

## High-fidelity simulation of wind-turbine incompressible flows with classical and aggregation AMG preconditioner

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# Outline

- Solve time-dependent incompressible Navier-Stokes equations
- Resolve near blade surface boundary layer and wake vortices
- Compare the two fundamental algebraic-multigrid (AMG) approaches :
  - ▶ Smoothed Aggregation AMG (SA-AMG), as implemented in MueLu (with linear solve in Tpetra Belos ICGS-GMRES);
  - ▶ Classical Ruge-Stüben AMG (C-AMG), as implemented in Hypra (with linear solve in Hypra's MGS-GMRES);
- Examine ExaWind baseline problem:
  - ▶ Vestas V27 wind turbine with sliding mesh interface
- Determine  $V$ -cycle complexity  $C$  and stencil widths  $S_{avg}$
- Compare GMRES iterations, solver time, set-up time.

# Exascale Computational Challenge

Simulation of wake turbulence difficult problem:

- Vestas V27 with 27m turbine diameter. 225 KW
- Matrices are re-initialized every time-step
- Large dynamic scale range and high aspect-ratios
- Sliding mesh adds skew-symmetric terms to non-symmetric matrices
- Ill-conditioned pressure-Poisson problem
- $C = 50$ ,  $\Delta t = 1e-4s$ ,  $\mathcal{O}(10000)$  time steps per revolution. 400 hours on Cori 24K cores
- Peta-scale single to exascale multiple turbines



# Incompressible Navier-Stokes Equations

Control Volume Finite Element Method results in block-matrix: saddle-point, indefinite

$$\begin{bmatrix} A & G \\ D & 0 \end{bmatrix} \begin{bmatrix} u \\ p \end{bmatrix} = \begin{bmatrix} f \\ b \end{bmatrix}$$

$A = I/\Delta t + \mu L + N$ , Laplacian  $L$ , viscosity  $\mu$  and nonlinear convection  $N$ .

Consider the block  $LU$  factorization of the matrix

$$\begin{bmatrix} A & G \\ D & 0 \end{bmatrix} = \begin{bmatrix} A & 0 \\ D & -DA^{-1}G \end{bmatrix} \begin{bmatrix} I & A^{-1}G \\ 0 & I \end{bmatrix}$$

Inversion of  $A^{-1}$  to form the Schur complement matrix  $S = -DA^{-1}G$  would be costly.

Matrix splittings (Chorin-Teman, Yosida) employ  $\tau = \text{diag}(A)^{-1}$ ,

$$\int L_1 \phi \, dV = \int \tau_1 \nabla \phi \cdot dA, \quad \int L_2 \phi \, dV = \int \tau_2 \nabla \phi \cdot dA$$

$B_1 = -L_1$  is the finite-volume Laplacian for the pressure-Poisson linear system

# Incompressible Navier-Stokes Equations

These matrices are introduced into an approximate  $LU$  block factorization as follows

$$\begin{bmatrix} A & 0 \\ D & B_1 \end{bmatrix} \begin{bmatrix} I & B_2 G \\ 0 & I \end{bmatrix} \begin{bmatrix} u^{n+1} \\ \Delta p^{n+1} \end{bmatrix} + \begin{bmatrix} I & 0 \\ DB_4 & B_3 \end{bmatrix} \begin{bmatrix} I & G \\ 0 & I \end{bmatrix} \begin{bmatrix} 0 \\ p^n \end{bmatrix} = \begin{bmatrix} f \\ b \end{bmatrix}$$

where  $B_2 = \tilde{\tau}_2 I$ ,  $B_3 = -L_2$  and  $B_4 = \tilde{\tau}_4 I$ ,  $\tilde{\tau}_i = \tau_i/\rho$ .

The equations solved at each outer nonlinear iteration of the time-step are given by

$$A\Delta\hat{u} = f - Gp^n - Au^n \quad (1)$$

$$-L_1\Delta p^{n+1} = D(\hat{u} + \tilde{\tau}_2 Gp^n) + L_2 p^n + b \quad (2)$$

$$u^{n+1} = \hat{u} - \tilde{\tau}_3 G\Delta p^{n+1} \quad (3)$$

where  $\Delta\hat{u} = \hat{u} - u^n$ ,  $\Delta p^{n+1} = p^{n+1} - p^n$ .

Solve for pressure increment (2) with restarted GMRES( $m$ ) and AMG preconditioner.

## Sliding Mesh: Nonsymmetric Matrices

- Sliding mesh based on discontinuous-Galerkin (DG) interior penalty (IP) term
- Adjacent  $\Omega_A$  and  $\Omega_B$  contribute non-symmetric terms in pressure-Poisson matrix
- Skew-Symmetric flux terms  $\hat{C}(A, B) = -\hat{C}(B, A)$  at interface  $\Gamma^{BA}$

$$\int_{\Gamma \setminus \Gamma^{AB}} \rho \hat{u} n_j d\Gamma + \int_{\Gamma^{AB}} \hat{C}(A, B) d\Gamma = 0$$

$$\int_{\Gamma \setminus \Gamma^{BA}} \rho \hat{u} n_j d\Gamma + \int_{\Gamma^{BA}} \hat{C}(B, A) d\Gamma = 0$$

$$\hat{C}(\alpha, \beta) = \frac{1}{2} (m_j^\alpha n_j^\alpha - m_j^\beta n_j^\beta) + \lambda_C^{\alpha\beta} (p^\alpha - p^\beta), \quad \lambda_C^{\alpha\beta} = \frac{\tau}{2} \left( \frac{1}{L^\alpha} + \frac{1}{L^\beta} \right)$$

## Algebraic Multigrid

Smoothed aggregation (SA-AMG) is based on strongly connected neighborhoods:

$$N_i(\theta) = \left\{ j : |a_{ij}| \geq \theta \sqrt{a_{ii} a_{jj}} \right\}$$

Define  $C_i$  as the set of nodes in aggregate  $i$  and  $\tilde{P}_{ij} = 1$ ,  $i \in C_j$ , and 0 otherwise.

Prolongator,  $P = \left( I - \omega D^{-1} A^F \right) \tilde{P}$  where  $D = \text{diag}(A)$ ,  $A^F$  is the filtered matrix,

The classical Ruge-Stüben AMG (C-AMG) algorithm works in two passes:

- The first pass will make a selection of coarse nodes based on the number of strong connections that each node has
- The second pass is a refinement pass. It checks to make sure there are enough coarse nodes that information is not lost

Given a threshold value  $0 < \theta \leq 1$ , the node  $u_i$  is strongly connected to  $u_j$  if

$$|a_{ij}| \geq \theta \max_{k \neq i} |a_{ik}|$$

The prolongation matrix  $P$  is constructed row wise.

## Set-up for C-AMG

Hypre–BoomerAMG : V-cycle

- parallel modified independent set (PMIS) coarsening of de Sterck (2004)
- strength of connection threshold  $\theta = 0.25$
- extended  $+i$  coarse–fine interpolation.  $pmax = 2$  elements interpolation stencil
- aggressive coarsening on first 3 levels with multi-pass interpolation  $pmax = 2$
- hybrid Gauss-Seidel smoother with 2 sweeps per level
- interpolation truncation  $\tau = 0.25$
- retain transpose in Galerkin triple-product
- Sparsification on first 3 levels: drop tolerances  $\gamma = [0.0, 0.01, 0.01]$ .



## Set-up for SA-AMG

Trilinos-MueLu : V-cycle

- symmetric SA coarsening
- unsmoothed prolongation  $\omega = 0$
- aggregate size min 3, max 8
- strength of connection threshold  $\theta = 0.03$  and distance Laplacian dropping
- implicit operator-stencil
- $L_1$  Gauss-Seidel smoothers. 2 sweeps
- re-balancing coarse matrices to improve parallel performance
- SuperLU coarse solver

## Complexity and Stencil Width

Operator complexity  $C$  is defined as

$$C = \sum_{l=0}^m nnz(A_l) / nnz(A).$$

Directly correlated to the solver execution time

Average stencil size  $s(A_l)$  is the average number of non-zero elements per row of  $A_l$

Maximum average stencil size,

$$S_{avg} = \max_{1 \leq l \leq m} s(A_l)$$

Directly correlated to the solver set-up time

## Vestas V27 Flow Field

- Turbulent air-flow modeling with wake vortex formation
- Rotational speed 43 RPM with a cross wind of 7.6 m/s

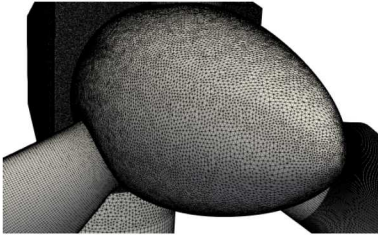


Figure: V27 41a 166M element mesh (45M pressure DOF).

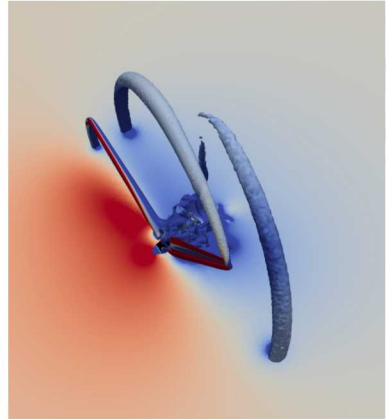


Figure: Pressure at 0.75sec. Isosurface of  $v = 10$  m/s.

## Pressure Solve and Set-up Times

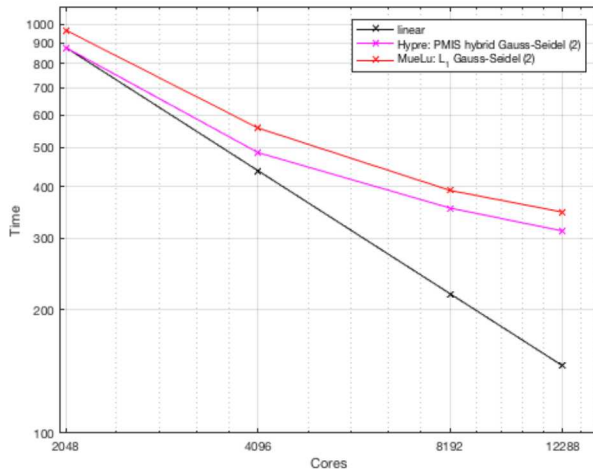
Model	$sw$	$C$	$S_{avg}$	$\theta$	Iterations	Solver (s)	Set-up (s)	Wall-clock (s)
Nalu+Hypre	2	1.149	21.4	0.25	17.7	58.0	24.5	355
Nalu+MueLu	2	1.150	19.6	0.03	25.8	54.9	24	392

Table: V27 41 R1 500M elem, 229M Pressure DOF, 27K DOF/core: 8192 cores Cori, 10 steps.

- SA-AMG with Chebyshev smoother led to non-convergence
- 2 sweeps reduce flops and communication
- Momentum solve now dominant (non set-up) computational cost
- High wall-clock due to sparse matrix initialization (local/global graphs, memory)

## Strong Scaling on NERSC-Cori

Total simulation times for 10 time steps of the V27 41 R1 500M elements



# Pressure-Poisson Solver

## Observations:

- GMRES(50) for Belos/MueLu, and GMRES(10) for Hypre–BoomerAMG.  $tol = 1e-5$
- Hypre: aggressive coarsening significantly lowers  $C$  and  $S_{avg}$ ; iterations increase
- Non-Galerkin sparsification further reduces solve and set-up times
- MueLu: unsmoothed prolongation reduce  $C$  and  $S_{avg}$

## Conclusions:

- Hypre and MueLu coarsening result in similar complexities  $C$  and solve times
- Hypre: higher computational cost per GMRES iteration
- Hypre: set-up costs increasing at higher core counts
- MueLu: higher GMRES iteration count that increases with core count
- MueLu: lower solve time with 2 smoother sweeps reduces communication

# Thank you! Questions?

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