



Numerical and Experimental Analysis of Sheared Fractures Flows

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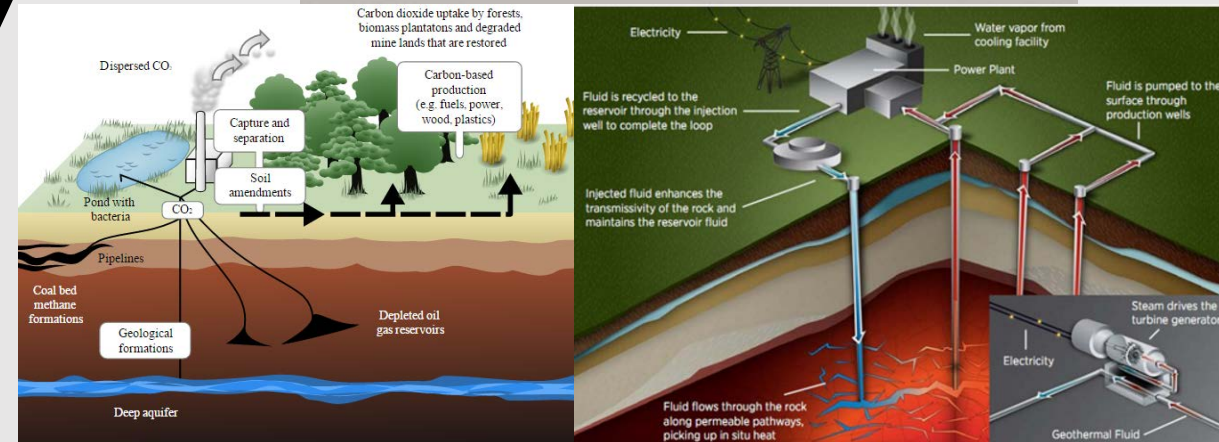
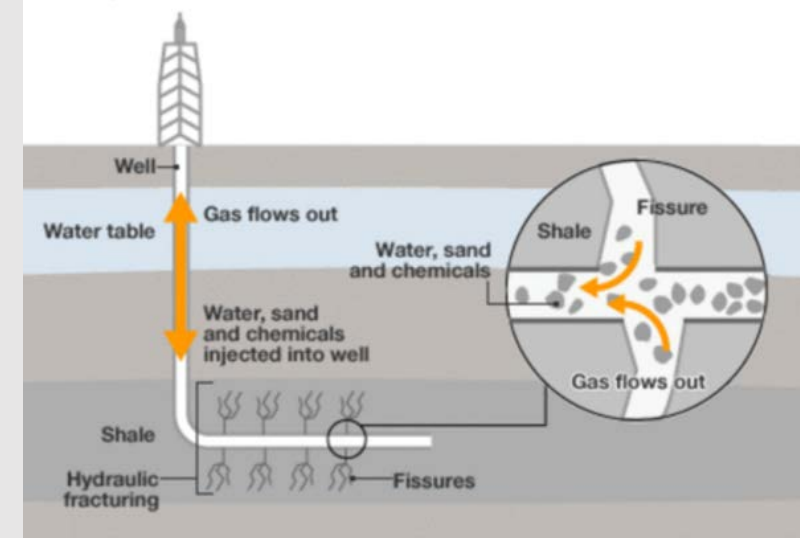


Outline

- Introduction
 - Fractures
 - Shearing
- Experimental Tests Rock Fractures at NETL in Morgantown
 - Preparing samples
 - Mechanical shearing
 - Computed tomography (CT) scan
 - Permeability measurement
- Numerical Simulations
 - Local Cubic Law (LCL) method and full Navier-Stokes simulations
 - Generating the geometry
 - Gridding
- Conclusions

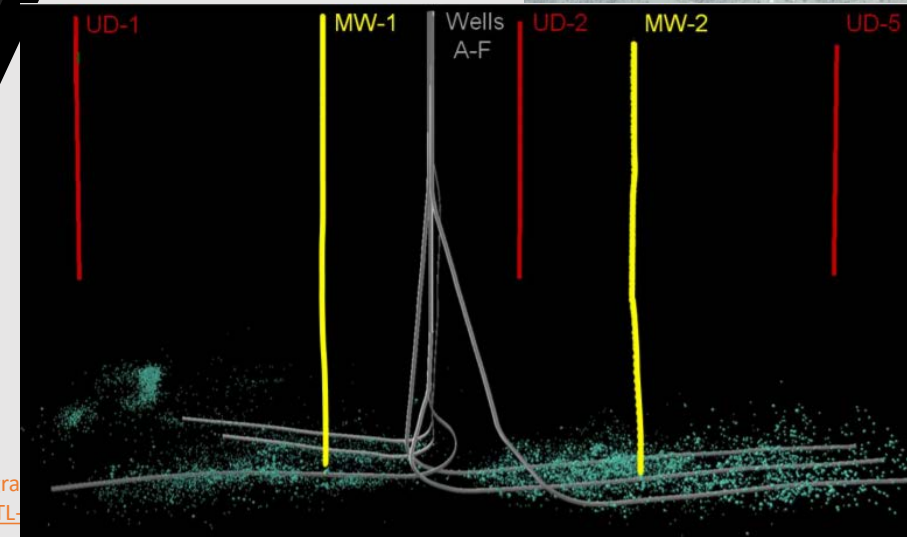
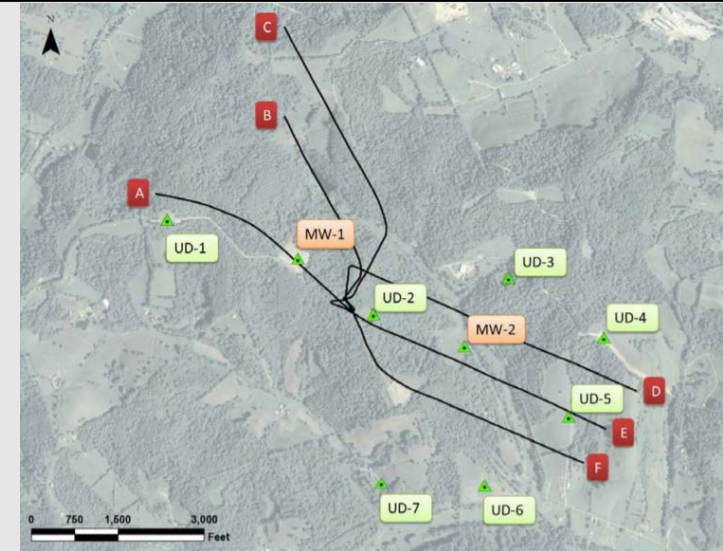
- Fractures are conduits in subsurface rocks
- Unconventional oil and gas resources
- Carbon sequestration reservoir
- Enhanced geothermal system

Shale gas extraction

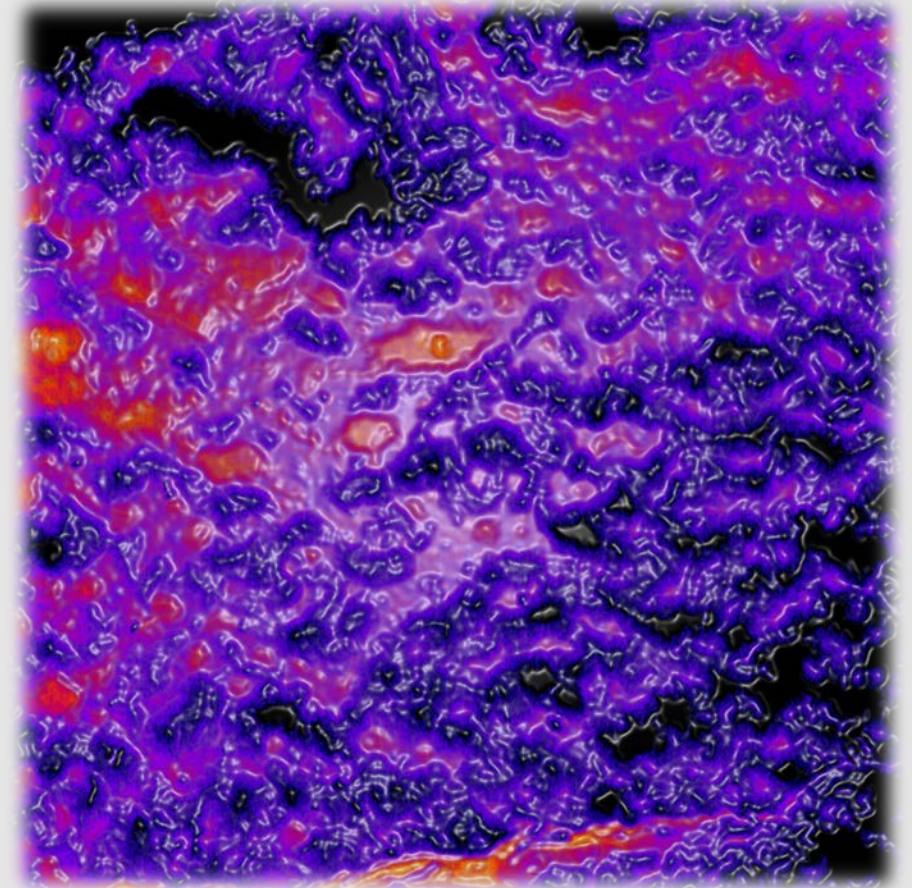


- Shearing is associated with micro-seismic events
 - Human Activities
 - Hydraulic fracturing
 - Enhance oil recovery
 - Geothermal operation
 - CO₂ Sequestration
 - Geometry changes

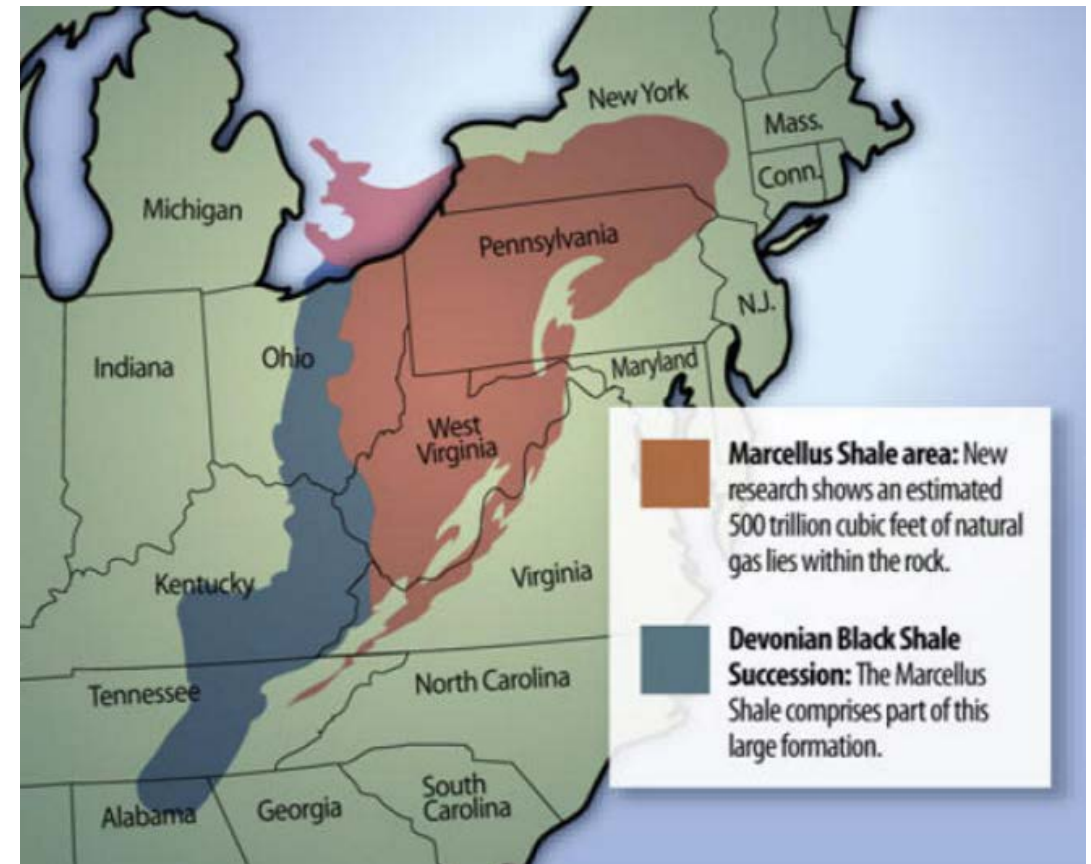
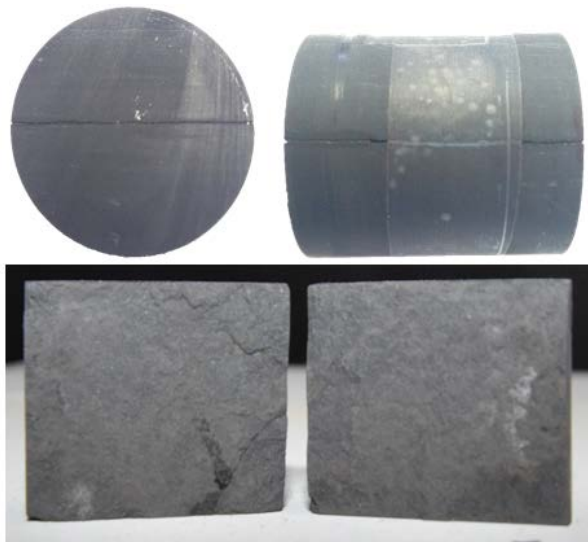
- Evolution of fracture hydraulic properties



Experimental Section

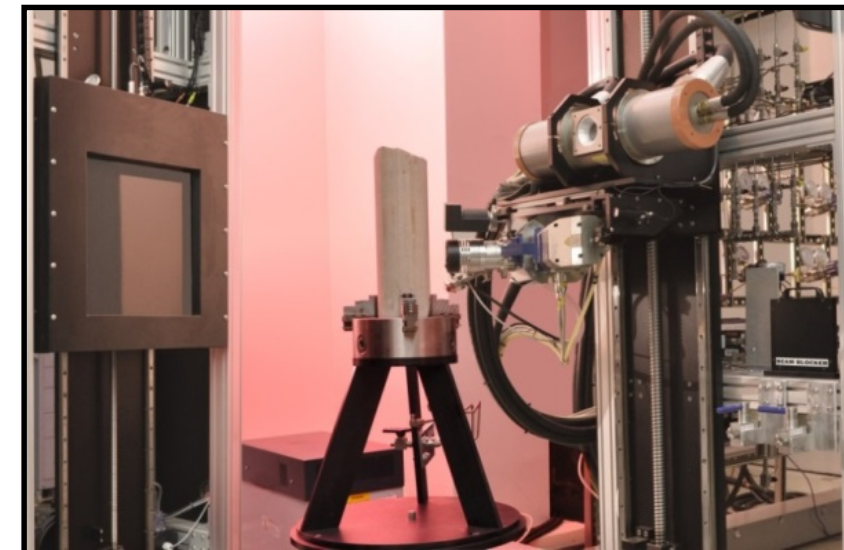
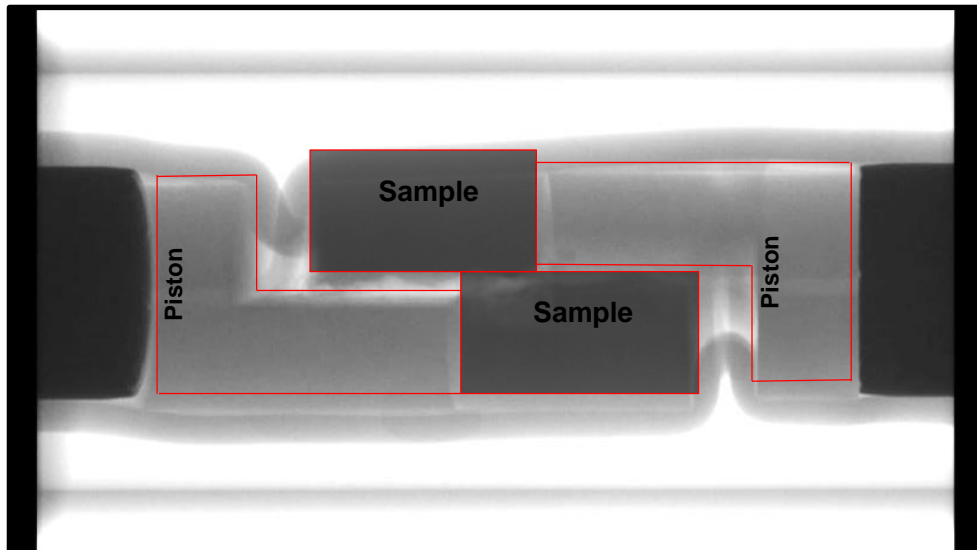
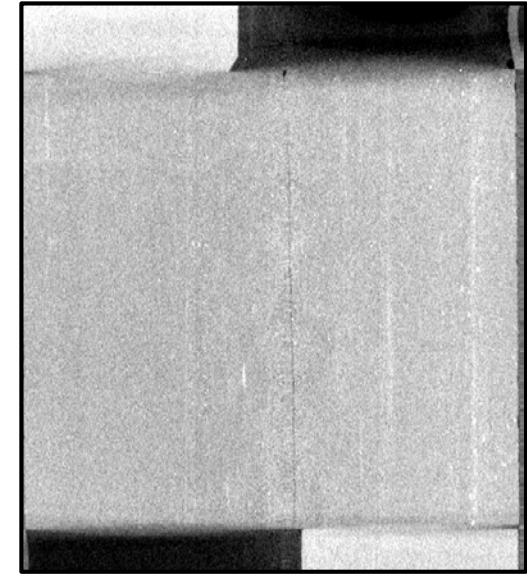


- Sample
 - Marcellus shale
 - Giant unconventional resource of natural gas
 - 3.8 (cm) diameter, 3.8 (cm) length
 - No natural fractures
 - Mechanically fractured

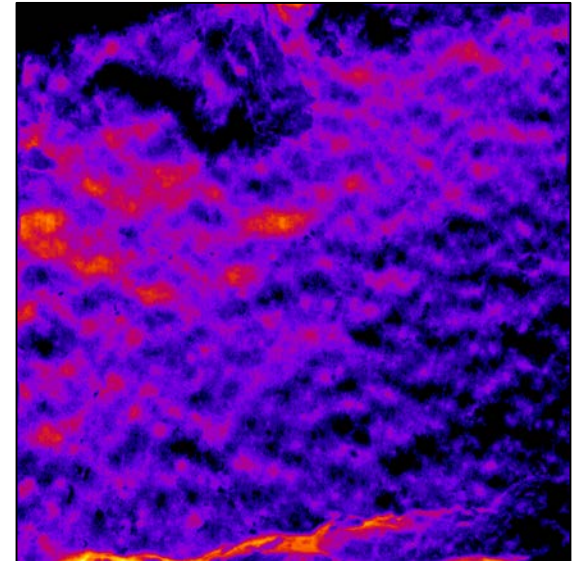
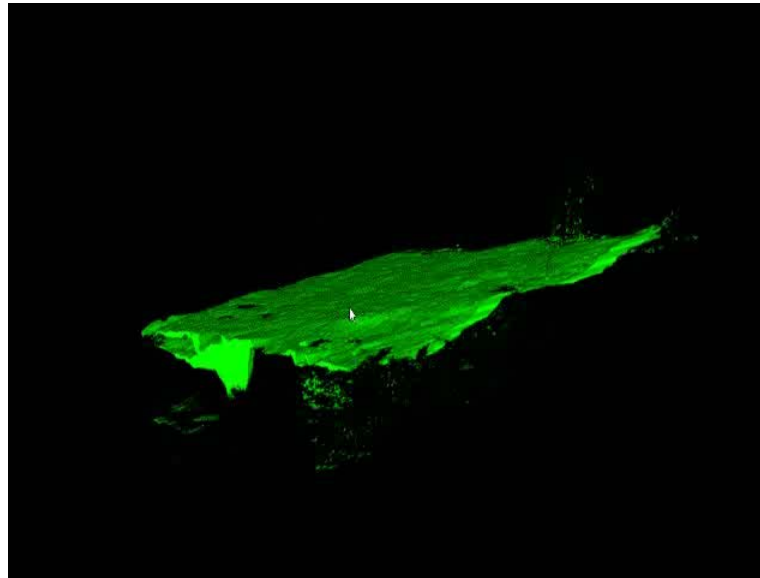
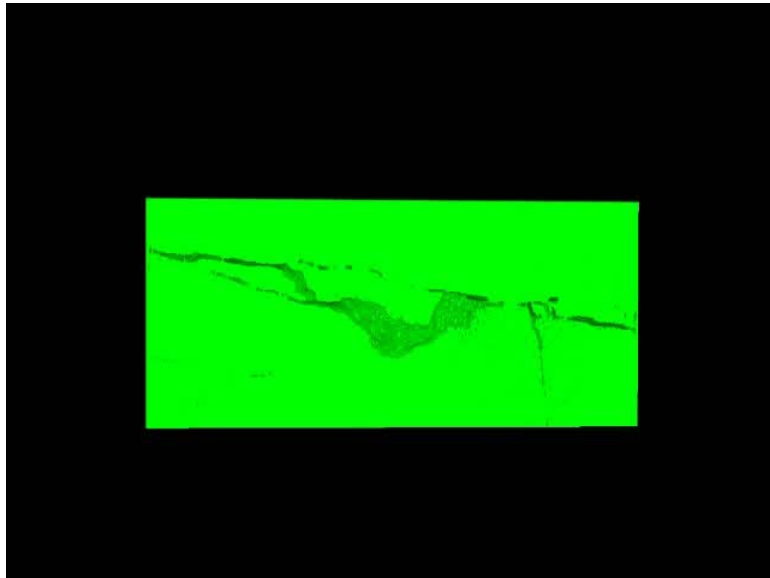
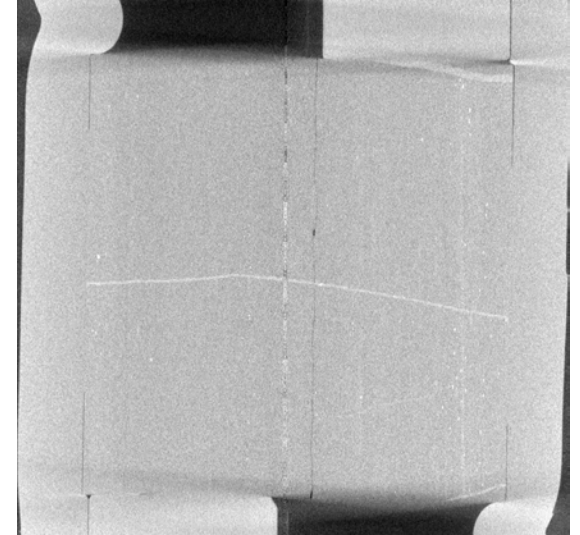


- Modified pistons within a Hassler core holder to shear fractured rocks in discrete steps
 - Total displacement of 4 cycles: 3.2 mm

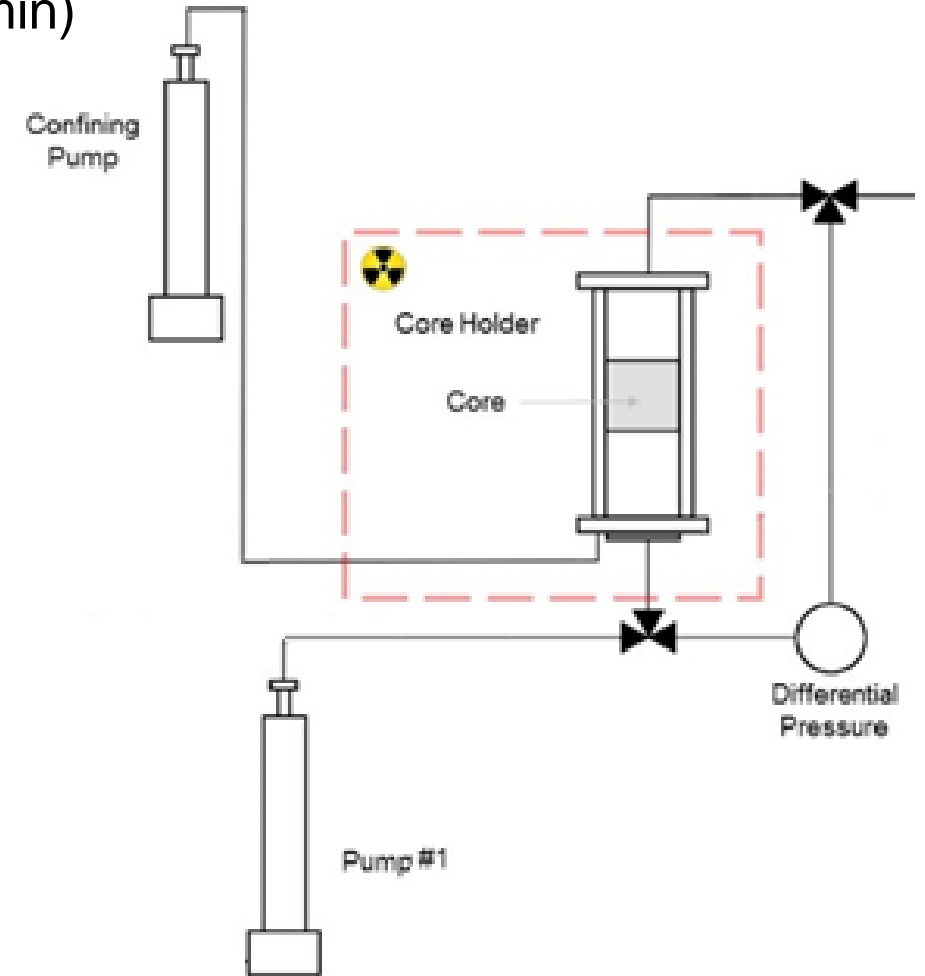
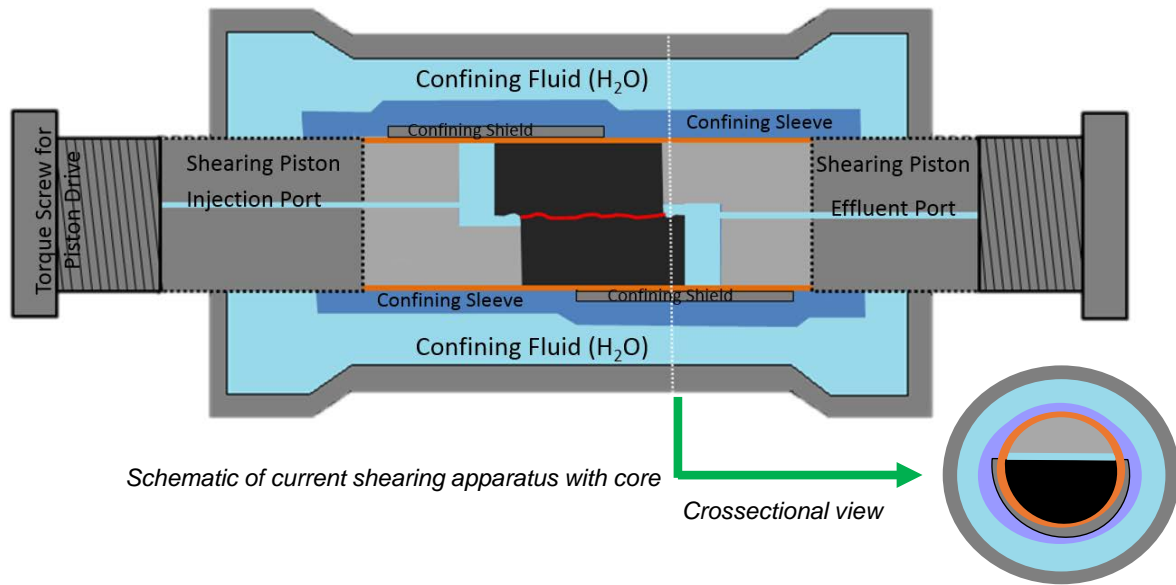
- Industrial computed tomography (CT) scanning with $26.8 \mu\text{m}^3$ resolution
 - Obtain the geometry of the fracture



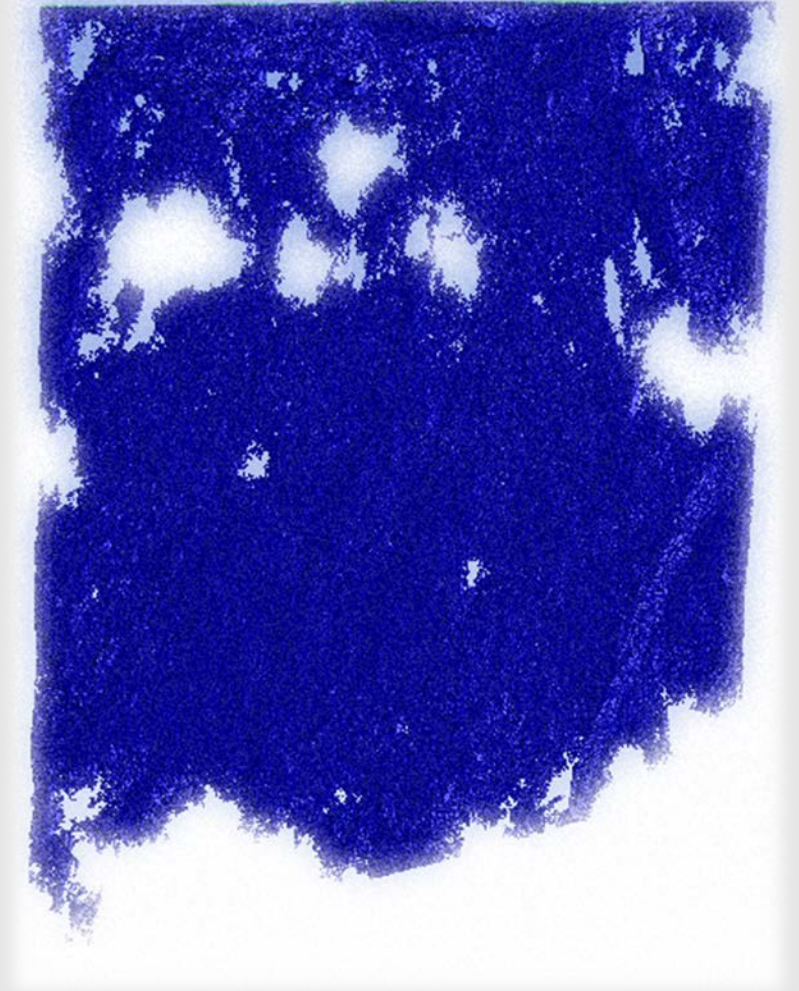
- CT scanning relies on capturing a large number of 2D x-ray
- Bulk matrix of rock was generated
- Fracture geometry was isolated via imageJ



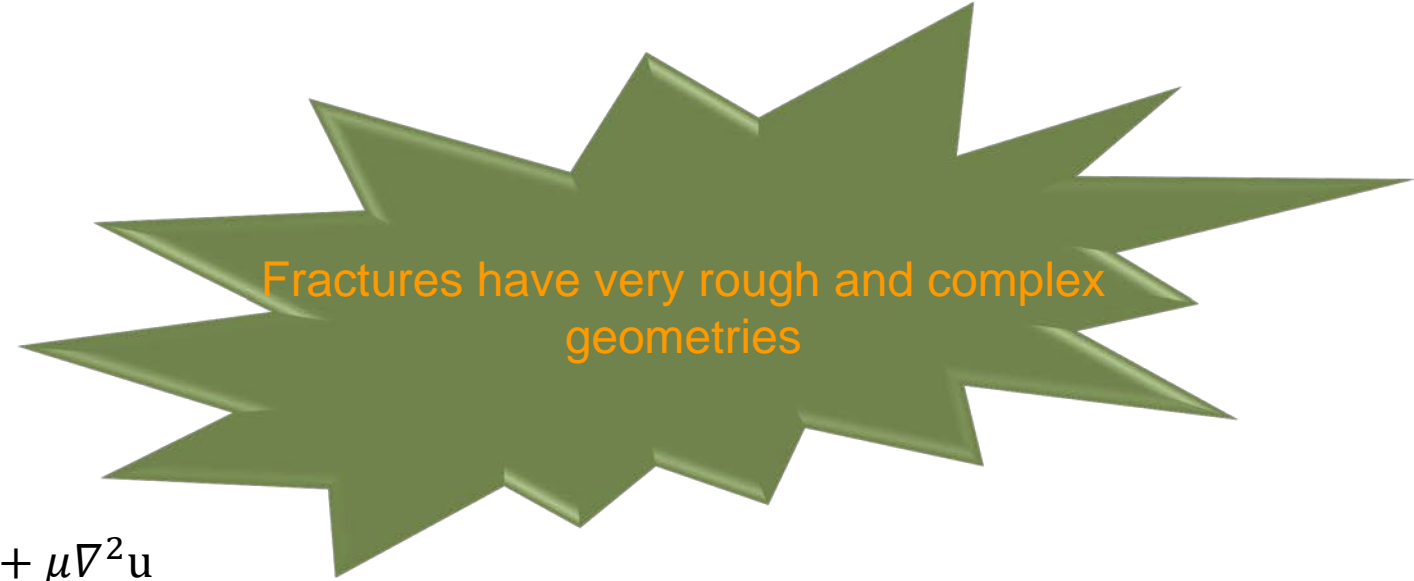
- Water fluid was injected with different flow rates (0-10 mL/min)
- Pressure drops were measured (0-2 MPa)




Numerical Section



- Cubic Law
 - Set of parallel plates
 - Obey the Cubic Law $\Delta p = \frac{12 \mu L}{Wh_{eq}^3} Q$
- LCL Model
 - Laminar creeping flow
 - Driven by a pressure gradient



Navier-Stokes Equation  $0 = -\nabla P + \mu \nabla^2 u$

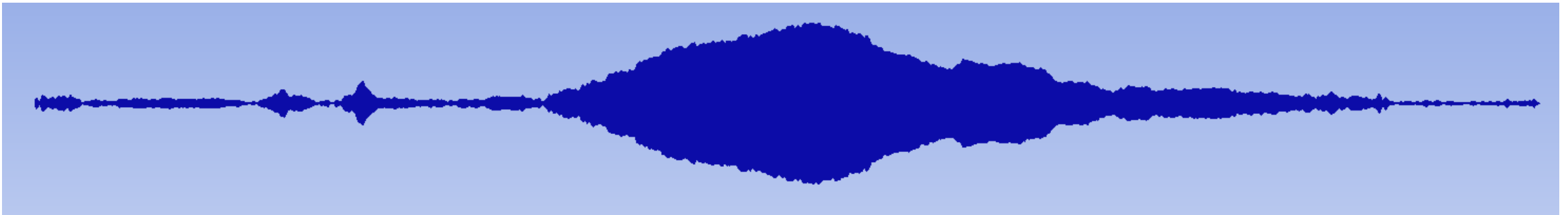
$$0 = -T_{x_{i,j}}(P_{i+1,j} - P_{i,j}) + T_{x_{i-1,j}}(P_{i,j} - P_{i-1,j}) - T_{z_{i,j}}(P_{i,j+1} - P_{i,j}) + T_{z_{i,j-1}}(P_{i,j} - P_{i,j-1})$$

$$T_x = \frac{h^3 \Delta z}{12 \Delta x}$$

$$T_z = \frac{h^3 \Delta x}{12 \Delta z}$$

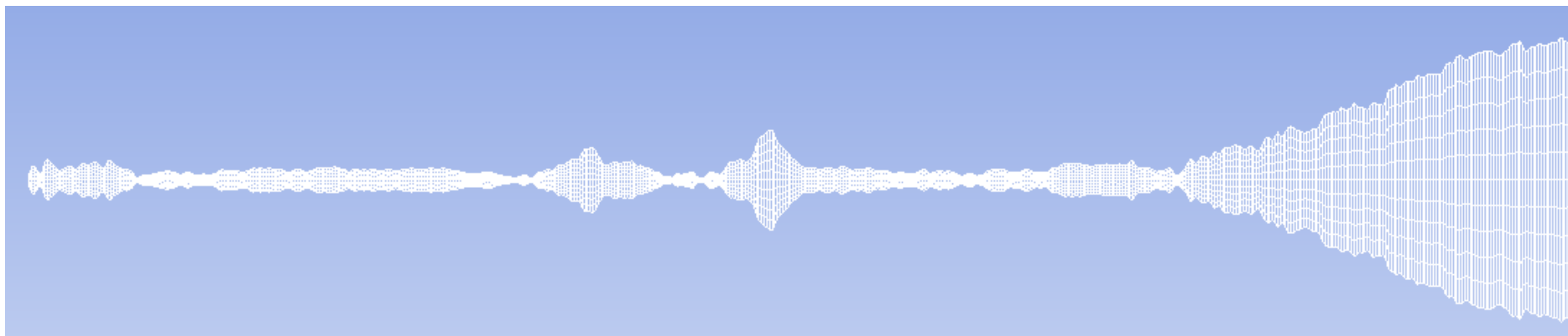
- ANSYS-Fluent Software
 - Solve Conservation of Mass and Momentum Equations

- Geometry
 - A 2D map of aperture values
 - No macroscopic undulation
 - The mid-surface is forced to be flat
 - Experimental shearing steps required the fracture to be planar
 - Reduced resolution map of fractures
 - 10x10 grids
 - The small scale features of the rough fracture
 - Need less computational time
 - Effect of scan resolution

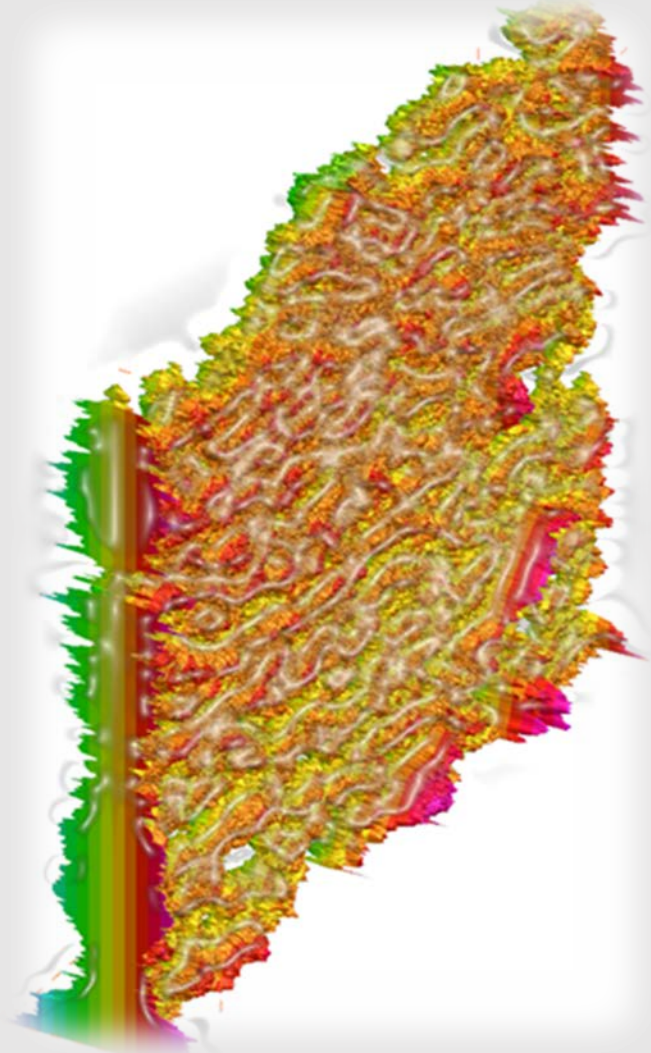


- Gridding (LCL and ANSYS-Fluent)
 - Each point of the aperture maps was transferred into a rectangular cell
 - No internal refinement for LCL
 - Internally refined for ANSYS-Fluent for accuracy and convergence

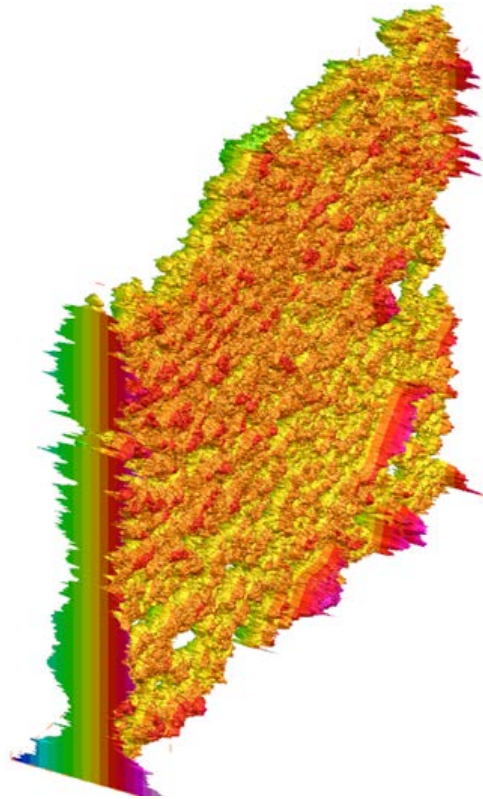
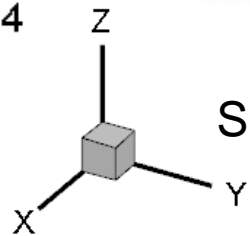
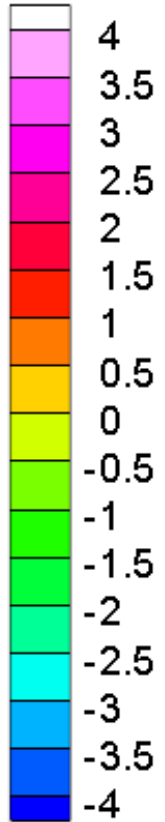
Case (N_x N_y N_z)	Number of elements	CPU time (min)	Obtained pressure drop (Pa)	Pressure drop difference %
(1 1 1)	13,690	0.23	134.45	-
(1 5 1)	68,450	0.50	372.10	176.76
(1 10 1)	136,900	1.08	394.85	6.11
(2 20 2)	1,095,200	12.45	399.40	1.63
(4 40 4)	8,761,600	240	402.90	0.88



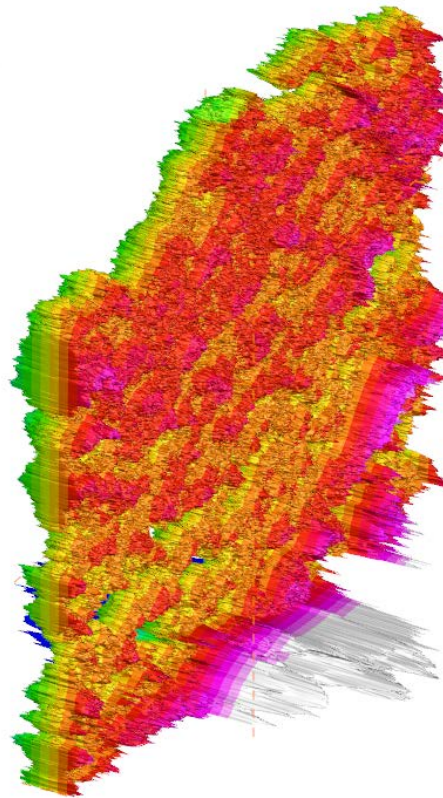
Results



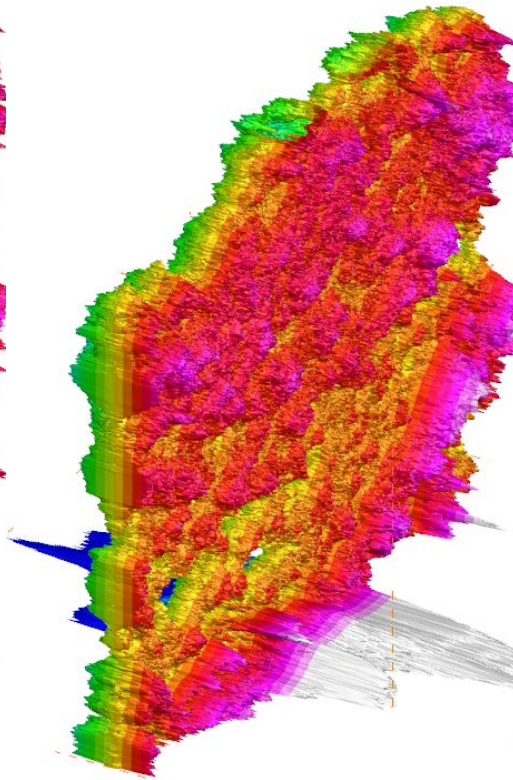
Height (mm)



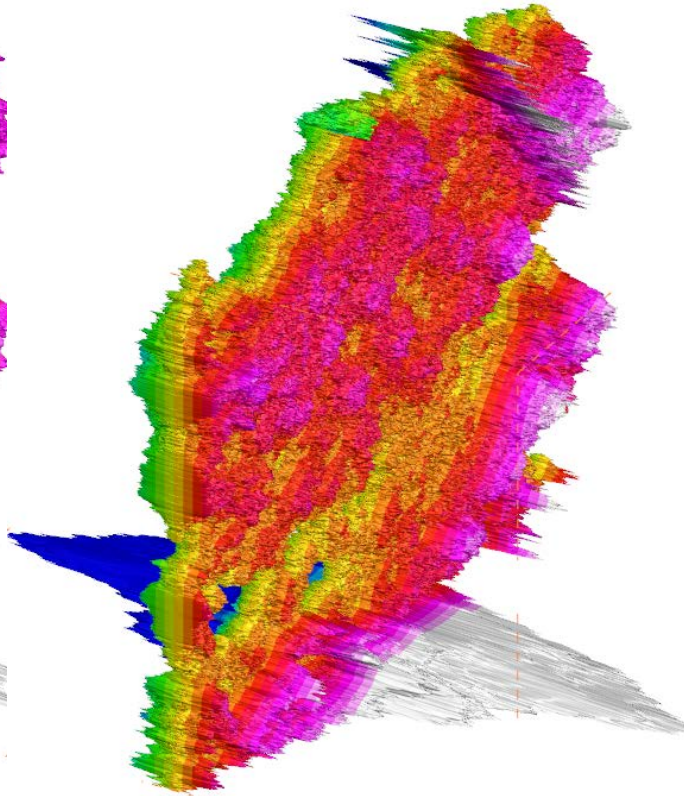
Shear Step 1



Shear Step 2



Shear Step 3



Shear Step 4

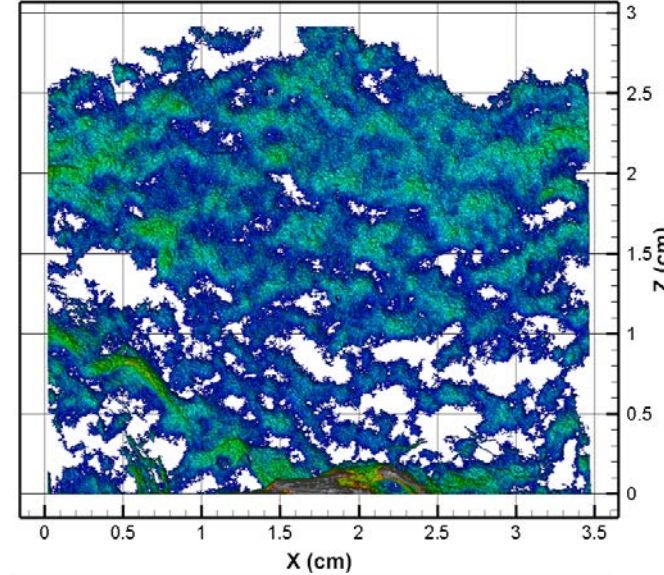
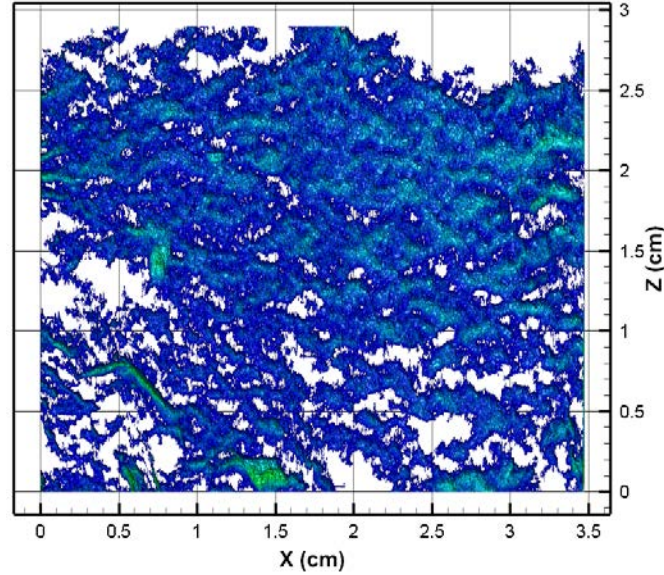
Aperture Maps

Height (mm)



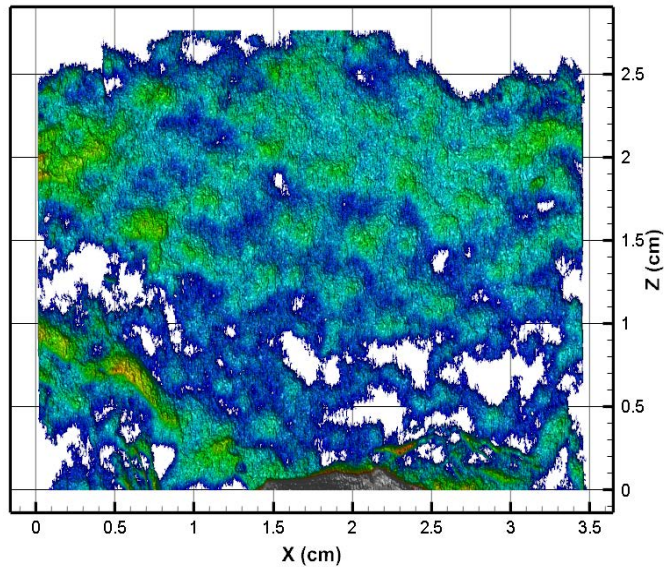
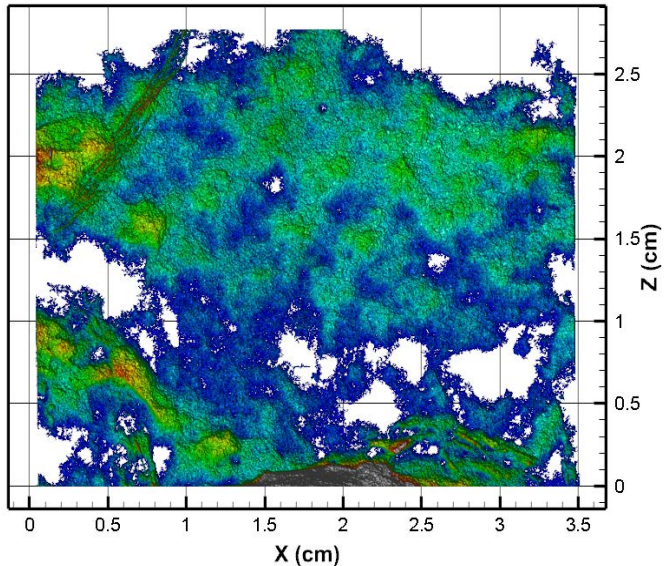
3.6
3.4
3.2
3.0
2.8
2.6
2.4
2.2
2.0
1.8
1.6
1.4
1.2
1.0
0.8
0.6
0.4
0.2

Shear Step 1



Shear Step 2

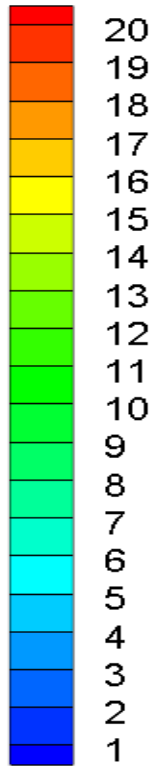
Shear Step 3



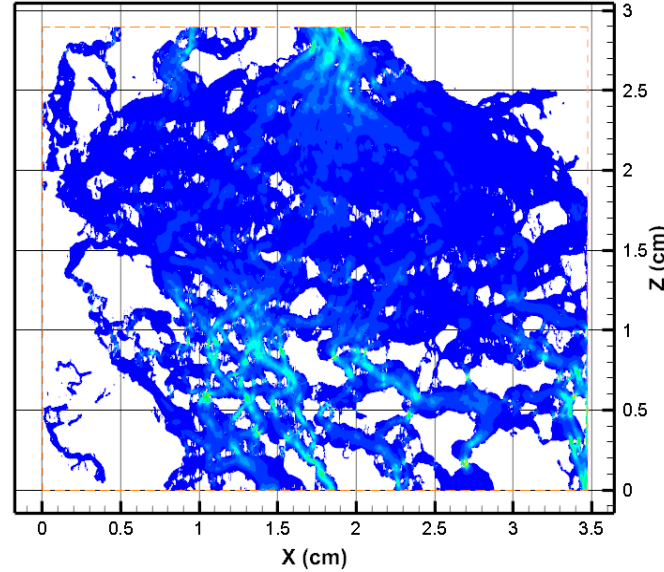
Shear Step 4

Velocity Contours

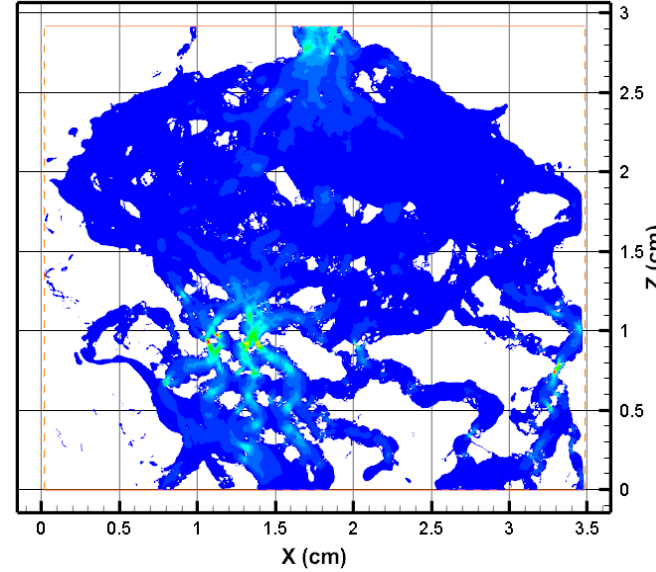
Velocity Magnitude (cm/s)



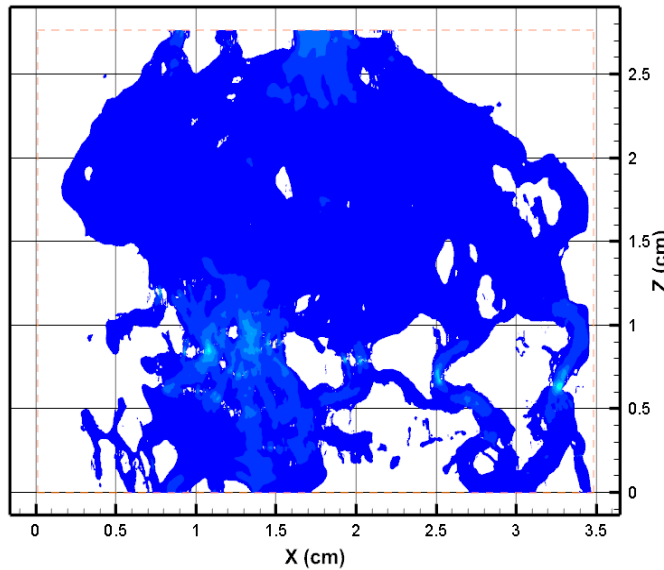
Shear Step 1



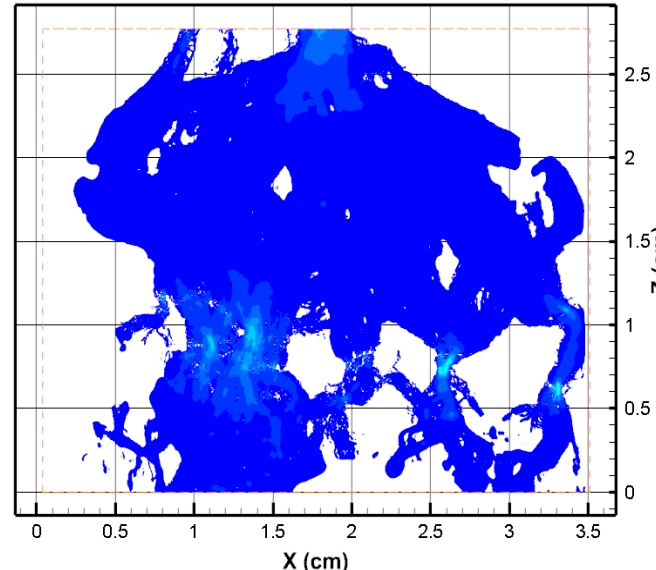
Shear Step 2



Shear Step 3

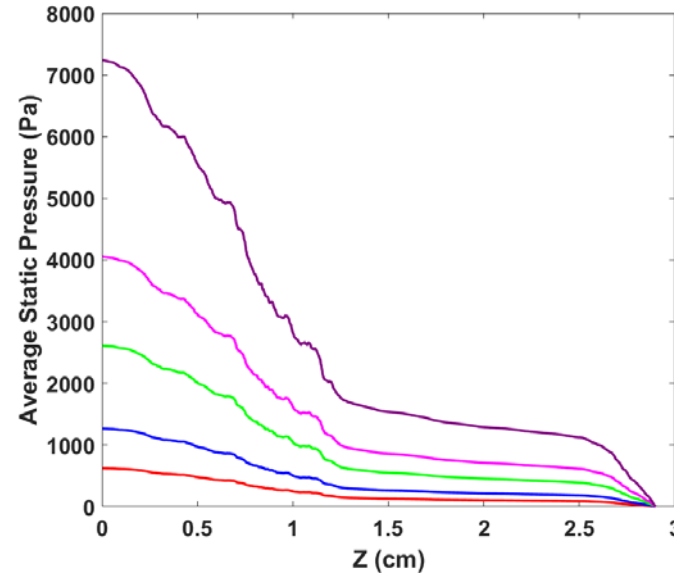


Shear Step 4

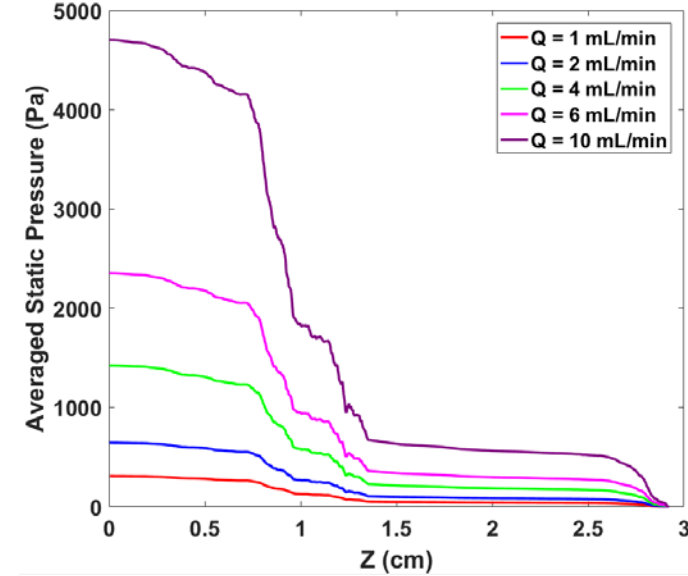


Pressure Drops

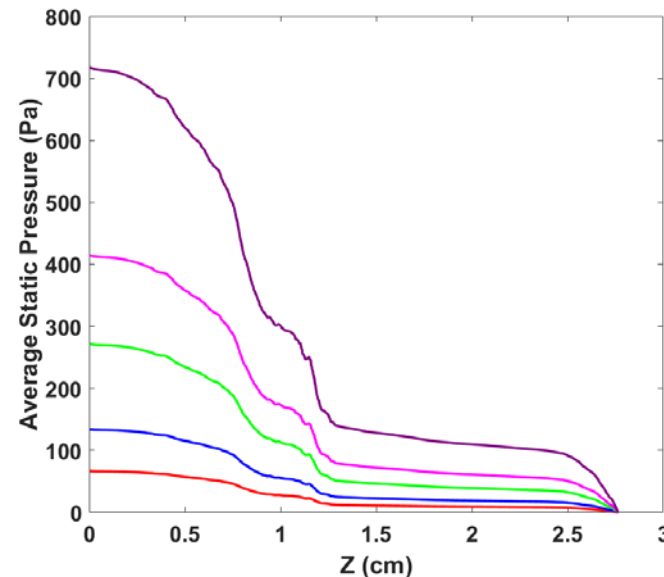
Shear Step 1



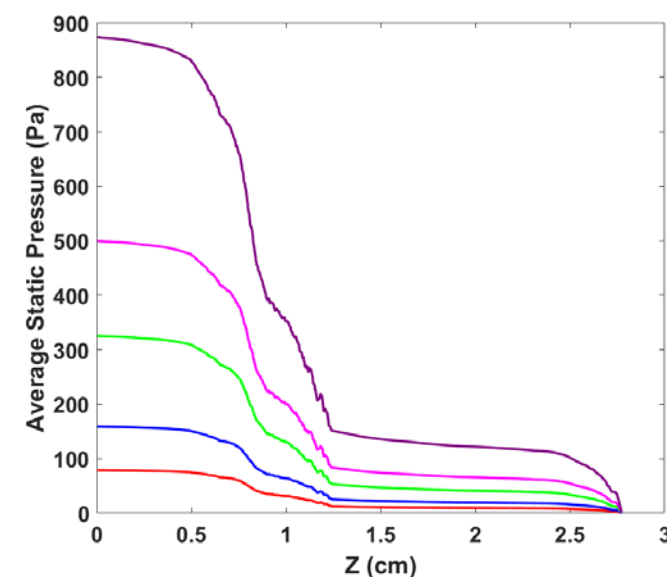
Shear Step 2



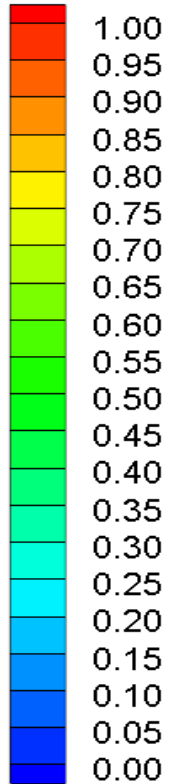
Shear Step 3



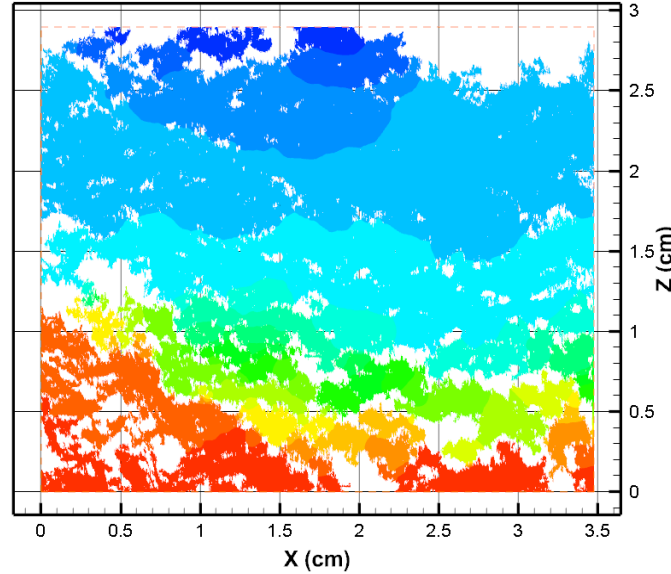
Shear Step 4



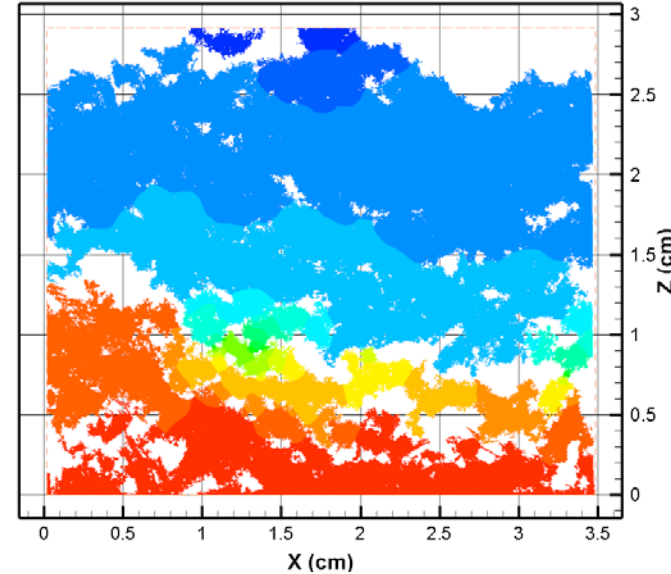
Normalized Pressure (Pa)



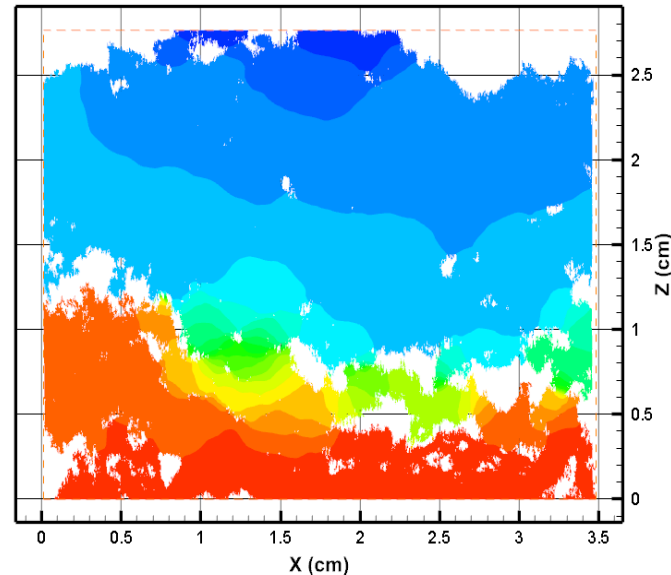
Shear Step 1



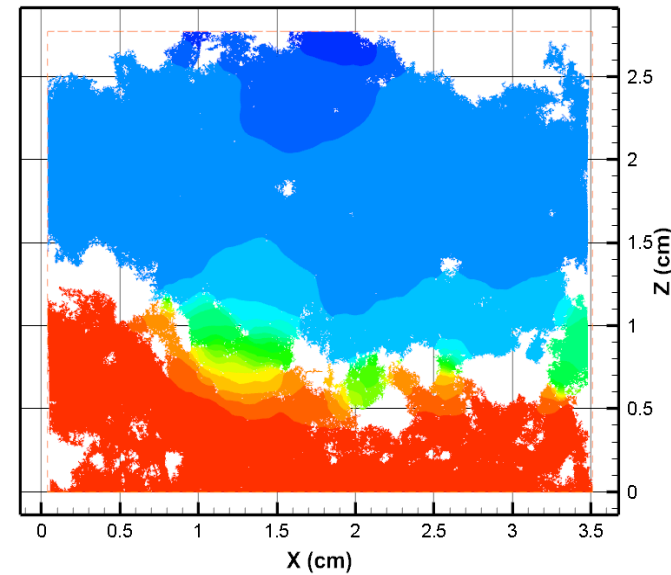
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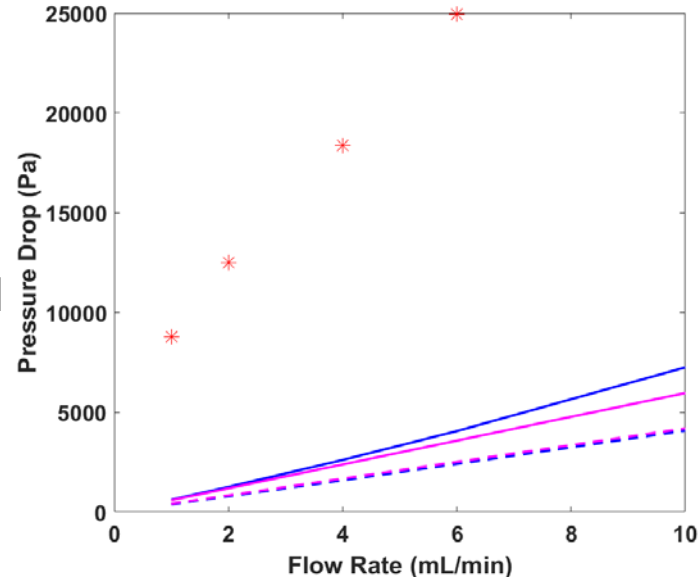
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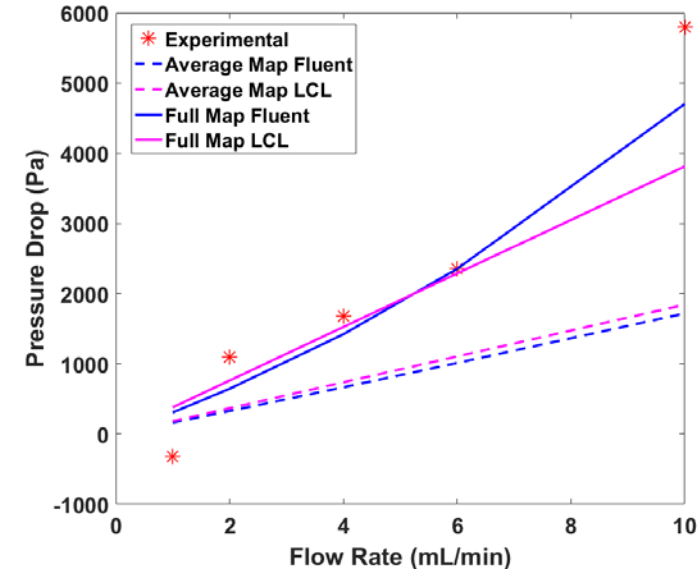
Shear Step 4



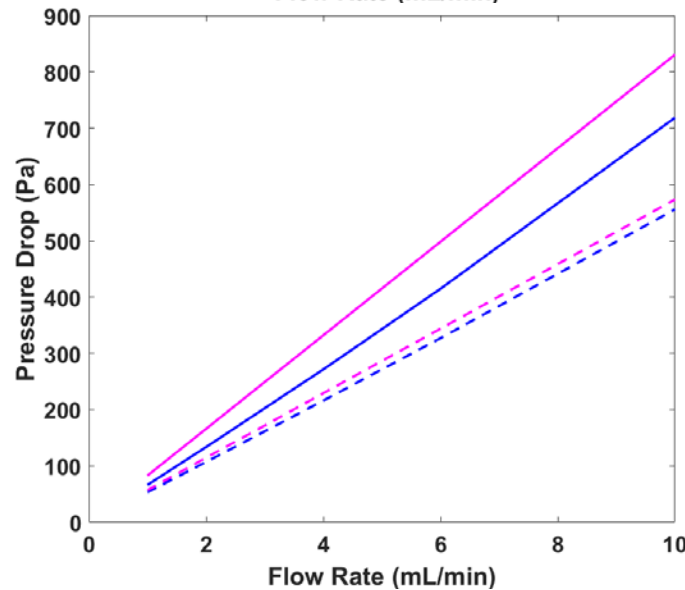
Shear Step 1



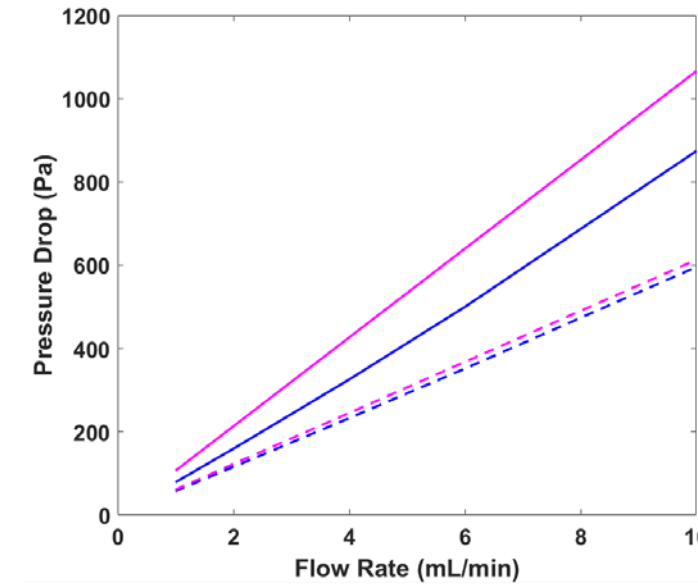
Shear Step 2



Shear Step 3



Shear Step 4



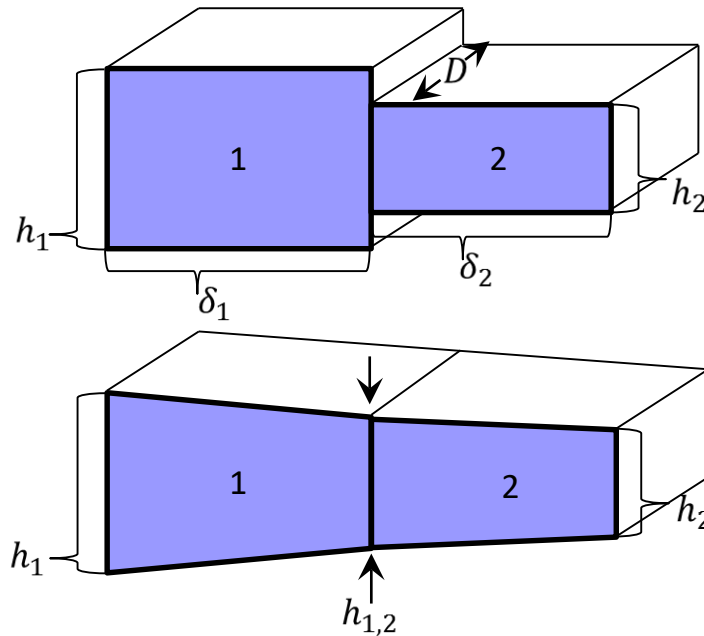
- A sheared Marcellus shale fracture was studied experimentally.
 - Sheared at different steps.
 - Permeability was measured at different flow rates.
 - The fracture was CT scanned at a high-resolution of 26.8 μm .
 - Geometry of the fractures was captured at each step.

- Low-resolution representations of the CT scans were created at 268 μm (average map).

- The fracture flows were studied numerically using the LCL method and full Navier-Stokes simulations for both the average and full maps.

- Shearing increased the average aperture
 - The corresponding pressure drops and average flow velocities decreased.
- Good agreement was observed between the results for the average map fractures.
- Small deviation was observed for the full map fractures.
- Pressure drops of the average map fractures was smaller compared to those of the full map fractures.
 - Important effects of small scale surface roughness on increasing the fracture pressure drops.

Grid Block Transition:



Local Cubic Law:

$$Q = \frac{(h_{1,2}^3 \cdot D)}{(12 \cdot \mu)} \cdot \frac{\Delta P_{1,2}}{\delta_{1,2}}$$

Stokes Tapered Plate Correction:

$$\delta_{1,2} = \frac{\delta_1 + \delta_2}{2} \quad \tan(\theta_{1,2}) = \frac{|h_1 - h_2|}{\delta_{1,2}}$$

$$h_{1,2}^3 = \left[\frac{2 \cdot h_1^2 \cdot h_2^2}{h_1 + h_2} \right] \cdot \left[\frac{3(\tan(\theta_{1,2}) - \theta_{1,2})}{\tan^3(\theta_{1,2})} \right]$$

This method strongly tends towards the smaller aperture