

Exceptional service in the national interest

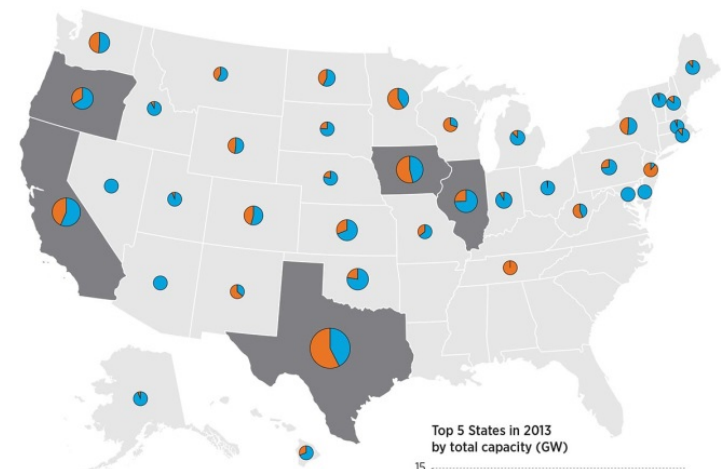


Wind Turbine Blade Reference Model for the U.S. Low Wind Resource Regions

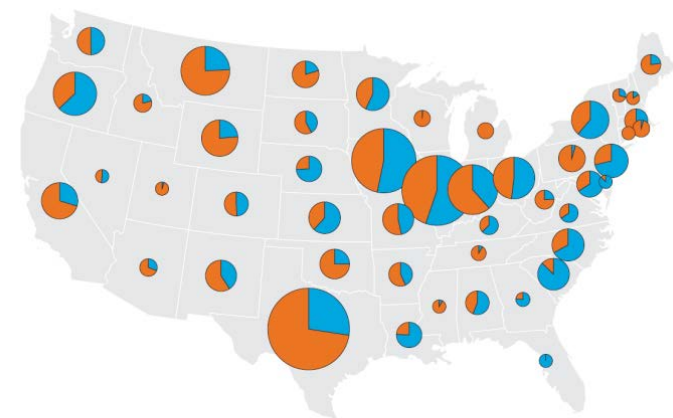
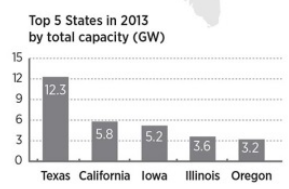
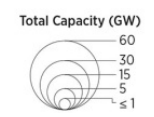
Brandon L. Ennis and Christopher L. Kelley

Wind energy sites are expanding

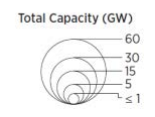
- The Department of Energy's Wind Vision report explores scenarios where wind contributes to 35% of the U.S. energy demand by 2050
- The projections include wind energy installations in the low wind-resource southeast which are currently absent
- Significant wind energy generation is projected in the Midwest states, where many of the better wind resource sites have been utilized
- There is a need for improved technologies and designs targeted at energy capture in low wind conditions



Total Wind Deployment
● Through 2008
● 2009 through 2013

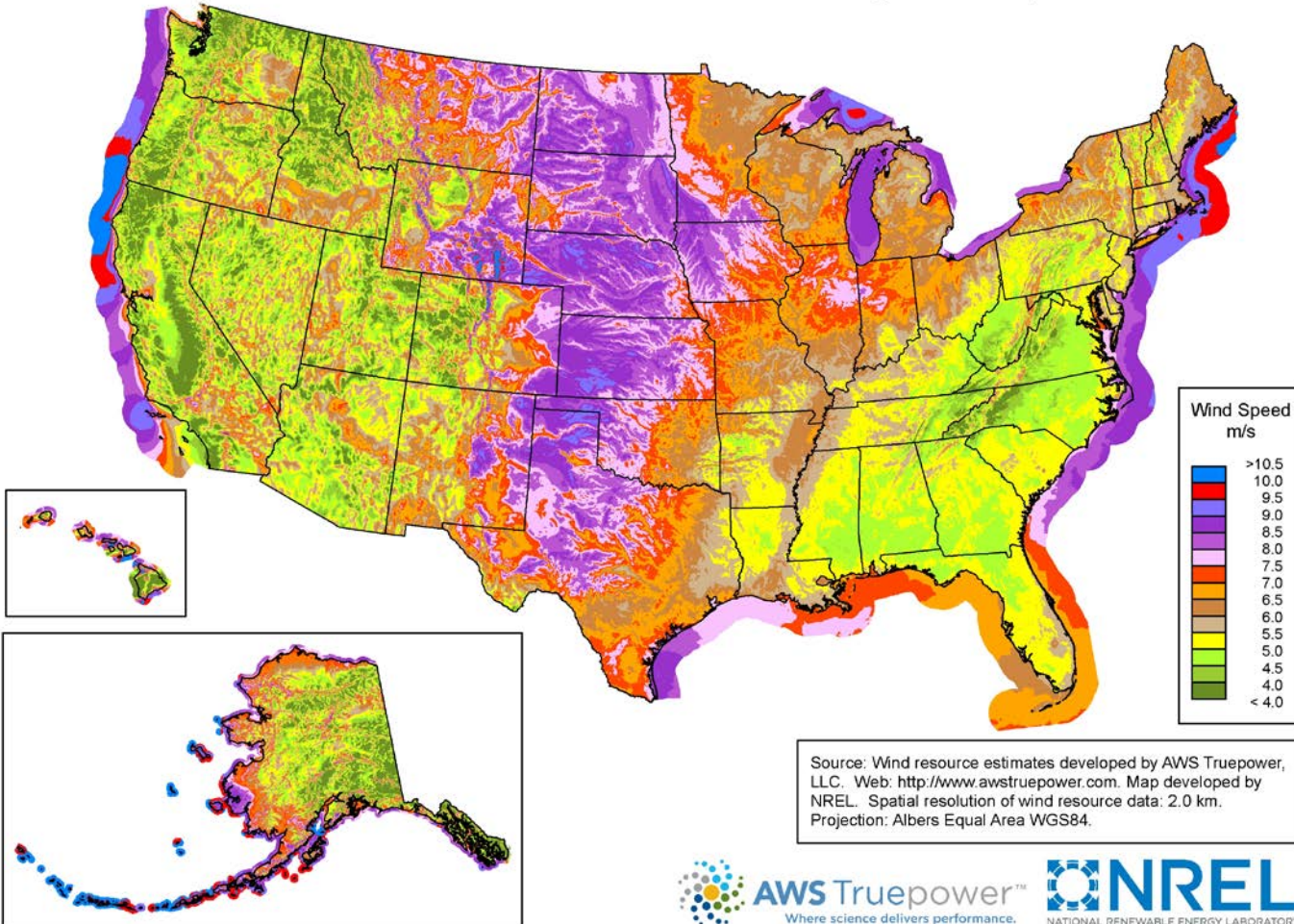


Total Wind Deployment
● Through 2030
● 2031 through 2050



Wind resource is too low for historical designs in parts of the U.S.

United States - Land-Based and Offshore Annual Average Wind Speed at 100 m



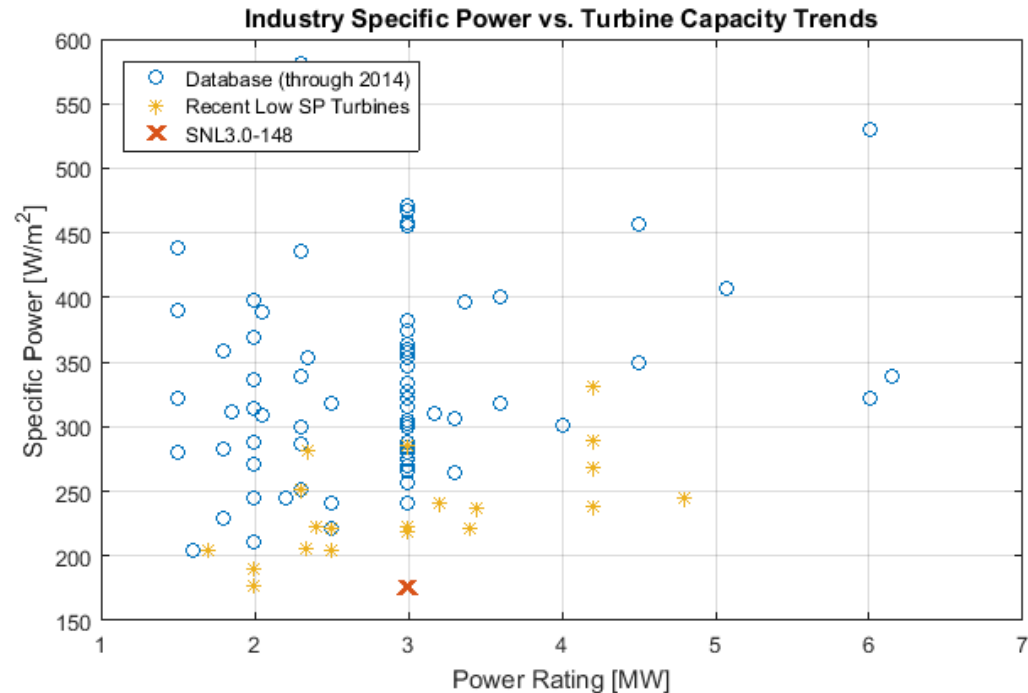
Midwest sites may have average wind speeds as low as 5.5-6.5 m/s

Interior southeast sites may have average wind speeds as low as 4.5-5.5 m/s

Source: Wind resource estimates developed by AWS Truepower, LLC. Web: <http://www.awstruepower.com>. Map developed by NREL. Spatial resolution of wind resource data: 2.0 km. Projection: Albers Equal Area WGS84.

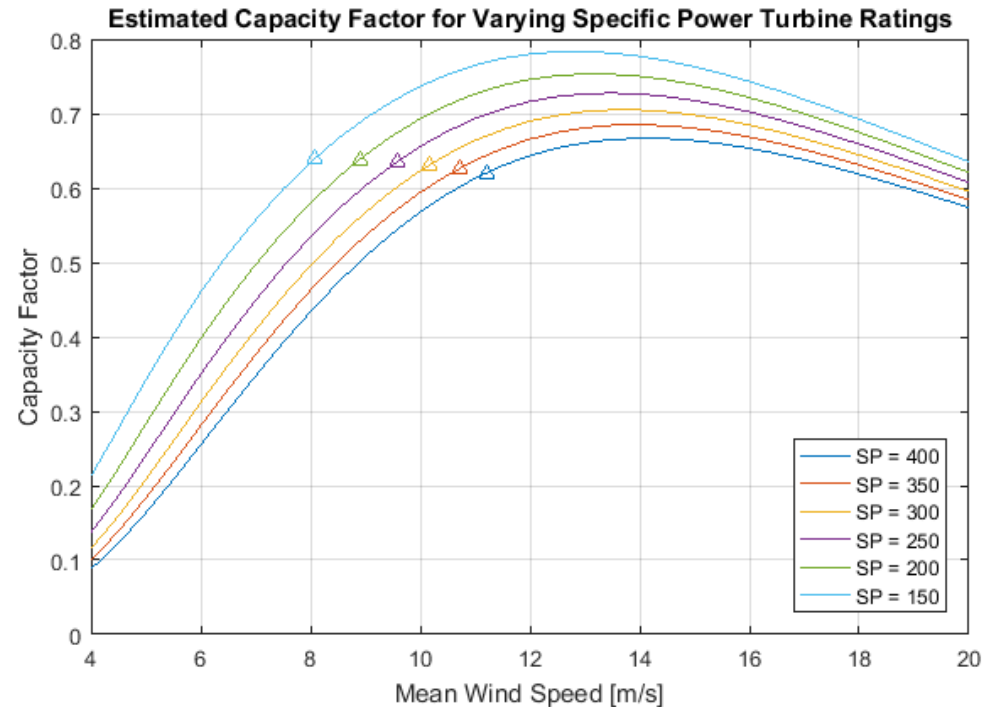
Industry trends for low wind sites

- The industry trend has been towards longer blades and lower specific power ratings for land-based wind turbines
- Vestas and GE both offer 2 MW turbines with specific power ratings below 200 W/m^2
- A blade reference model is needed to study the unique challenges for designing cost-effective low specific power wind turbines



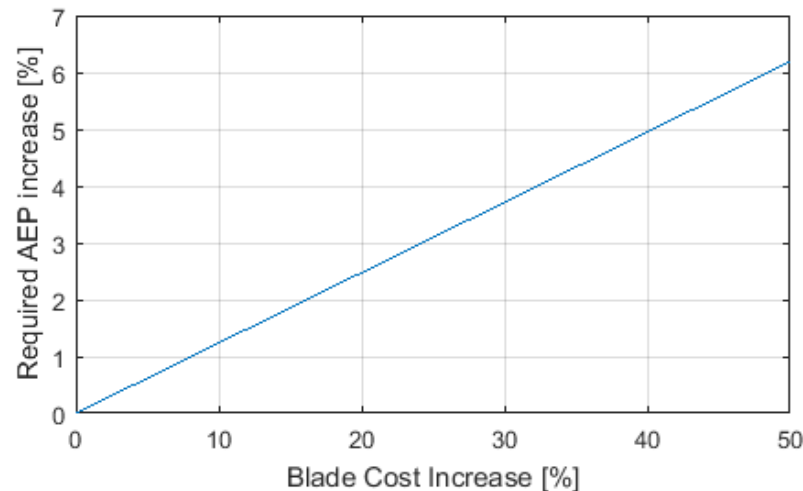
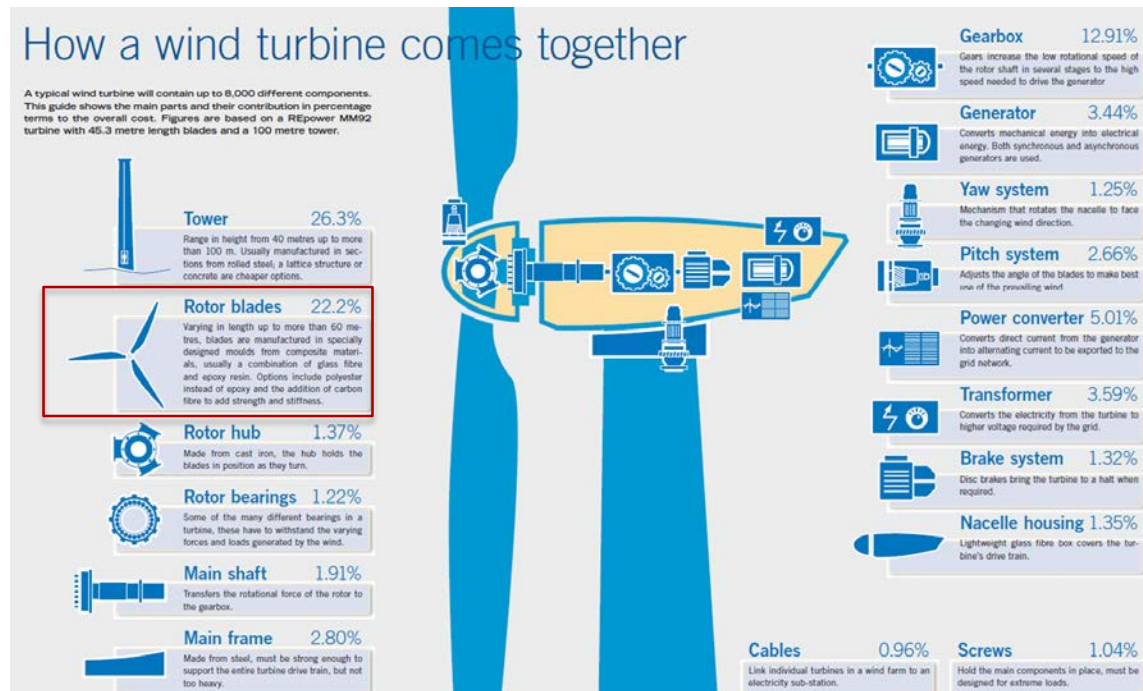
Specific power and energy capture

- Wind turbine capacity factor is inherently higher for low specific power designs due to:
 - Increased energy capture at the same wind speed
 - Reduction in the turbine's rated wind speed
- At 6 m/s, the energy production is over 80% higher for a specific power design of 150 versus 400 W/m²
- Can increase the energy capture while maintaining constant system loads



Effect on the cost of energy

- Design decisions are not based on power or efficiency, but on cost of energy
- Blades contribute to 20-25% of the total turbine capital cost
 - A 25% increase in the blade cost only increases the turbine cost by ~5-6%
 - Assuming turbine capital costs are 55% of total costs, a 25% increase in blade cost is justified by a 3% increase in AEP to maintain LCOE



*Source: EWEA

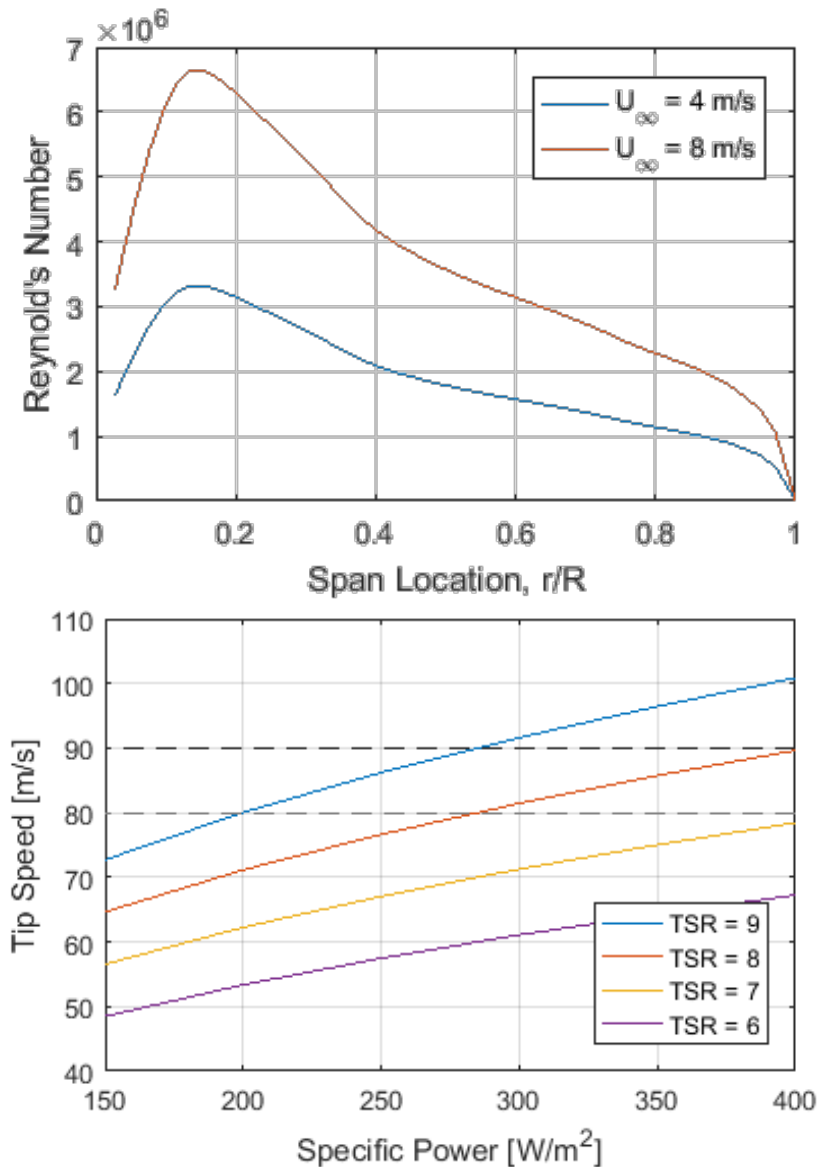
SNL3.0-148 Reference Blade Model

Publicly available reference model that is representative of the industry shift towards low specific power wind turbines for land-based sites. Can be used to identify and address the unique challenges faced for these machines, such as materials, controls, and aeroelastic coupling and tailoring.

- 3 MW power rating
- 148m turbine diameter
- 72m blade length
- 175 W/m² specific power
- Three blade, upwind
- TSR = 9
- Lightly loaded tip
 - Matches the root bending moment of the “optimal” induction design ($a=1/3$) while increasing energy capture through a longer blade
- Tower and turbine reference models from IEA Task 37 will be used with the blade model

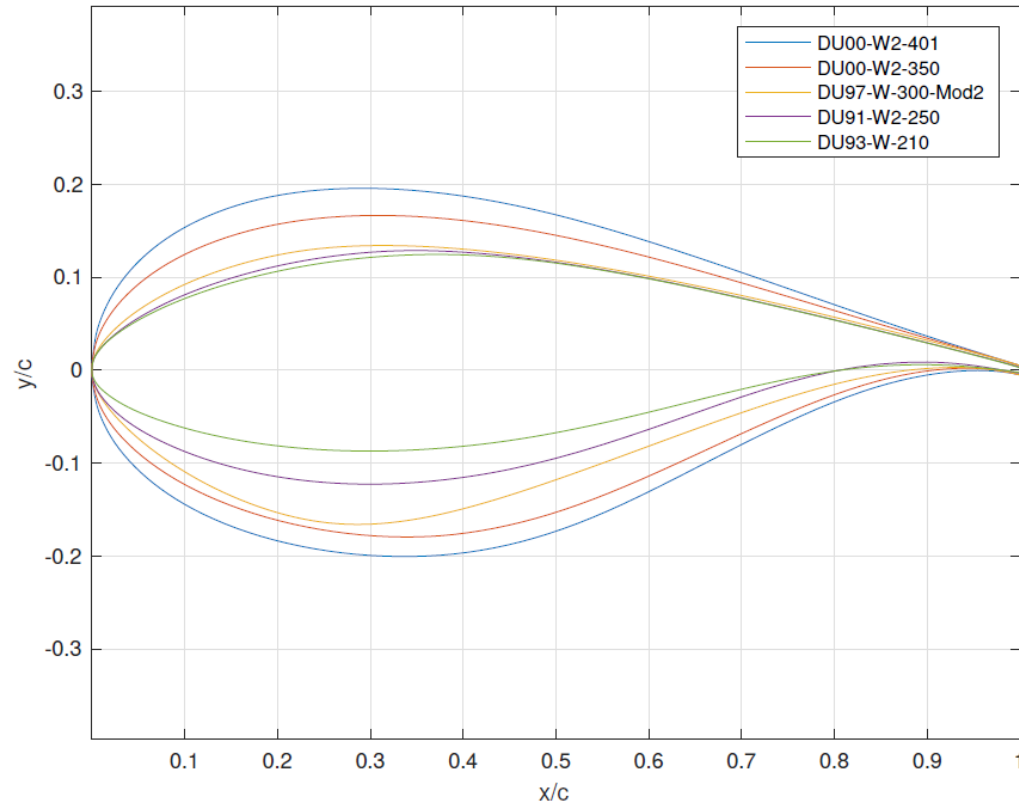
Interesting features of low Specific Power Turbines

- High Reynold's number
 - Thicker airfoils can be used outboard to increase structural efficiency
 - Improved airfoil performance
- No Region 2.5
 - The entire region below rated power can be operated at the design point, Region 2
 - Can operate at a lower design efficiency ($a < 1/3$) with an equivalent operational efficiency
- Reduced tip speed / noise



Airfoil selection and placement

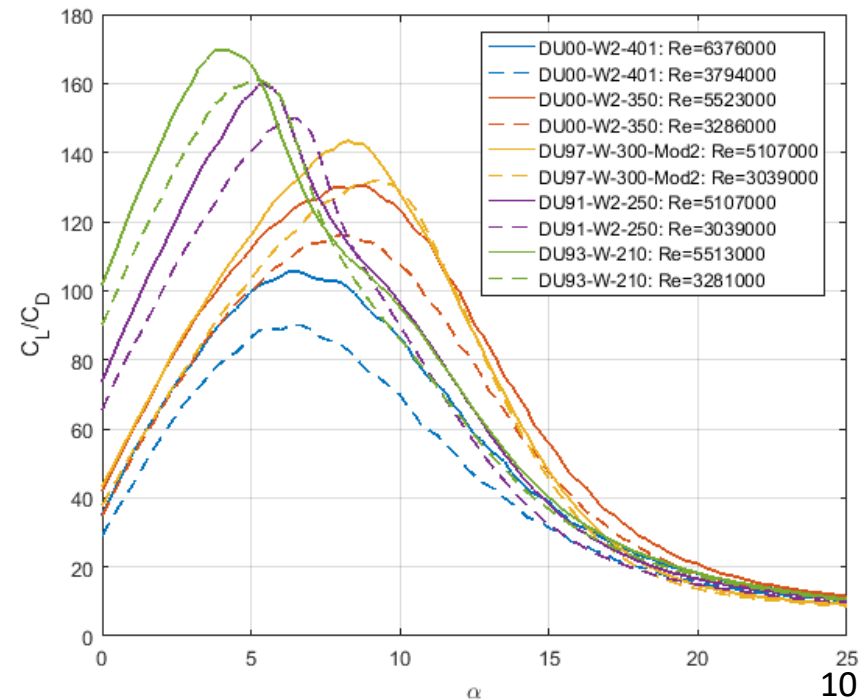
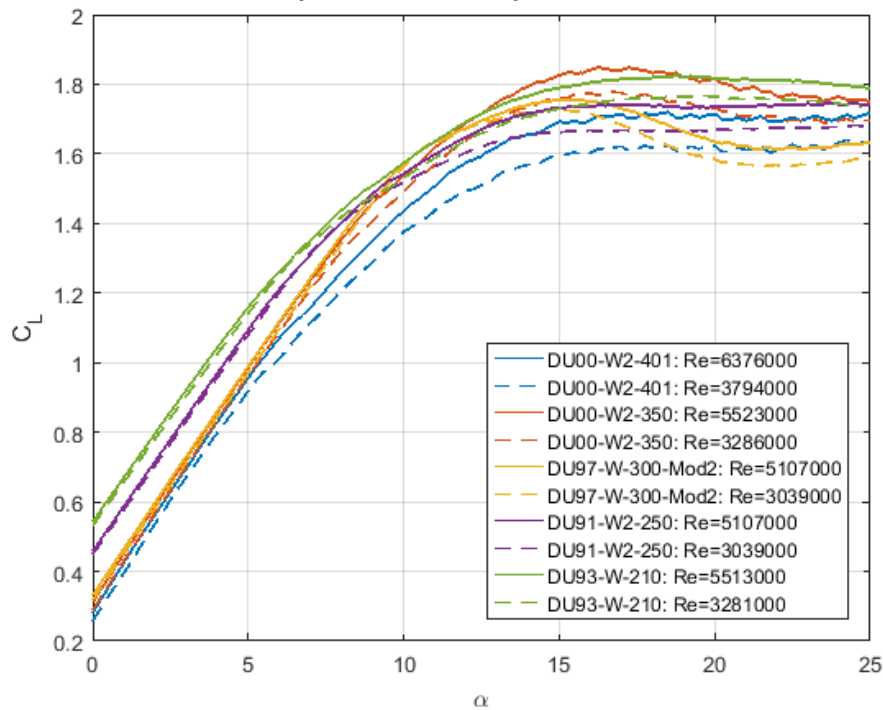
Airfoil Name	Percent Thick	Blade Span (r/R)
Circle	100%	0.00
DU00-W2-401	40%	0.12
DU00-W2-350	35%	0.23
DU97-W-300-Mod2	30%	0.40
DU91-W2-250	25%	0.74
DU93-W-210	21%	0.96



- DU-series airfoils were selected with similar shapes chosen that enable smooth transitions and lofting along the blade
- However, many of these airfoils were designed for stall-regulated machines and weren't designed to be an "airfoil family"

Simulated airfoil polars

- The absence of high Reynold's number experimental data forces the use of simulated airfoil polars in the design
 - There is a need for high Reynold's number designed and tested airfoils
- Design point chosen to operate at max lift to drag ratio
 - Produces an aerodynamically efficient blade, but a slender blade – may not be optimal from a cost of energy viewpoint



Low-induction rotor design

Optimization Parameters

$$\text{maximize}_{a(r/R)} \quad w \frac{AEP}{AEP_0} + (1 - w) \frac{C_P}{C_{P_0}}$$

$$\text{subject to} \quad M_{\text{rated}} = M_{0_{\text{rated}}}$$

$$P_{\text{rated}} = P_{0_{\text{rated}}}$$

$$0 < a < 0.5$$

$$\lambda = 9$$

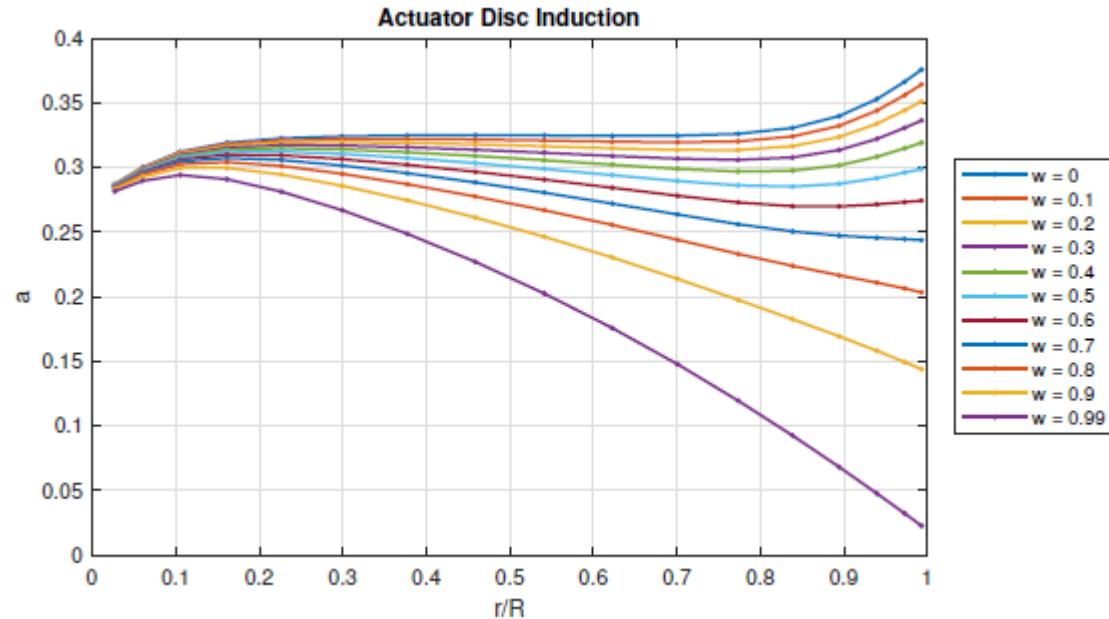
$$B = 3$$

$$\frac{L}{D} = 120, \quad \frac{r}{R} > 0.9$$

$$\frac{L}{D} = 160 \frac{r}{R}, \quad \frac{r}{R} \leq 0.9$$

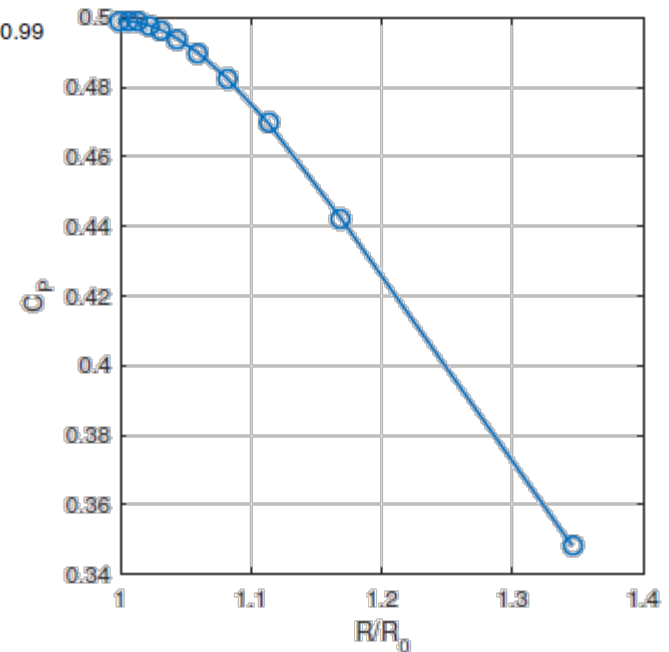
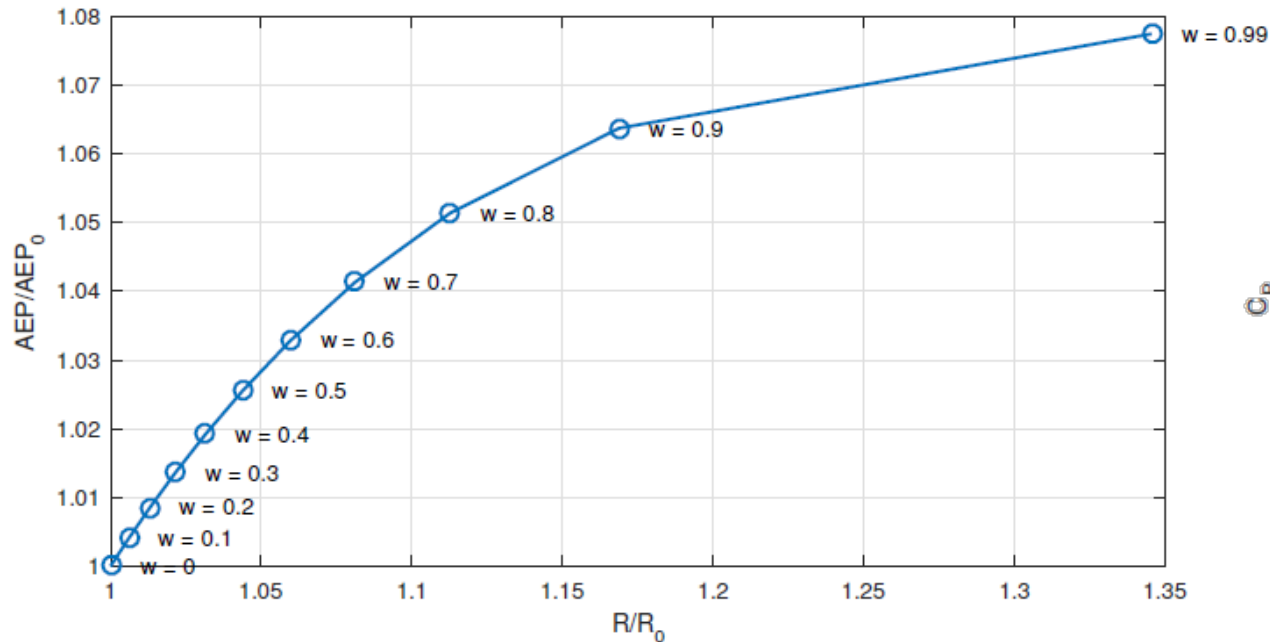
IEC Class III, Rayleigh Distribution, $U_{\text{mean}} = 7.5\text{m/s}$

Only Region 2 and 3, constant C_P until rated



*Christopher L. Kelley, presentation at WESC 2017

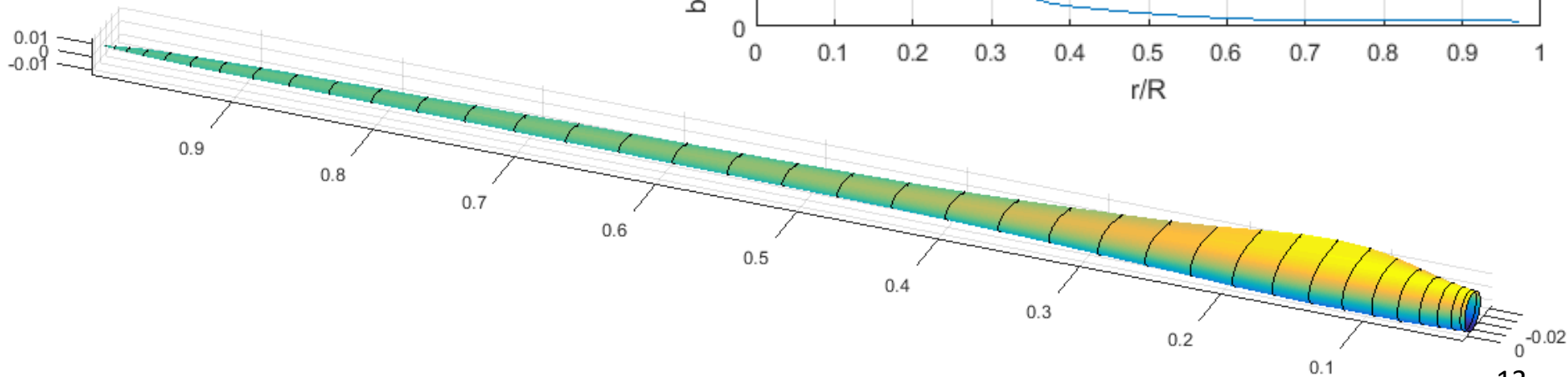
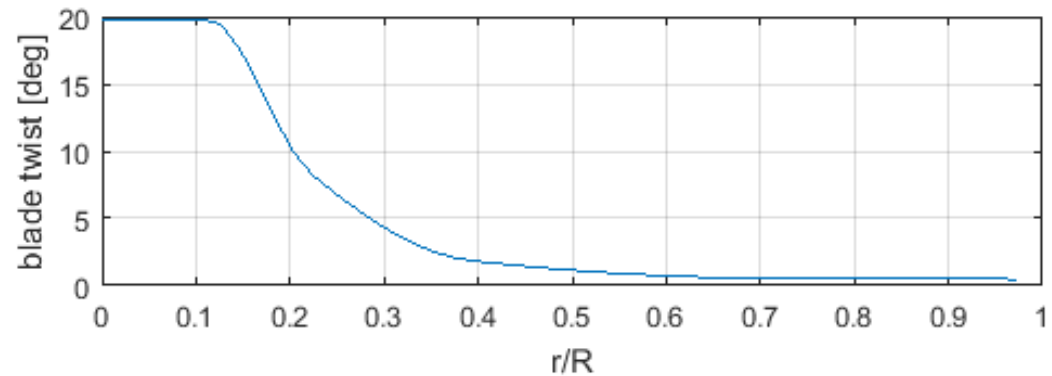
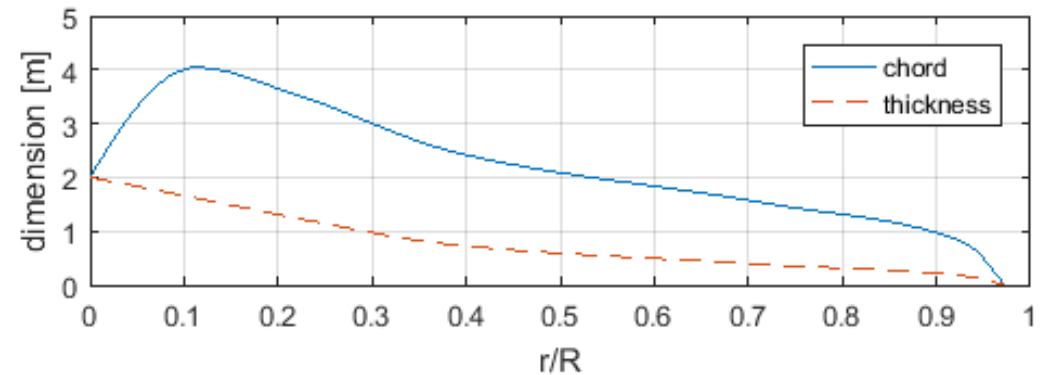
Low-induction rotor design



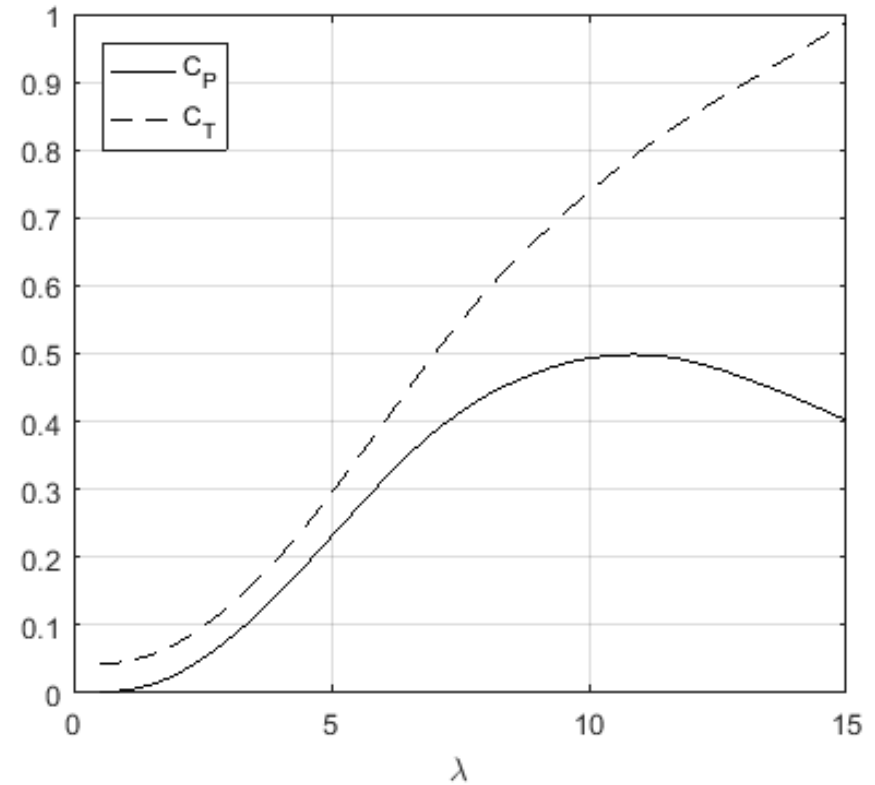
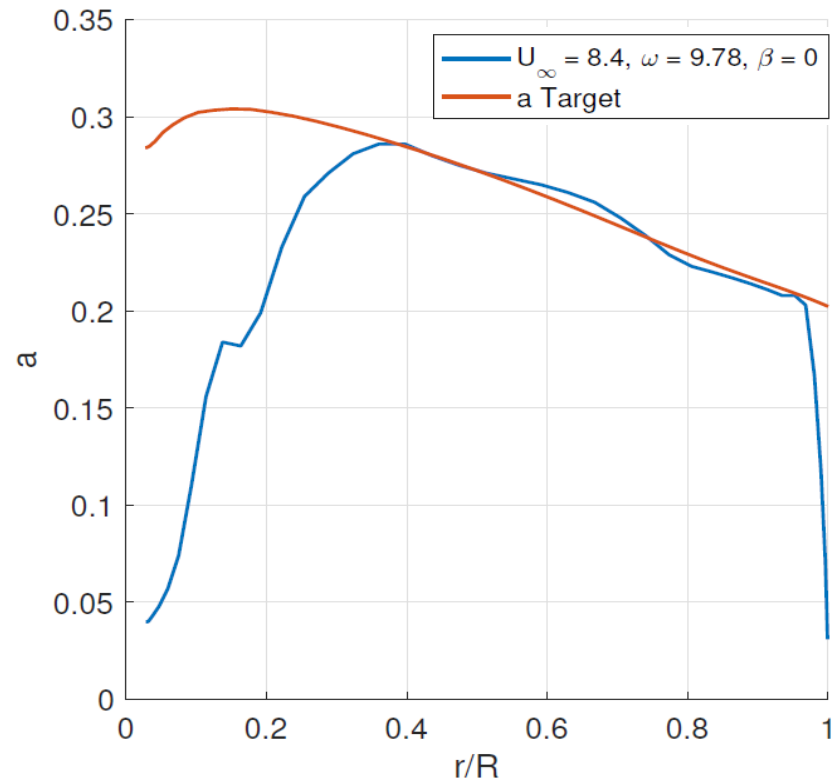
- Weighting factor of 0.8 (80% weight to AEP, 20% weight to Cp) was chosen for the SNL3.0-148 model as a good trade-off between energy capture and blade length
 - Compared with an optimally designed blade ($a=1/3$), it has an 11% increase in rotor radius and a 5% increase in annual energy production (AEP)

Initial blade design properties

- Realistic chord and twist profiles were designed that produce the induction profile, with limitations included for manufacturability and transportation
- Blade solidity = 2.85%



Initial blade design properties



- Initial aerodynamic design matches the desired induction profile from 40% span outboard, and is limited inboard due to the restrictive chord and twist limitations
- At the design point: $C_p = 0.47$, $C_t = 0.67$

Next steps

- Iterative process to produce the final aerodynamic and structural design (SNL3.0-148.s0)
 - All-fiberglass design
 - IEC III-A
- Blade models will be released publicly for use by the broader research community
- Aerodynamic design will be utilized to assess the usefulness of different carbon fiber materials in the spar cap from a blade cost analysis
 - Part of the DOE-funded SNL/ORNL/MSU optimized carbon fiber project