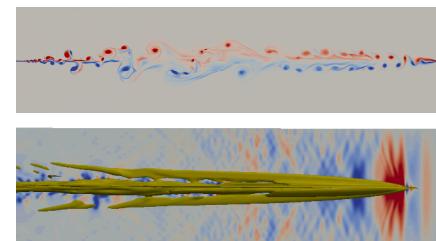
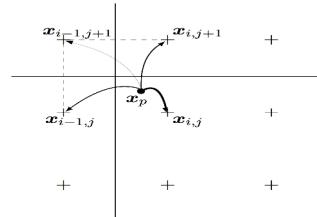
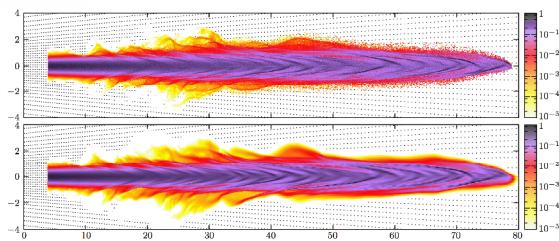


A dense spray solver for injection LES

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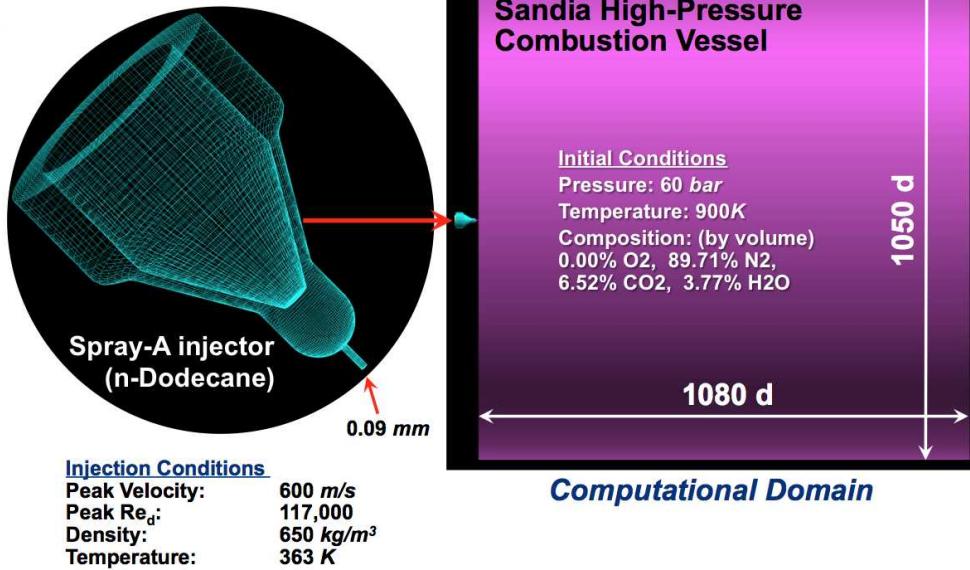
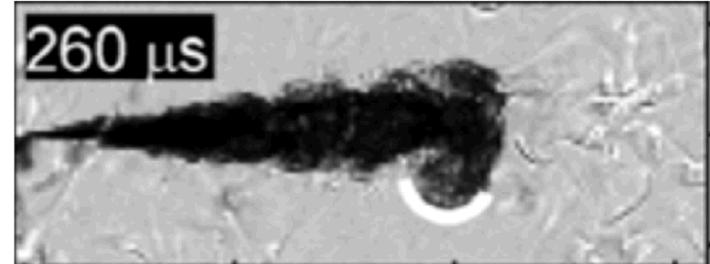
OUTLINE

- 1 Motivation**
- 2 Model**
- 3 Numerics**
- 4 Results**
- 5 Conclusion**

MOTIVATION – Liquid fuel injection

- Inlet is turbulent (+ cavitation)
- Chamber flow high pressure and sonic
- Atomization process not understood

=> all these phenomena drive **mixing** and **combustion**

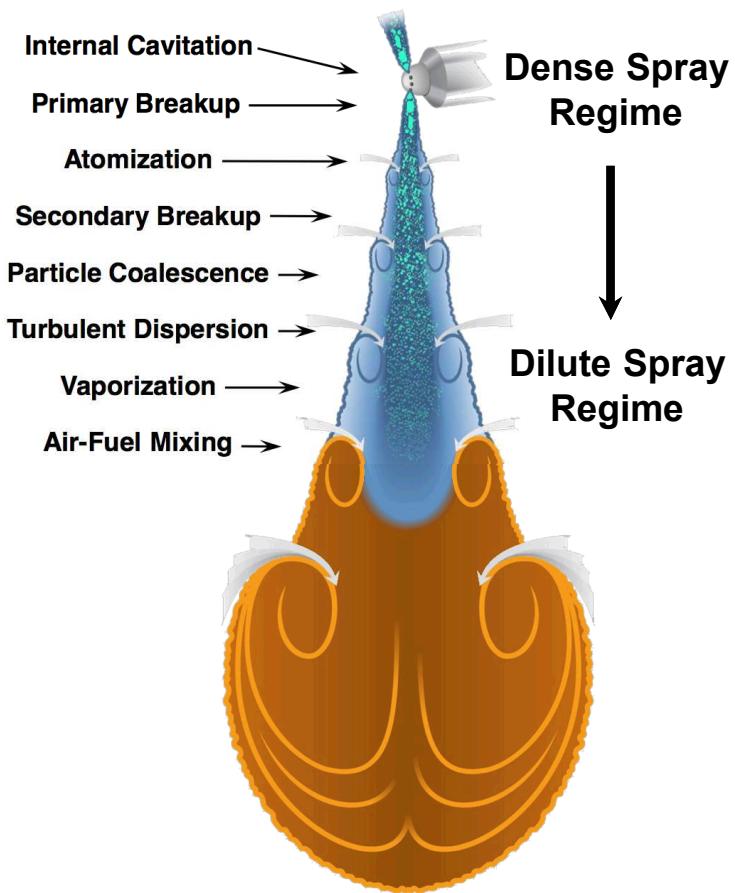


Need
 a **high fidelity** though
affordable simulation

MODEL – Euler-Euler spray

A simplified but promising approach

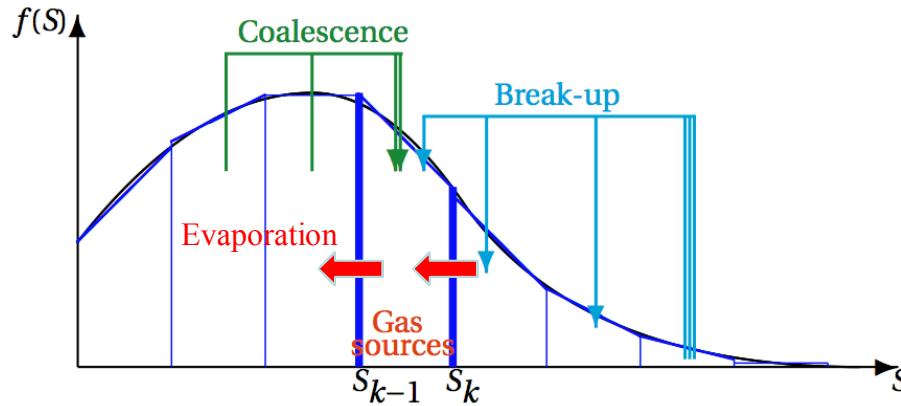
- Coupled NS-PGD (Pressureless Gas Dynamics) can **emulate at once**
 - the inertial behavior of the dense liquid **core**
 - the break-up and dispersion of liquid **blobs** (prescribes size of droplets)
 - the **dilute spray regime**
- ...provided some modeling
= need **closures!**



MODEL – Sectional method

A cost-efficient way to capture polydispersity

- Various drop sizes are treated as a continuum



$$\begin{aligned}
 N_{\text{sec}} \text{ systems} \quad \left\{ \begin{aligned}
 \partial_t n_k + \partial_x \cdot (n_k \mathbf{u}_k) &= {}^2C_k^n + {}^2B_k^n + {}^2E_k^n \\
 \partial_t m_k + \partial_x \cdot (m_k \mathbf{u}_k) &= {}^2C_k^m + {}^2B_k^m + {}^2E_k^m \\
 \partial_t (m_k \mathbf{u}_k) + \partial_x \cdot (m_k \mathbf{u}_k \otimes \mathbf{u}_k) &= m_k \mathbf{F}_k + {}^2C_k^u + {}^2B_k^u + {}^2E_k^u \\
 \partial_t (m_k h_k) + \partial_x \cdot (m_k h_k \mathbf{u}_k) &= m_k \mathbf{H}_k + {}^2C_k^h + {}^2B_k^h + {}^2E_k^h
 \end{aligned} \right. \quad \rightleftharpoons \text{Navier-Stokes with sources}
 \end{aligned}$$

...many integral source terms to compute

MODEL – Euler-Euler spray (E-ES)

Pressureless Gas Dynamics (PGD) decouples Lagrangian advection

- The coupled NS-PGD* system:

$$\left\{
 \begin{aligned}
 \partial_t \rho_g Y_f + \partial_x \rho_g Y_f \mathbf{u}_g &= \omega_f + \sum_k \mathbf{E}_k^{m-g} \\
 \partial_t \rho_g Y_i + \partial_x \rho_g Y_i \mathbf{u}_g &= \omega_i \quad , \quad i \in \llbracket 1; N_{\text{species}} \rrbracket, i \neq f \\
 \partial_t \rho_g \mathbf{u}_g + \partial_x \rho_g \mathbf{u}_g \otimes \mathbf{u}_g &= -\partial_x p + \sum_k \left(-\mathbf{F}_k + \mathbf{u}_k \mathbf{E}_k^{m-g} \right) \\
 \partial_t \rho_g e_g + \partial_x \rho_g e_g \mathbf{u}_g &= -p \partial_x \mathbf{u}_g + \sum_k \left(-\mathbf{H}_k + \mathbf{F}_k (\mathbf{u}_g - \mathbf{u}_k) + h_k \mathbf{E}_k^{m-g} \right) \\
 \partial_t m_k + \partial_x m_k \mathbf{u}_k &= \mathbf{E}_{k+1}^m + \mathbf{B}_k^{m+} + \mathbf{C}_k^{m+} - (\mathbf{E}_k^m + \mathbf{E}_k^{m-g} + \mathbf{B}_k^{m-} + \mathbf{C}_k^{m-}) \\
 \partial_t m_k \mathbf{u}_k + \partial_x m_k \mathbf{u}_k \otimes \mathbf{u}_k &= \mathbf{F}_k + \mathbf{u}_{k+1} \mathbf{E}_{k+1}^m + \mathbf{B}_k^{u+} + \mathbf{C}_k^{u+} - \mathbf{u}_k (\mathbf{E}_k^m + \mathbf{E}_k^{m-g} + \mathbf{B}_k^{m-} + \mathbf{C}_k^{m-}) \\
 \partial_t m_k h_k + \partial_x m_k h_k \mathbf{u}_k &= \mathbf{H}_k + h_{k+1} \mathbf{E}_{k+1}^m + \mathbf{B}_k^{h+} + \mathbf{C}_k^{h+} - h_k (\mathbf{E}_k^m + \mathbf{E}_k^{m-g} + \mathbf{B}_k^{m-} + \mathbf{C}_k^{m-})
 \end{aligned}
 \right. \quad \left. \begin{array}{l} \text{pressureless} \\ \text{sections} \end{array} \right\} \quad k \in \llbracket 1; N_{\text{sec}} \rrbracket$$

*obtained from kinetic theory or conservation principles

$$\partial_t f + \partial_x \mathbf{c} f + \partial_c \mathbf{F} f + \partial_\theta \mathbf{H} f + \partial_r \mathbf{E} f = \mathbf{B} + \mathbf{C}$$

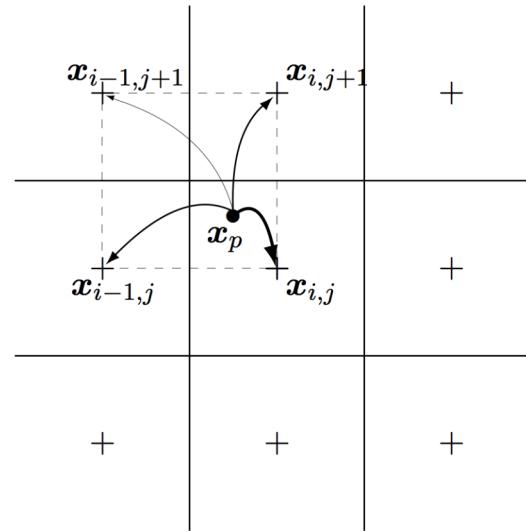
NUMERICS

Outline

- 1) Time integration tailored **splitting**

$$\begin{array}{c}
 \text{Gas transport } \mathcal{T}_g \\
 \hline
 \text{Section transport } \mathcal{T}_k
 \end{array}
 = \begin{array}{c}
 \text{Coupling } \mathcal{R} \\
 \mathcal{F} + \mathcal{H} + \mathcal{E}
 \end{array} + \begin{array}{c}
 \text{Spray sources} \\
 \mathcal{B} + \mathcal{C}
 \end{array}$$

- 2) PGD transport novel **semi-Lagrangian scheme**



NUMERICS – Time integration

A Tailored Operator Splitting

Operator splitting

- Recycle legacy solvers
- Robust time integration
- Local properties enforced
- Adaptable accuracy

$$\begin{array}{c}
 \text{Gas transport } \mathcal{T}_g \\
 \hline
 \text{Section transport } \mathcal{T}_k
 \end{array}
 = \begin{array}{c}
 \text{Coupling } \mathcal{R} \\
 \mathcal{F} + \mathcal{H} + \mathcal{E}
 \end{array} + \begin{array}{c}
 \text{Spray sources} \\
 \mathcal{B} + \mathcal{C}
 \end{array}$$

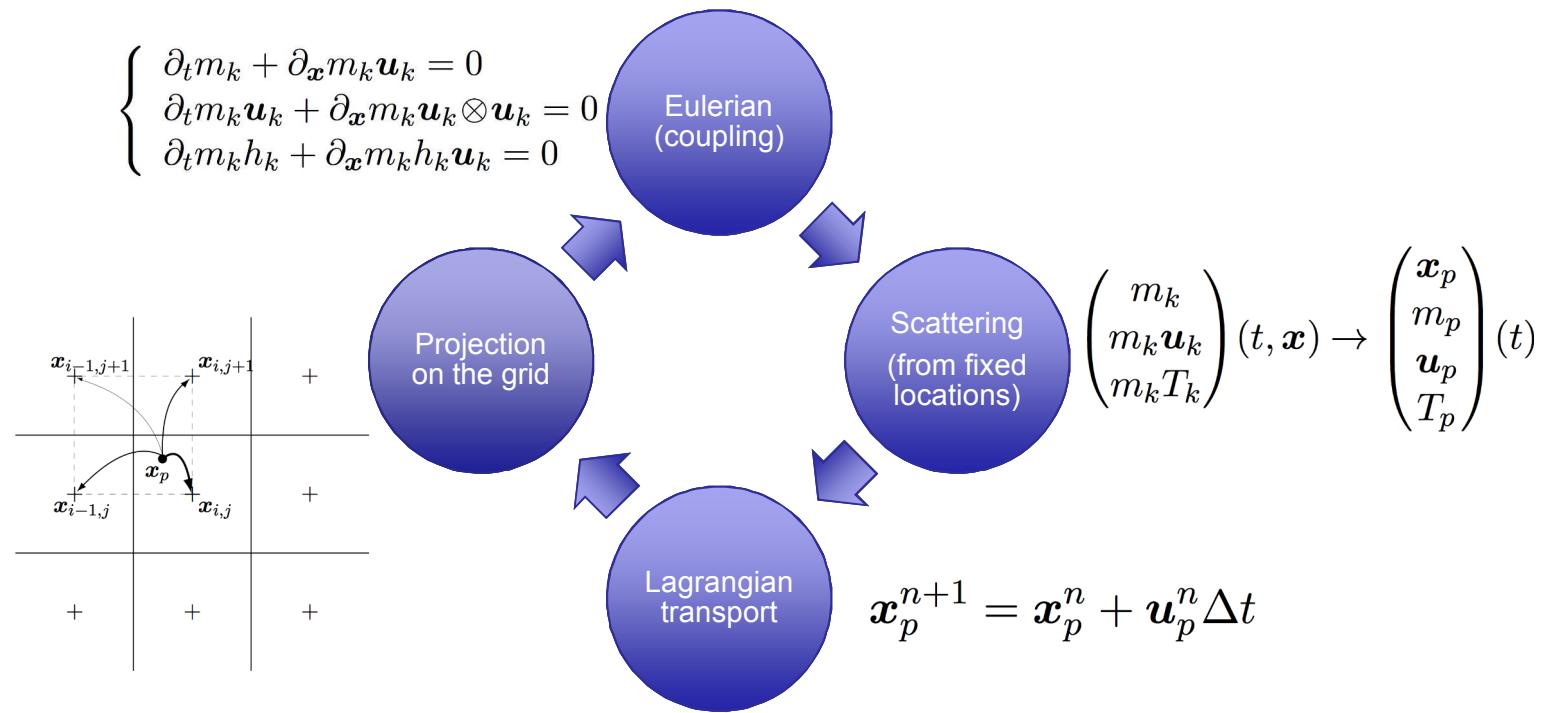
- to integrate all phase exchange terms \mathcal{R} at once (RK4)
 - Realizability, conservativity, equilibrium
 - Strong couplings
- to integrate spray sources $\mathcal{B} + \mathcal{C}$
 - Realizability and convergence
 - Strong particle-particle coupling

$$U^{n+1} = \mathcal{R} \prod_{k=1}^{N_{\text{sec}}} (\mathcal{T}_k) \mathcal{T}_g U^n$$

$$U^n = \begin{pmatrix} \rho_g Y_i \\ \rho_g \mathbf{u}_g \\ \rho_g e_g \\ n_k \\ m_k \\ m_k \mathbf{u}_k \\ m_k h_k \end{pmatrix}^n$$

NUMERICS – PGD transport

A robust and accurate answer to PGD peculiarities

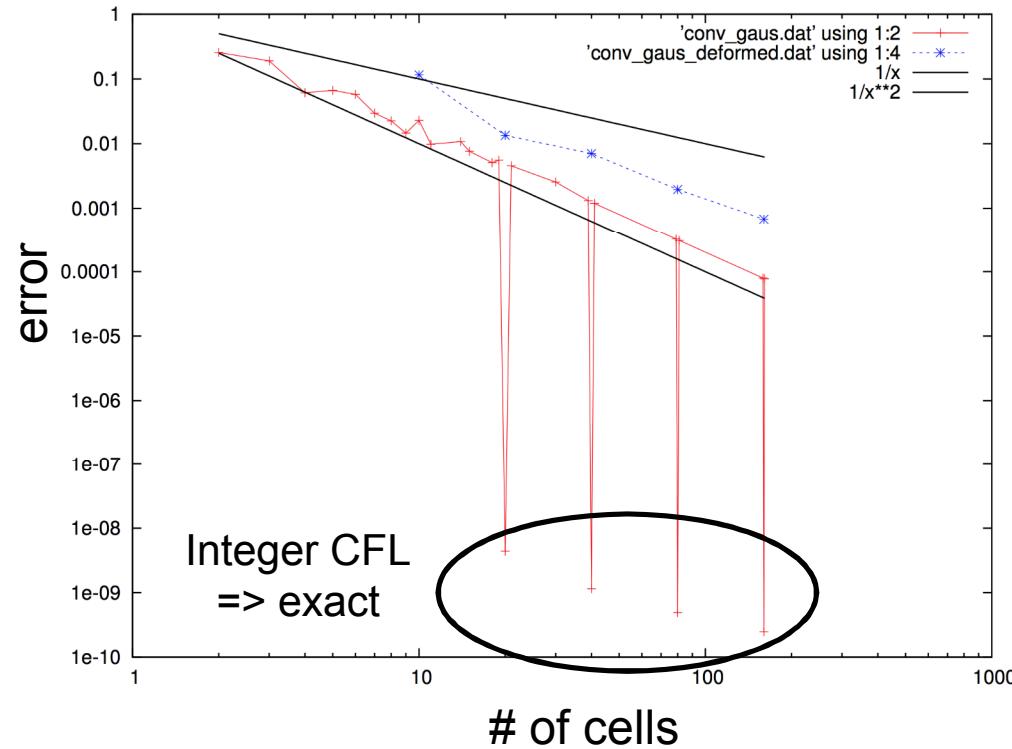
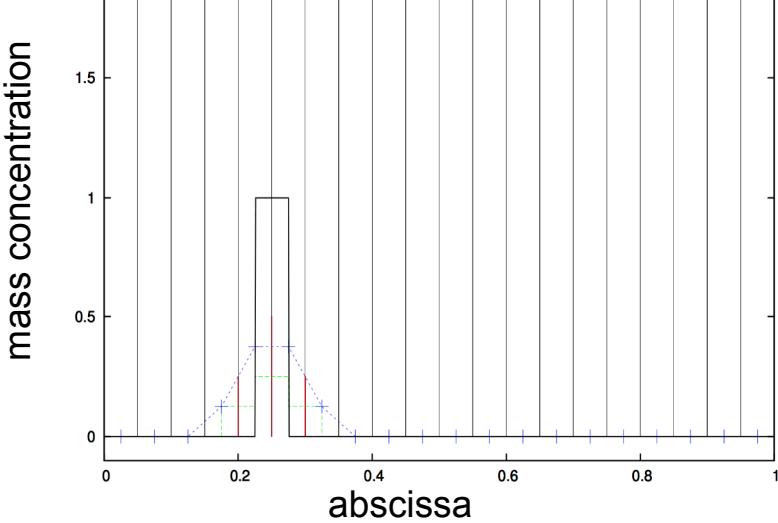


- **Novel semi-Lagrangian PGD transport scheme**
 - **Deterministic: no noise**
 - **Localizes spray info at mesh nodes: good for coupling**
 - **Easier load balancing**
 - **No fluxes to be computed: reduce cost and numerical diffusion**

NUMERICS – PGD transport

Transport is 2nd order in space

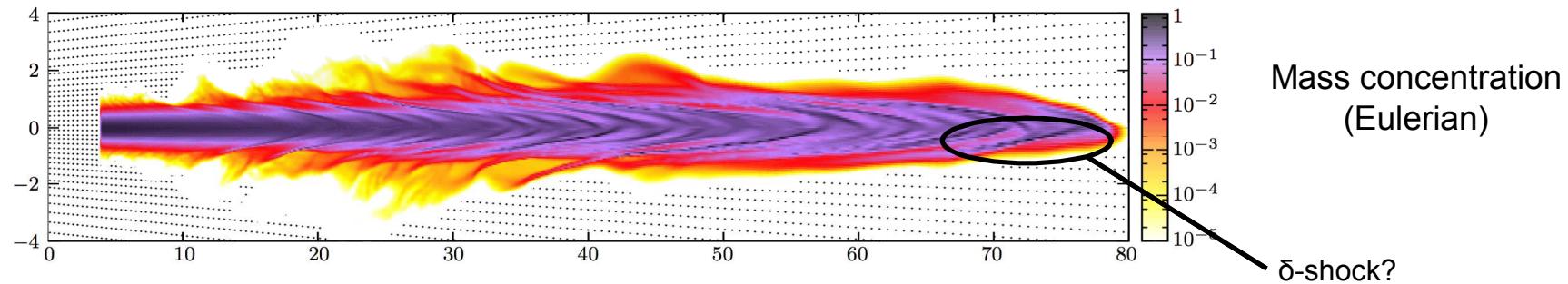
- No CFL constraint (unconditionally stable)
- Handles vacuum
- Handles δ -shocks



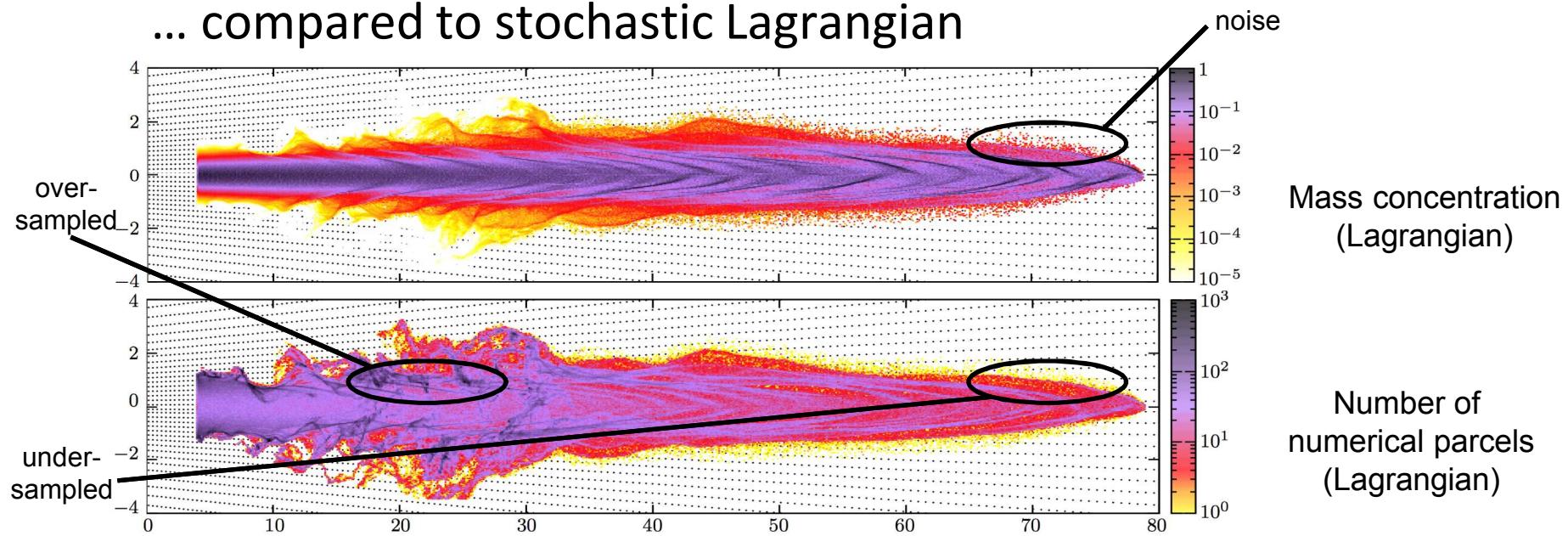
RESULTS – PGD transport

2D test with prescribed flow field

- Obtained **cost-efficient** and **accurate** results



... compared to stochastic Lagrangian

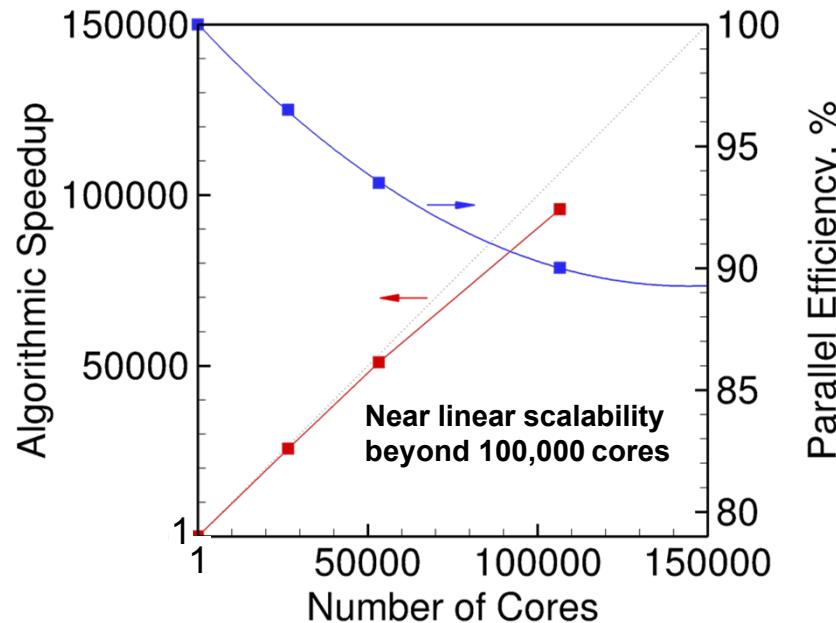


NUMERICS – Raptor

A general solver optimized for LES

- Theoretical framework
 - Fully-coupled, compressible conservation equations
 - Real-fluid equation of state (high-pressure phenomena)
 - Detailed thermodynamics, transport and chemistry
 - Multiphase flow, spray
 - Dynamic SGS modeling (No Tuned Constants)
 - Advanced UQ methods for error/sensitivity analysis

(No
Tuned Constants)



- Numerical framework
 - Staggered finite-volume differencing (non-dissipative, discretely conservative)
 - Dual-time stepping with generalized preconditioning (all-Mach-number formulation)
 - Detailed treatment of geometry, wall phenomena, BC's

- High-performance computing framework (Advanced parallel programming model that makes optimal use of advanced MP-computer architectures)
- Results from strong and weak scaling on Oak Ridge National Laboratory CRAY XK7 (Titan), June 2013
 - Test case – jet-in-cross-flow, 500-million cells
 - Strong scaling: 24,000 to 120,000 cores, > 90% efficiency
 - Weak scaling: 500-million-cells/24,000-cores to 2-billion-cells/120,000-cores, < 4% increase in CPU time
- Currently being refactored for hybrid multi-core parallelism and GPU acceleration (MPI/OpenMP/OpenACC)

RESULTS – Momentum Coupling

Comparison between E-ES and CLSVOF

- ✓ Supersonic injection
 - velocity plug-flow boundary
 - no thermal transfer

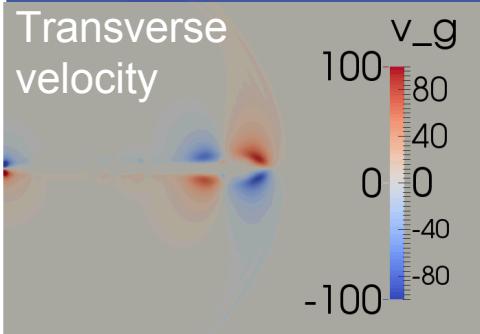
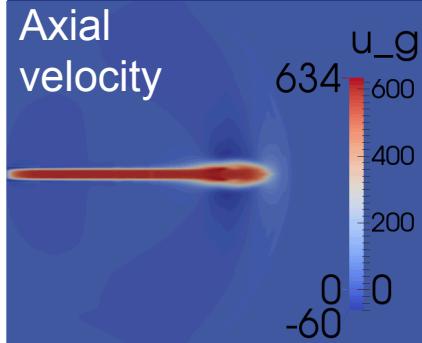
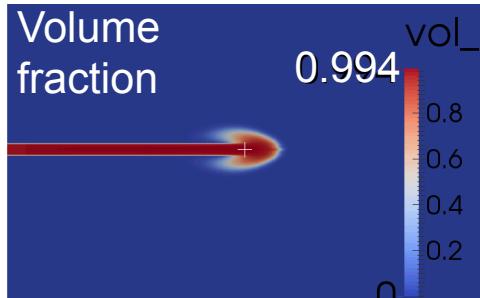
- ✓ Agreement on **gas entrainment**

- ★ Liquid density discrepancy results from **pressureless** assumption

- ★ Jet tip is different because of **lack of surface tension**

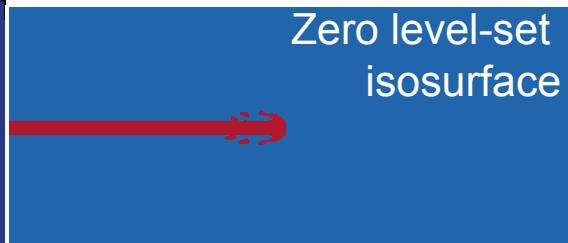
Raptor with E-ES

$\Delta x = 12.5 \mu\text{m}$, $\Delta t = 8 \text{ ns}$

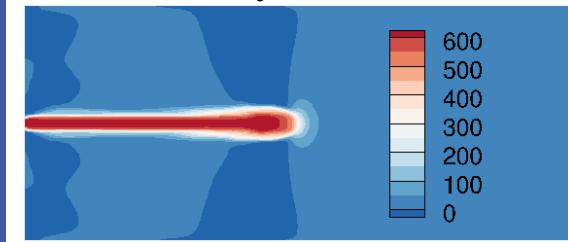


CLSVOF

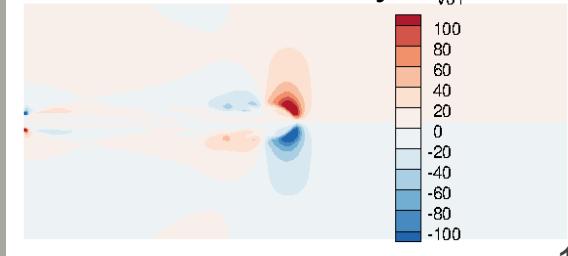
$\Delta x = 13.3 \mu\text{m}$, $\Delta t \sim 6 \text{ ns}$



Axial velocity



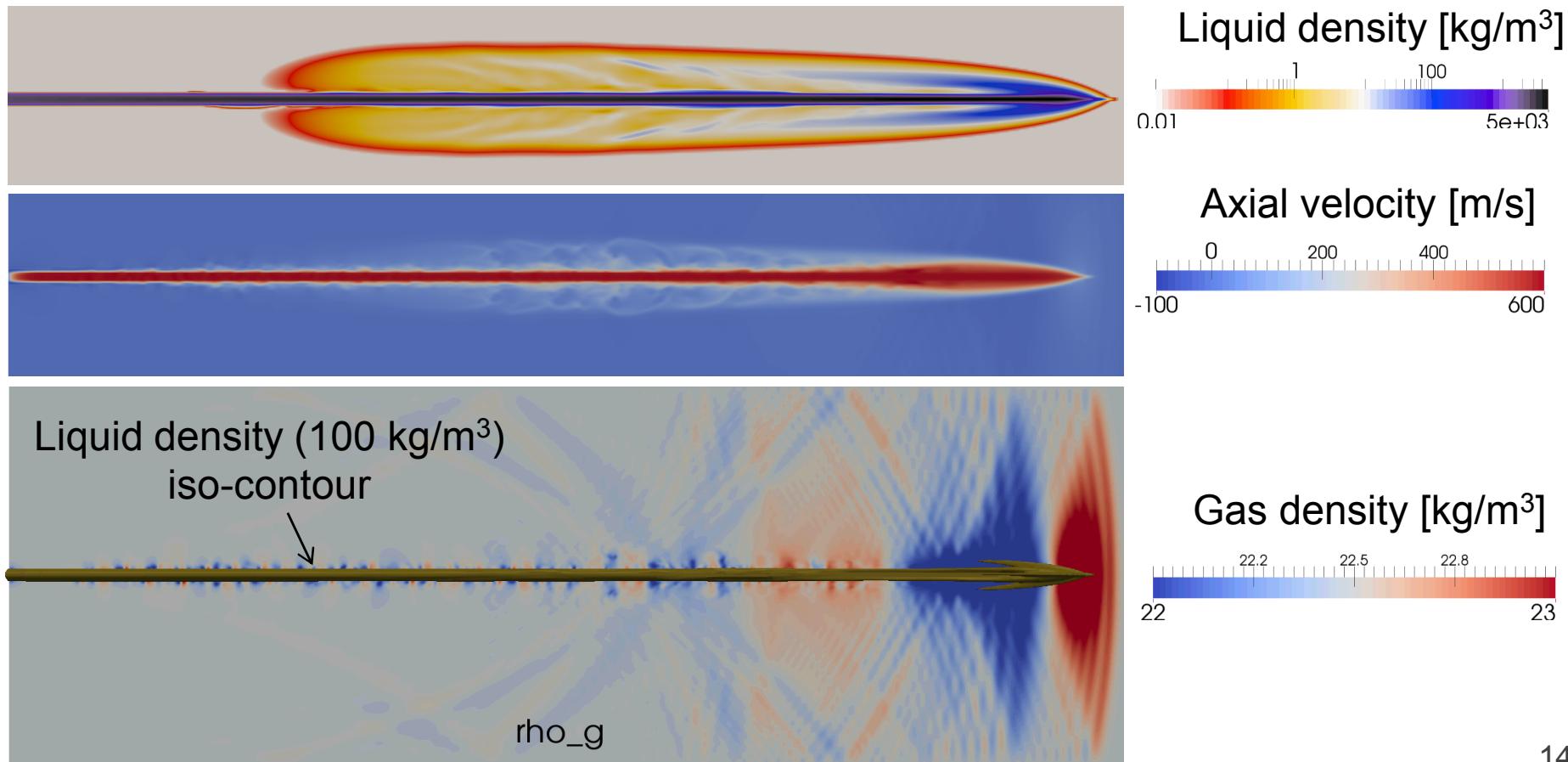
Transverse velocity



RESULTS – Momentum coupling

Entrainment and induced turbulence by jet injection

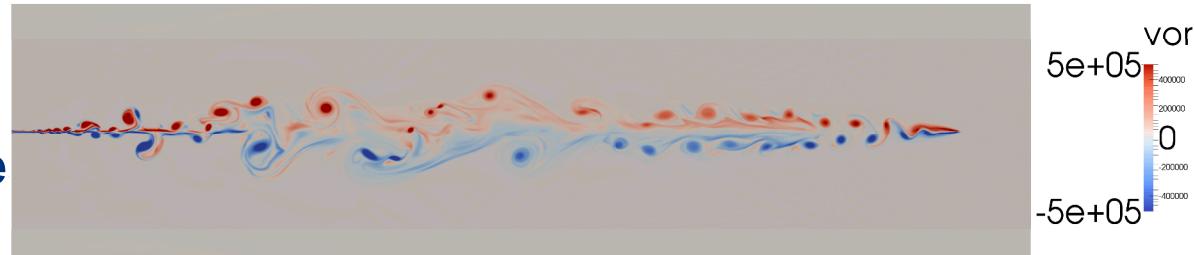
- Executed with **RAPTOR + E-ES**



CONCLUSION

Spray tools

- **kinetic theory**
- **microscopic closure**
- **dedicated numerics**



... are promising to efficiently **handle injection**.

Perspectives (1 year)

- **Dense core dynamics**
 - pressure
 - turbulence
 - surface tension
- **High-pressure mixing**
 - atomization
 - “evaporation”
 - LES closure
- **Combustion**
 - chemistry
 - LES closure
 - numerics