



Frequency Response Function Matching for Test Fixture Design



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PRESENTED BY

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- Fixture Design Background and Motivation
- Design Problem Definition
- Proposed Levelset-CDFEM Approach
- Initial Problem and Levelset-CDFEM Results
- Conclusions

Goal during design and production:

- Ensure that system and its components will survive

To qualify components:

- Estimate system and component mechanical environments
- Perform laboratory tests to prove margin

Possible errors with the above process:

- Predicted system environments
- Predicted component environments
- Unrepresentative component test



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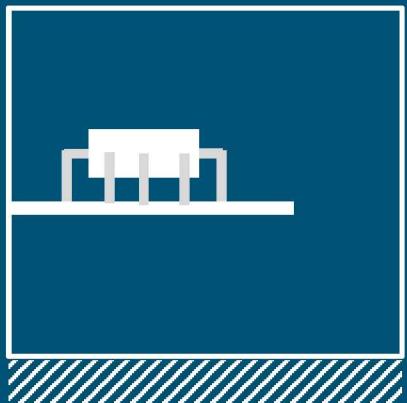
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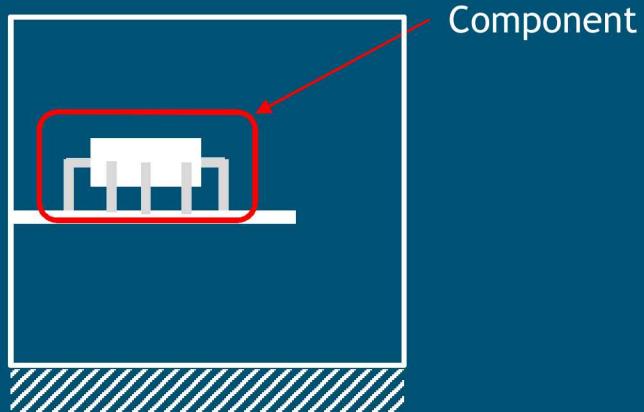
- Predicted system environments
- Predicted component environments
- Unrepresentative component test

Bad Fixturing, an example



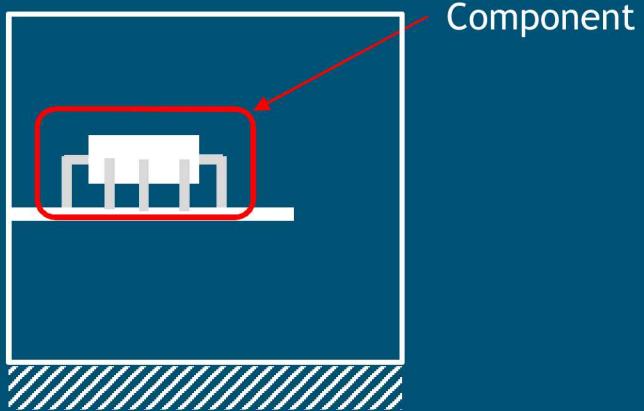
In System

Bad Fixturing, an example



In System

Bad Fixturing, an example

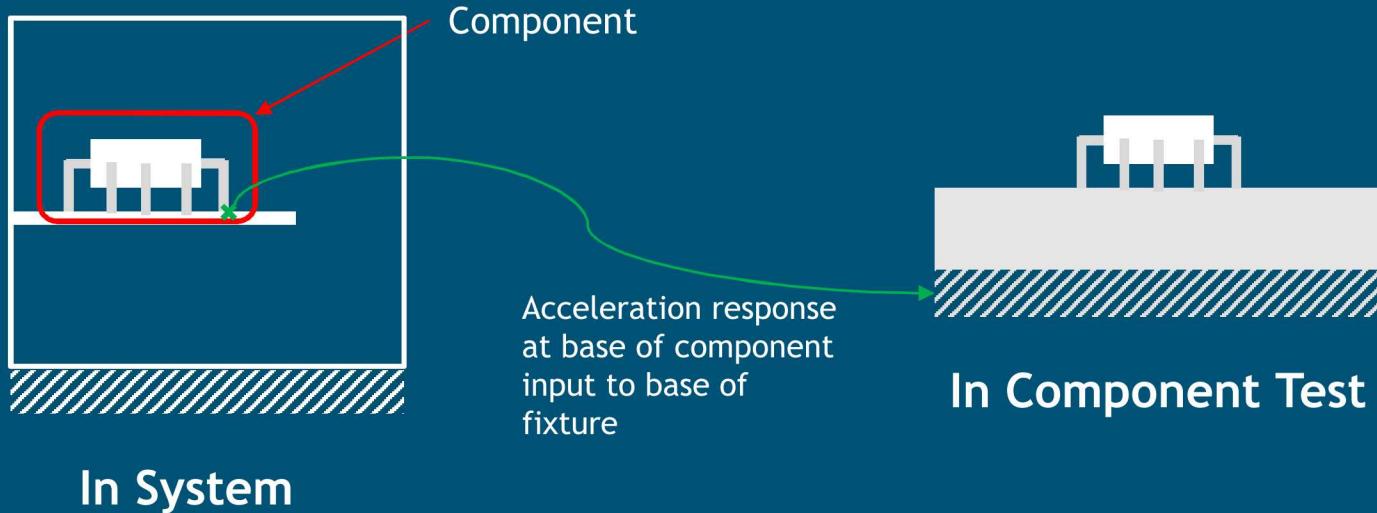


In System

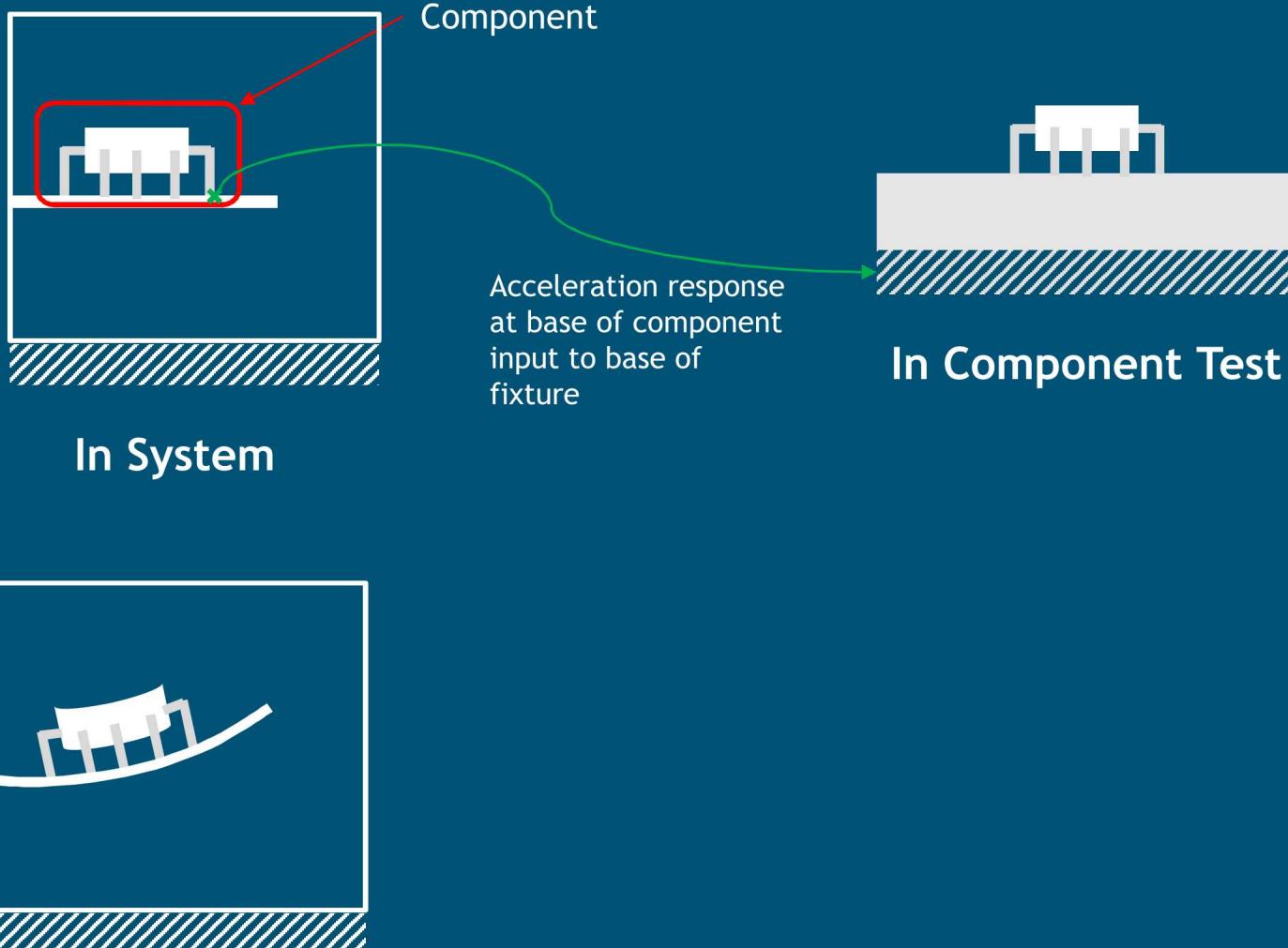


In Component Test

Bad Fixturing, an example

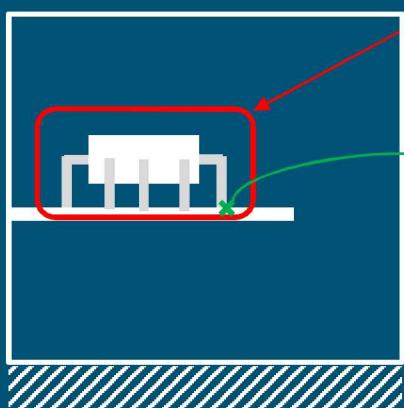


Bad Fixturing, an example



**System response at
plate first frequency**

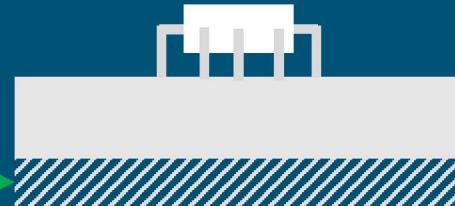
Bad Fixturing, an example



In System

Component

Acceleration response
at base of component
input to base of
fixture



In Component Test



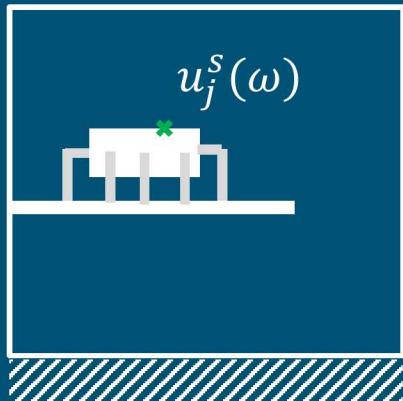
**System response at
plate first frequency**

Cannot replicate this
deformation (and possible
failure mode) with above
component test!

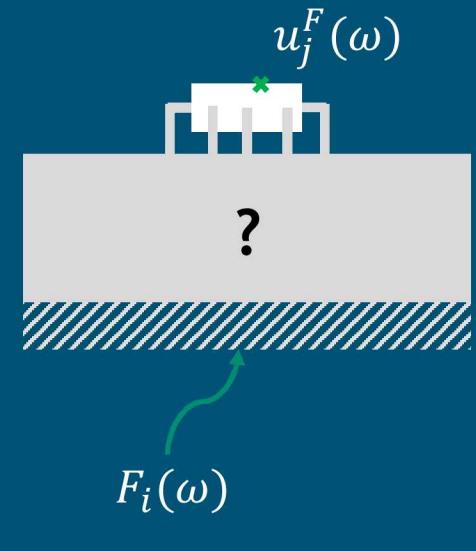
Proposed Approach

Design test fixture that results in component dynamics similar to those of component in system

Restated: Design test fixture such that the Frequency Response Functions relating input (shaker) excitation to component response are as similar to those of the full system as possible.



Objective
Minimize difference
between $u_j^s(\omega)$ and $u_j^F(\omega)$



Proposed Approach

Ma, Zheng-Dong, Noboru Kikuchi, and Hsien-Chie Cheng. "Topological design for vibrating structures." *Computer methods in applied mechanics and engineering* 121.1-4 (1995): 259-280.

Ma, Z-D., Noboru Kikuchi, and I. Hagiwara. "Structural topology and shape optimization for a frequency response problem." *Computational mechanics* 13.3 (1993): 157-174.

Shu, Lei, et al. "Level set based structural topology optimization for minimizing frequency response." *Journal of Sound and Vibration* 330.24 (2011): 5820-5834.

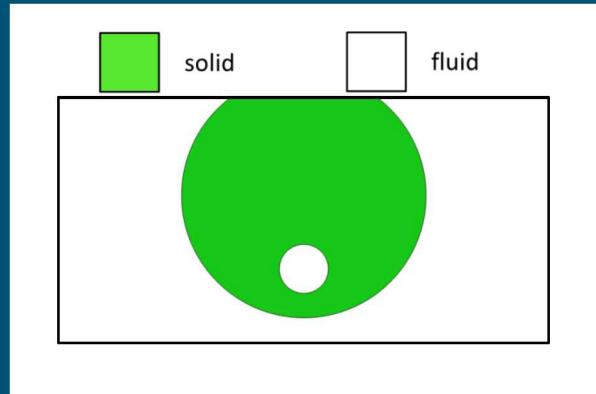
Jensen, Jakob S. "Topology optimization of dynamics problems with Padé approximants." *International journal for numerical methods in engineering* 72.13 (2007): 1605-1630.

Rong, J. H., et al. "Topology optimization of structures under dynamic response constraints." *Journal of Sound and Vibration* 234.2 (2000): 177-189.

Challenges and approach

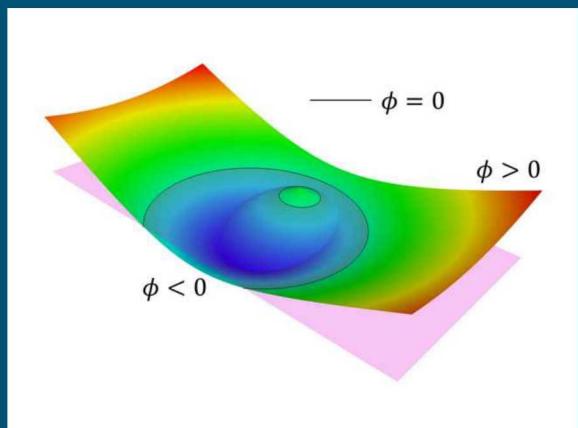
Initial research using both commercial and Plato density method software:

- Significant amounts of intermediate material
- Small material densities led to ill conditioning of linear system
- Non-convex



Our proposed approach: Levelset-CDFEM

- Good:
 - No intermediate material
 - No ill conditioning from void material
 - Start from meaningful geometry (shape optimization)
- Bad:
 - Implementation complexity
 - Computational cost

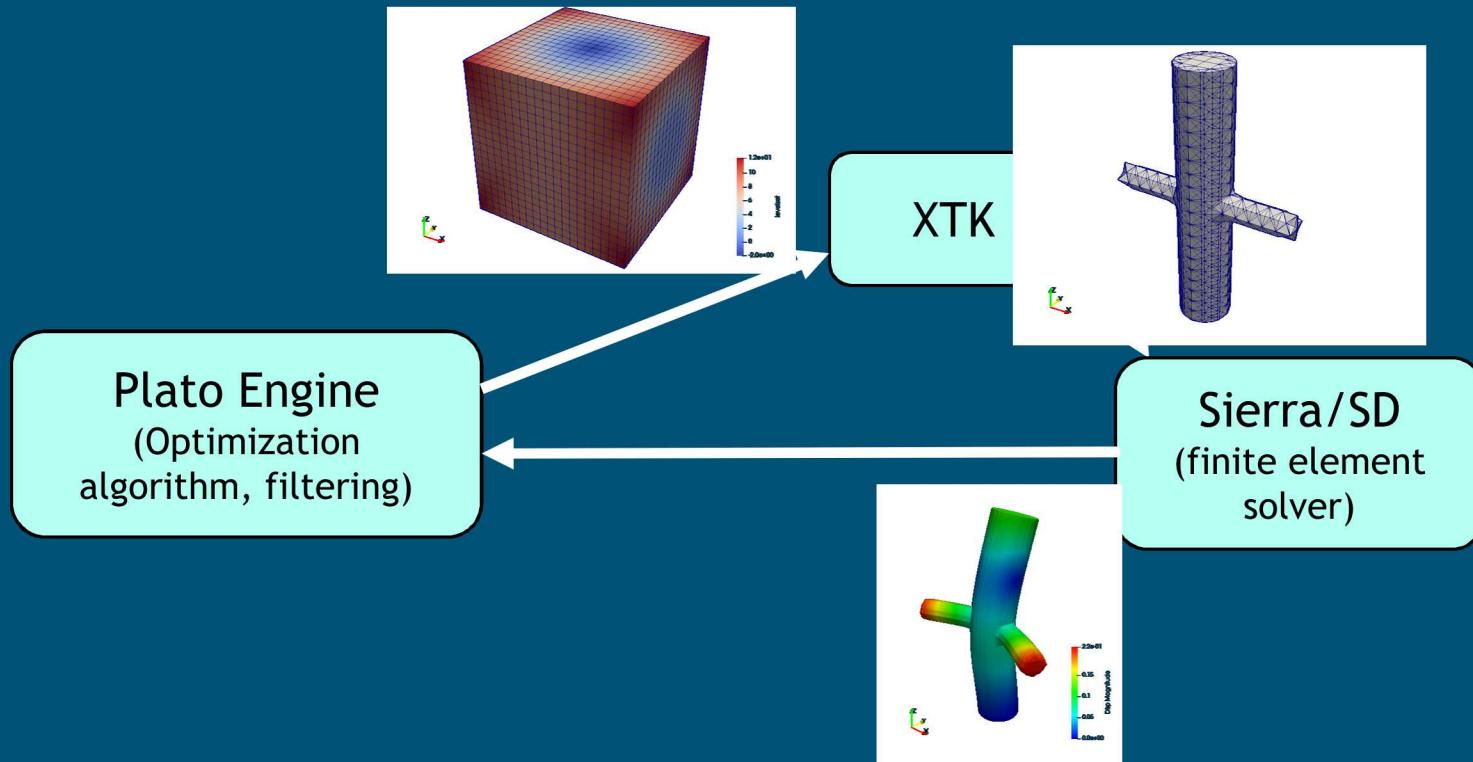


Levelset-CDFEM Approach



How will we implement this?

- Nodal finite element discretization of levelset field
- XFEM ToolKit (XTK) library from CU Boulder (Keenan Doble and Prof Kurt Maute)
 - Produce conformal tetrahedral mesh (CDFEM)
 - Future: incorporate multipoint constraints to construct XFEM system
- Sierra/Structural Dynamics (SD) as finite element solver
- XTK and Sierra/SD wrapped in topology optimization framework provided by new Plato Engine architecture



The Design Problem

Minimize:
$$\sum_{k=1}^{N_\omega} \left[\frac{\kappa}{2} \left(\{\mathbf{u}^k\} - \{\mathbf{u}_S^k\} \right)^T [\mathbf{Q}] \left(\{\mathbf{u}^k\} - \{\mathbf{u}_S^k\} \right) \right]$$

s, \mathbf{u}

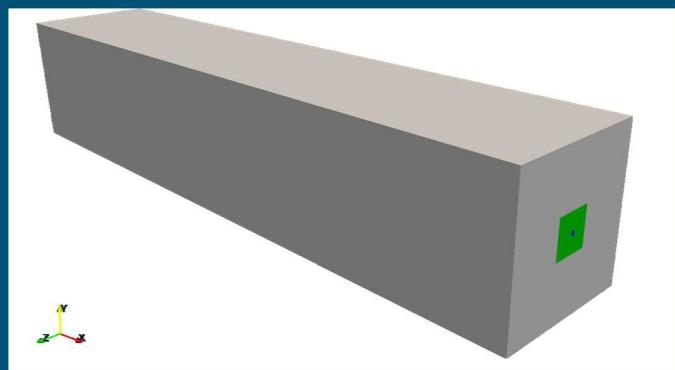
Subject to:
$$[K(\mathbf{s})] \{\mathbf{u}^k\} + i\omega_k [C(\mathbf{s})] \{\mathbf{u}^k\} - \omega_k^2 [M(\mathbf{s})] \{\mathbf{u}^k\} - \{\mathbf{f}_k\} = \{\mathbf{0}\}$$

Consider a beam:

- Traction in x, y and z applied on green patch
- Measured response at blue point
- Fixed left end

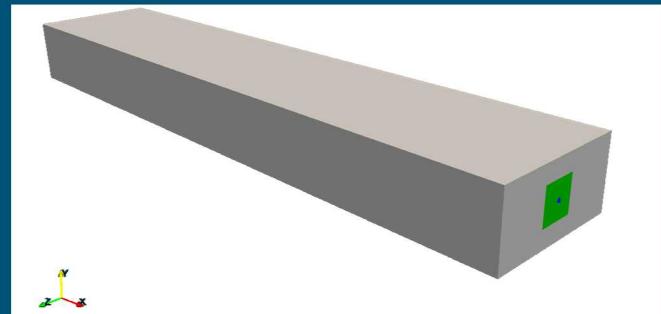
Design domain:

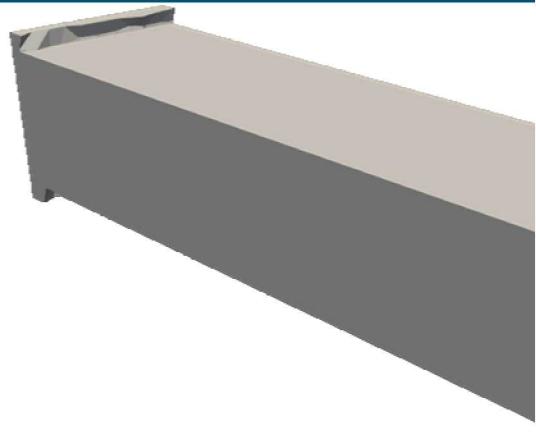
4 cm x 4 cm x 20 cm



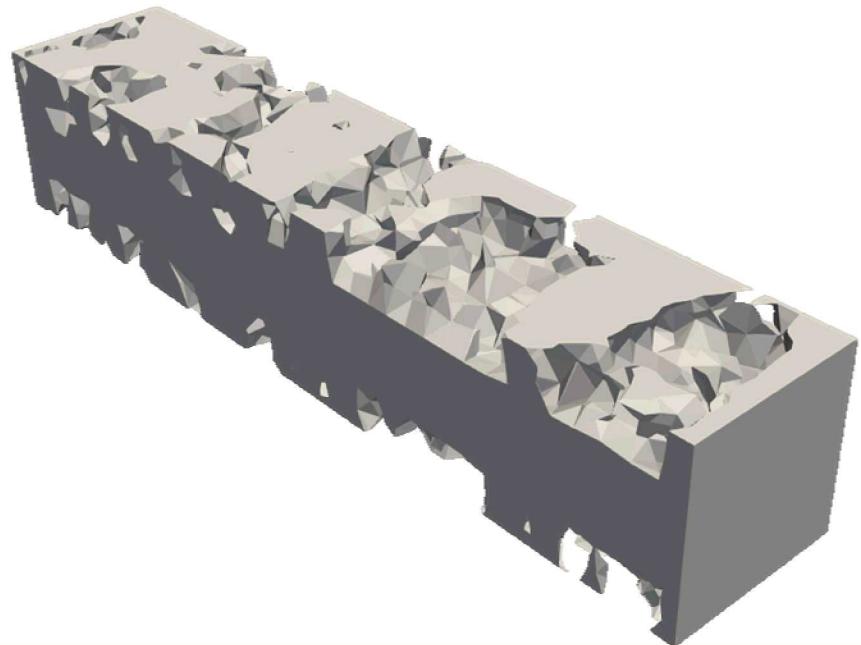
κ	Scaling coefficient
\mathbf{u}^k	displacement degrees of freedom for frequency k
\mathbf{u}_S	System (match) displacement degrees of freedom
N_ω	Number of evaluation frequencies
\mathbf{Q}	degree of freedom boolean/weighting matrix
$K(\mathbf{s})$	Finite element stiffness matrix
ω_k	K-th frequency
$C(\mathbf{s})$	Finite element damping matrix
$M(\mathbf{s})$	Finite element mass matrix
\mathbf{f}_k	Nodal external force at frequency k

Measure \mathbf{u}_S from reference beam:
2cm x 4cm x 20cm



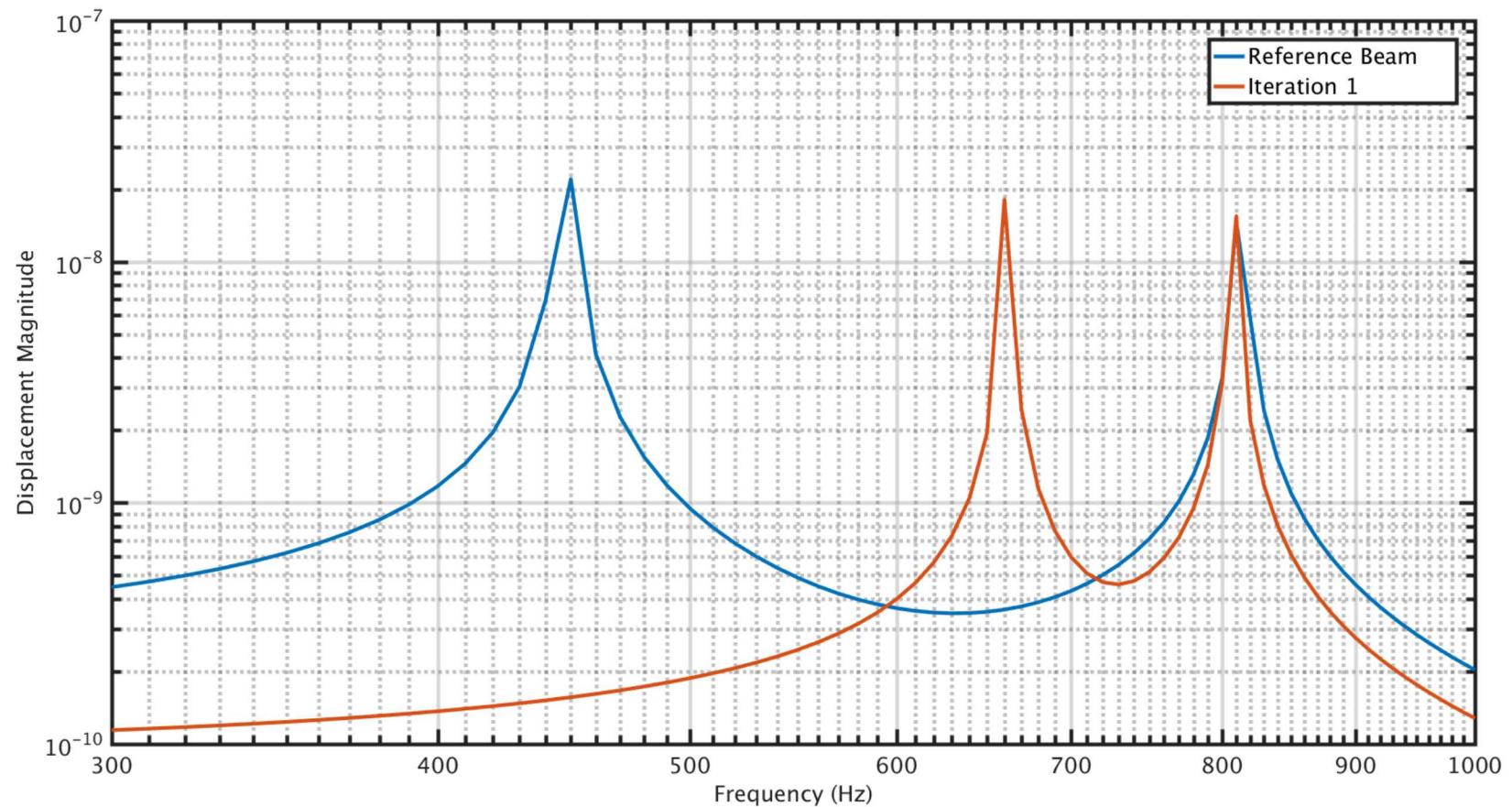


Initial Design

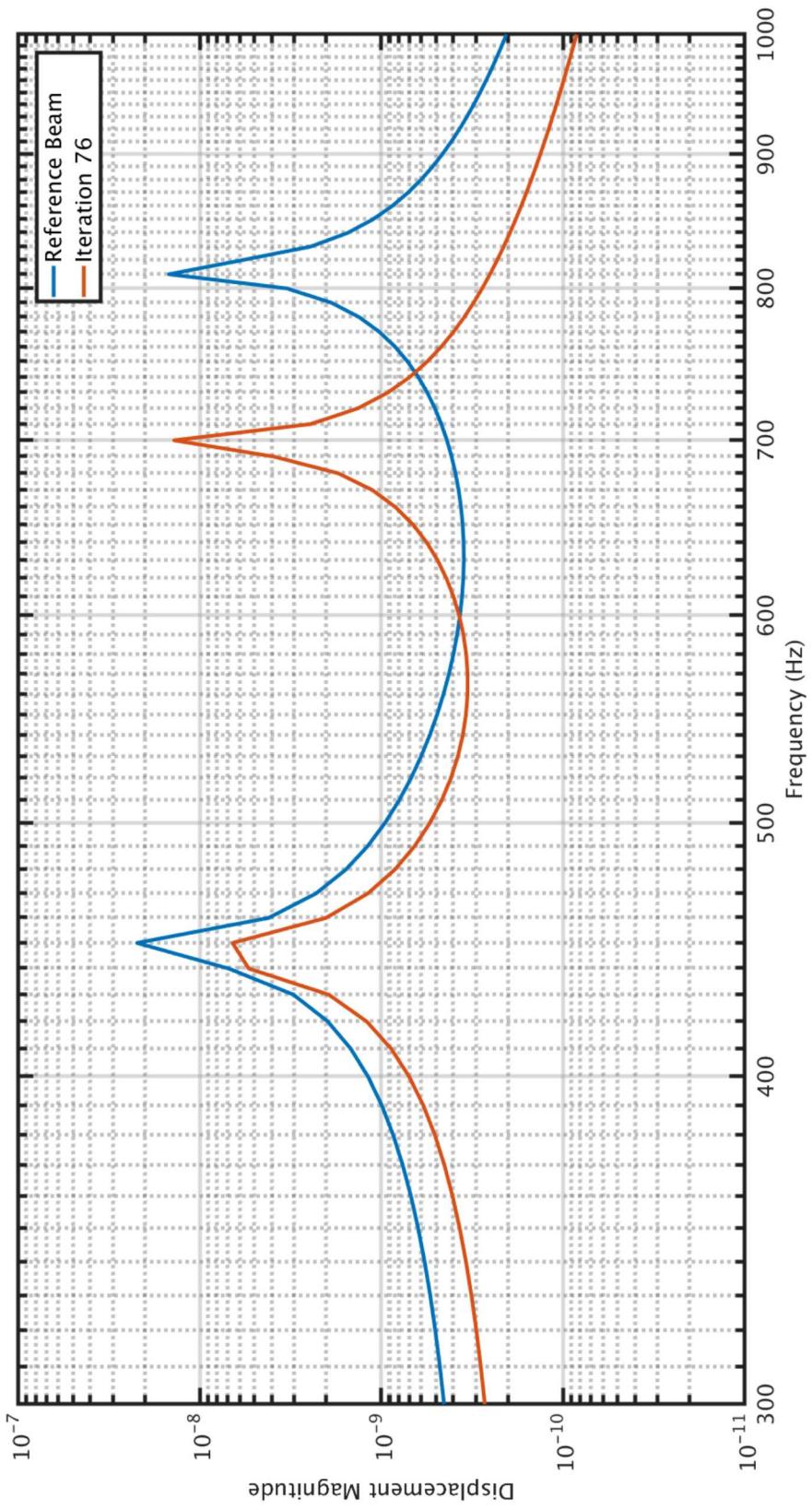


Final Design

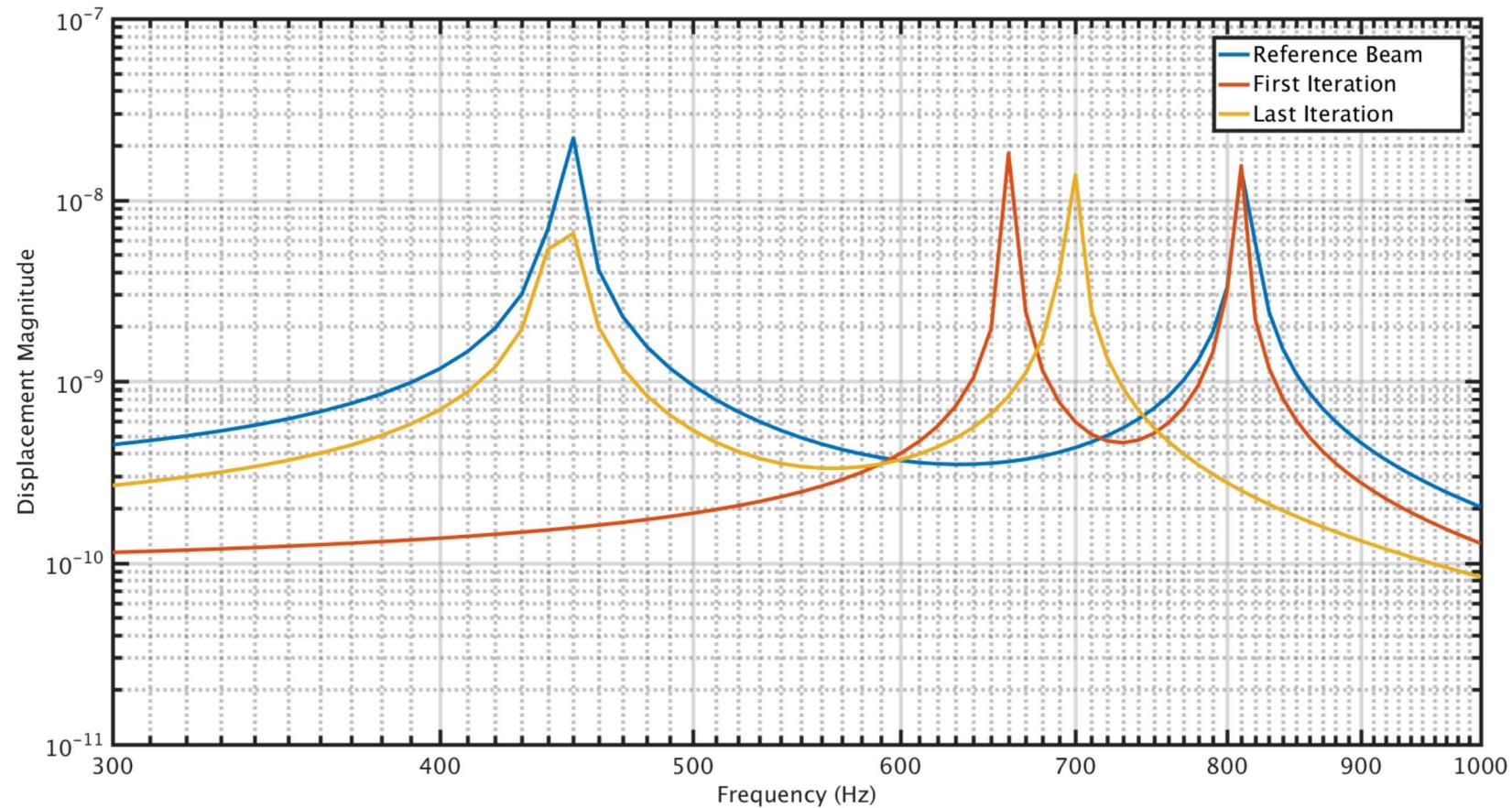
Initial Design Response



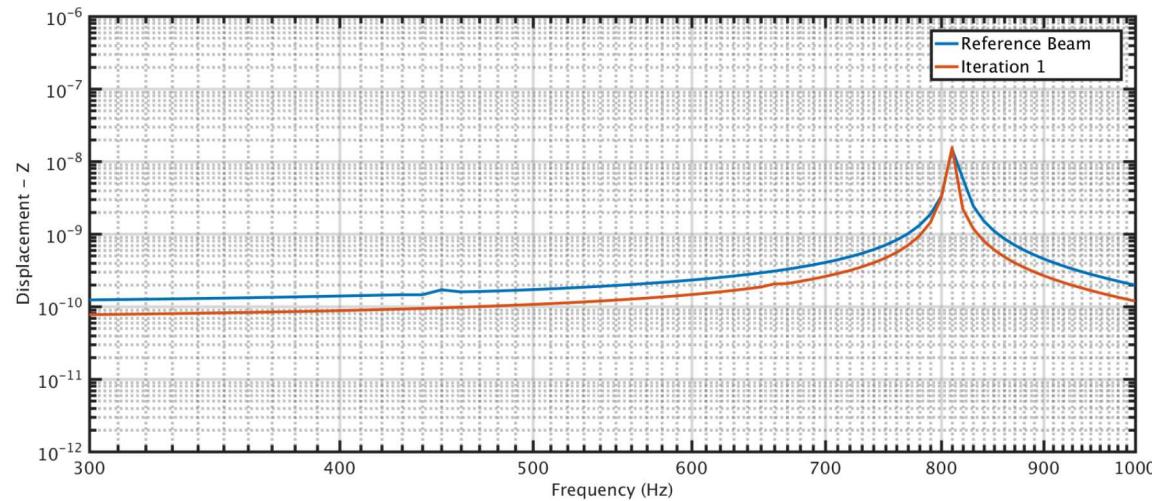
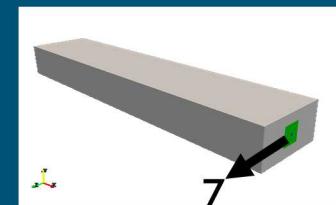
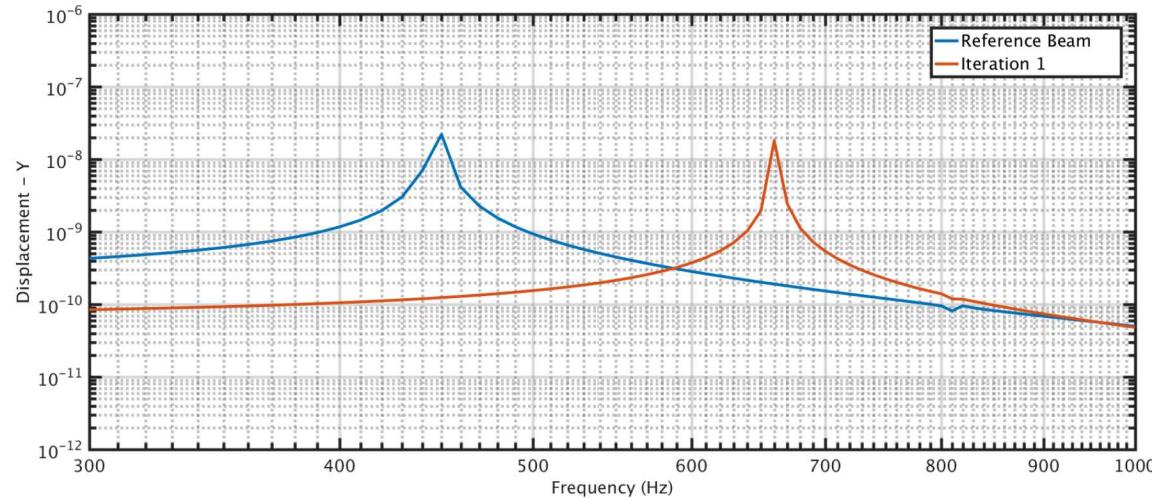
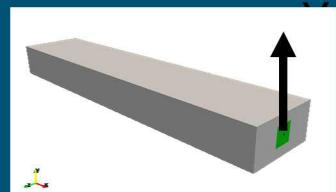
Final Design Response



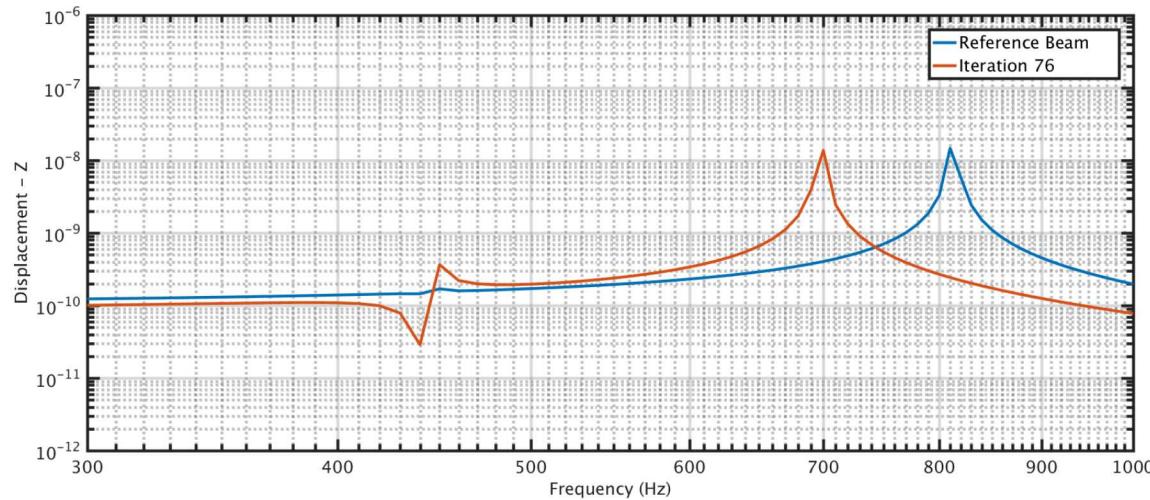
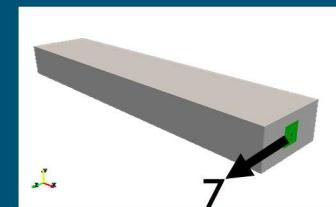
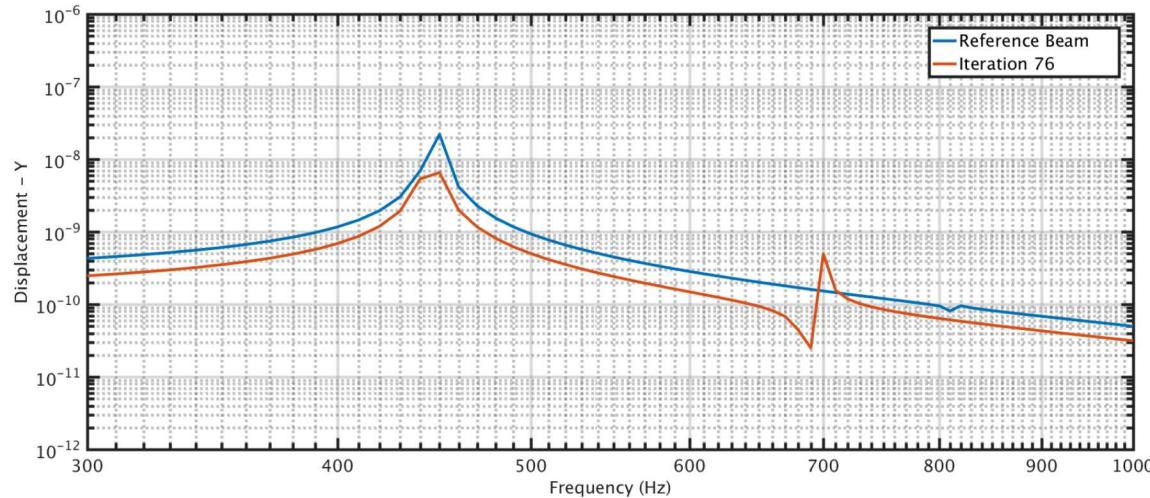
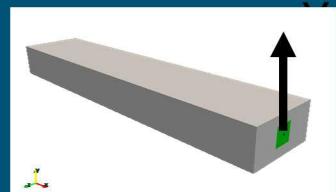
Initial and Final Response



Initial Design Response by Coordinate



Initial Design Response by Coordinate



Conclusions

Problem as posed: density method may have fundamental difficulties

Little available literature on dynamics matching

Levelset-CDFEM Pros:

- Verification problem consistency
- No ill conditioning due to void material
- Easy to start with simple geometry optimization problems and expand

Levelset-CDFEM Cons:

- Non-trivial implementation and verification cost
- Speed penalty for reinitializing solvers
- Filters don't provide geometry control