

Phenomenological Modeling of Nonlinear Behavior in Ferroelectric Materials



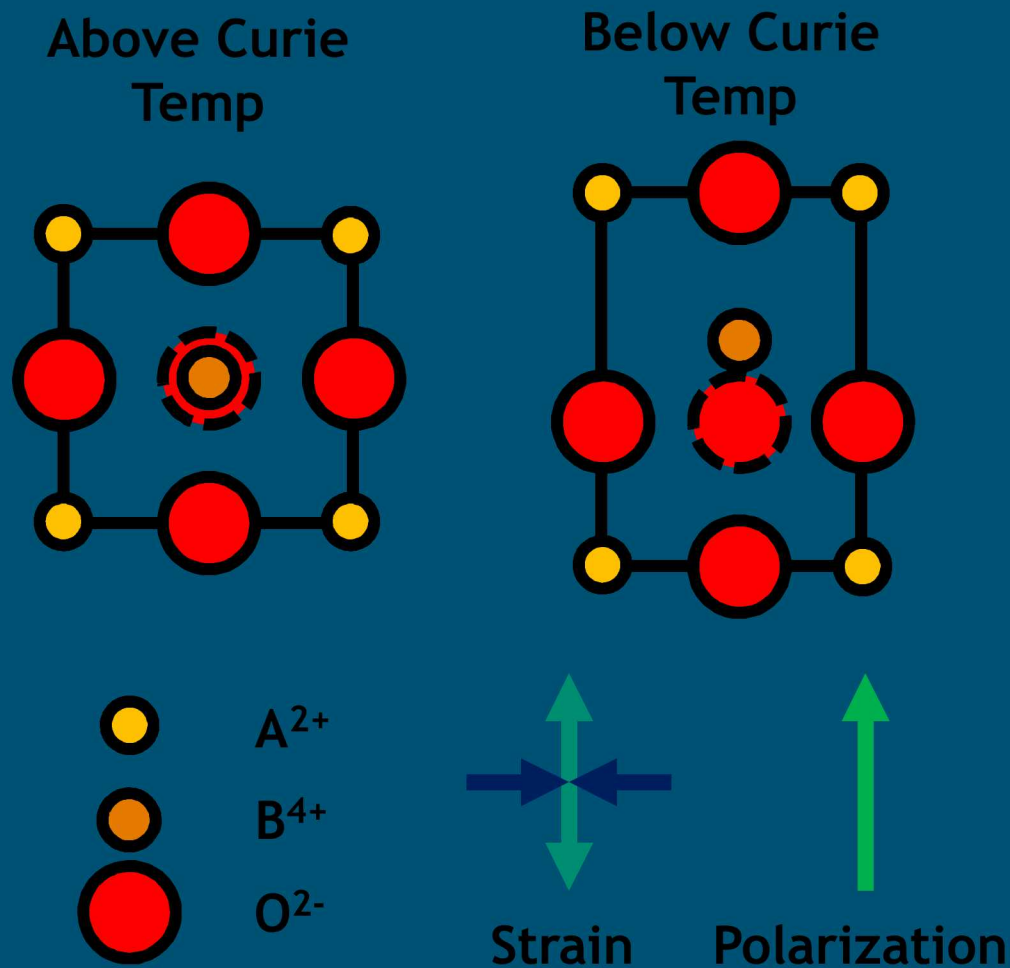
WMRIF Early Career Scientist competition

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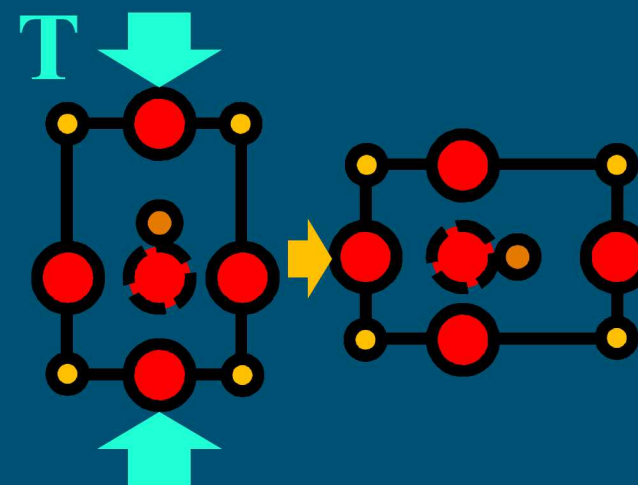
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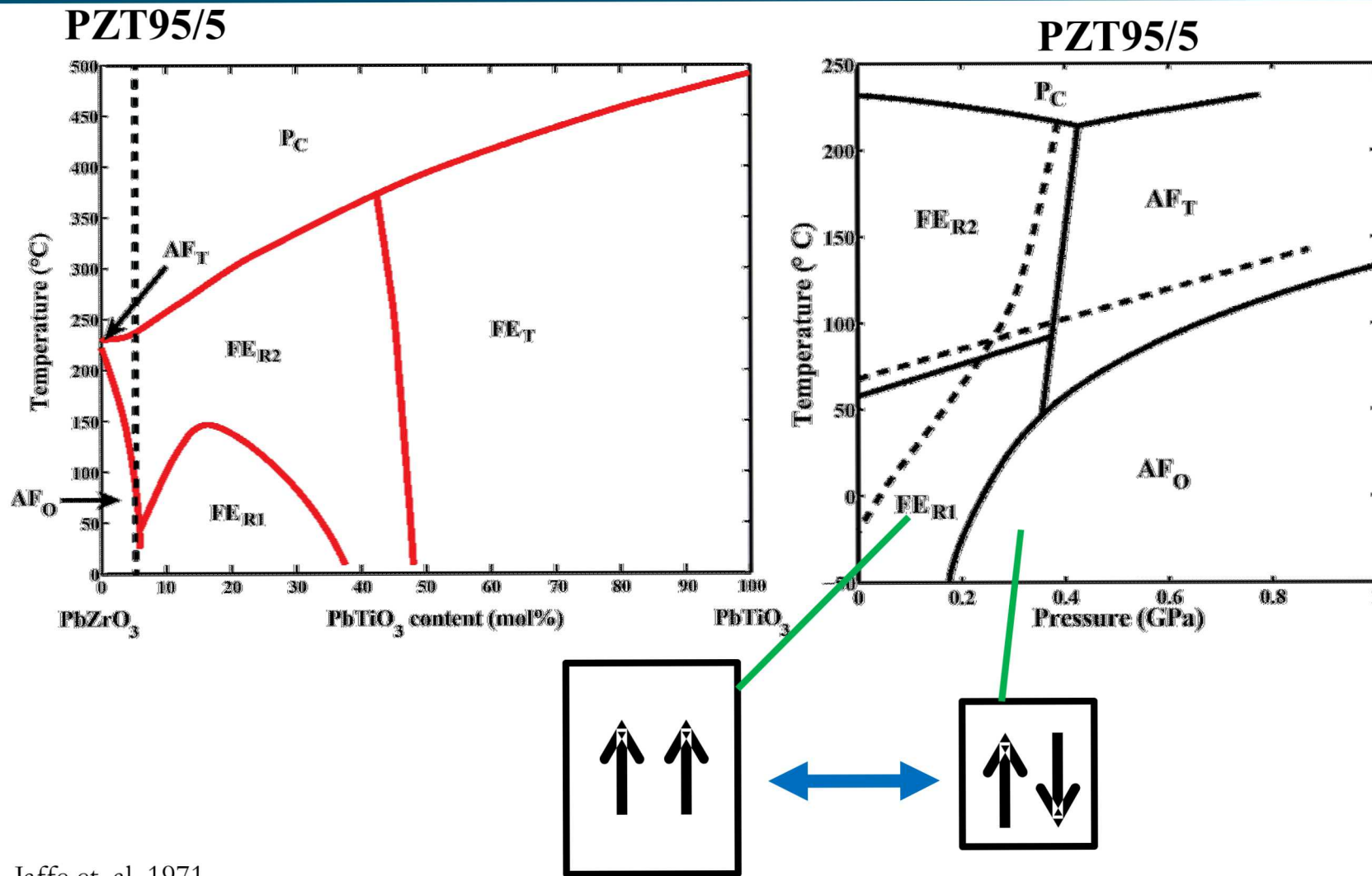
Wen Dong

- Background: Ferroelectric Ceramics and PZT95/5
- Micromechanical Approach
- Switching Criteria
- Simulation of PZT95/5

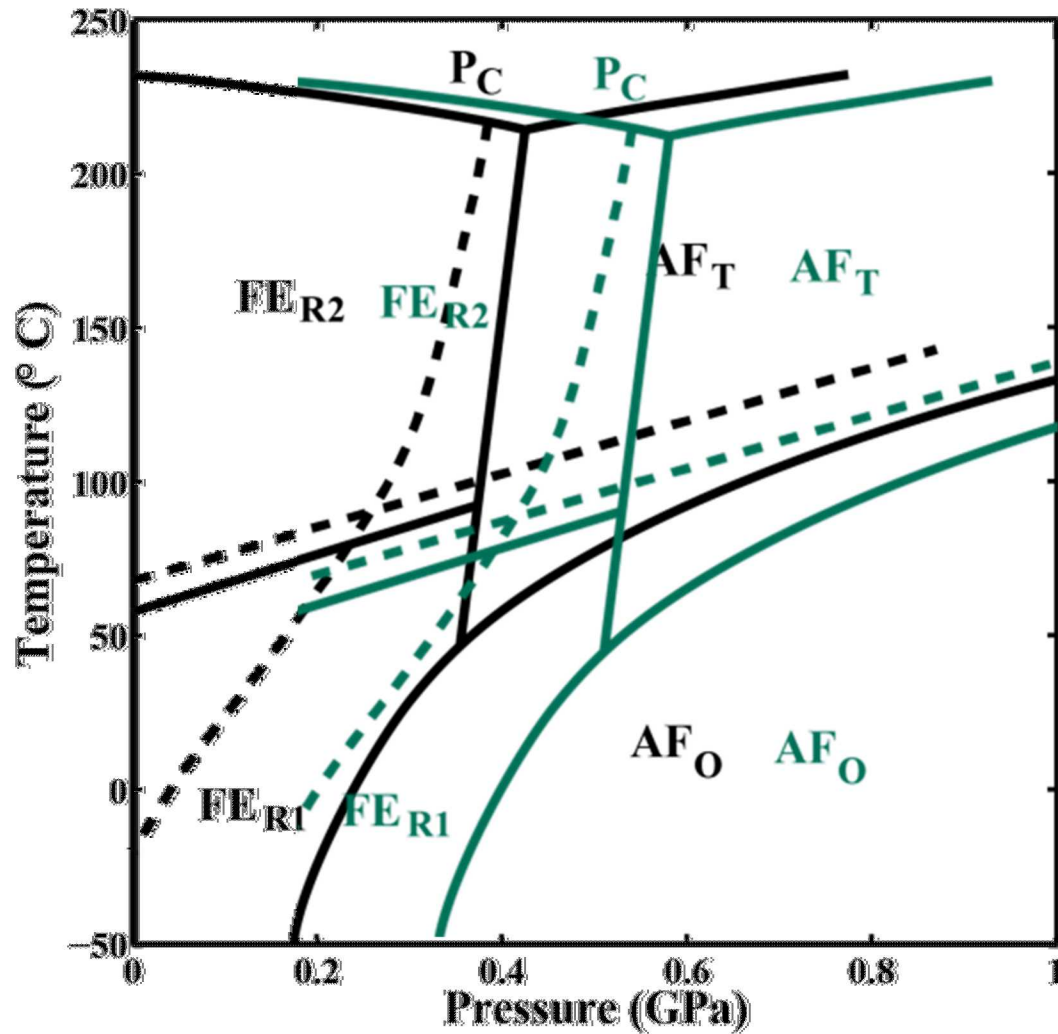


- ❖ Cubic above Curie Temp
- ❖ Shift of ions positions below Curie temperature causes spontaneous polarization and strain.
- ❖ Orientation of polarization and strain is associated with phase.
- ❖ Switching between polarization orientations can be induced by electric field or stress (Domain-switching).

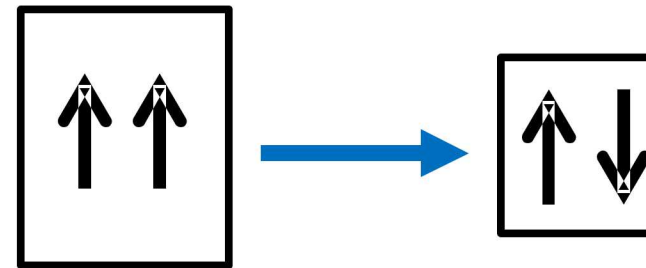




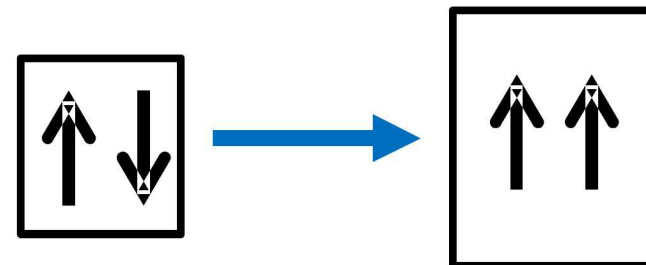
Jaffe et. al. 1971
Fritz and Keck 1978

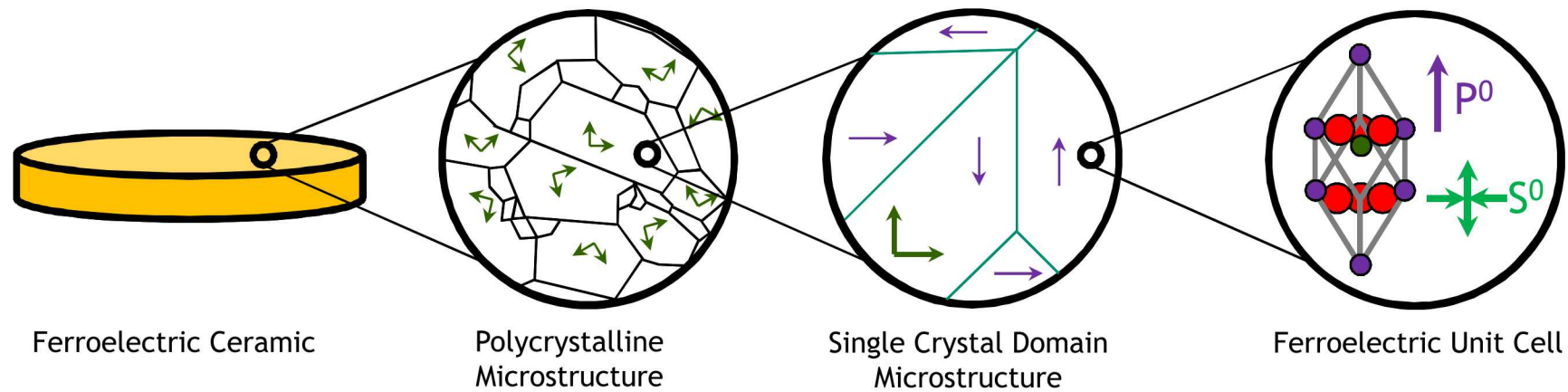


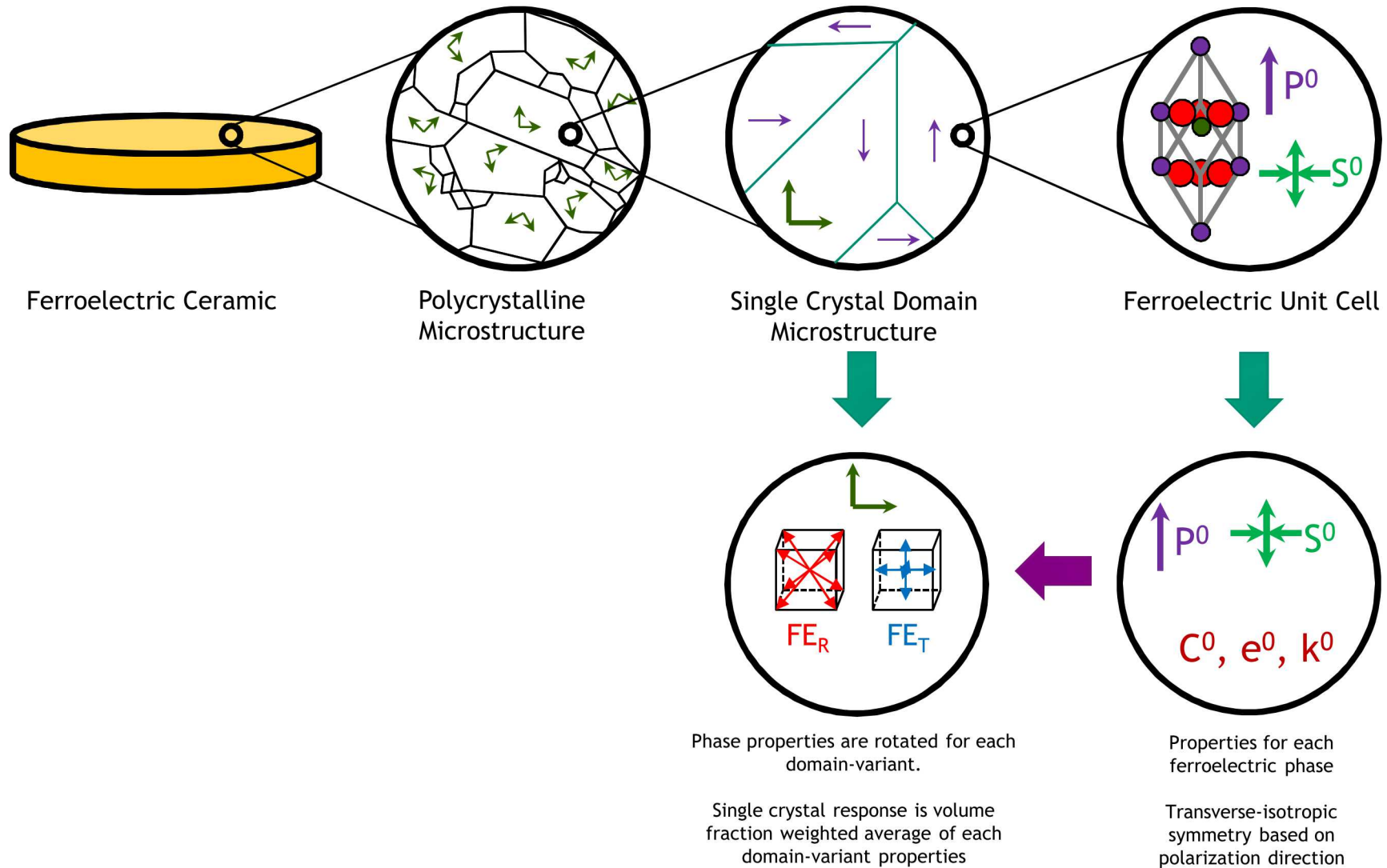
Application of pressure stabilizes antiferroelectric phase

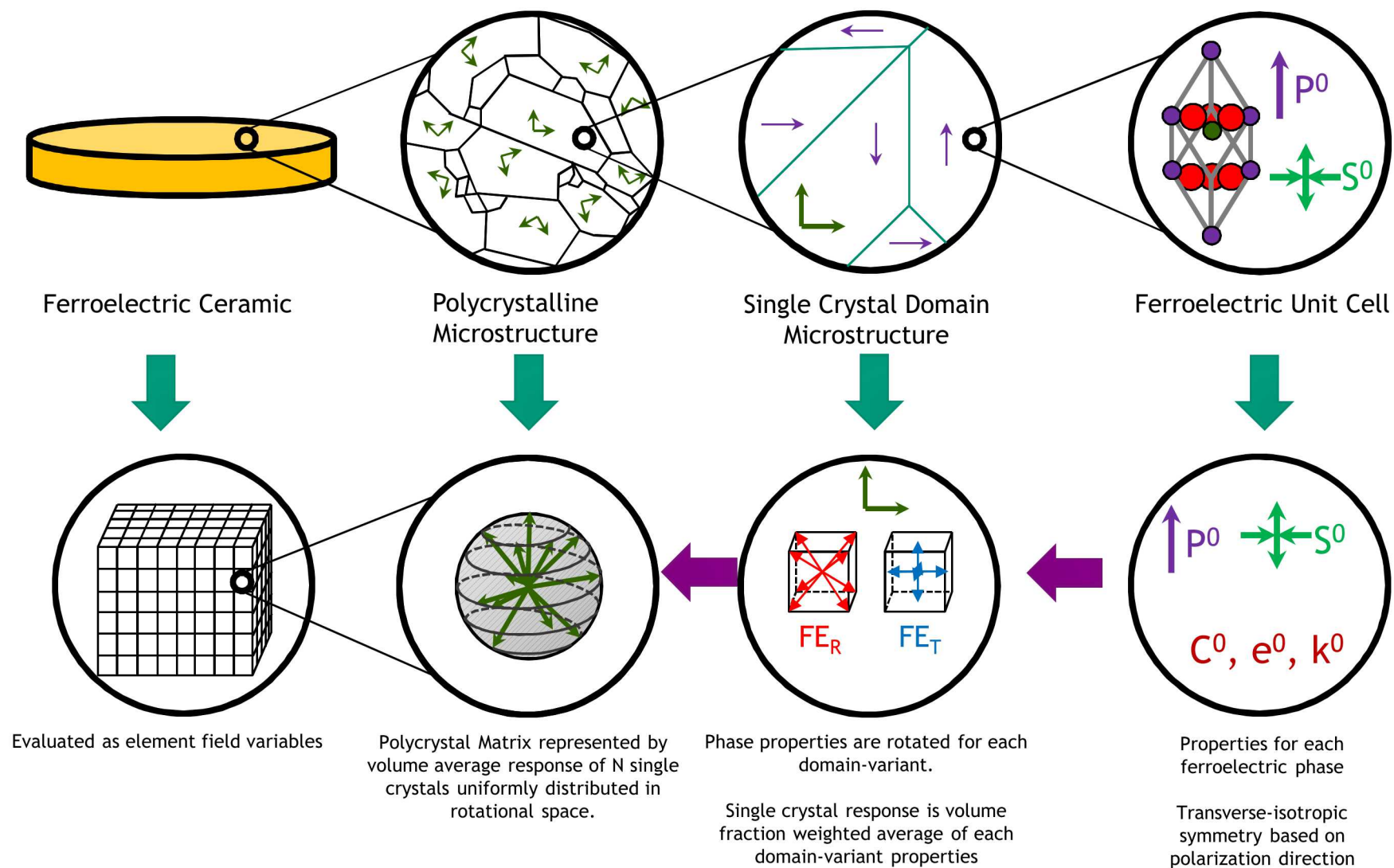


Application of electric field stabilizes ferroelectric phase









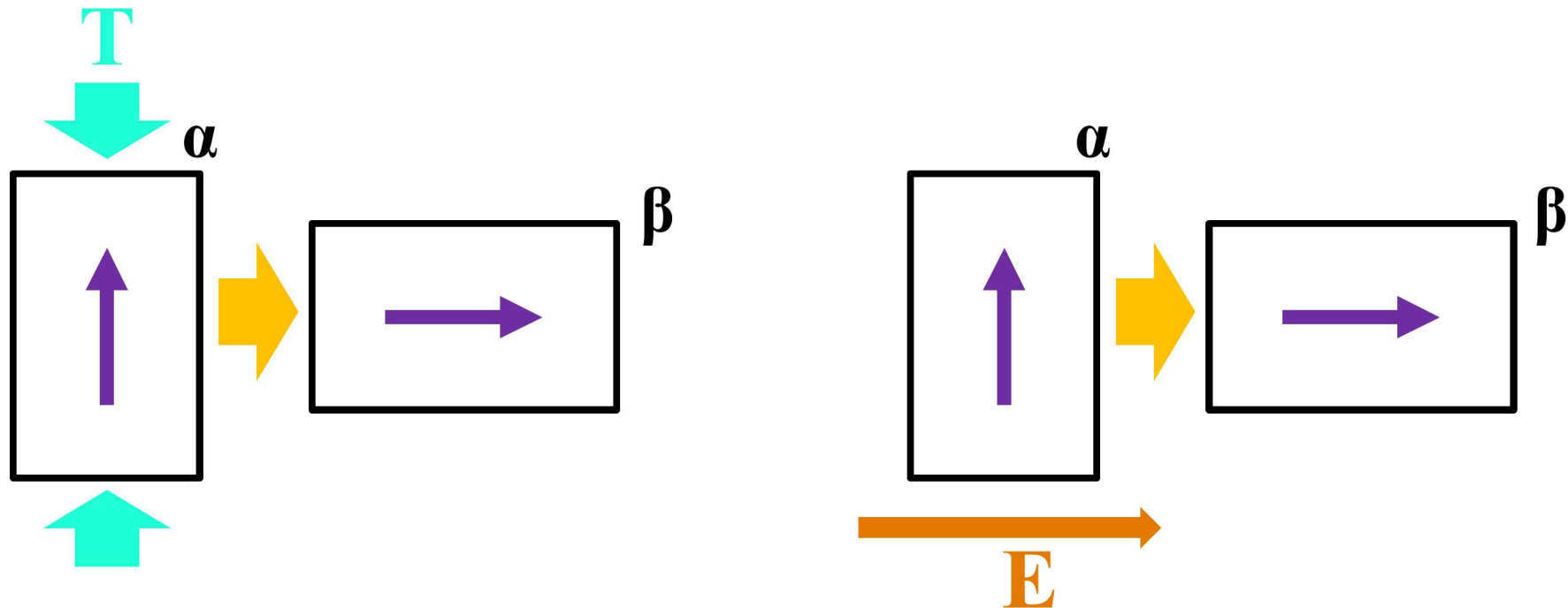
$$g^{\alpha \rightarrow \beta} > 0$$

$$g^{\alpha \rightarrow \beta} = T : \Delta S^{\alpha \rightarrow \beta} + E \cdot D^{\alpha \rightarrow \beta} - B^{\alpha \rightarrow \beta}$$

Driving force of
Transformation

Work performed by
the transformation

Energy barrier for
transformation



Switching Criteria - Distributed Switching Criteria

Needed to capture:

Second order (continuous) transitions
Defects/inhomogeneity in the material

Relative volume fractions of β in α - β system

$$\Phi^{\alpha \rightarrow \beta} = \frac{v^{\beta}}{v^{\alpha} + v^{\beta}}$$

Deviation of driving force of transformation
from switching criteria

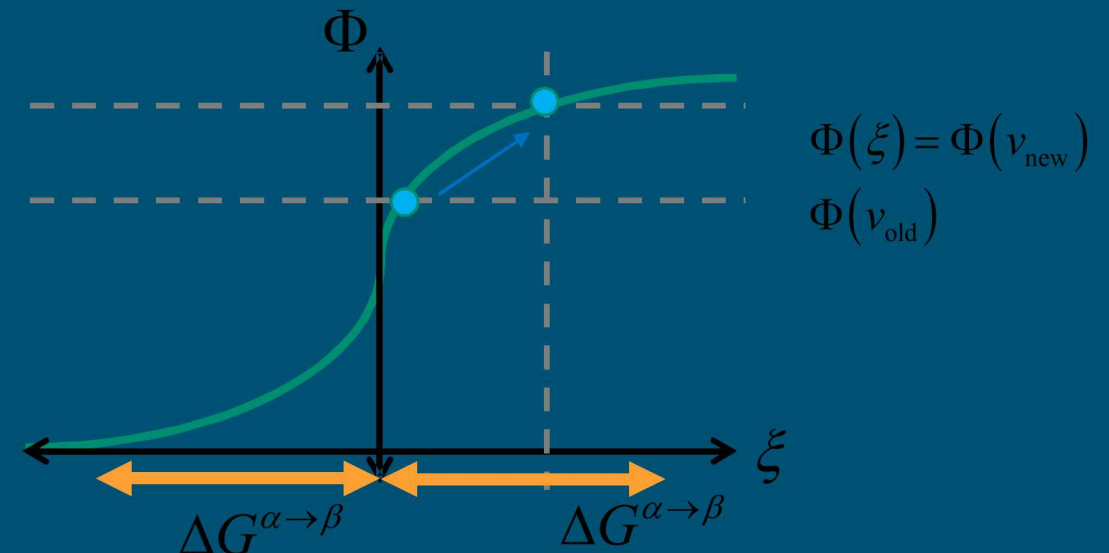
$$\xi^{\alpha \rightarrow \beta} = \frac{g^{\alpha \rightarrow \beta}}{\Delta G^{\alpha \rightarrow \beta}}$$

In the variant α to β transformation, if

$$\Phi(\xi) > \Phi(v_{\text{old}})$$

Then the volume fractions are adjusted such that

$$v_{\text{new}} = v_{\text{old}} + \Delta v \quad \Phi(v_{\text{new}}) = \Phi(\xi)$$



Switching Criteria - Intergranular Interactions

Remnent polarization and strain difference between each grain and the matrix.

$$\Delta \mathcal{P} = \overline{\mathcal{P}}_m^{\text{Grain}} - \overline{\mathcal{P}}_m^{\text{Matrix}}$$

$$\Delta \mathcal{S}_{ij} = \overline{\mathcal{S}}_{ij}^{\text{Grain}} - \overline{\mathcal{S}}_{ij}^{\text{Matrix}}$$

Incompatibility stresses and electric fields

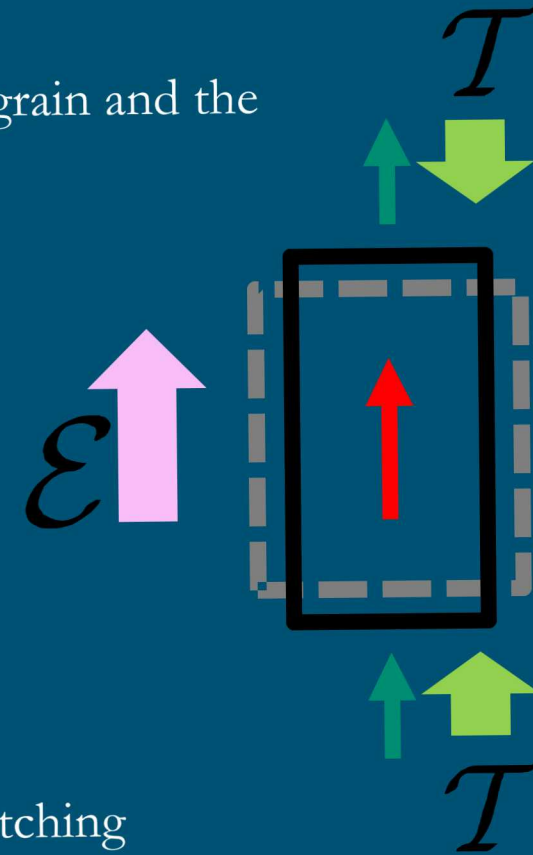
$$\mathcal{E}_m = \left(\kappa_{mn}^{\text{Matrix}} \right)^{-1} \Delta \mathcal{P}_n$$

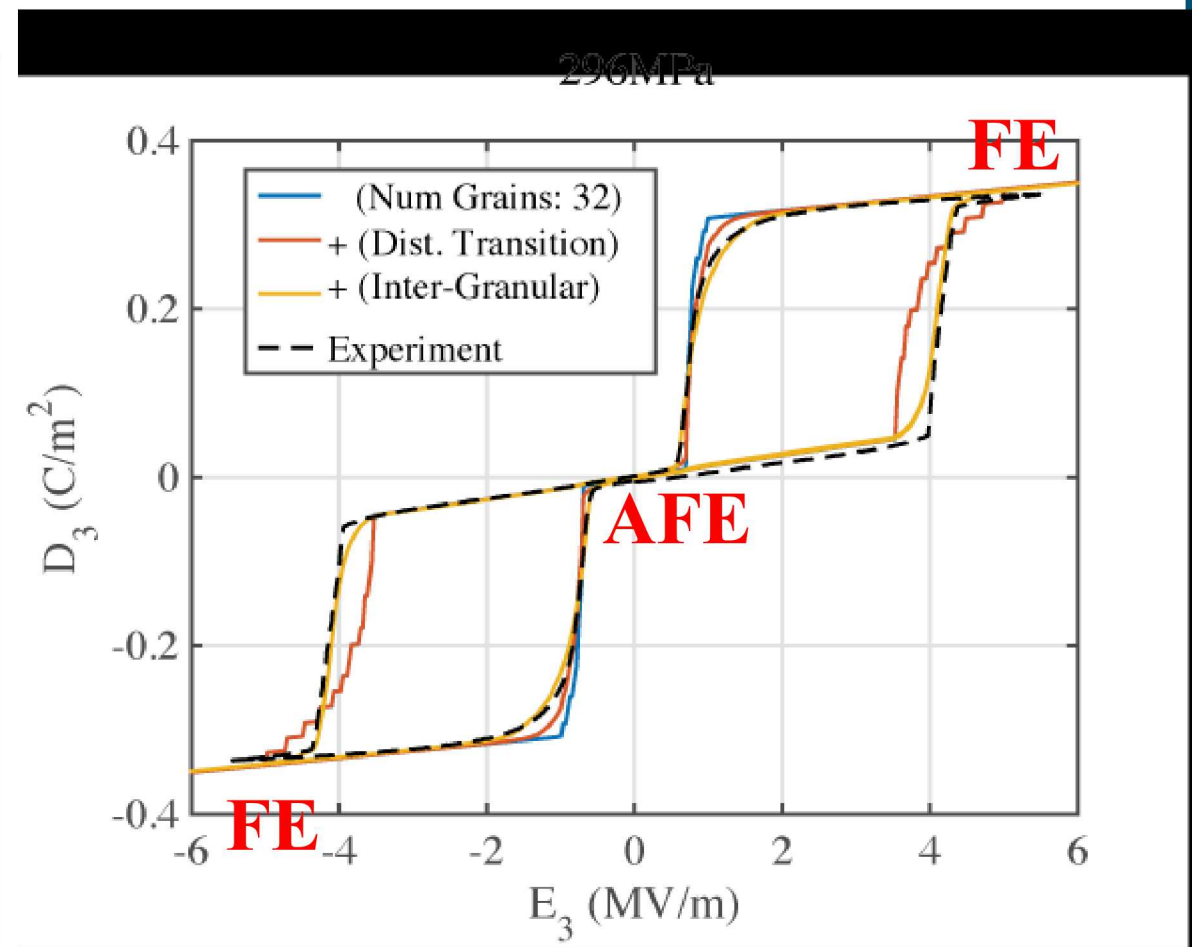
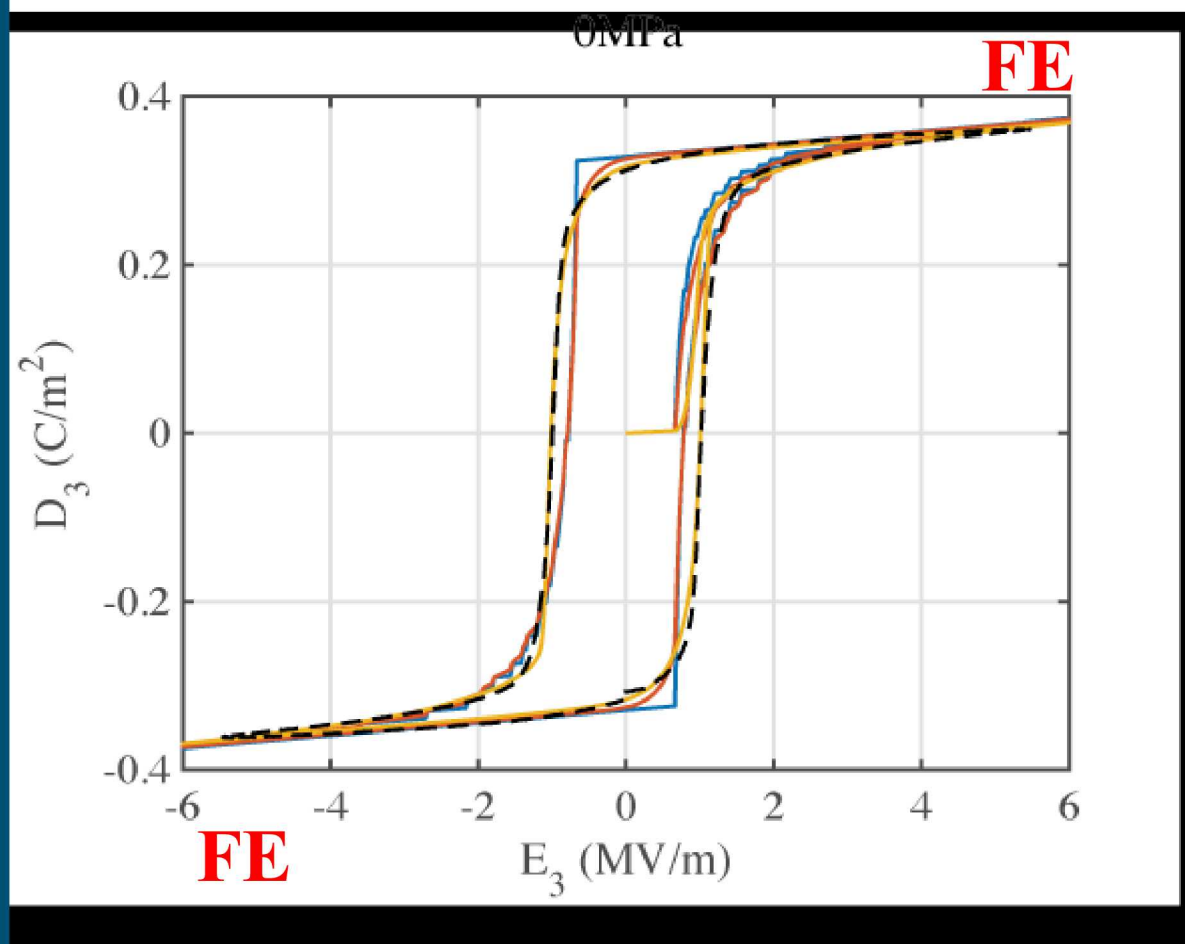
$$\mathcal{T}_{ij} = c_{ijkl}^{\text{Matrix}} \Delta \mathcal{S}_{kl}$$

Local corrected stresses and electric fields used by the switching criterion

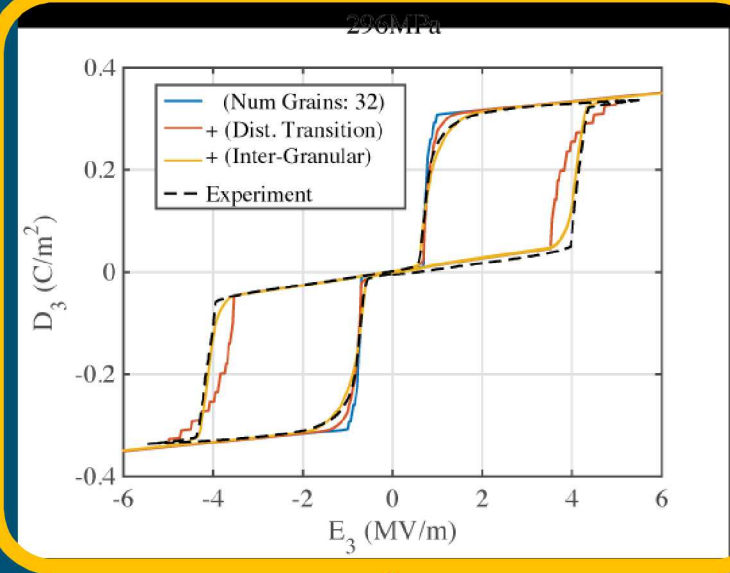
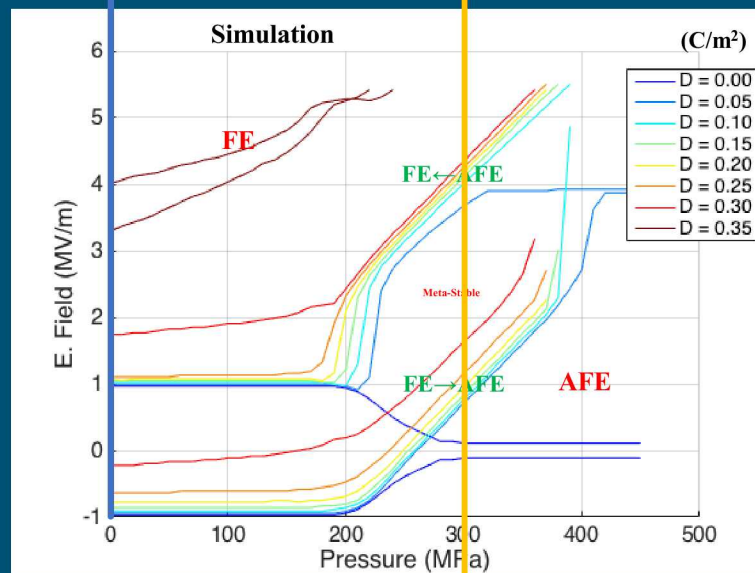
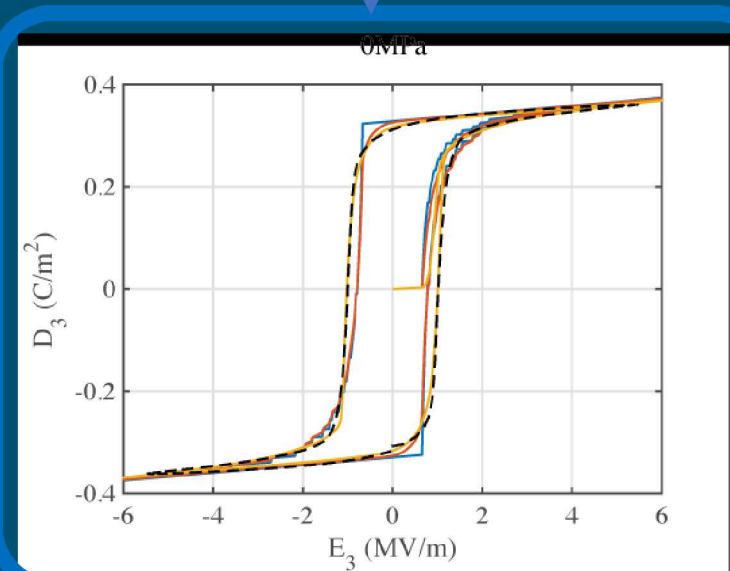
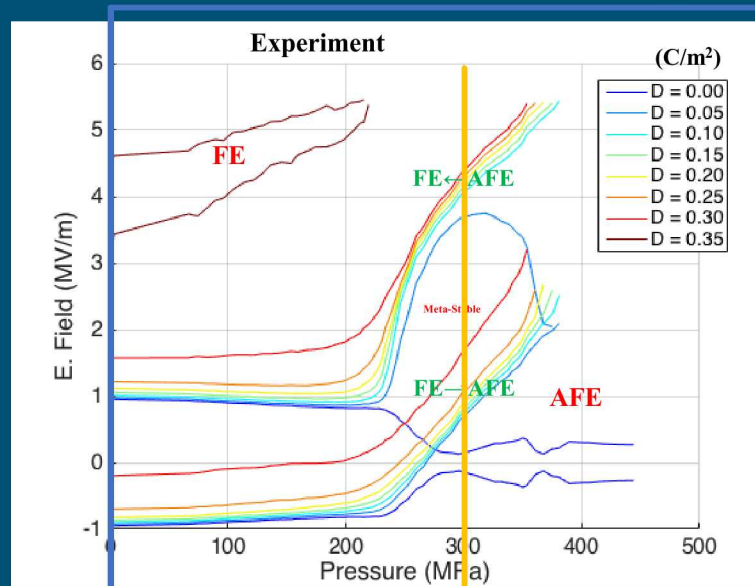
$$E_m^{\text{Local}} = E_m^{\text{Matrix}} + f_E \mathcal{E}_m$$

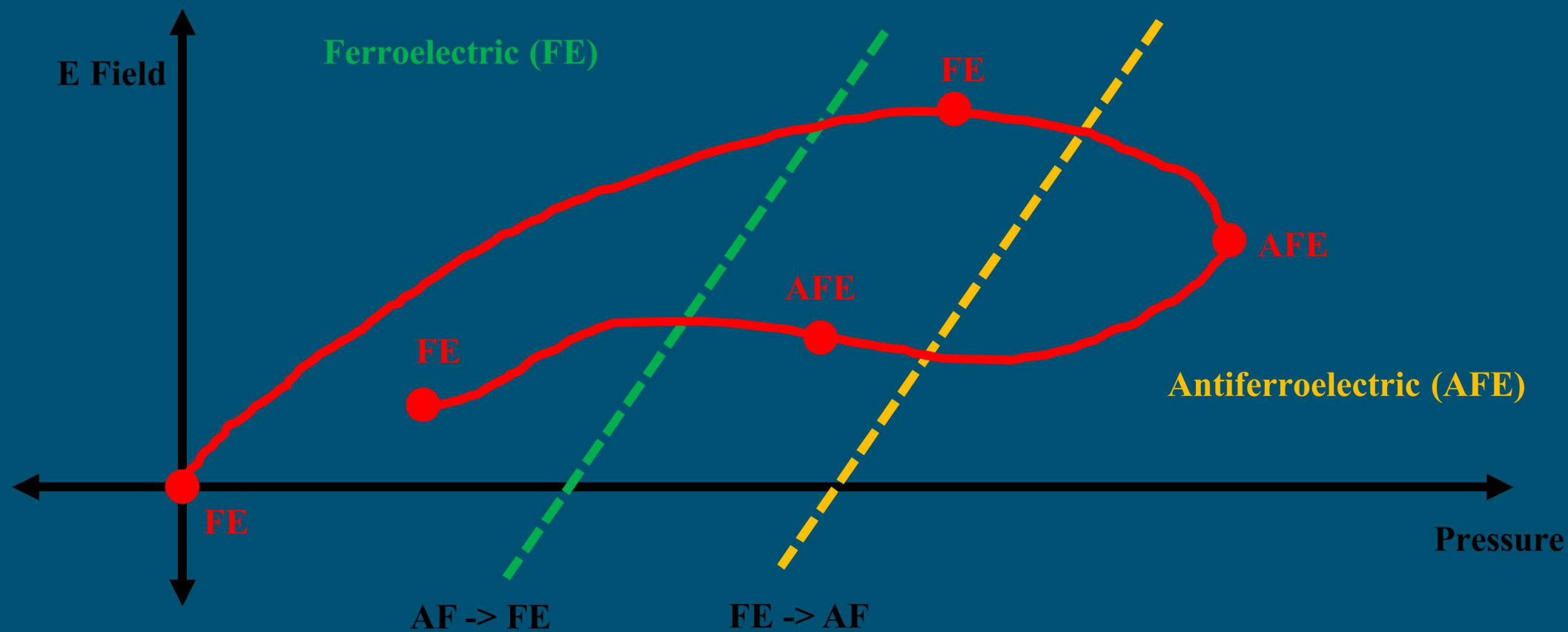
$$T_{ij}^{\text{Local}} = T_{ij}^{\text{Matrix}} + f_M \mathcal{T}_{ij}$$





Simulation of PZT95/5 – Phase Diagrams





Micromechanical approach is used to capture the heterogeneous characteristics of ceramic PZT95/5 without resolution of the microstructure.

Energy based switching criteria are used to govern both domain-switching and phase transformation transitions.

Distributed-transitions and Inter-granular interactions allow for improved capture of hysteresis behavior.

The combination of these techniques results in a model that successfully captures the domain-switching and phase transformation phenomena in ferroelectric ceramics as demonstrated in PZT95/5.