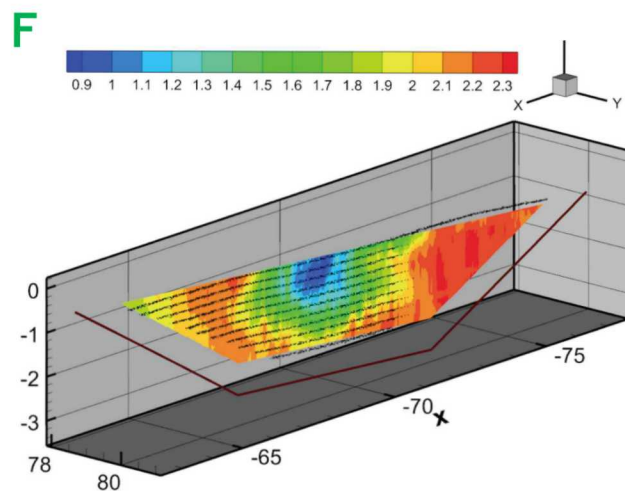
7 Real-time load measurements – Instream Energy System testing



Torque sensor



Drag/thrust load sensor



ENERGY Energy Efficiency & Renewable Energy

Assessing and Testing Hydrokinetic Turbine Performance and Effects on Open Channel Hydrodynamics: An Irrigation Canal Case Study

Budi Gunawan
Water Power Technologies Department, Sandia National Laboratories, Albuquerque NM USA

Vincent S. Neary
Water Power Technologies Department, Sandia National Laboratories, Albuquerque NM USA

Josh Mortensen
Technical Service Center, Hydraulic Investigations and Laboratory Services, United States Bureau of Reclamation, Denver CO USA

Jesse D. Roberts
Water Power Technologies Department, Sandia National Laboratories, Albuquerque NM USA

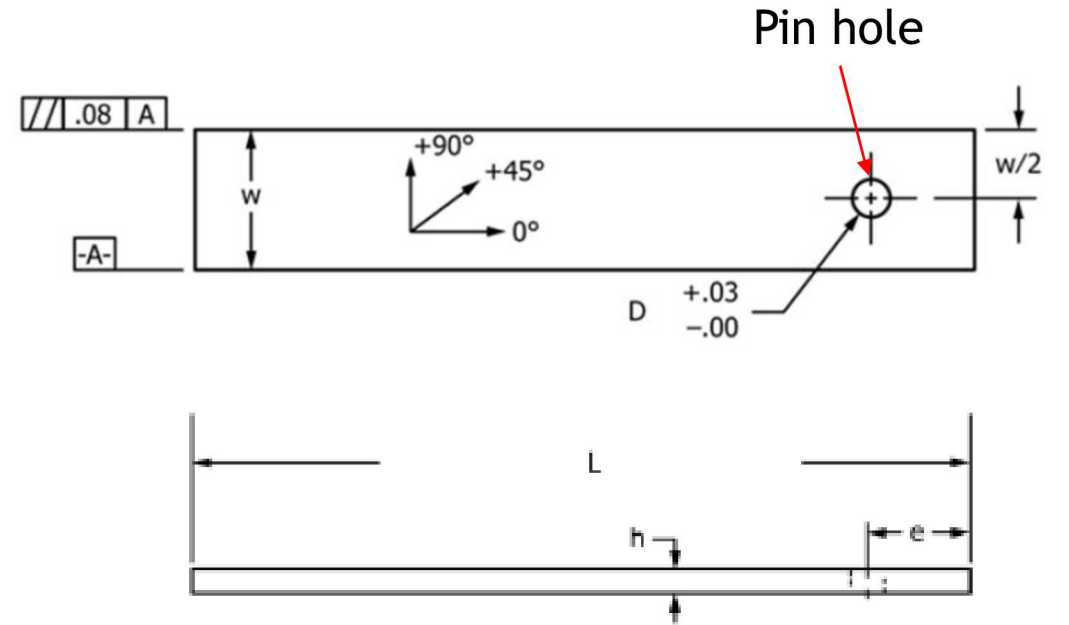
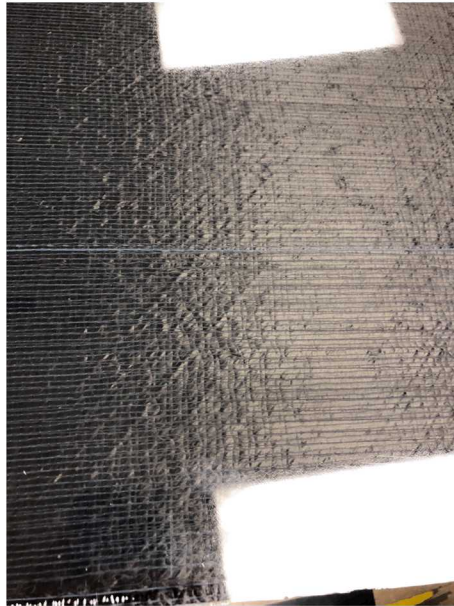
March 2017

Prepared for Department of Energy, Office of Energy Efficiency & Renewable Energy, and Water Power Technologies Office

FY18 work: bolted joint testing

9 Bolted joint testing - ASTM D5961

ASTM D5961: Standard Test Method for Bearing Response of Polymer Matrix Composite Laminates



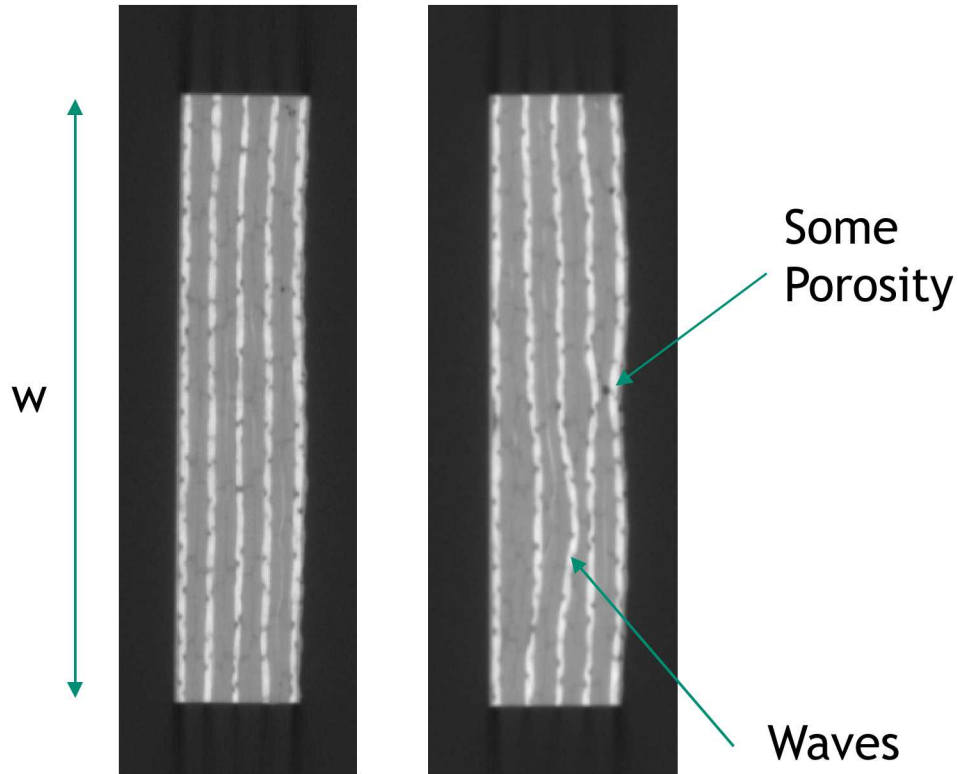
Parameter	Standard Dimension, mm
fastener or pin diameter, d	$6 + 0.00/-0.03$
hole diameter, D	$6 + 0.03/-0.00$
thickness range, h	2-4
length, L	135
width, w	36 ± 1
edge distance, e	18 ± 1
countersink	none

FIG. 1 Double-Shear and Single-Shear One-Piece Test Specimen Drawing (SI)

ASTM D5961

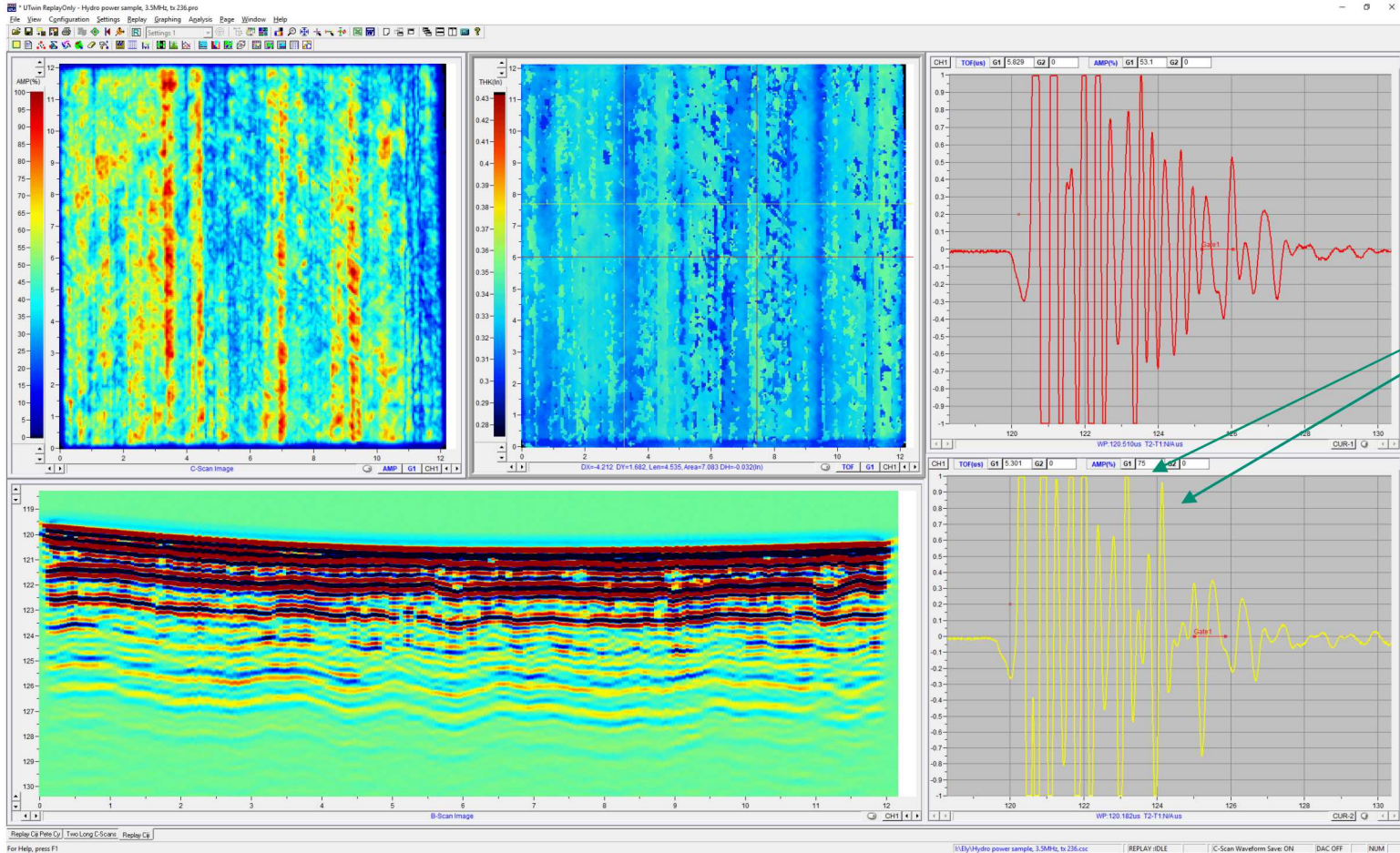
Non Destructive Inspection – CT Scanning

NDI team: Ray Ely, Ciji Nelson, Eddie Moffitt, Dennis Roach

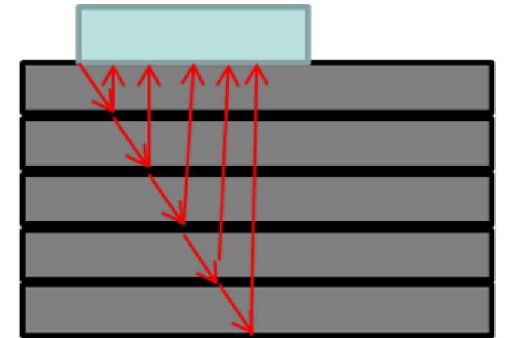


- CT Scans will identify such as porosity and wave, contributed to premature failures
- Overall the specimens appear fairly “clean”, with some occasional porosity and waves
- Due to its high accuracy CT Scans can be used as a reference method for quantifying the effectiveness of other NDI techniques
- CT Scanning may not be the most cost effective solution for performing QA inspections on an ongoing basis

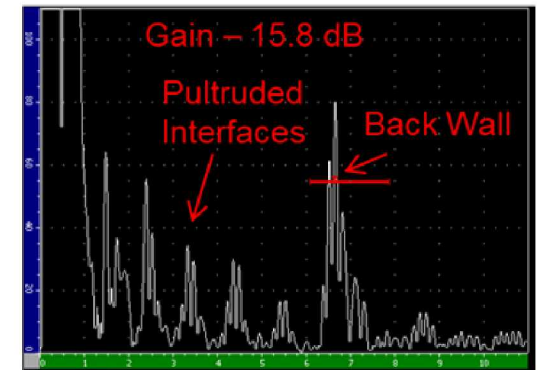
Non Destructive Inspection – Ultrasonic Immersion Testing



Multiple Reflections at Interfaces



Signal return schematic of pultruded sheet interfaces shown on A-Scan



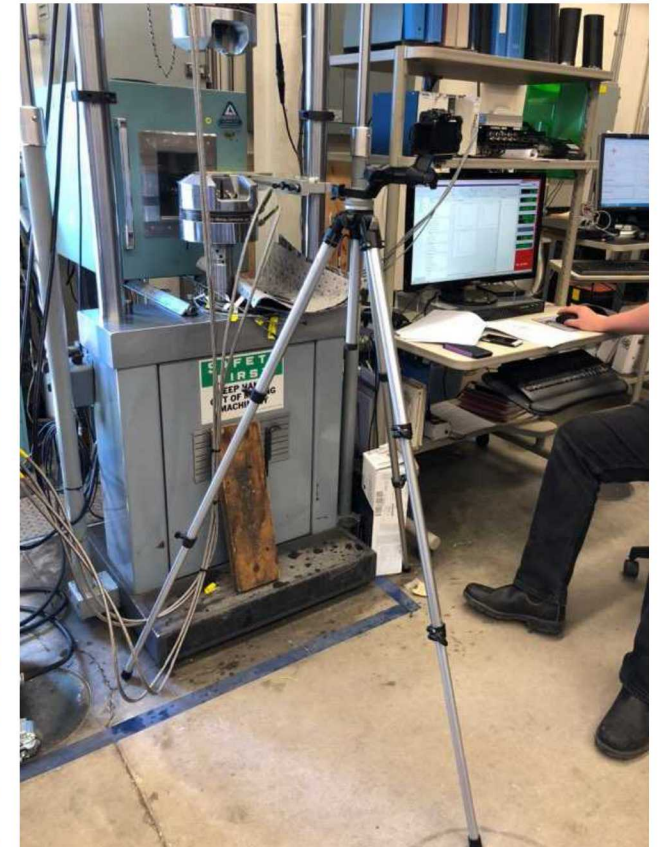
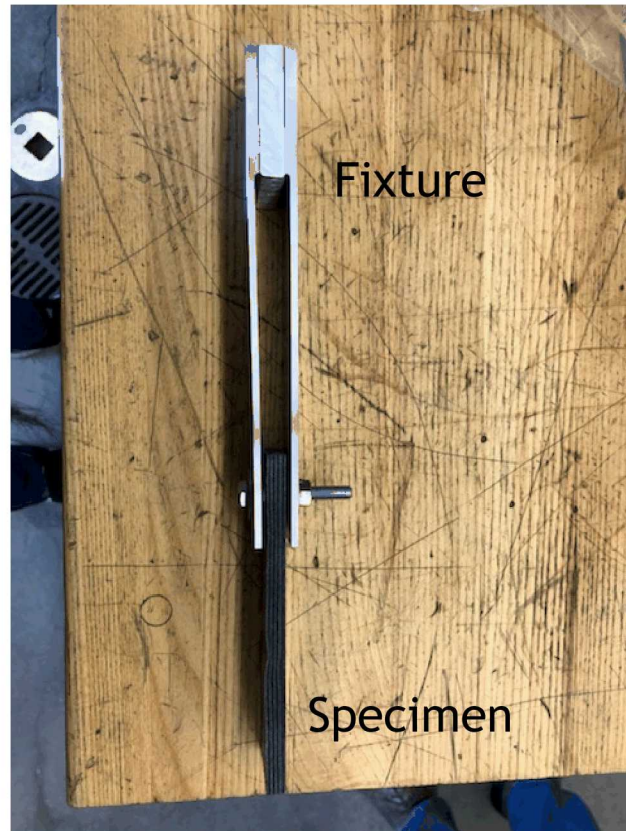
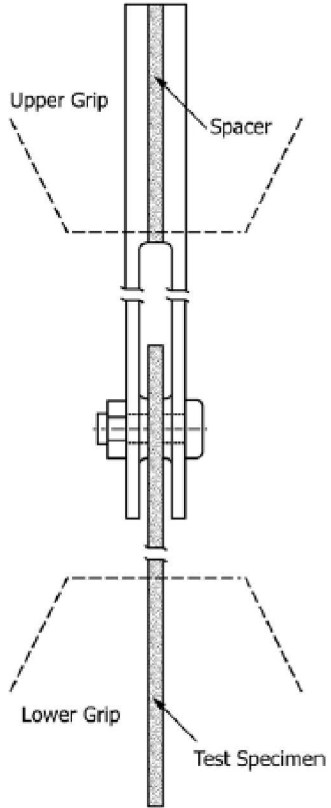
- Ultrasonic immersion testing was performed on a 12" x 12" section cut from the panel as the tensile coupons
- Initial scans showed multiple signal reflections at the alternating carbon/glass interfaces, which result in significant signal attenuation
- Similar results as previous work with multiple layers of pultruded carbon

Bearing Response Testing – Test setup

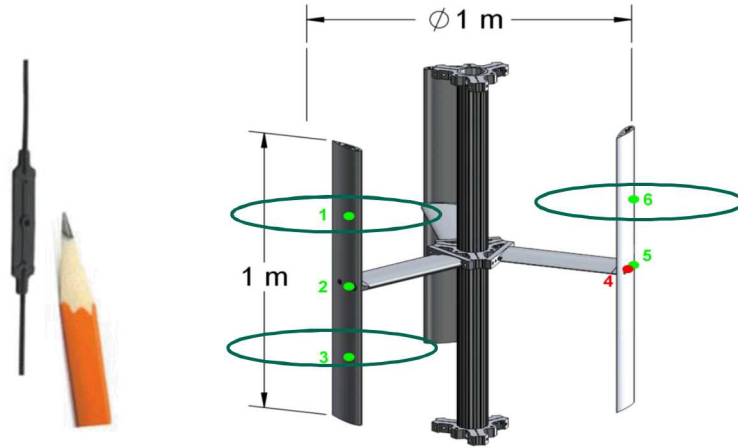
Tensile test team: Mathew Ingraham, James Nicholas, Mariana Castenada, Budi, Bernie

Data output rate: 20 Hz

Measurement time: a few minutes per specimen

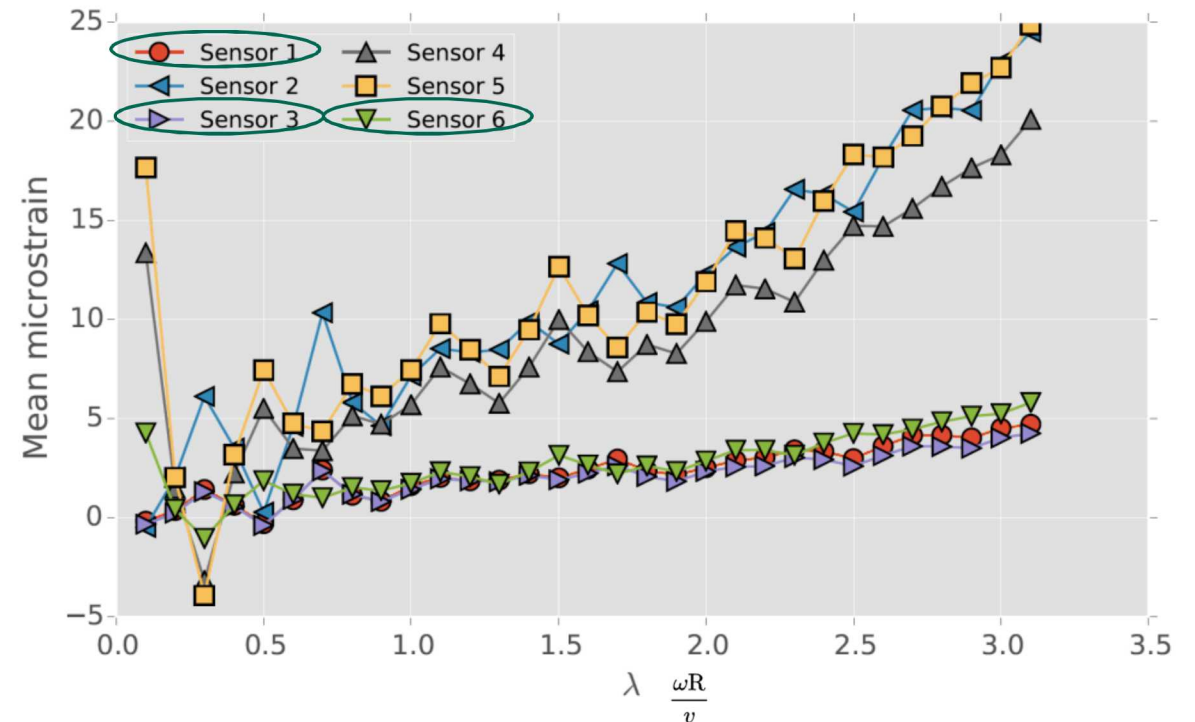


Fiber optic sensor for strain measurement



FBG sensor:

- Low noise (immune to EMI)
- Waterproof
- Small in size
- Rapidly becoming an instrument of choice for wind energy

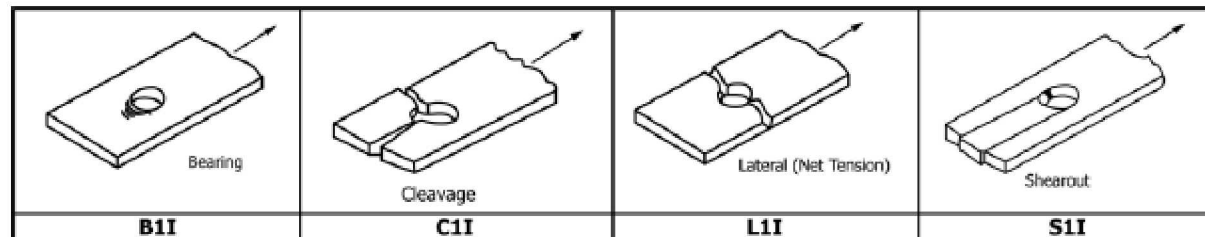


Bearing Response Testing – Failure

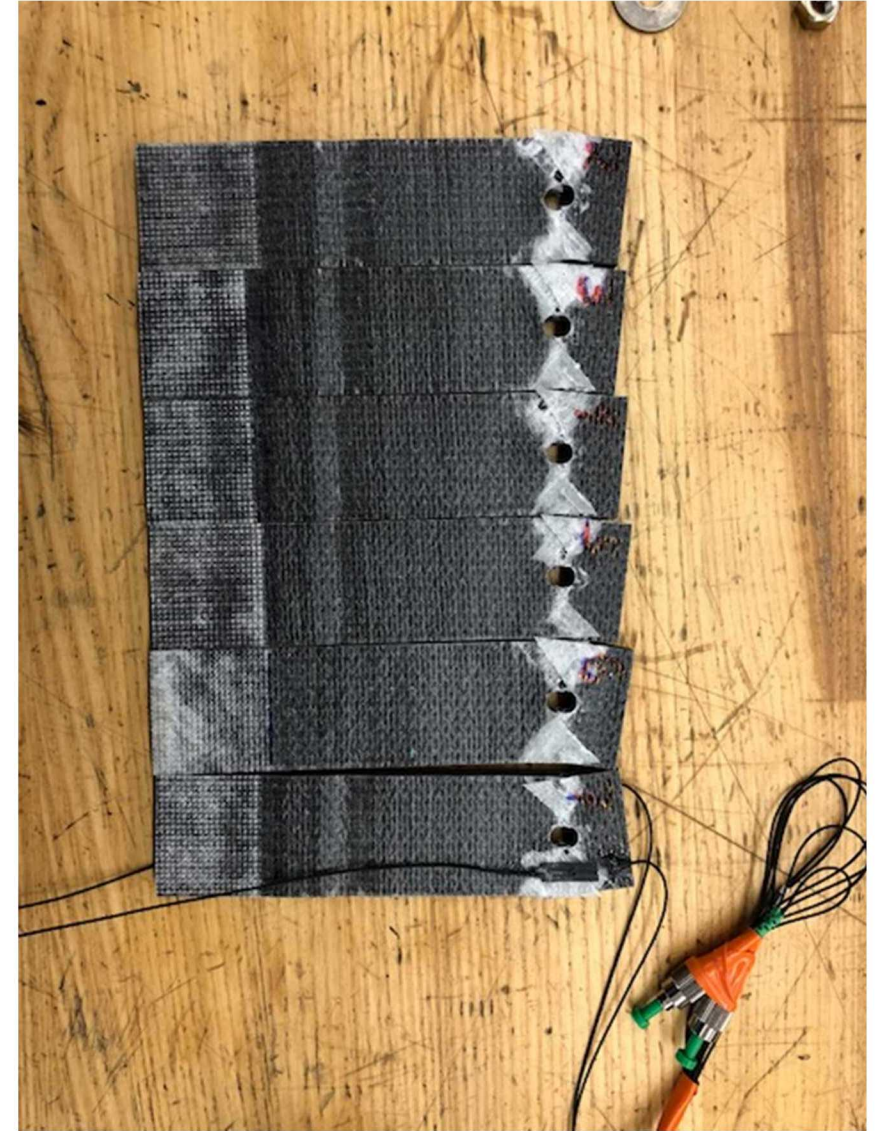
Front

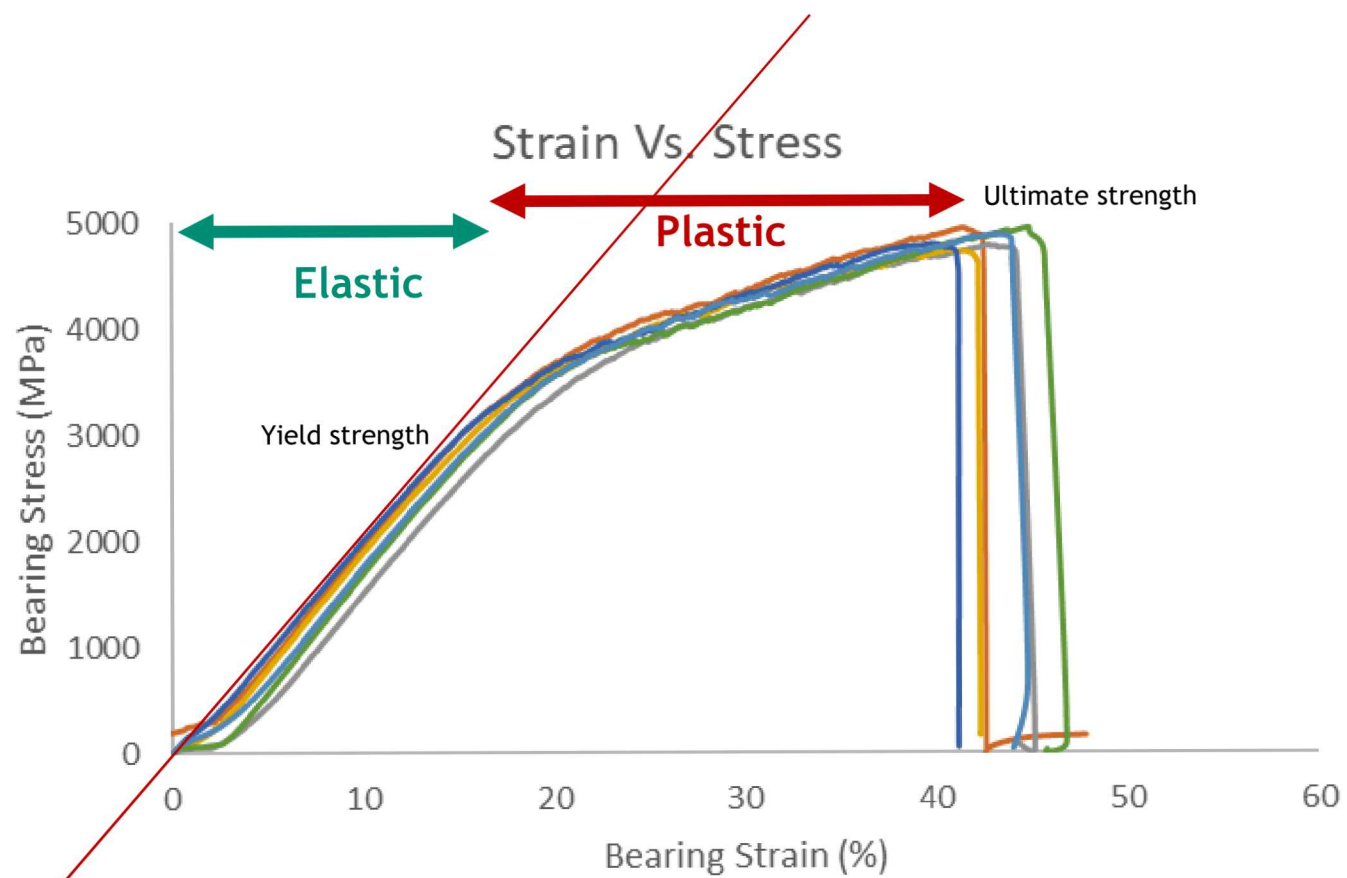


Back

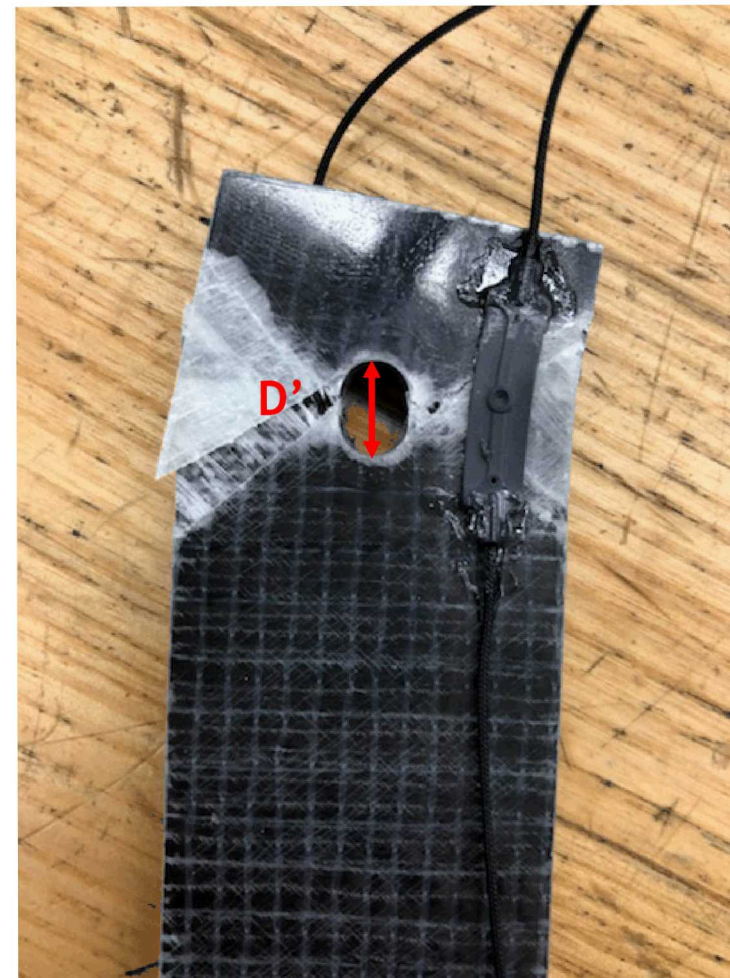


Bearing Test Failure Codes With Illustrations of Common Modes
ASTM D5961





$(D' - D) / D$ in percent



Next steps

Load and sensor

- Continue testing for bolted joint panels, for wet samples and fatigue testing
- Determine design loads for large subcomponent to be tested in FY19
- Instrument subcomponent with load sensors
- Open water testing of subcomponent at PNNL's Marine Science Lab

Non destructive inspection

- Better understand inspection needs (e.g., interply delaminations vs. bondline inspections may drive different inspection methods and optimization)
- Optimize inspections, which may include changes in probe frequency, gate changes and application of Time Corrected Gain (TCG) to account for the signal attenuation
- Evaluate additional inspection methods, such as Phased Array Ultrasonics, and Resonance

Feedback and recommendation are more than welcome!

Bernadette Hernandez-Sanchez
Sandia National Laboratories
baherna@sandia.gov

or

Budi Gunawan
Sandia National Laboratories
bgunawa@sandia.gov