

Shock Waves and Defects in Energetic Materials, a Match Made in MD Heaven

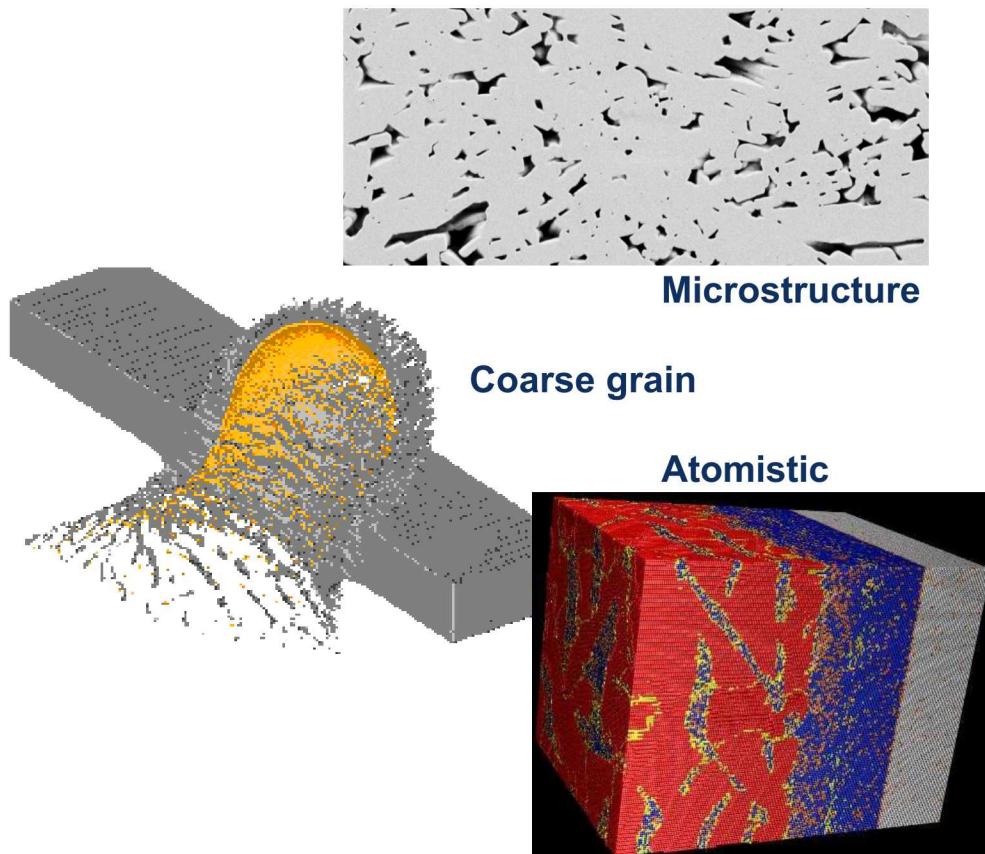
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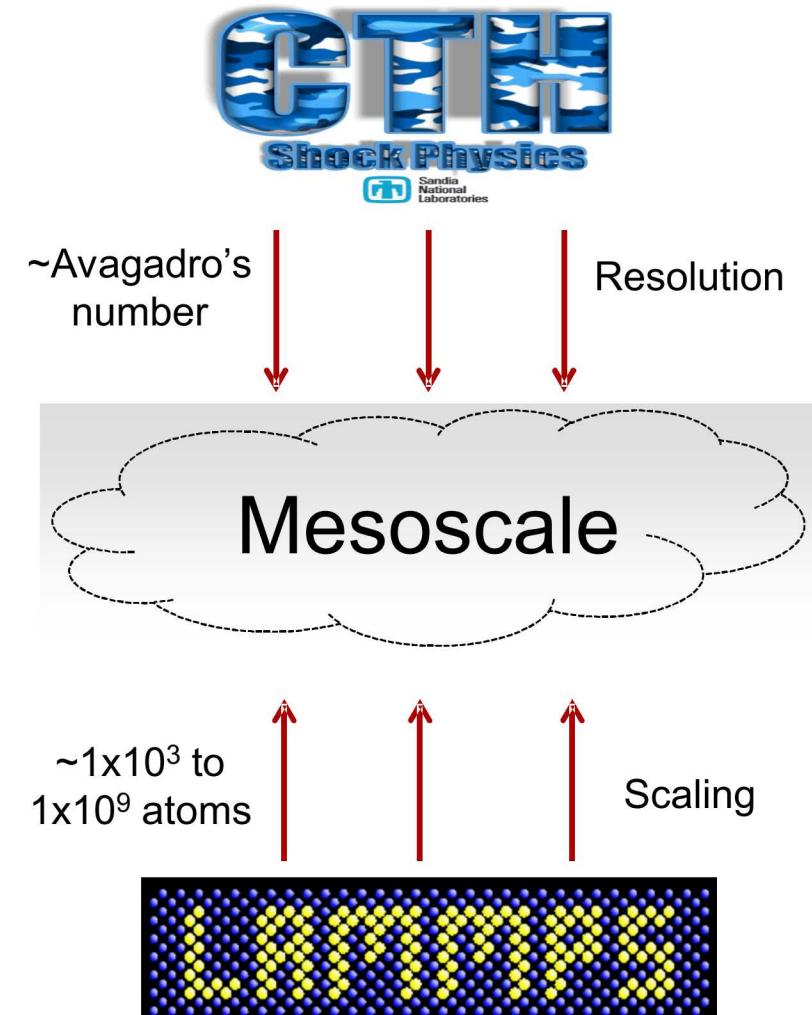
APS March 2017 Meeting

March 14, 2017

Mesoscale Materials Modelling

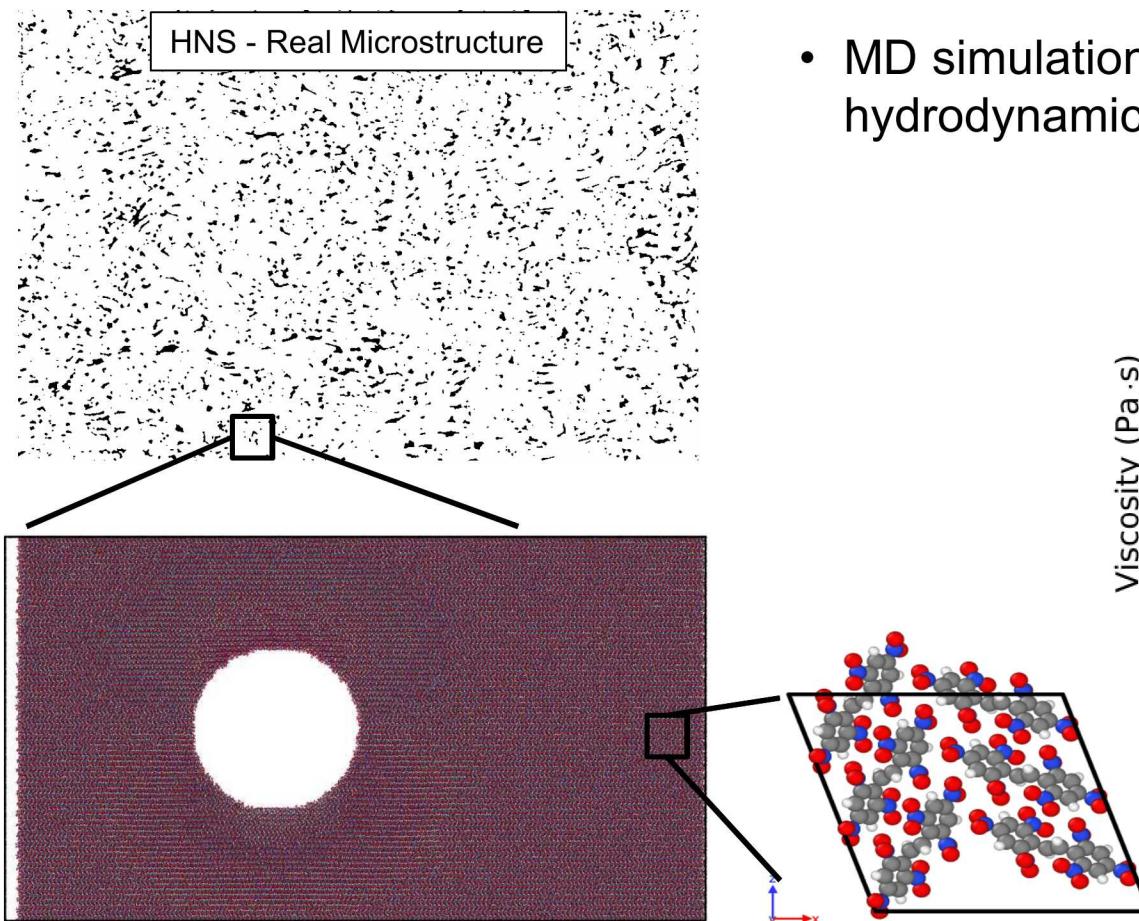


- Generally challenging problems involving physics at many length/time scales
- Shock to detonation transition in energetics fits the bill of being truly “mesoscale”

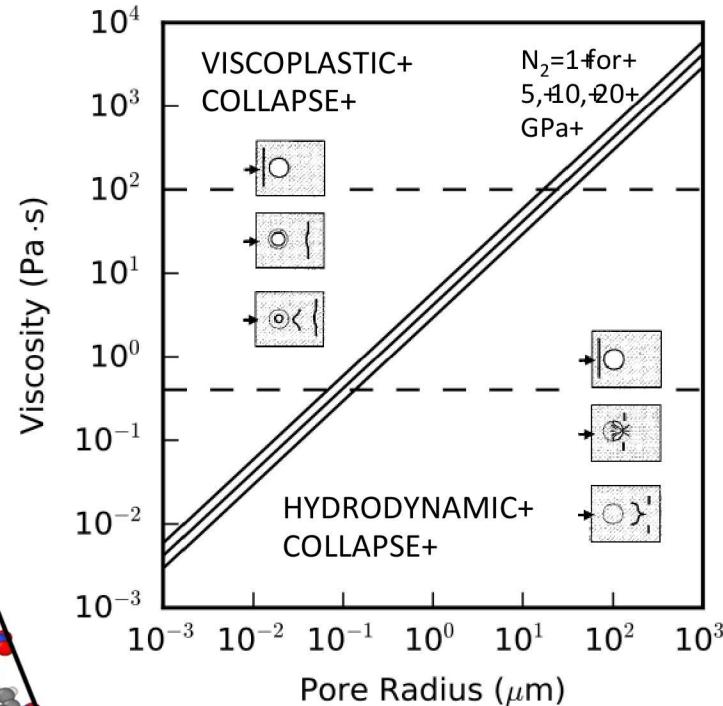


But Why Molecular Dynamics?

- Want a predictive power that spans from atoms to devices

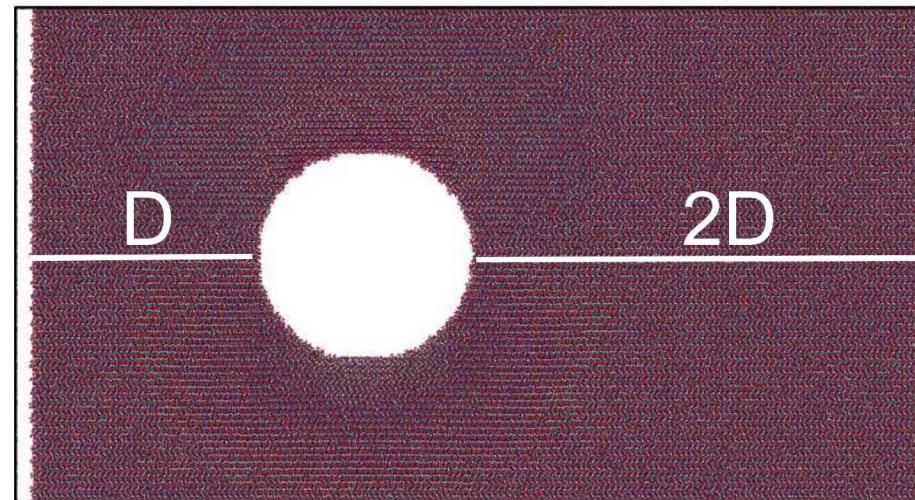
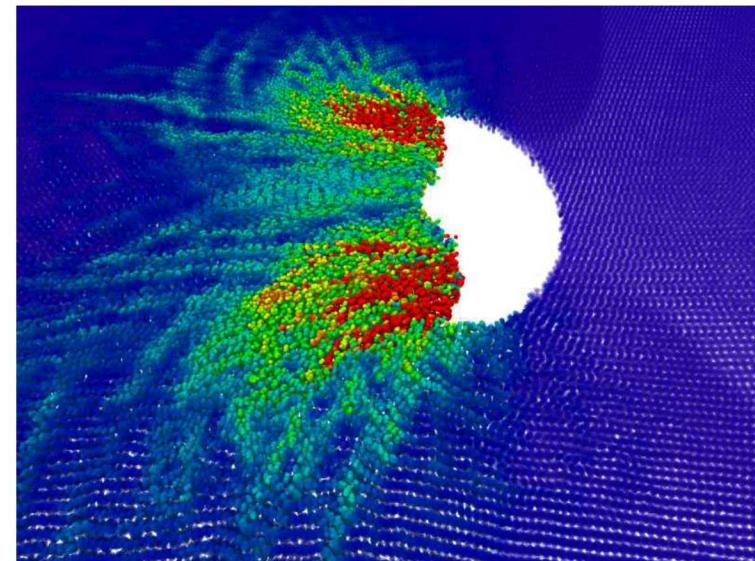
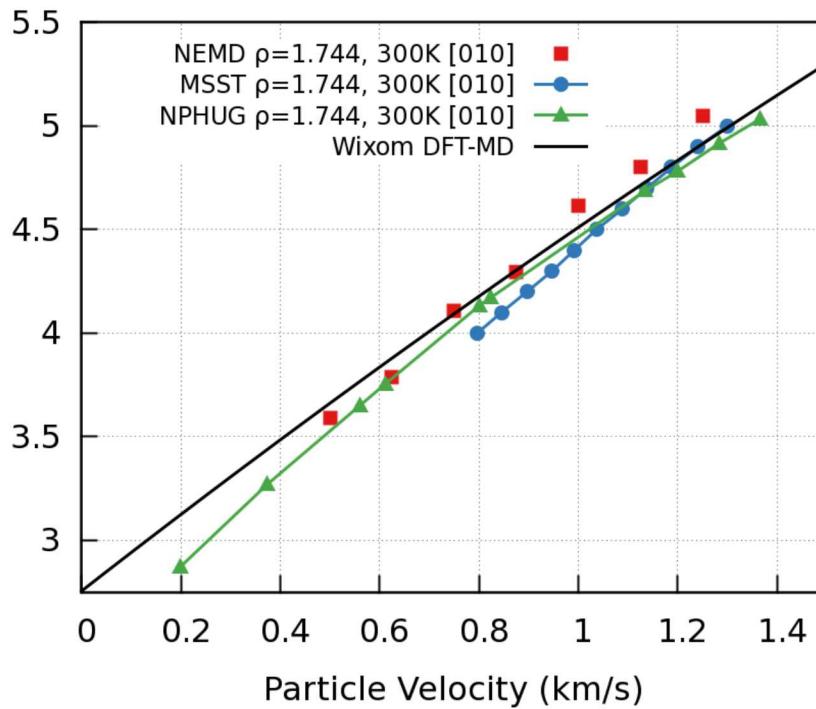


- Results inform and train continuum models for mesoscale applications**
- MD simulations need to span the hydrodynamic to viscoplastic range



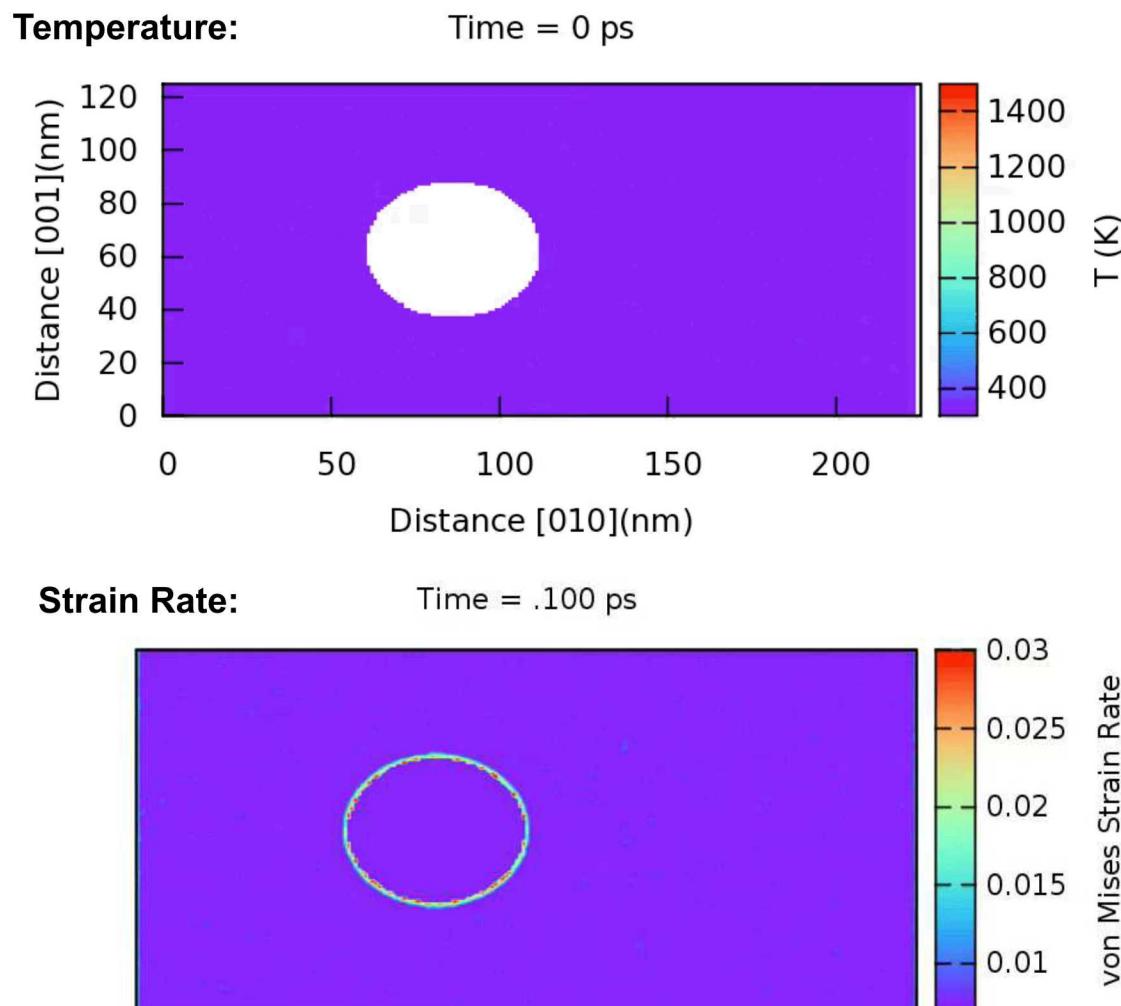
Validation of the Interatomic Potential

- Need to define a test geometry for both codes (LAMMPS, CTH)
- Small adjustments made to ReaxFF-lg potential for HNS

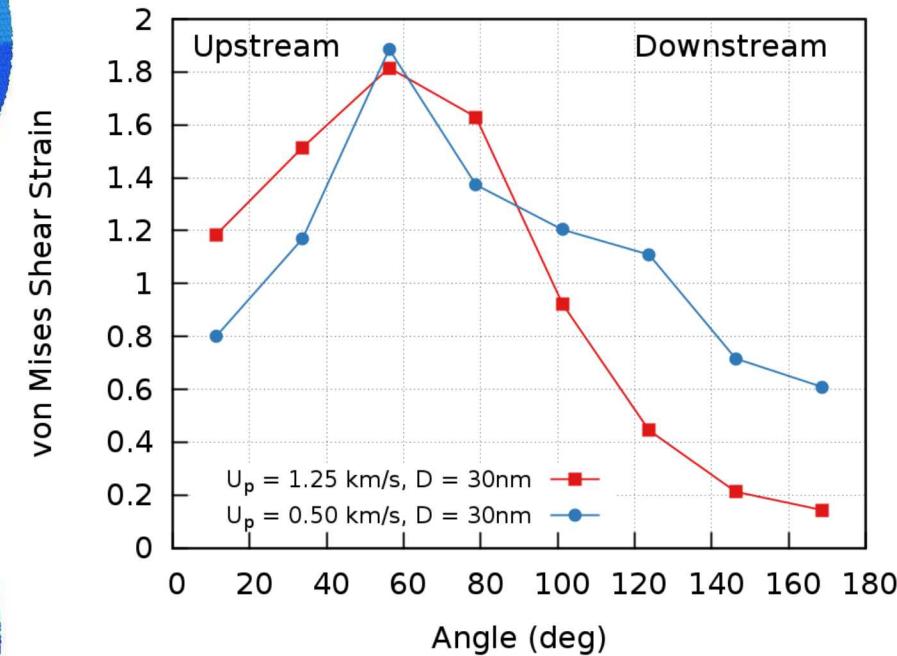
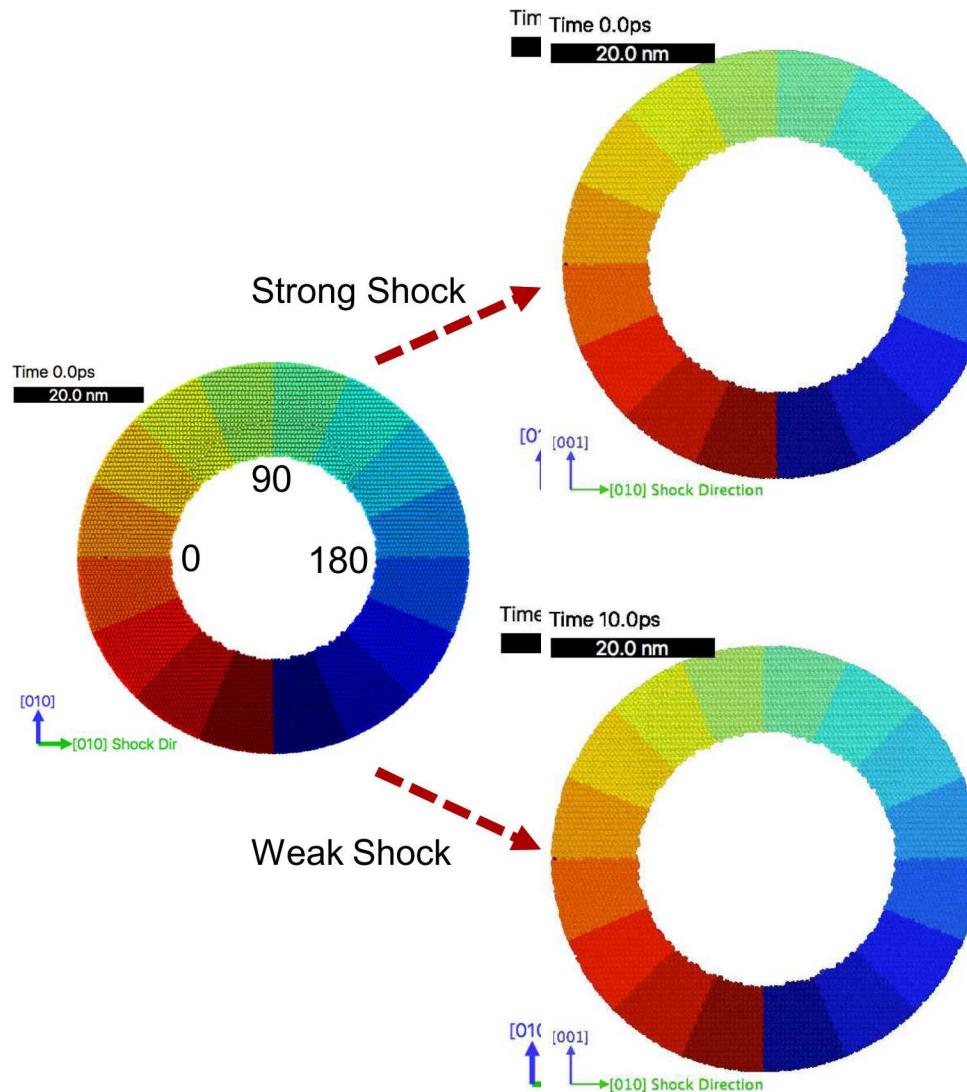


Shock to Initiation, Deflagration

- Detailed chemistry is incorporated in these MD potentials, hot spot evolution is captured naturally.
- Current computing capabilities for ReaxFF within LAMMPS is $\sim 10^8$ atoms, which is $1\mu\text{m}$ by $0.5\mu\text{m}$ of HNS
- KOKKOS-Reax/c package circumvents memory overflow errors and makes the code portable to hybrid architectures

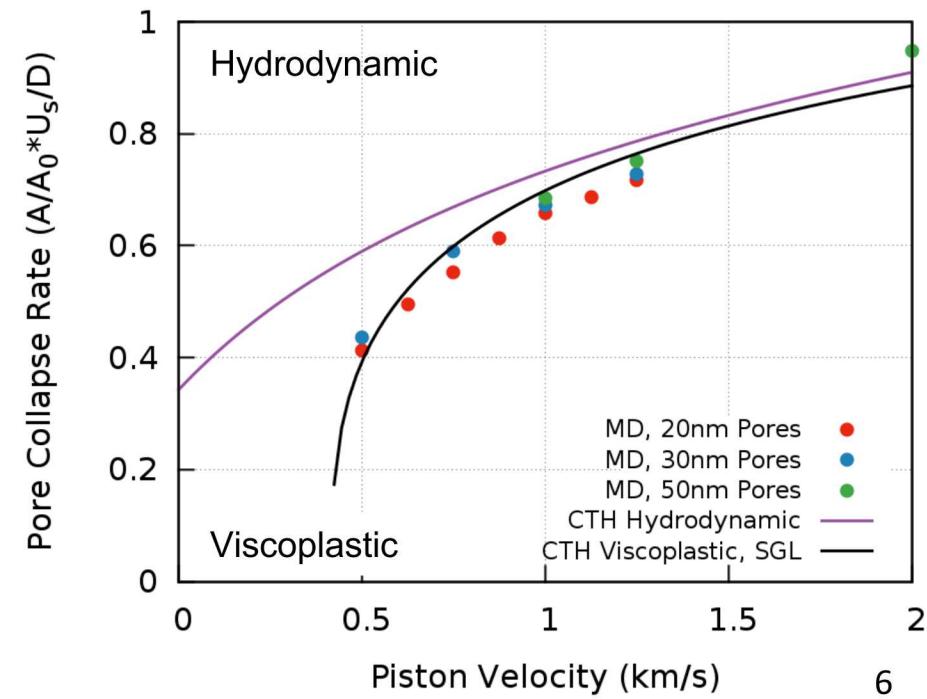
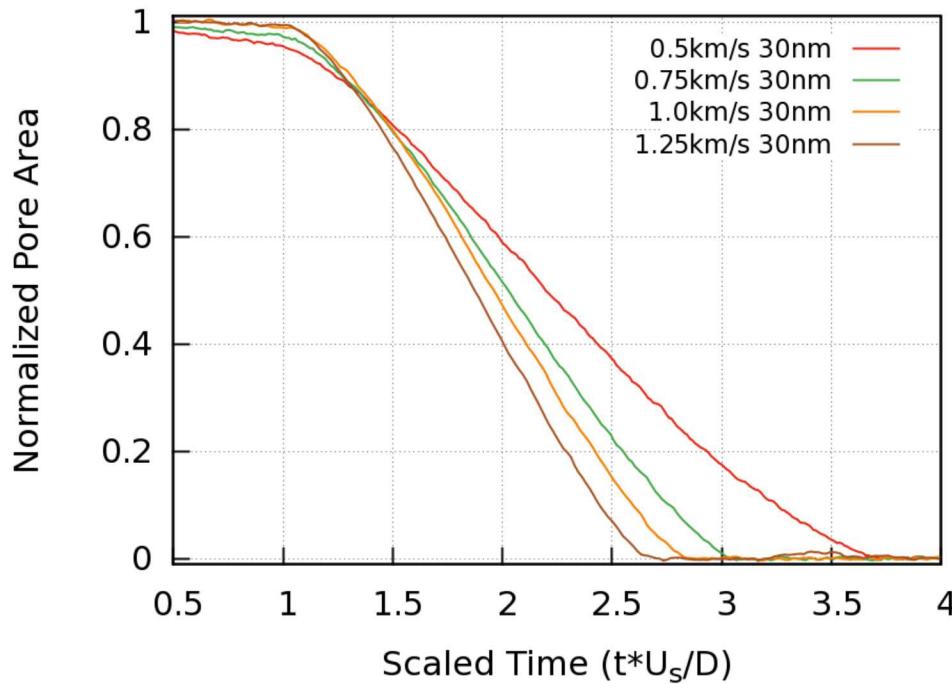


Hydrodynamic vs. Viscoplastic Pore Collapse



Connection to the Continuum Scale

- Pore size has a weak effect on pore collapse behavior, at least in the MD accessible range which for us was up to $0.25\mu\text{m}$ ($1.3 \cdot 10^8$ atoms).
- CTH strength model is fitted based on the MD prediction of pore collapse rate



Strain Rate Dependent Model – Steinberg and Lund (1989)

- We believe that only a strain rate-dependent model can match MD results for viscoplastic pore collapse; EPPVM and Johnson-Cook are not up to the task.
 - Assume a constant shear modulus of $G_0 = 5686 \text{ MPa}$
 - Neglect work hardening but assume $Y_A = 140 \text{ MPa}$
 - Assume linear variation of the Grüneisen parameter, $\gamma_0 = 1.625$
 - Melt temperature $T_{m0} = 588 \text{ K}$

Yield Strength:

$$Y = \{Y_T(\dot{\varepsilon}_p, T) + Y_A f(\varepsilon_p)\}$$

Shear Modulus:

$$G(P, T) = G_0$$

Work Hardening:

$$Y_A f(\varepsilon_p) = Y_A \leq Y_{max}^*$$

Thermal Activation:
(Implicit Equation)

$$\dot{\varepsilon}_p = \left\{ \frac{1}{C_1} \exp \left[\frac{2U_K}{kT} \left(1 - \frac{Y_T}{Y_P} \right)^2 \right] + \frac{C_2}{Y_T} \right\}^{-1}$$

SGL 4 DOF Best Fit

$$C_1 = 2.025 \times 10^{11} \text{ s}^{-1}$$

$$C_2 = 11.25 \text{ dyne-s/cm}^2$$

$$Y_P = 1114 \text{ MPa}$$

$$U_K = 0.1358 \text{ eV}$$

$$Y_T \leq Y_P$$

Melting Curve:
($Y = 0$ when $T \geq T_m$)

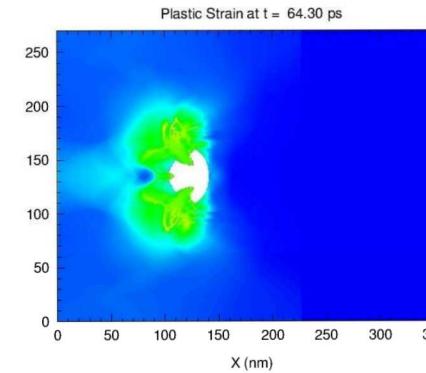
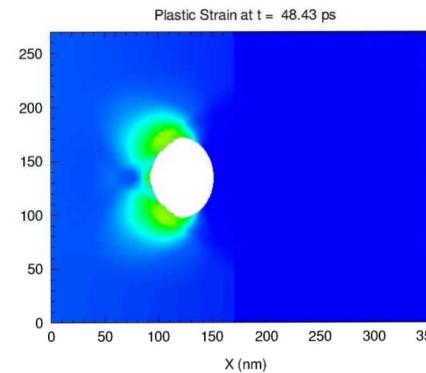
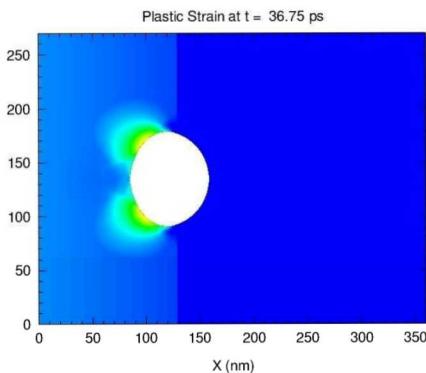
$$T_m = T_{m0} \exp \{2a(1 - 1/\eta)\} \eta^{2(\gamma_0 - a - 1/3)}$$

Grüneisen parameter:

$$\gamma = \gamma_0 / (1 + \mu)$$

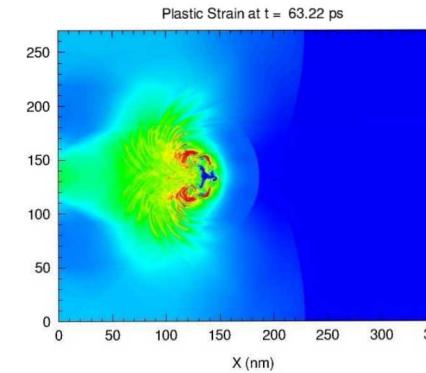
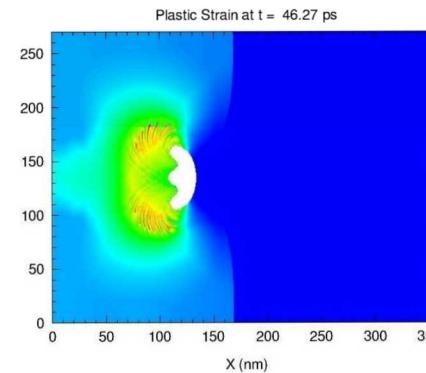
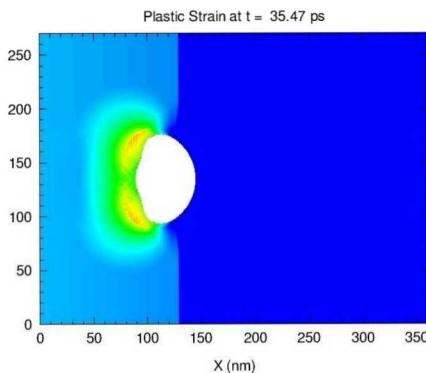
Strain Rate Dependent Model – Results

0.6 km/s

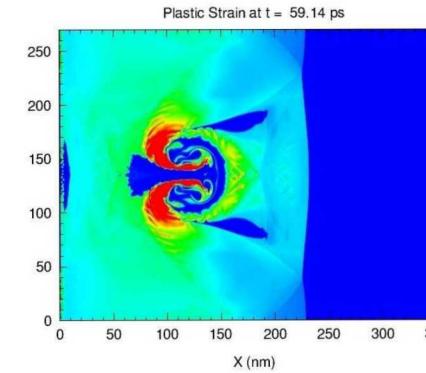
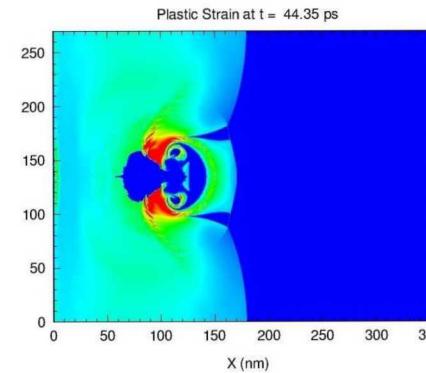
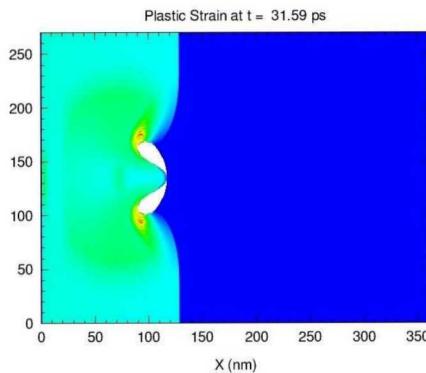


**Viscoplastic
Response**

1.0 km/s



2.0 km/s



**Hydrodynamic
Response**

Conclusions and Path Forward

- By training a strain-rate dependent CTH strength model for HNS to reproduce MD predicted viscoplastic shock response, we have been able to obtain consistent pore collapse behavior.
- Initiation behavior as a function of this viscoplastic character is an avenue for future work on both the MD and CTH codes.

