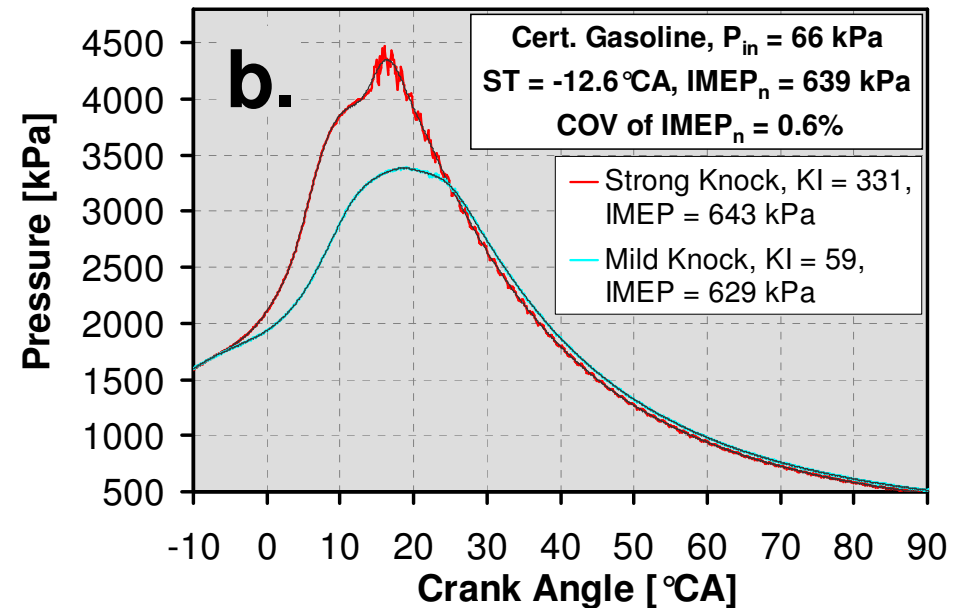
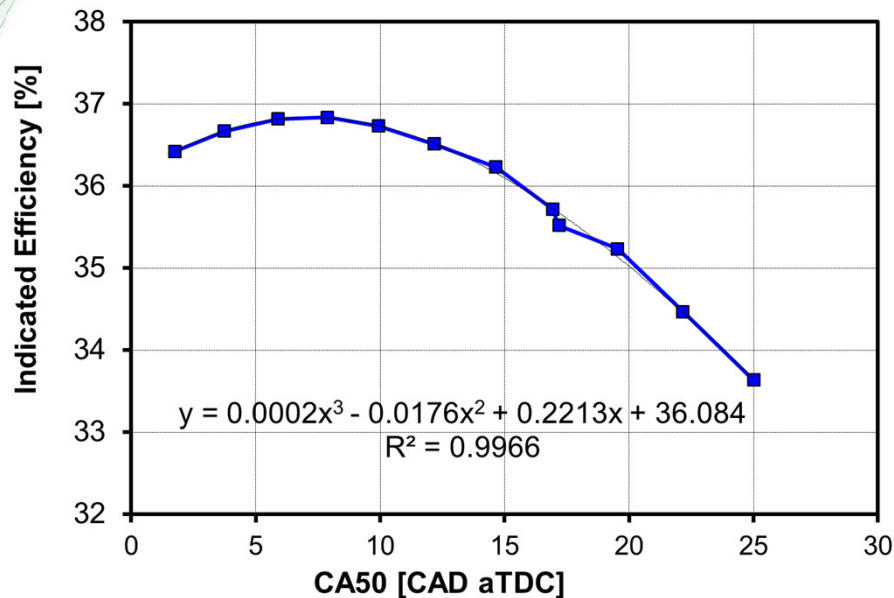


The Use of Transient Operation to Evaluate Fuel Effects on Knock Limits Well Beyond RON Conditions in Spark-Ignition Engines

David Vuilleumier and Magnus Sjöberg
Sandia National Laboratories

2017-01-2234

Introduction



- Efficient operation of SI engines requires combustion phasing near $10^\circ CA$.
- In practice, knocking significantly inhibits SI engine efficiency by forcing delayed combustion phasing.
- Knocking also prevents increases in engine compression ratio.
- Anti-knock quality of fuel is important.

Fuels Matrix

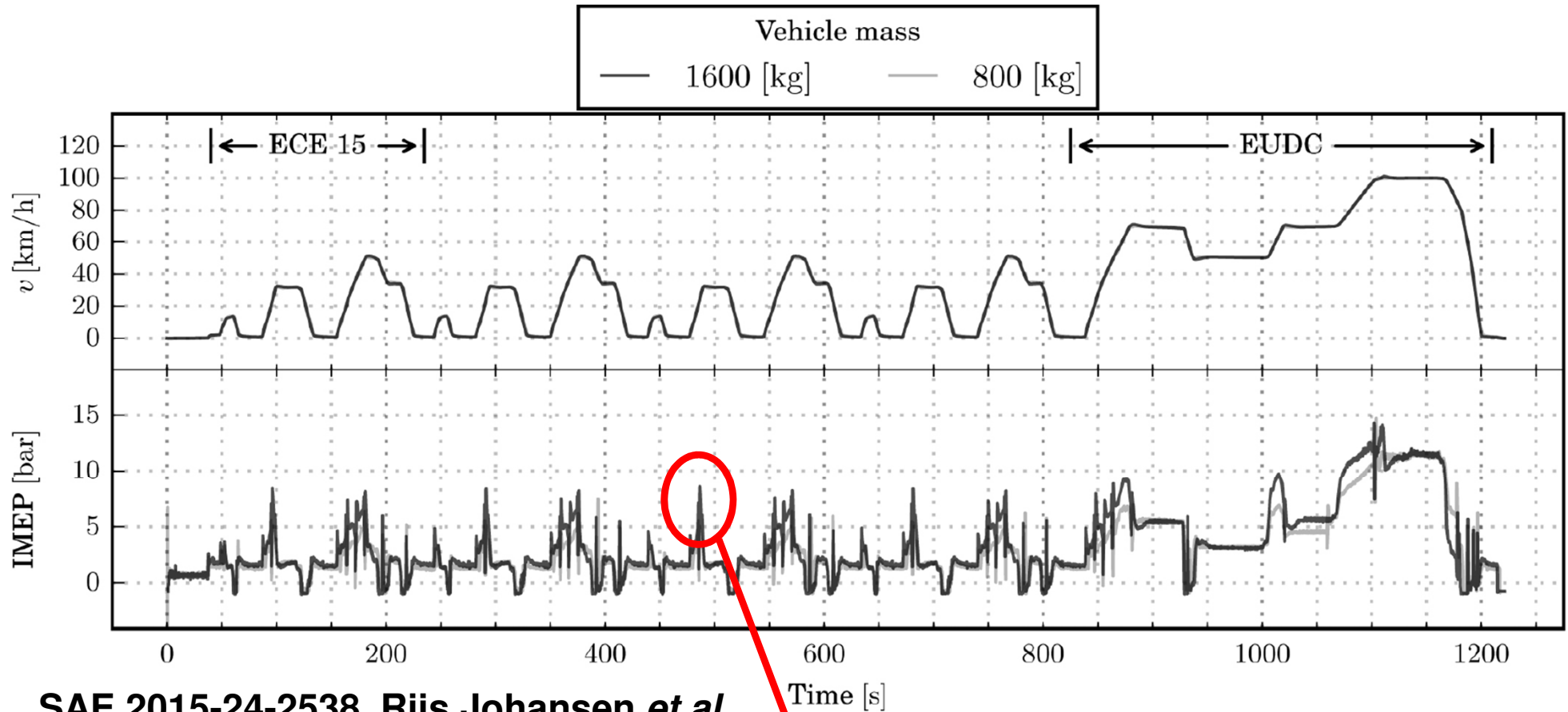
- Customer selects fuel based on AKI or RON.
- However, RON and MON are both important.
- Here, study three RON = 98 fuels, and one regular E10 gasoline.
- $S = \text{RON} - \text{MON}$.
- Octane sensitivity and composition vary greatly.



	E10 RD5-87	Alkylate	E30	High Aromatic
S	7	1	10	11
RON	92	98	98	98
MON	85	97	88	87
Ethanol [vol.%]	11	0	30	0
Aromatics [vol.%]	21	0	8	31
T90 [°C]	?	106	155	158

Relevance of RON & MON for Transients?

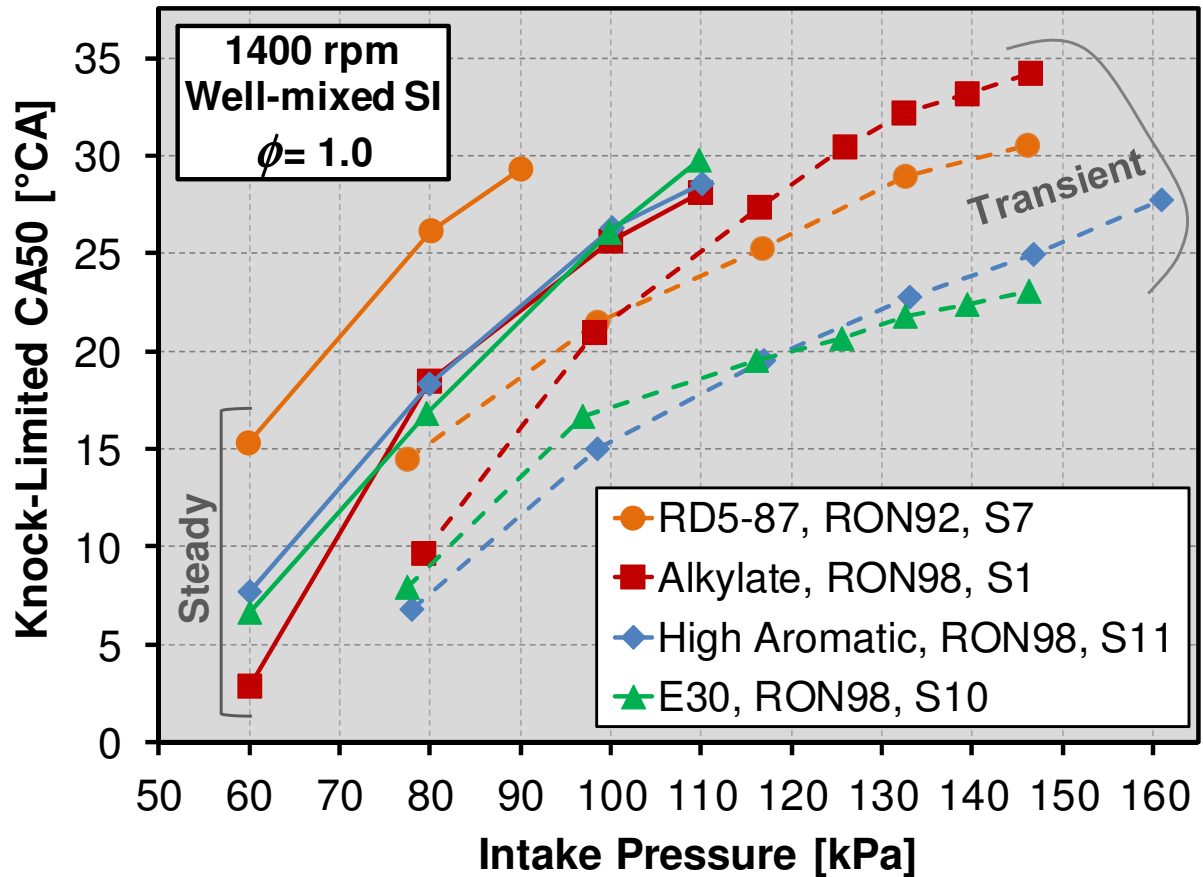
- RON and MON are determined for steady-state conditions.
- Actual vehicle operation is usually not steady-state.



SAE 2015-24-2538, Riis Johansen *et al.*

- What is the relevance of RON and MON for load transients?

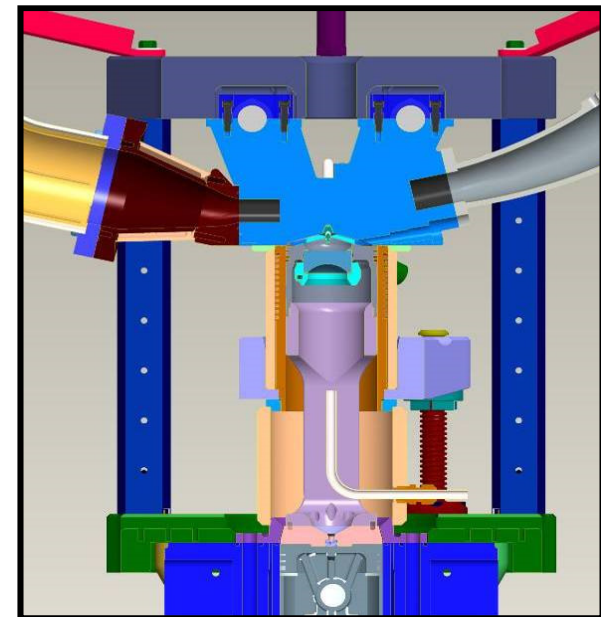
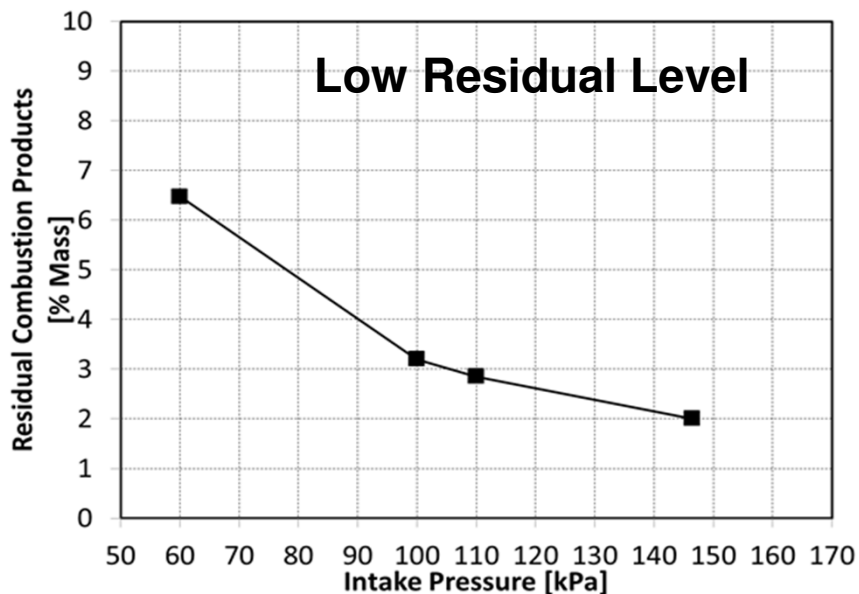
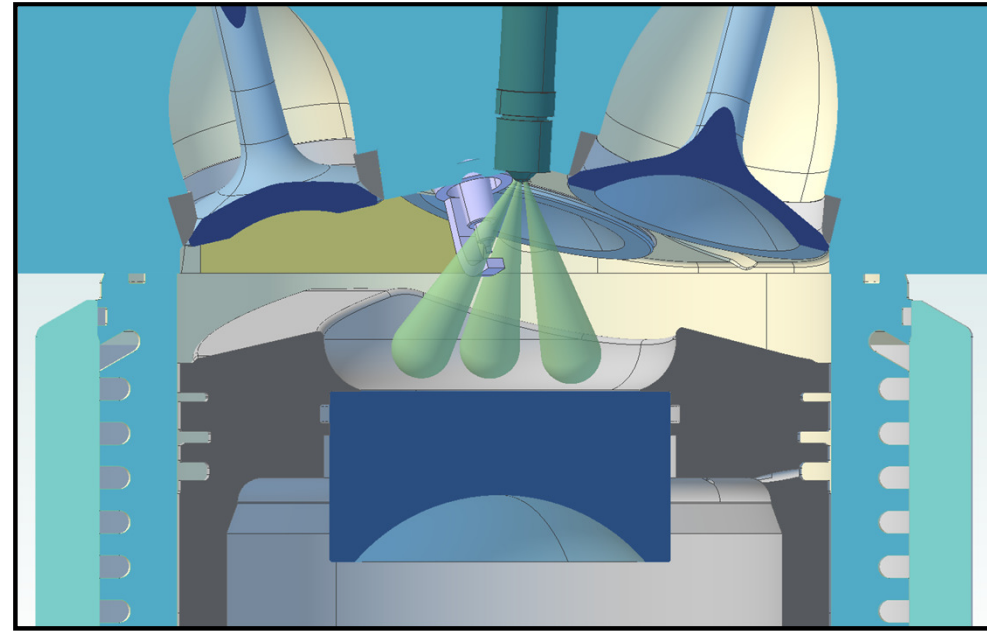
Load-Transient Operation Reveals Benefit of High-S Fuels



- Steady-state: RON98 fuels overlap for $P_{in} = 100$ kPa.
- Acquire load-transient data as well.
 - Thermally analogous to a temporary increase of load from idle \Rightarrow cooler than steady state.
- High-S fuels provide strong knock suppression for transient operation.
- May be highly beneficial for vehicle acceleration.

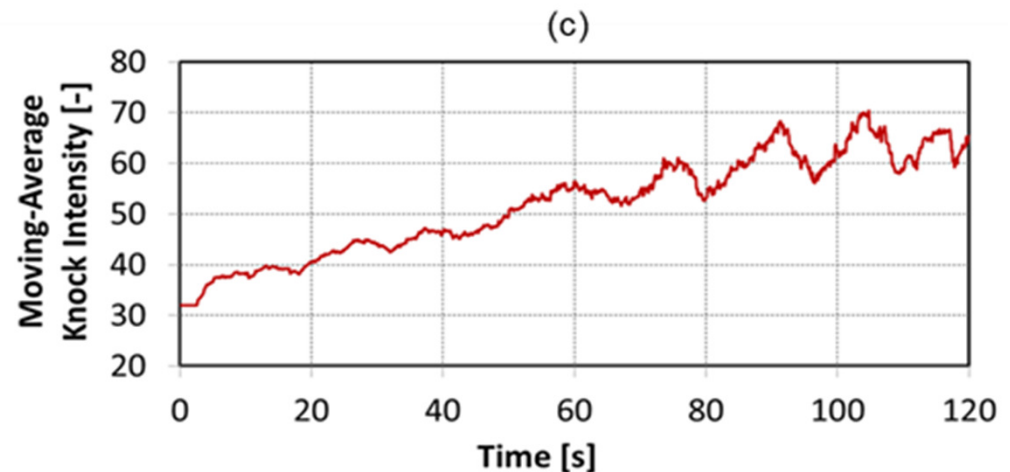
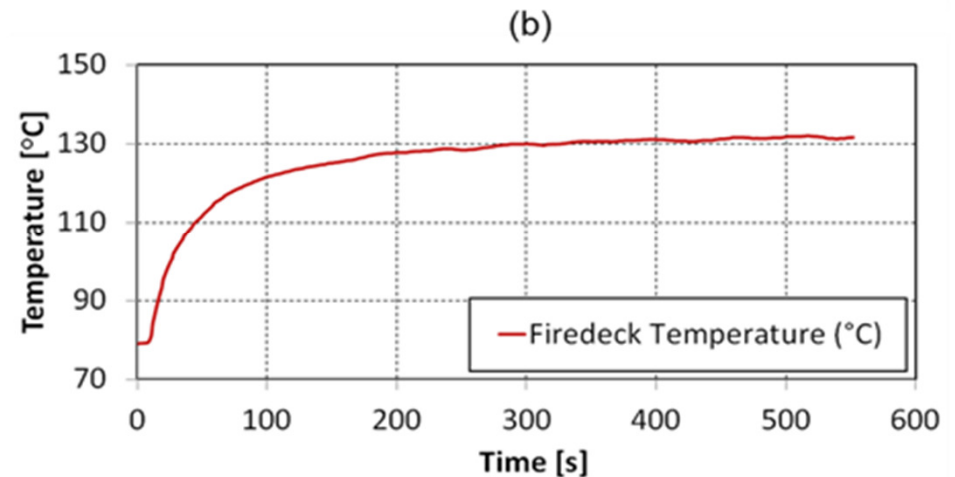
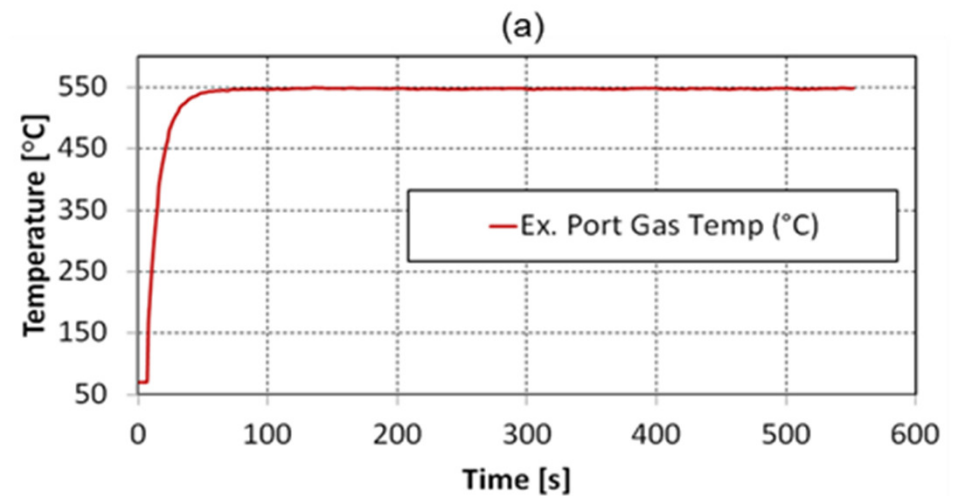
Research Engine Characteristics

- DISI, CR = 12:1, 0.55 L.
- Well-mixed charge operation.
 - 3- or 4- injection strategy for low PM emissions.
- Single intake valve.
 - Intake swirl.
 - No valve overlap.



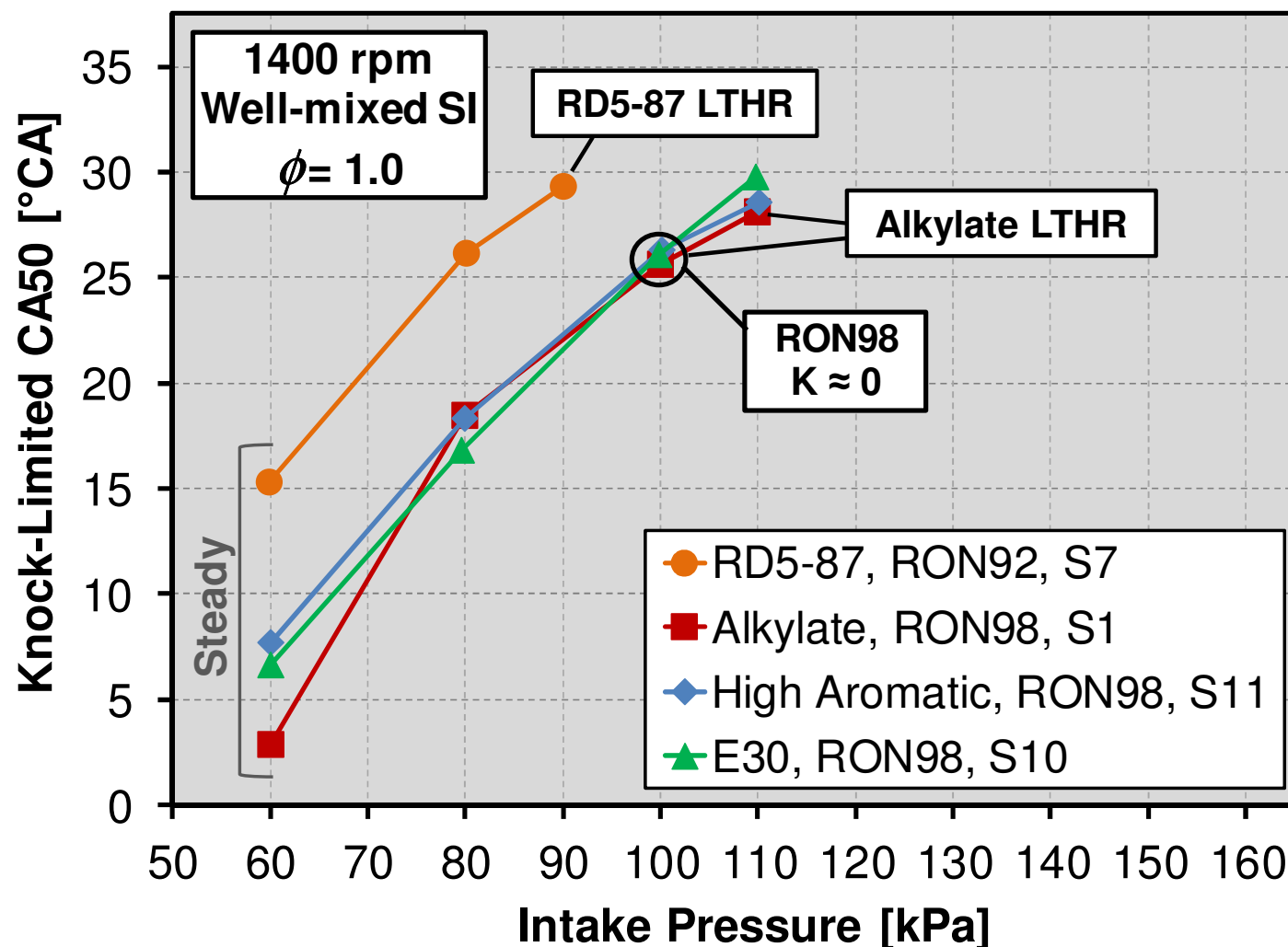
Establish Steady-State

- Motored to steady-fired operation.
- E30 fuel, $P_{in} \approx 79$ kPa, $ST = -5.6^\circ\text{CA}$.
- Time constants ≈ 10 's of s.
- True steady-state KL operation is not achieved for many minutes.
- Adjust Spark Timing (ST) to achieve Knock Intensity (KI) ≈ 70 kPa.
- Record 500 consecutive cycles.
- Report average CA50 as KL-CA50.

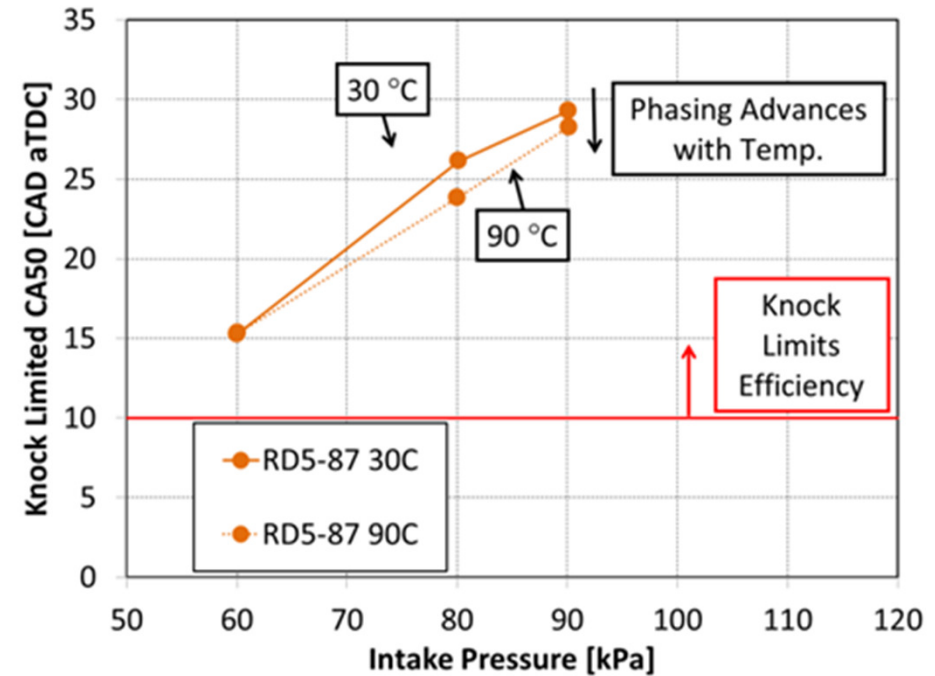
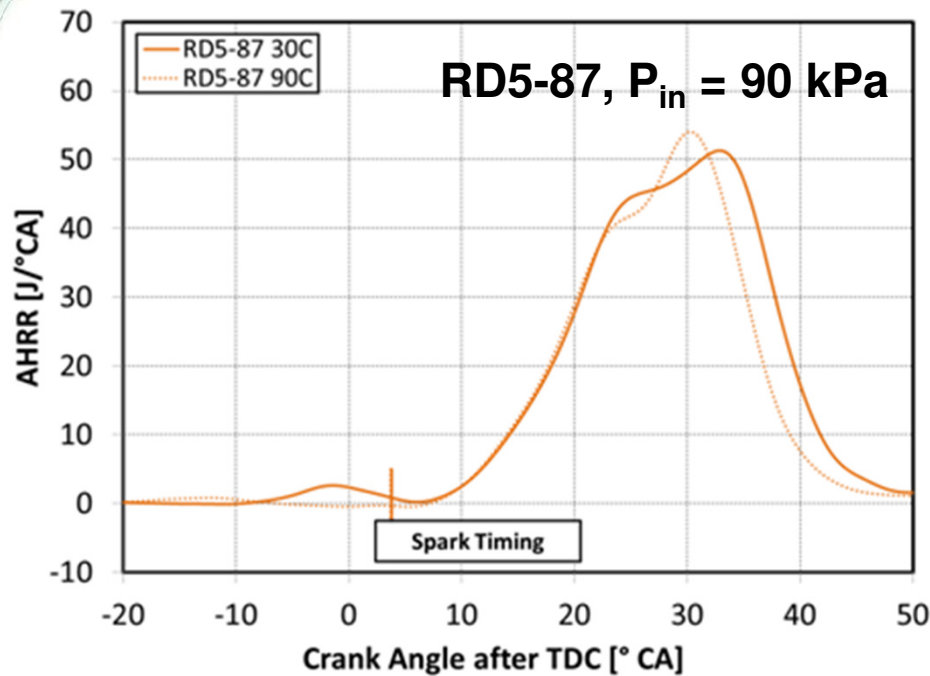


Steady-State Operation Reveals Benefit of High-RON Fuels

- RON98 fuels provide knock suppression benefits, compared to RON92 fuel.
- RD5-87 develops low-temperature heat release (LTHR) at highest P_{in} .

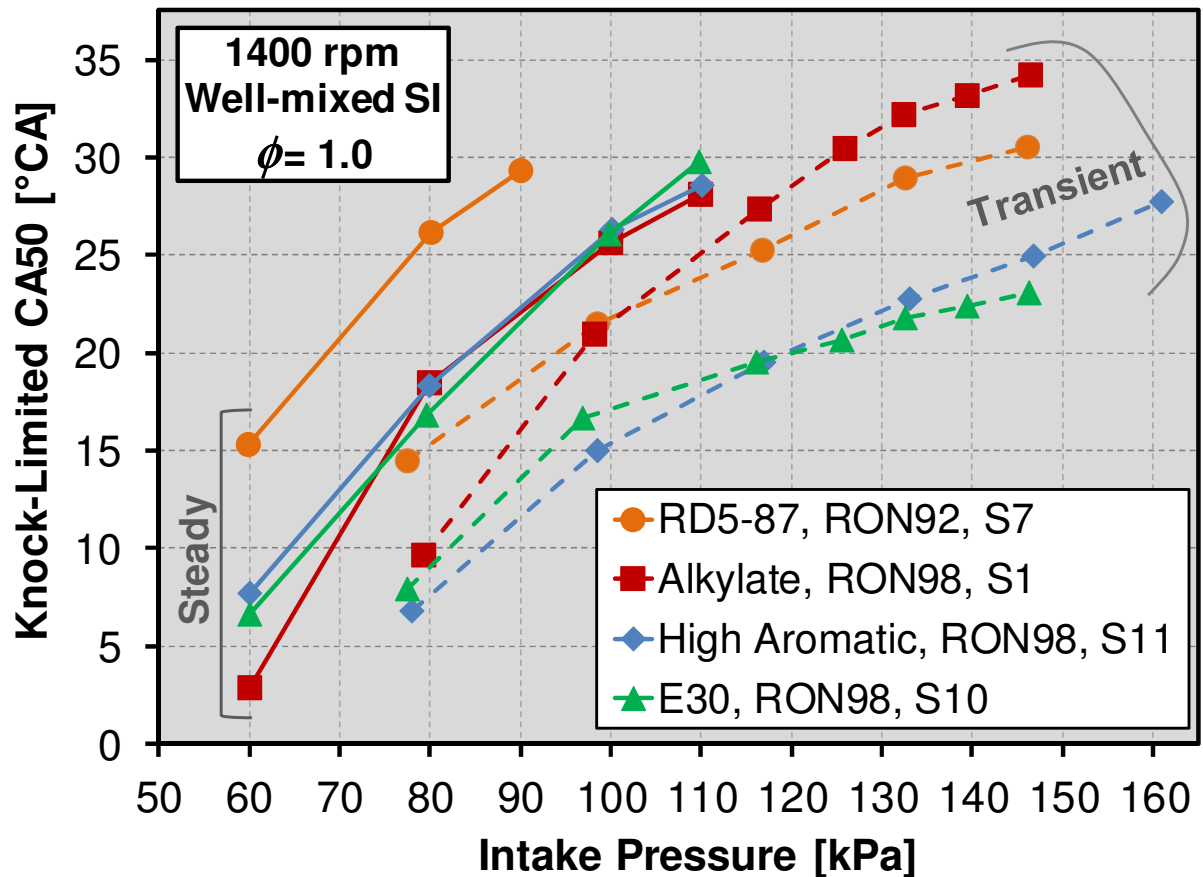


RD5-87 and Alkylate Exhibit NTC Behavior



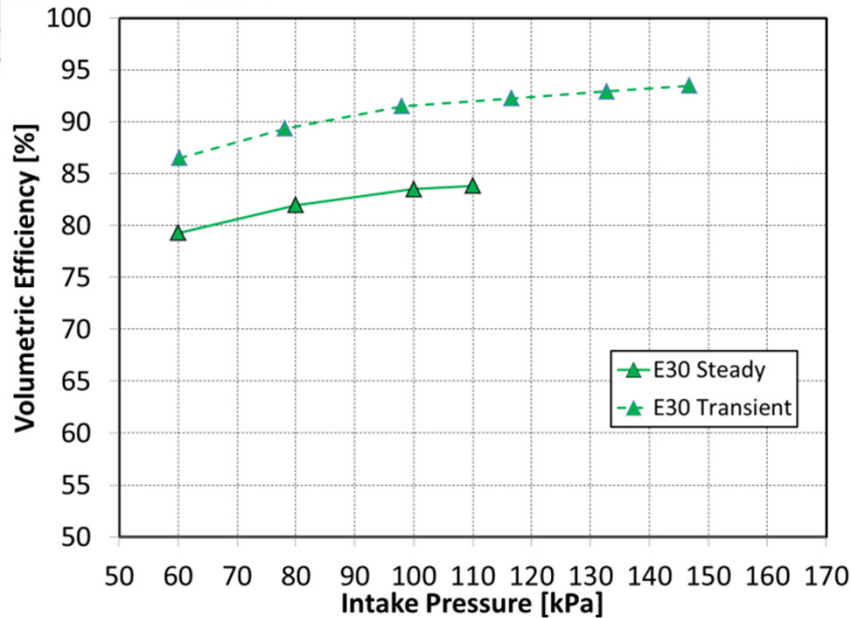
- RD5-87 develops LTHR at highest P_{in} .
- Increased T_{in} suppresses LTHR, and KL-CA50 advances.
- RD5-87 and Alkylate both show clear NTC behavior in this regime.
 - See SAE Paper 2017-01-0662 for detailed examination of RON98 fuels.
- Even so, the reduction of temperatures for load-transient operation provides strong knock-suppression benefit for all fuels \Rightarrow

Load-Transient Operation Reveals Benefit of High-S Fuels

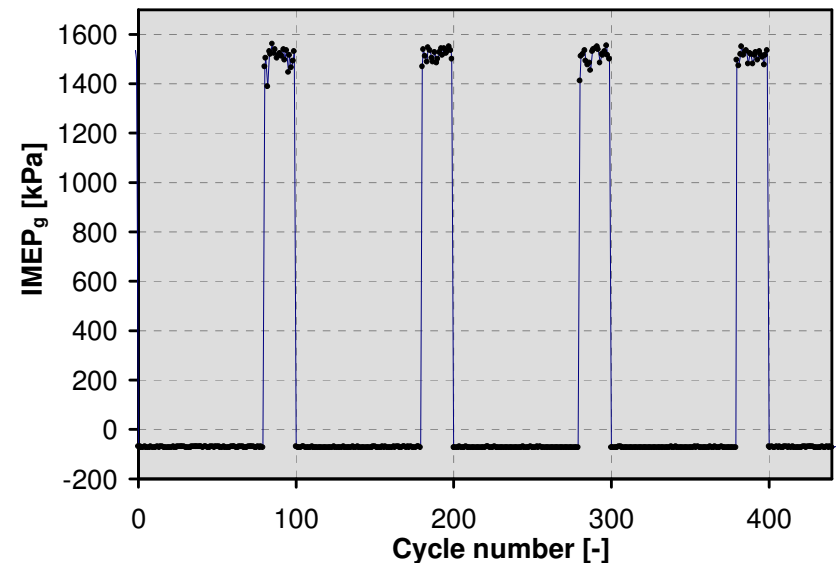
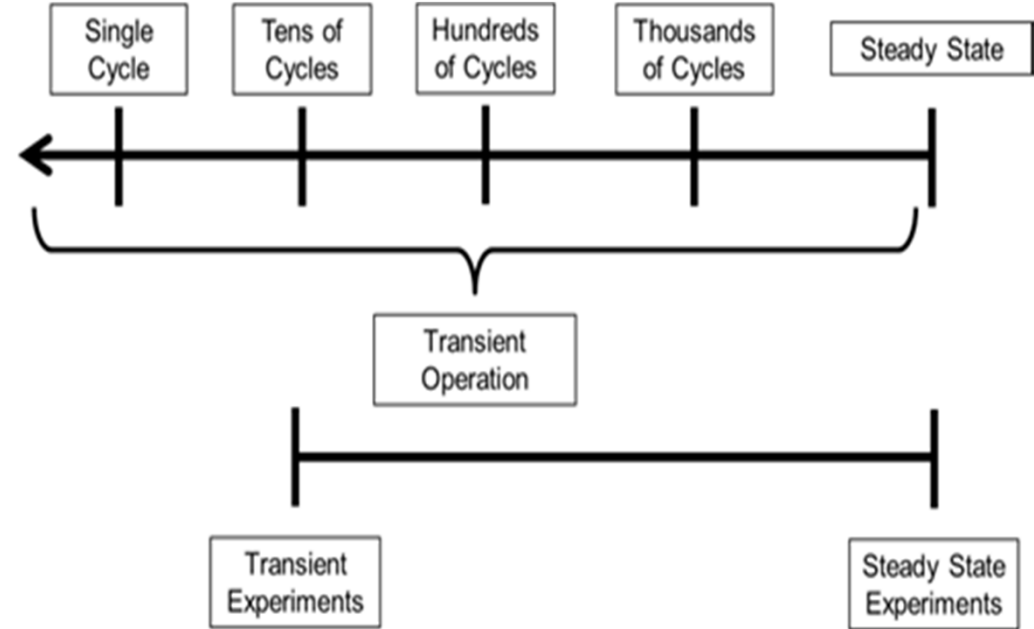


- The reduction of temperatures for load-transient operation provides strongest knock-suppression benefit for fuels with moderate to high S.
- Smallest benefit for low-S Alkylate.
 - Alkylate fuel is deep into NTC regime for steady-state operation.
 - Displays LTHR even for cooler transient operation.

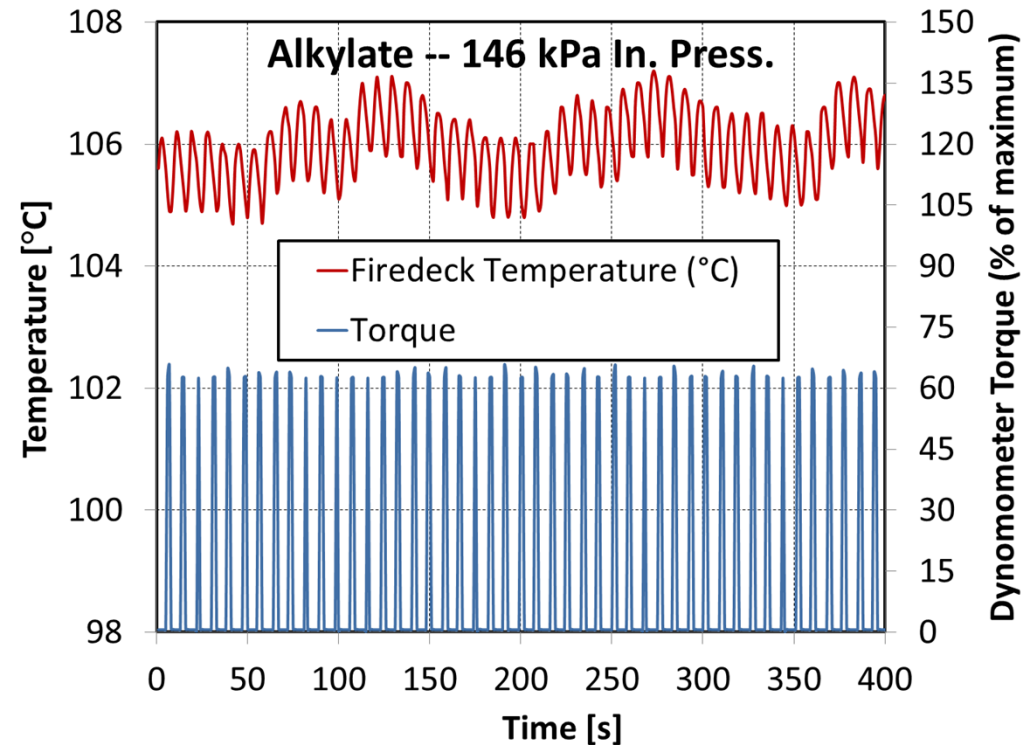
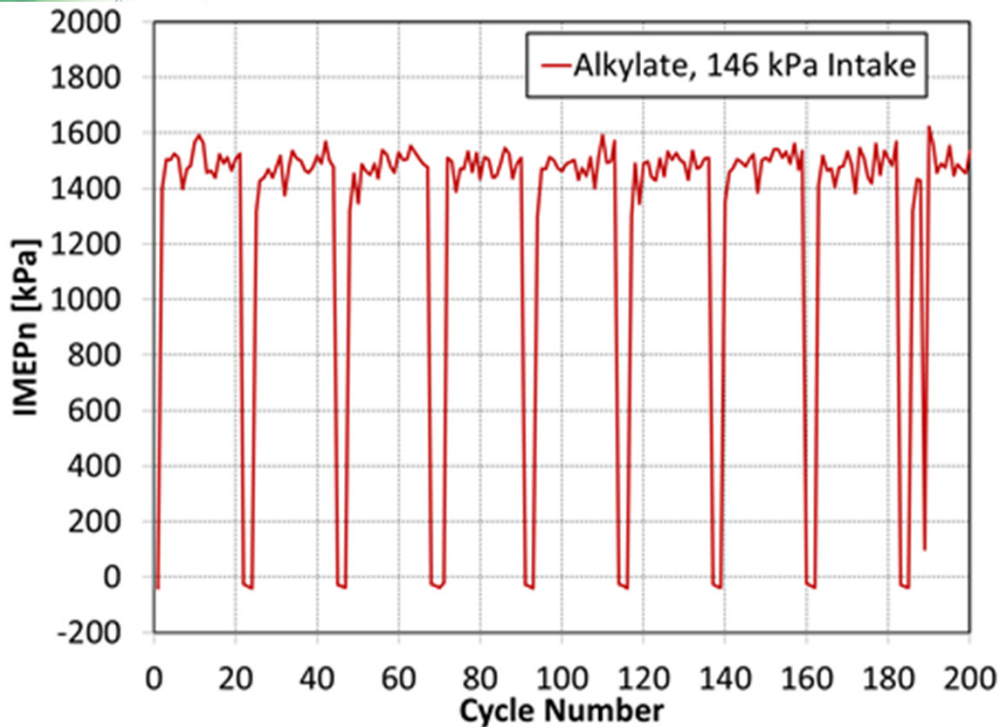
Test Regimes: Steady State and Transient



- First fired cycle likely not representative of real operation.
 - Cold air-only residuals.
- Consider 10's of cycles, by operating in a 20 fired / 80 skipped mode.
- Lower thermal state is evidenced by higher volumetric efficiency.

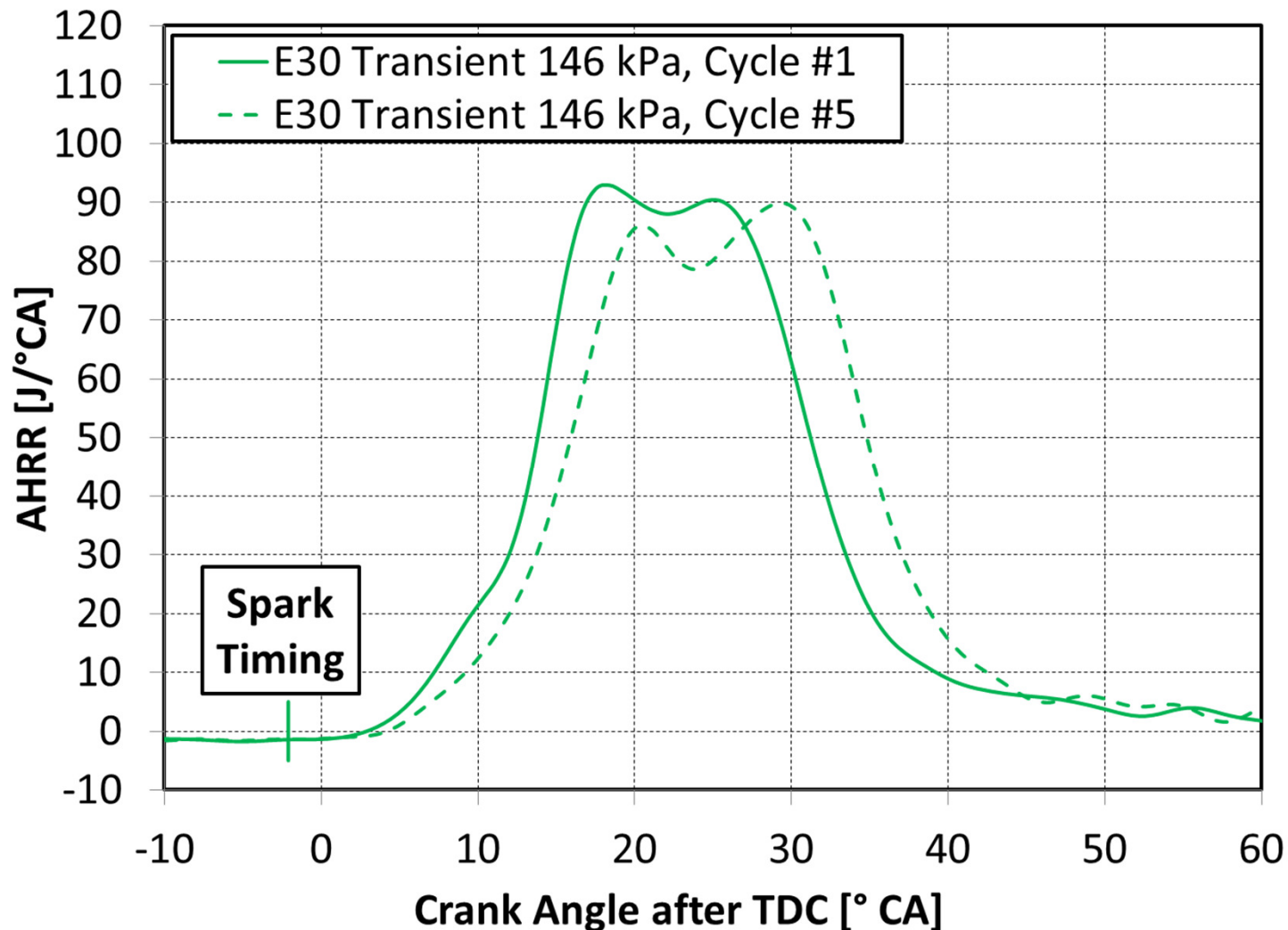


Data Collection: 20/80 Firing Cycle



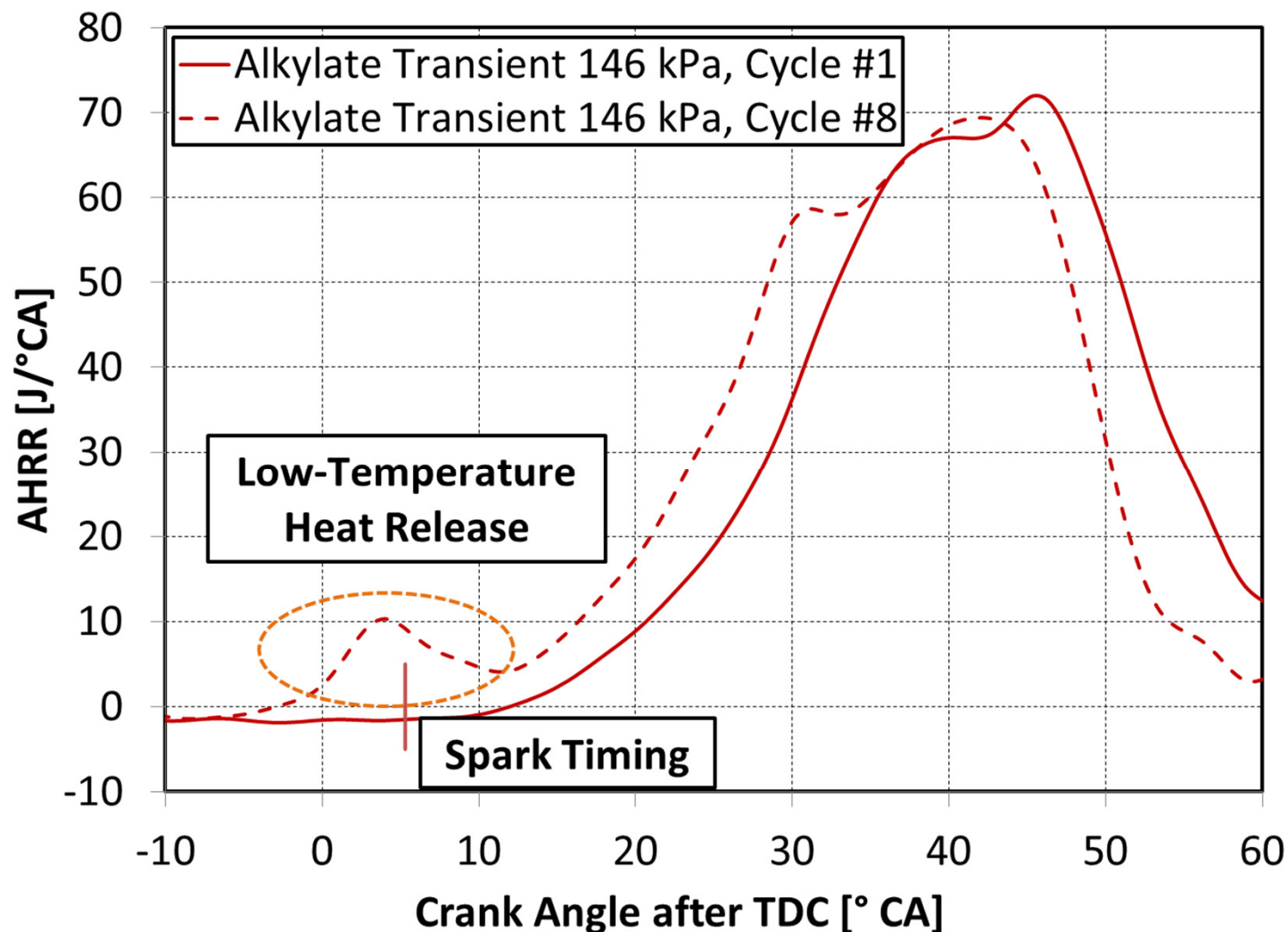
- 20 fired cycles followed by 80 motored cycles
 - Only 3 motored cycles are recorded – 1 ahead of sequence and 2 afterwards.
 - **50 repetitions** of 20/80 sequence are recorded = **1000 fired cycles**.
- Fluctuations seen in both firedeck temperature and dynamometer torque
 - Effects of 20/80 sequence and cooling-water control.
 - Firedeck temperatures 25°C lower than steady-state KL operation.

E30 Heat Release



- E30 exhibits consistent AHRR across batch of 20 cycles
- Highly repeatable end-gas autoignition observed, which leads to light knock

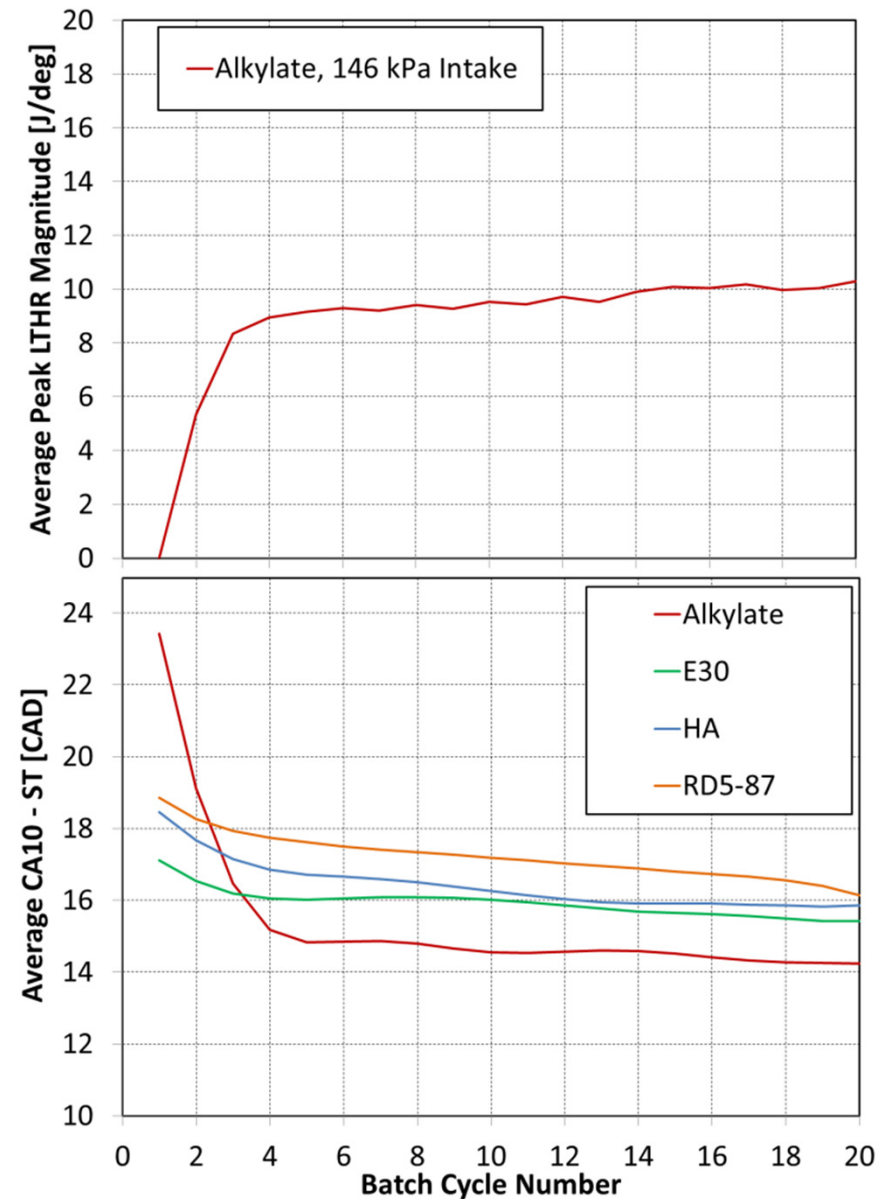
Alkylate Heat Release



- Alkylate AHRR exhibits strong transient behavior for each 20-cycle batch.
- LTHR never occurs on first cycle, but occurs on all subsequent cycles.
- End-gas autoignition exhibit greater variation \Rightarrow occasional strong knock.

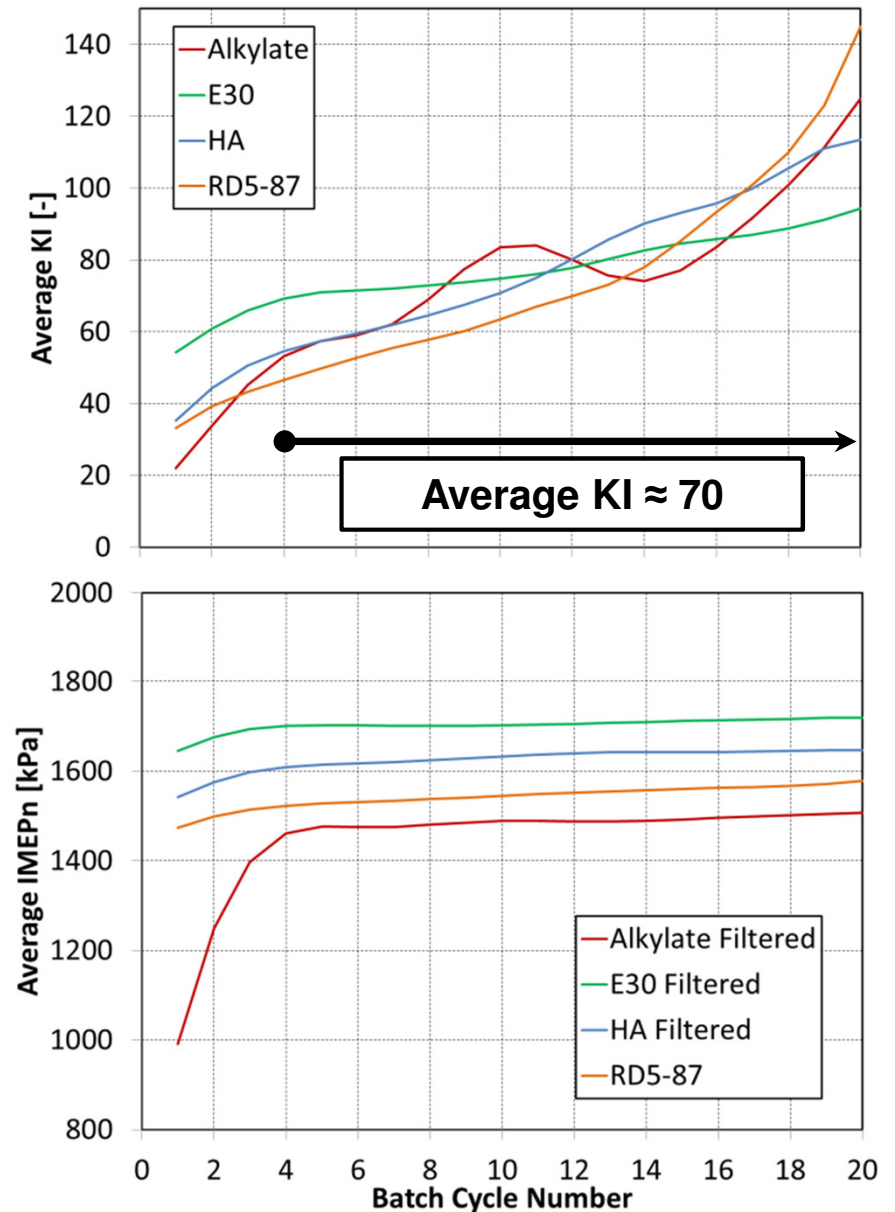
20-Cycle Transient

- Only Alkylate shows clear LTHR for 20/80 load-transient operation.
- LTHR magnitude builds rapidly when firing starts for each 20-cycle batch.
- Alkylate flame development is very slow without LTHR.
- Averages are based on 50 repetitions.



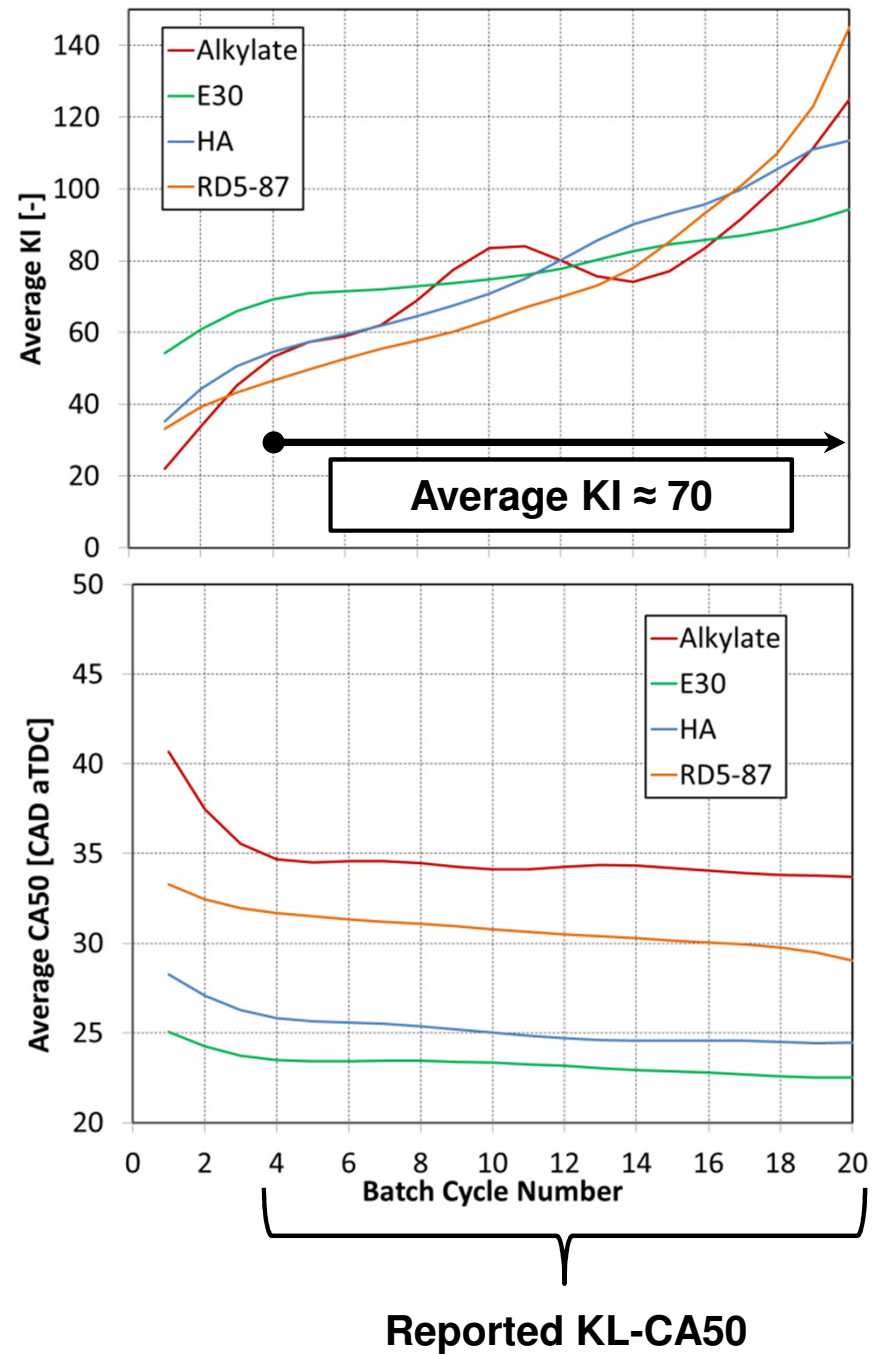
20-Cycle Transient

- IMEP approaches quasi-steady state surprisingly quickly.
- Alkylate was prone to misfire on the first cycle.
 - Slow flame development.
 - Alkylate never knocks on first cycle.
- Generally, Knock Intensity increases steadily for all fuels.
- Spark timing adjusted for $KI \approx 70$ for last 17 cycles.



20-Cycle Transient

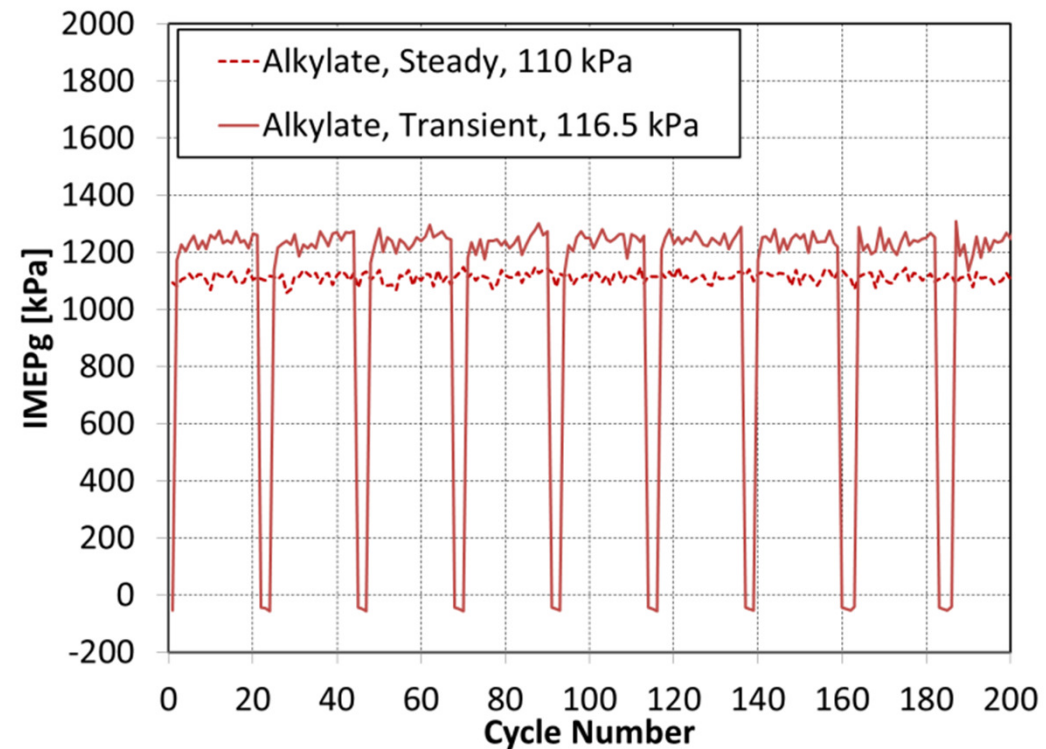
- Spark timing adjusted for $KI \approx 70$ for last 17 cycles.
- Average of last 17 cycles reported as KL-CA50.
 - Eliminates effect of residual transient.



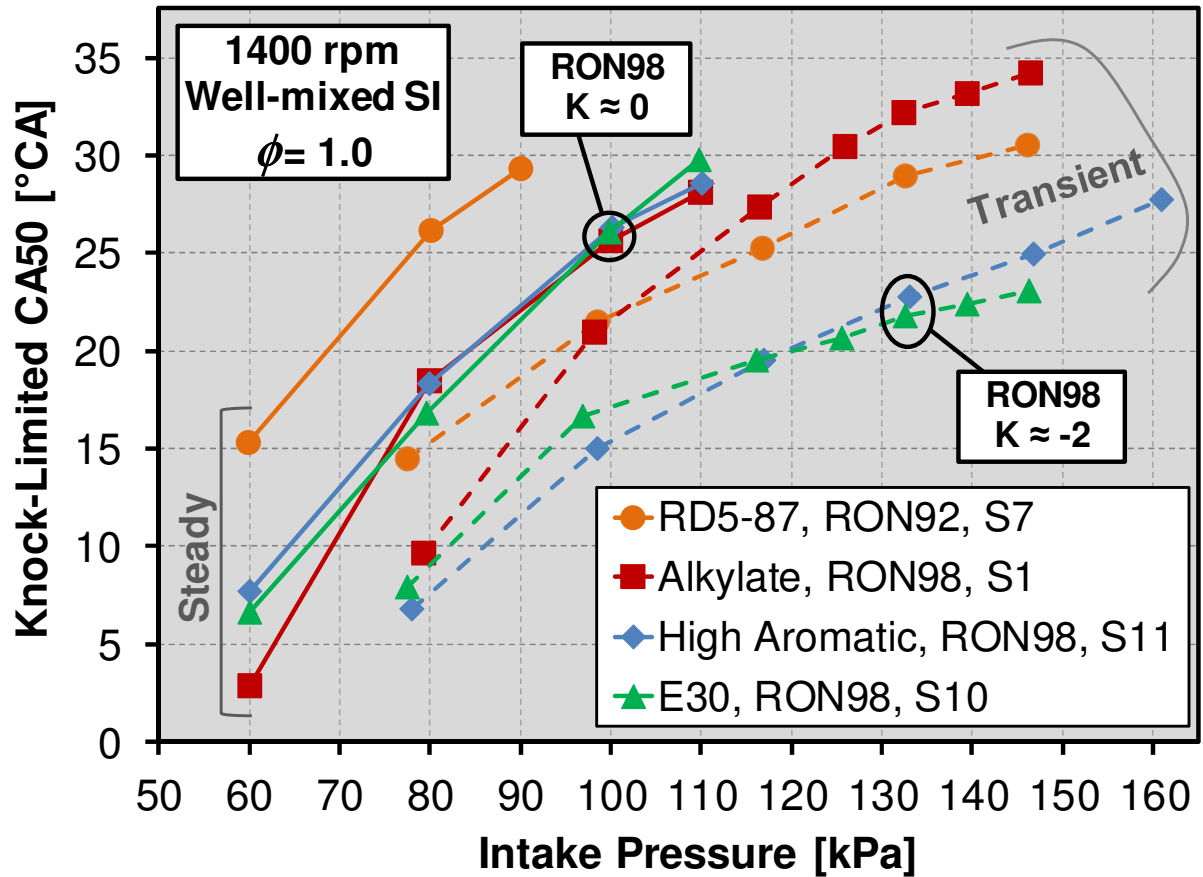
Stability of 20-Cycle Transient

- Across full 20-cycle batch, IMEP variability is higher than steady-state.
- However, COV of last 17 cycles is comparable to steady-state.
 - When residual transient is excluded.

Fuel	Alkylate	Alkylate
Intake Pressure	110 kPa	116.5 kPa
Operation	Steady State	Transient
KL-CA50	28.1 CAD aTDC	27.3 CAD aTDC
COV IMEP	1.6 %	-
COV IMEP All 20 Fired	-	7.8 %
COV IMEP Final 17 Fired	-	1.9 %

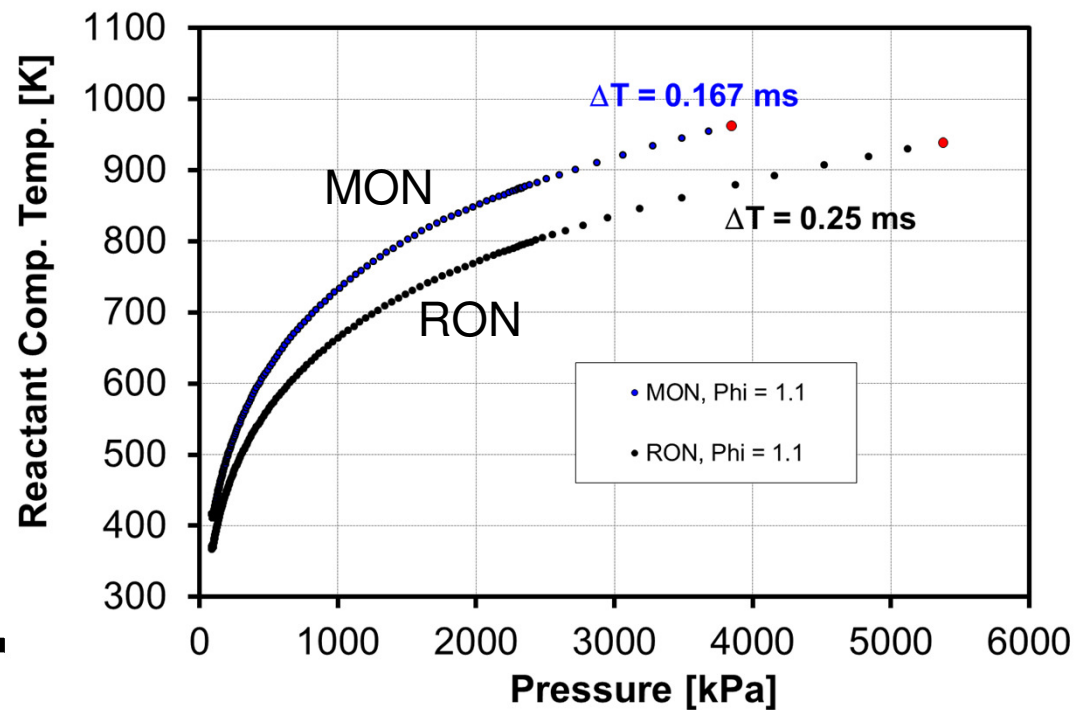


Load-Transient Operation Reveals Benefit of High-S Fuels



- Steady-state: All RON98 fuels provide knock suppression benefits, compared to RON92.
- Load Transient: RON98 low-S Alkylate fuel is outperformed by RON92 RD5-87 fuel.
- Put these results in context of Octane-Index framework.

Octane Index Framework



**Beyond
MON**

**Beyond
RON**

$K > 1$
Ex: Heated
intake / high
residuals HCCI

Lower pressure
for a given
temperature

K=1

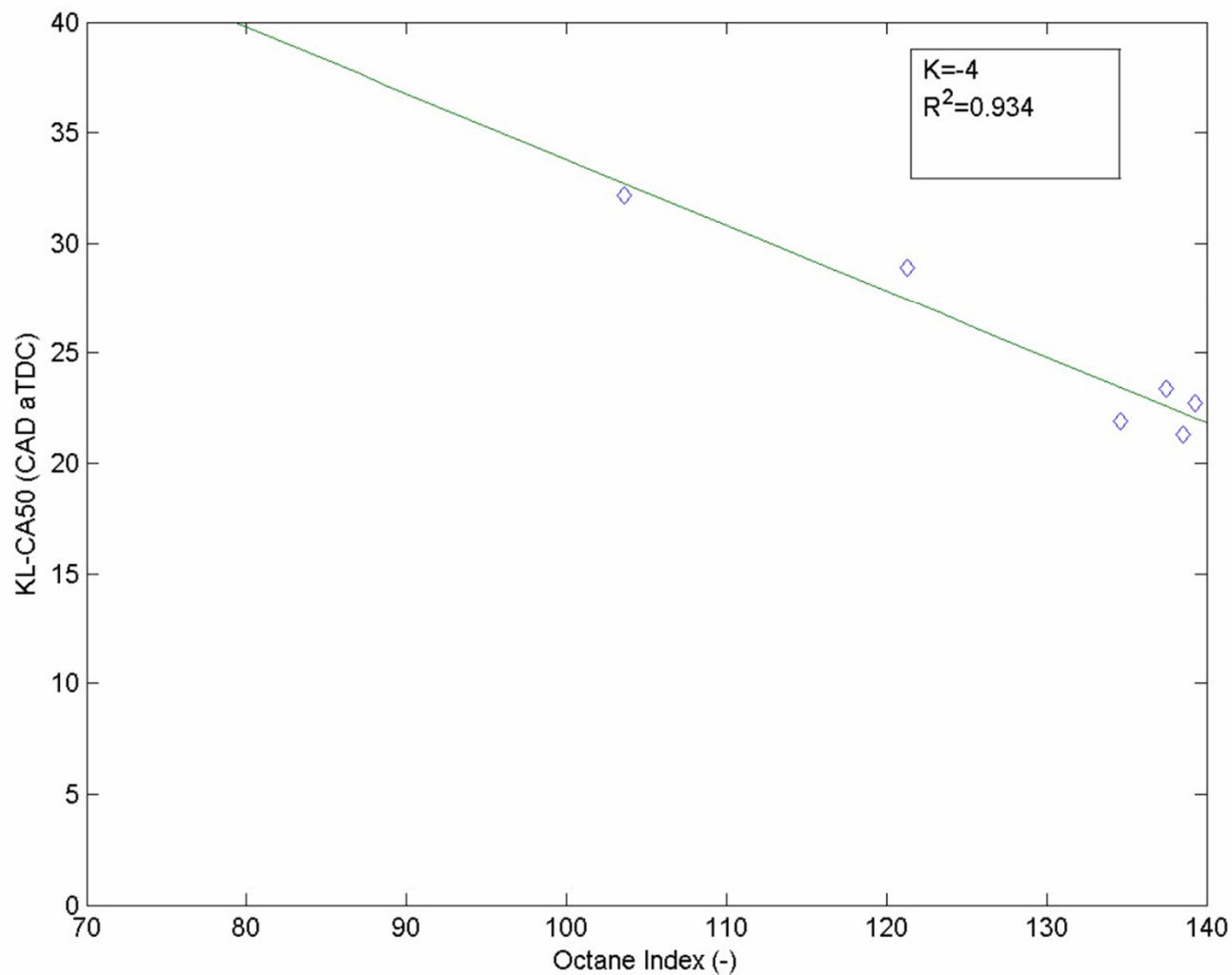
Higher
pressure for a
given
temperature

K=0

$K < 0$
Ex: Boosted SI,
GCI

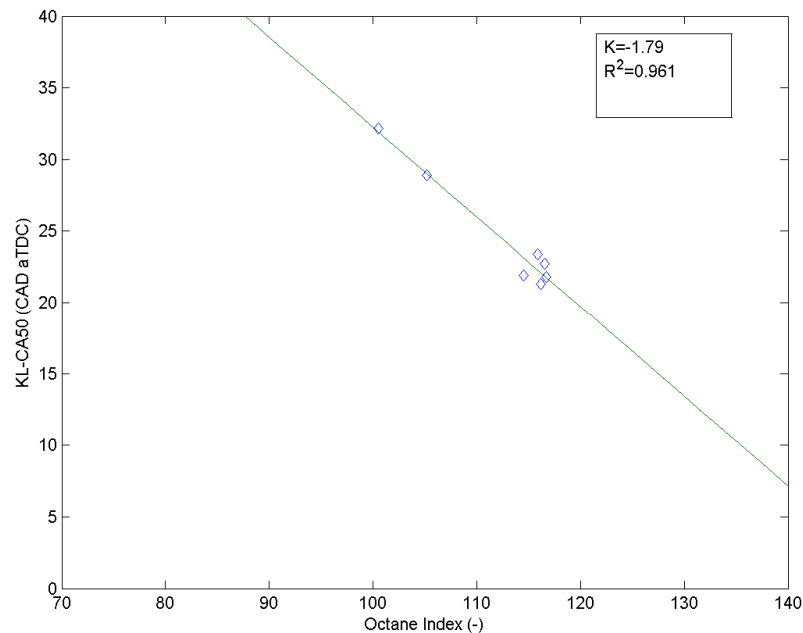
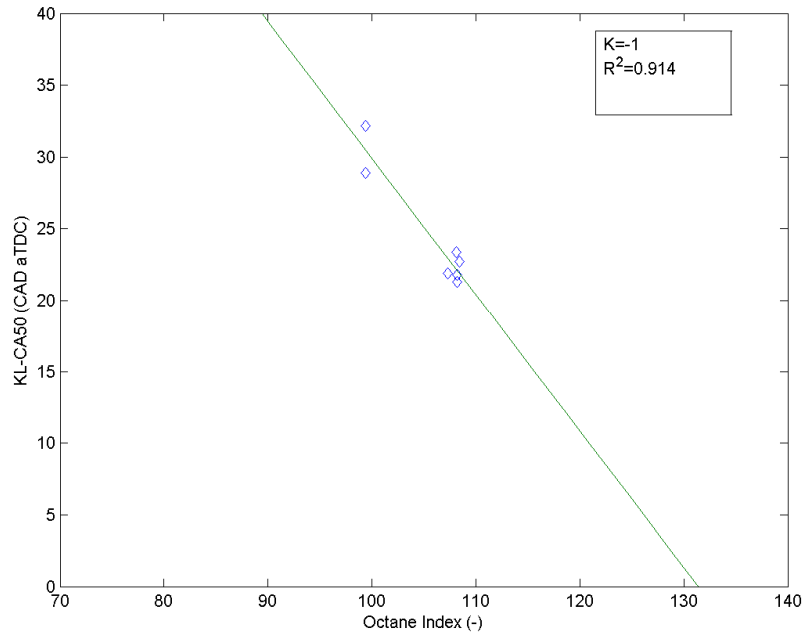
OI Reference: Kalghatgi, SAE 2001-01-3584.

Calculation of K





Calculation of K

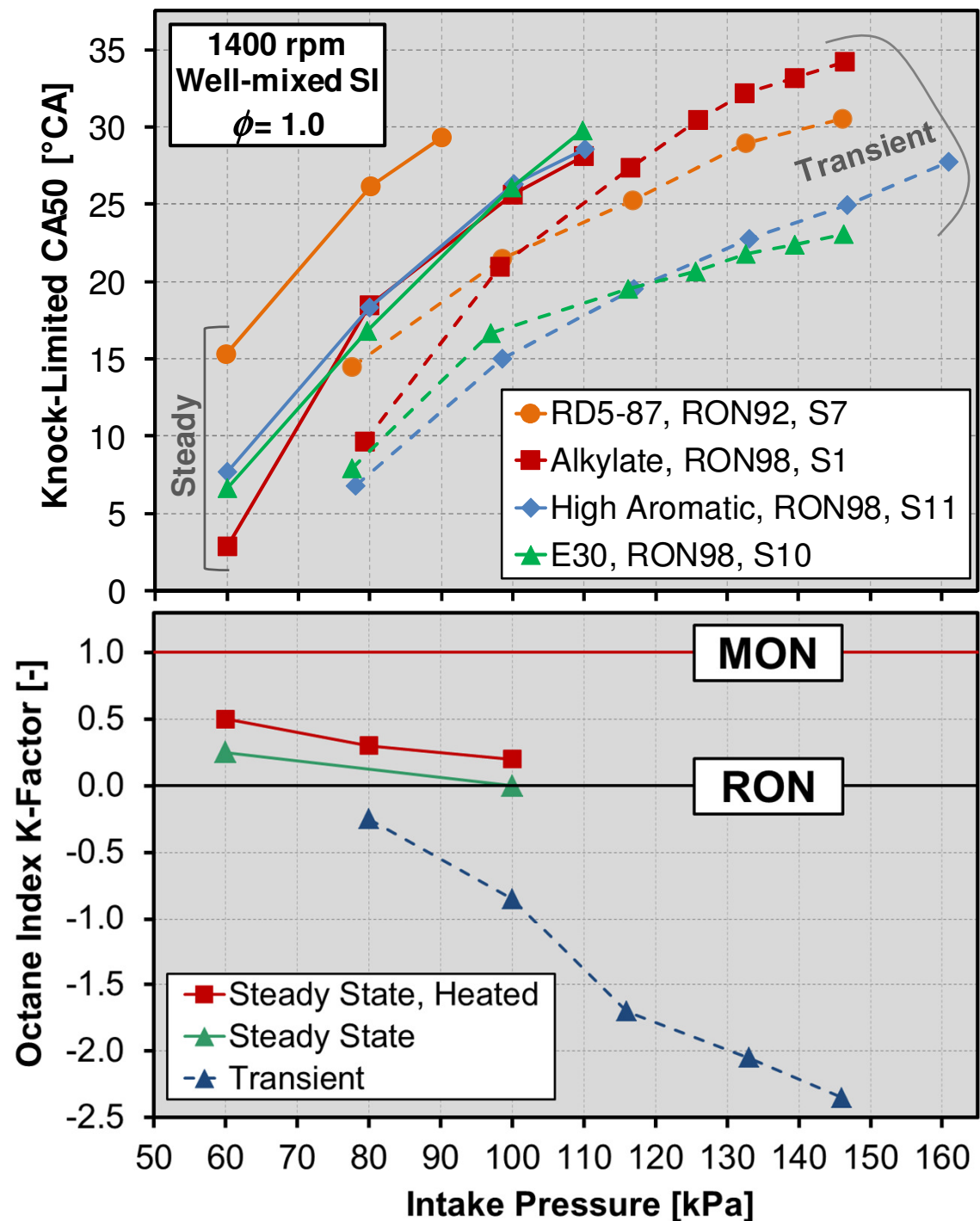


$$\text{Octane Index} = \text{RON} - K \cdot S$$

- Linear regression between KL-CA50 and Octane Index (OI) values to determine K at each operating condition
- Sweep across range of K values
- Calculate OI for each fuel for each K value
- Determine which K value yields best fit between OI and KL-CA50 data

K-Factor

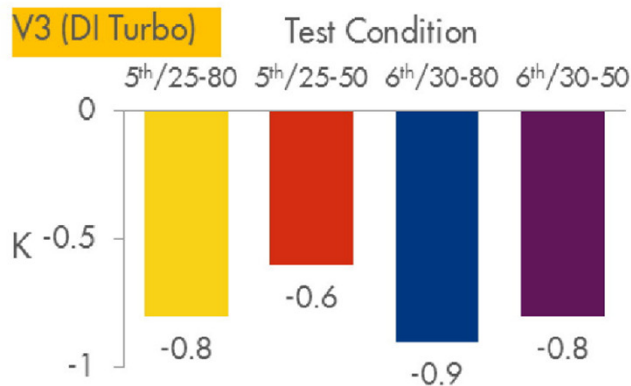
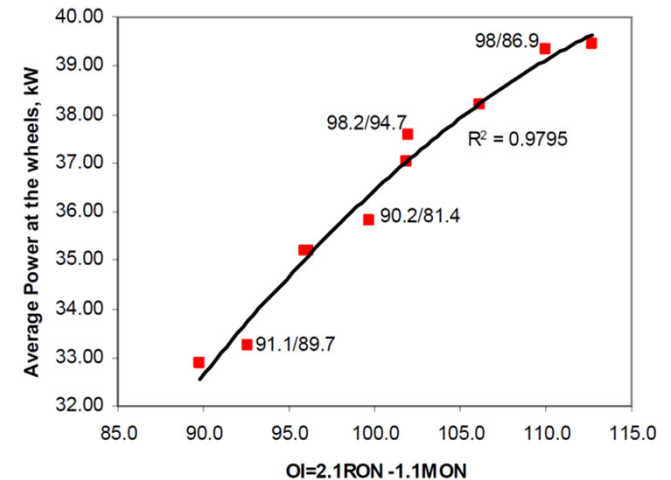
- Steady-state operation falls between $K = 0$ and $K = 0.5$.
 - $T_{in} = 30^{\circ}\text{C}$ or 90°C
- Transient operation result in $K < 0$, “beyond RON” conditions.
- Realistic?



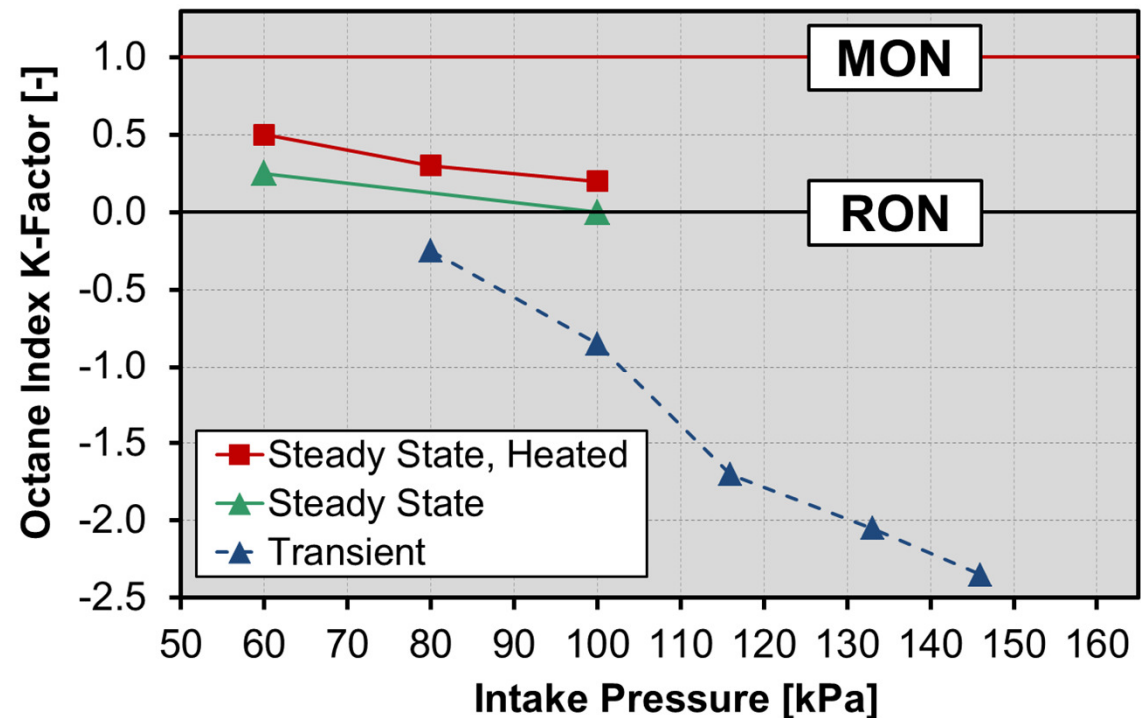
K-Factors for Actual Vehicle Operation

- These highly negative K-factors are consistent with literature.
- Naturally aspirated PFI 2003 Mercedes CLK1: $K = -1.1$ during high-gear acceleration.
- Turbocharged DISI 2012 vehicle: $K = -0.6$ to -0.9

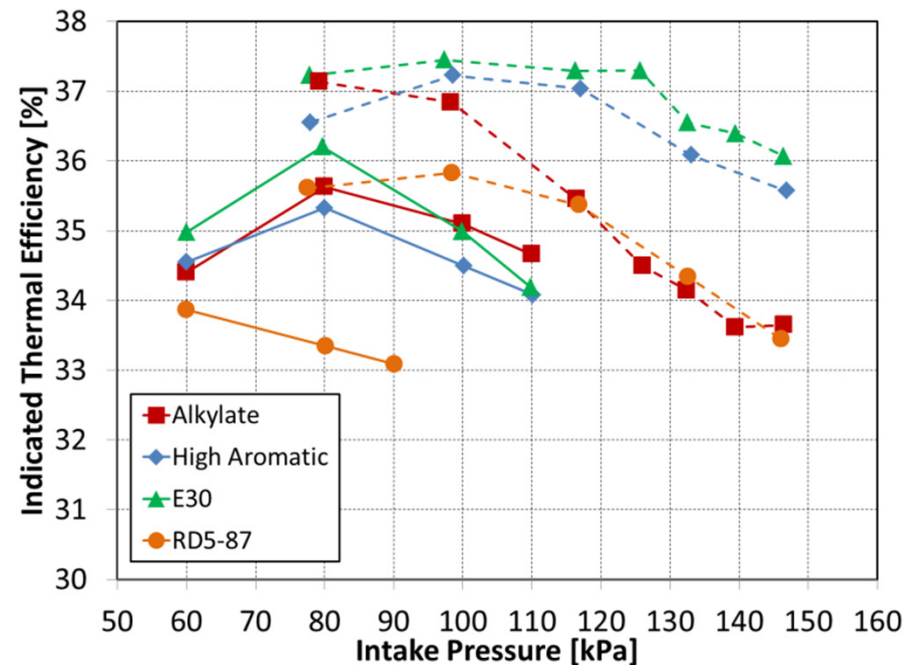
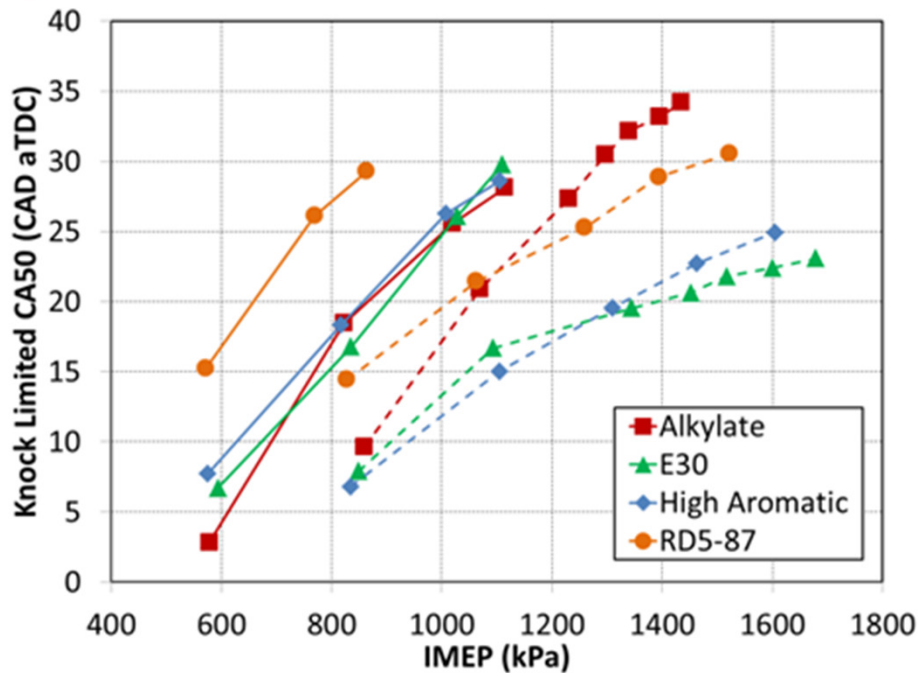
Kalghatgi, SAE 2005-01-0239



Prakash *et al.*, SAE 2016-01-0834



Fuel Performance



- Higher load of high-S fuels is consistent with other studies showing faster acceleration.
- Higher efficiency is an important benefit, and justifies further fuels research.

Conclusions

- Load-transient operation results in significantly improved KL-CA50's relative to steady-state performance for all tested fuels.
 - Due to the lower thermal state of the engine structure under transient operation.
- Transient operation allow the exploration of a wide range of Octane Index K values, from 0.5 to -2.35.
- Boosted conditions lead to “beyond RON” conditions in which high-RON, **high-S fuels** exhibit **improved performance** over a high-RON, low-S fuel.
- LTHR is critical to the autoignition of the Alkylate fuel under transient conditions.
 - The primary effect of LTHR is a reduction in the flame-development time.
 - The first fired cycle for this fuel, which displayed no LTHR, never knocked.

Kevin Stork, Gurpreet Singh
Leo Breton, Mike Weismiller



U.S. DEPARTMENT OF
ENERGY



Co-Optimization of
Fuels & Engines



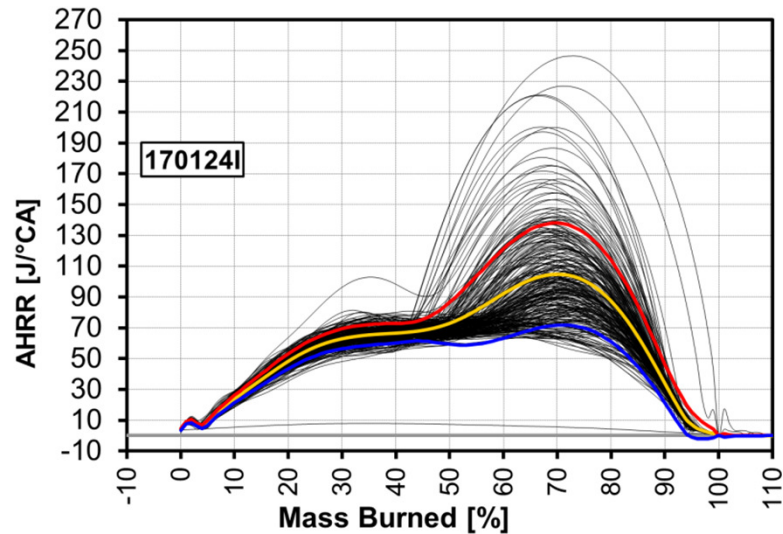
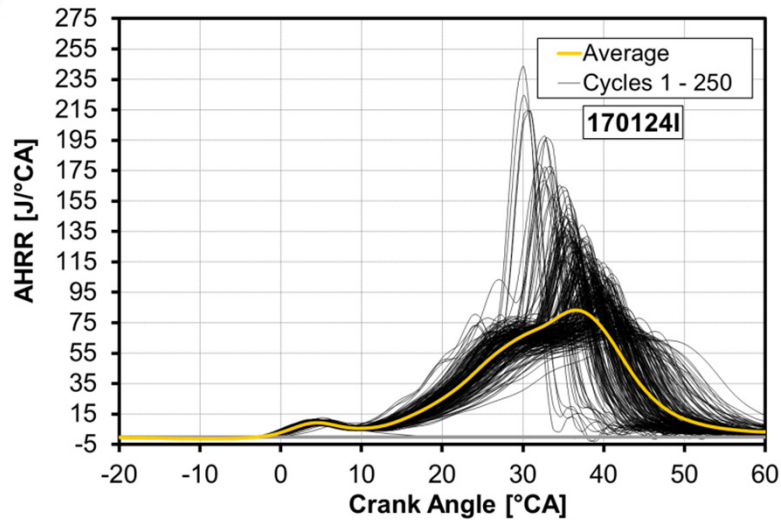
Acknowledgements

The authors would like to thank Alberto Garcia, Gary Hubbard, Keith Penney, and Tim Gilbertson for their dedicated support of the DISI laboratory.

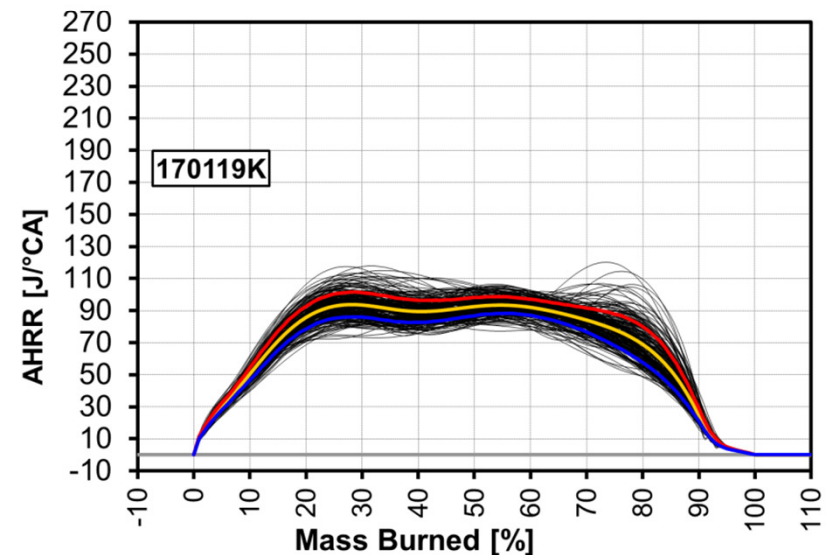
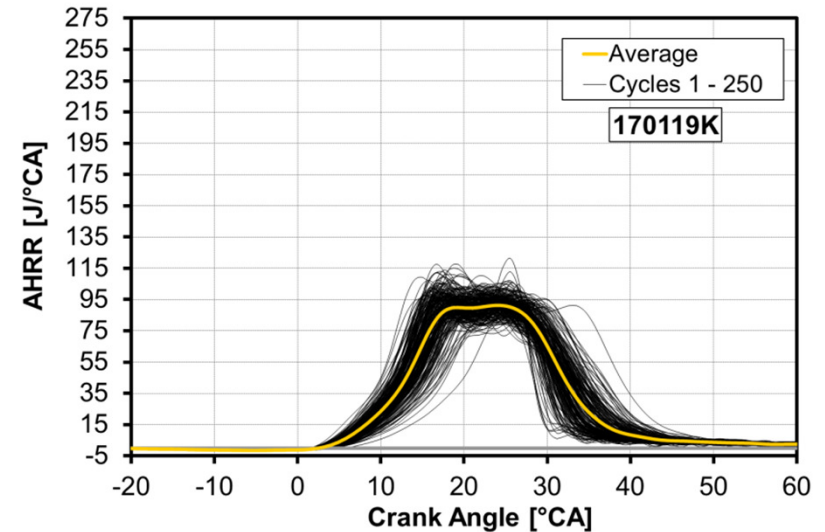
The work was performed at the Combustion Research Facility, Sandia National Laboratories, Livermore, CA. This research was conducted as part of the Co-Optimization of Fuels & Engines (Co-Optima) project sponsored by the U.S. Department of Energy (DOE) Office of Energy Efficiency and Renewable Energy (EERE), Bioenergy Technologies and Vehicle Technologies Offices. Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

KL-CA50 at 146 kPa Intake Pressure: AHRR Stability

Alkylate



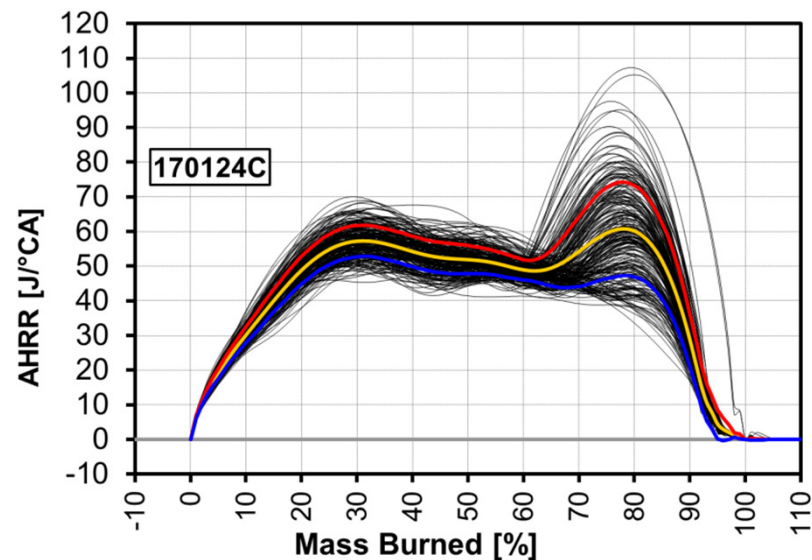
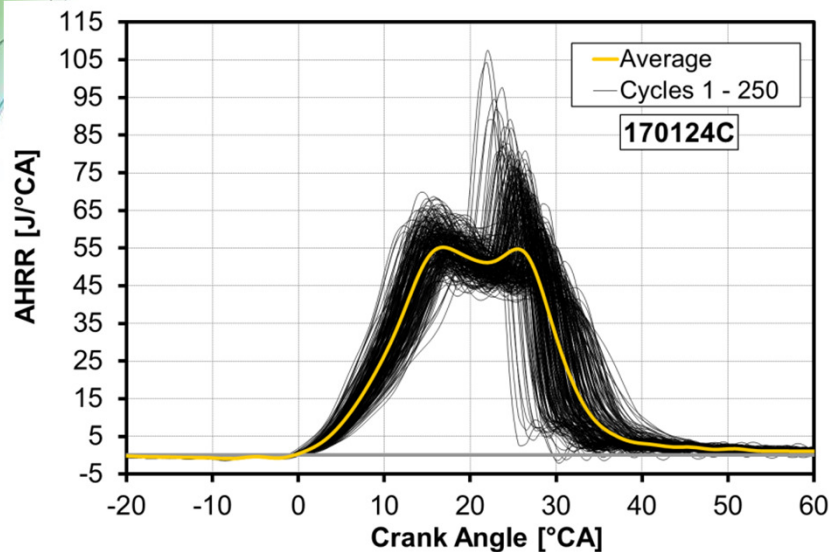
E30



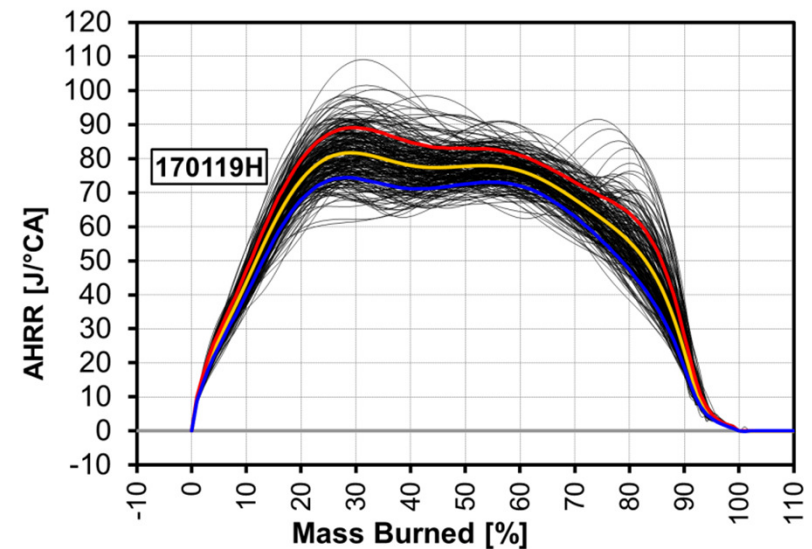
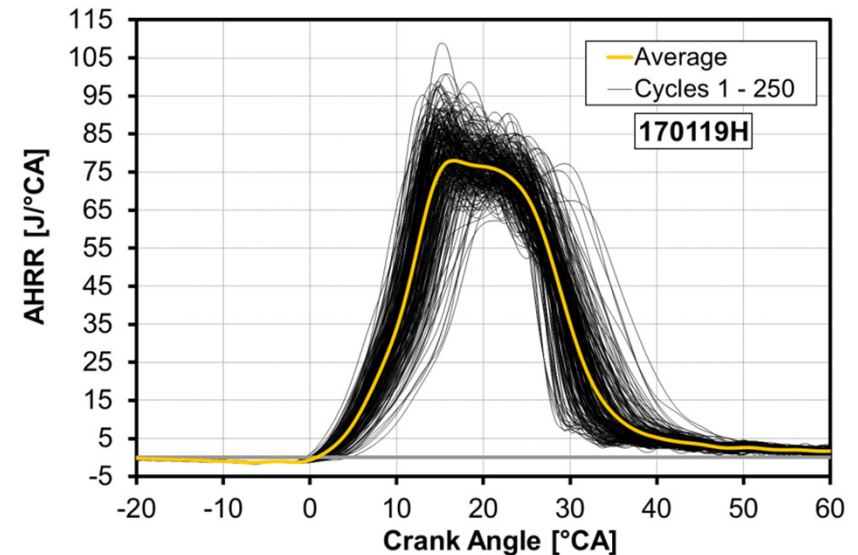
- Alkylate shows strong end-gas autoignition, and large variability
 - Comparison is skewed by variations in KL-CA50 at constant intake pressure

KL-CA50 = 21 CAD aTDC: AHRR Variation

Alkylate: Pin = 98 kPa



E30: Pin = 126 kPa



- With KL-CA50 fixed, Alkylate still shows larger variation in end-gas autoignition than E30