



Polymer degradation principles - characterization challenges for sorption and transport phenomena

Mathew Celina, Erik Linde, Nick Giron

Organic Materials Science Dept. 1853
Sandia National Laboratories, Albuquerque, NM 87185-1411

44th PolyMAC, Albuquerque, NM, June 26 – 28, 2018



*Exceptional
service
in the
national
interest*



Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

Approved for unlimited public release, SAND2018-XXXX



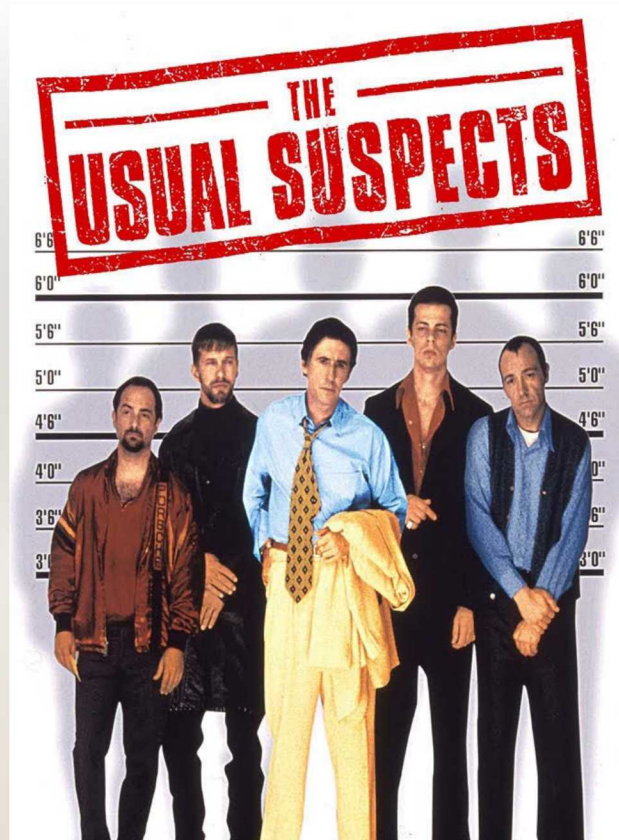
Do you know this movie?



Do these guys look suspicious?



Do you know this movie?



**In applied polymer science the USUAL SUSPECT is often DIFFUSION
A variable that often explains our 'real data' and the anomalies**



Motivation and Challenges

Polymer degradation and materials characterization often involves diffusion processes, reagent transport (O_2 , H_2O) and exchange of small molecules

- **Aging - Off-gassing - Compatibility**
- **Oxidative aging**
- **Hydrolytic aging**
- **Drying and best processing of materials**
- **Solvent loss, trapped species, delayed release**
- **Swelling and reversible stress states**

Ongoing broad research goals to measure, model and predict sorption, diffusion and permeation processes

Goals: Improved diagnostic methods, time resolved spectroscopy, understanding material behavior, quantitative predictions, mechanistic evaluation, spatially and time dependent degradation chemistry



The Simple View

$$\overset{D}{\text{Diffusivity}} \times \overset{S}{\text{Solubility}} = \overset{P}{\text{Permeability}}$$

(diffusion constant)

- Specific material properties for polymer and penetrant
- Fick's law offers time and concentration relationships
- Guiding data are available in Polymer Handbook and Polymer Property text books

Whenever motion and TIME is involved we consider DIFFUSION
When we quantify reactions and masses we need PERMEATION



The Big Picture View

Basics

Diffusivity	Diffusion
Permeability	Permeation
Solubility	Sorption
Time	Rates
Fick's law	Diffusion constant
Slow	Dissolved species
Transport	
Concentration	Square root
Non-linear	Migration
Small molecules	

Complicating Extras

Depth T_g
Mean free path
Mobility variations
Mean square collision diameter
Free volume
Polymer chain flexibility
Desorption
Differential equations
Gradient Partial pressure

Consequences

Diffusion profile
Diffusion control
Local properties
Local reactivity varies
Max. Penetration
Spatial dependence
Surface degradation
Permeative Flux
Trapped species
Quantitative off-gassing difficult

All the things that we didn't really study in 'physical chemistry'

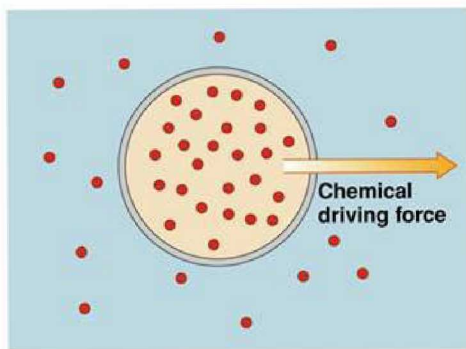
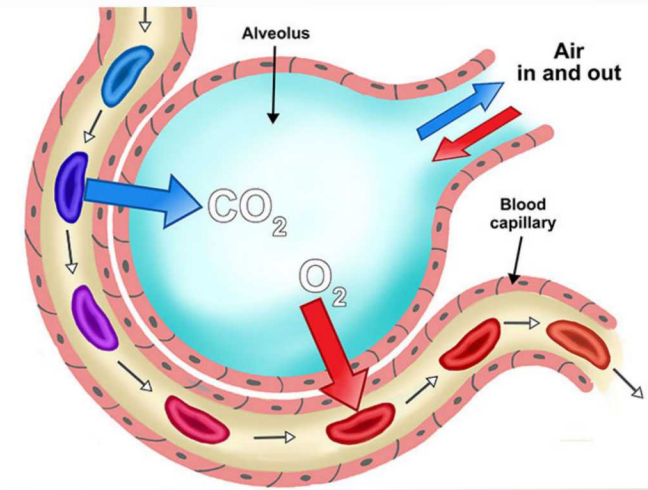


Diffusion is Everywhere

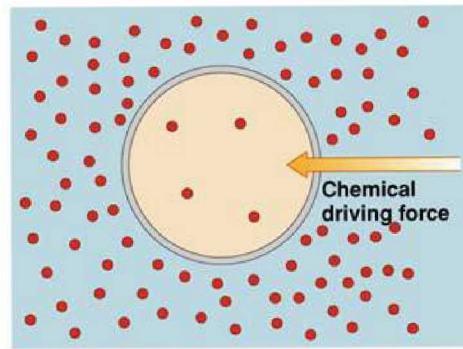
DIFFUSION



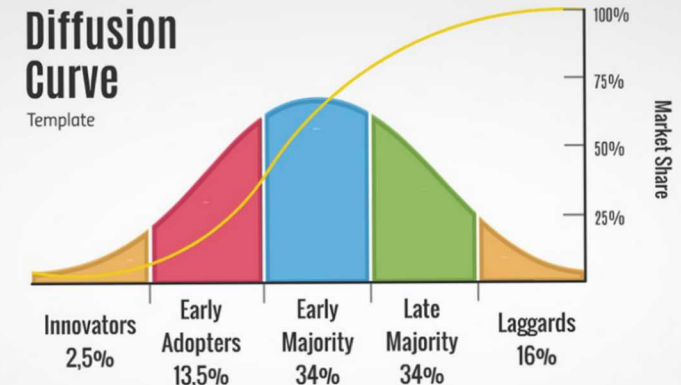
An Ink Drop Gradually Dissolves into a Glass of Water by **DIFFUSION**



(a)



(b)



Our creativity is hopefully also diffusing forward



Mathematical Description - Polymer Oxidation

MODEL CONCEPT - OXIDATION & DIFFUSION

Oxidation rate derived from the
Basic Auto-Oxidation Scheme (BAS):

$$-r_{O_2} = \phi = \frac{k_a[O_2]}{k_b[O_2] + 1}$$

Incorporation into Fick's second law:

$$\frac{\partial \theta}{\partial \tau} = \nabla^2 \theta - \frac{\alpha \theta}{\beta \theta + 1}$$

Pressure dependence of oxidation rate:

$$\frac{\phi}{\phi_0} = \frac{\beta + 1}{\beta + 1/\theta}$$

DLO model parameters:

$$\frac{\alpha}{\beta + 1} = \frac{\phi_0 L^2}{P_{ox} p_0}$$

$$\begin{aligned} \alpha &= \frac{k_1 L^2}{D} \\ \beta &= k_2 S p_0 \\ \theta &= p/p_0 \\ \tau &= \frac{t D}{L^2} \\ \chi &= x/L \\ P_{ox} &= D S \\ [O_2] &= S p_0 \text{ (Henry's Law)} \end{aligned}$$

MODEL PARAMETERS

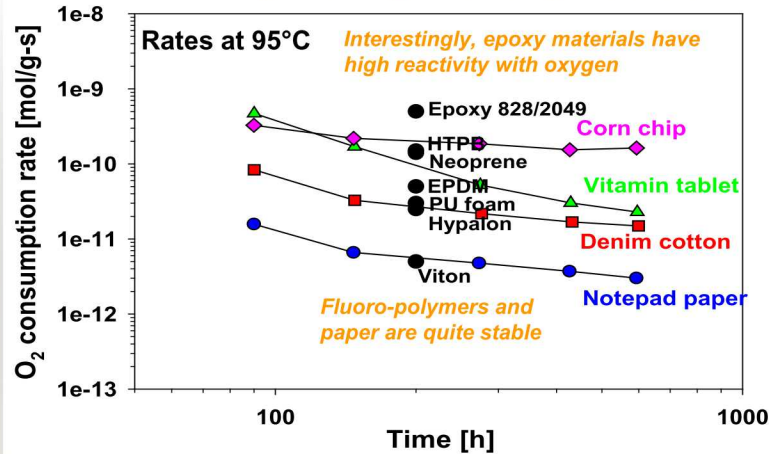
$k_a, k_b \dots$	BAS overall rate constants
$\alpha, \beta \dots$	DLO model parameters
$\phi \dots$	Oxidation rate [mol/g/s]
$\theta \dots$	Relative oxygen partial pressure
$P_{ox} \dots$	Oxygen Permeability [ccSTP/cm/s/cmHg]
$D \dots$	Diffusivity [cm ² /s]
$S \dots$	Solubility [mol/cc/cmHg]
$p_0 \dots$	Oxygen partial pressure (reference) [cmHg]
$\chi \dots$	Relative position
$L \dots$	Thickness (reference) [cm]
$\tau \dots$	Normalized time
$t \dots$	Time [s]
$\Omega \dots$	Spatial integrator depending on dimension
$\varphi \dots$	Simplex interpolation function

- Many years of developmental work – SNL is a global leader
- Interdisciplinary material science is the foundation for aging models

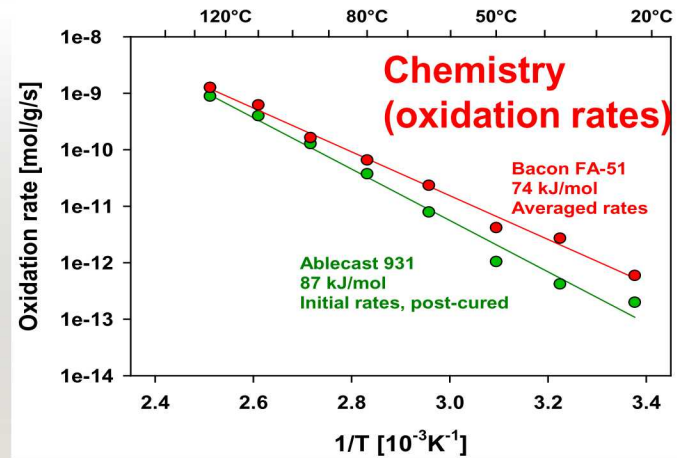


Reactive Diffusion Models Development

Polymer oxidation relevant to reliability and degradation processes

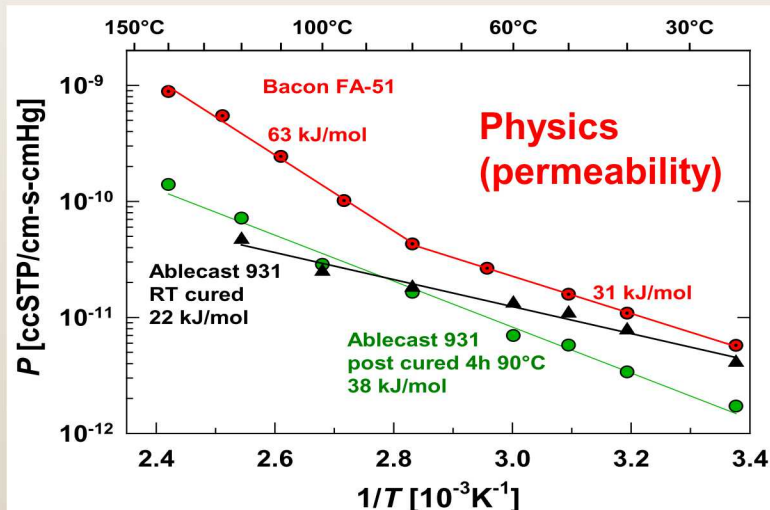


Measured intrinsic oxidation behavior for epoxies in Bell XI

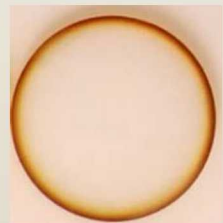
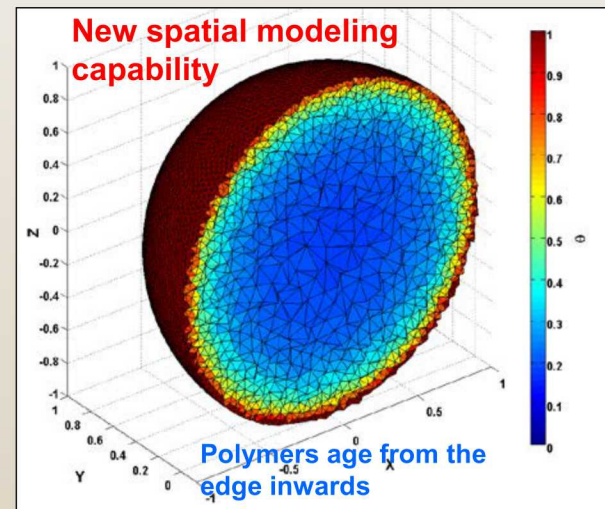


Celina MC, Dayile AR, Quintana A. A perspective on the inherent oxidation sensitivity of epoxy materials. Polymer 2013;54:3290.

Measured oxygen permeation for epoxy materials in Bell XI



Applied FEM DLO model capability for spatially resolved polymer degradation



Exptl. Aged epoxy

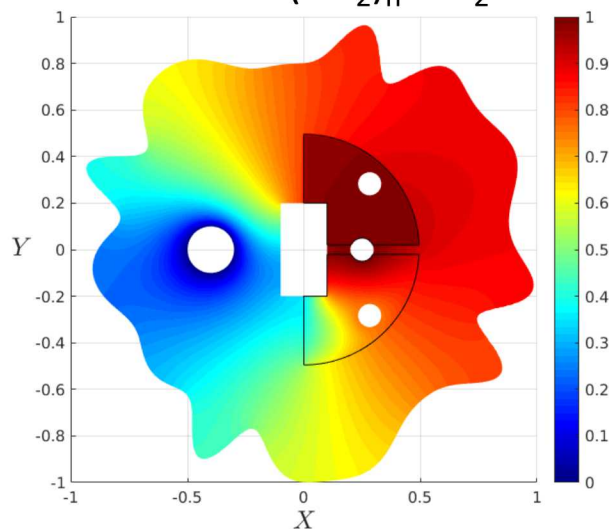


Polymer Aging and Predictive Behavior: Principles of Oxidative Polymer Degradation

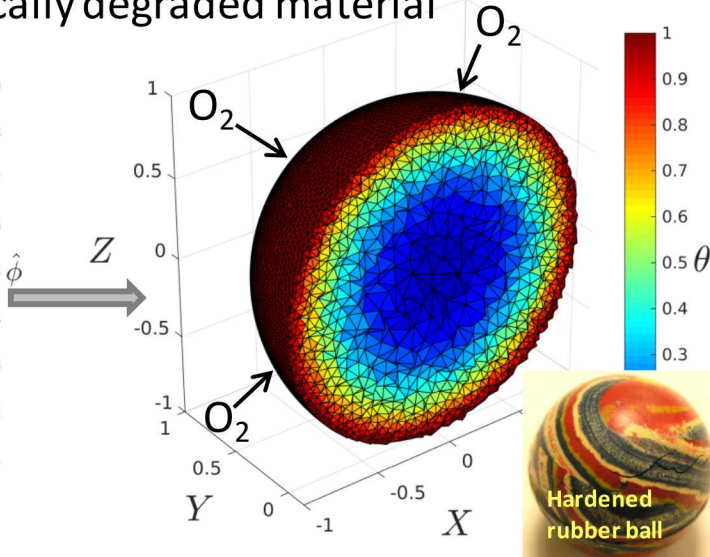
- Continuing SNL leadership with state of the art mathematical models
- Requires understanding of oxidation and reactive diffusion processes



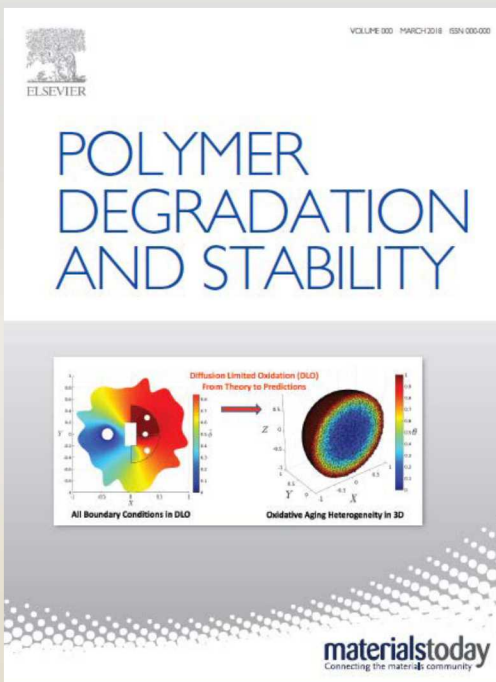
Heterogeneous Polymer Degradation: From the Theory of Oxidation to Predictions 1D Definitions to describe 3D Surface Diffusion Limited Oxidation (DLO)



All Boundary Conditions in DLO



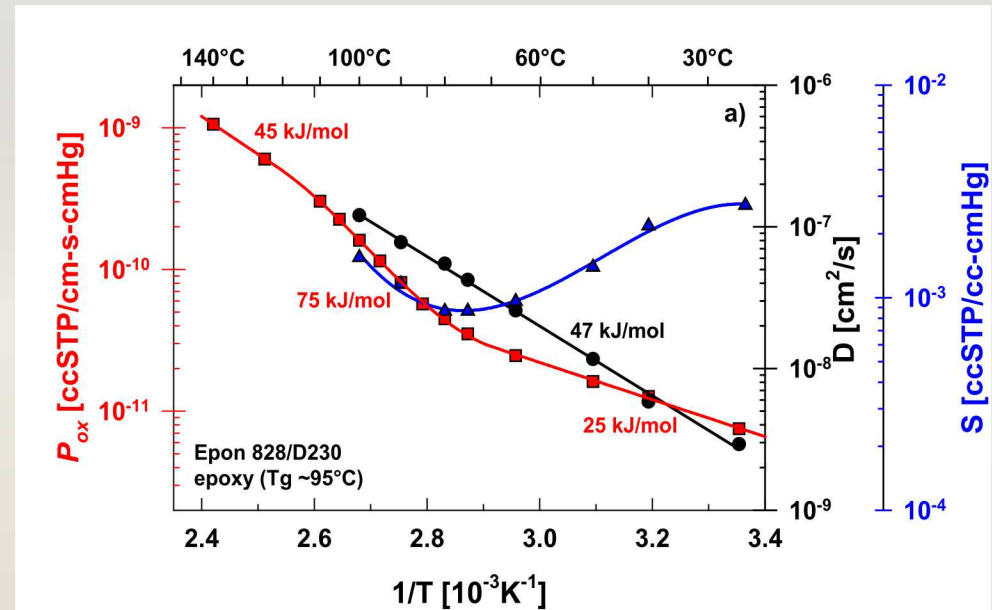
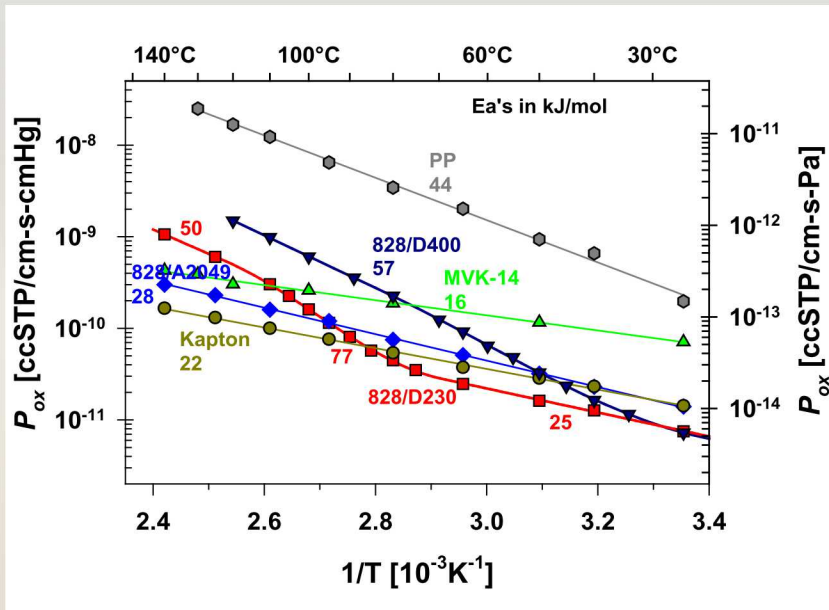
Oxidative Aging Heterogeneity in 3D



Published Review of Current Status in this Field, Added Innovative Mathematical Definitions and Concepts (PDST Inaugural Journal Cover)

O₂ Permeation and Diffusivity with T

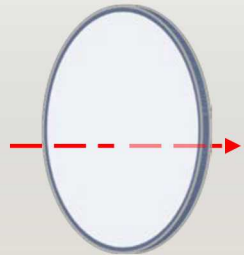
- Developed instrument and computational method to determine D from time dependent flux curves with temperature
- Systematic characterization for a few thermosets and PP



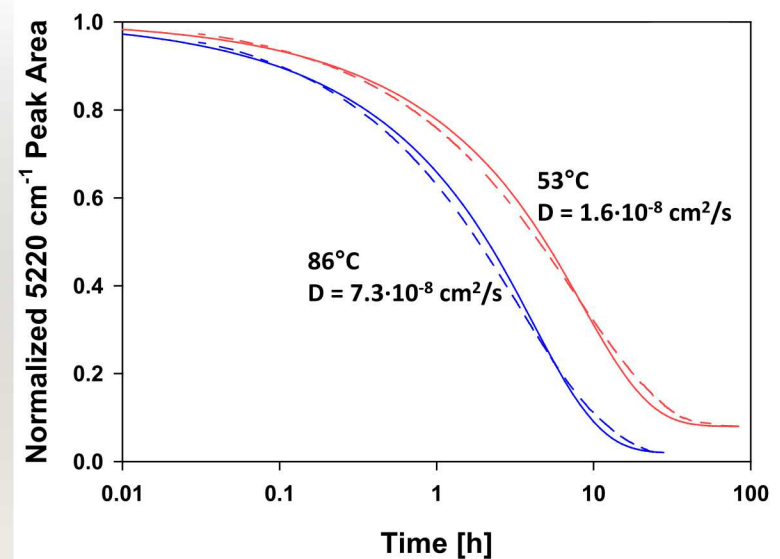
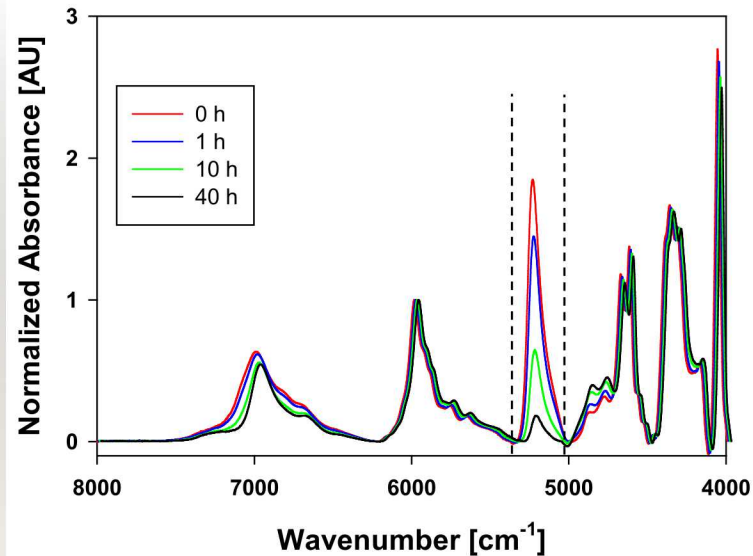
T_g induces change in free volume, but does not affect Diffusivity (solubility instead)
This is in contrast with the literature expectations (Cohen-Turnbull model)



Monitoring Water Content by NIR



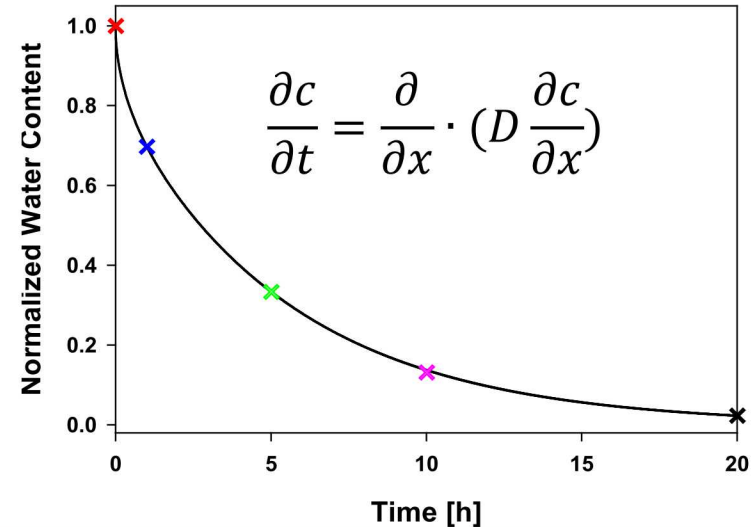
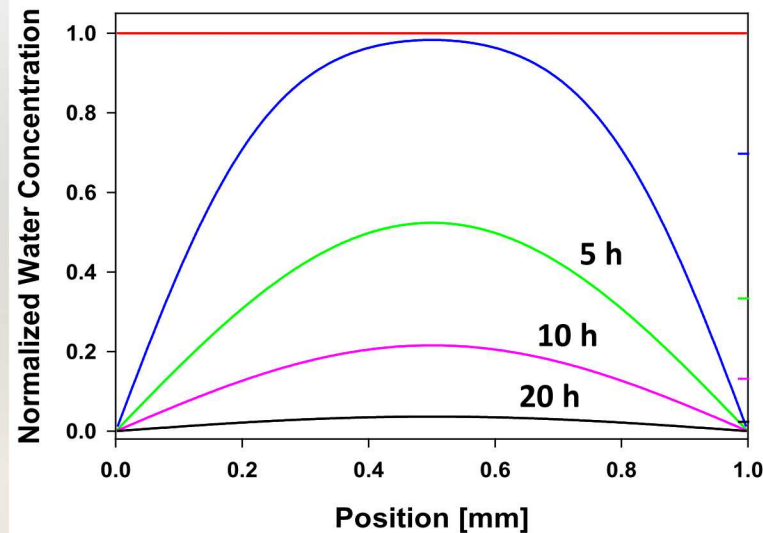
Diameter ≈ 40 mm
Thickness ≈ 1 mm



- Transmission near IR spectroscopy monitors physically dissolved water content within a sample
- Changes in the ‘water band’ around 5220 cm^{-1} were used to follow the desorption kinetics from a disc-shaped sample
- Thin discs (thickness \ll diameter) allows for 1D simplification



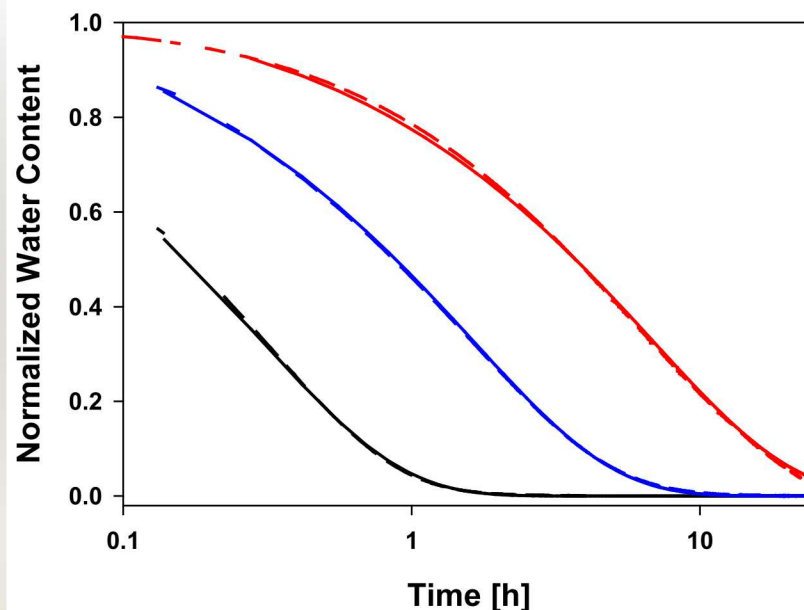
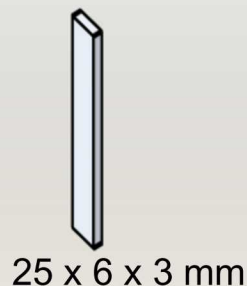
1D Fickian Diffusion



- Desorption follows Fickian diffusion with a constant D
- A finite difference model was used yielding the spatial water distribution and average water content as a function of time
- D was obtained through fitting the simulated desorption curve with the experimental data

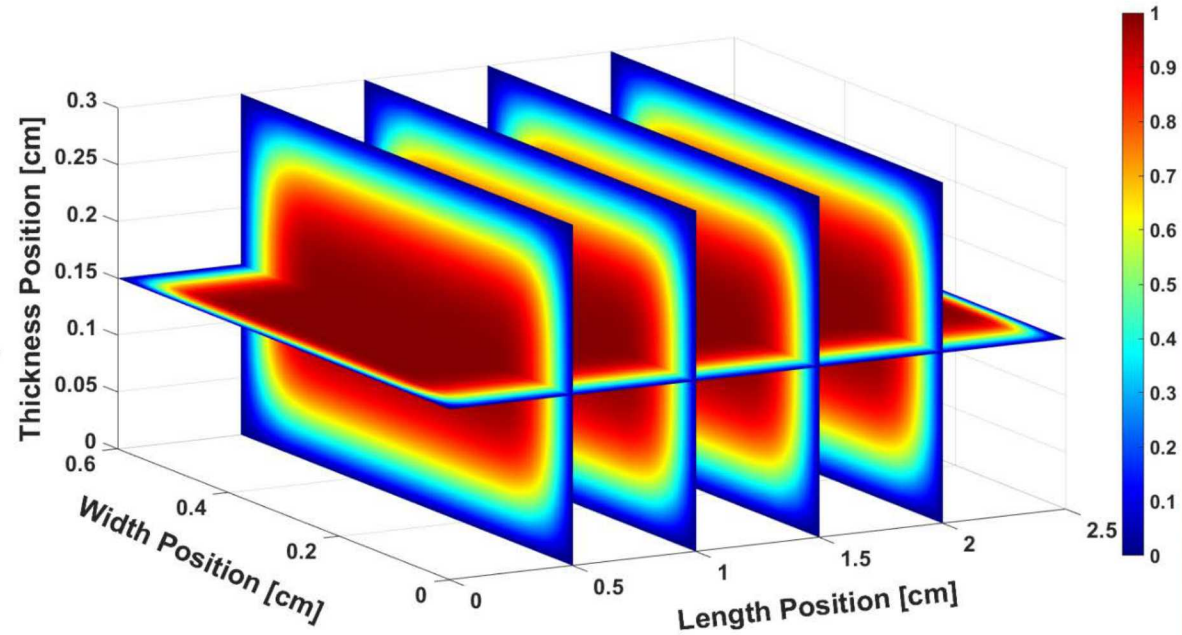
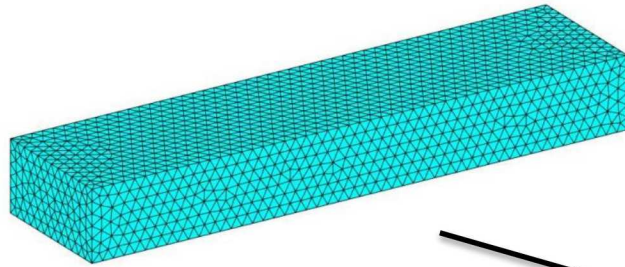


Weight Loss Kinetics by TGA



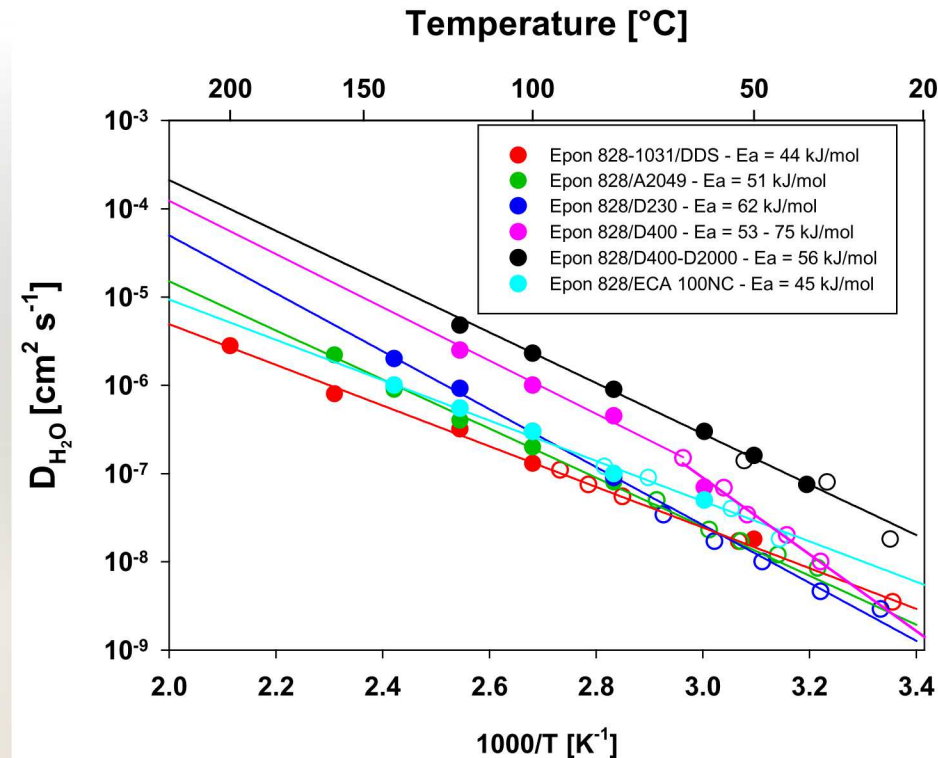
- TGA enables measurements at higher temperatures
- The mass loss follows Fickian diffusion
- The samples dimensions require 3D modeling to extract D

3D Finite Element Model



- The 3D finite element model is used to extract D based on average water content given by the TGA drying curve
- Simulations yield the spatially and temporally resolved water concentration in the material

D as a Function of T



- Most materials show a single E_a for diffusivity over the investigated temperature range (linear Arrhenius)
- One material, Epon 828/D400, shows a change in E_a at T_g ($\sim 65^\circ\text{C}$), from 53 kJ/mol below to 75 kJ/mol above T_g
- For most materials T_g has no influence on E_a of D**



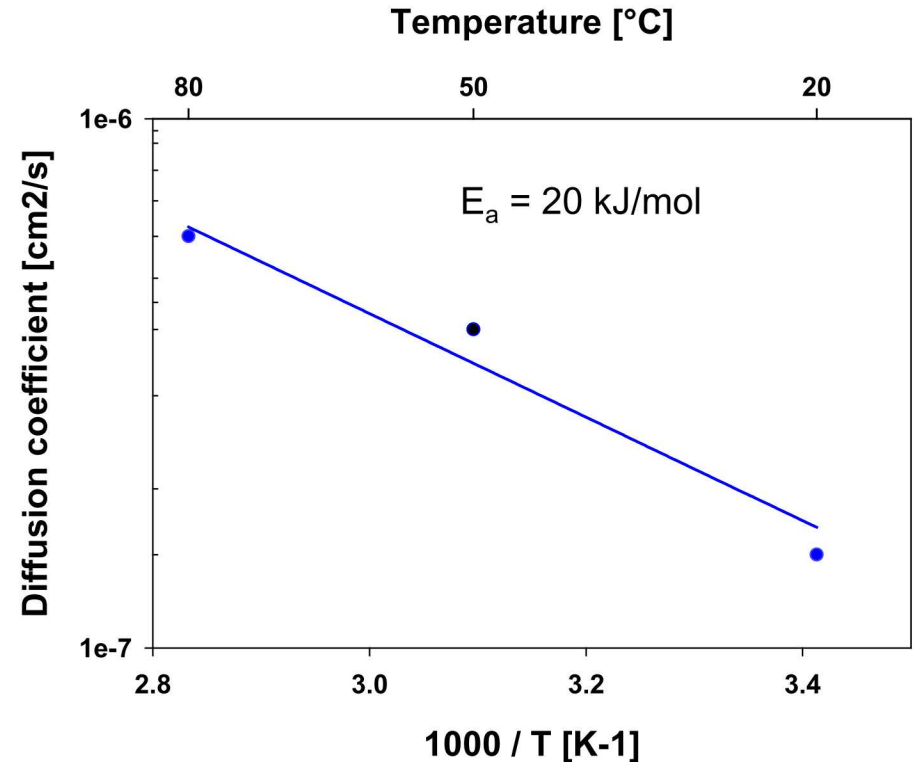
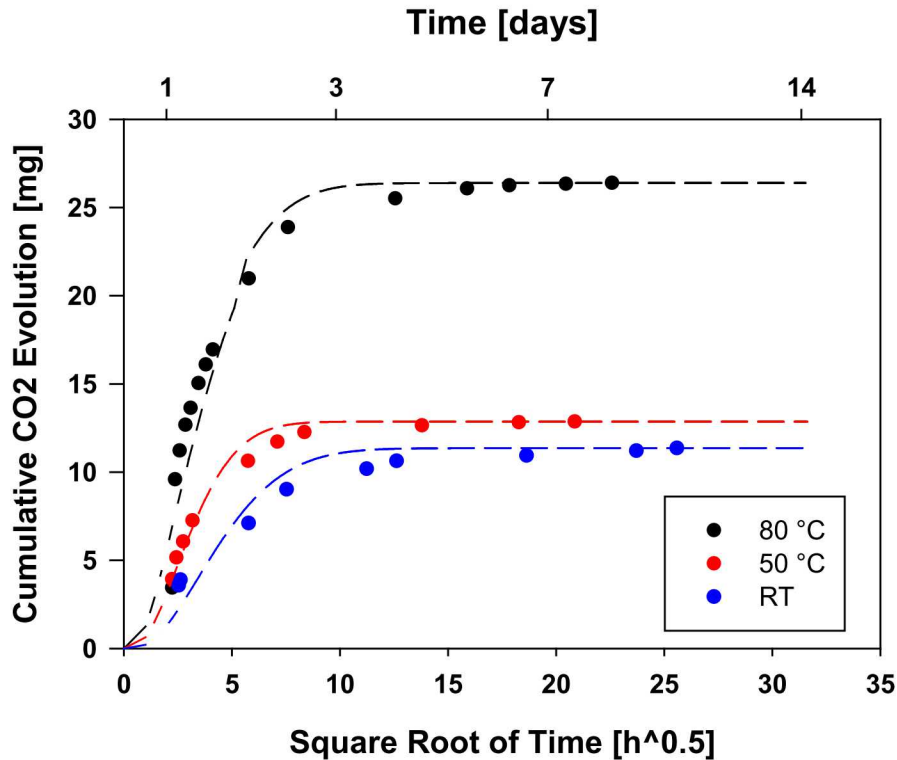
Volume Increase – Free Volume

	Measured uptake [100·g _{H2O} /cc _{polymer}]	D 65°C [cm ² /s]	E _{a,D} [kJ/mol]	Ideal volume increase without free volume [%]	Measured volume increase [%]	Fraction of water occupying free volume [%]
E828 –E1031/DDS	5.8	3.0*10 ⁻⁸	44	5.8	4.2	28
E828/A2049	2	3.2*10 ⁻⁸	51	2	1.3	35
E828/D230	3.3	3.5*10 ⁻⁸	62	3.3	2.0	39
E828/D400	3.6	1.3*10 ⁻⁷	<65°C: 75 >65°C: 53	3.6	2.4	33
E828/D400- D2000	3.8	3.7*10 ⁻⁷	56	3.8	N/A	N/A
E828/ECA 100NC	1.6	6.1*10 ⁻⁸	45	1.6	0.8	50

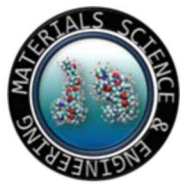
- Max water uptake for epoxies is ~ 15 to 60 mg_{H2O}/cc_{Polymer}
- The volume increase is smaller than the sum of the volume of polymer and the volume of absorbed water
- Some absorbed water occupies the free volume ranging from 28% (DDS cured) to 50% (ECA 100NC cured)
- Solubility and diffusivity are independent parameters
- **Despite some free volume and glassy state, the materials swell significantly even at RT**



CO₂ Evolution Curves from PU

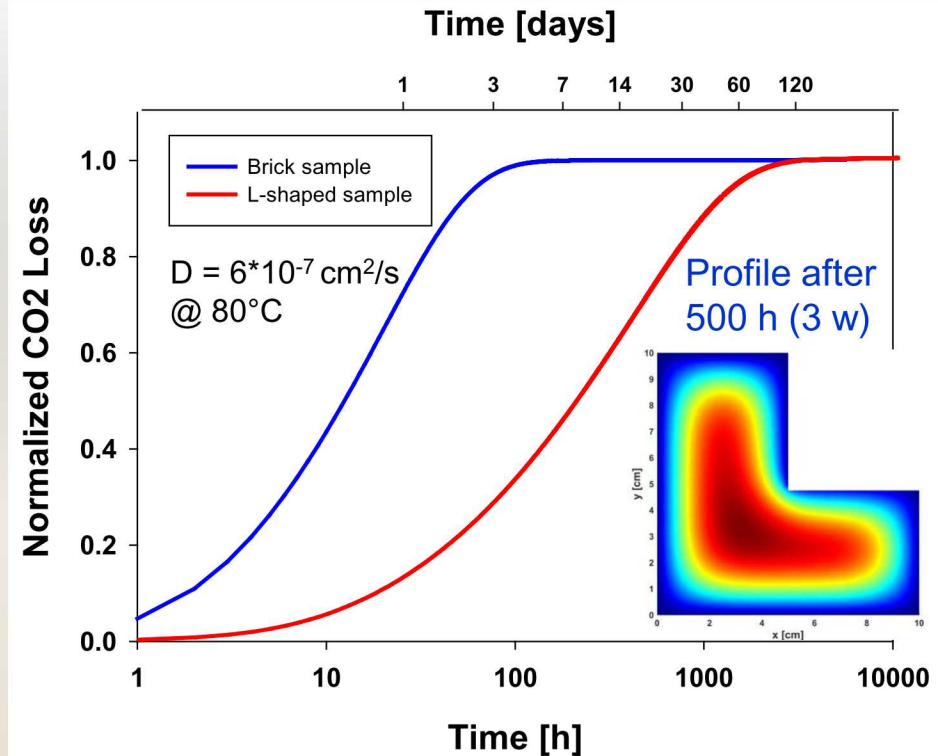
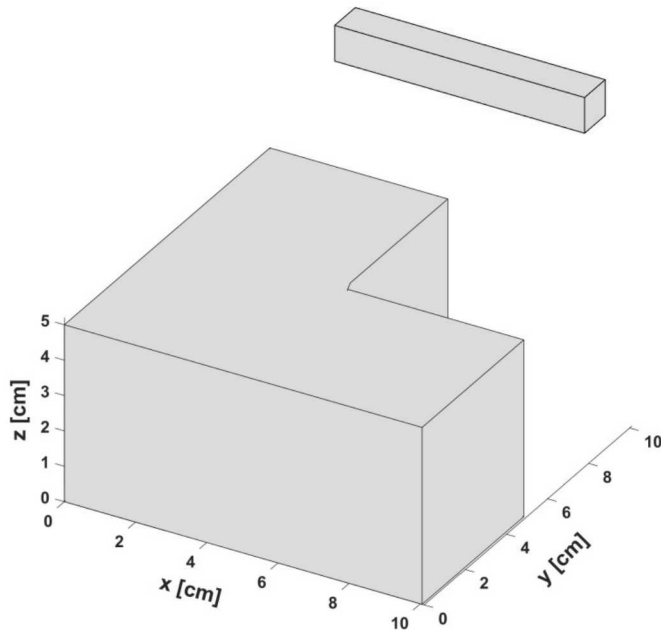


- CO₂ mass loss was fitted with a single D FEM model for that specific geometry.
- A diffusion coefficient also defines the initial linear slope of CO₂ yield in a plot against square root of time; a higher D leads to a higher slope.
- The value of the E_a (20 kJ/mol) for D is of similar magnitude as observed for other diffusion phenomena, such as water in epoxies.



Simulating CO_2 Loss from Other Shapes

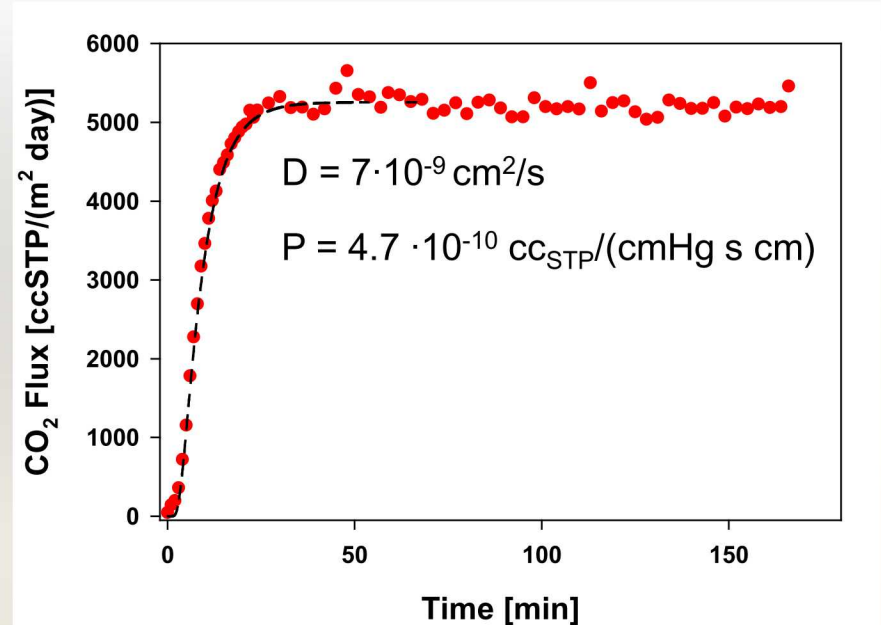
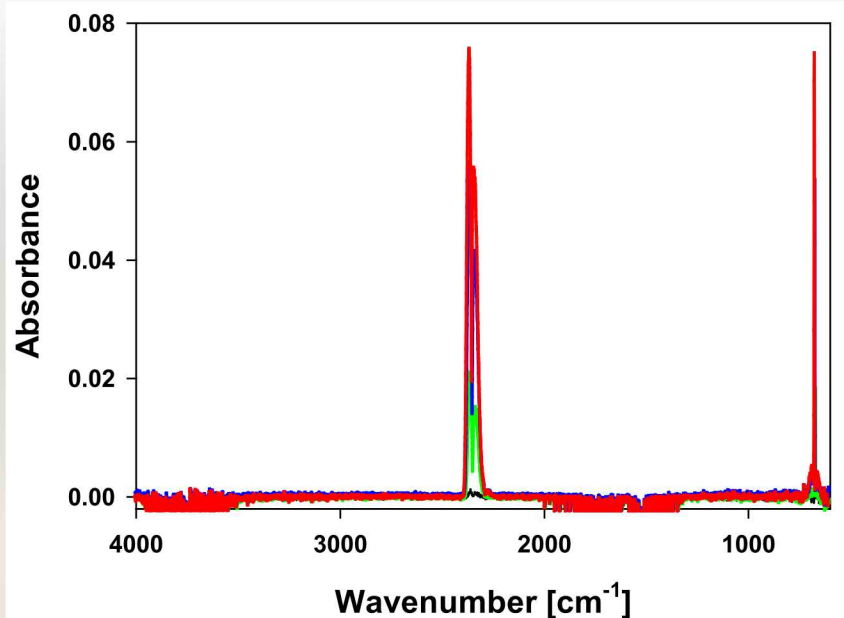
Size comparison of the brick sample run at 80°C and a simulated L-shaped sample



- By using the values of D obtained from the experimental data, the behavior of other, more complex shapes can be assessed.
- Long-term physical desorption at RT can be predicted.



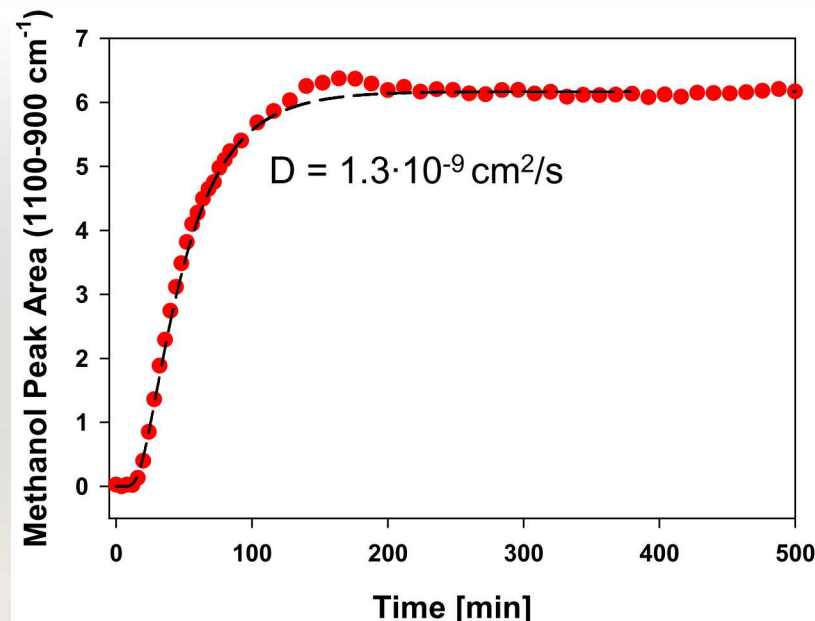
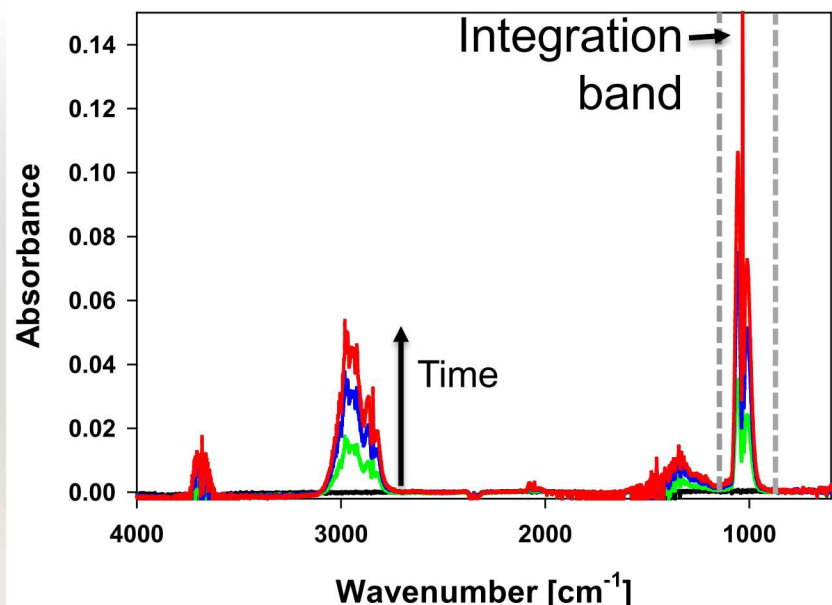
Gas Transport Quantification with mid-IR



- **Goal: Proof of principle to monitor organic vapor diffusion using mid-IR**
- Permeation of CO₂ through a 50 µm Kapton film at 100°C determined using a newly developed mid-IR based method
- Quantification used spectral integration at 672–665 cm⁻¹
- Permeability can be obtained using Fick's first law, and diffusivity is obtained from the time-lag



Organic Vapor Transport through Films



- **Goal: Monitor organic vapor diffusion using IR gas spectroscopy**
- Permeation of methanol through a 50 μm Kapton film at 50°C
- The permeate is detected in IR cell by a flow of dry N_2 at 10 cc/min
- The time-dependent flux matches theory for Fickian diffusion
- Methanol causes significant swelling, which likely increases effective D
- Calibration is required to obtain permeability



CONCLUSION

- Established principles of water sorption and permeation for encapsulation, adhesives and thermosets. Quantification enables guidance throughout SNL
- We lead the aging community through understanding and quantification of O₂ transport through polymers and its local reactivity
- We have started to measure volatile diffusion and are exploring appropriate methods to help SNL community for compatibility and off-gassing
- **IMPACT:**
 - **Our science basis has enabled diagnostics and helped material requalification**
 - **We have recommended improved processing conditions for specific materials**
 - **We assist with material selection and identification of concerns for continued use of materials or replacements**
- **Publications:**
 - Overview of DLO modeling and approaches to predict heterogeneous oxidative polymer degradation. Quintana A, Celina MC. Polym Degrad Stab 2018;149:173.
 - Oxygen diffusivity and permeation through polymers at elevated temperature. Celina MC, Quintana AD. *Polymer* 2018; accepted.
 - Water Diffusion with Temperature Enabling Predictions for Sorption and Transport Behavior in Thermoset Materials. Linde E, Giron NH, Celina MC. Polymer 2018; in revision.



Conclusions

Impact on Service Life Prediction, Polymer Aging Phenomena:

- Despite high T_g glassy epoxy materials absorb water at RT and expand, leading to dynamic mechanical stress that can be an additional concern for reliability and long-term performance
- Accelerated aging studies that involve water, hydrolytic degradation, and weathering must take transport kinetics into account in order to obtain better predictive data (surface wetting vs. partial water uptake or full saturation)