

# The Full MoS<sub>2</sub> Monty...Temperature!

T. Babuska<sup>1</sup>, J. Curry<sup>1</sup>, B. L. Nation<sup>1</sup>, B. Krick<sup>2</sup>, N. Argibay<sup>1</sup>

<sup>1</sup>Materials Science and Engineering Center  
Sandia National Laboratories, NM, USA

<sup>2</sup>Department of Mechanical Engineering and Mechanics  
Lehigh University, PA, USA

## Introduction

Everybody knows MoS<sub>2</sub>. Consensus in the literature however, has not been reached on how MoS<sub>2</sub> performs at extreme temperatures due to the nature of difficulty for extreme temperature testing. Performance at the extremes is crucial for aerospace applications. This poster presents a tribometer capable of making measurements at extreme temperatures. Using variable temperature friction tests, it can be seen that MoS<sub>2</sub> has low friction throughout extreme temperatures and has a thermal to athermal transition in friction behaviour and wear at room temperature.

## Variable Temperature Tests

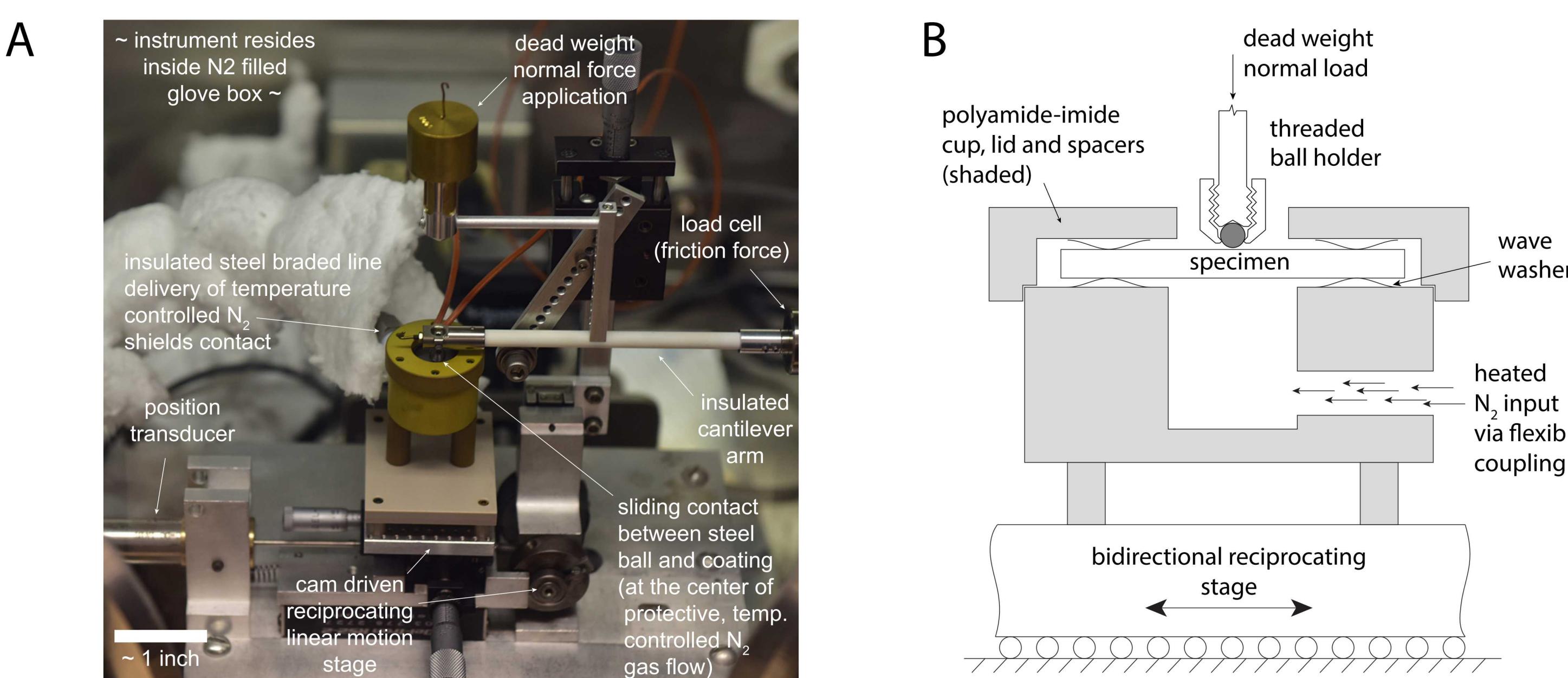


Fig. 1. (A) Annotated picture of the high temp-cryo tribometer. (B) Diagram of PAI flowcell (C) Typical trace of friction and temperature vs. cycles

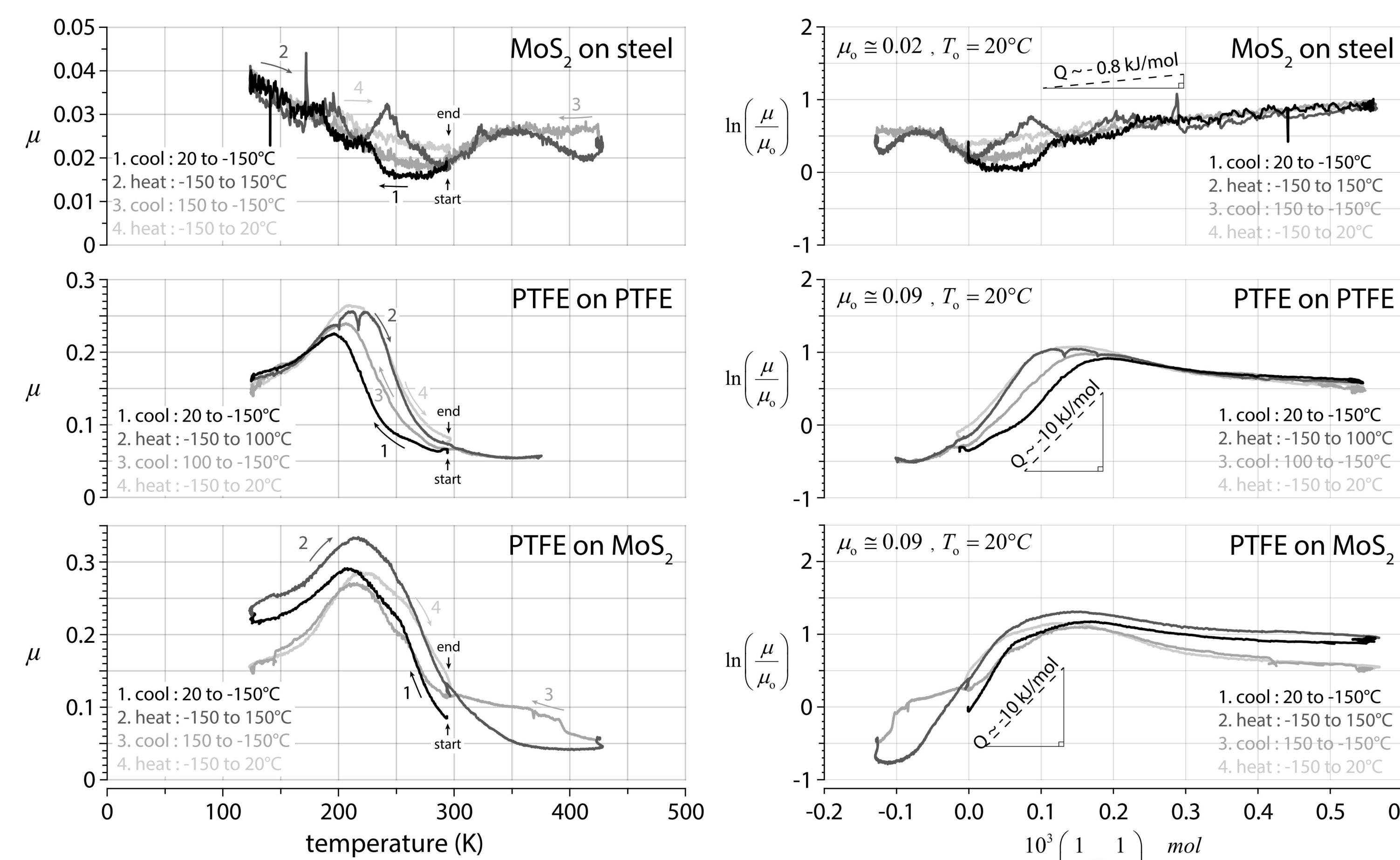
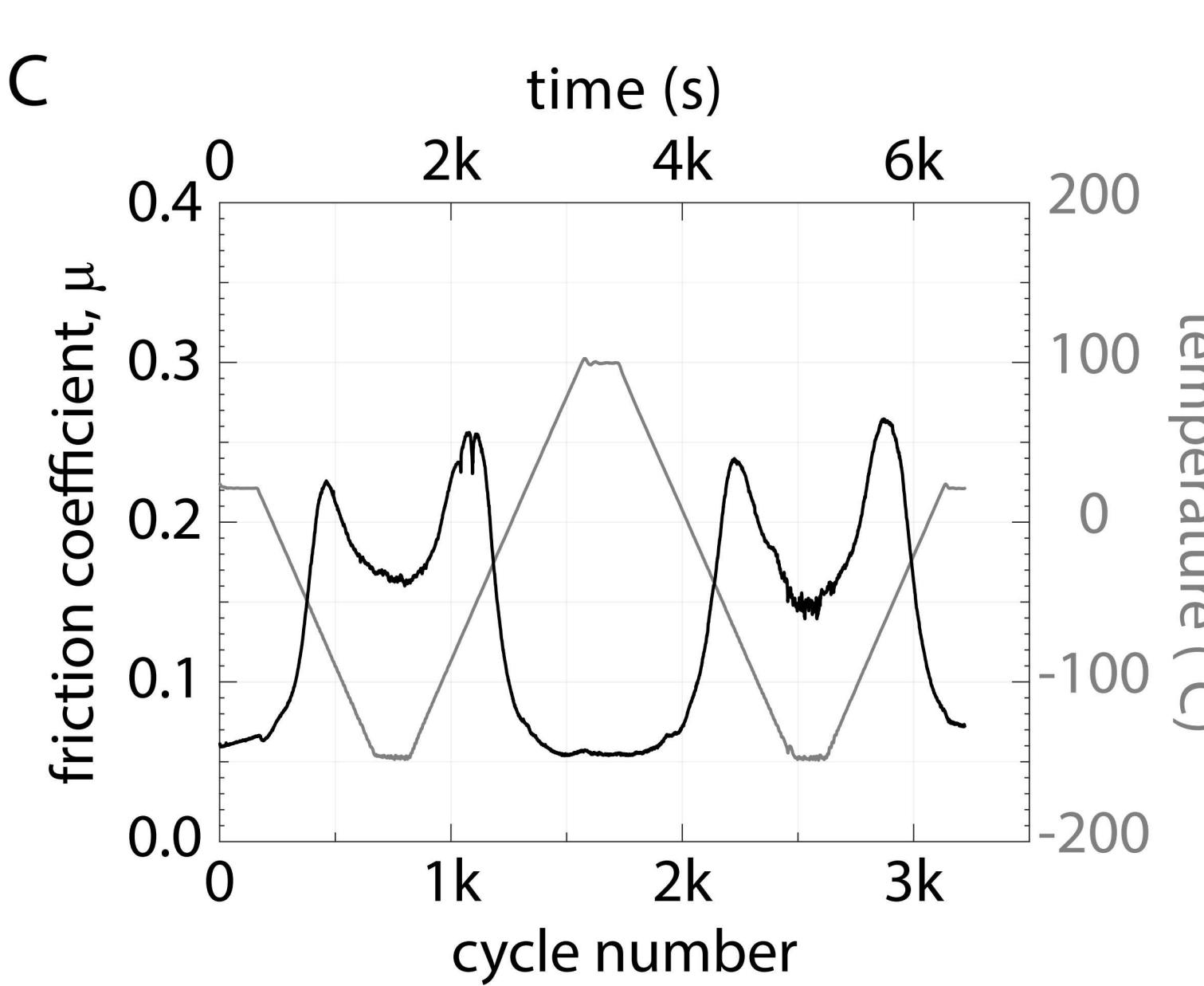


Figure 2: Temperature ramps similar to that shown in Fig. 1c were performed for MoS<sub>2</sub> on Steel, PTFE on PTFE and PTFE on MoS<sub>2</sub>. The left column shows friction vs. temperature plots for each of the three tests. The right column shows the same data plotted in Arrhenius form with normalized friction and temperature

For MoS<sub>2</sub> on Steel, weak thermal friction behaviour can be seen with an activation energy of  $Q \sim 0.8 \text{ kJ/mol}$ . A transition in friction behaviour to athermal is seen around 20 °C. Self-mated PTFE was run to calibrate the tester. Three distinct friction transitions can be seen at -100 °C, 20 °C and 116 °C correlating to mobility changes in the amorphous and crystalline regions of the PTFE. A PTFE ball was run on MoS<sub>2</sub>, the similarity in friction behaviour to self-mated PTFE corroborates the hypothesis that near-surface deformation of the lower shear strength material accommodates sliding.

## Temperature Dependent Wear of MoS<sub>2</sub>

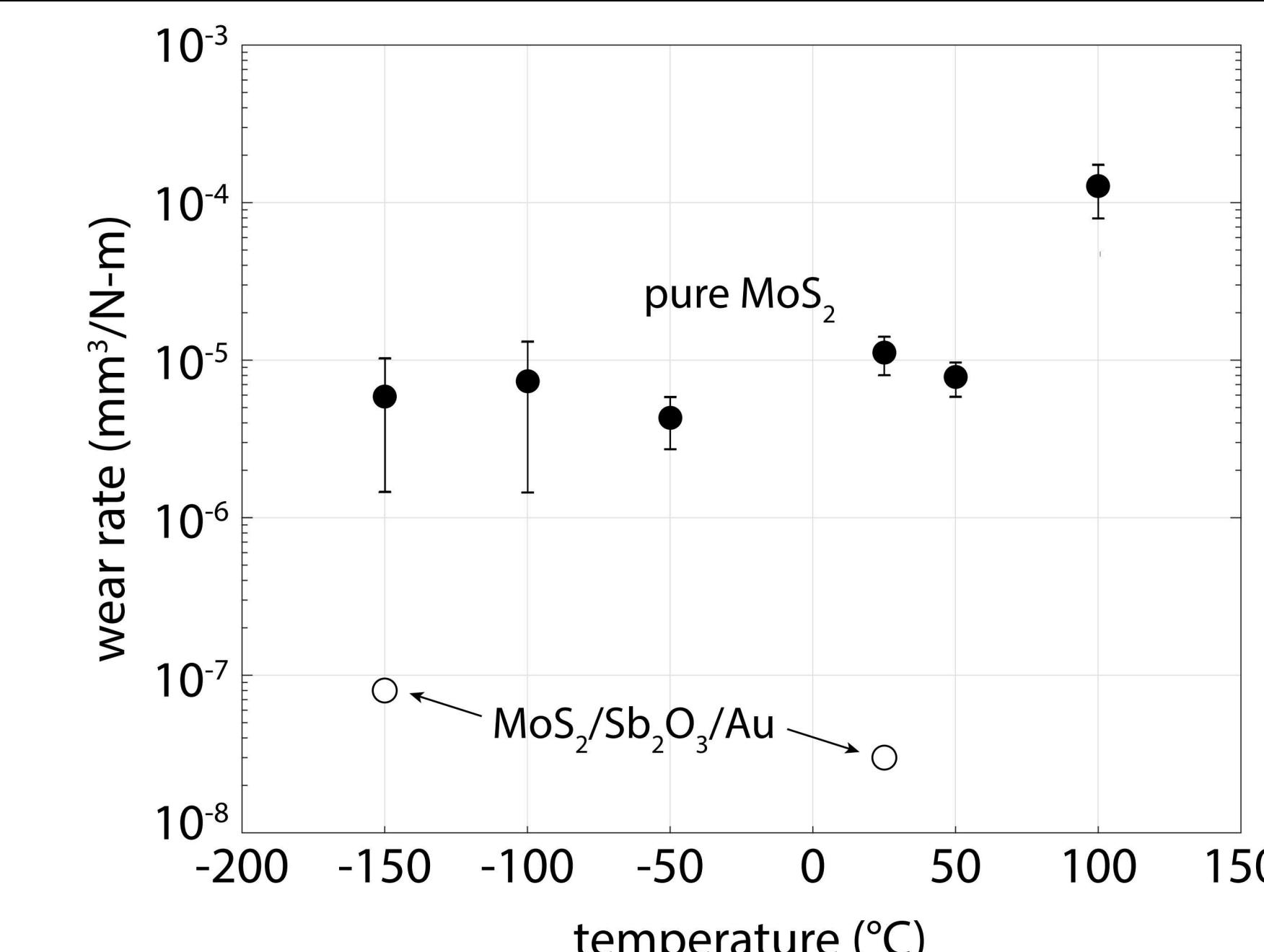


Figure 3: Wear Rates for Pure MoS<sub>2</sub> and Composite MoS<sub>2</sub> for temperatures between -150 °C and 100 °C



Sandia National Laboratories

The wear of pure MoS<sub>2</sub> transitions from thermal to athermal behaviour at approximately 50 °C. This temperature is approximately  $kT$  for pure MoS<sub>2</sub>. We hypothesize that at temperatures above  $kT$ , the increased phonon energy inhibits the lasting formation of long-range ordered sheets of MoS<sub>2</sub> leading to increased wear and friction.

## Arrhenius, Amontonian, or Neither?

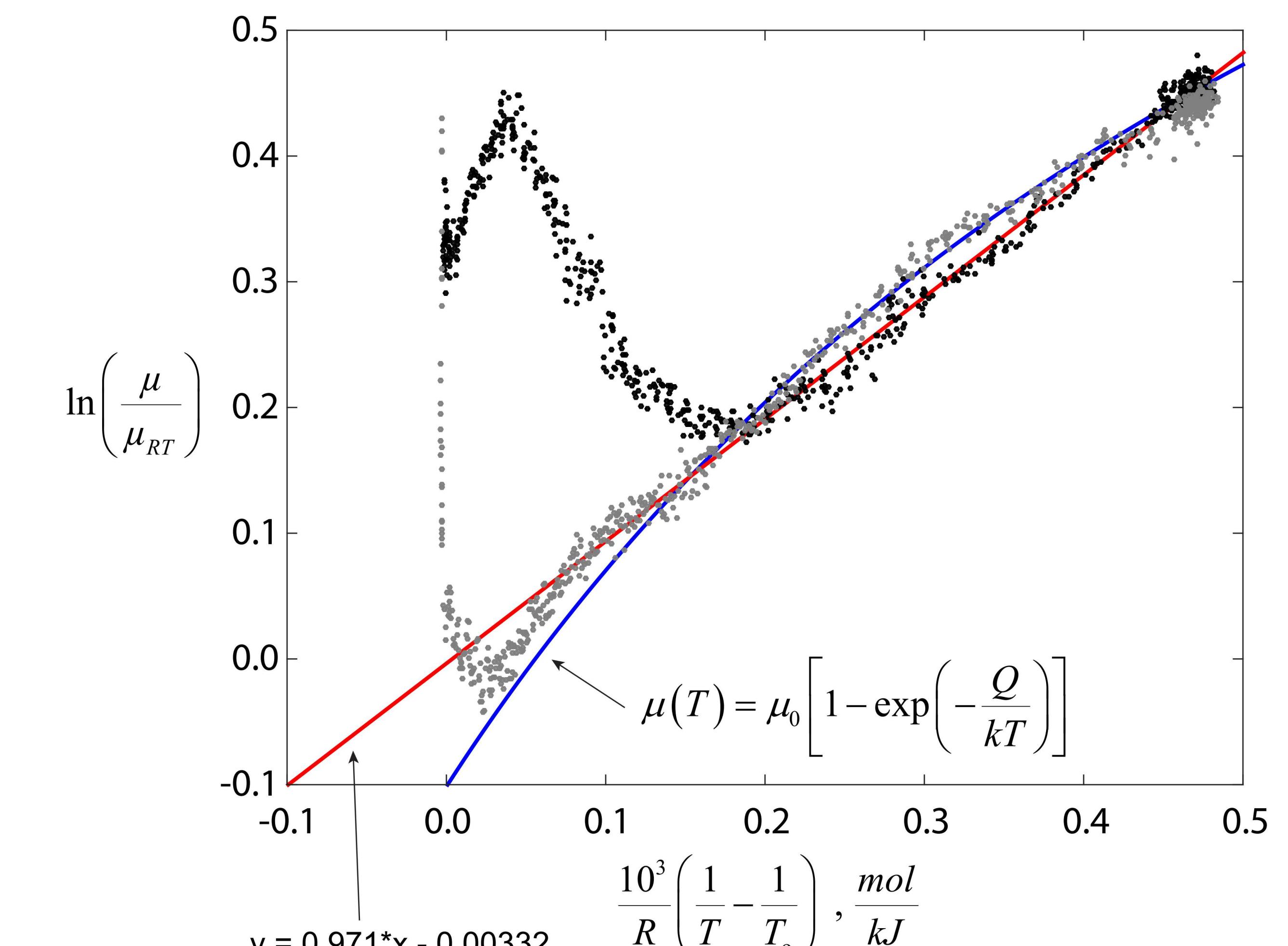


Figure 4: Temperature ramp similar to Fig. 1c performed for MoS<sub>2</sub> on Steel. An Arrhenius plot of normalized friction and temperature is shown.

The curvature in fig. 4 implies that MoS<sub>2</sub> does not follow Arrhenius behavior nor Amontonian. We hypothesize that the curvature is representative of a change in the fundamental shear strength of MoS<sub>2</sub>. The shear strength of MoS<sub>2</sub> is a function of temperature, defect density and commensurability.

## Acknowledgments

Rand Garfield for help in designing and building the tribometer and heating stage



Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. DOE's NNSA under contract DE-AC04-94AL85000