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# Determining series resistance for equivalent circuit models of a PV module

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**MODELING COLLABORATIVE**



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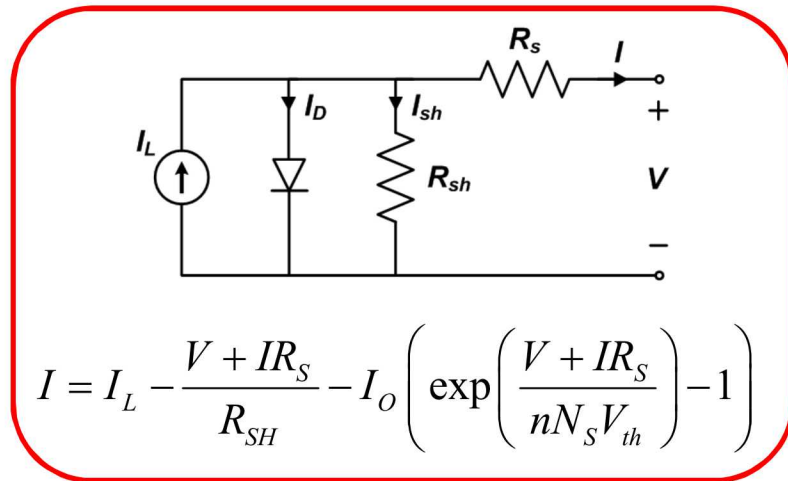
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# Outline

- Background on single diode PV models
- Describe methods to ‘measure’ series resistance for a PV device
- Show that measured series resistance differs from the  $R_s$  parameter for the single diode model
- Outline a method to determine the  $R_s$  parameter, and
- Compare with the methods to measure series resistance

# Equivalent circuit models

- Most popular PV performance models use a **single diode equivalent circuit** model (Pvsyst, CEC model, PlantPredict, Helioscope, PV\*SOL, etc.)



## Single diode equation

Describes a single IV curve using 5 parameters

$$I_L(E, T_C) = \frac{E}{E_0} \left[ I_{L0} + \alpha_{Isc} (T_C - T_0) \right]$$

$$I_O = I_{O0} \left( \frac{T_C}{T_0} \right)^3 \exp \left( \frac{1}{k} \left( \frac{E_{g0}}{T_0} - \frac{E_g(T_C)}{T_C} \right) \right)$$

$$R_{sh} = R_{sh0} \frac{E_0}{E} \quad R_s, n \text{ constant}$$

## Auxiliary equations

Describe how 5 parameters change with irradiance and temperature (e.g., De Soto model)

Single diode equation + Auxiliary equations = PV performance model

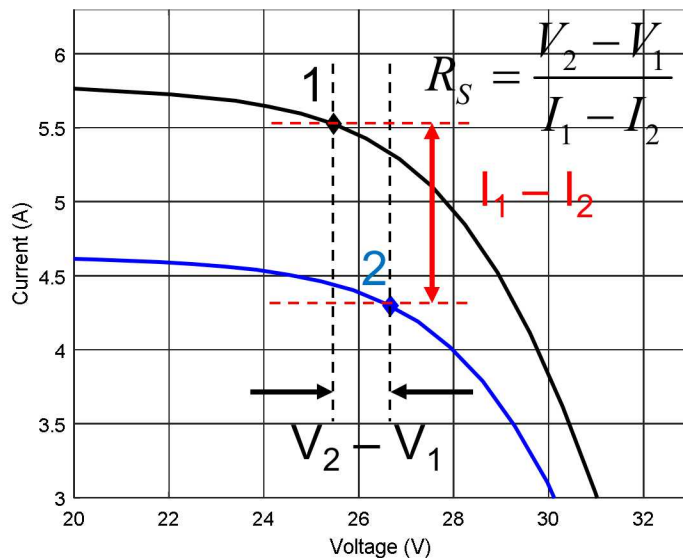
# Parameters for single diode models

- Most often parameters are determined by optimization
  - E.g., CEC model (in SAM) [Dobos] simultaneously determines parameters by fitting STC IV curve at  $I_{sc}$ ,  $P_{mp}$  and  $V_{oc}$ , and matching temperature coefficients
  - Pvsyst provides a user-driven utility to determine parameters by visually matching inputs (e.g., measured IV curve, datasheet values)
- Parameters determined by optimization are **implicitly linked** with other parameter values
  - Different optimization objectives will return different parameter sets
  - A parameter set may replicate the IV curve but individual values may lack physical meaning

*Methods to find individual parameters would be of significant value for model verification and module analysis*

# Techniques to “measure” $R_s$

- We examine six methods from literature [Pysch] to find  $R_s$  from a small number of IV curves: *Swanson*, *Bowden*, *suns-Voc*, *Pysch*, *IEC60891-1*, *IEC60891-2*
- E.g., *Swanson* uses two IV curves at different irradiances and same temperature
  - *Bowden* similar to *Swanson*
  - *Pysch* = *Swanson* with more IV curves
  - *suns-Voc* compares an IV curve to the *suns-Voc* curve
  - IEC 60891 method translate an IV curve to a target irradiance and temperature
  - Translation involves an  $R_s$  quantity



# We tested the Rs methods

- Simulate IV curves using the CEC model for representative cSi, CdTe modules
  - Irradiance from 400 to 1100 W/m<sup>2</sup>
  - Temperature 25, 35, 45
  - With and without noise on current (N(0, 0.15%))
- Recover Rs value by applying each method to simulated IV curves

TABLE I. CEC MODEL PARAMETERS FOR THE SIMULATED MODULES

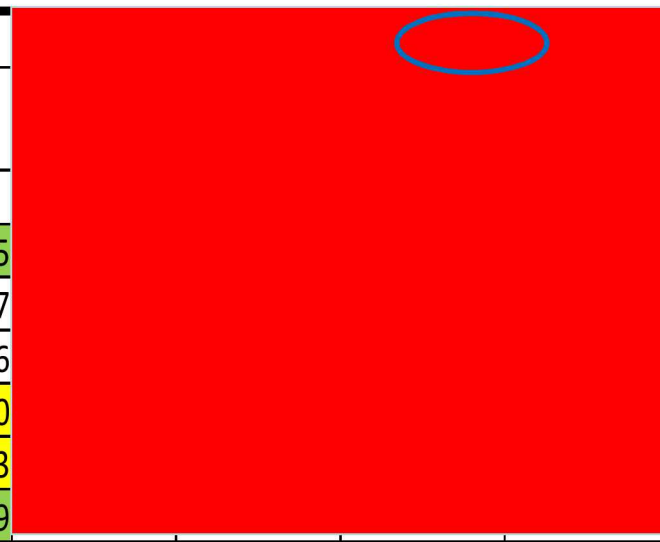
Parameter	cSi 240W	CdTe 72W
$I_{L0}$	8.0 A	1.15 A
$\alpha_{Isc}$	0.8 mA/K	0.35 mA/K
<i>Adjust</i>	0.0	0.0
$I_{O0}$	0.5 nA	0.3 nA
$E_{g0}$	1.121 eV	1.475 eV
$R_{S0}$	0.2 $\Omega$	0.5 $\Omega$
$R_{SH0}$	1000 $\Omega$	800 $\Omega$
$n_0$	1.05	1.40
$N_s$ (cells in series)	60	114

TABLE II. ESTIMATED Rs VALUES FOR SIMULATED MODULES AT STC

Rs method	cSi: true Rs value <b>0.2000 <math>\Omega</math></b>			
	No noise	With noise (100 replicates)		
		5th	Mean	95th
Bowden	0.2051	0.2031	0.2054	0.2085
Swanson	0.2694	-0.2054	0.2244	0.5187
Pysch	0.2584	0.0881	0.2352	0.4076
suns-Voc	0.2144	0.2031	0.2129	0.2230
IEC60891-1	0.2129	0.1992	0.2147	0.2273
IEC60891-2	0.1989	0.1798	0.1985	0.2159

Error < 3%,  
but **biased**

Error < 10%,  
but **biased**



# Why the failure to recover Rs?

Rs estimators (e.g., Swanson) are approximations of the single diode equation

- Omitted terms involve other parameters:  $R_{SH}$ ,  $n$ ,  $I_0$

1. Solve the single diode equation for  $V = V(I)$

$$V = (I_L + I_O - I)R_{SH} - IR_S - nN_S V_{th} W(\psi(I)), \quad \psi(I) = \frac{I_O R_{SH}}{nN_S V_{th}} \exp\left(\frac{(I_L + I_O - I)R_{SH}}{nN_S V_{th}}\right)$$

2. Substitute into  $V_2 - V_1$  and solve for Rs

$$R_S \approx \frac{V_2 - V_1}{I_1 - I_2} - \frac{nN_S V_{th}}{I_1 - I_2} \left( \ln \frac{R_{SH1}}{R_{SH2}} + \ln \frac{\ln \xi_2}{\ln \xi_1} + \text{other terms} \right), \quad \xi_1 = \frac{I_{O1} R_{SH1}}{nN_S V_{th}} \exp\left(\frac{(I_{SC1} - I_1)R_{SH1}}{nN_S V_{th}}\right)$$

Approximation  
of Rs

Difference between  
approximate and true value

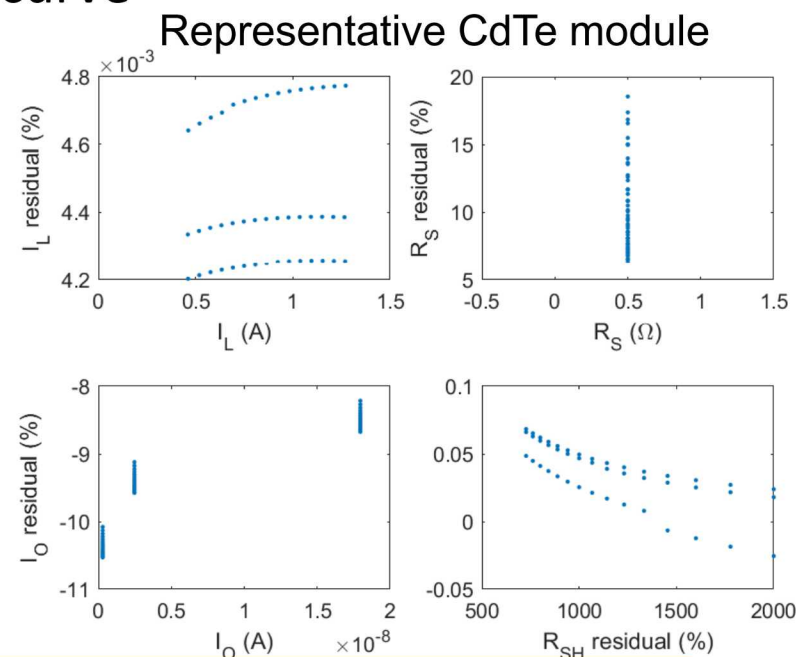
Explains bias

Approximation error increases with larger  $n$ ,  $N_s$  (CdTe module), smaller  $I_1 - I_2$  (Swanson method)

# Joint estimation of all 5 parameters

- Simplification of Sandia method [Hansen]
- Simulate a set of 45 IV curves ( $G = 400\text{-}1100\text{ W/m}^2$ ;  $T_c = \{25\ 35\ 45\}$ )
- Recover 5 parameters for each IV curve

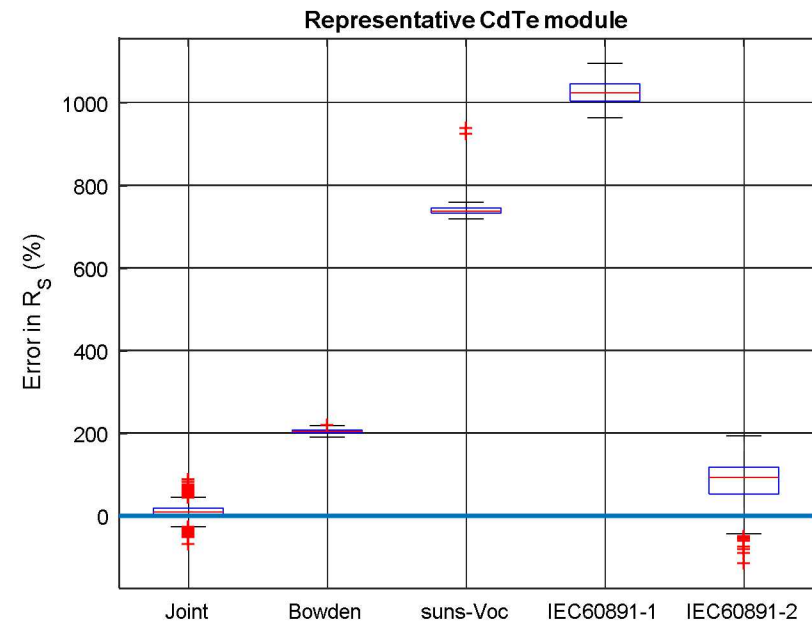
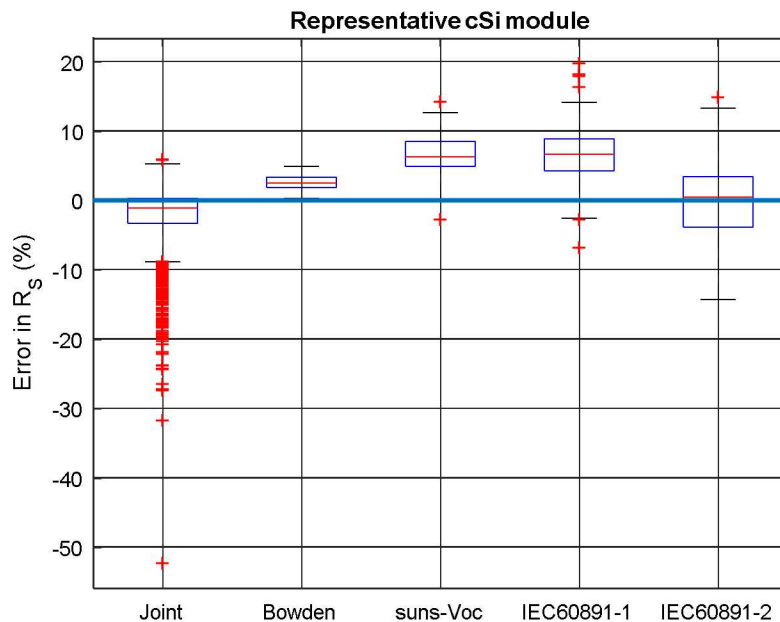
1. Determine  $n$  by regressing  $V_{oc}$  onto  $G$  ( $\text{W/m}^2$ )
  - a. Uses a set of IV curves
2. For each IV curve, find  $R_{SH}$  from slope near  $I_{sc}$
3. For each IV curve, start with  $I_L \approx I_{sc}$ 
  - a. Calculate  $I_o$ ,  $R_s$  (see paper)
  - b. Update  $I_L$  (see paper)
  - c. Iterate a few times



Parameters are recovered with error  $<10\%$  but  
Errors are sensitive to small changes in estimated  $n$

# Joint estimation vs Rs methods

- For cSi, joint estimation method is comparable to Rs methods
  - Error less biased, sensitivity to error similar
- For CdTe, joint estimation method provides reasonable results; other methods fail



# Conclusions

- Methods to ‘measure’ series resistance (e.g., Swanson’s technique) do not reliably recover the  $R_s$  parameter for the single diode model
- The ‘measured’ series resistance values are affected by diode and shunt currents
- We conclude that the  $R_s$  parameter should be determined jointly with other diode model parameters
  - Caution must be taken to verify accuracy of optimization methods
  - Recommend testing methods by recovering known values from simulated IV curves