



SAND2018-6625PE

# Uncertainty Analysis of Consequence Management (CM) Data Products

AMS International Technical Exchange on  
Uncertainty in Radiological Aerial Measurements

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## Project Background

- DOE NNSA Consequence Management (CM) has been asked for many years to quantify how good (certain) our data products are
- This project is a first attempt at **quantifying uncertainty** of the Derived Response Level (DRL) values that are used for CM data products
  - DRL = a level of radioactivity in the environment that would be expected to produce a dose equal to the corresponding Environmental Protection Agency (EPA) Protective Action Guide (PAG)
- Ultimate goal is to quantify the **confidence** in the values used for **CM data products** to ensure that appropriate public and worker protection decisions are supported by defensible analysis
- Uncertainty analyses can help CM **identify major sources of uncertainty** and motivate additional studies to **minimize** these sources of uncertainty

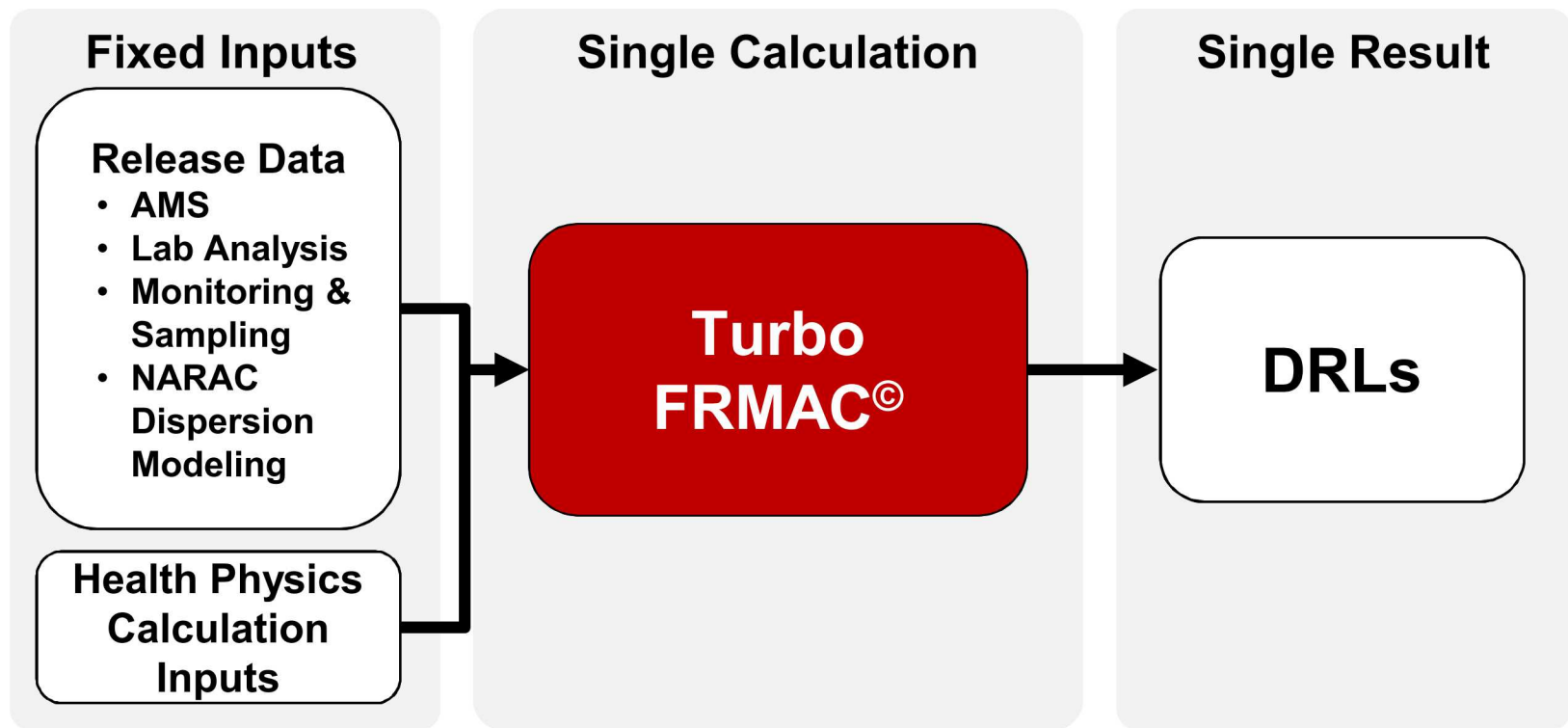
- Detonation of **Cesium-137 or Americium-241 radiological dispersal device (RDD)** on level terrain with stable wind class
- Idealized particle size distribution (particles created by detonation and atmospherically dispersed are all 1  $\mu\text{m}$  diameter)
- Source term of sufficient quantity to create an activity per area equal to the DRL at a hypothetical location downwind
- **Public Protection DRL** calculation was performed for the **Early Phase (Total Dose), Early Phase (Avoidable Dose), and First Year** time phases and used all FRMAC defaults, as specified in FRMAC Assessment Manual, Vol. 1

Scenario	Deposition DRL ( $\mu\text{Ci}/\text{m}^2$ )			
	Single Radionuclides		1:1 Mixture	
	Cs-137	Am-241	Cs-137	Am-241
Early Phase (TD)	3.30E+02	4.64E-02	4.64E-02	4.64E-02
Early Phase (AD)	1.70E+03	8.66	8.62	8.62
First Year	42.0	4.15	3.78	3.78

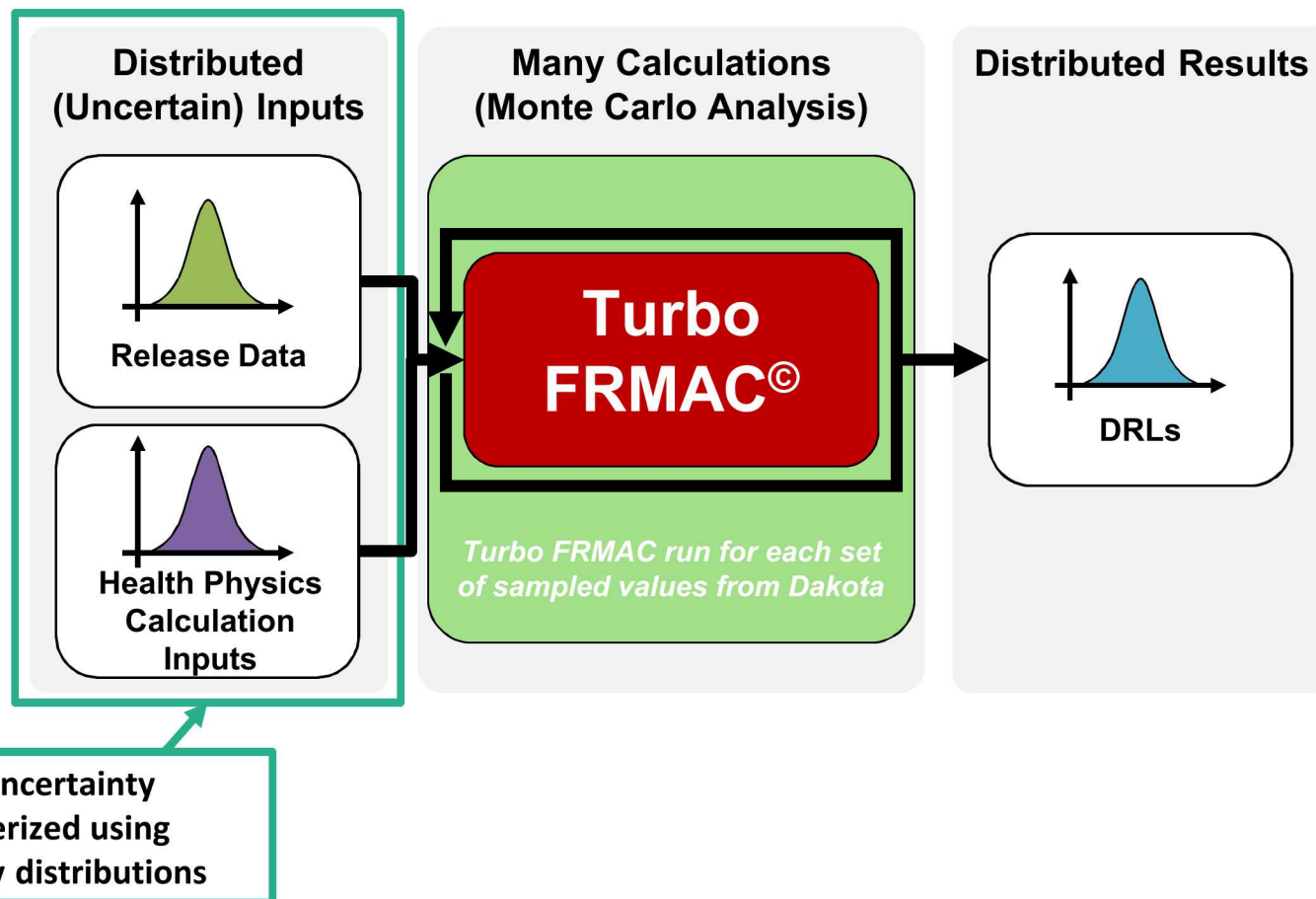
# Uncertainty Quantification Methods

- Uncertainty in context of CM
  - **Variation (error) of a measurement** from the exact value being measured; termed **uncertainty** in the fixed value of a measurement
  - **Input uncertainty leads to output uncertainty**, meaning that final DRL results are estimates of the true DRL value
- For example, suppose that the **actual** activity per area is  $330 \mu\text{Ci}/\text{m}^2$ 
  - Suppose that the laboratory measures the activity per area from a sample.  
**How much will this measurement differ from the actual value?**
  - Uncertainty in this estimate contributes to uncertainty in the final DRL estimate.  
**How close is this estimate to the actual DRL value?**
- **Monte Carlo analysis** used to characterize uncertainty

- **Response calculations** use **fixed inputs** to run a single calculation with a **single result**

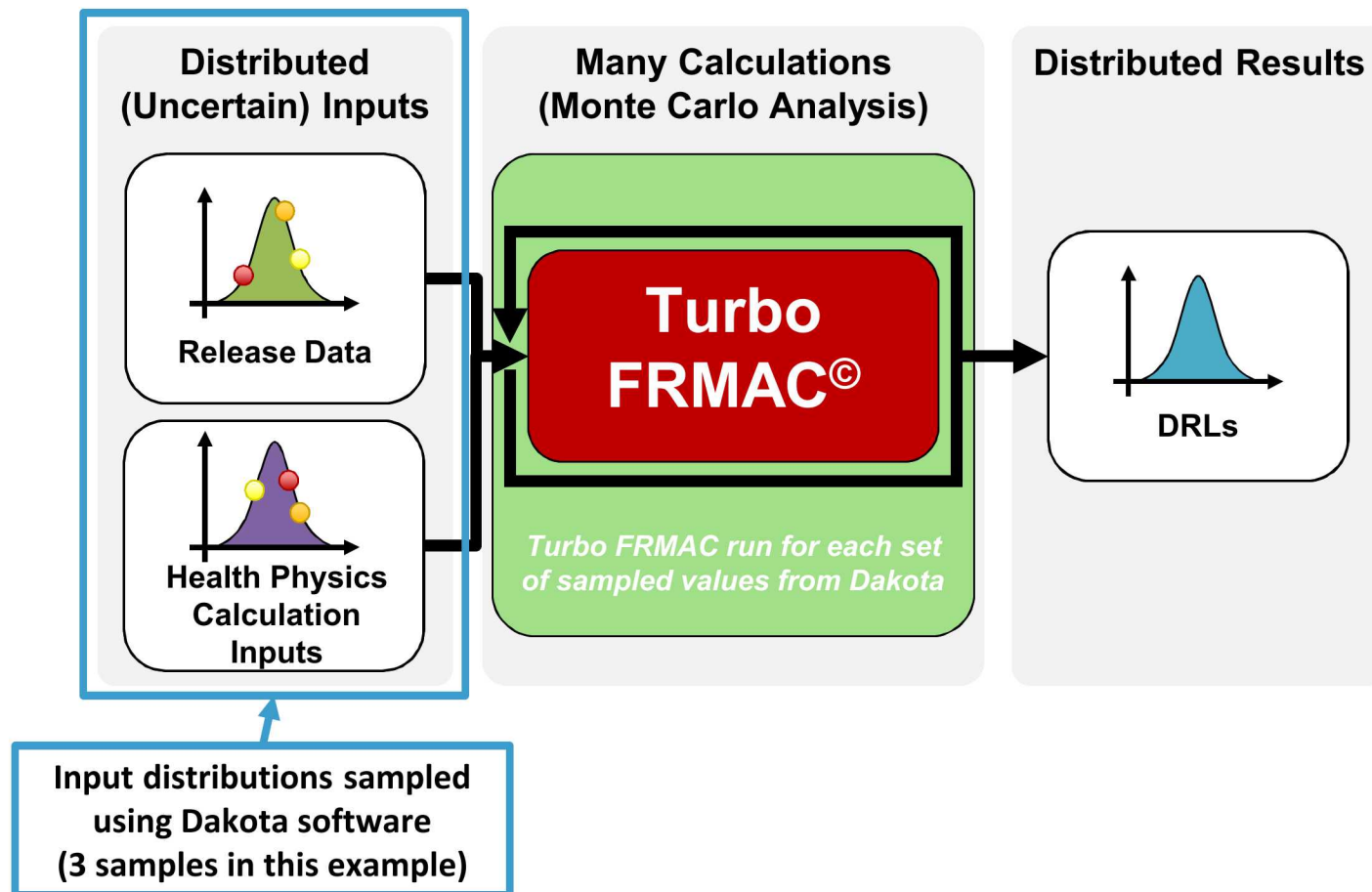


- **Monte Carlo analysis** used to **propagate uncertainty** from inputs through the model to the outputs

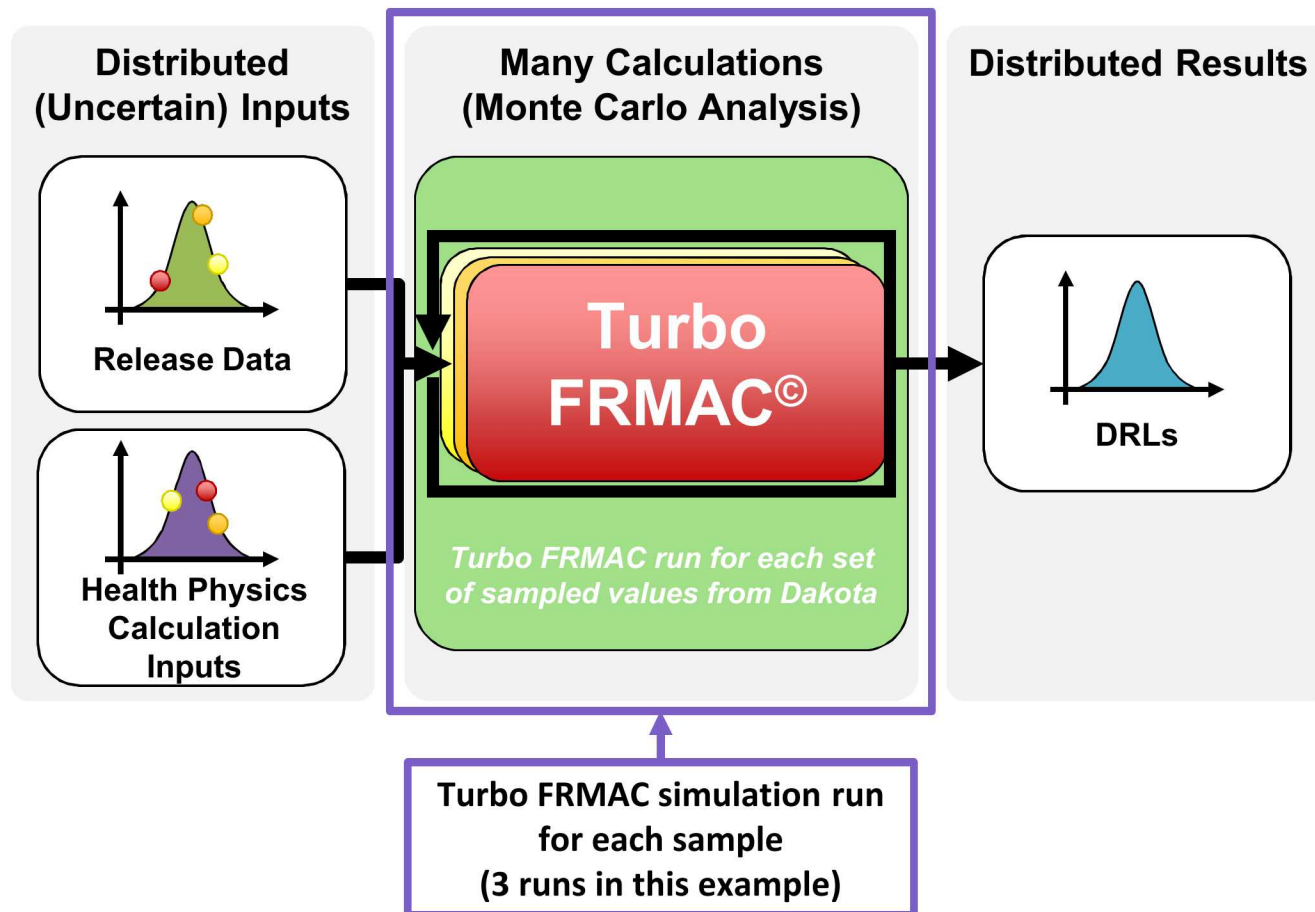




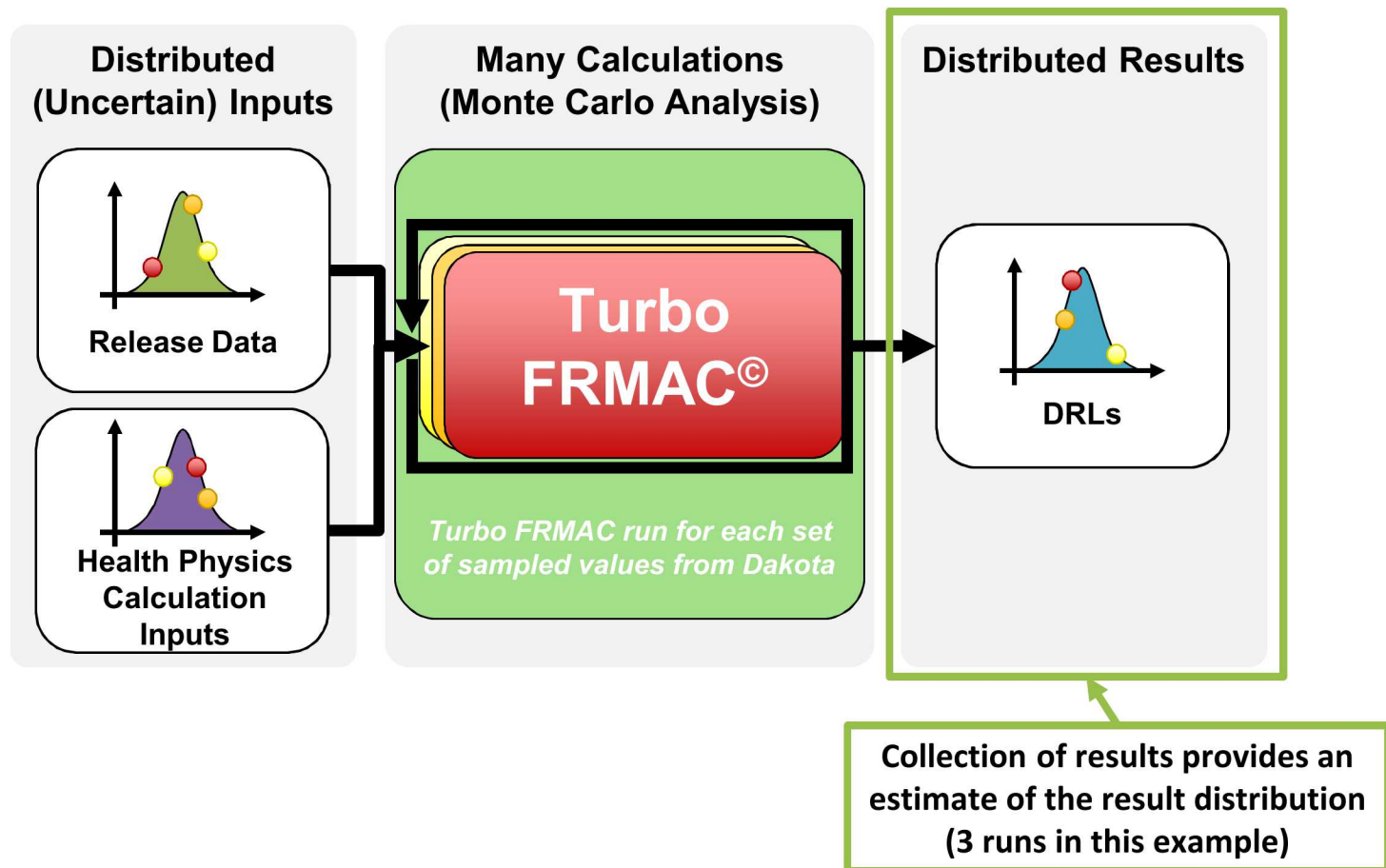
- **Input probability distributions** characterize uncertain inputs and are **sampled** using Sandia's Dakota software



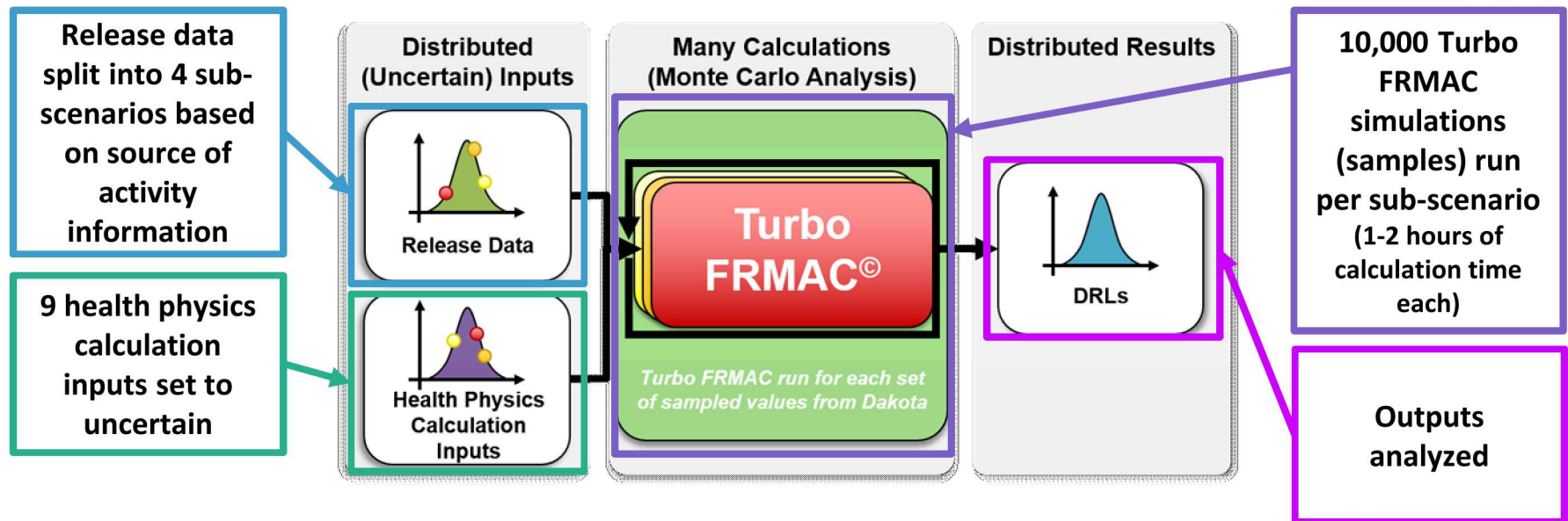
- **Turbo FRMAC** simulation run for **each sample** taken from input distributions



- **Collection of results** from each simulation provides an **estimate of the distribution** of the result of interest (DRL)



- Samples from input distributions taken using **Latin hypercube sampling (LHS)**
- A **large sample size** is needed to create a precise estimate of the output distribution
- **Turbo FRMAC updated** to read in and run each set of input samples and save all outputs for each simulation

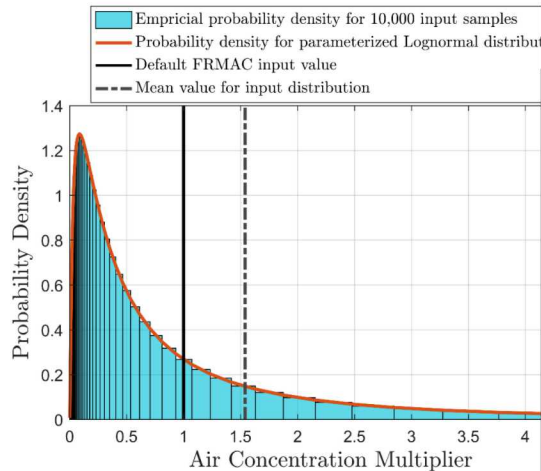


## Sources of Uncertainty

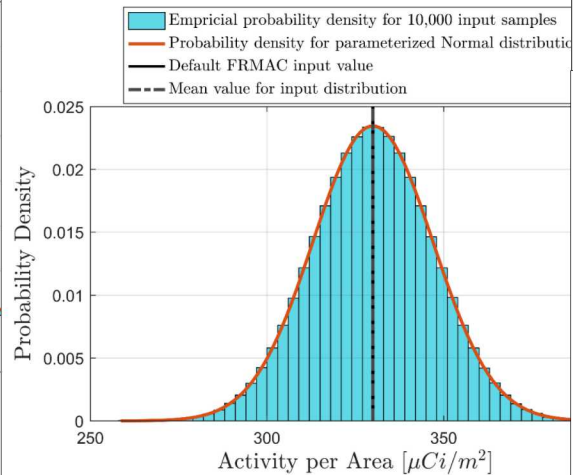
- **DRLs** are calculated based on **measured or projected** concentrations of **radionuclides** in the environment
- The **concentration sources** considered in this analysis include:
  - NARAC plume projections
  - Laboratory Analysis
  - In Situ Deposition
  - AMS measurements
- **Nine uncertain inputs** that contribute to uncertainty in the health physics calculations of Public Protection DRLs were assigned probability distributions
- **Input distributions** were **selected** based on uncertainty information from **published data and/or expert opinion**

- Distribution forms and parameters describe the **possible values** for an input and are **sampled** for each simulation
- Figures below show **examples** of assigned distributions

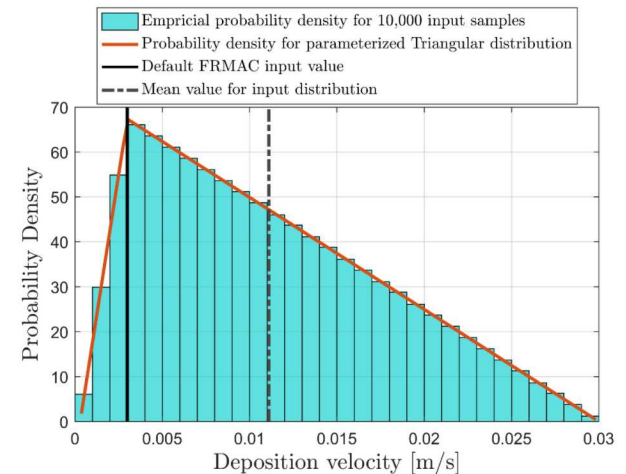
*Lognormal distribution for  
Air Concentration Multiplier*



*Normal distribution for  
Activity per Area*



*Triangular distribution for  
Deposition Velocity*



## AMS Measurement Uncertainty



- Initial processing of the data **converts the gross count rate** in the detector to a corrected equivalent net count rate at a nominal altitude:

$$N = K(N_g - N_0)e^{B(z-z_0)}$$

$K$ : Conversion factor for count rate

$N_g$ : Gross count rate in the detector during the measurement

$N_0$ : Mean count rate estimate due to airborne background radiation

$B$ : Effective attenuation coefficient

$z$ : Altitude above ground level

$z_0$ : Nominal altitude

- The uncertainty for the coefficient to convert a net count rate in the aerial system to a ground-level quantity (exposure rate, or deposition concentration) depends upon the ground and aerial measurements along a calibration line

- The **aerial components of the uncertainty** are related to the knowledge of the height above ground level (AGL) while performing the measurements at multiple altitudes (altitude spiral)
  - Radar altimeter uncertainty =  $\pm 0.7$  m
  - GPS uncertainty =  $\pm 3$  m
- The **uncertainty in the effective attenuation coefficient** results from atmospheric conditions as well as the variability of the actual flight altitudes during passes over the calibration line
  - Attenuation coefficient =  $1.674 \times 10^{-3} \text{ ft}^{-1}$  with an SD of  $4.58 \times 10^{-5} \text{ ft}^{-1}$  (2.74%)
- The **uncertainty in the raw counts in the detector**, either from the ground contamination or from the aircraft background, follow **normal statistics**

Platform	Nominal Altitude AGL	Estimated Count Rate cps/(330 $\mu\text{Ci}/\text{m}^2$ )	Background (cps)
Fixed-wing	50 m	$7.85 \times 10^5$	870
	150 m	$4.72 \times 10^5$	870
Helicopter	50 m	$3.14 \times 10^6$	3500
	150 m	$1.89 \times 10^6$	3500

- To calculate the **total uncertainty** for the aerial measurements, the contributions from the different components must be propagated:

$$\begin{aligned}\sigma_N^2 &= \sigma_K^2 (N_g - N_0)^2 e^{2B(z-z_0)} + (\sigma_{N_g}^2 + \sigma_{N_0}^2) K^2 e^{2B(z-z_0)} \\ &+ \sigma_B^2 K^2 (N_g - N_0)^2 e^{2B(z-z_0)} (z - z_0)^2 + \sigma_z^2 K^2 (N_g - N_0)^2 e^{2B(z-z_0)} B^2\end{aligned}$$

- A **simplifying assumption** is made that the aircraft is flown precisely at the nominal altitude ( $z = z_0$ )

- For extraction of a low-level Am-241 signal from the data collected with an aerial platform, a **3-window extraction process** is likely to be used
- In this process, the spectrum is broken down into three components: Am-241 signal region (36-72 keV) and two background regions (21-36 and 72-87 keV)
- A ratio,  $R$ , of the counts in the signal region ( $N_{a,0}$ ) to the counts in the background region ( $N_{b,0}, N_{c,0}$ ) is determined by data collected over an uncontaminated area:

$$R = \frac{N_{a,0}}{N_{b,0} + N_{c,0}}$$

- The ratio is used to calculate the expected counts in the signal region, in the absence of contamination. The **excess counts** in the signal region are taken to be from the contamination:

$$N_{\text{Am}} = N_a - R \times (N_b + N_c)$$

- The **extracted counts must be corrected** for the measurement altitude, and a scale factor to convert the result to an activity concentration on the ground:

$$A = K \times (N_a - R \times (N_b + N_c)) \times e^{\mu(z-z_0)}$$

$A$ : Deposited activity

$K$ : Conversion factor for the count rate at altitude  $z_0$

$\mu$ : Effective attenuation coefficient

$z$ : Altitude above ground level

$z_0$ : Nominal altitude

Platform	Nominal Altitude AGL	ROI a0 (36-72 keV)	ROI b0 (21-36 keV)	ROI c0 (72-87 keV)	Ratio	Ratio Uncertainty
Fixed-wing	50 m	841.4	140	503.2	1.31	0.069
	150 m	617.3	103.8	289.4	1.57	0.101
Helicopter	50 m	3365.7	559.9	2012.8	1.31	0.034
	150 m	3341	557.5	1827.3	1.40	0.038

- If the uncertainties are propagated in the normal manner, the variance is:

$$\begin{aligned}
 \sigma_A^2 &= \sigma_K^2 (N_a - R \times (N_b + N_c))^2 \times e^{2\mu(z-z_0)} \\
 &+ \sigma_\mu^2 K^2 (N_a - R \times (N_b + N_c))^2 e^{2\mu(z-z_0)} (z - z_0)^2 \\
 &+ \sigma_z^2 K^2 (N_a - R \times (N_b + N_c))^2 e^{2\mu(z-z_0)} \mu^2 \\
 &+ (\sigma_a^2 + R^2 \times (\sigma_b^2 + \sigma_c^2) + (N_b + N_c)^2 \times \sigma_R^2) K^2 e^{2\mu(z-z_0)},
 \end{aligned}$$

- The correction of only the count rate and its uncertainty is considered first. If the conversion factor is set to 1 and it is assumed that the mission is flown at nominal altitude ( $z = z_0$ ), the uncertainty reduces:

$$\begin{aligned}
 \sigma_A^2 &= \sigma_z^2 N_{Am}^2 \mu^2 \\
 &+ \left( (N_{Am} + N_{a,0}) + R^2 \times (N_{b,0} + N_{c,0}) + (N_{b,0} + N_{c,0})^2 \times \sigma_R^2 \right)
 \end{aligned}$$

- Uncertainties calculated using the previously described methods must then be **propagated to a ground contamination value** that includes calibration uncertainty for use in Turbo FRMAC<sup>®</sup> calculations
- $K$  is a scaling factor determined by a combination of aerial and ground measurements at a calibration area

$$K = \frac{A'}{N'} \qquad \sigma_K = \frac{A'}{N'} * \sqrt{\left(\frac{\sigma_{A'}}{A'}\right)^2 + \left(\frac{\sigma_{N'}}{N'}\right)^2}$$

- Ground contamination,  $A$ , is then calculated:

$$A = K * N \qquad \sigma_A = (K * N) * \sqrt{\left(\frac{\sigma_K}{K}\right)^2 + \left(\frac{\sigma_N}{N}\right)^2}$$

# Cs-137 and Am-241 AMS Uncertainties

Assuming Fixed Wing at 150 m AGL

## Single Radionuclide

Scenario	Cs-137			Am-241		
	Mean ( $\mu\text{Ci}/\text{m}^2$ )	Standard Deviation ( $\mu\text{Ci}/\text{m}^2$ )	Relative Error	Mean ( $\mu\text{Ci}/\text{m}^2$ )	Standard Deviation ( $\mu\text{Ci}/\text{m}^2$ )	Relative Error
Early Phase (TD)	3.30E+02	9.31	3%	4.64E-02	1.46	3148%
Early Phase (AD)	1.70E+03	47.9	3%	8.66	1.71	20%
First Year	42.0	1.27	3%	4.15	1.54	37%

## 1:1 Mixture

Scenario	Cs-137			Am-241		
	Mean ( $\mu\text{Ci}/\text{m}^2$ )	Standard Deviation ( $\mu\text{Ci}/\text{m}^2$ )	Relative Error	Mean ( $\mu\text{Ci}/\text{m}^2$ )	Standard Deviation ( $\mu\text{Ci}/\text{m}^2$ )	Relative Error
Early Phase (TD)	4.64E-02	4.81E-01	1037%	4.64E-02	1.46	3148%
Early Phase (AD)	8.62	5.34E-01	6%	8.62	1.71	20%
First Year	3.78	4.90E-01	13%	3.78	1.53	40%

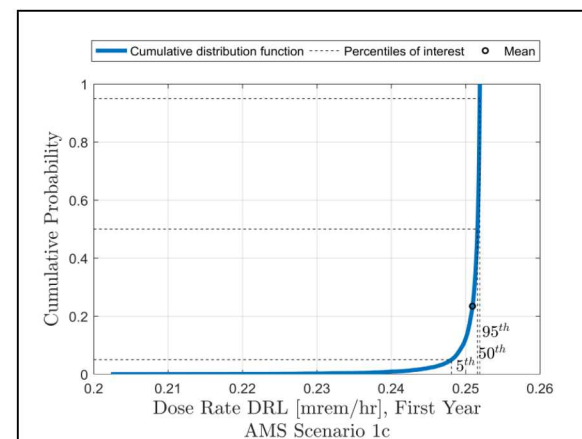
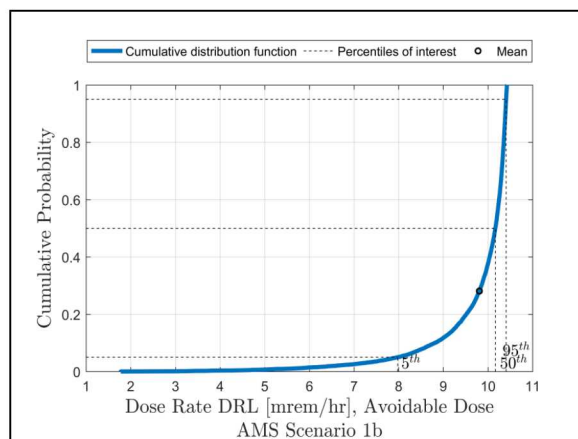
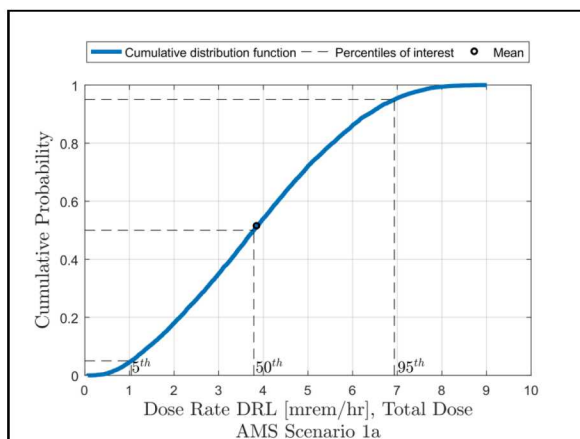


## Uncertainty Analysis Results

- Performed **10,000 simulations** to generate a set of results for each output of interest
- **Sensitivity analysis methods** tell us how much of the **uncertainty in the output** is explained by the **uncertainty in the input**
- Linear rank regression technique applied for the purposes of this project
  - **Inputs ranked in terms of importance** by standardized rank regression coefficient (SRRC) value
- **Preliminary FY18 results** using AMS measurement uncertainty are presented

## Dose Rate DRL (mrem/hr)

Scenario	Default	Mean	5th	50th	95th	Mean/ Default	95th/ 5th
Early Phase (TD)	1.98	3.857	1.043	3.786	6.934	1.94	6.65
Early Phase (AD)	10.2	9.808	7.979	10.165	10.407	0.96	1.30
First Year	0.2516	0.2509	0.2481	0.2516	0.2519	1.00	1.02



- Mean and Default DRLs are at most about a factor of 2 different
- Appears that there is little uncertainty in the Dose Rate DRL for the Early Phase (AD) and First Year time phases

- Sensitivity results show that **Deposition Velocity** is the important input when the dose includes plume inhalation
- When plume dose is not included, **groundshine** drives the dose, but the inputs are not important because they are cancelled out in the DRL ratio
- AMS measurement uncertainty associated with Cs-137 at these activity levels is **not important** to the DRL uncertainty

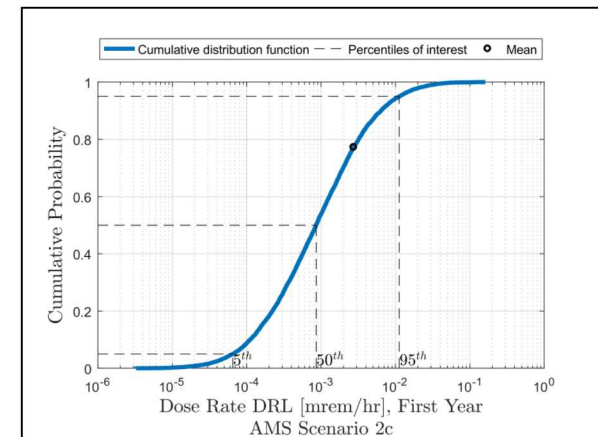
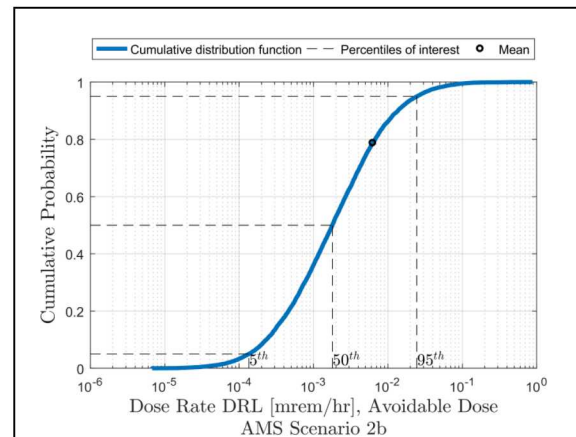
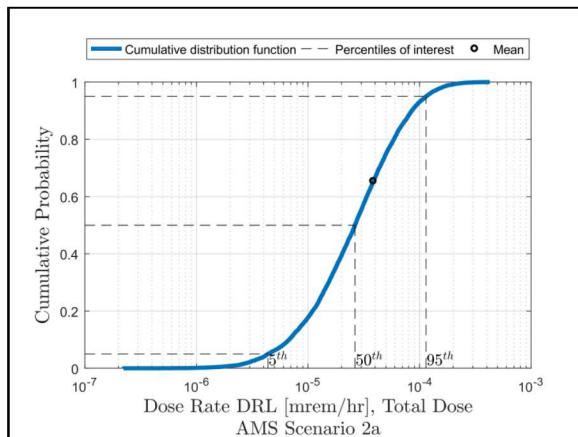
Early Phase (TD) Dose Rate DRL, $R^2 = 0.942$		
Variable Name	$R^2$	SRRC
Deposition Velocity	0.621	0.788
Cs-137 Inhalation Dose Coefficient Multiplier	0.752	-0.360
Breathing Rate, Light Exercise, Adult Male	0.820	-0.259
Deposition External Dose Coefficient Multiplier	0.886	0.258
Weathering Coefficient Multiplier	0.926	0.199
Ground Roughness Factor	0.938	0.108
Resuspension Coefficient Multiplier	0.942	-0.065
Breathing Rate, Activity Averaged, Adult Male	0.942	-0.010
Plume External Dose Coefficient Multiplier	0.942	-0.004
Cs-137 Activity per Area	0.942	0.000

Early Phase (AD) Dose Rate DRL, $R^2 = 0.984$		
Variable Name	$R^2$	SRRC
Resuspension Coefficient Multiplier	0.888	-0.941
Cs-137 Inhalation Dose Coefficient Multiplier	0.930	-0.205
Deposition External Dose Coefficient Multiplier	0.951	0.143
Breathing Rate, Activity Averaged, Adult Male	0.967	-0.129
Weathering Coefficient Multiplier	0.981	0.115
Breathing Rate, Light Exercise, Adult Male	0.984	0.000
Cs-137 Activity per Area	0.984	0.000
Deposition Velocity	0.984	0.000
Plume External Dose Coefficient Multiplier	0.984	0.000
Ground Roughness Factor	0.985	0.061

*First Year results similar to Early Phase (AD)*

## Dose Rate DRL (mrem/hr)

Scenario	Default	Mean	5th	50th	95th	Mean/ Default	95th/ 5th
Early Phase (TD)	1.10E-05	3.85E-05	4.38E-06	2.63E-05	1.14E-04	3.49	26.06
Early Phase (AD)	2.06E-03	6.26E-03	1.35E-04	1.79E-03	2.44E-02	3.04	180.16
First Year	9.89E-04	2.75E-03	6.52E-05	8.59E-04	1.12E-02	2.78	172.48



- Mean and Default DRLs are at most about a factor of 3.5 different
- The spread of the DRL distribution increases for the Early Phase (AD) and First Year time phases



- Sensitivity results show that **Deposition Velocity** is the important input when the dose includes plume inhalation
- When plume dose is not included, **resuspension inhalation** drives the dose, so those inputs become important
- AMS measurement uncertainty associated with Am-241 at these activity levels is **not important** to the DRL uncertainty

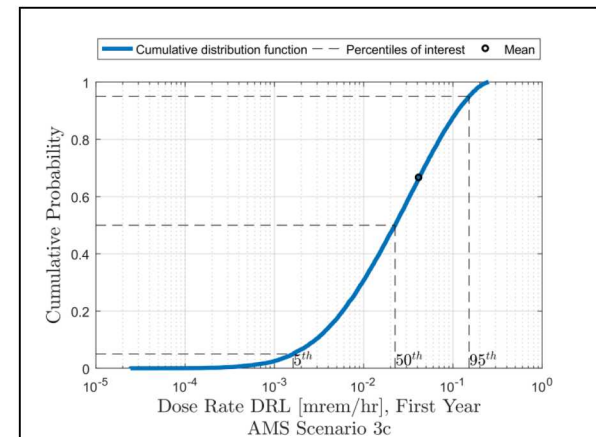
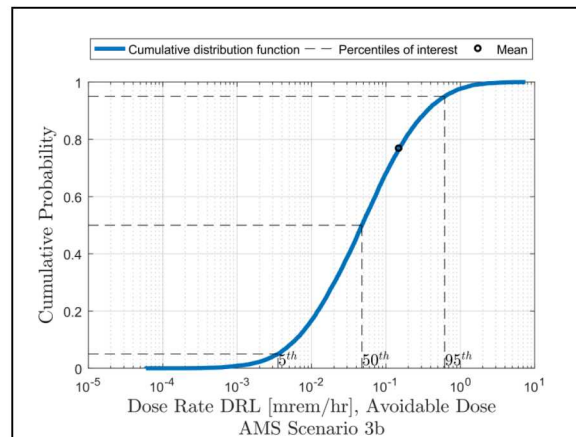
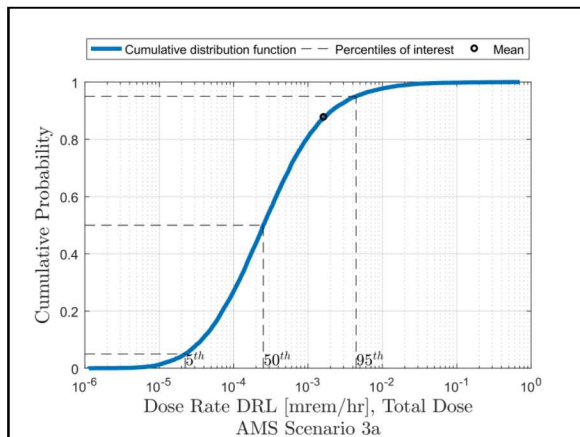
Early Phase (TD) Dose Rate DRL, $R^2 = 0.940$		
Variable Name	$R^2$	SRRC
Deposition Velocity	0.481	0.693
Am-241 Inhalation Dose Coefficient Multiplier	0.791	-0.556
Breathing Rate, Light Exercise, Adult Male	0.845	-0.230
Deposition External Dose Coefficient Multiplier	0.897	0.228
Weathering Coefficient Multiplier	0.928	0.176
Ground Roughness Factor	0.937	0.096
Resuspension Coefficient Multiplier	0.940	-0.058
Am-241 Activity per Area	0.940	0.000
Plume External Dose Coefficient Multiplier	0.940	0.000
Breathing Rate, Activity Averaged, Adult Male	0.940	-0.009

Early Phase (AD) Dose Rate DRL, $R^2 = 0.977$		
Variable Name	$R^2$	SRRC
Resuspension Coefficient Multiplier	0.812	-0.900
Am-241 Inhalation Dose Coefficient Multiplier	0.927	-0.338
Deposition External Dose Coefficient Multiplier	0.945	0.137
Breathing Rate, Activity Averaged, Adult Male	0.961	-0.123
Weathering Coefficient Multiplier	0.973	0.111
Ground Roughness Factor	0.977	0.059
Breathing Rate, Light Exercise, Adult Male	0.977	0.000
Am-241 Activity per Area	0.977	0.000
Deposition Velocity	0.977	0.000
Plume External Dose Coefficient Multiplier	0.977	0.000

*First Year results similar to Early Phase (AD)*

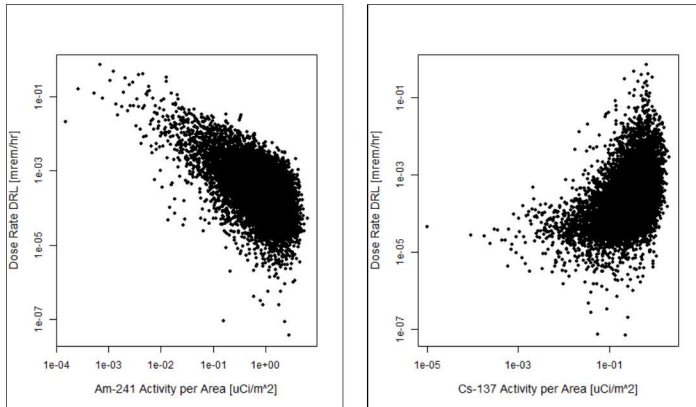
## Dose Rate DRL (mrem/hr)

Scenario	Default	Mean	5th	50th	95th	Mean/ Default	95th/ 5th
Early Phase (TD)	2.89E-04	1.64E-03	2.23E-05	2.51E-04	4.42E-03	5.67	197.90
Early Phase (AD)	5.37E-02	1.50E-01	3.54E-03	4.75E-02	6.15E-01	2.79	173.71
First Year	2.36E-02	4.17E-02	1.62E-03	2.25E-02	1.52E-01	1.77	93.46



- Mean and Default DRLs are at most about a factor of 6 different
- Greatest spread of this DRL is associated with the Early Phase (TD) scenario using the 1:1 mixture of Cs-137:Am-241

- Sensitivity results show that Am-241 and Cs-137 measurement uncertainty is **very important** for the Early Phase (TD) scenario



- When plume dose is not included, Am-241 **resuspension inhalation** drives the dose, so those inputs become important

Early Phase (TD) Dose Rate DRL, $R^2 = 0.892$		
Variable Name	$R^2$	SRRC
Am-241 Activity per Area	0.274	-0.524
Cs-137 Activity per Area	0.521	0.499
Deposition Velocity	0.715	0.439
Am-241 Inhalation Dose Coefficient Multiplier	0.835	-0.346
Breathing Rate, Light Exercise, Adult Male	0.856	-0.144
Deposition External Dose Coefficient Multiplier	0.874	0.137
Weathering Coefficient Multiplier	0.888	0.116
Ground Roughness Factor	0.891	0.057
Cs-137 Inhalation Dose Coefficient Multiplier	0.892	0.007
Resuspension Coefficient Multiplier	0.892	-0.035

Early Phase (AD) Dose Rate DRL, $R^2 = 0.974$		
Variable Name	$R^2$	SRRC
Resuspension Coefficient Multiplier	0.798	-0.892
Am-241 Inhalation Dose Coefficient Multiplier	0.910	-0.336
Deposition External Dose Coefficient Multiplier	0.929	0.137
Breathing Rate, Activity Averaged, Adult Male	0.944	-0.122
Am-241 Activity per Area	0.957	-0.116
Weathering Coefficient Multiplier	0.969	0.110
Ground Roughness Factor	0.972	0.055
Breathing Rate, Light Exercise, Adult Male	0.974	0.000
Cs-137 Inhalation Dose Coefficient Multiplier	0.974	0.000
Deposition Velocity	0.974	0.000

*First Year results similar to Early Phase (AD)*



- FY17-18 accomplishments:
  - Developed a **comprehensive method** to assess overall uncertainty of the values used for CM data products
  - **Identified uncertainty distributions** for Public Protection DRL inputs
  - Developed an **automated process** that utilizes **Turbo FRMAC and Dakota** software to perform uncertainty analyses for Assessment calculations
- **Uncertainty analyses** for study scenarios using the developed framework are currently underway
  - Preliminary results indicate that measurement uncertainty is important to DRL results when there is more than one radionuclide in the mixture and the associated uncertainty is large enough
- Need to determine if/how uncertainty analysis results can be used to **inform protective action decisions**

Thank you!

Questions?

Additional Slides

Input	Default Value	Distribution Type	Mean	SD	Mode	Lower Bound	Upper Bound	Units
Deposition Velocity	3.00E-3	Triangular			3.00E-3	3.00E-4	3.00E-2	m/s
Breathing Rate – Light Exercise, Adult Male	1.50	Normal	1.75	0.42		0.54	3.00	m <sup>3</sup> /hr
Breathing Rate – Activity-Averaged, Adult Male	0.92	Triangular			0.92	0.54	1.50	m <sup>3</sup> /hr
Ground Roughness Factor	0.82	Normal	0.82	0.082		0	1	--
Resuspension Coefficient Multiplier <sup>‡</sup>	1	Lognormal <sup>+</sup>	1	4.2				--
Weathering Coefficient Multiplier <sup>‡</sup>	1	Lognormal <sup>+</sup>	1	1.2				--
Deposition External Dose Coefficient Multiplier	1	Triangular			0.8	0.5	1.5	--
Inhalation Dose Coefficient Multiplier – Cs-137 <sup>§</sup>	1	Lognormal <sup>+</sup>	1	1.5				--
Inhalation Dose Coefficient Multiplier – Am-241	1	Lognormal <sup>+</sup>	1	2.0				--
Plume External Dose Coefficient Multiplier	1	Triangular			0.8	0.5	1.5	--

\* This uncertainty multiplier is multiplied by a user-defined air concentration value to sample air concentration with uncertainty. This distribution is calculated from the comparison of NARAC predictions to experimental data.

+ The means and standard deviations (SD) listed for lognormal distributions on this table are the geometric mean and geometric standard deviation, respectively. The lognormal distribution is defined by parameters  $\mu$ , the mean of the natural logarithm of the data, and  $\sigma$ , the standard deviation of the natural logarithm of the data. Then, the geometric mean ( $GM$ ) is given by  $GM = e^{\mu}$  and the geometric standard deviation ( $GSD$ ) is given by  $GSD = e^{\sigma}$ .

‡ These multipliers are to be applied only to the coefficients outside the exponentials in the Resuspension and Weathering Factors

§ This multiplier is specifically for Cs-137, Type F, Effective (Whole Body). Ba-137m is present at equilibrium with Cs-137 at the start of the time phase. The uncertainty in the Ba-137m inhalation dose coefficient is neglected because its ingrowth from Cs-137 over the dose commitment period dominates the delivered dose. The Cs-137 inhalation dose coefficient accounts for dose and uncertainty from the ingrowth of Ba-137m. (per communication with Keith Eckerman on May 10, 2017)

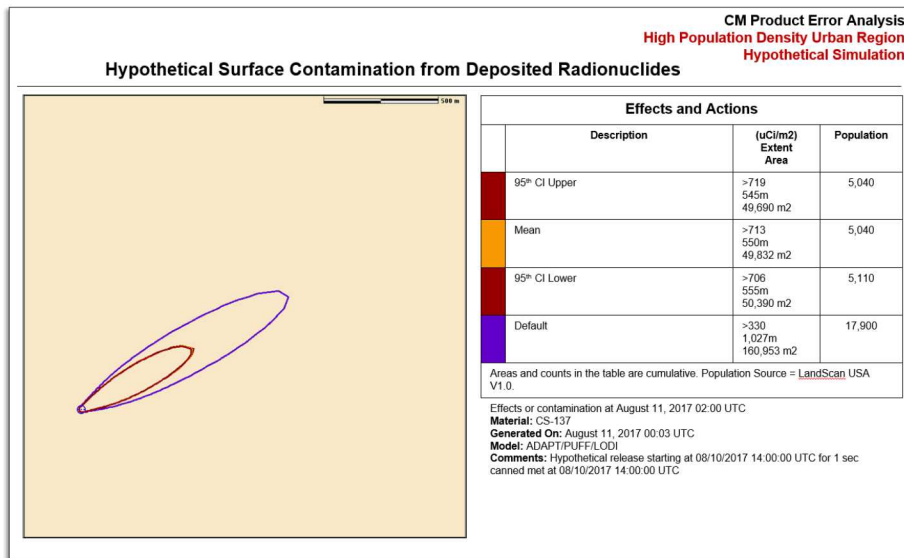
Input	Reference
Air Concentration Uncertainty Multiplier – NARAC	Developed in collaboration with FRMAC scientists at RSL and NARAC
Activity per Area – In Situ	
Activity per Area – AMS	
Activity per Area – Laboratory Analysis	
Deposition Velocity	<i>Evaluation of Severe Accident Risks: Quantification of Major Input Parameters</i> , NUREG/CR-4551, Vol. 2, Rev. 1, Part 7, U.S. Nuclear Regulatory Commission, Washington, DC, 1990
Breathing Rate – Light Exercise, Adult Male	Developed using information from 2011 EPA Exposure Factors Handbook
Breathing Rate – Activity-Averaged, Adult Male	Based on approach used by RESRAD for a similar parameter - <i>Development of Probabilistic RESRAD 6.0 and RESRAD-BUILD 3.0 Computer Codes</i> , NUREG/CR-6697, ANL/EAD/TM-98, Argonne National Laboratory, Argonne, IL, 2000
Ground Roughness Factor	No uncertainty information available. Developed based on 10% measurement uncertainty described in Beck, H.L., <i>Exposure Rate Conversion Factors for Radionuclides Deposited on the Ground</i> , EML-378, U.S. Department of Energy Environmental Measurements Laboratory, New York, NY, 1980
Resuspension Coefficient Multiplier	Maxwell, R. and Anspaugh, L., “An Improved Model for Prediction of Resuspension” in <i>Health Physics</i> , Vol. 101, pp. 722-730, December 2011
Weathering Coefficient Multiplier	No uncertainty information available. Developed based on information in Anspaugh reference: Golikov, V.Y., Balonov, M.I., Jacob, P., “External Exposure of the Population Living in Areas of Russia Contaminated Due to the Chernobyl Accident” in <i>Radiat Environ Biophys</i> , Vol. 41, pp. 185-193, 2002
Deposition External Dose Coefficient Multiplier	Eckerman, K., <i>Radiation Dose and Health Risk Estimation: Technical Basis for the State-of-the-Art Reactor Consequence Analysis Project</i> , Oak Ridge National Laboratory, Oak Ridge, TN, 2012
Inhalation Dose Coefficient Multiplier	
Plume External Dose Coefficient Multiplier	Assigned per conversation with Keith Eckerman on March 20, 2017

## Convergence Results for Dose Rate DRL

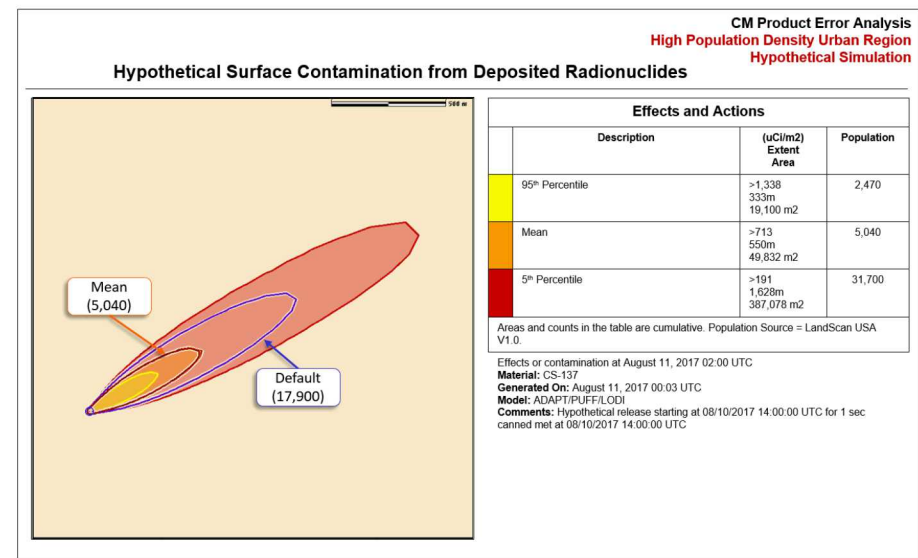
Scenario	Lower Bound of 95% CI	Mean	Upper Bound of 95% CI
Early Phase (TD) – Cs-137	3.82	3.86	3.89
Early Phase (AD) – Cs-137	9.79	9.81	9.83
First Year – Cs-137	0.25088	0.25093	0.25097
Early Phase (TD) – Am-241	3.78E-05	3.85E-05	3.93E-05
Early Phase (AD) – Am-241	5.87E-03	6.26E-03	6.67E-03
First Year – Am-241	2.62E-03	2.75E-03	2.89E-03
Early Phase (TD) – 1:1	1.38E-03	1.64E-03	1.91E-03
Early Phase (AD) – 1:1	0.143	0.150	0.157
First Year – 1:1	4.08E-02	4.17E-02	4.27E-02

- **95% Confidence Intervals (CI)** are interpreted as follows: ‘there is a 95% confidence that the true value of the mean falls within this interval.’

- The following **example data products** use the **uncertainty analysis results** for the Cs-137 Deposition DRL from the FY17 NARAC simulations



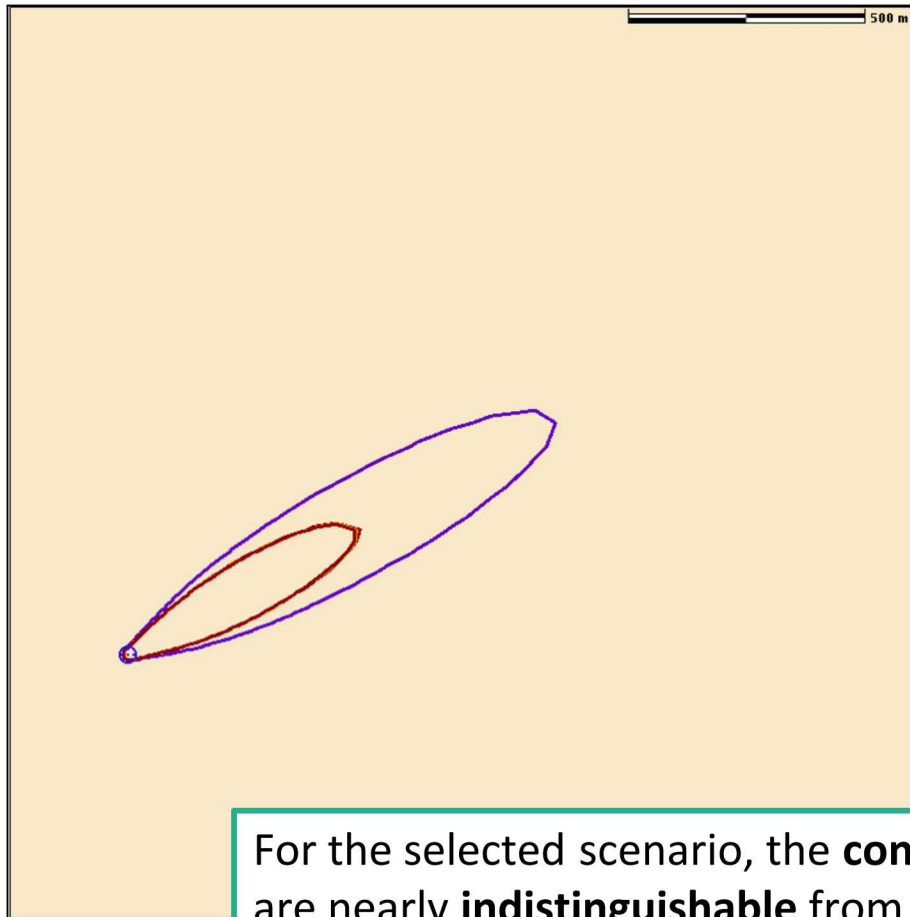
**Confidence intervals**  
characterize sampling uncertainty



**5<sup>th</sup> and 95<sup>th</sup> percentiles**  
describe uncertainty in result of interest



## Hypothetical Surface Contamination from Deposited Radionuclides



Effects and Actions			
	Description	(uCi/m2) Extent Area	Population
	95 <sup>th</sup> CI Upper	>719 545m 49,690 m2	5,040
	Mean	>713 550m 49,832 m2	5,040
	95 <sup>th</sup> CI Lower	>706 555m 50,390 m2	5,110
	Default	>330 1,027m 160,953 m2	17,900

Areas and counts in the table are cumulative. Population Source = LandScan USA V1.0.

Effects or contamination at August 11, 2017 02:00 UTC

**Material:** CS-137

**Generated On:** August 11, 2017 00:03 UTC

**Model:** ADAPT/PUFF/LODI

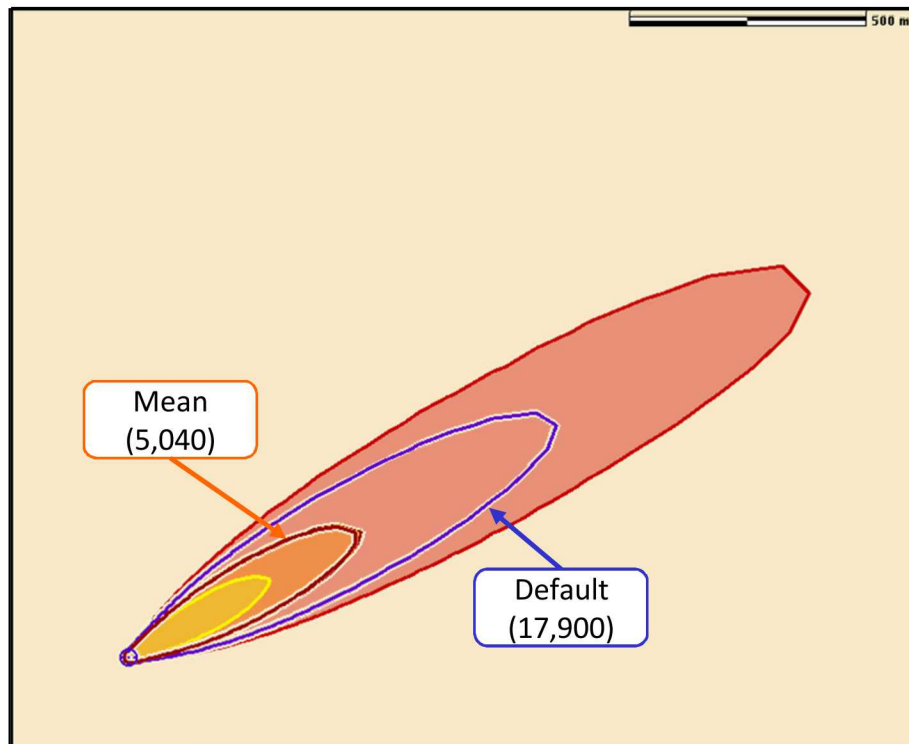
**Comments:** Hypothetical release starting at 08/10/2017 14:00:00 UTC for 1 sec  
canned met at 08/10/2017 14:00:00 UTC

For the selected scenario, the **confidence interval (CI) contours** are nearly **indistinguishable** from the mean contour

- CIs calculated using non-parametric bootstrap approach
- CI results demonstrate that the sampling method and sample size used for this analysis **adequately capture the uncertainty in the mean**



## Hypothetical Surface Contamination from Deposited Radionuclides



Effects and Actions			
	Description	(uCi/m²) Extent Area	Population
	95 <sup>th</sup> Percentile	>1,338 333m 19,100 m²	2,470
	Mean	>713 550m 49,832 m²	5,040
	5 <sup>th</sup> Percentile	>191 1,628m 387,078 m²	31,700

Areas and counts in the table are cumulative. Population Source = LandScan USA V1.0.

Effects or contamination at August 11, 2017 02:00 UTC

Material: CS-137

Generated On: August 11, 2017 00:03 UTC

Model: ADAPT/PUFF/LODI

Comments: Hypothetical release starting at 08/10/2017 14:00:00 UTC for 1 sec  
canned met at 08/10/2017 14:00:00 UTC

For the selected scenario, the **default DRL** contour covers **nearly three times** the area covered by the **mean DRL** contour

- Protective action recommendations **based on default method** would result in a **significantly larger impacted population** when compared to the mean
- Distribution of DRL values** represented by **5<sup>th</sup> and 95<sup>th</sup> percentiles** shows that **extreme values** encompassing areas that are **much larger and much smaller** than the default, respectively, are possible