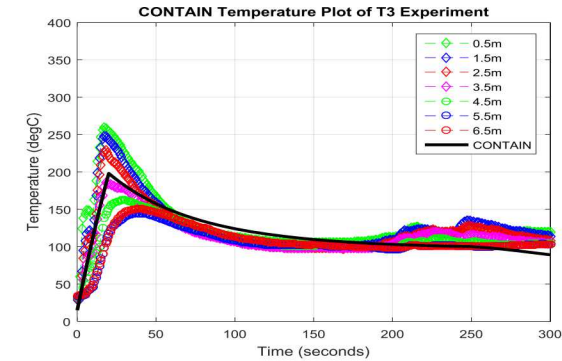
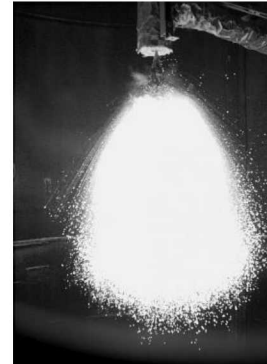
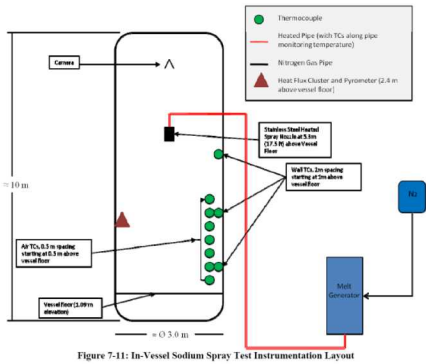


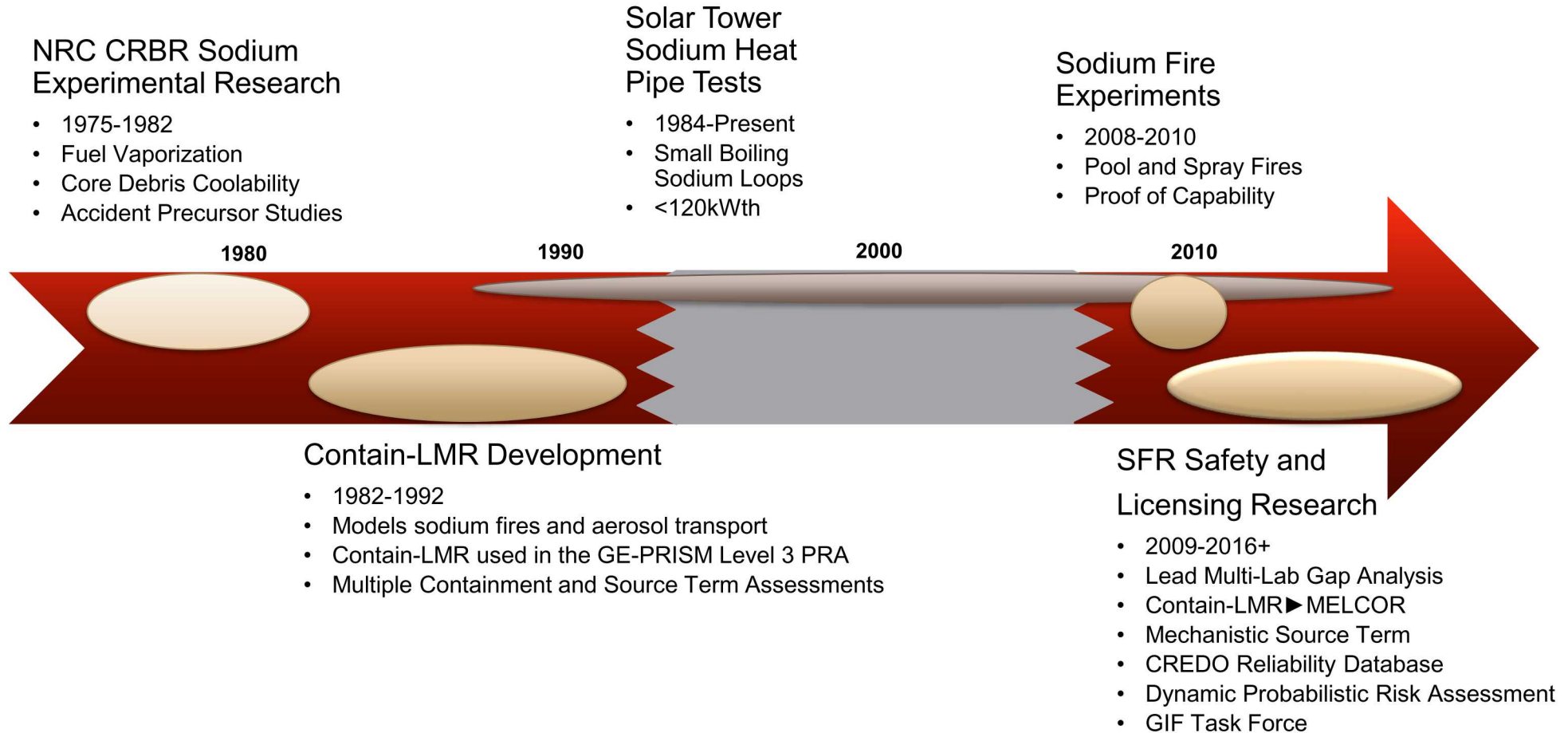
Exceptional service in the national interest



2010 LDRD Sodium Fires and MELCOR-Na

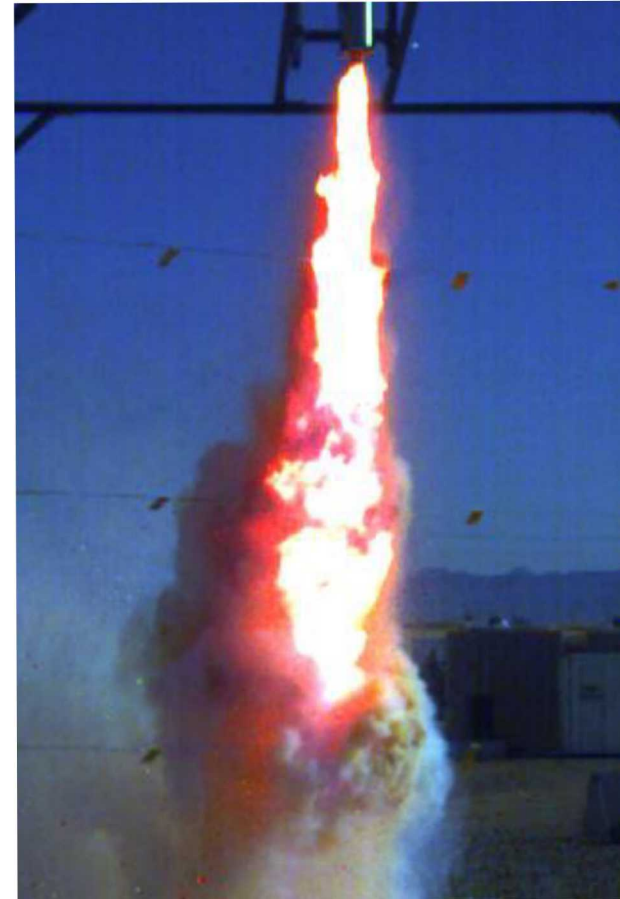
Matthew Denman
Andrew Clark, Larry Humphries, David Louie
Severe Accident Analysis and Risk and Reliability Analysis
Presentation to the IRSN
October 10th 2016

Sandia Sodium Reactor Safety Research



Outline

- MELCOR-Contain/LMR Integration
 - Sodium Fire Testing
 - Outdoor Pool and Spray Fires
 - In-Vessel Fires at Surtsey
 - Sodium Fire Modeling





SNL Sodium Fire Testing

2008-2010

Surtsey Facility

Quick overview of Outdoor Tests

In-depth examination of In-vessel Tests



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Sodium Fire Testing At SNL

- Goals
 - Establish a general metal fire expertise and analysis capability at SNL to address a key safety issue for the next generation of nuclear reactors.
- Sodium Spray Fires Experiments
 - 2 outdoor and 2 in-vessel experiments
 - Measured spray heat fluxes and temperatures
 - Varied average droplet diameters and sodium temperatures
- Sodium Pool Fire Experiments
 - 11 outdoor experiments
 - Measured surface heat fluxes and pool temperatures
 - Varied thickness ratio of the stainless steel substrate to the liquid sodium

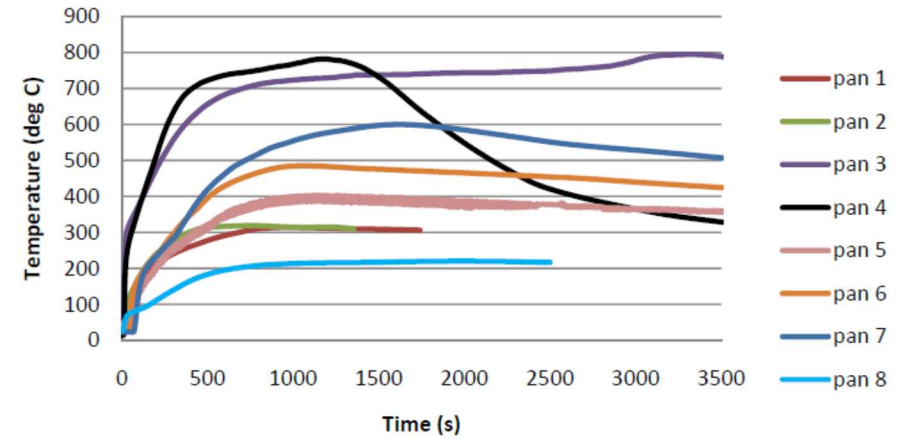
Surtsey Pool Fires

- Outdoor experiments, variable wind conditions and humidity (low)
- Various pan sizes and thermal couple layouts were used
- Average Pan temperatures plateaued at $\sim 800^{\circ}\text{C}$

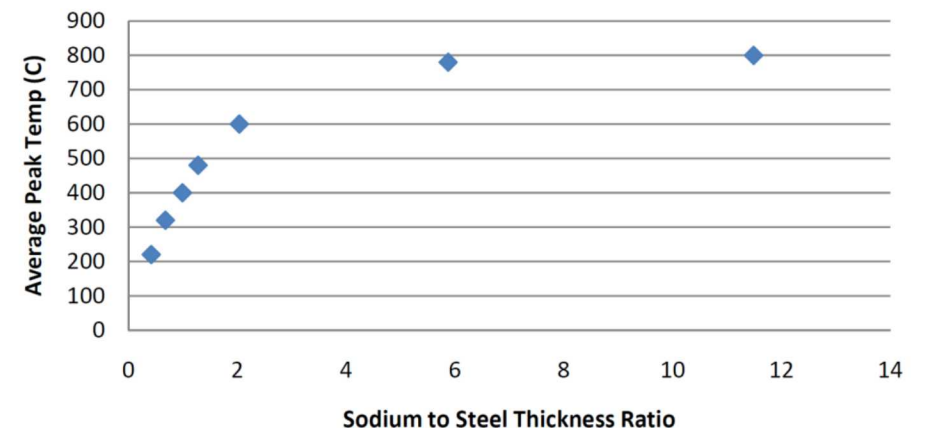
Table 2-3: Summary of Sodium Pool Fire Tests

Test Number	Diameter of Pan (m)	Height of Pan (m)	Mass of Sodium (kg)	Base Steel Thickness (mm)	Melt Generator Pressure at System Dump Time (psi)	Average Peak Temperature at Bottom of Pan (deg C)	Thickness Ratio (liquid sodium/stainless steel)
Pool 1	0.6	0.0508	2.6	15.875	2.6	320	0.7
Pool 2	0.6	0.0508	2.6	15.875	2.2	320	0.7
Pool 3	0.3	0.127	4.4	6.35	2.4	800	11.5
Pool 4	0.2	0.1778	1.0	6.35	2.5	780	5.9
Pool 6	0.6	0.0508	4.8	15.875	3.2	480	1.3
Pool 7	0.6	0.0508	7.8	15.875	3.4	600	2.0
Pool 8	0.6	0.0508	1.6	15.875	3.6	220	0.4
Pool 9	0.6	0.0508	6.0	15.875	3.6	490	1.6
Pool 10	0.6	0.1016	11.6	15.875	3.2	746	3.0
Pool 11	0.6	0.1016	9.6	15.875	3.9	648	2.5

Average Bottom Pan Peak Temperatures vs Time



Average Bottom Pan Peak Temperatures



Pan 9 – D=0.6m, R=1.6, M=6kg Na Top View



Pan 9 – D=0.6m, R=1.6, M=6kg Na Side View



Thermal Camera Imaging Pool Fire

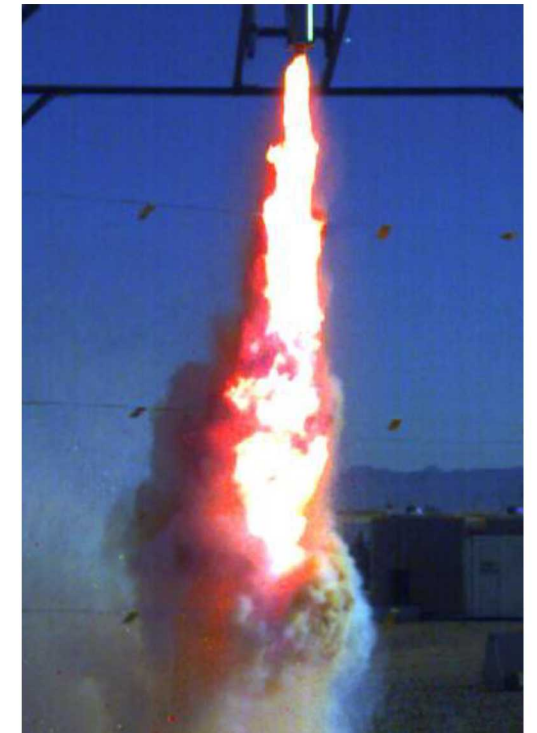


Outdoor Spray Fire Tests

Table 1: Summary of Outdoor Sodium Spray Fire Experiments

Location	Height of Spray (ft)	Amount of Na (kg)	Flow rate (kg/s)	Width of Spray at Ground (ft)	Median Particle Size Diameter (mm)	Temperature of Sodium (deg C)
Outdoor	15	4	1	2.4	~6	500
Outdoor	15	4	0.5	1.2	~10	500

- Objective: Understand the impact of flow rate and particle diameter on spray fires
- Sprays were directed onto a steel pan below the spray nozzle
- The slower and large diameter sprays resulted in subsequent pool fire



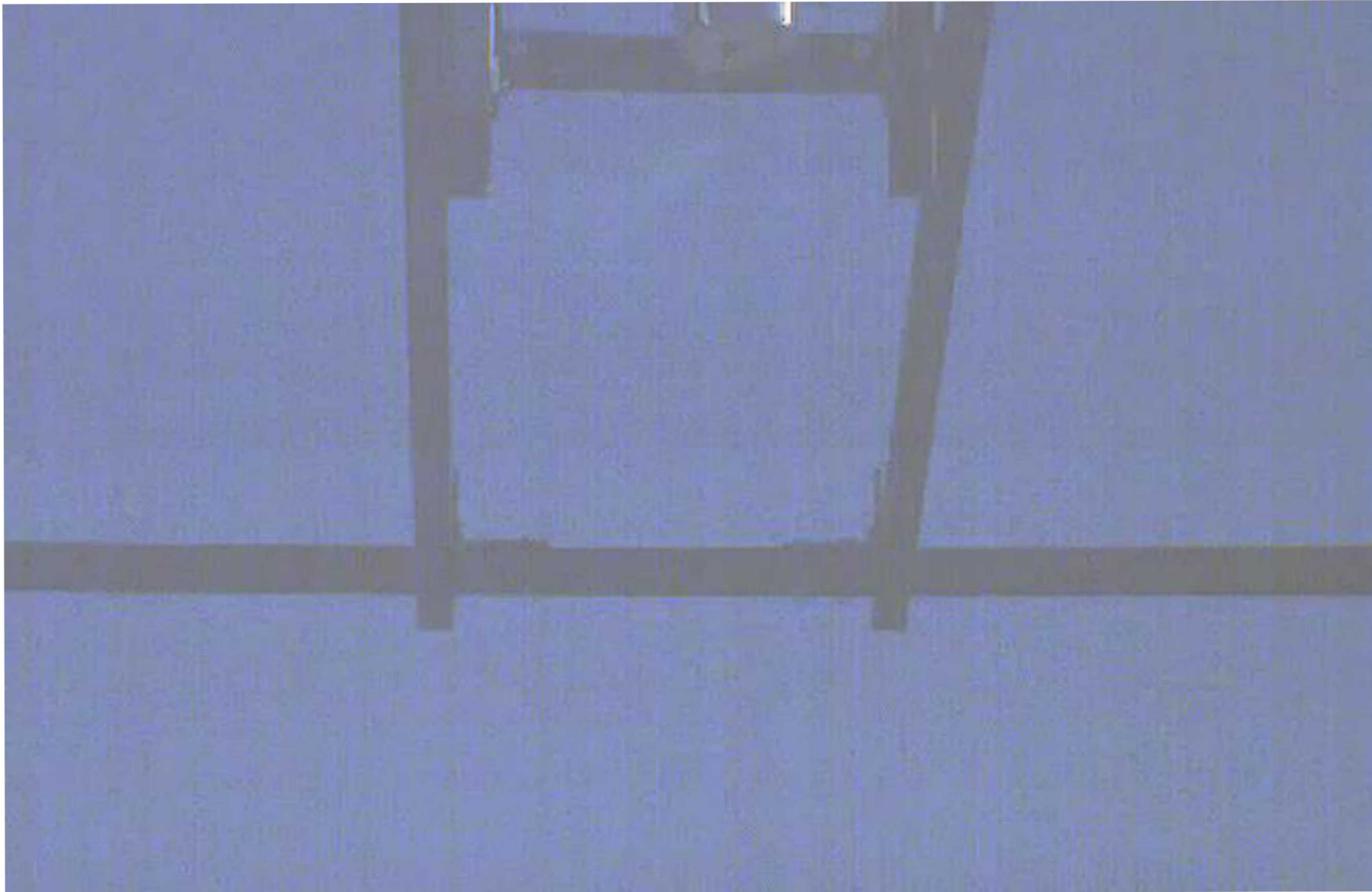
High Pressure Spray (T1)



Low Pressure Spray (T2) (1 of 2)



Low Pressure Spray (T2) (2 of 2)



Surtsey In-vessel Spray Fires

- Spray fire experiments conducted at Surtsey Facility at SNL
 - T3 sodium is near the ignition point.
 - T4 port failure causes a 6" diameter hole ~ 10 seconds into the accident
 - Sodium was sprayed onto a 5000 PSI limestone(?) concrete floor at the bottom of the vessel

Test #	T1	T2	T3	T4
Location	Outside	Outside	In-Vessel	In-Vessel
Height of Spray (m)	4.6	4.6	5.3	5.3
Amount of Na (kg)	4	4	20	20
Flow rate (kg/s)	1	0.5	1	1
Initial temperature of sodium (°C)	500	500	200	500
Melt generator pressure at system dump time (MPa)	2.14	0.196	2.12	2.12

In-Vessel Na Spray Fire Tests

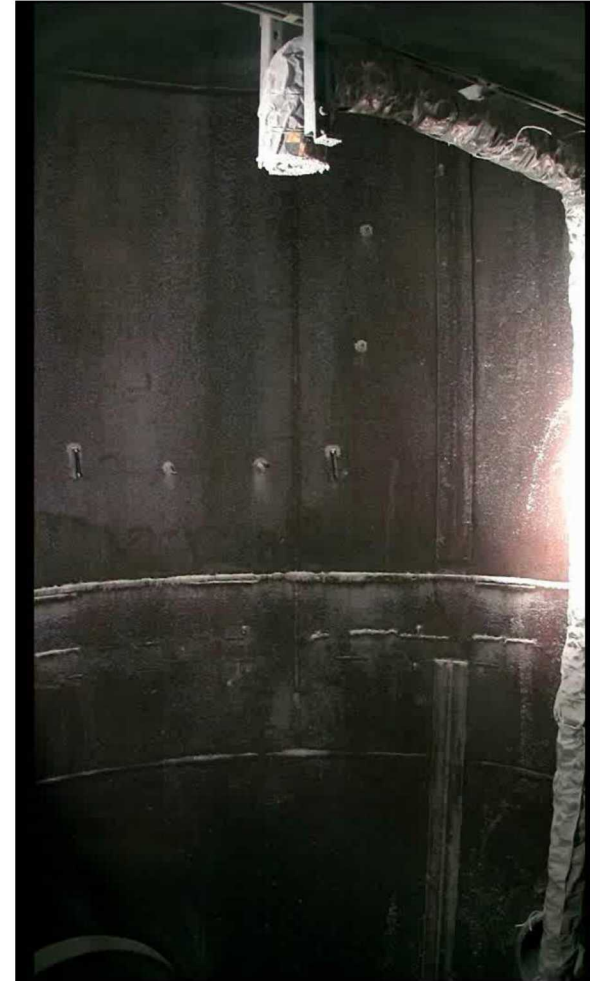
Side View

T3 Experiment



SAND2016-6688 PE

T4 Experiment



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In-Vessel Na Spray Fire Tests Top View

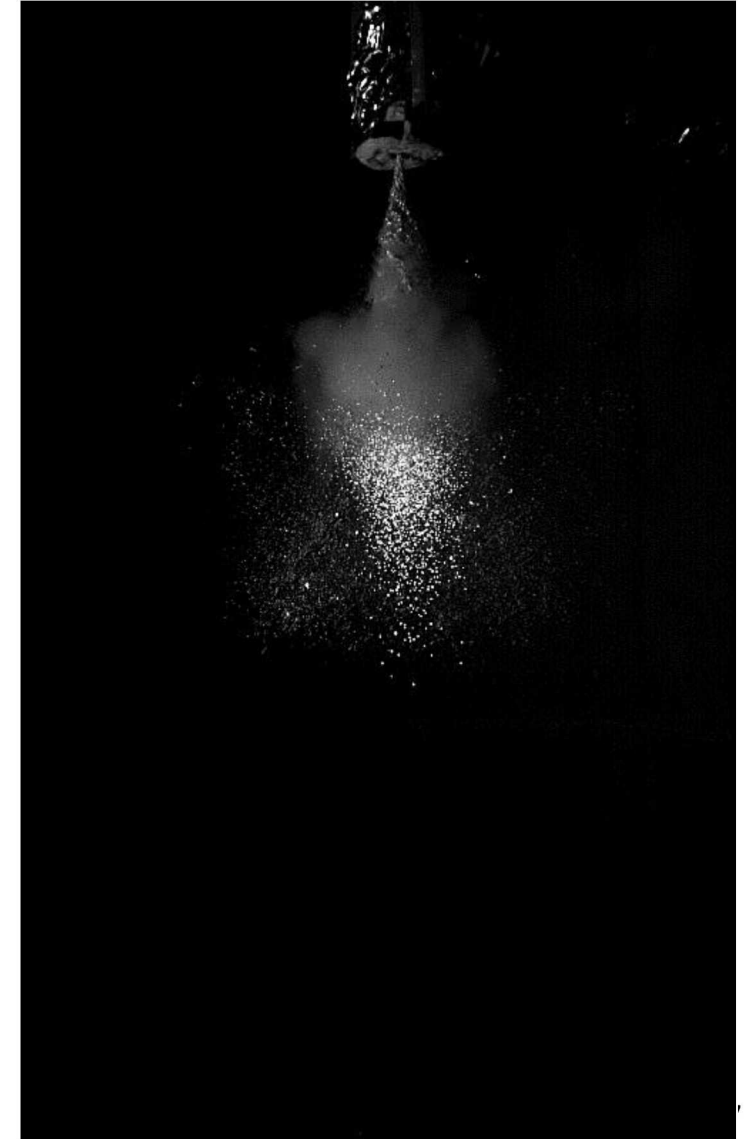
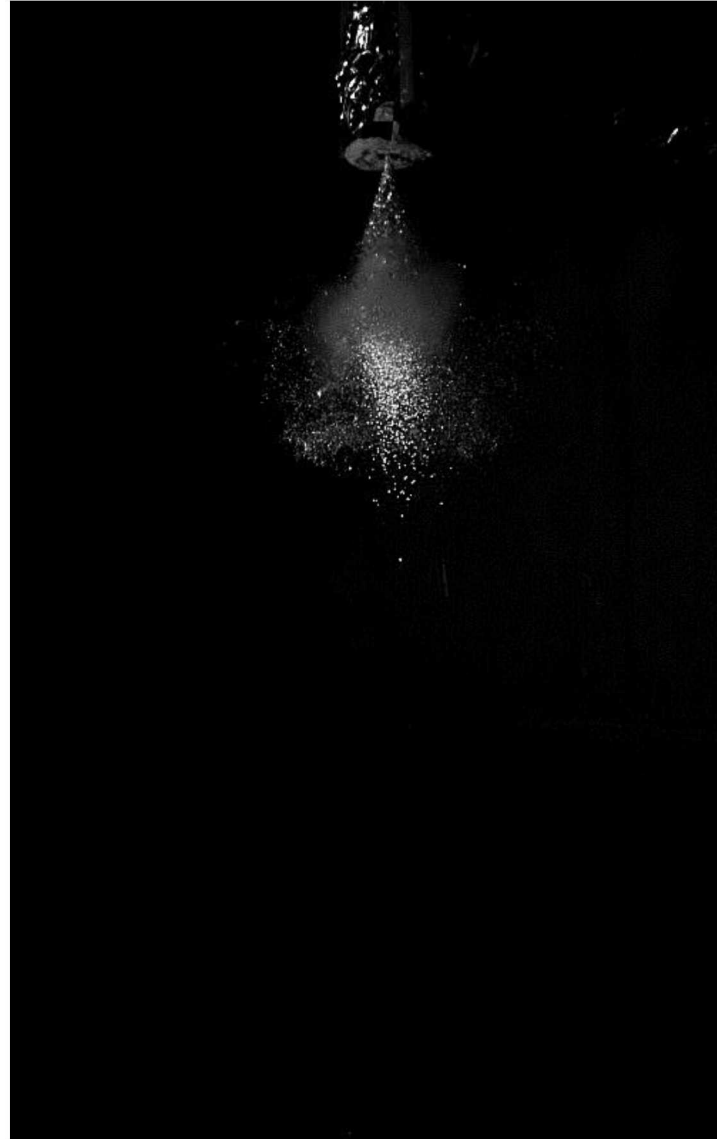
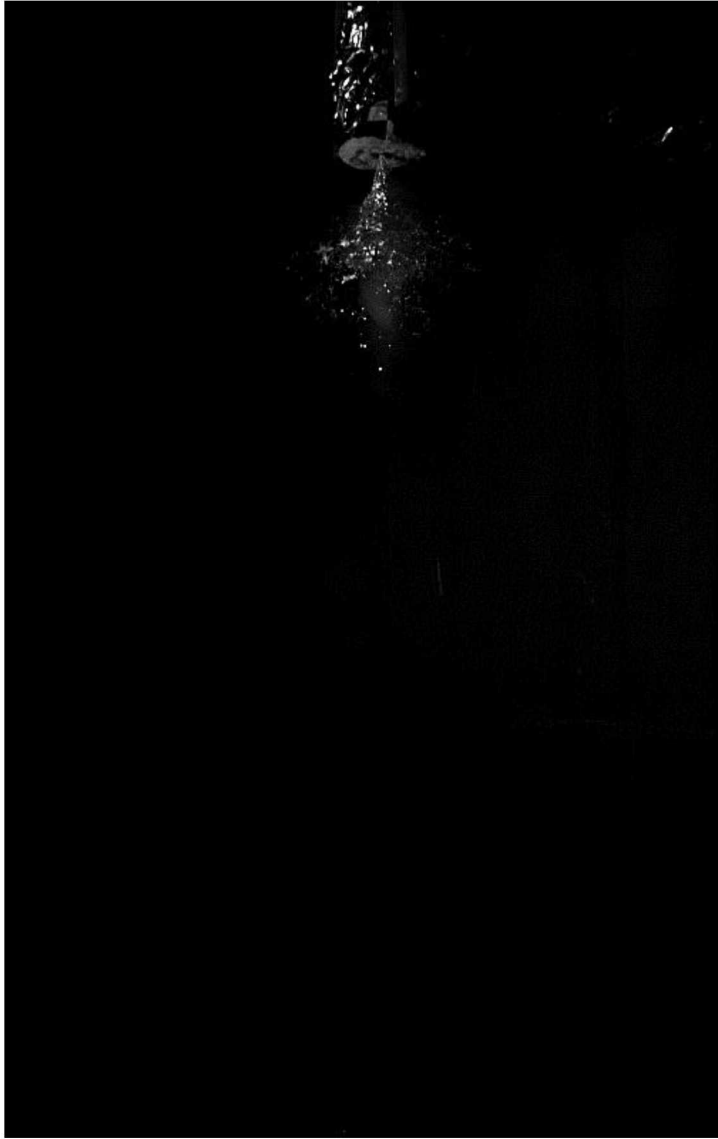
T3 Experiment



T4 Experiment

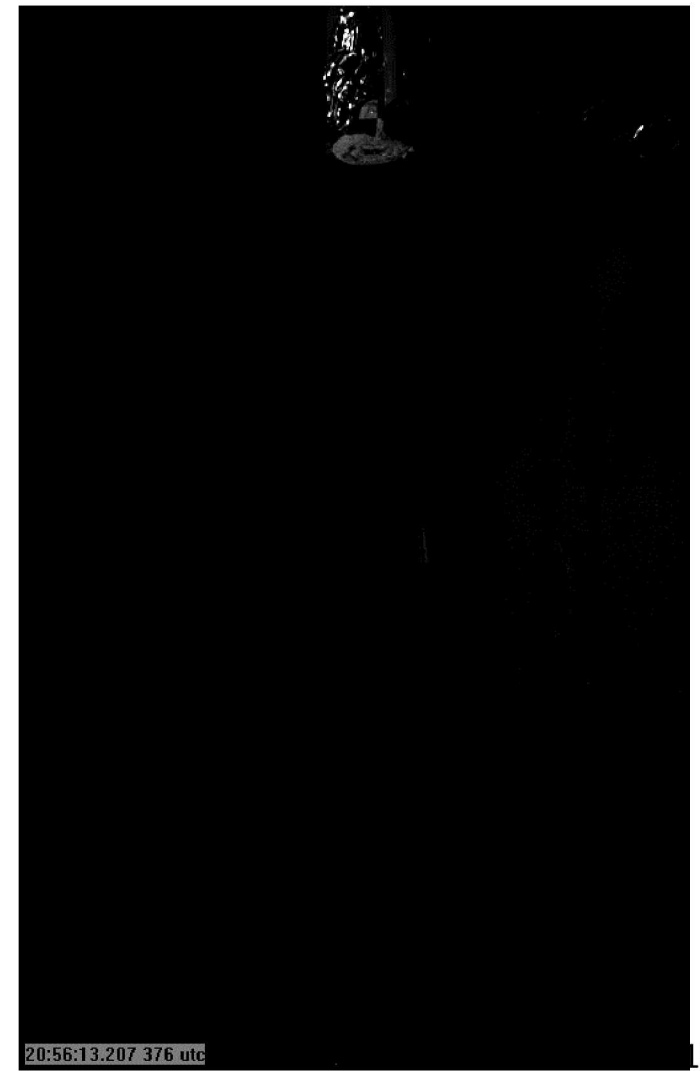


Screen Capture from T3 Early



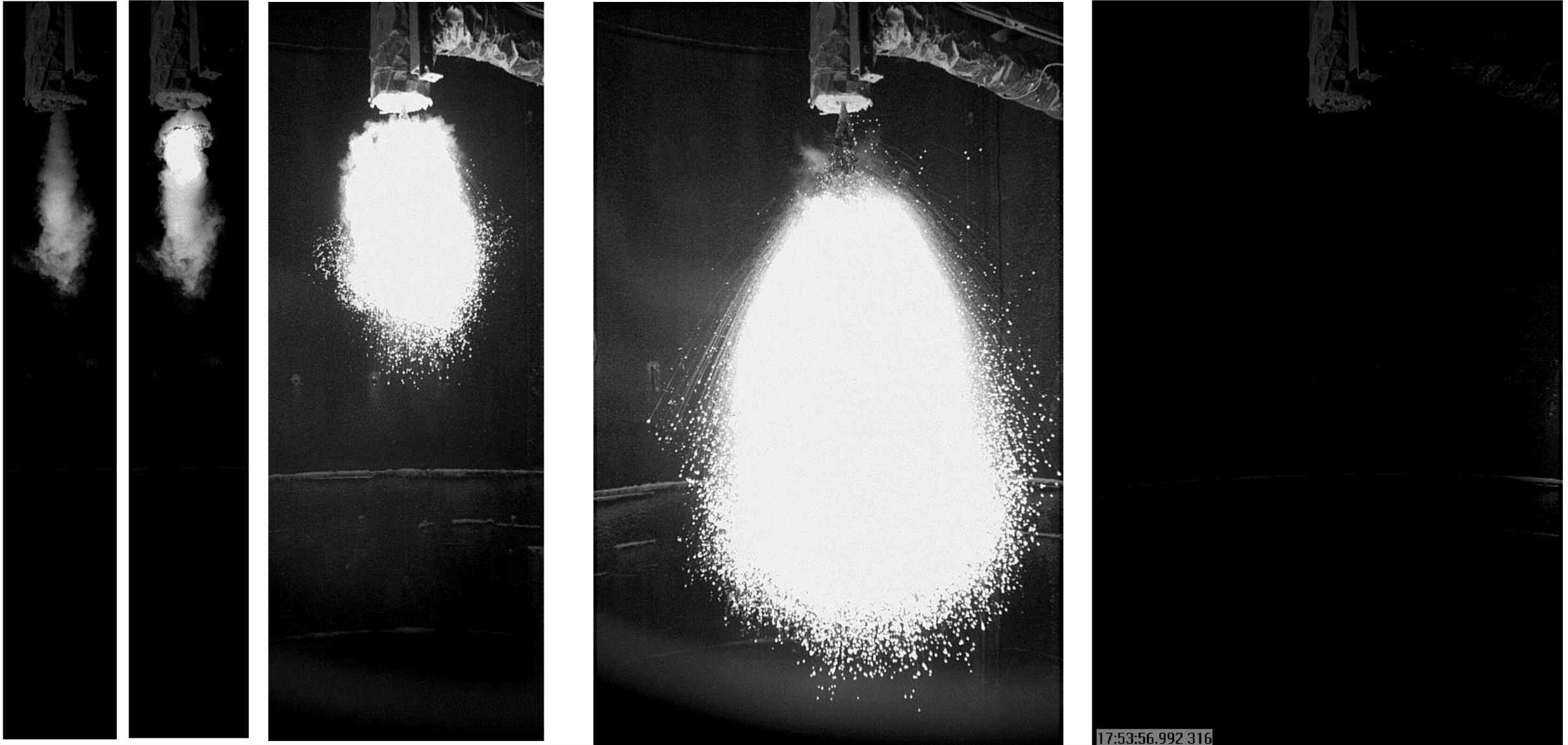
Screen Capture from T3 Late

SAND 2010-6911P



Screen Capture from T4

SAND2011-8856C



17:53:56.992 316

Concrete Ablation



Data Collected

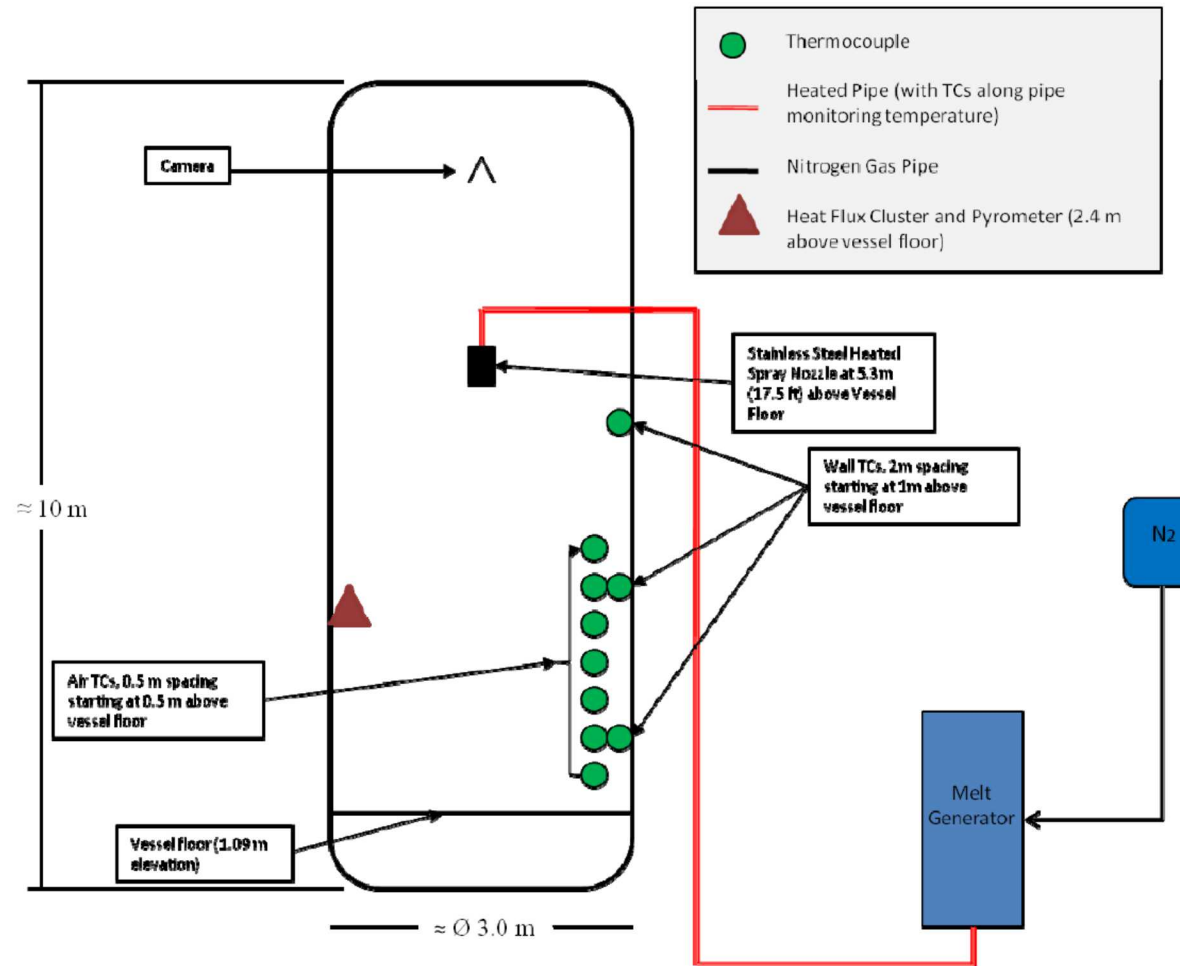
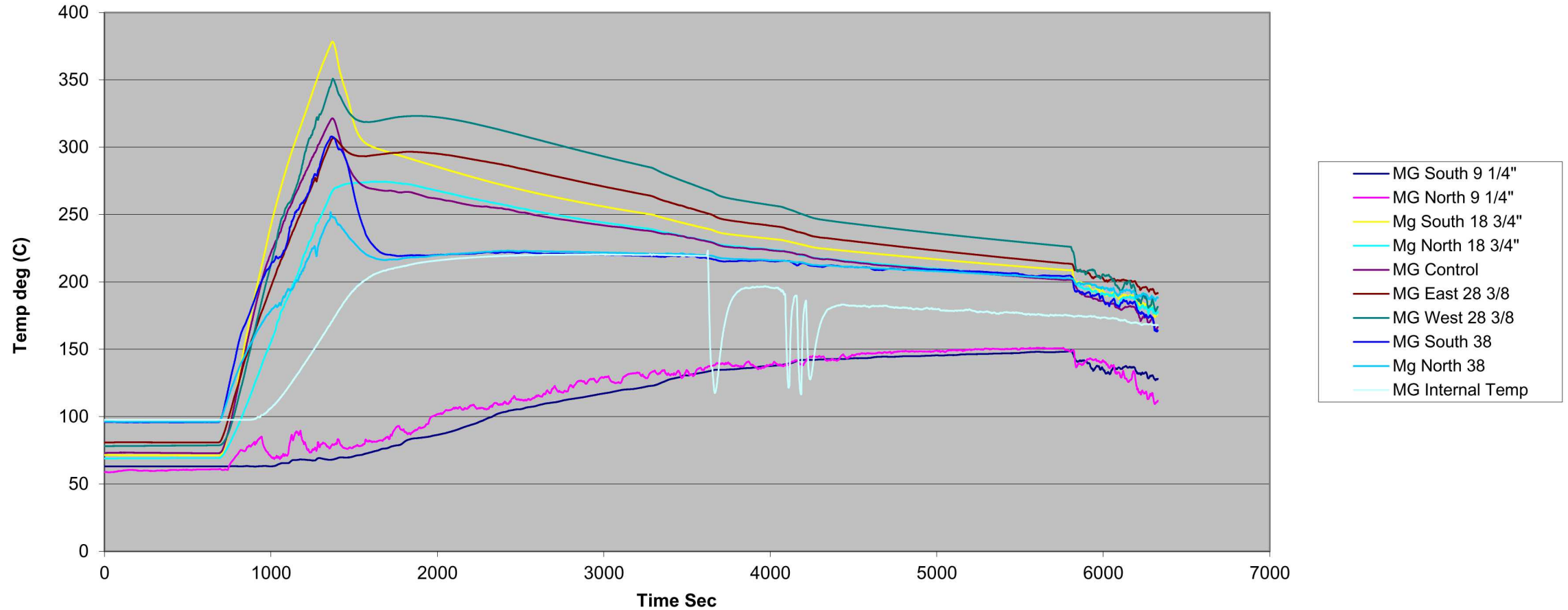


Figure 7-11: In-Vessel Sodium Spray Test Instrumentation Layout

T3 Data

Melt Generator Temperature

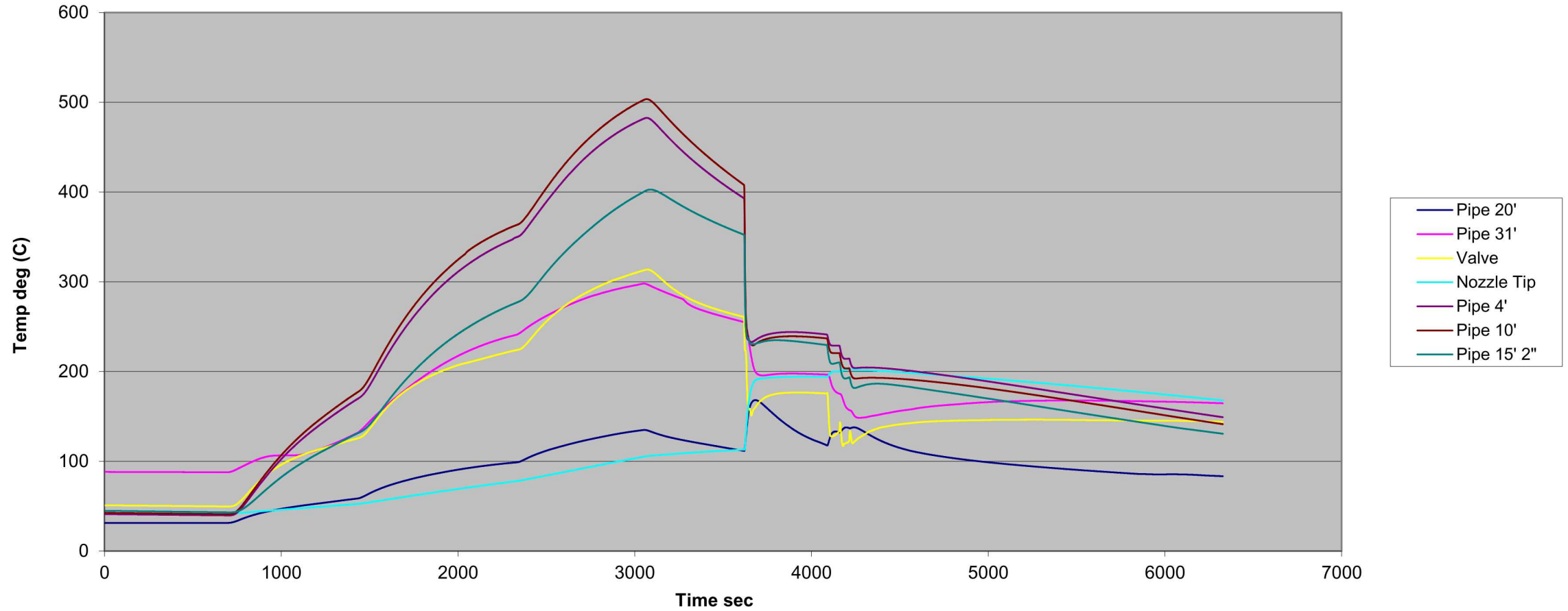
MG temp



T3 Data

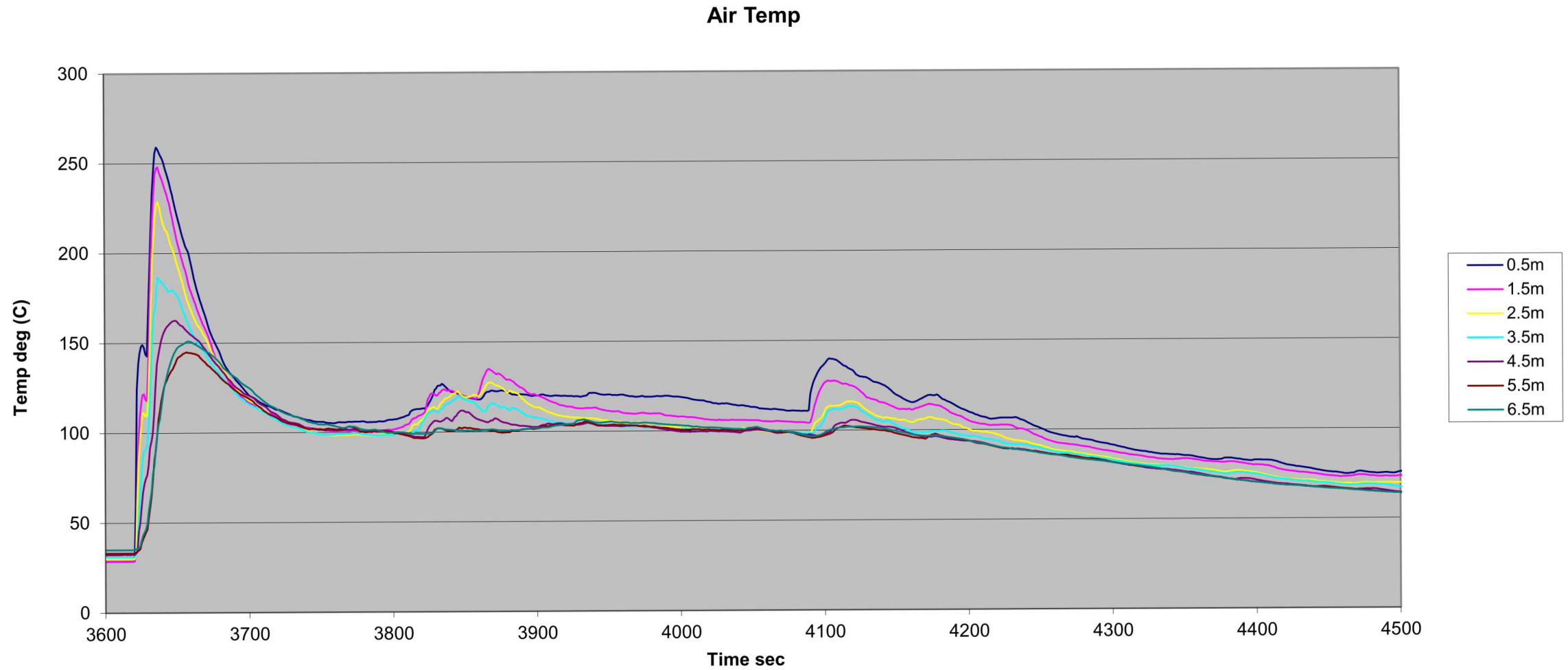
Pipe Temperatures

Pipe Temps



T3 Data

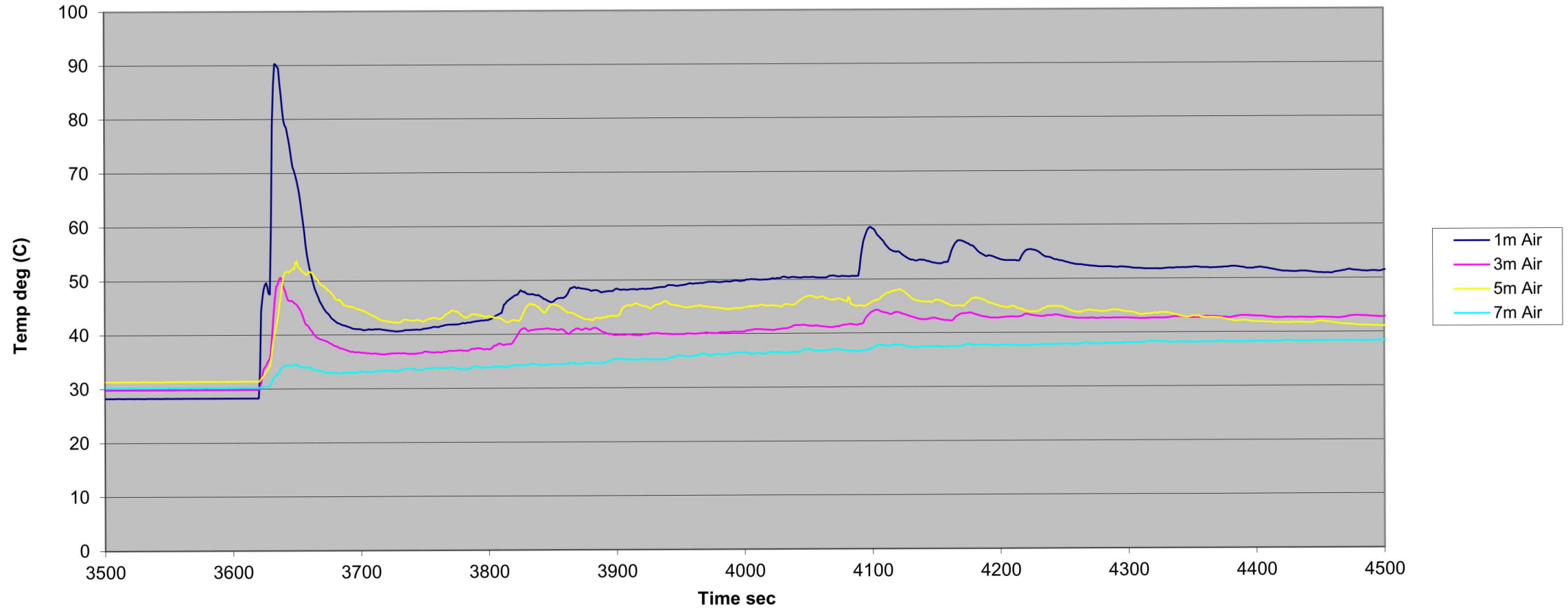
Air Temperature



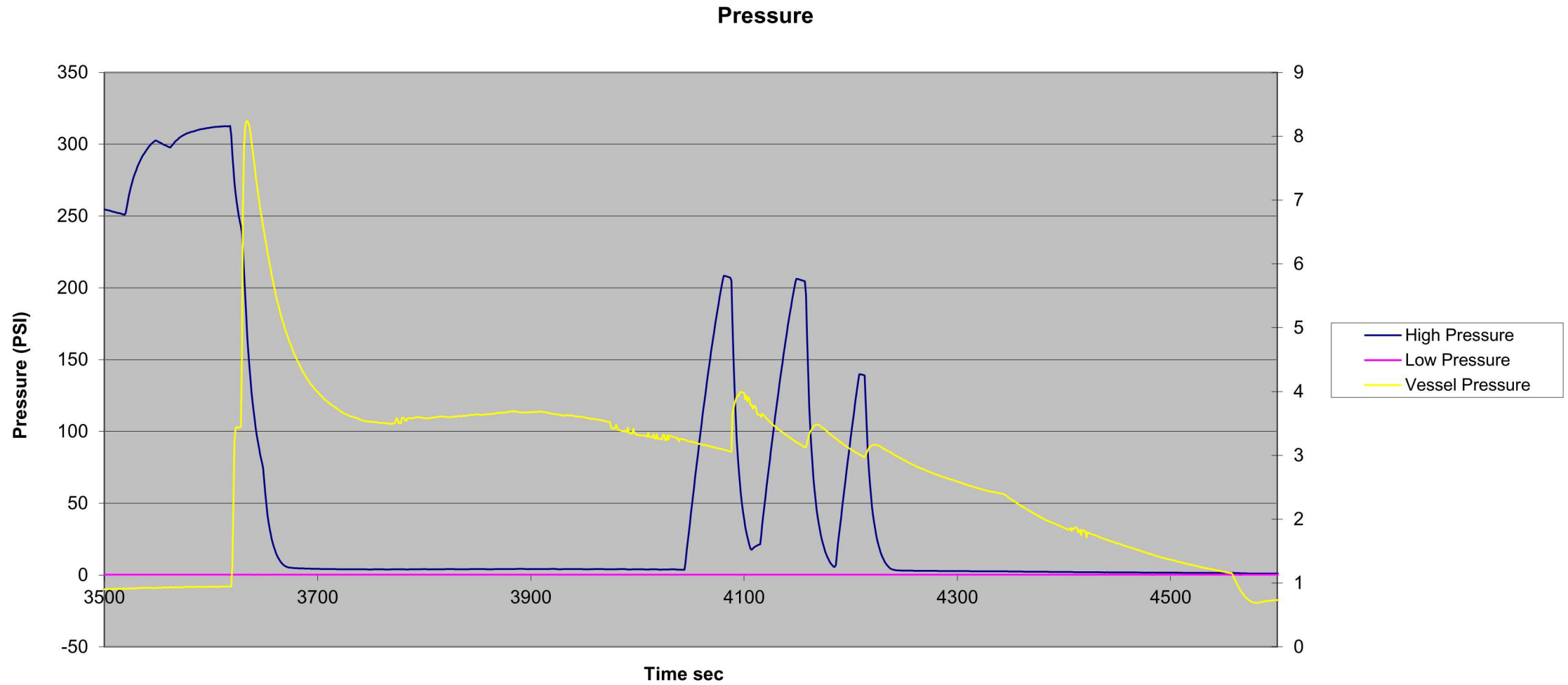
T3 Data

Wall Temperature

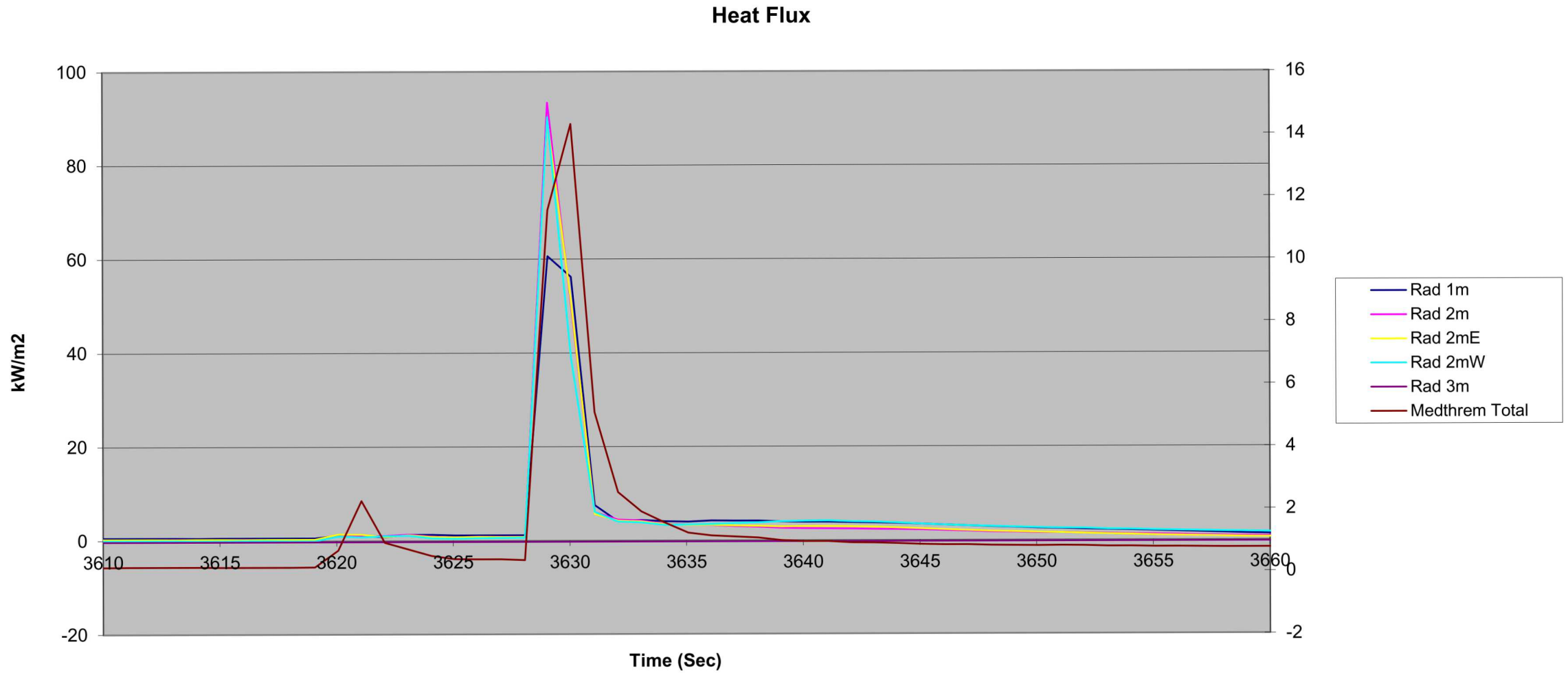
Wall Temp



T3 Data Pressures



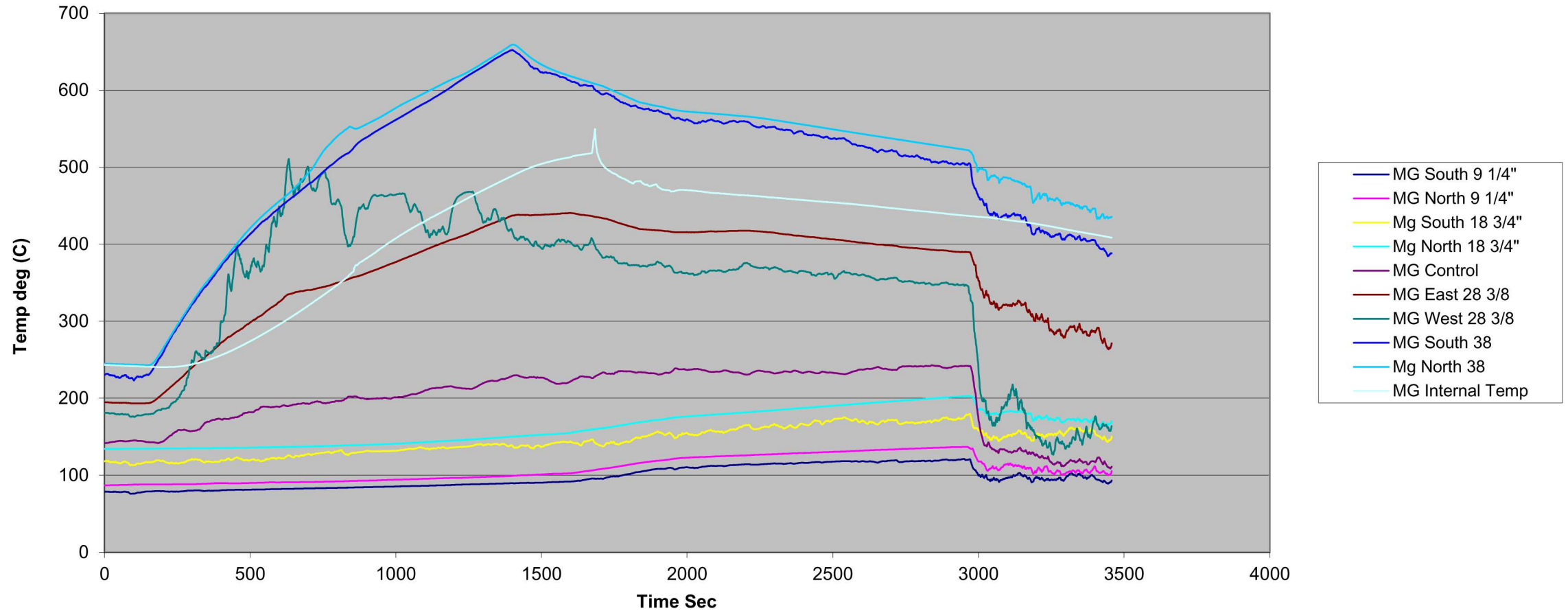
T3 Data Heat Flux



T4 Data

Melt Generator Temperature

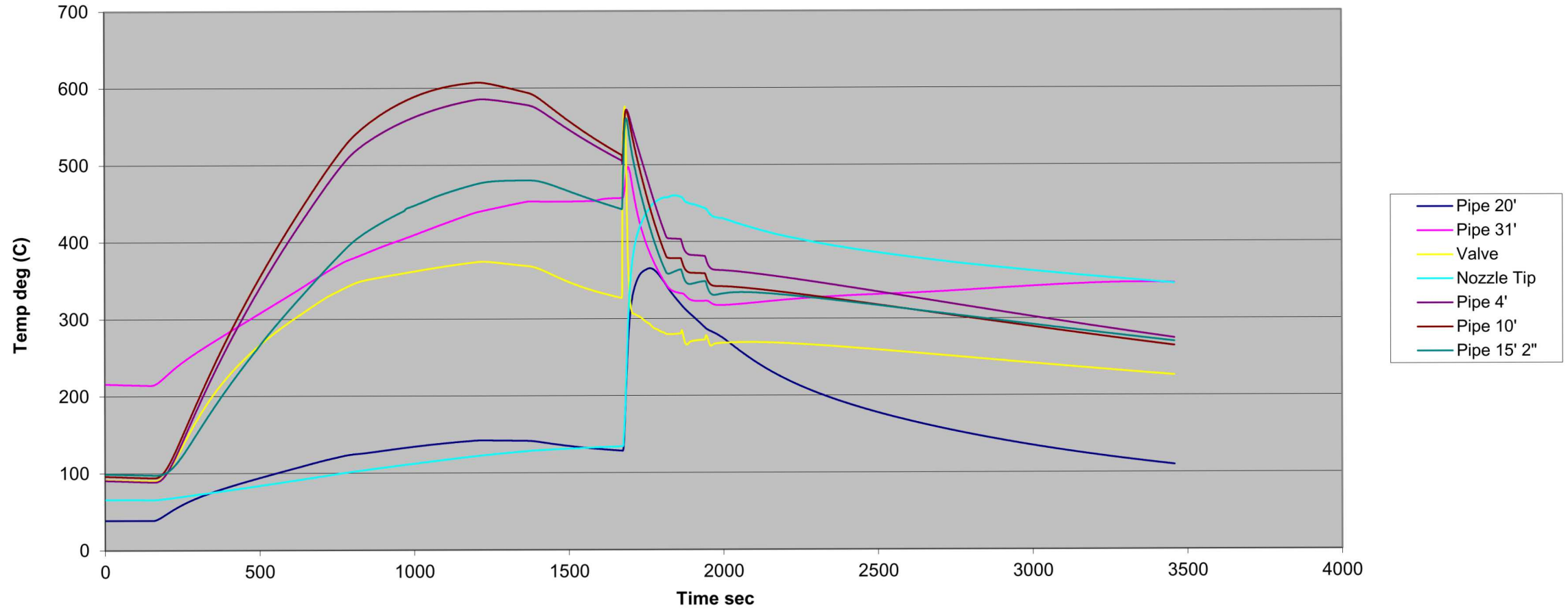
MG temp



T4 Data

Pipe Temperatures

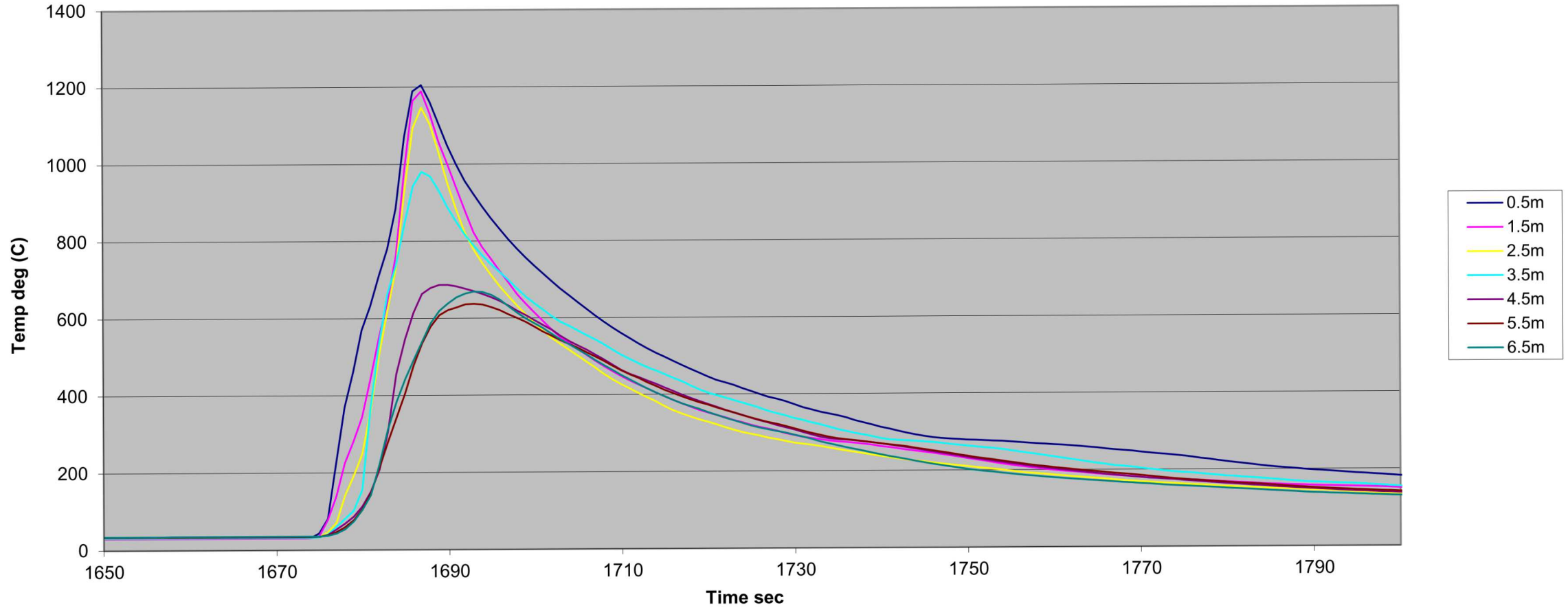
Pipe Temps



T4 Data

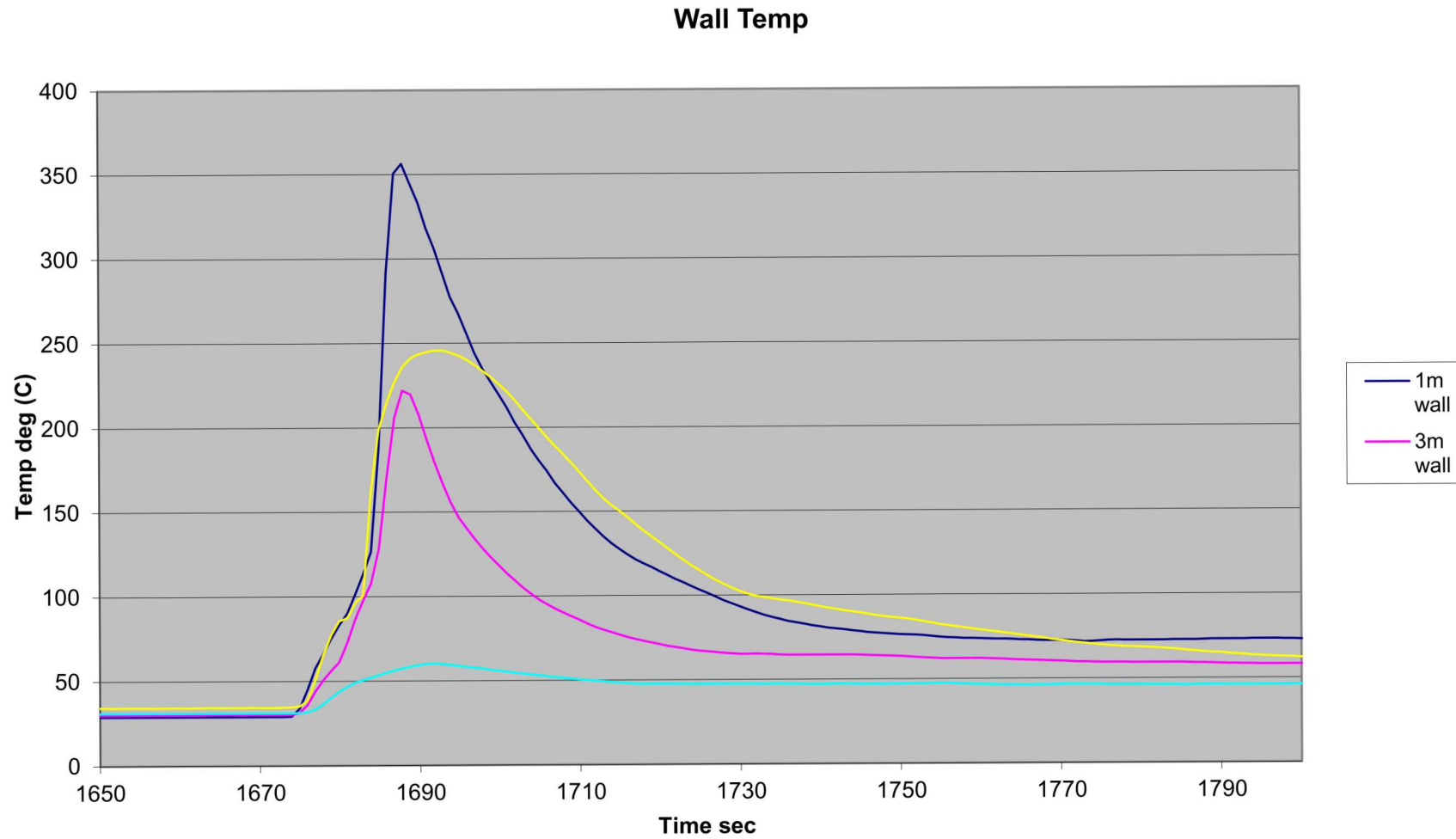
Air Temperature

Air Temp

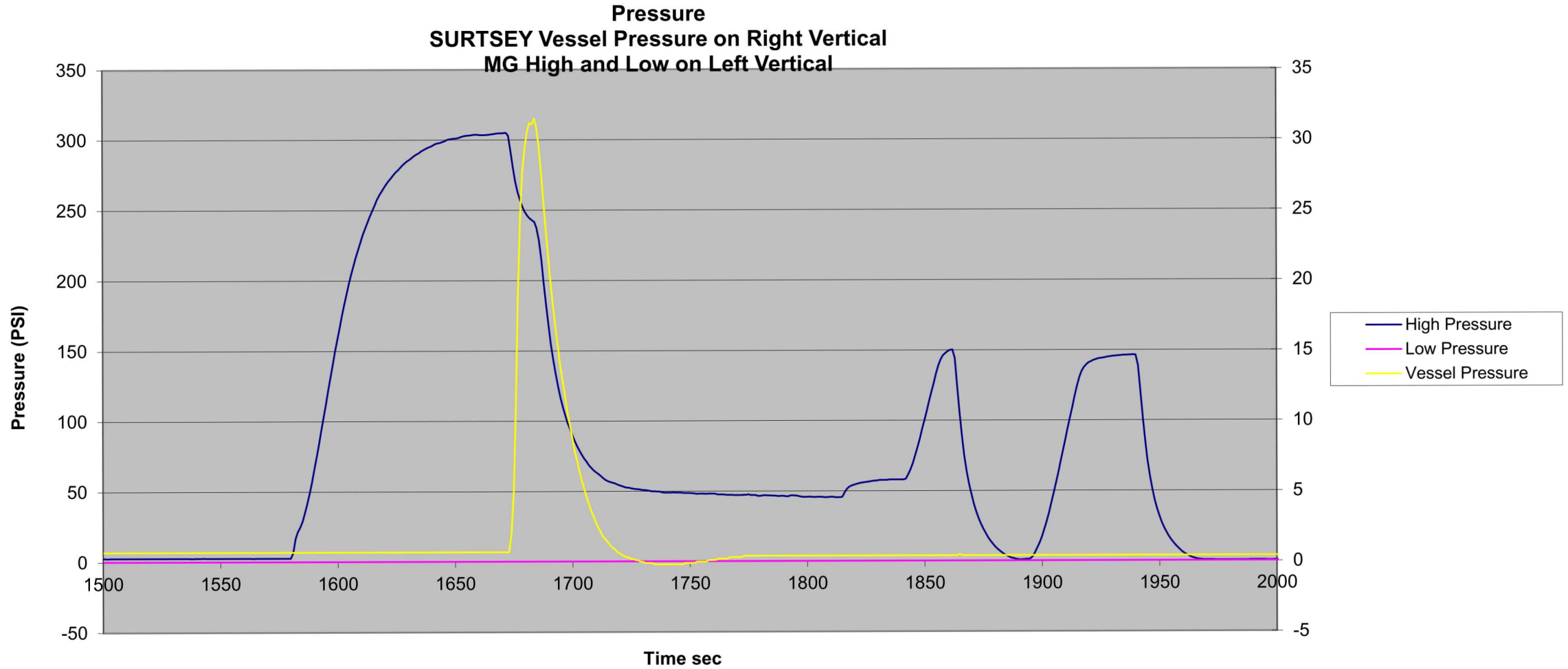


T4 Data

Wall Temperature

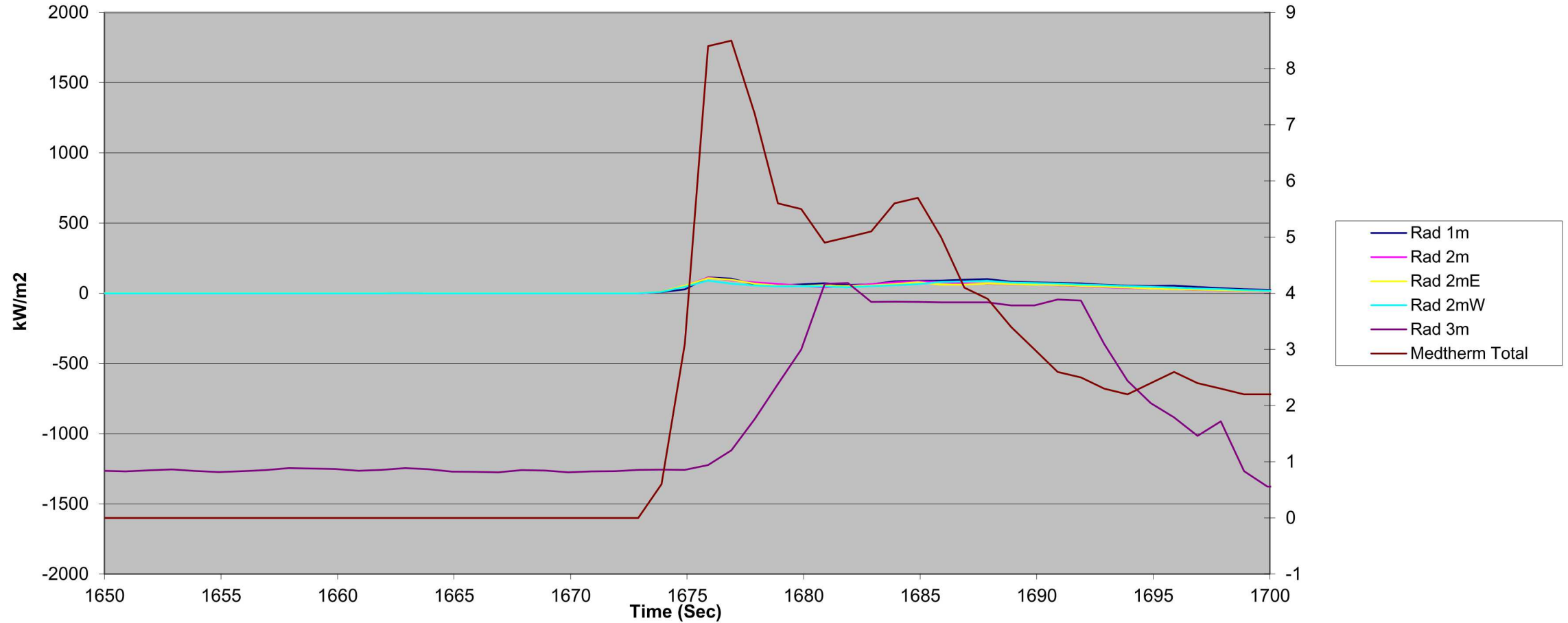


T4 Data Pressures



T4 Data Heat Flux

Heat Flux
Note: Rad 3m does not seem to be working properly
Medtherm Total on Right Vertical All Rad on Left Vertical



Open T3&T4 Collaboration Questions

- How do we treat the multiple ignitions in the T3?
- Do we re-evaluate the DME for the spray fires?
- Do we model the concrete in the bottom of Surtsey?
 - MELCOR cannot yet do sodium concrete interactions.
- Do we only model the initial pressurization rise in T4?
 - If we model beyond the 6 inch diameter port failure, do we model leakage prior to the complete depressurization?

Sodium Mass Injected	20 kg
Duration of Sodium Spray	Approximately 20 seconds
Spray Height	5.3 m
Sodium Mass Flowrate	1 kg/s
Sodium Outlet Nozzle Velocity	9.34 m/s
Outlet Nozzle Pressure	2.01 MPa (291 psi)
Initial Sodium Temperature	200°C, 500°C
Nozzle Orifice Diameter	1.23 cm
Mean Droplet Diameter (DME)	2.0 mm
Vessel Free Volume	99 m ³
Vessel Thickness	1 cm



SNL Sodium Fire Modeling

Experiments

MELCOR/Contain-LMR

CNWG



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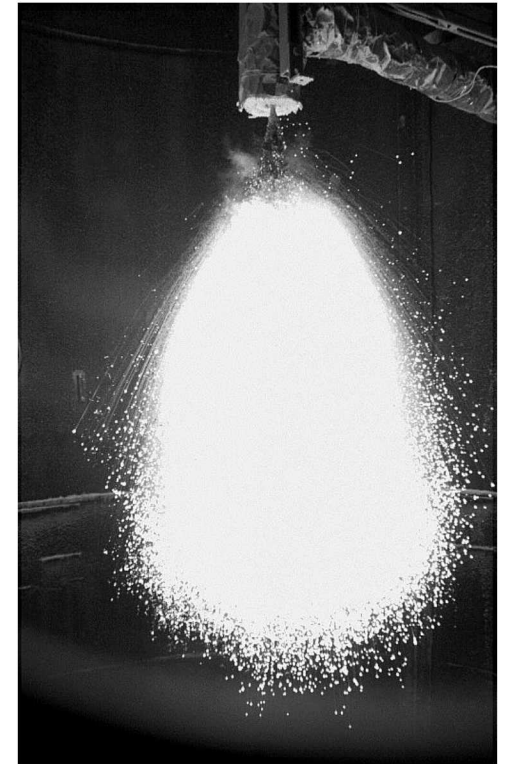


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MELCOR and CONTAIN-LMR Integration

- Motivation:
 - Provide CONTAIN-LMR sodium accident analysis capability under MELCOR integrated severe accident code for SFR source term assessments, level 2/3 PRA, and containment DBA analyses.
- Current Status:
 - Sodium chemistry models from CONTAIN-LMR are being implemented into MELCOR 2.1
 - Data structures for the newly created Sodium Chemistry Package for MELCOR are being developed
 - Additional interface data variables are being added for the atmosphere chemistry model.
- Expected Schedule:
 - Implementation of all Na chemistry models by the end of FY16
 - A combination of experimental and code-to-code and benchmarking studies will be conducted in FY17
- The MELCOR sodium models will be used in:
 - Trial source term calculations funded by DOE or private vendors
 - JAEA Sodium Fire modeling collaboration with SNL and JAEA experiments
 - Planned MELCOR and ASTEC-Na crosswalk



MELCOR Integration Work Scope

- Project Motivation and Objective
 - Address the regulatory infrastructures requirements regarding accident analyses for reactor systems,
 - A sodium coolant accident analysis code is necessary to provide regulators with a means to perform confirmatory analyses for future sodium reactor submissions.
- Solution Strategy
 - Implementation of sodium phenomenology models into an integrated, full-featured, actively maintained, severe accident code
 - CONTAIN-LMR models implemented into the MELCOR code
 - MELCOR is a mature integrated severe accident code
 - Used by NRC for level 2 and level 3 PRA analysis for LWR as well as
 - Used for containment DBA analysis
 - 30 years of development
 - New modeling added to MELCOR will be enabled only when sodium models are specified by user, and will not impact code performance.

Sodium Coolant in MELCOR 2.1

- Sodium Working fluid
 - Implement Sodium Equations of State (EOS)
 - Implement Sodium thermal-mechanical properties
- Two models implemented
 - Fusion safety database (FSD)
 - SIMMER database with supplemental SAS4a information
- Sodium properties for FSD are mainly read from an input file, so it is easy to adapt for other liquid metal fluids
- Test problems have been created demonstrating model capability
- Some improvement, particularly for FSD, may require additional assessment and development

Sodium Models from CONTAIN-LMR

- DOE has funded Sandia starting from FY13
 - We are Integrating all sodium physics and chemistry models into MELCOR 2.1 with the sodium coolant fluid capability
 - Spray fire chemistry
 - Pool fire chemistry
 - Atmosphere chemistry
 - Two condensable options (in atmosphere)
 - Sodium condensation
 - Water condensation
 - Sodium concrete interaction (SLAM model)
 - Sodium/debris interactions (no interest from DOE)
 - Internally, we are upgrading CONTAIN2 (last version) with CONTAIN-LMR sodium models

Spray Fire Chemistry

- Based on NACOM spray model from BNL
 - Input requirement: fall height, mean diameter and source
 - Internal droplet size distribution (11 bins) from Nukiyama-Tanasama correlation
 - Reactions considered:
 - (S1) $2 \text{ Na} + \frac{1}{2} \text{ O}_2 \rightarrow \text{ Na}_2\text{O}$,
 - (S2) $2 \text{ Na} + \text{ O}_2 \rightarrow \text{ Na}_2\text{O}_2$
 - Fixed ratio of peroxide and monoxide $\left(\frac{1.3478 \cdot F_{\text{Na}_2\text{O}_2}}{1.6957 - 0.3479 \cdot F_{\text{Na}_2\text{O}_2}} \right)$
 - CONTAIN Routine Ported to MELCOR: SPRAY
 - Tracked quantities include:
 - Mass of Na (spray, burned, pool), O_2 (consumed), $\text{Na}_2\text{O}_2 + \text{Na}_2\text{O}$ (produced)
 - Energy of reactions

Pool Fire Chemistry

- Based on SOFIRE II code from ANL
 - Reactions considered:
 - (P1) $2 \text{Na} + \text{O}_2 \rightarrow \text{Na}_2\text{O}_2$,
 - (P2) $4 \text{Na} + \text{O}_2 \rightarrow 2 \text{Na}_2\text{O}$
 - Reactions depend on the oxygen diffusion as: $D = \frac{6.4315 \times 10^{-5}}{P} T^{1.823}$
 - Input requirement:
 - F1 – fraction of O_2 consumed for monoxide,
 - F2 – fraction of reaction heat to pool,
 - F3 – fraction of peroxide mass to pool, &
 - F4 – fraction of monoxide mass to pool
 - PFIRE routine will be ported to MELCOR 2.1
- Sodium pool modeling – heat transfer
- Tracked quantities:
 - Mass of Na(pool, burned), O_2 (consumed), $\text{Na}_2\text{O}_2 + \text{Na}_2\text{O}$ (produced)
 - Energy of reactions

Atmospheric Chemistry

- A number of reactions have been considered:
 - (A1) $\text{Na(l)} + \text{H}_2\text{O (l)} \rightarrow \text{NaOH(a)} + \frac{1}{2}\text{H}_2$
 - (A2) $2 \text{Na(g,l)} + \text{H}_2\text{O (g,l)} \rightarrow \text{Na}_2\text{O(a)} + \text{H}_2$
 - (A3) $2 \text{Na(g,l,a)} + \frac{1}{2}\text{O}_2 \text{ or } \text{O}_2 \rightarrow \text{Na}_2\text{O(a)} \text{ or } \text{Na}_2\text{O}_2\text{(a)}$
 - (A4) $\text{Na}_2\text{O}_2\text{(a)} + 2 \text{Na(g,l)} \rightarrow 2 \text{Na}_2\text{O(a)}$
 - (A5)
 - $\text{Na}_2\text{O(a)} + \text{H}_2\text{O (g,l)} \rightarrow 2\text{NaOH(a)}$
 - $\text{Na}_2\text{O}_2\text{(a)} + \text{H}_2\text{O (g,l)} \rightarrow 2\text{NaOH(a)} + 0.5\text{O}_2$
- All these reactions are assumed to occur:
 - Atmosphere (g), aerosol, surfaces (i.e., HS)
 - The order of the reactions are given

Atmospheric Chemistry (concluded)

- Porting routines:
 - CHEMRX - main driven routine to call:
 - CHMGAS – gas-to-gas reactions
 - CHMAER – aerosol-to-gas reactions
 - CHMDEP – deposited aerosol reactions
 - CHMREP – aerosol-to-liquid reactions on surfaces
 - Interface variables – RN, CVH, NCG, BUR packages
- Outputs
 - Reaction number, reaction energy, byproducts (Na classes, H₂), gas and liquid consumed (Na, H₂O, O₂)
 - In MELCOR, H₂ burn is not calculated in CHEMRX. Instead, user needs to invoke BUR package

Sodium Chemistry (NAC) Package Development (in progress)

- To better manage the sodium related models, particular for chemistry models
- Create “new” NAC Package
 - Data structures – in module (M_NAC)
 - NaCL(5), old-new variables, input parameters
 - RN to NAC class structure – tracks aerosol products
 - Na modeled as condensable, H₂O modeled as aerosol
 - Sensitivity coefficient development (a minimum set for now)
 - Interface variables, interface with many packages, for examples:
 - NCG – O₂ and H₂
 - HS – condensate, deposits
 - CVH – H₂O, reaction energies
 - RN – aerosol interactions
 - Calling sequence for NAC model executions

Aerosol Mapping

RN Class

Class	Class Name	Chemical Group	Representative	Member Elements
1	XE	Noble Gas	Xe	He, Ne, Ar, Kr, Xe, Rn, H, N
2	CS	Alkali Metals	Cs	Li, Na, K, Rb, Cs, Fr, Cu
3	BA	Alkaline Earths	Ba	Be, Mg, Ca, Sr, Ba, Ra, Es, Fm
4	I2	Halogens	I ₂	F, Cl, Br, I, At
5	TE	Chalcogens	Te	O, S, Se, Te, Po
6	RU	Platinoids	Ru	Ru, Rh, Pd, Re, Os, Ir, Pt, Au, Ni
7	MO	Early Transition Elements	Mo	V, Cr, Fe, Co, Mn, Nb, Mo, Tc, Ta, W
8	CE	Tetravalent	Ce	Ti, Zr, Hf, Ce, Th, Pa, Np, Pu, C
9	LA	Trivalents	La	Al, Sc, Y, La, Ac, Pr, Nd, Pm, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu, Am, Cm, Bk, Cf
10	UO2	Uranium	UO ₂	U
11	CD	More Volatile Main Group	Cd	Cd, Hg, Zn, As, Sb, Pb, Tl, Bi
12	AG	Less Volatile Main Group	Ag	Ga, Ge, In, Sn, Ag
13	BO2	Boron	BO ₂	B, Si, P
14	H2O	Water	H ₂ O	H ₂ O
15	CON	Concrete	CON	- - -
16	CSI	Cesium iodide	CsI	CsI
17	CSM	Cesium Molybdate	CsM ¹	CsM ¹

RN Class to NAC Class

Rn Class	NAC Class
H2O (CL 14)	NaCL(1)
Na (New)	NaCL(2)
NaOH (new)	NaCL(3)
Na2O (new)	NaCL(4)
Na2O2 (new)	NaCL(5)

Specified Details on NAC Package

- MELGEN records
 - NAC_INPUT
 - NAC_RNCLASS
 - NAC_ATMCHEM
 - NAC_SPRAY
 - NAC_PFIRE
 - NAC_CONDENSE
 - NAC_SLAM
 - NAC_SC
- Plot and control function variables
- Outputs

Summary

- With the new Sodium Fire Modeling capabilities being added into MELCOR, the US is poised address identified safety and licensing gaps for US sodium reactors
 - Validation of these new tools remains a key component to ongoing SFR safety related research
 - IRSN/SNL collaboration is key to improving the understanding of sodium fire phenomenology

Acknowledgement

- The Sodium Fire Tests were funded under a SNL LDRD from 2007-2010.
- MELCOR-Na development is funded by the Office of Nuclear Energy of U.S. Department of Energy WP#: AT-17SN170204.
- SNL/IRSN collaborative research is covered under the existing NRC/IRSN MOU. SNL work related to this collaboration is funded under the MELCOR/ASTEC crosswalk.

Thank You