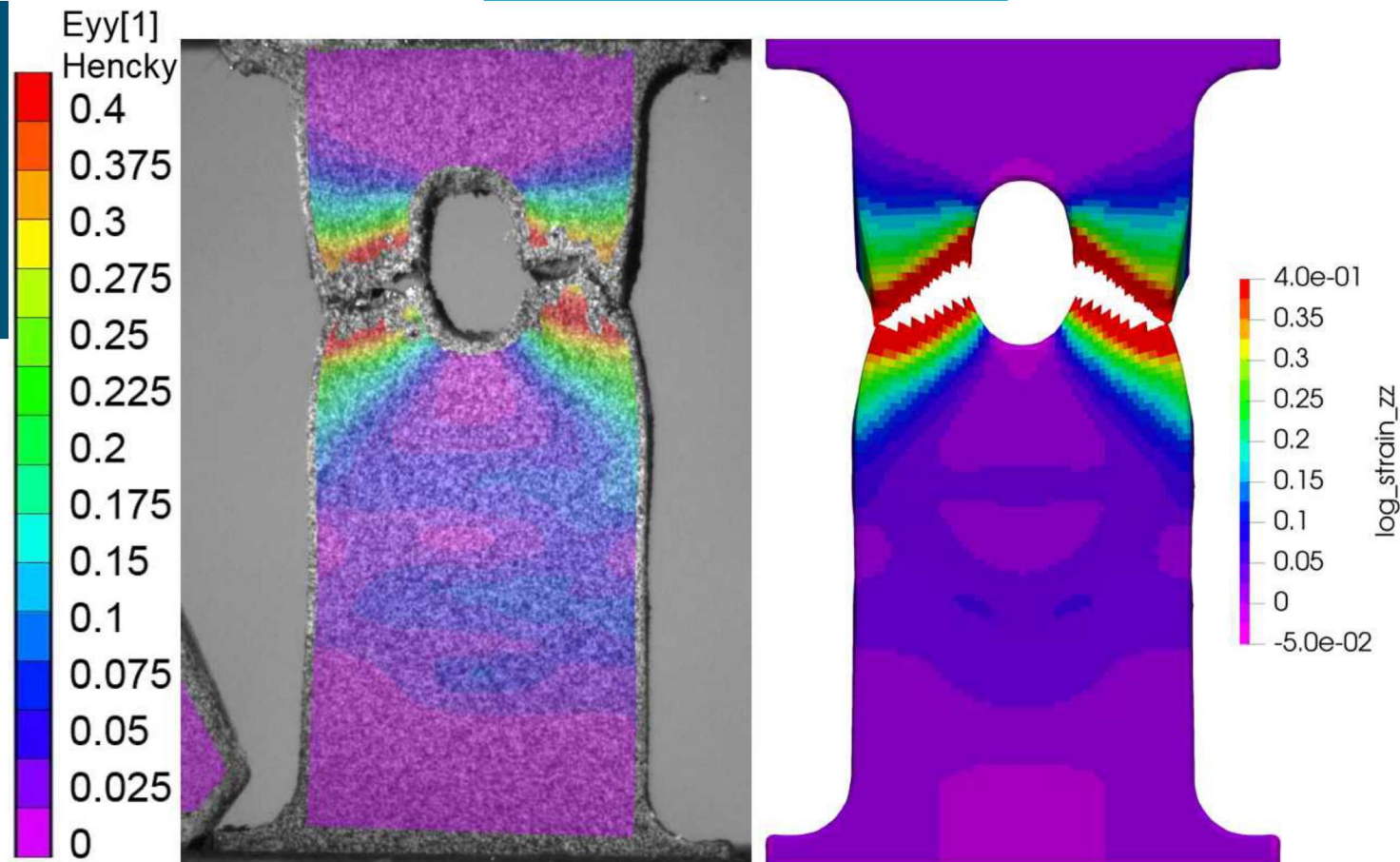


BLIND PREDICTION OF THE RESPONSE OF AN ADDITIVELY MANUFACTURED TENSILE TEST COUPON LOADED TO FAILURE

Lindsay Gilkey¹, John L. Bignell¹,
Remi Dingreville¹, Scott E. Sanborn¹, and
Chris A Jones²

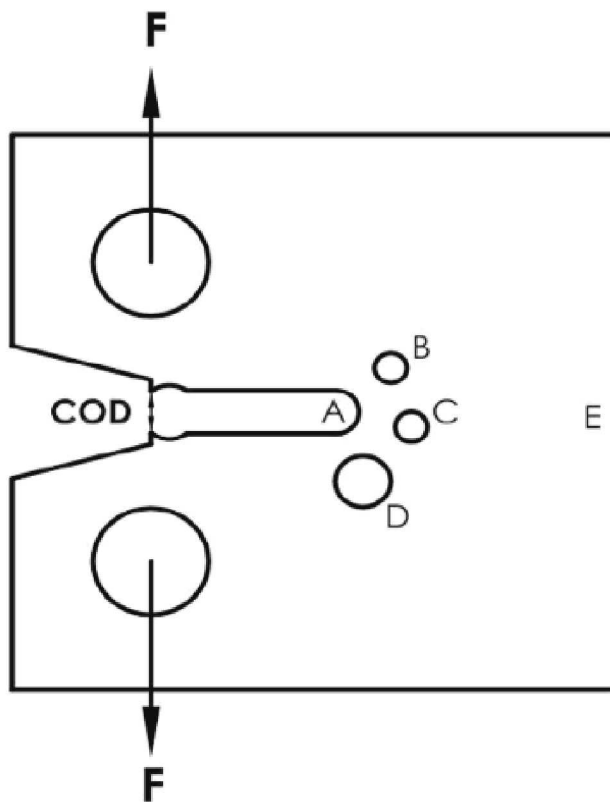
¹ Sandia National Laboratories, Albuquerque, NM

² Kansas State University, Manhattan, KS



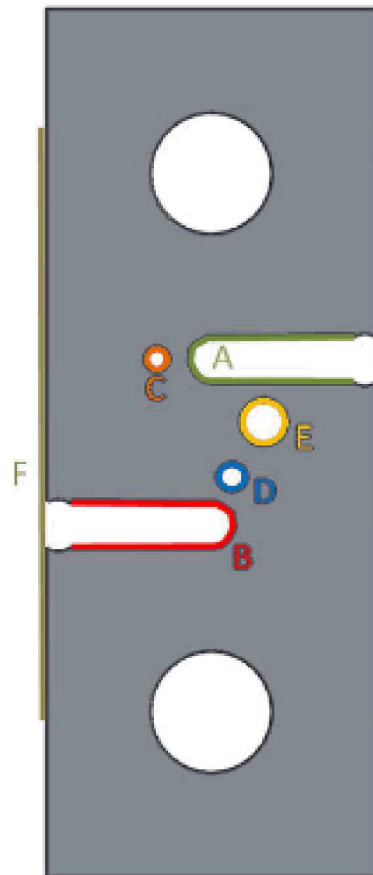
Gauging the state-of-the-art of fracture modeling: Blind prediction through the Sandia Fracture Challenge (SFC)

SFC - 2012



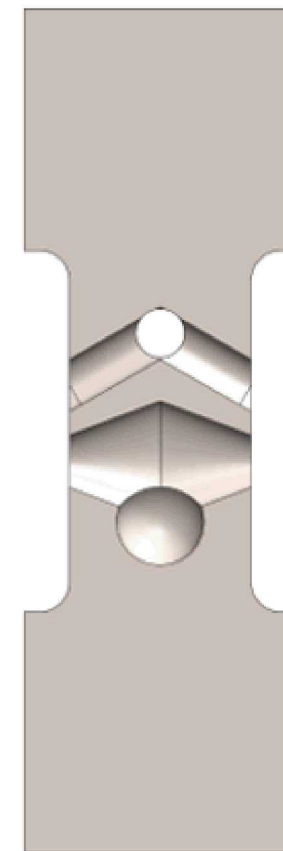
Quasi-static loading
Stainless steel

SFC2 - 2015



Quasi-static and dynamic loading
Higher Loading Rates

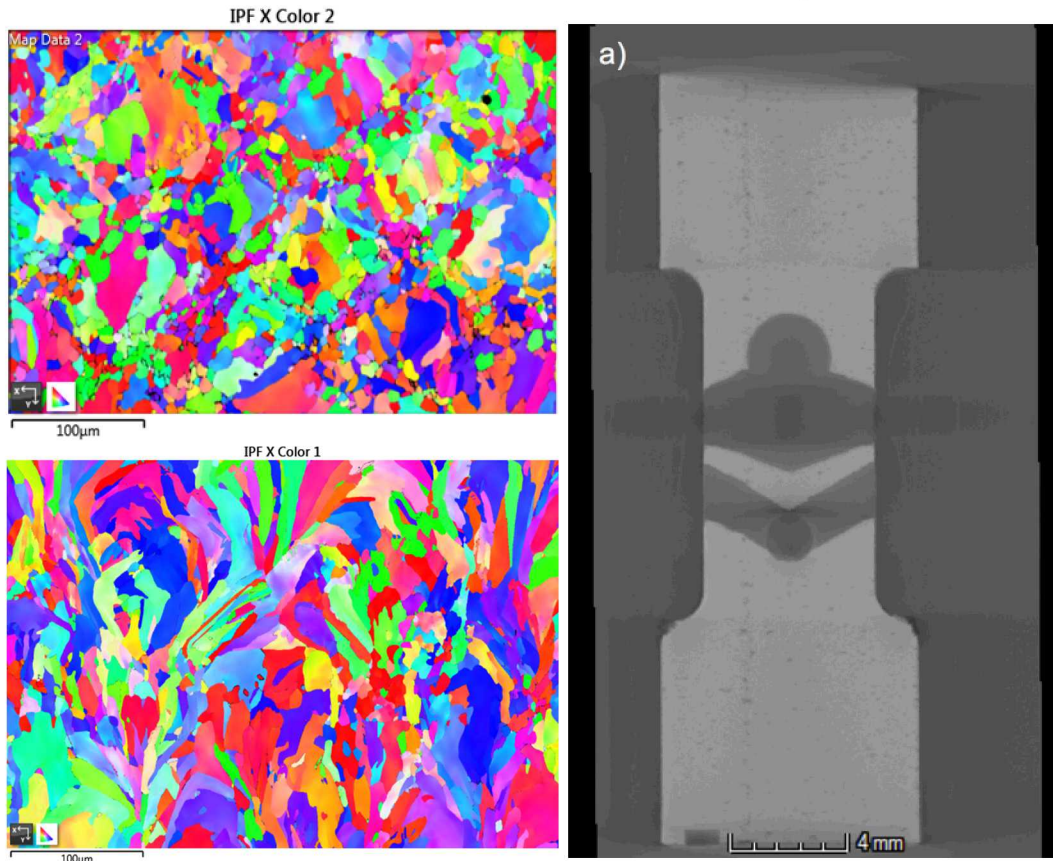
SFC3 - 2017



Complex inner geometry
AM component

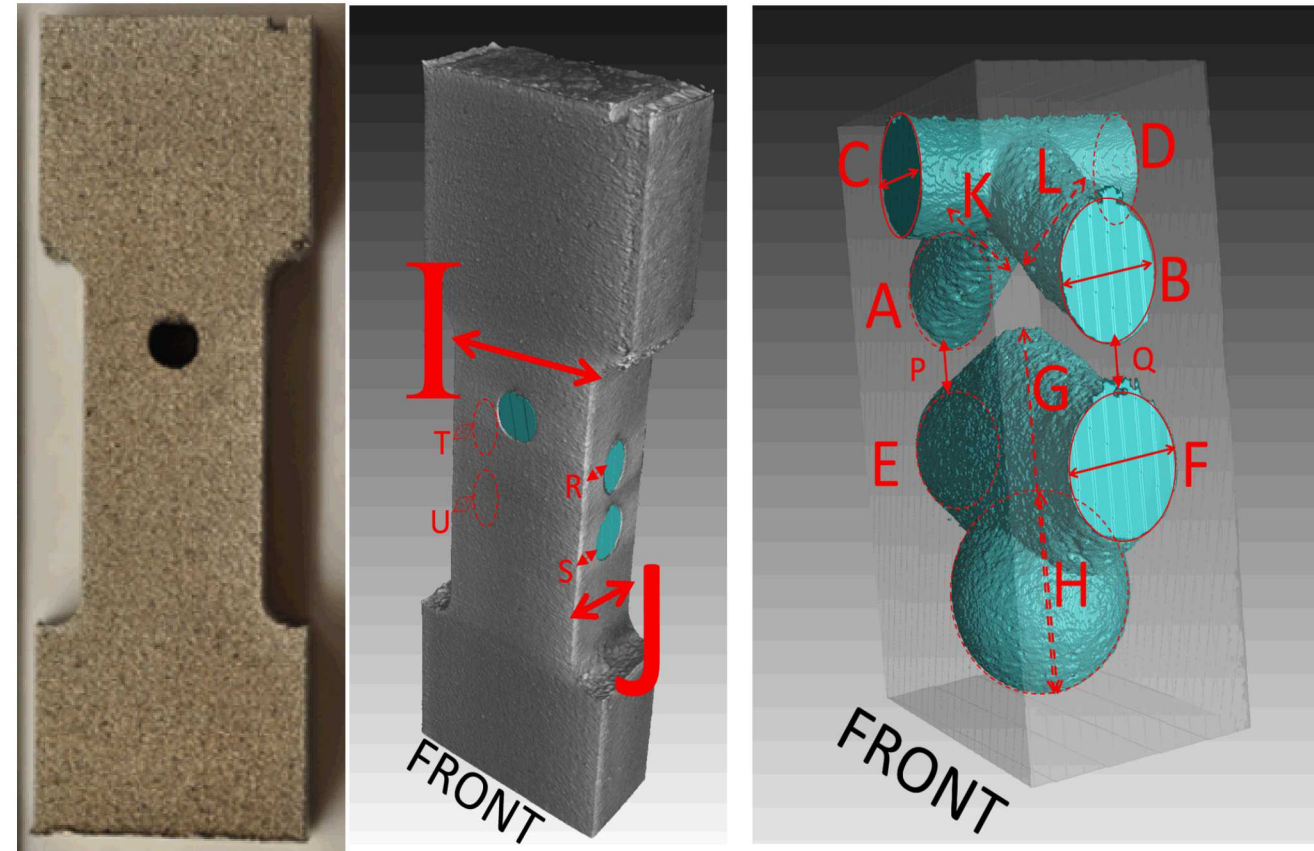
Modeling fracture for AM components is challenging

AM Material Variability



- Property variability
- Residual stresses
- Inhomogeneous
- Porosity and defect inclusion

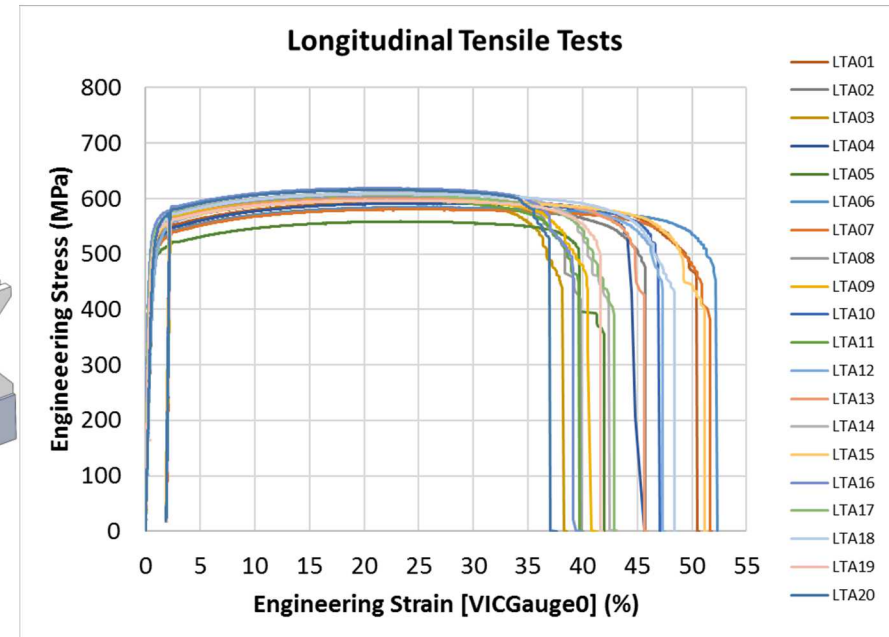
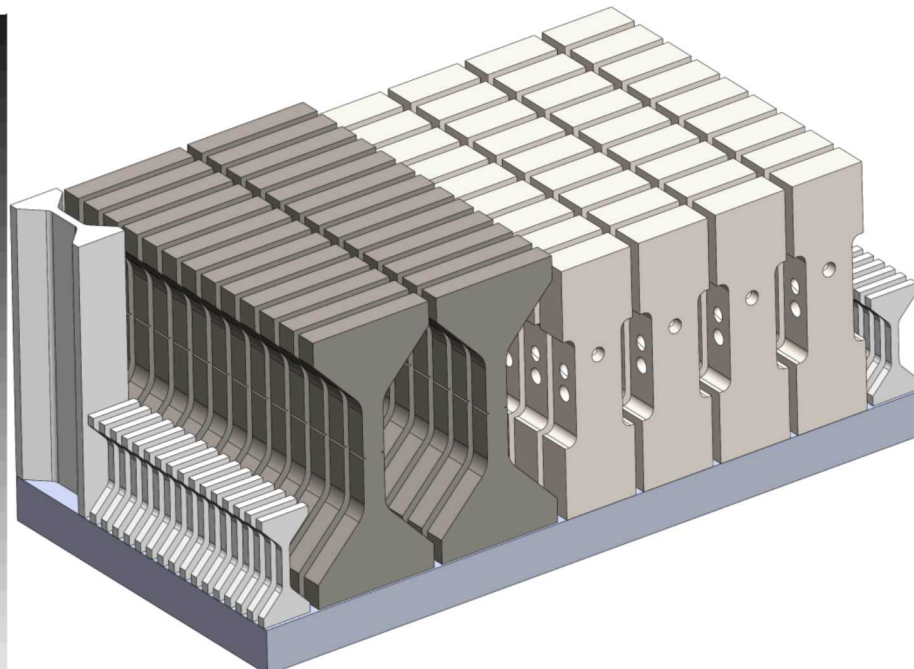
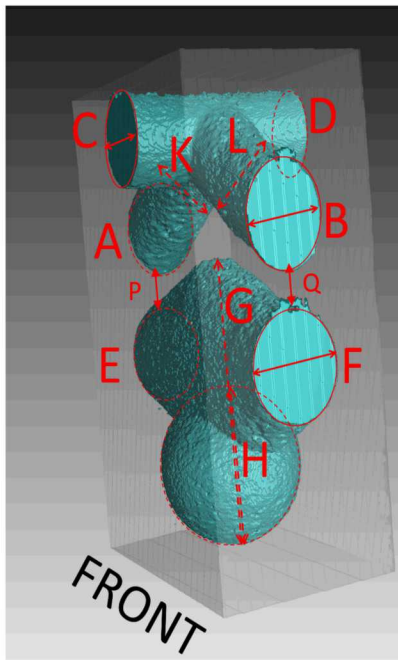
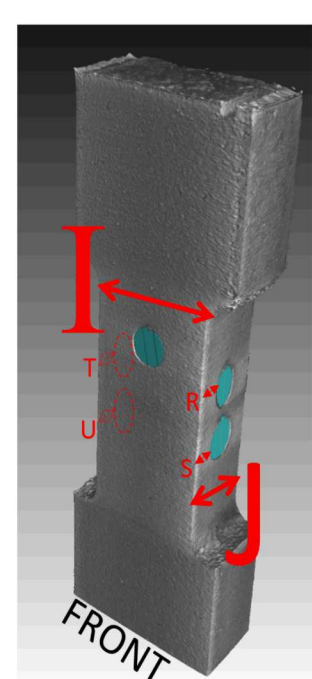
AM Component Geometry



- Complex Geometry
- Non machinable
- Geometric variability
- Surface finish

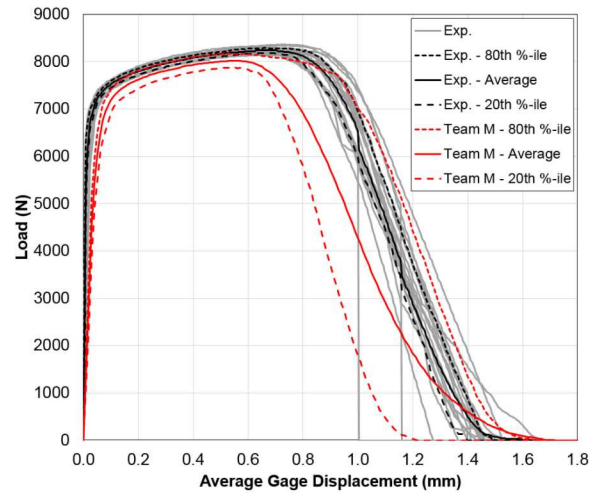
What was provided for the fracture challenge

- Detailed **geometric data** on specimen dimensions
- CT scan images for longitudinal, notched, and challenge coupons.
- **Porosity** distribution.
- Post-test fracture shape images for longitudinal, transverse, and notched coupons.
- Post-test SEM images of **fracture surface** for longitudinal and notched coupons.
- **Force vs gage displacement** for longitudinal, transverse, and notched coupons.

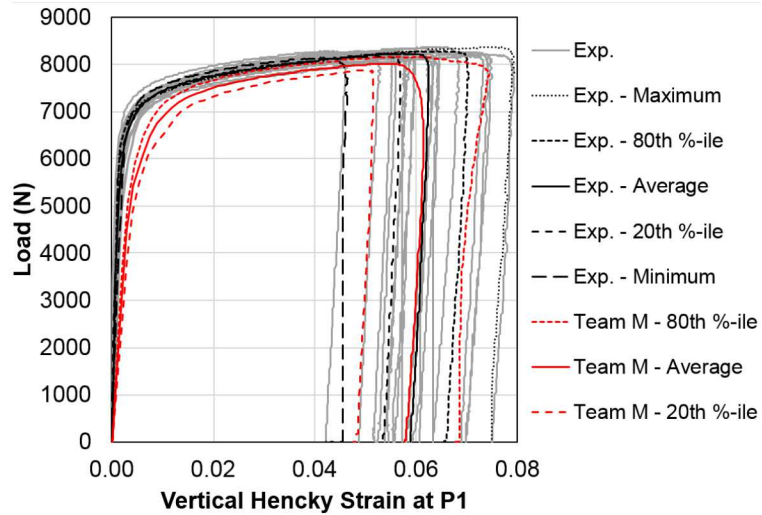


Questions asked to evaluate quality of predictions

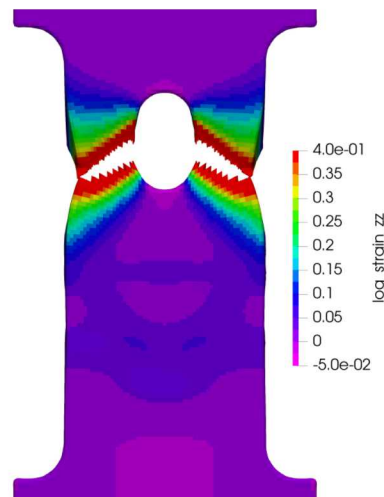
Load vs Displacement



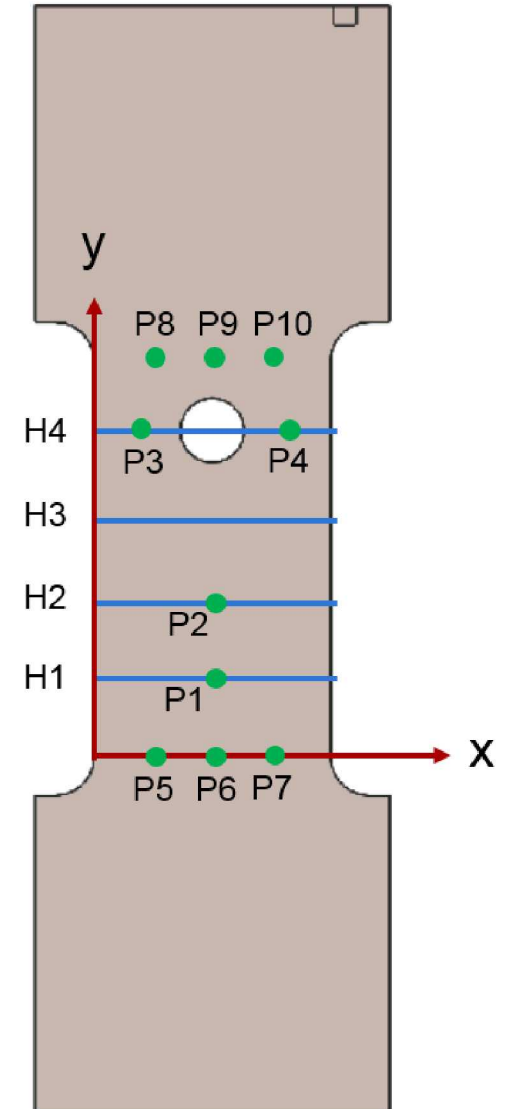
Load vs Strain



Fracture Path

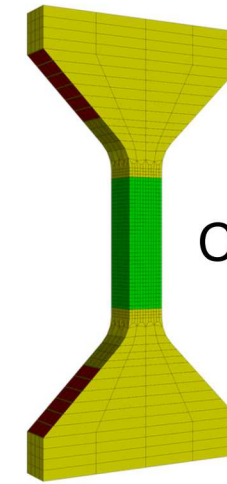


Local metrics



Modeling fracture of the challenge problem using a nonlinear, rate- and temperature- dependent continuum model

Hardening behavior: $\sigma = \sigma_y + A\epsilon_p^n$

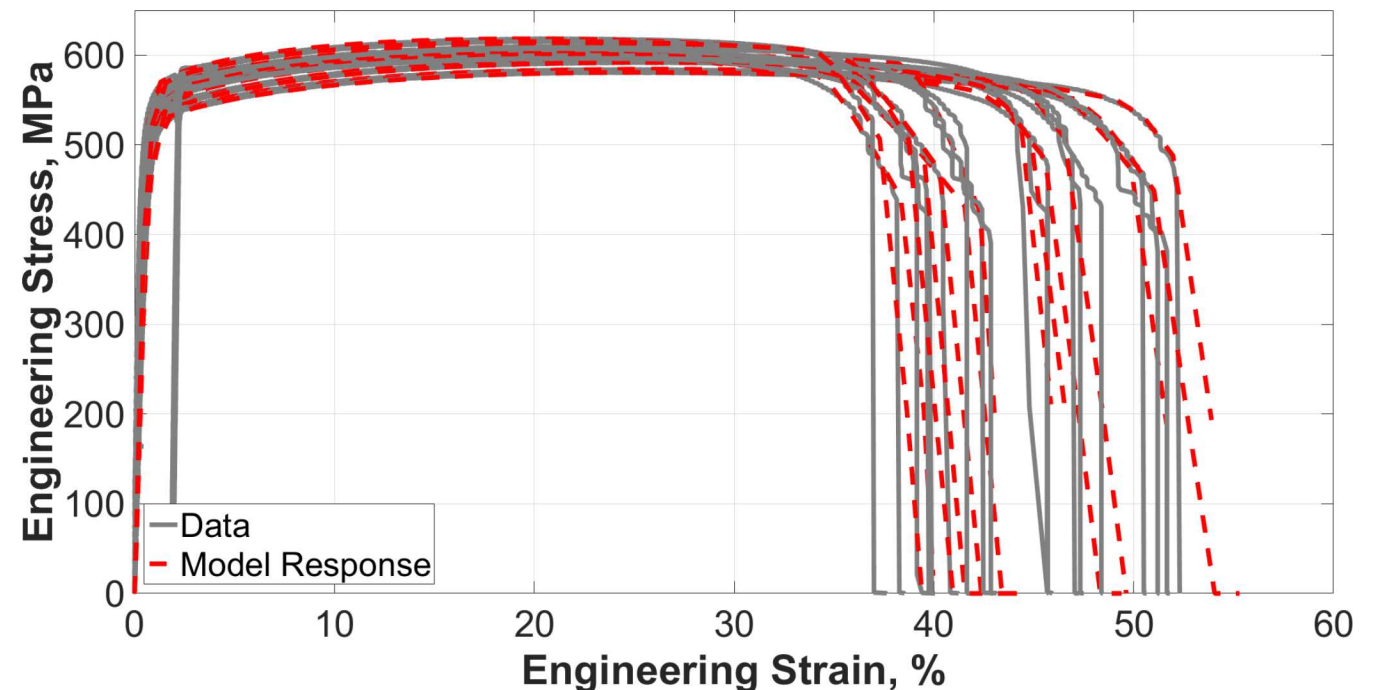


Coupon A Mesh

Parameters Determined through Calibration:

Parameter	Upper	Lower	Mean	Std. Dev.
A (MPa)	666.0	578.3	633.9	21.0
n	0.80	0.66	0.76	0.03
σ_y (MPa)	533.9	495.7	512.5	12.4
E (GPa)	189.0	83.9	129.5	26.2
f_d	0.90	0.55	0.80	0.12
f_ϵ	0.75	0.38	0.54	0.12
f_t	140.0	80.0	102.6	17.4

Coupon A Longitudinal Tensile Test Data and Model Results

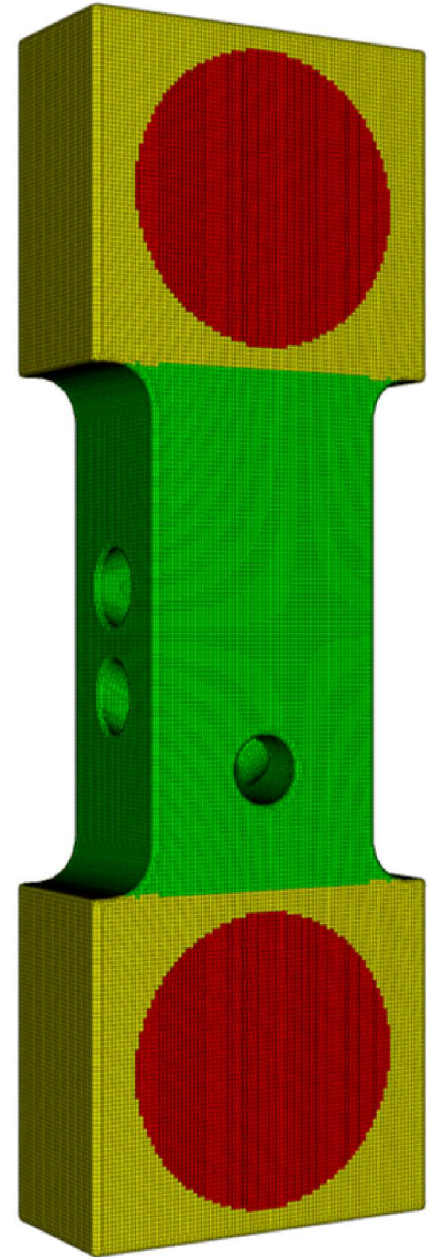
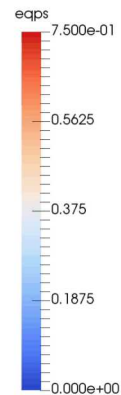


7

Modeling approach for challenge coupon

- Implicit
- Thermally-coupled
- Transient dynamic model for challenge geometry.

Time: 0.0 Seconds



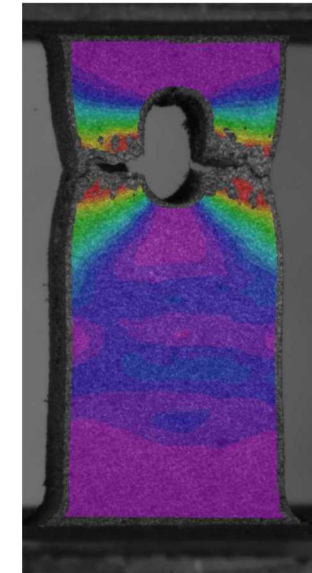
Challenge Experimental Results

- 19 sets of experiments
- Load displacement curves
- Digital Image Correlation (DIC) strain gauges
- Line samples at force levels
- DIC at crack initiation and failure

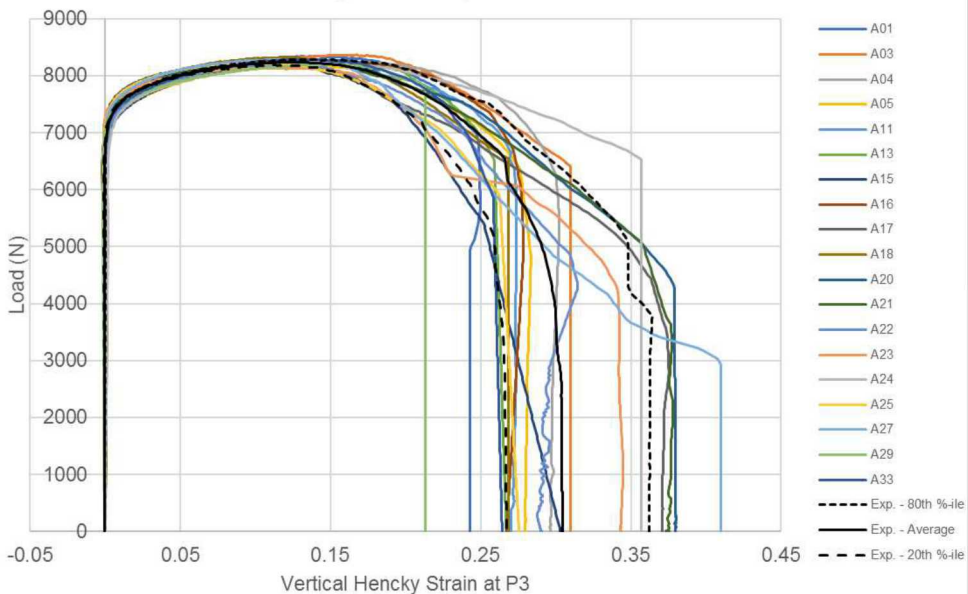
Crack Initiation



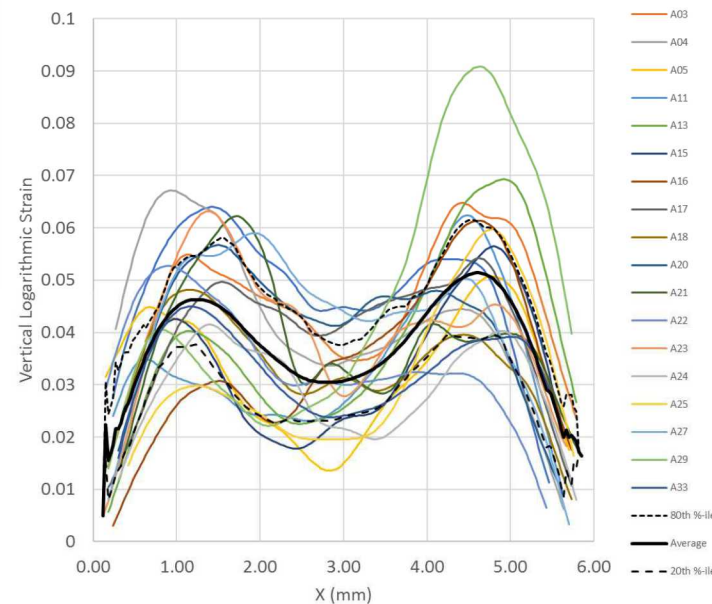
Failure



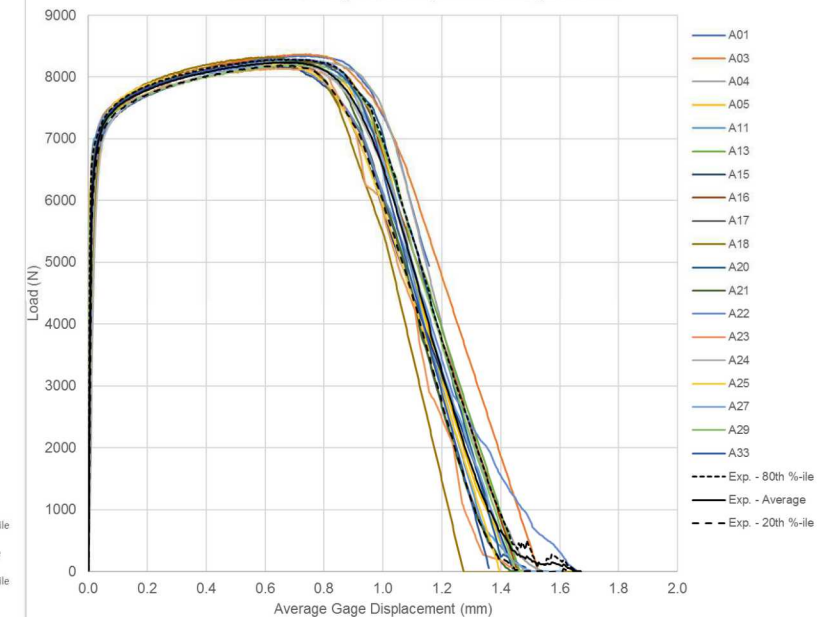
SFC3 Challenge Geometry Load vs. Vertical Strain at P3



H2 at F4

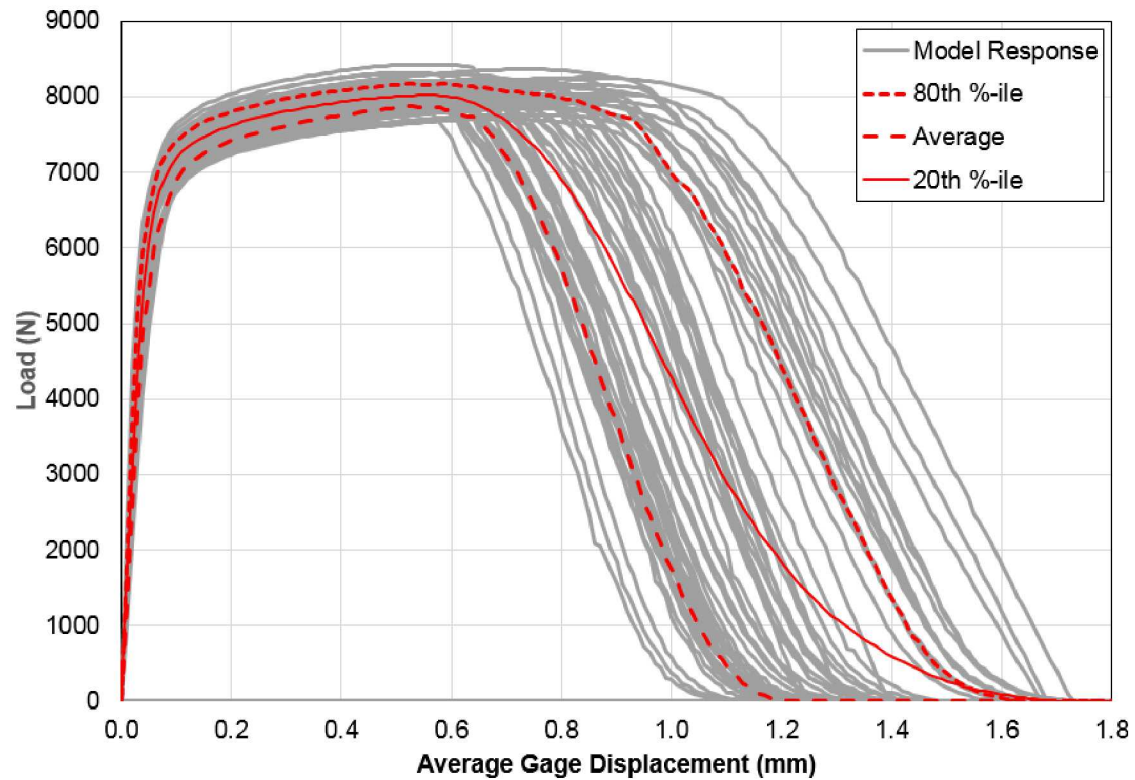


SFC3 Challenge Geometry Load vs. Displacement

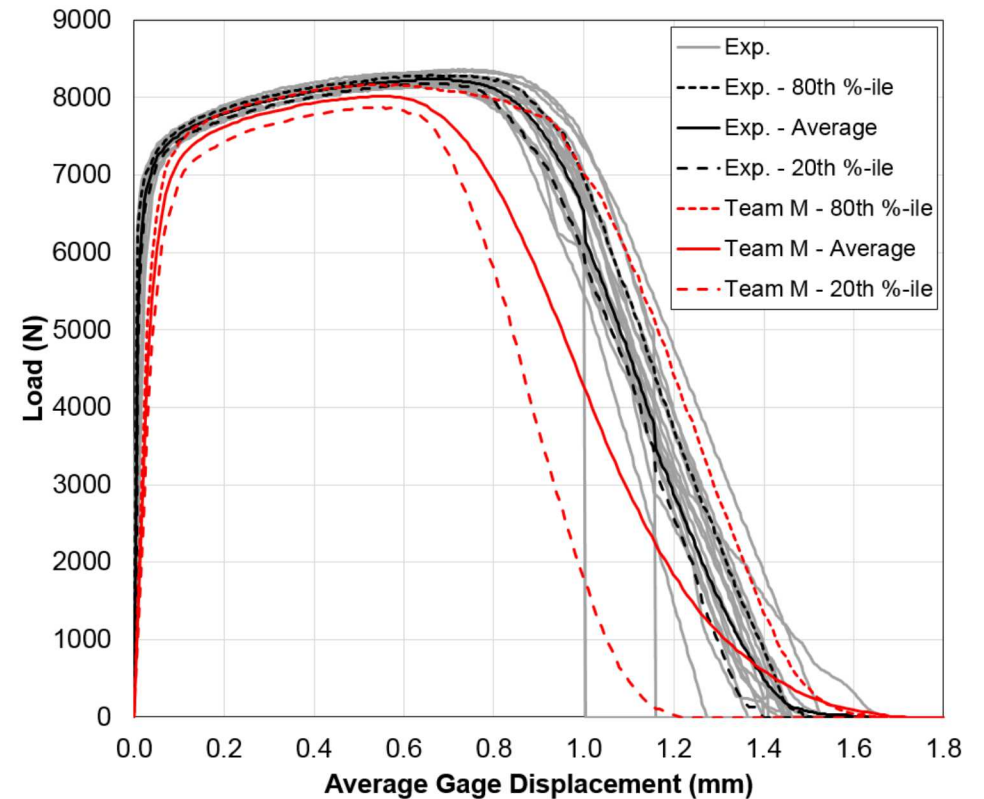


Comparison with blind prediction: Applied load vs. gauge displacement

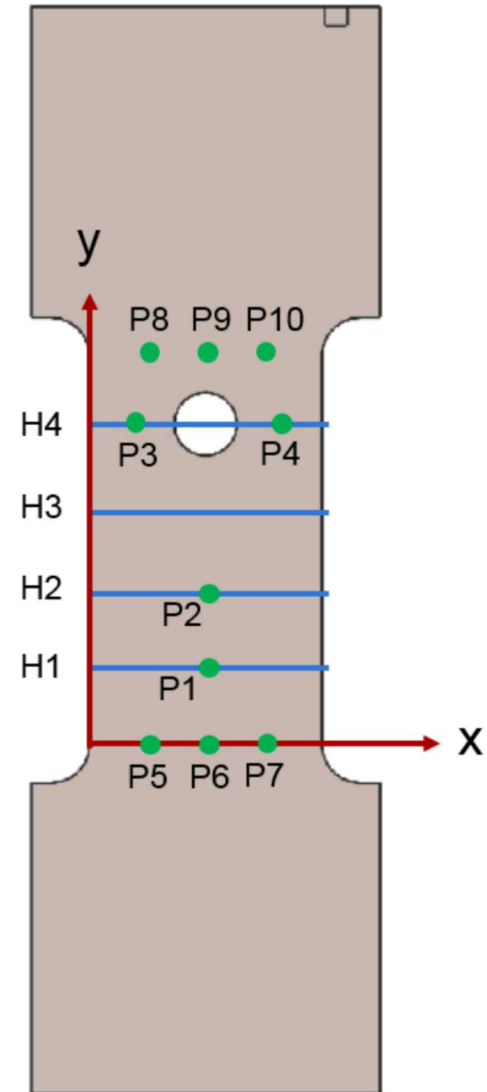
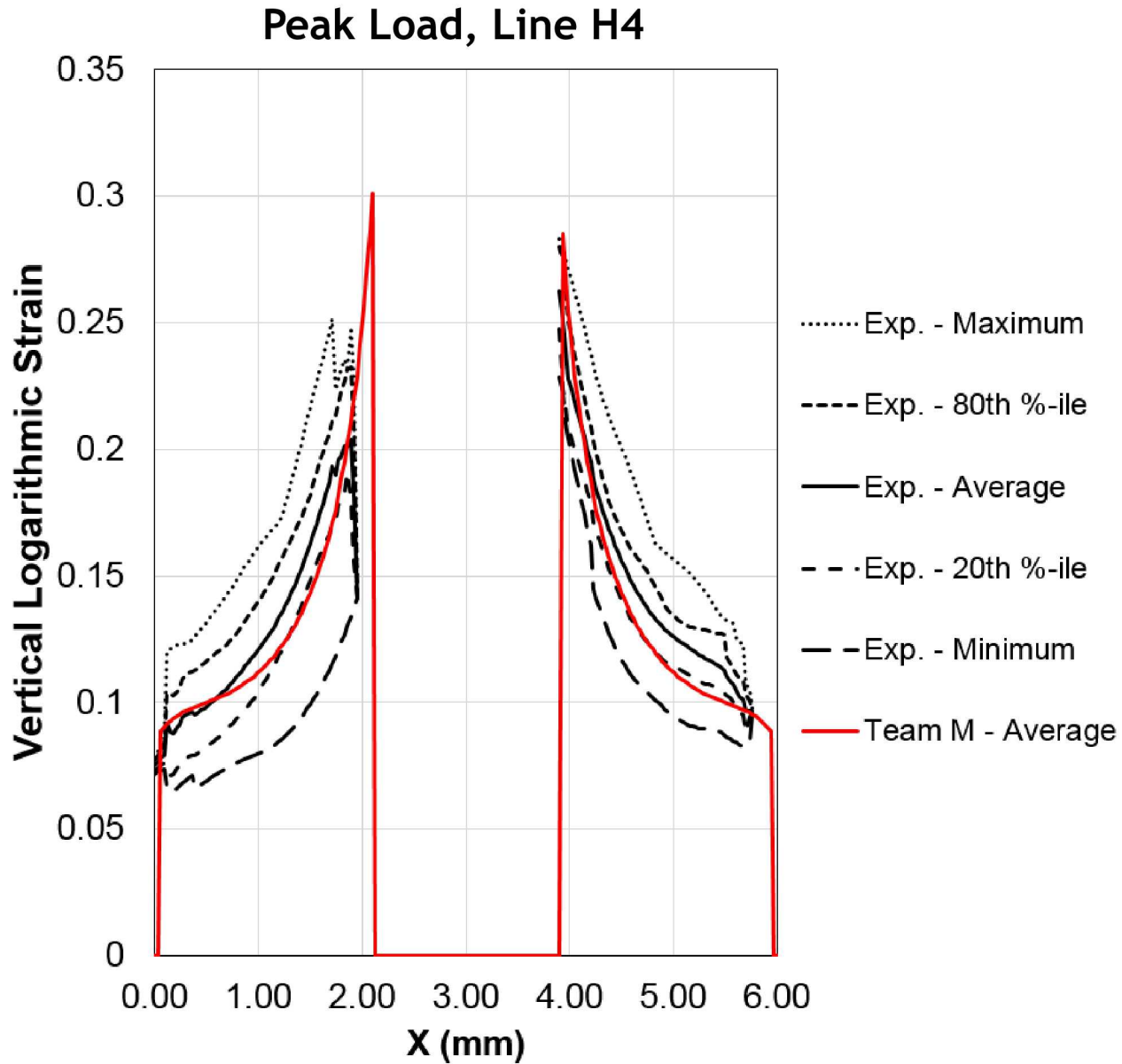
Challenge Coupon Blind Prediction Model Results



Challenge Coupon Experimental and Model Results

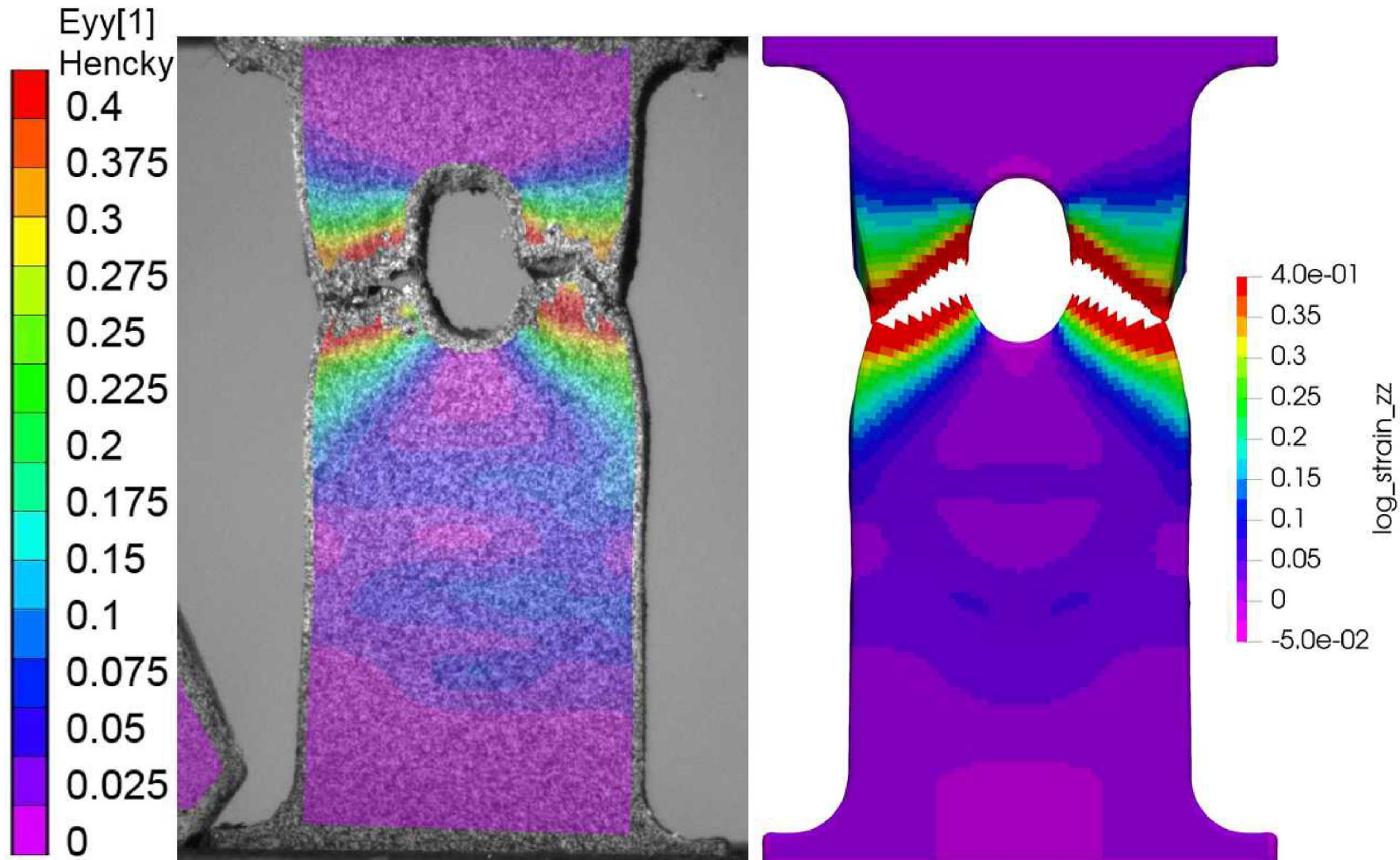


Comparison with blind prediction: Load concentration



Comparison with blind prediction: Local strain field and fracture profile

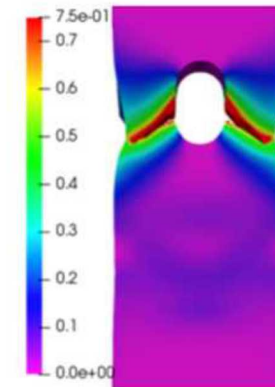
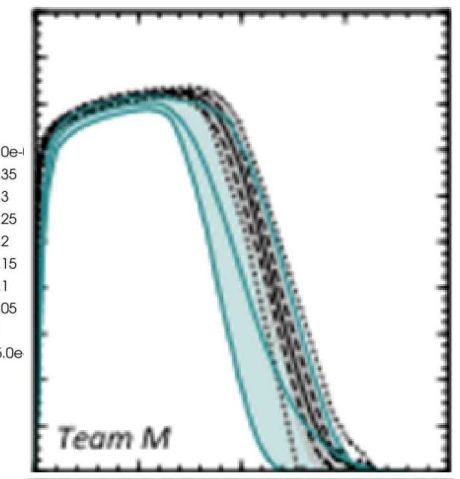
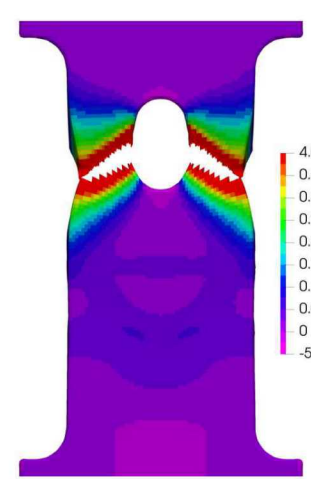
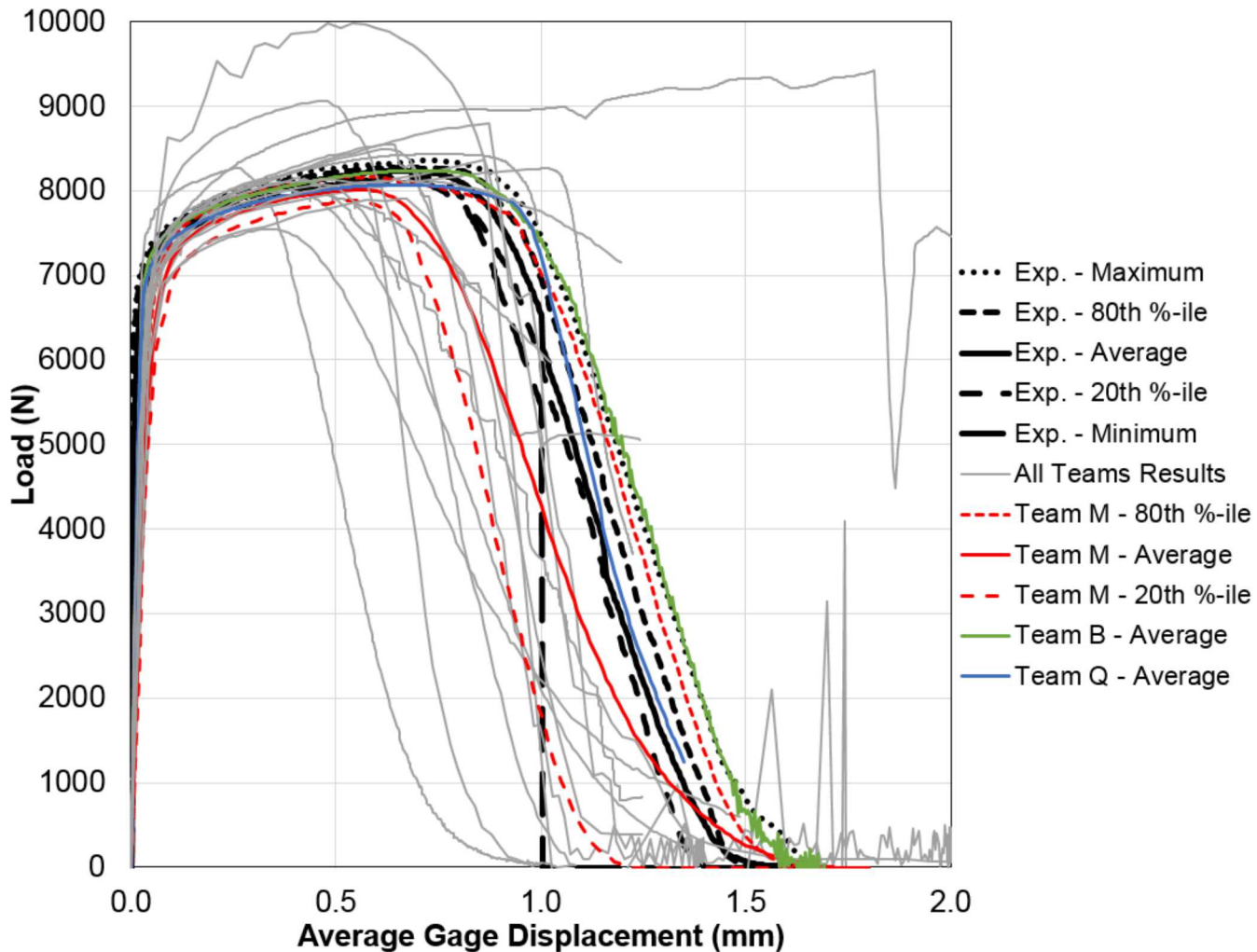
Challenge Coupon Surface Strain Profile at Coupon Failure



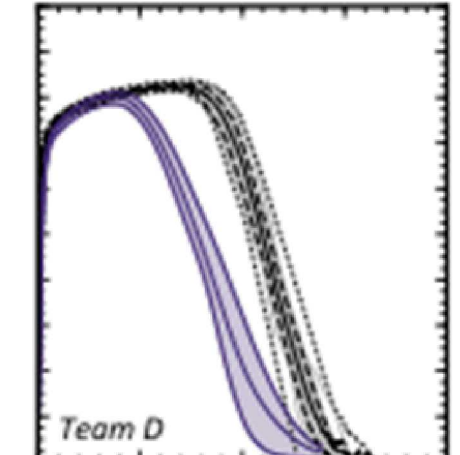
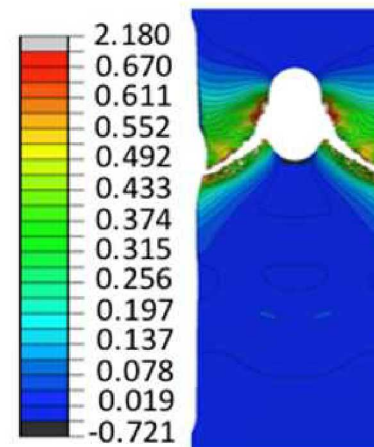
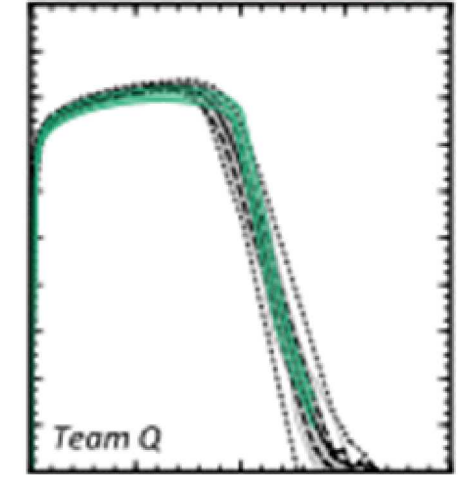
Comparison with the modeling community

21 teams participating.

Load vs Displacement, All Teams



Team Q



Possible sources of **discrepancy between prediction and results**:

- Size effects.
- Surface finish.
- Variability of material properties.

Where are we in terms of modeling fracture?

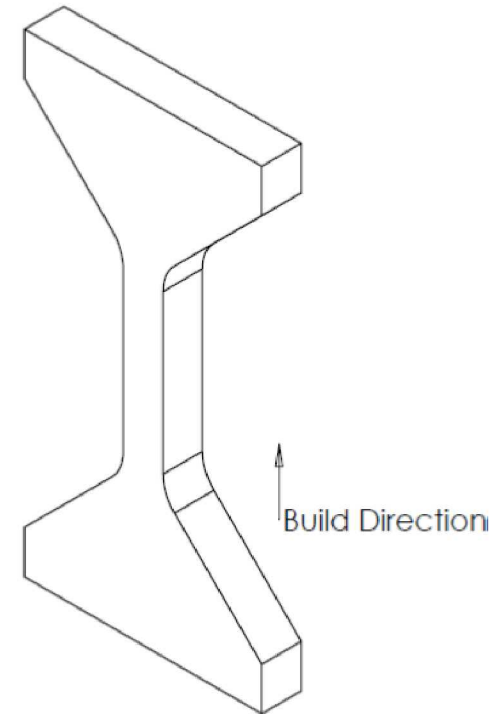
- Challenge did not capture coupling between material variability (AM processes) and complexity of geometry (AM components).
- Response of coupon insensitive to some of the characteristics of AM components.
- Some of the teams that did well used simple approaches.





Parameters Determined Through Calibration:

A	Power Law Coefficient	} Step 1
n	Power Law Exponent	
σ_y	Initial Material Yield Stress	
E	Young's Modulus	
f_d	Failure Decay	} Step 2
f_ϵ	Fracture Toughness	
f_t	Failure Strain in Uniaxial Tension	



Coupon A

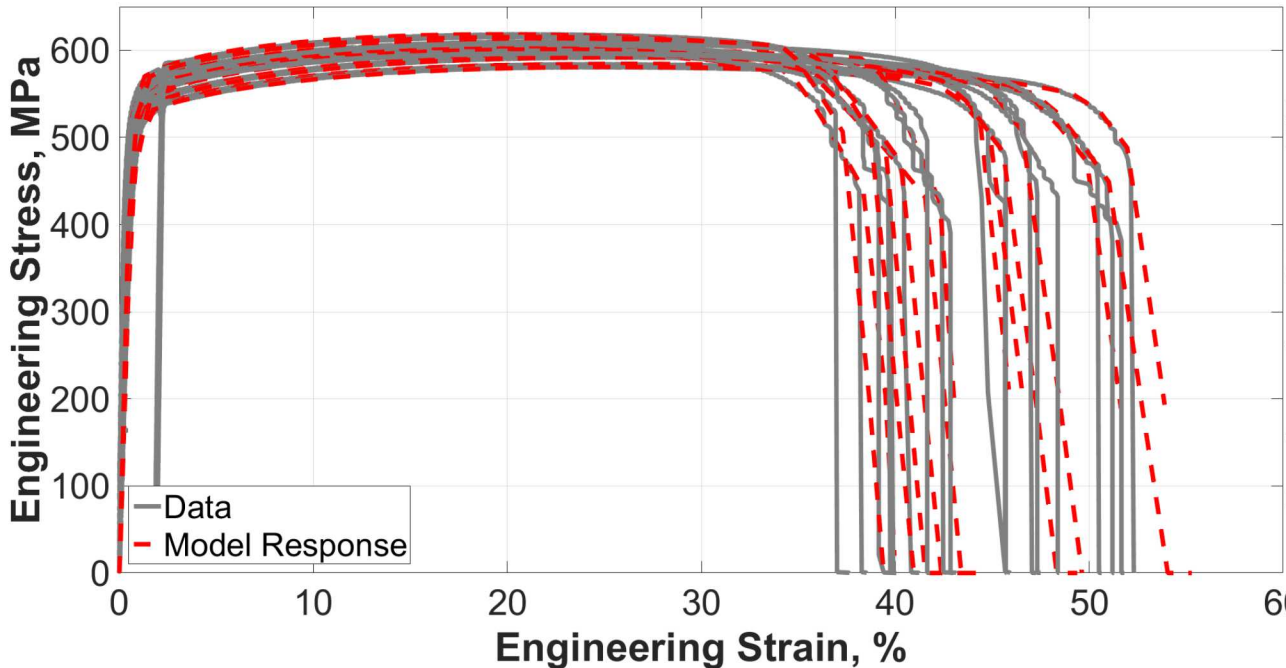
Calibration Process:

- **Step 1:** A, n, σ_y , and E values determined for each of the longitudinal tensile tests (Coupon A), failure disabled in model.
- **Step 2:** f_d , f_ϵ , and f_t determined based on failure response, using values found through Step 1.

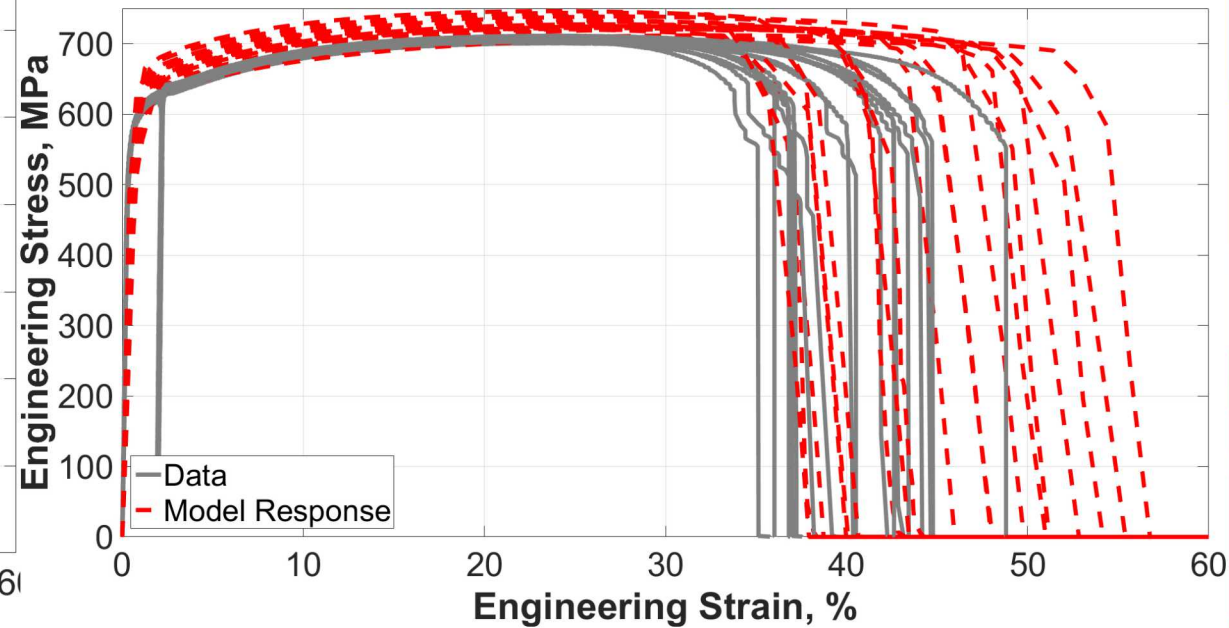
Transverse coupon A data was used to determine scaling parameters for the shape of the Hill yield surface.

- Model was reevaluated for the transverse build direction using the previously determined parameters.

Coupon A Longitudinal Test Data and Model Results



Coupon A Transverse Test Data and Model Results



Coupon B used for comparative purposes.

- Similar size to challenge geometry
- Not used during parameter determination, model evaluated at previously determined parameters from Coupon A.

Coupon B (Notched) Test Data and Model Results

