

# The Full MoS<sub>2</sub> Monty... Stress!

B. L. Nation<sup>1</sup>, T. Babuska<sup>1</sup>, J. Curry<sup>1</sup>, B. Krick<sup>2</sup>, M. Chandross<sup>1</sup>, N. Argibay<sup>1</sup>

<sup>1</sup>Materials Science and Engineering Center  
Sandia National Laboratories, NM, USA

<sup>2</sup>Department of Mechanical Engineering and Mechanics  
Lehigh University, PA, USA

## Introduction

Everybody knows MoS<sub>2</sub>. It is shown throughout the literature that MoS<sub>2</sub> does not follow Amonton's law. The friction behavior is a function of material properties of MoS<sub>2</sub> such the shear strength and contact pressure. At high enough contact pressures, we show that MoS<sub>2</sub> behaves amontonian. We hypothesize that the transition from non-amontonian to amontonian behavior is due to plastic deformation of the substrate.

The man, the myth, the legend...Irwin Singer

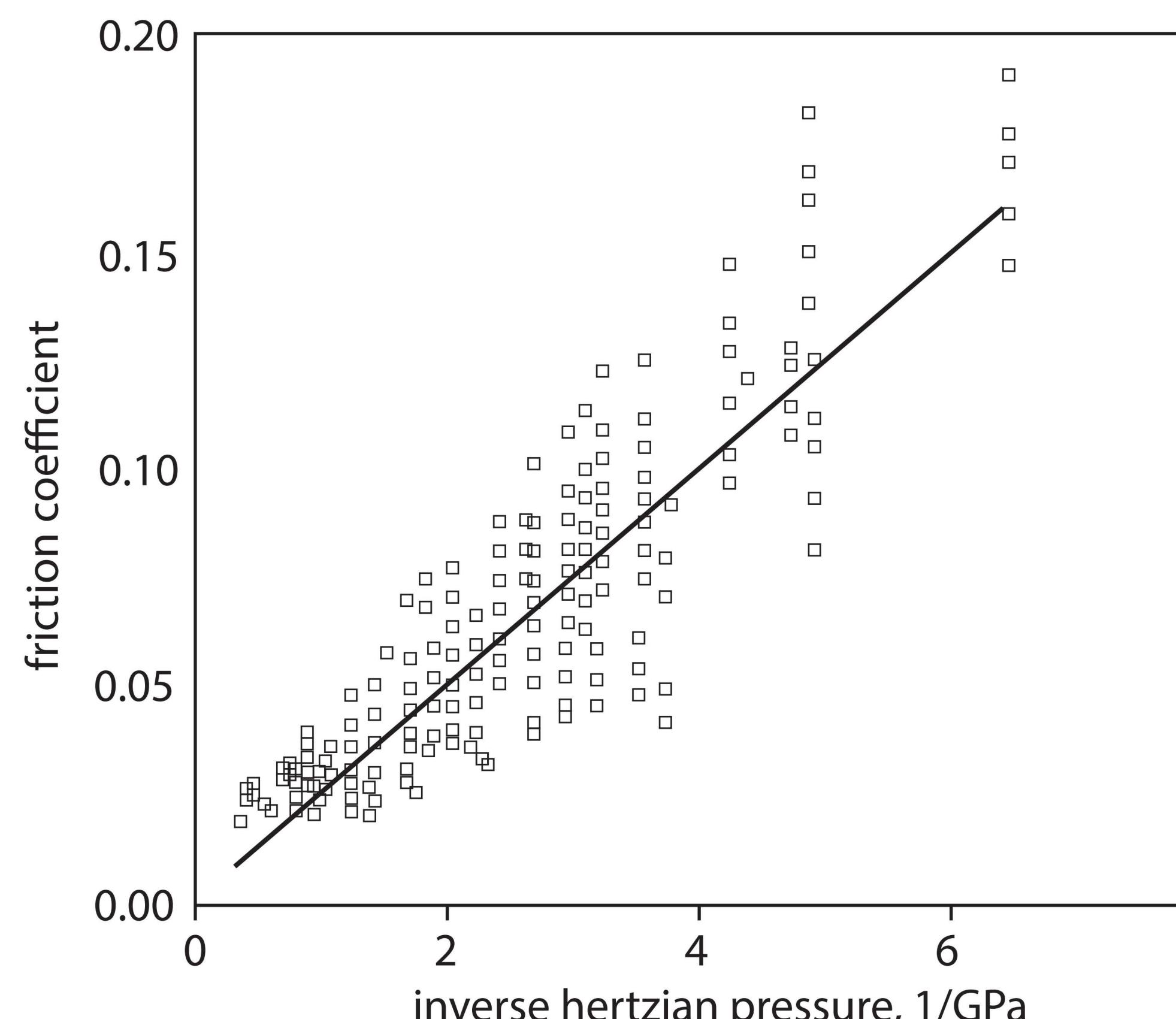


Figure 1: Friction Coefficient vs. Inverse Hertzian Pressure for pure MoS<sub>2</sub>

The non-amontonian behavior is shown in Fig. 1. The slope shown is the shear strength of MoS<sub>2</sub> and is ~28 MPa. As the inverse hertz pressure gets small (large contact pressure), Singer notes that the friction coefficient starts to plateau. Why is the shear strength constant and why does friction plateau??

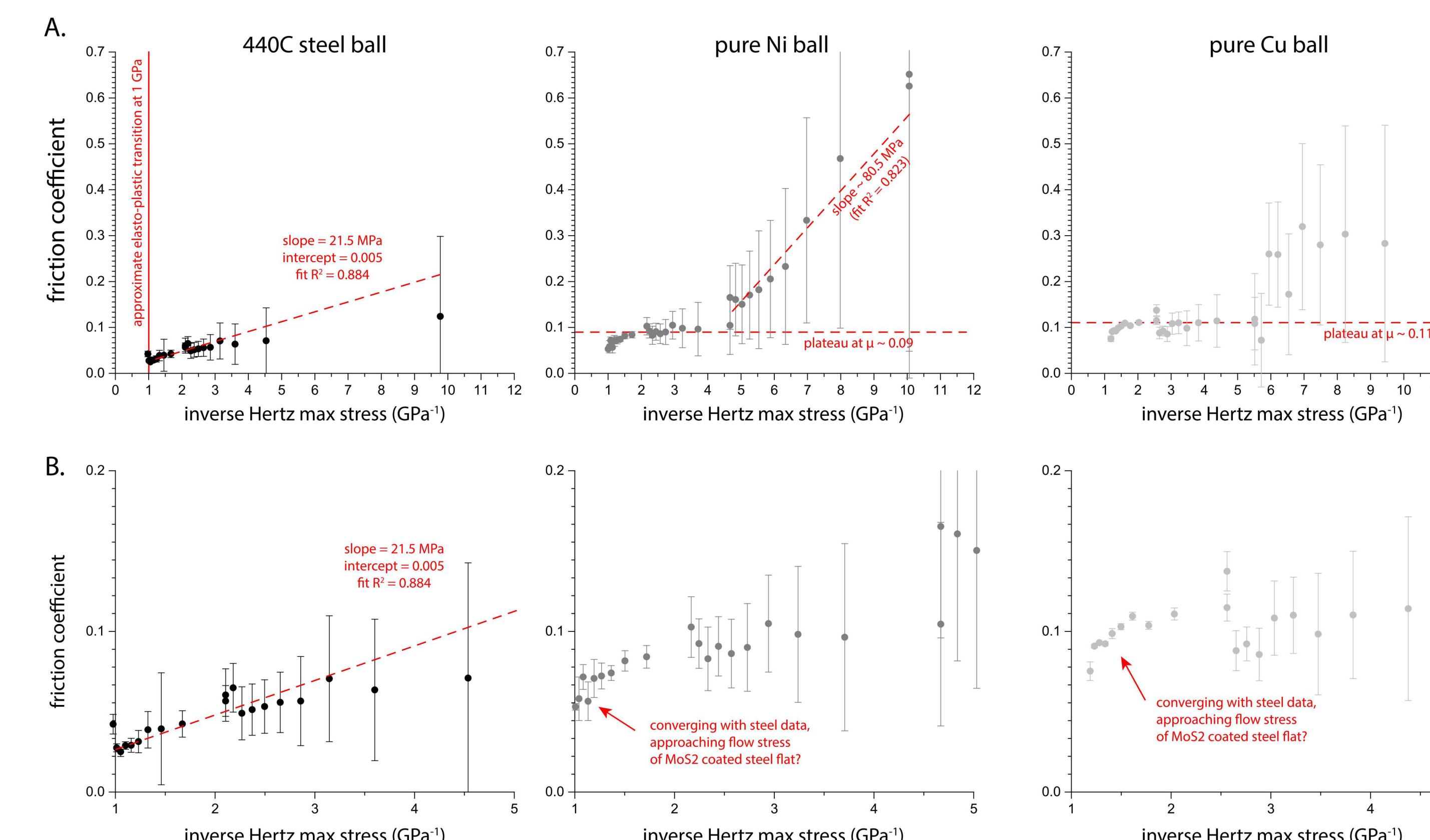


Figure. 2: (A) Plots of friction coefficient vs. inverse Hertz max stress for 440C steel on MoS<sub>2</sub>, pure Ni ball on MoS<sub>2</sub> and pure Cu ball on MoS<sub>2</sub> (B) The same plots as in 2A but focused on the high stress regions (<5 GPa<sup>-1</sup>) and low friction regimes (< 0.2).

Friction coefficients were measured using three different counterfaces on sputtered pure MoS<sub>2</sub> over different contact pressures. For steel on MoS<sub>2</sub>, the results mimick that of Singer's, with a shear strength of ~21 MPa. We see the start of the friction plateau at ~1GPa where the elasto-plastic transition for steel lies.

This transition is further pronounced in copper and nickel tests on MoS<sub>2</sub> where significant plateaus in friction coefficient are seen below ~5 GPa<sup>-1</sup> for copper and below ~6 GPa<sup>-1</sup> for nickel. Both the nickel and copper tests converge to the elasto-plastic transition for steel around 1 GPa<sup>-1</sup>, likely due to the steel substrate that the MoS<sub>2</sub> was sputtered on. We also see a slightly larger shear strength for MoS<sub>2</sub> on the copper tests. These plateaus correlate well with the elasto-plastic transitions for all three materials.

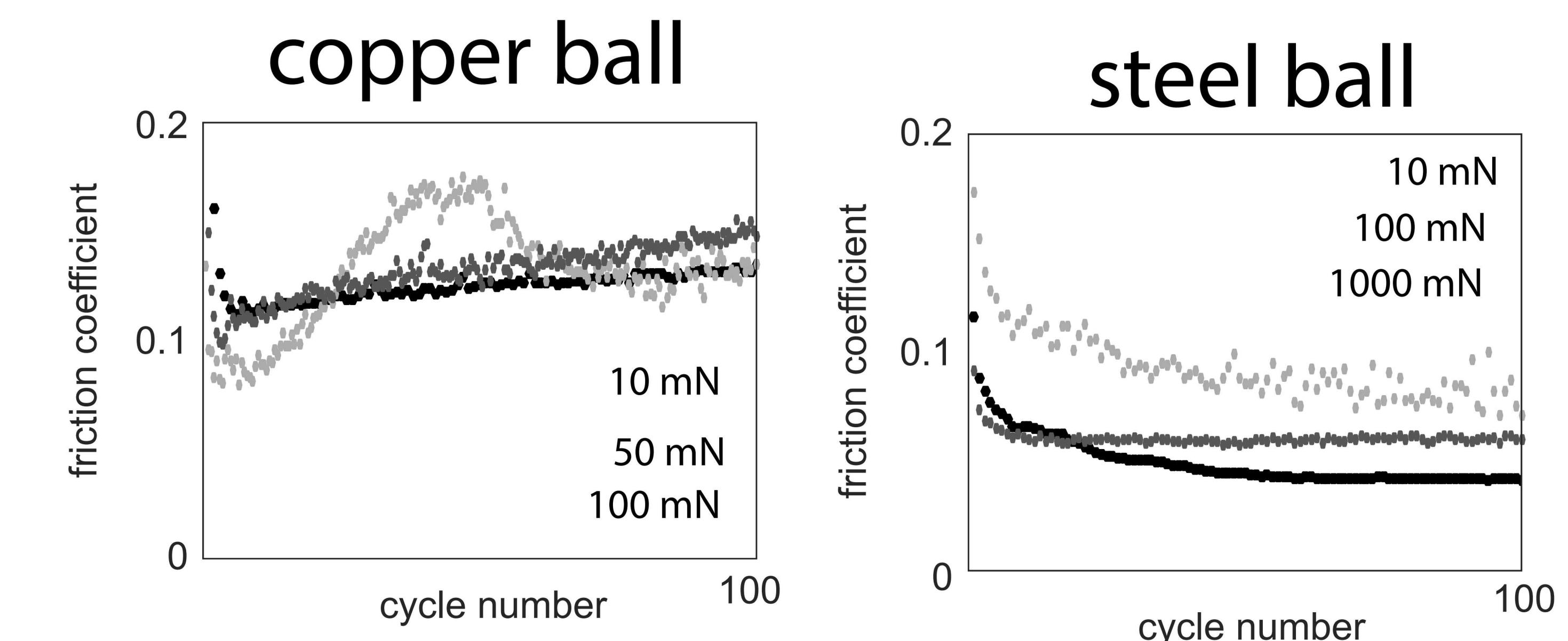


Figure. 3: Evolution of friction coefficient for copper and steel on pure MoS<sub>2</sub> at different contact pressures

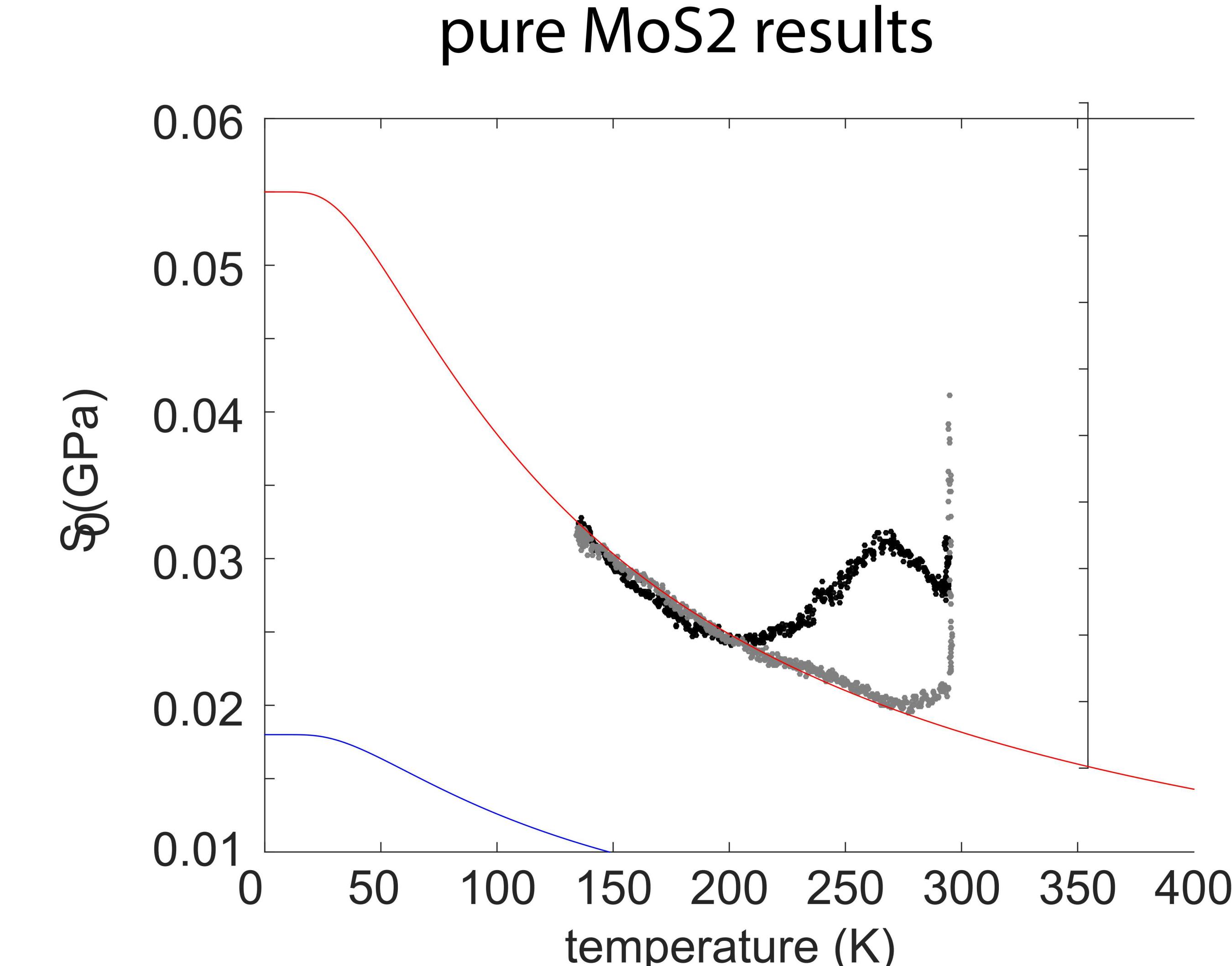


Figure. 4: Ramped temperature friction test ran on MoS<sub>2</sub> at 1 GPa contact pressure. Models of shear strength for MoS<sub>2</sub> over temperature using nudge-elastic band models match the experimental data well.

## Acknowledgments