

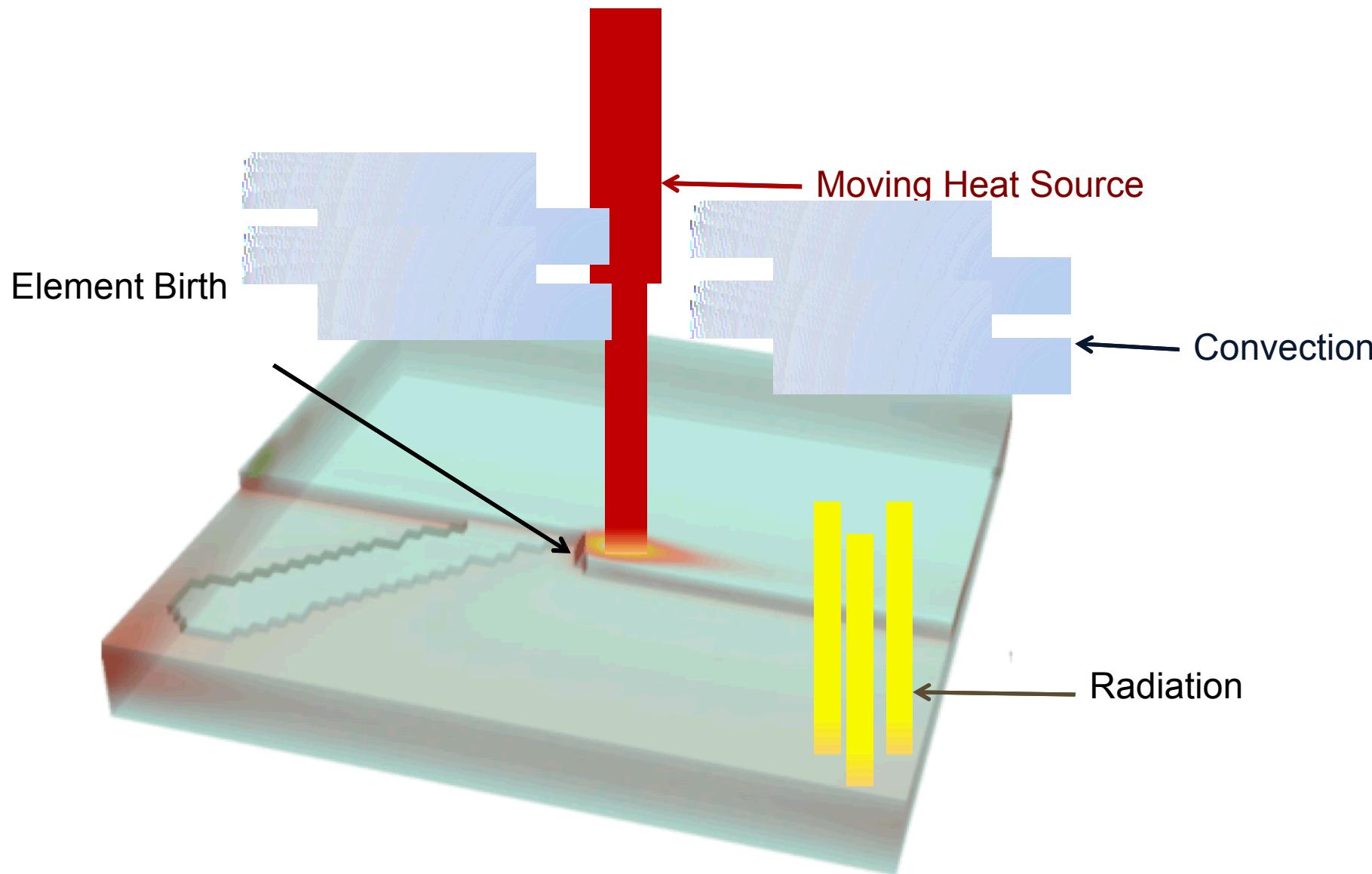
Multi Scale Solid Mechanics Models of Additive Manufacturing

Kurtis Ford, Lauren Beghini, Theron Rodgers, Joe Bishop, Kyle Johnson, Brad Trembacki



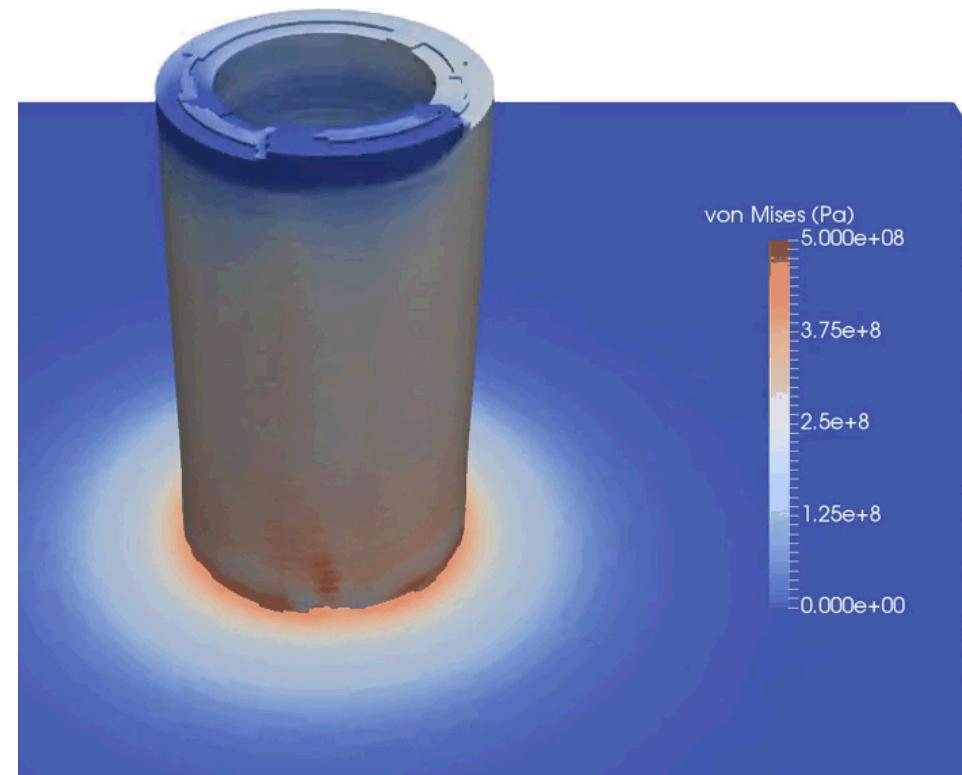
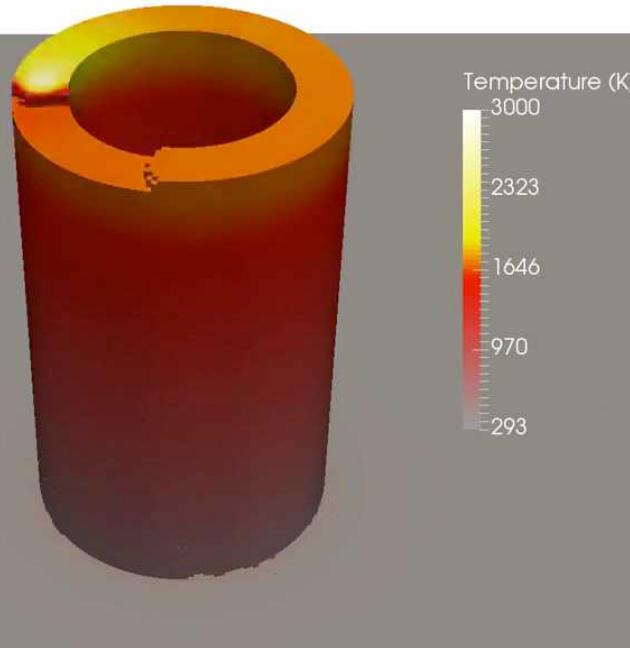
Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

Additive Process Model at Sandia

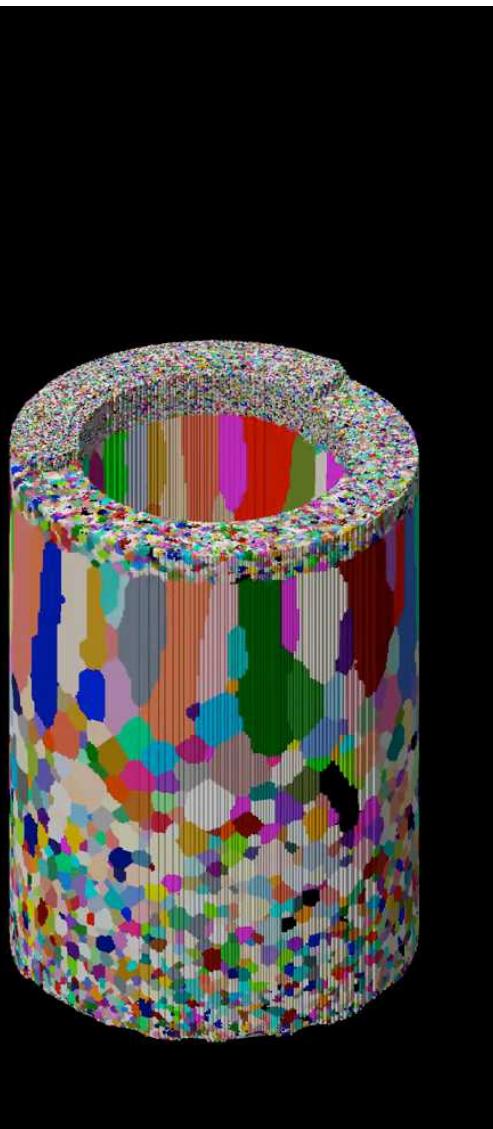


Hot Spot to Approximate Melt Pool

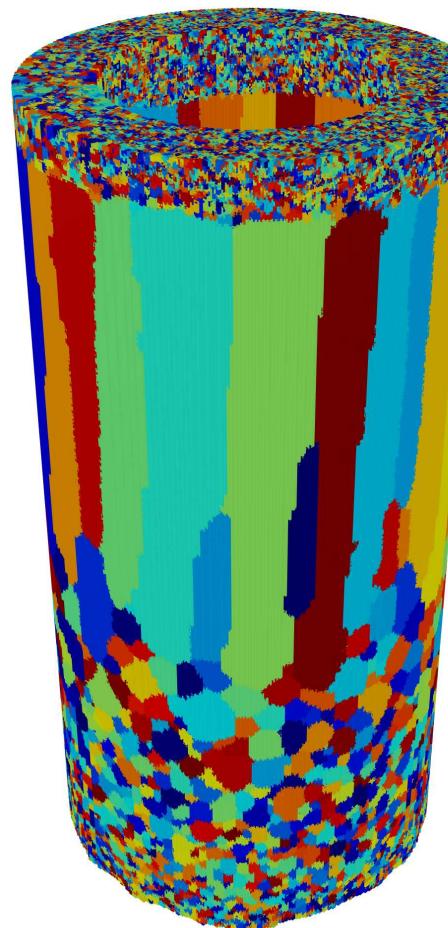
Time: 305.52 s



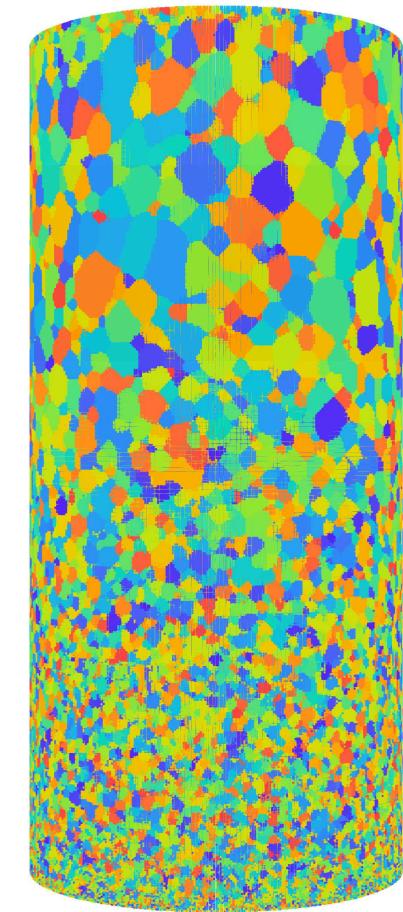
Grain Growth Predicted by Thermal History



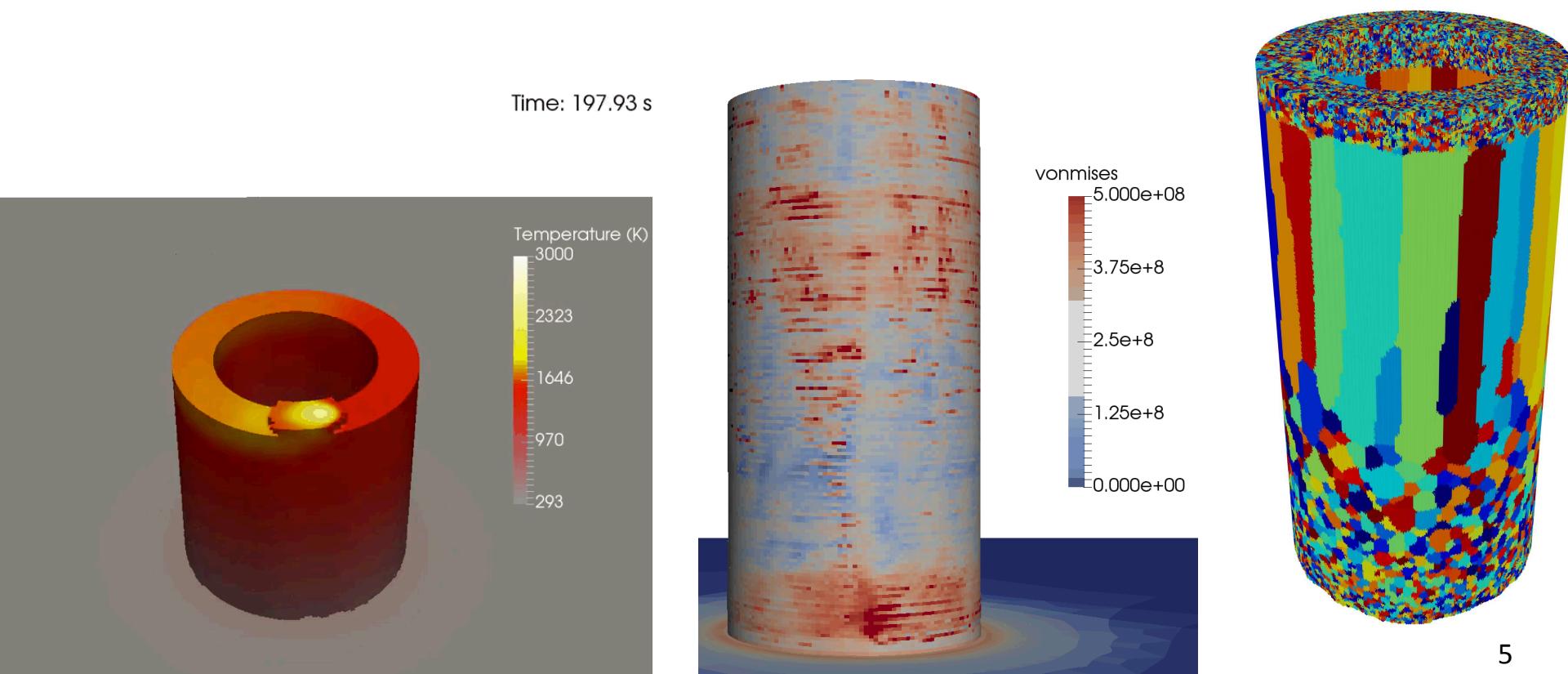
Single Build



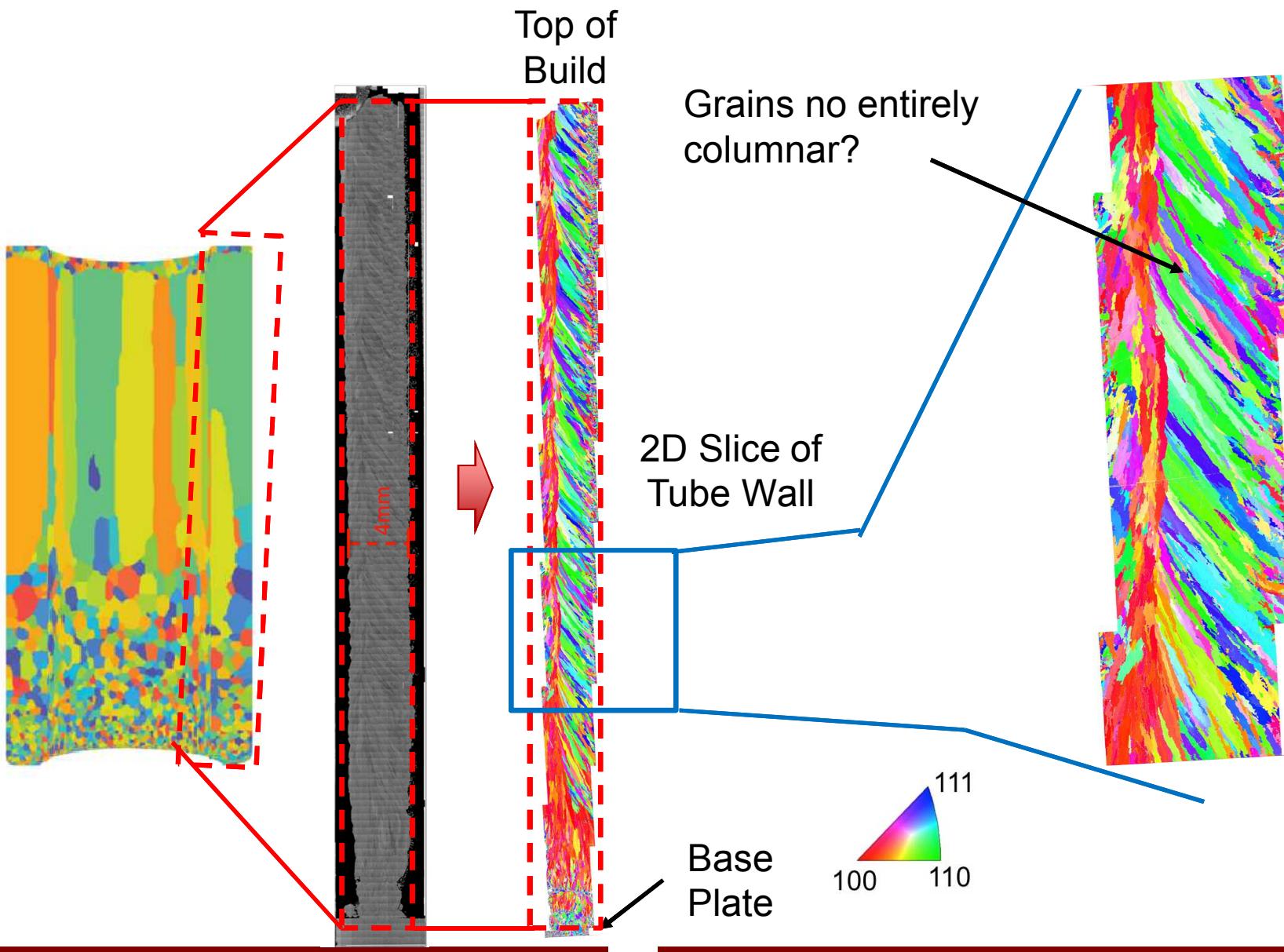
Double Build – 8 Second
Inter-layer Delay



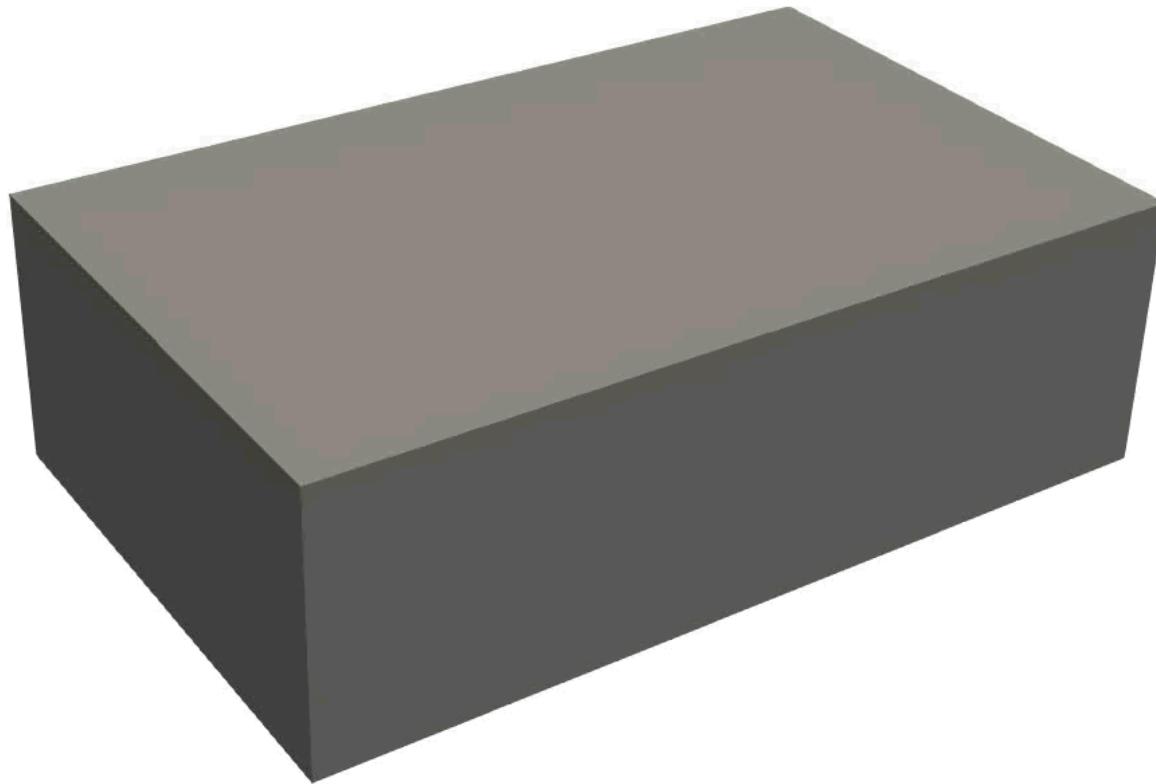
Scalable Part Scale Model



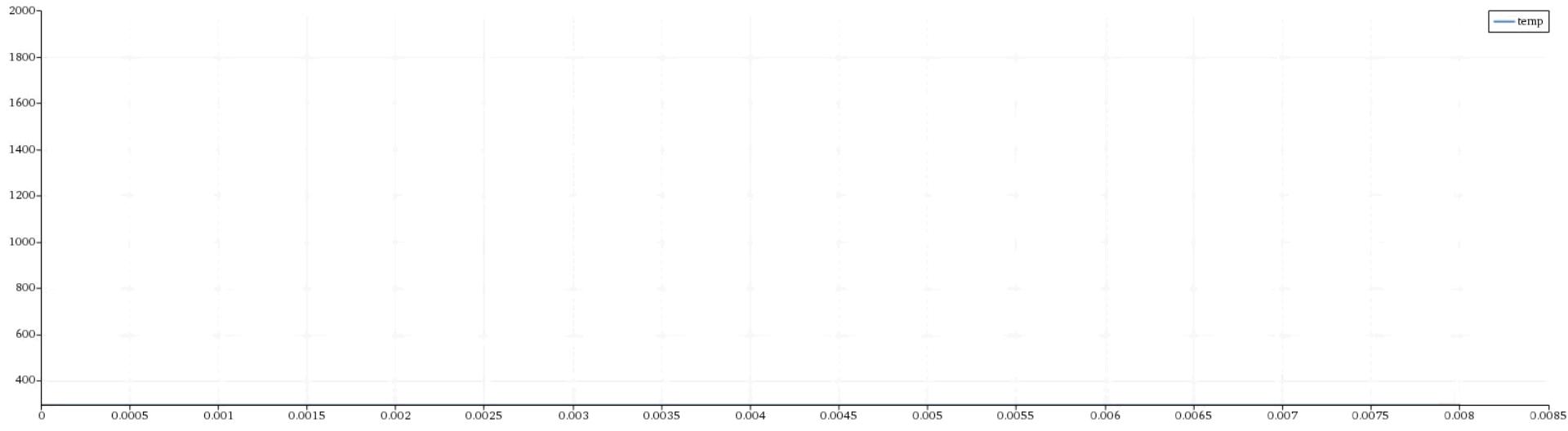
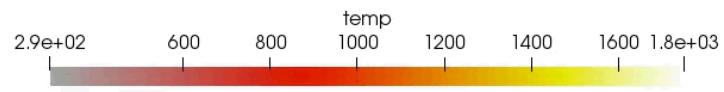
Experimental Comparison - Microstructure



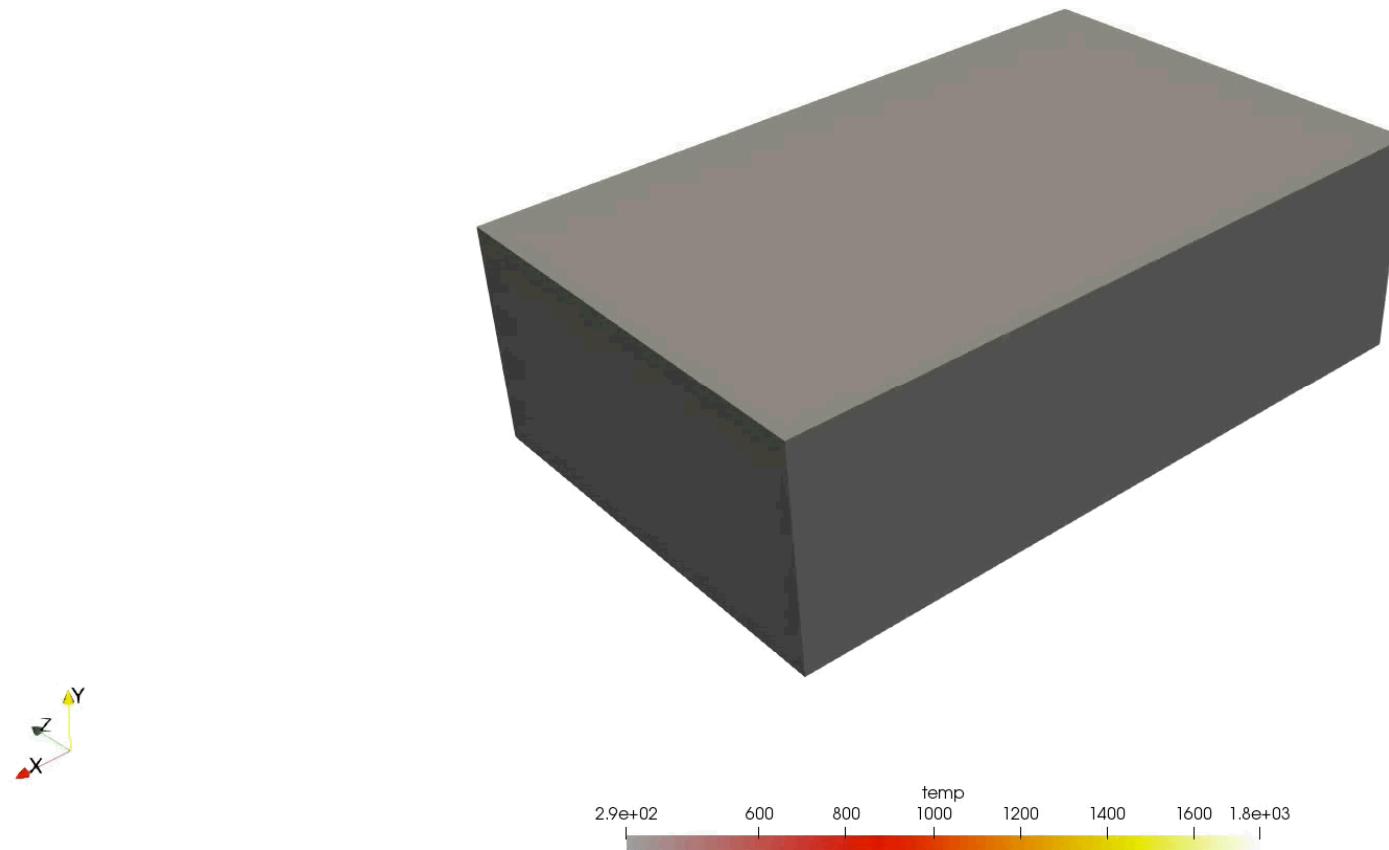
Part Scale Model of Wall

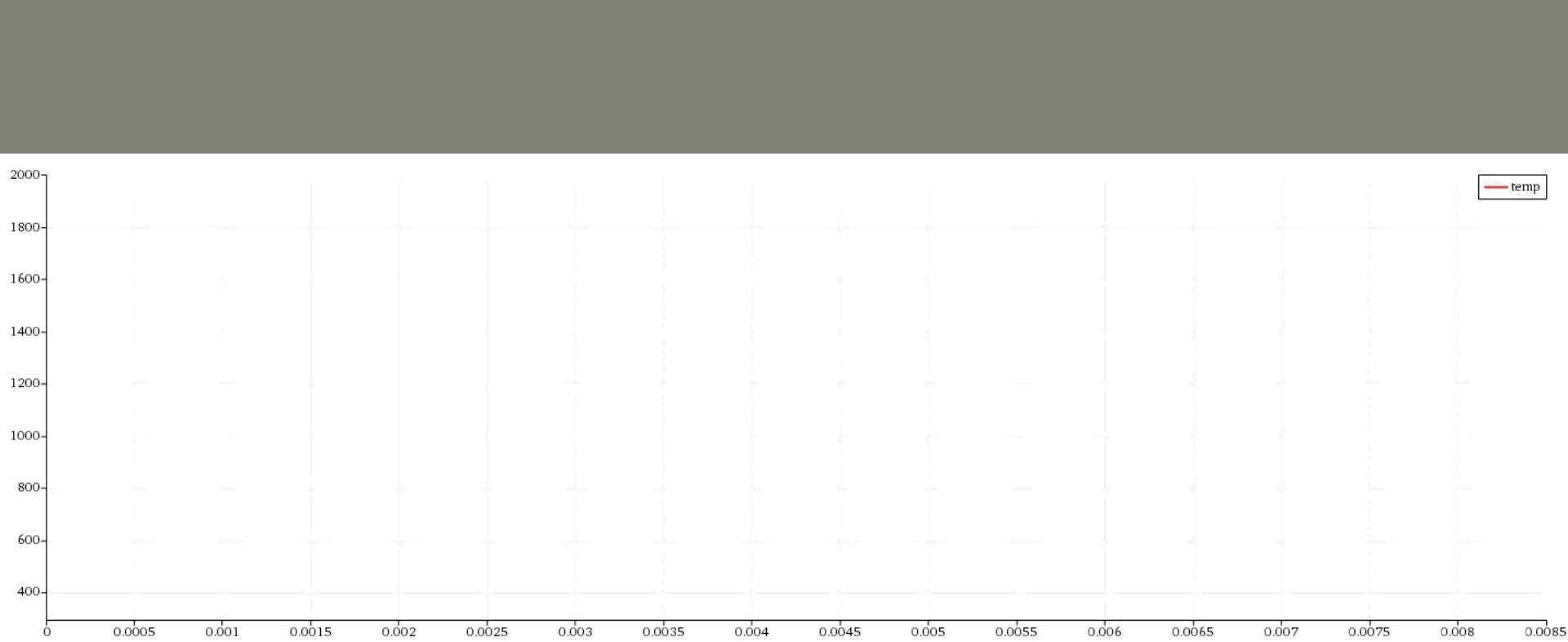
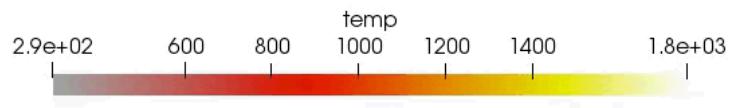


Part Scale

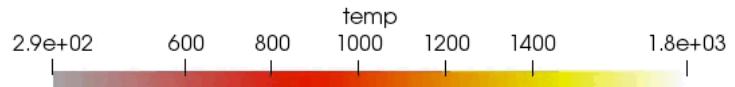
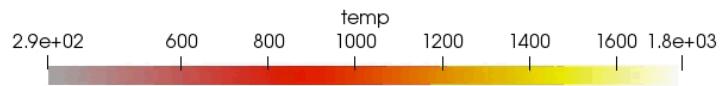


Fluid Model of Wall

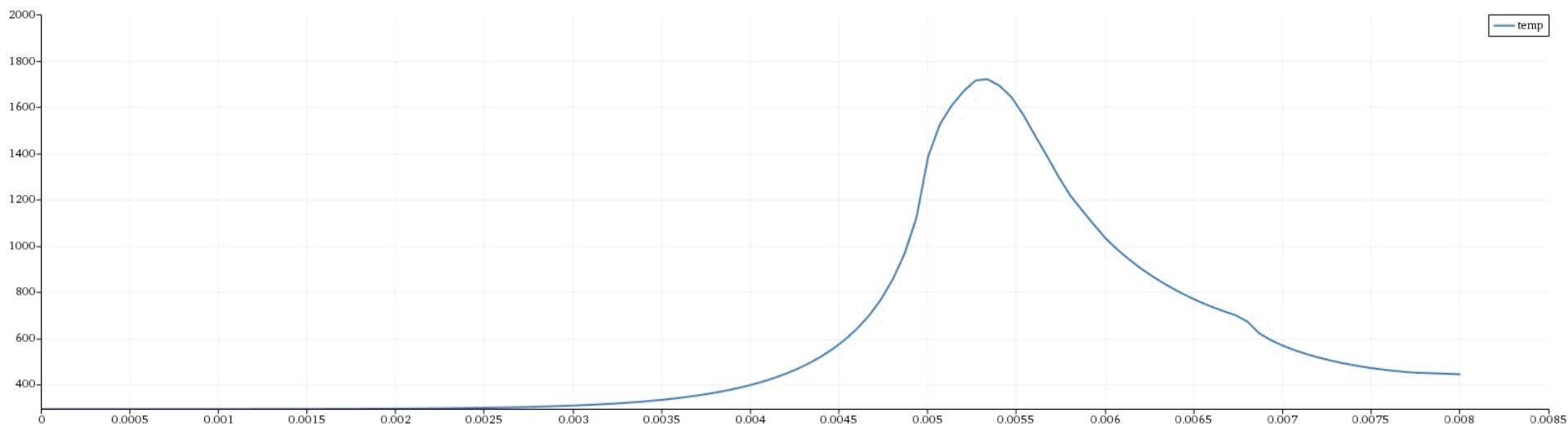
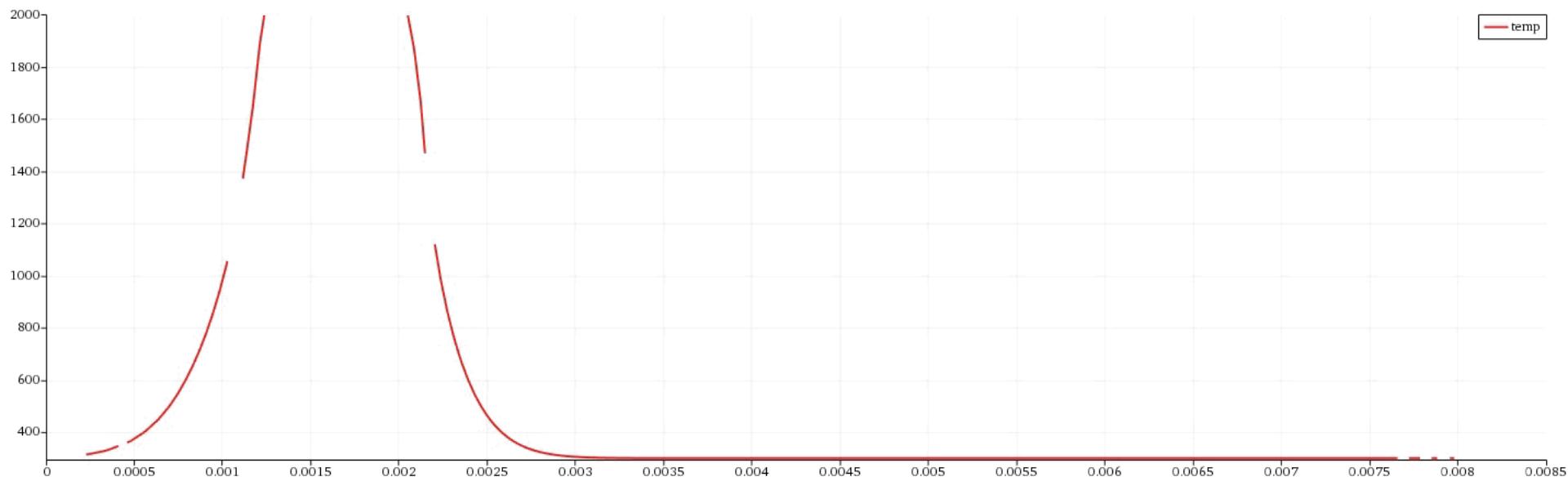




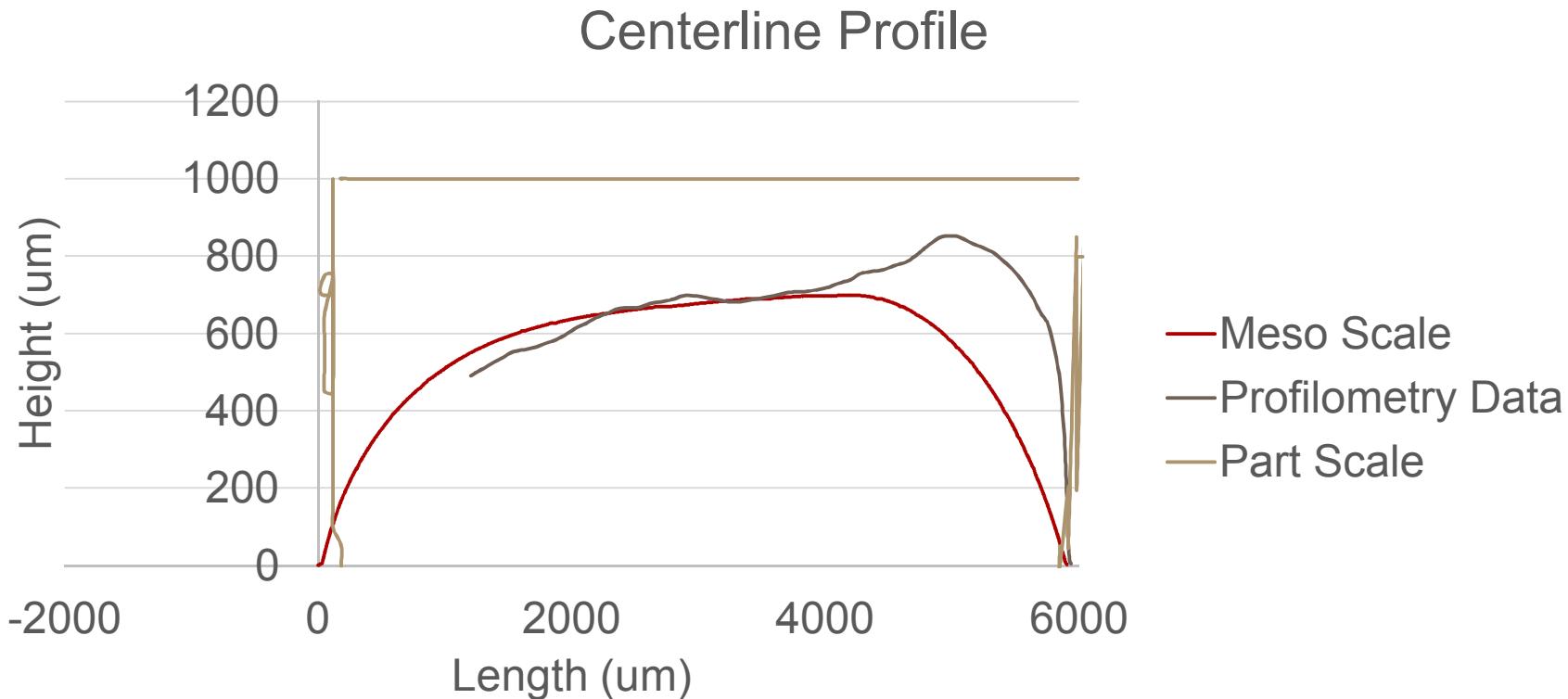
Comparison



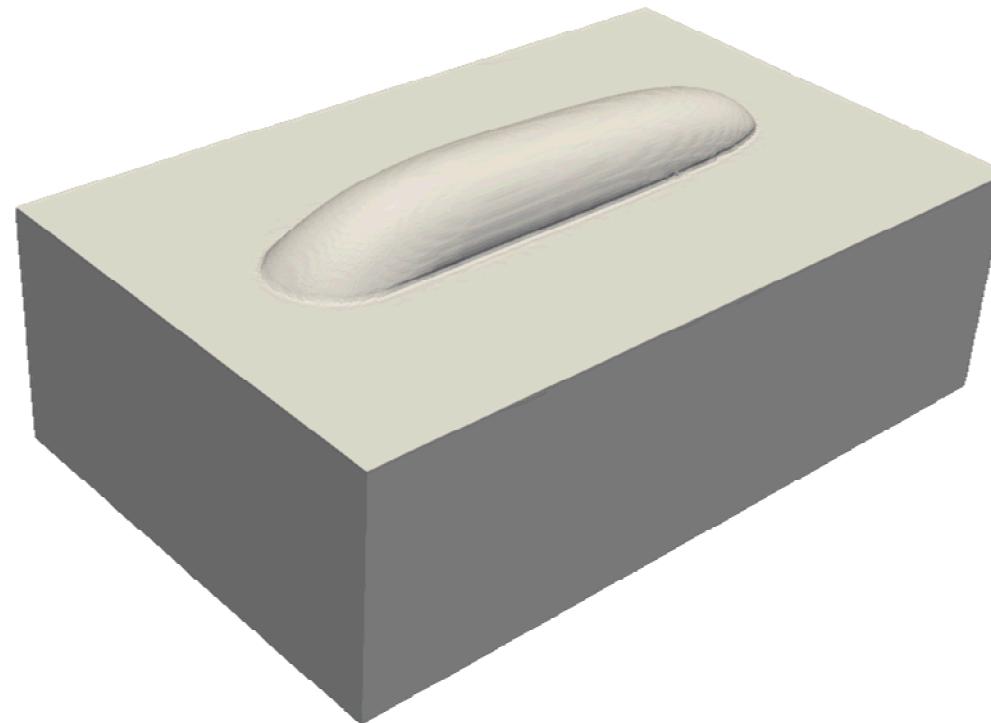
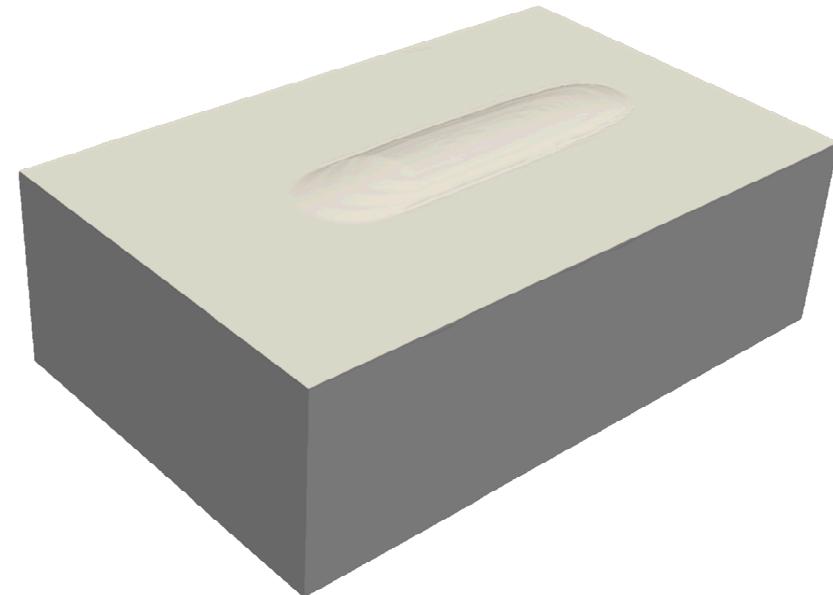
Comparison Continued



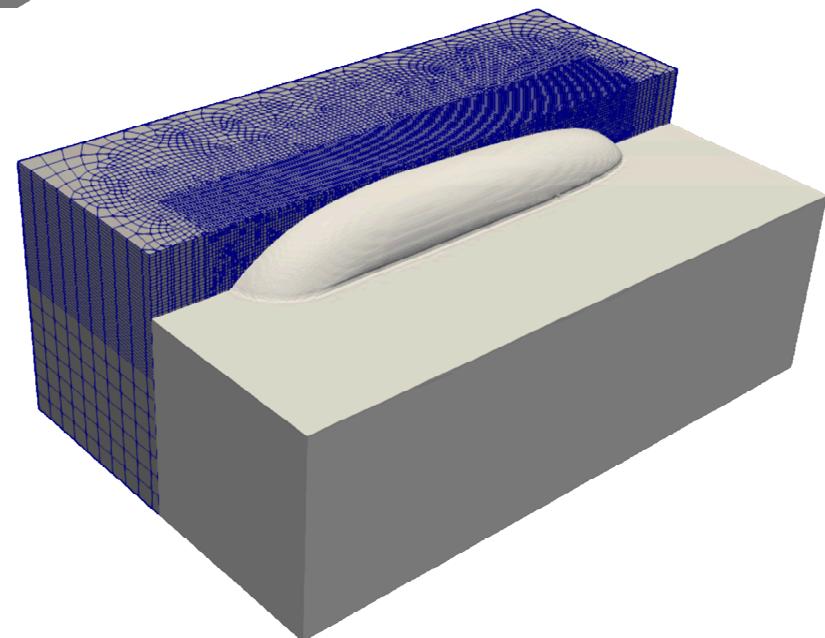
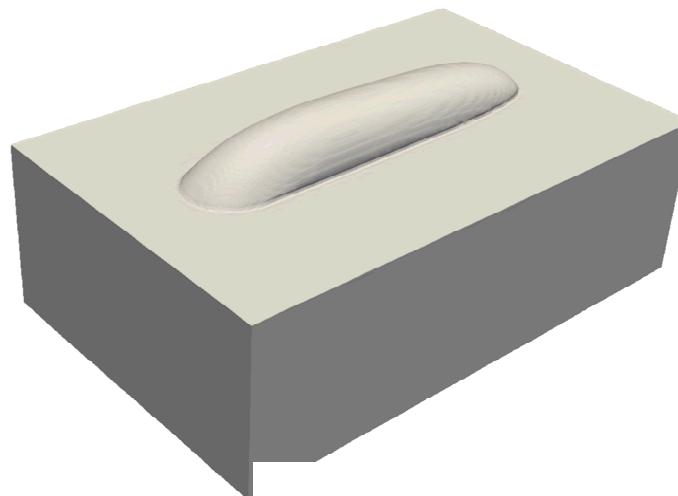
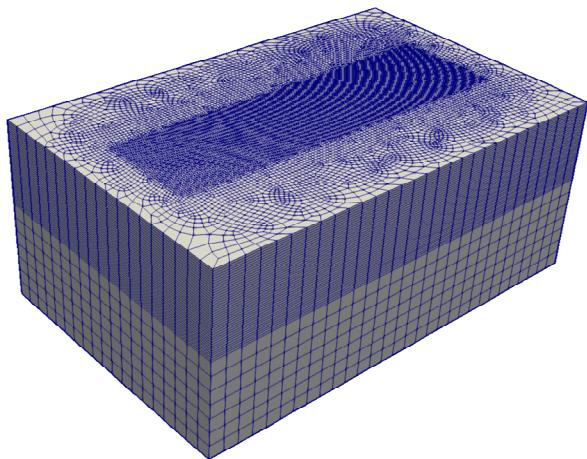
Multi Scale Model Comparsion

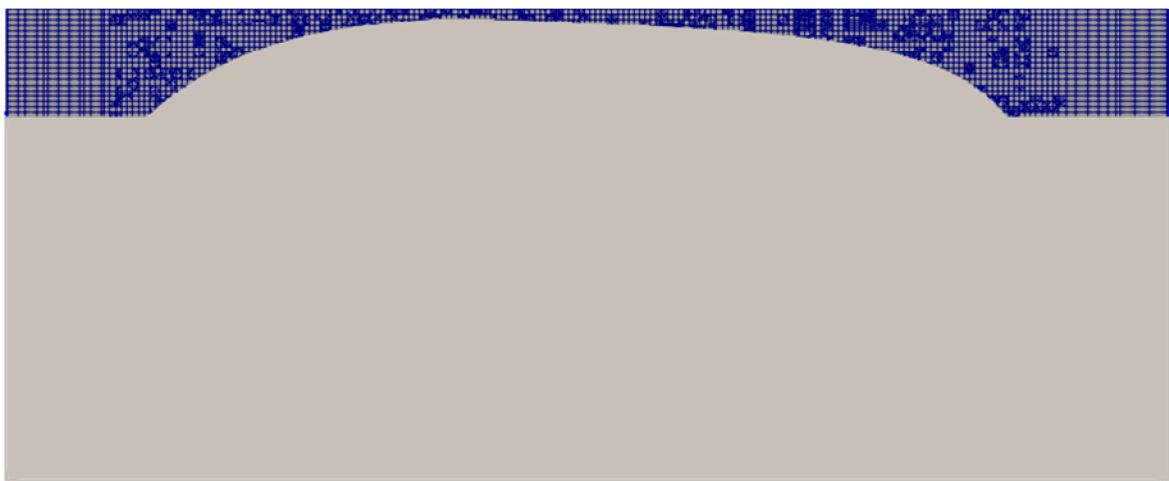
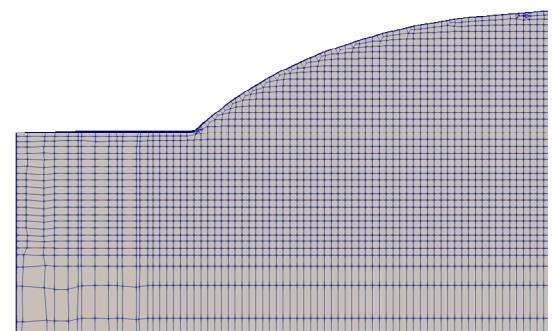
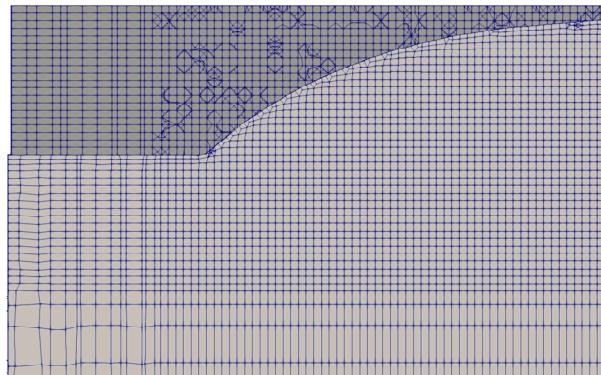
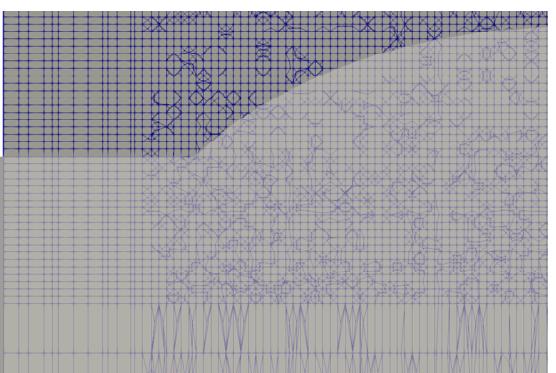
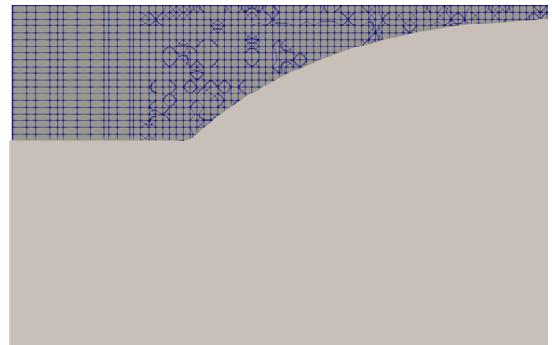


Generate STL of Evolving Geometry

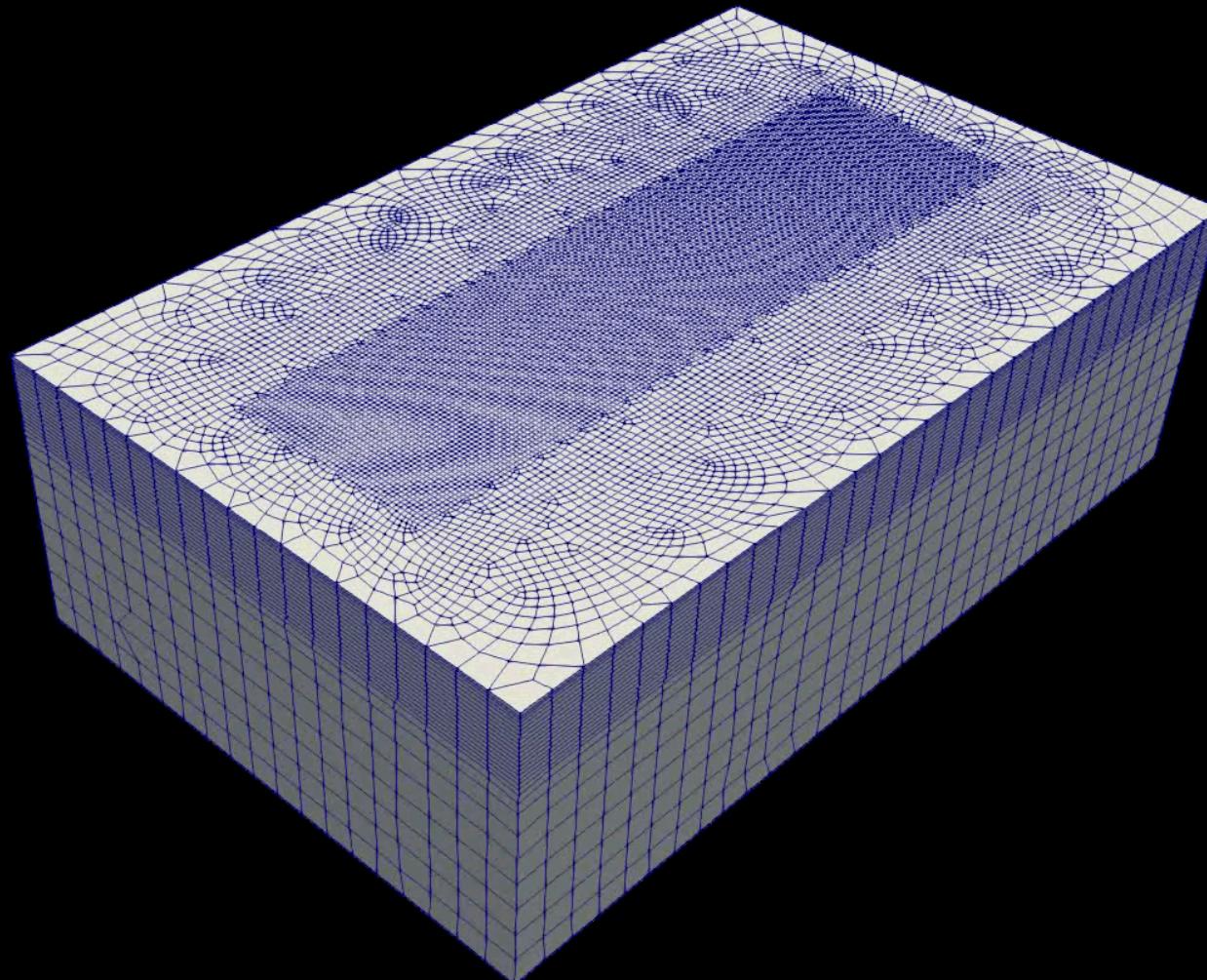


Mesh Evolving





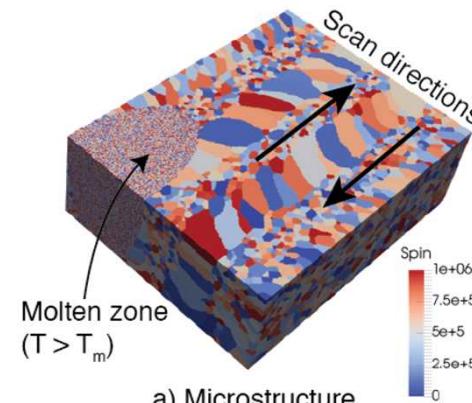
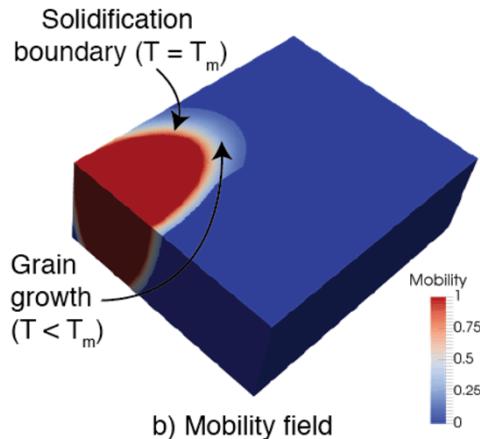
High Quality Hex Mesh



The KMC method

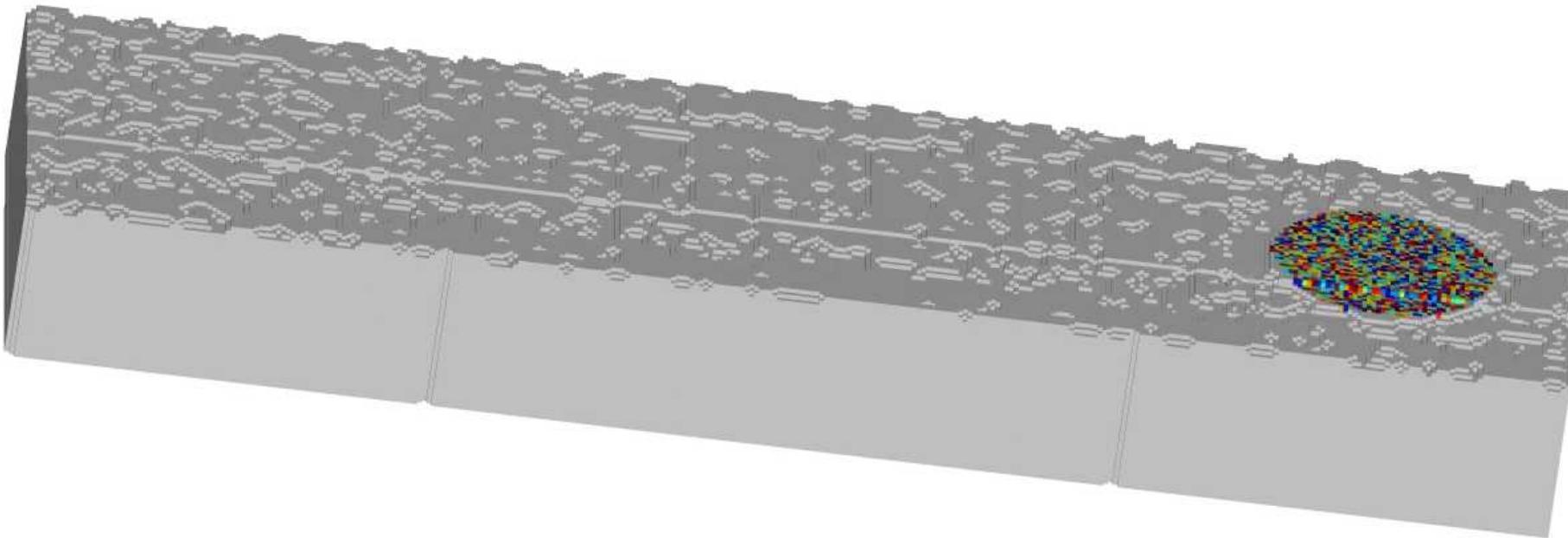
$$M(T) = M_0 \exp\left(\frac{-Q}{RT}\right)$$

$$P = \begin{cases} M(T) \exp\left(\frac{-\Delta E}{k_B T_s}\right), & \text{if } \Delta E > 0 \\ M(T), & \text{if } \Delta E \leq 0 \end{cases}$$

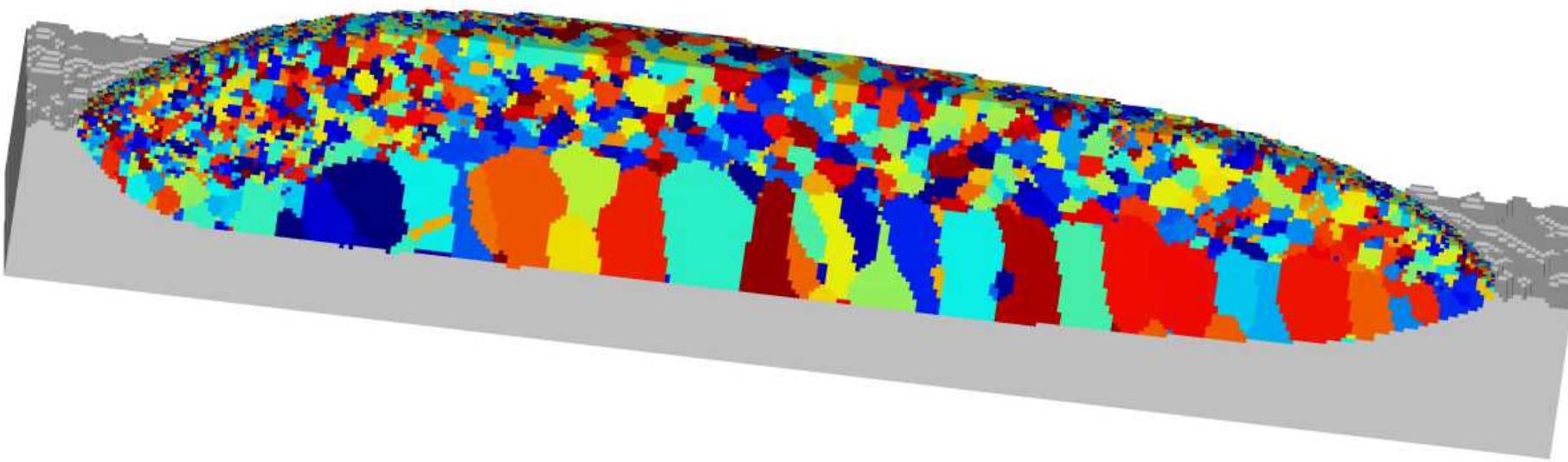


- The molten zone randomizes grain identities when it enters a region.
- Along the trailing surface, voxels either join existing columnar grains or form new grains.
- The temperature gradient creates a corresponding gradient of grain boundary mobilities via an Arrhenius relationship.

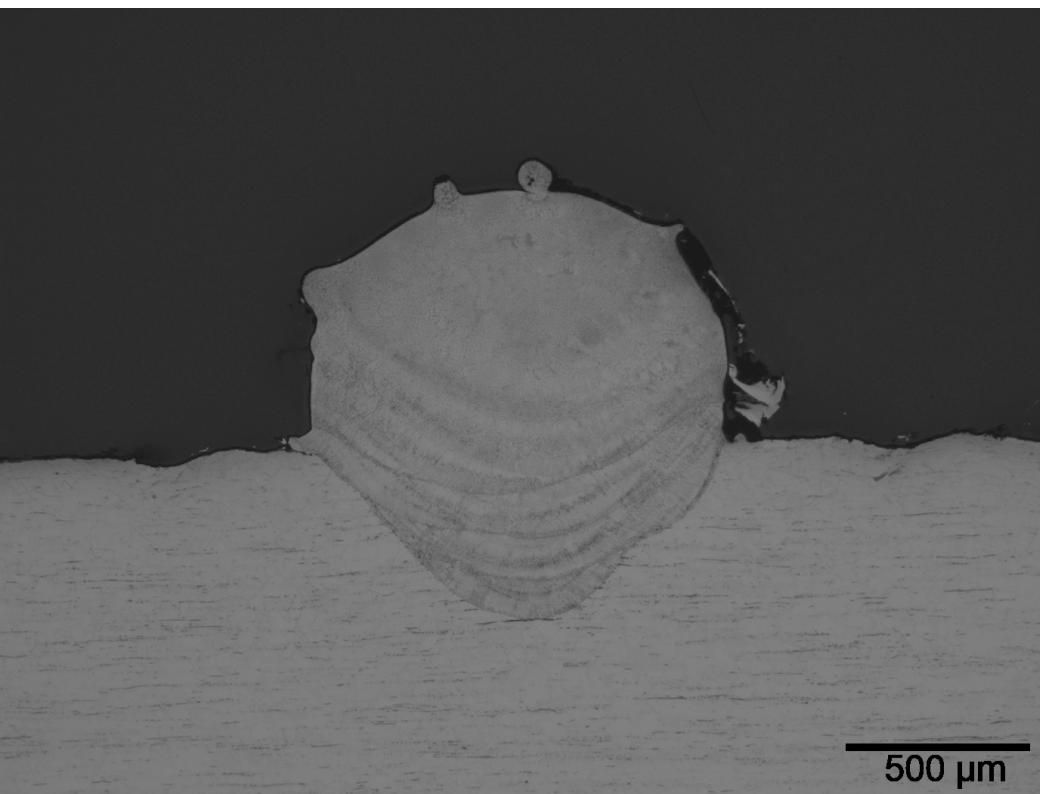
Micro Structure



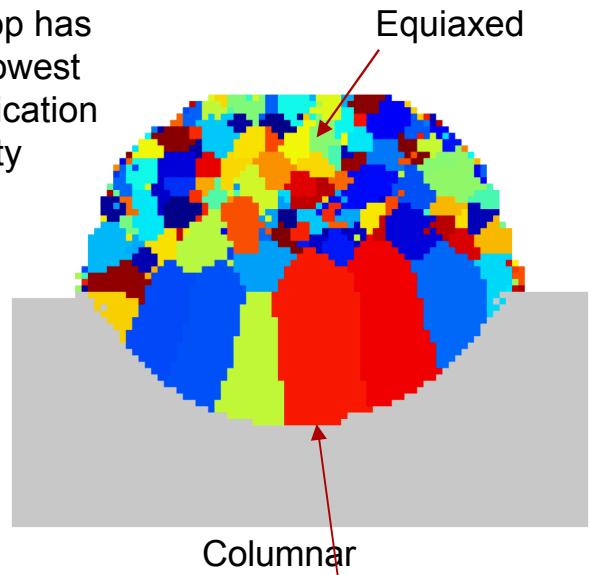
Micro Structure Cross Section



Microstructure Data Compared to Model



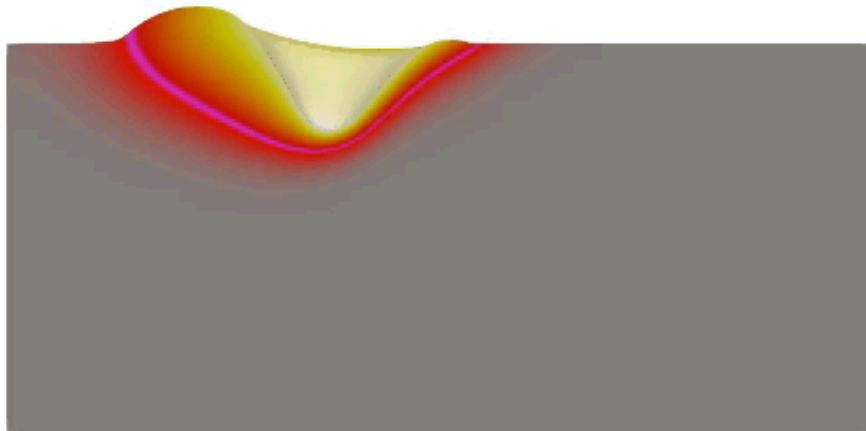
The top has
the slowest
solidification
velocity



After the first pass the grains are all equiaxed. When it gets remelted it begins to grow columnar grains because your solidification velocity higher (the boundary between the molten zone and the solid part of the material how fast that moves). The grains from the first pass seed the new growth and that causes a column. In the previously melted stuff there are nucleation sites.

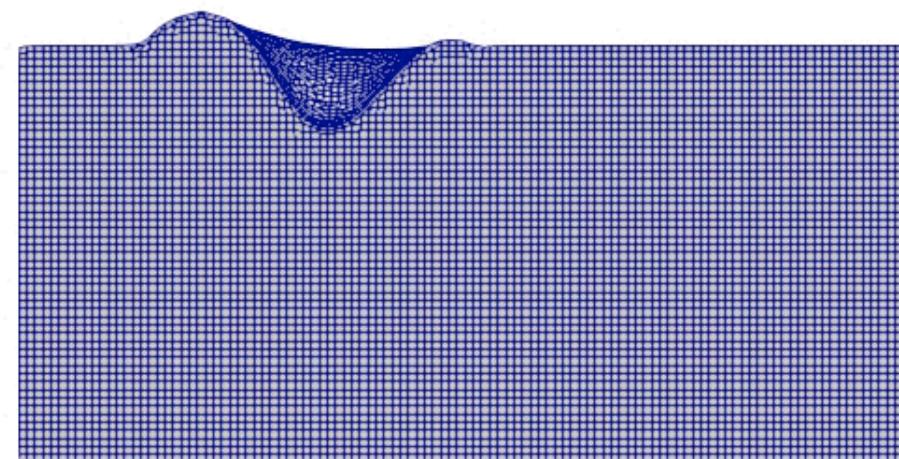
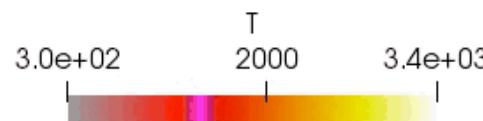
Every grain has a spin that is randomly assigned in the molten pool. At the solid liquid interface the spins are adjusted to minimize surface energy of the grain they are a part of. According to the Potts Monte Carlo Method. Spin refers to an arbitrary energy defined between each representative volume. The energy is based on how the local representative volumes compare to one another. In the pool the energy can be anything from 0 to 1e5. Which suggests that there are 1e5 unique nucleation grains. The number or spin is an identifier or a grain i.d. It's more energetically favorable to have common neighbors because your potential energy is minimized. The potential energy is normalized.

Solid mechanics Couple

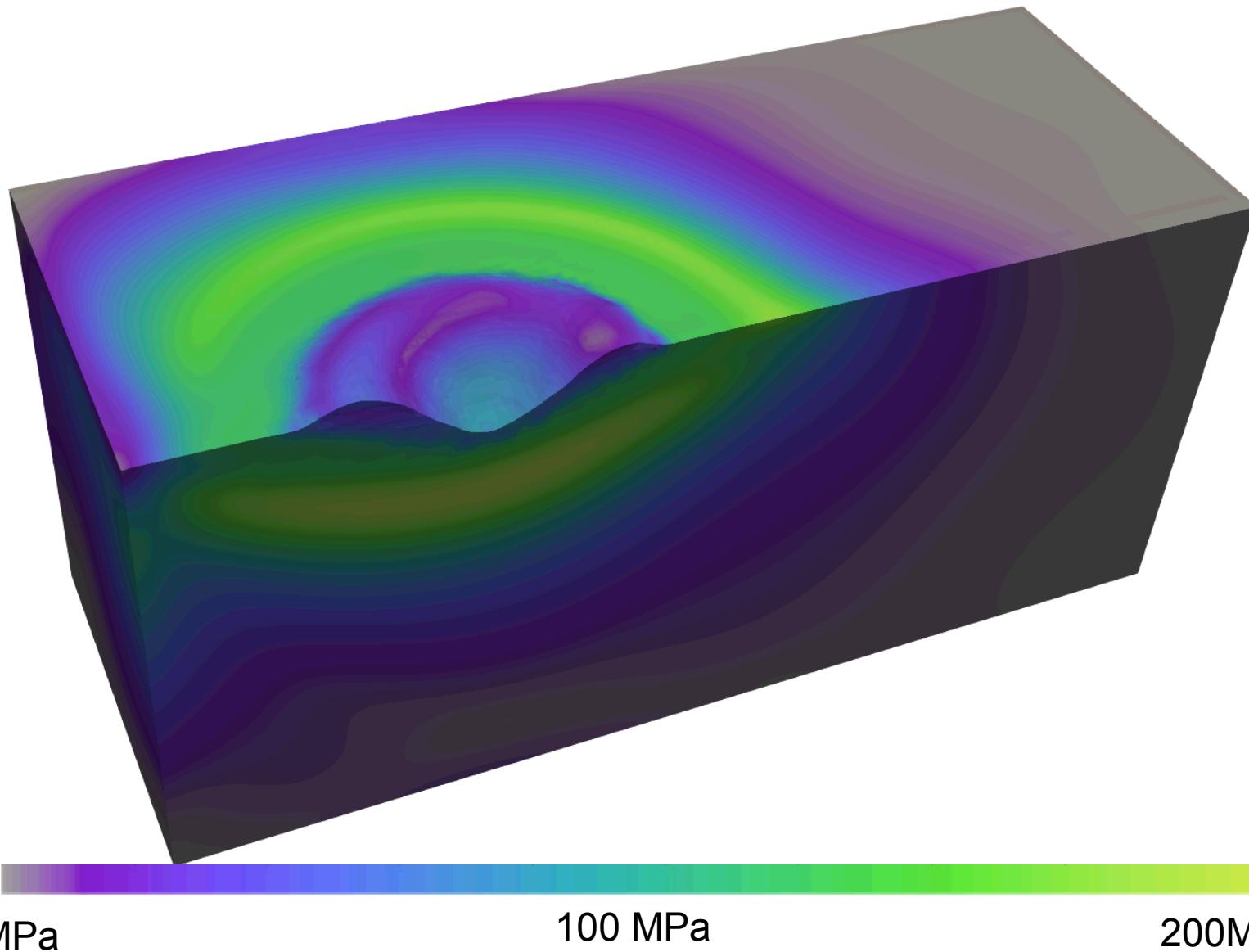


Map Temperature History to conformal
mesh of CDFEM geometry

Drastically reduce stiffness of “melted
Elements



Process Stress Predicted by Model



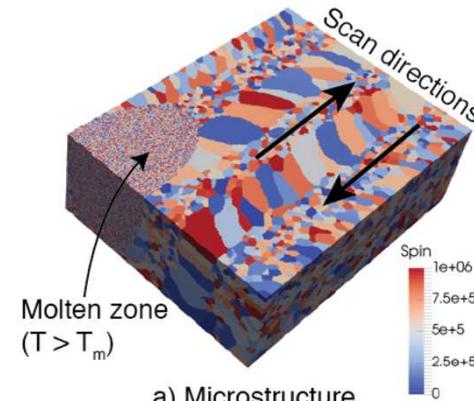
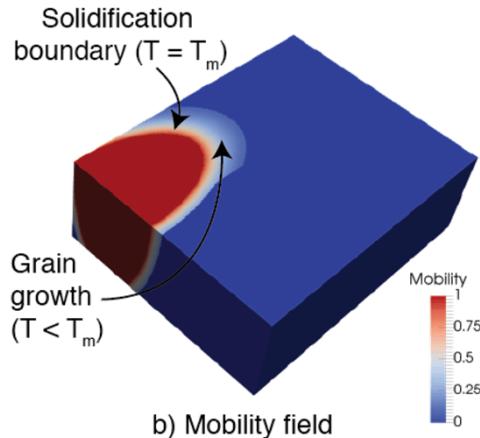
Conclusion

- Neglecting fluid mechanics leads to incorrect morphology
- CDFEM mesh can be converted to a Hex mesh using sculpt
- Mapped temperature history has been used to generate a microstructure that compares well with experimental measurements
- Temperature histories can be used to map a residual stress

The KMC method

$$M(T) = M_0 \exp\left(\frac{-Q}{RT}\right)$$

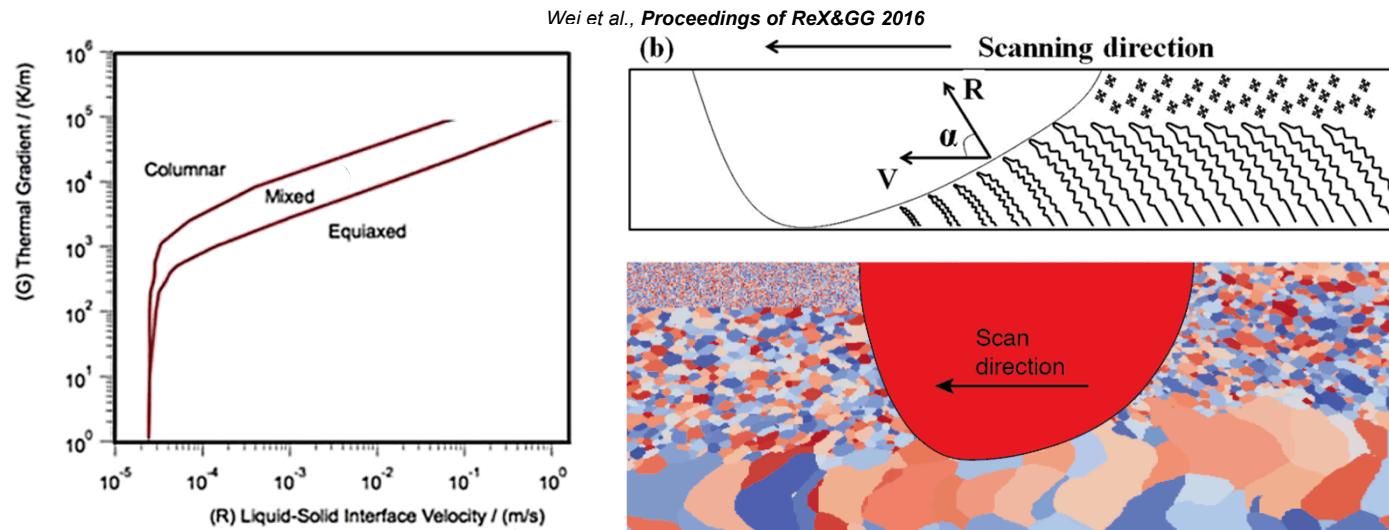
$$P = \begin{cases} M(T) \exp\left(\frac{-\Delta E}{k_B T_s}\right), & \text{if } \Delta E > 0 \\ M(T), & \text{if } \Delta E \leq 0 \end{cases}$$



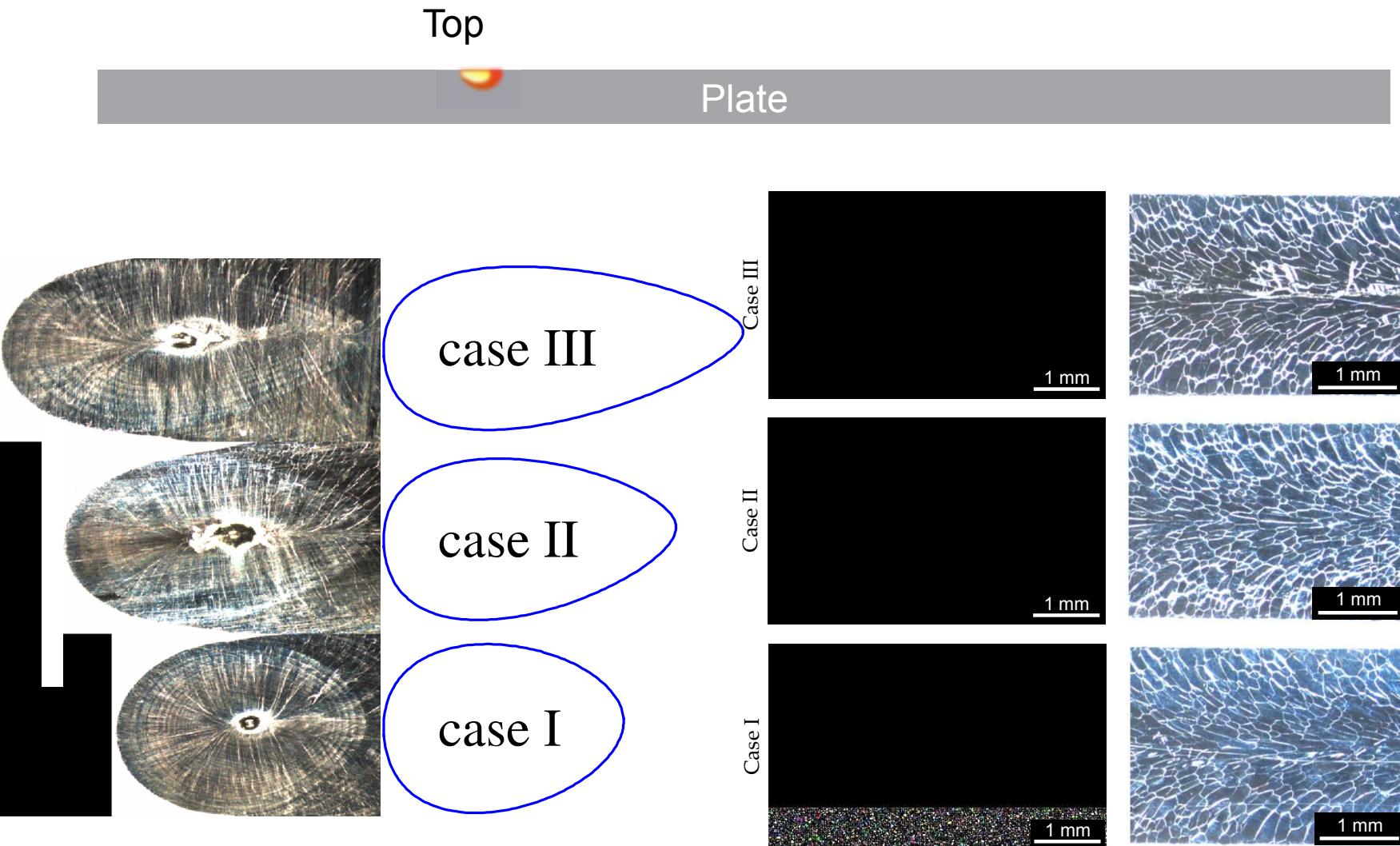
- The molten zone randomizes grain identities when it enters a region.
- Along the trailing surface, voxels either join existing columnar grains or form new grains.
- The temperature gradient creates a corresponding gradient of grain boundary mobilities via an Arrhenius relationship.

Columnar vs equiaxed microstructures

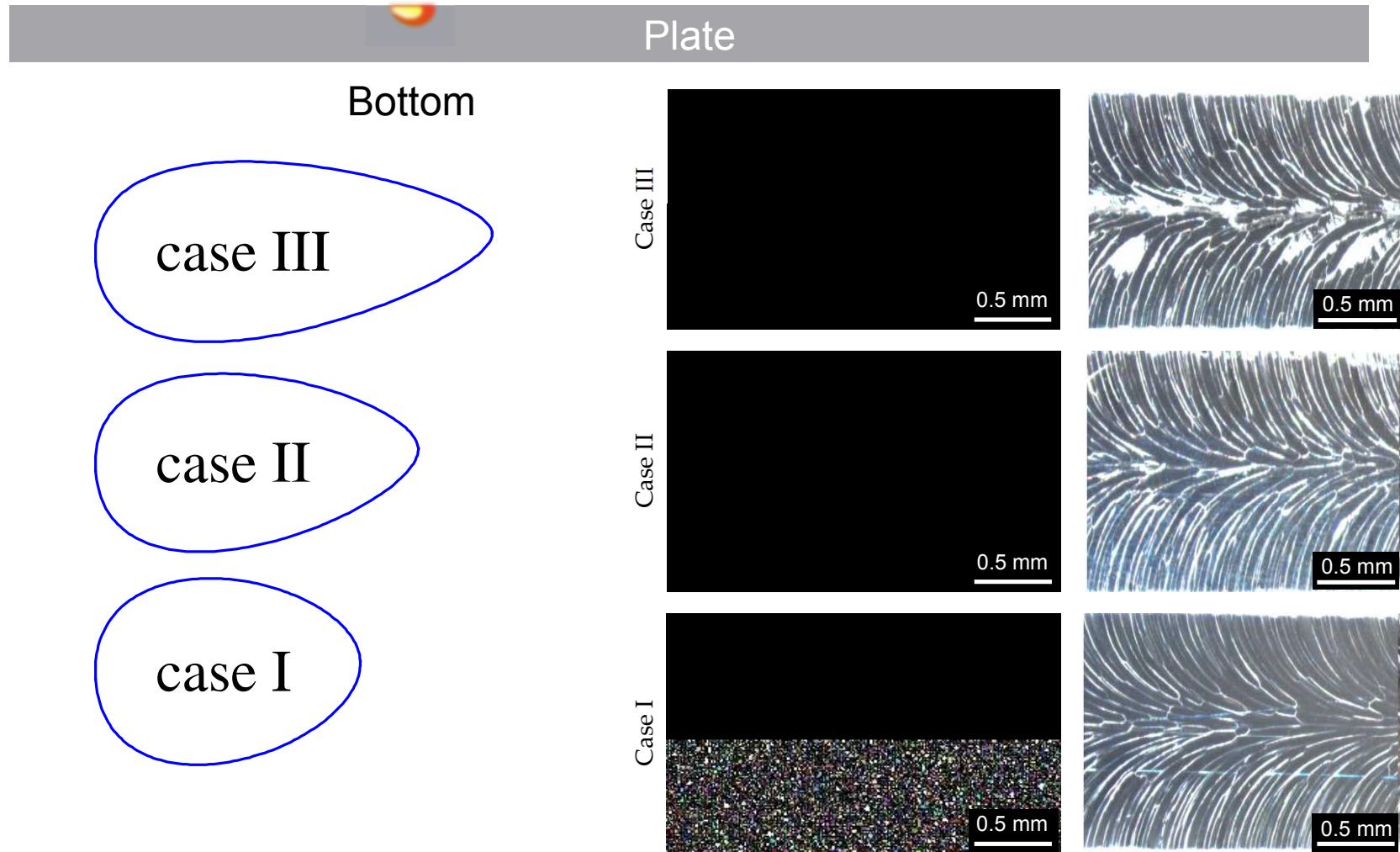
- Solidification grain morphology can be predicted through the ratio of temperature gradient (G) and solidification front velocity (R).
- For many melt pool geometries, G is smaller at the top (where curvature is lowest) and larger at the bottom. Resulting in smaller, equiaxed grains at the top and larger, columnar grains at the bottom.



Grain Shape Sensitivity to Melt Pool

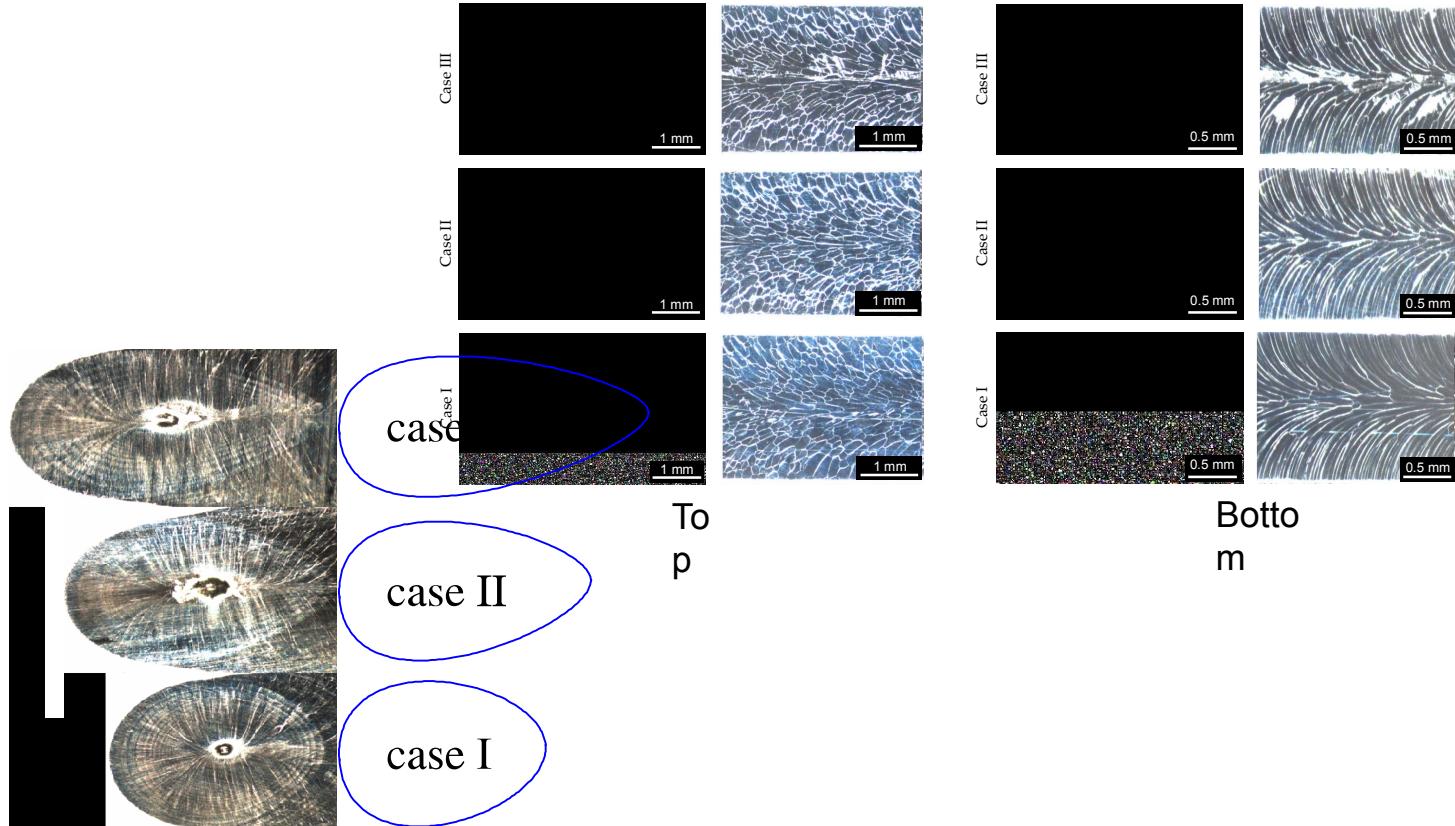


Grain Shape Sensitivity to Melt Pool

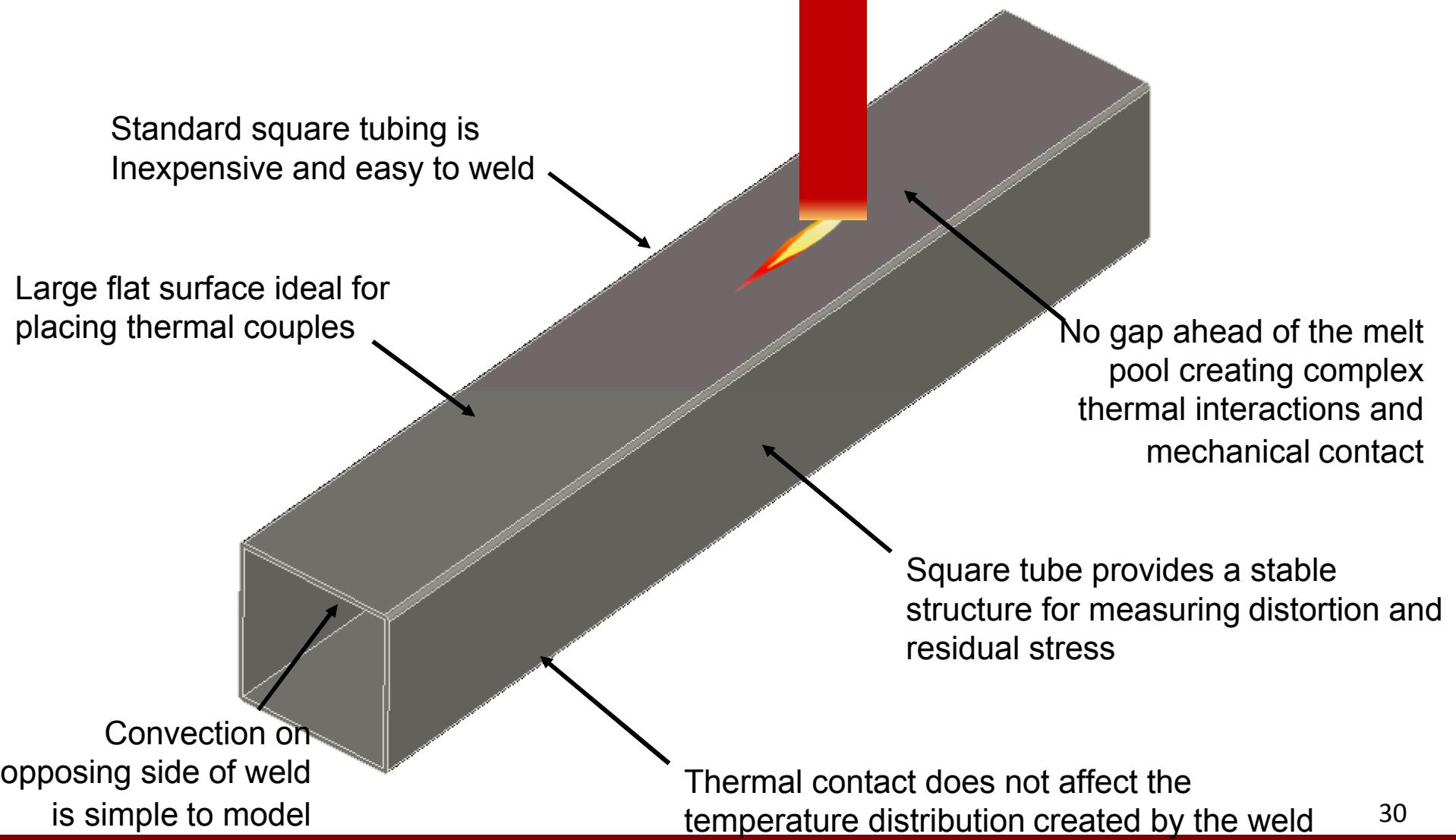


Application to welding

Rodgers et al., MSMSE 2017

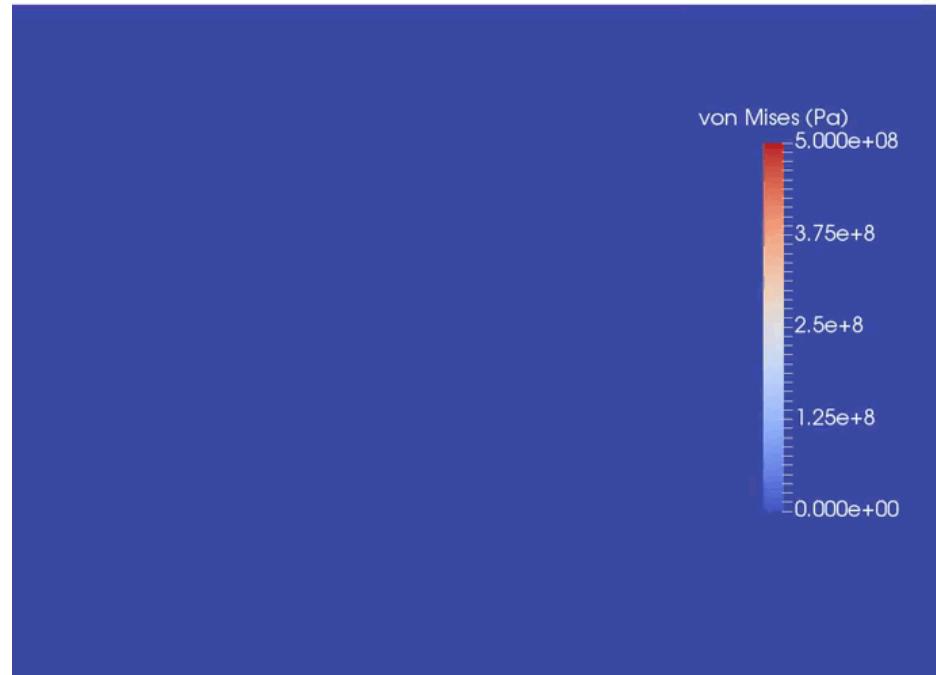
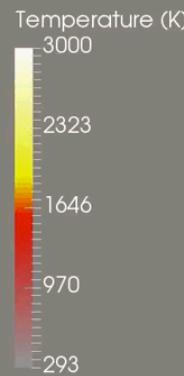


New Test: Weld Bead on a Tube



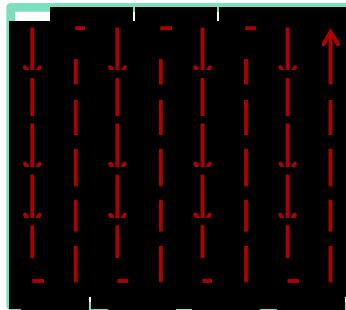
Hot Spot to Approximate Melt Pool

Time: 0.00 s



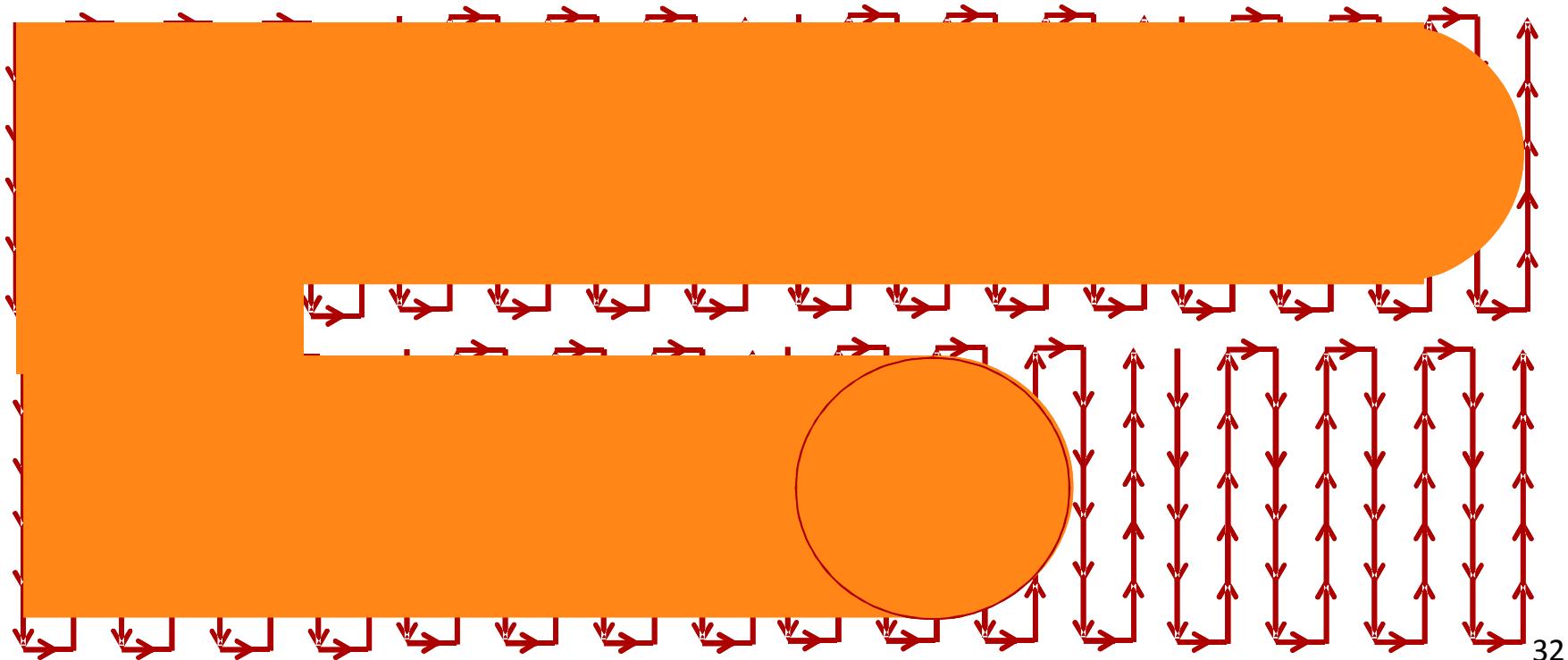
Hot Spot to Approximate Raster Pattern

Raster “Island”

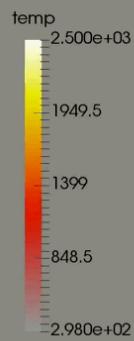
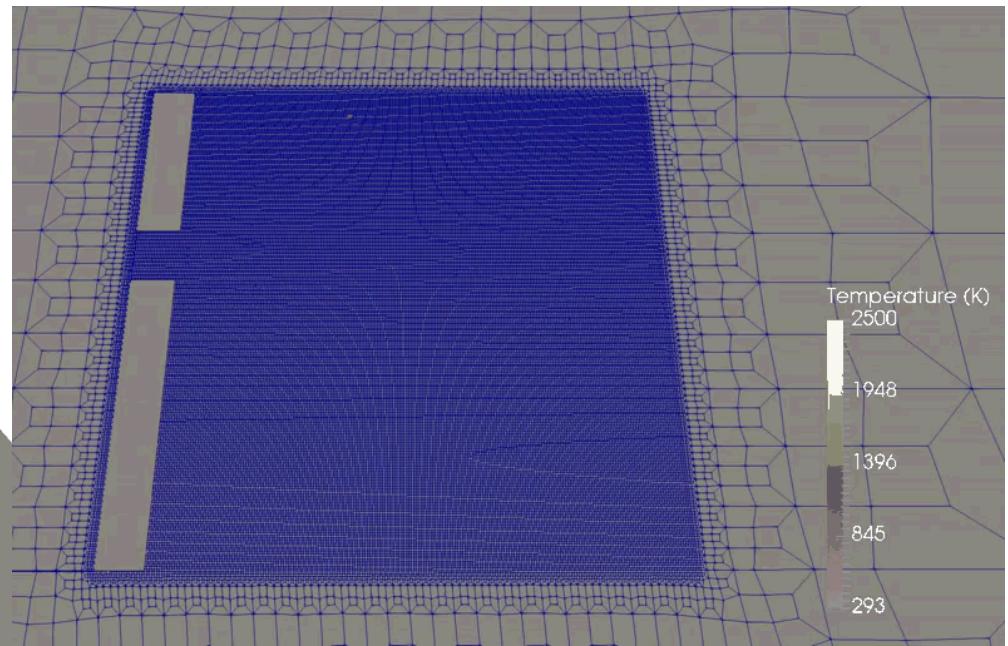
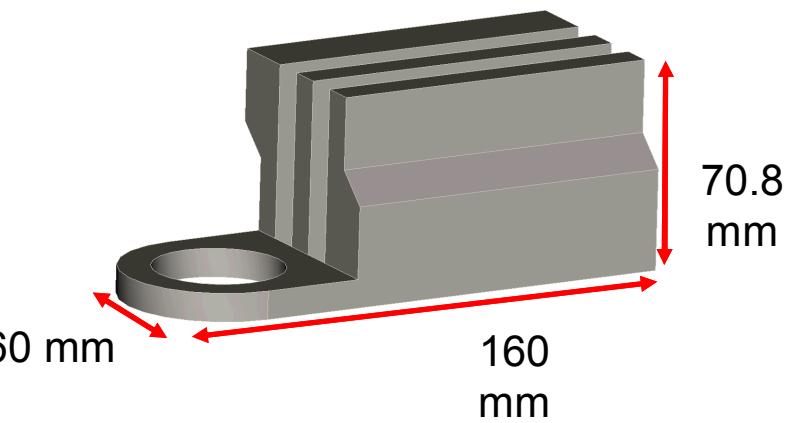


H

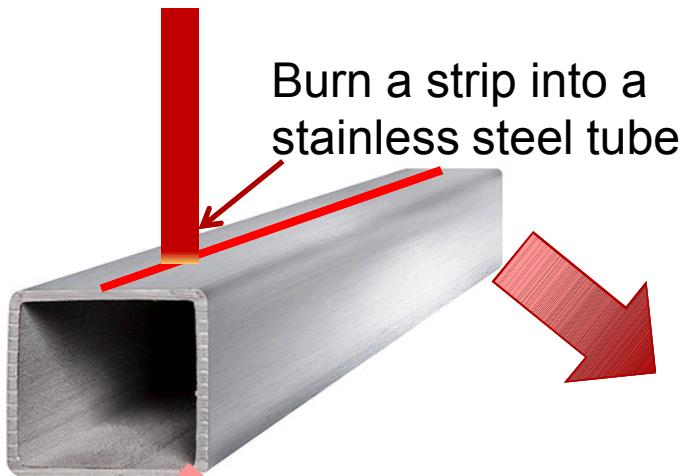
Averaged
Hot Spot



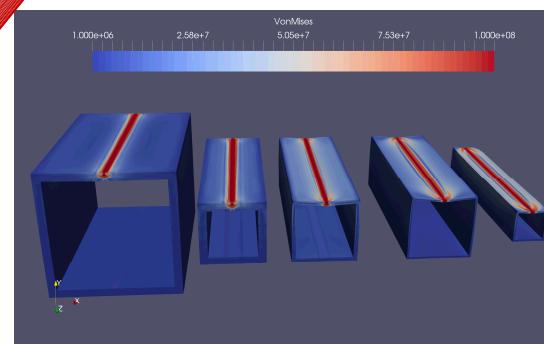
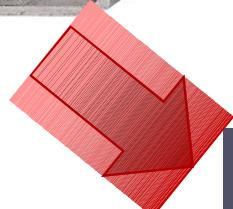
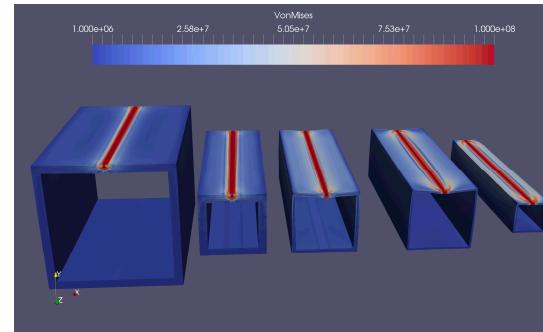
Hot Spot to Approximate Raster Pattern



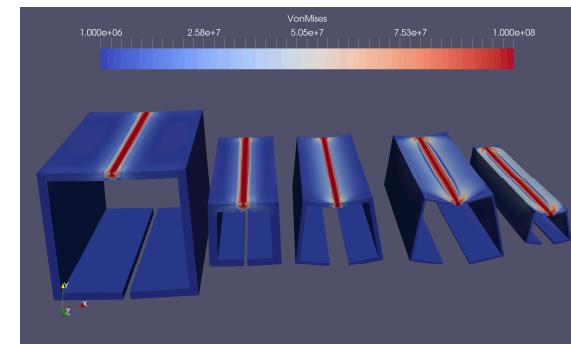
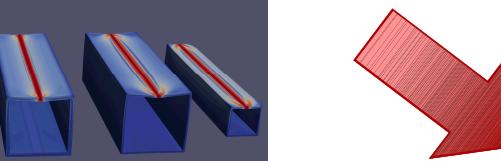
Model a Bead with Both Methods



Model Stress of Bead
with a part solid
thermal model



Model Stress of Bead
with a meso scale
fluid model



Measure Stress
Experimentally

Additional Physics in Meso Scale Fluid Model

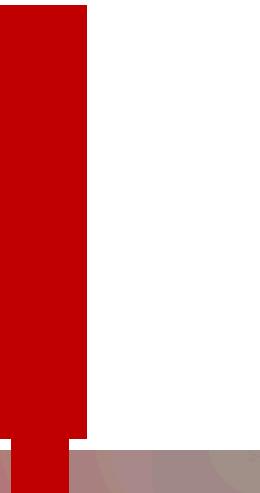
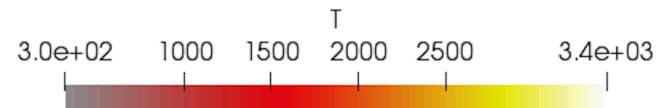
Hot Spot Equivalent to Laser Spot



Detailed Morphology
Prediction via CDFEM



Temperature Dependent
Fluid Capillary Effects
Included



Localized Heating
of Air

Depth Dependent Laser
Absorption. (Allows Key Holing)

Additional Physics in Meso Scale Fluid

Model Continued

- The entire metal medium is treated as a incompressible liquid:

Continuity:

$$\nabla \cdot v = 0$$

Momentum:

$$\rho \frac{\partial v}{\partial t} + \rho v \cdot \nabla v = \nabla \cdot \sigma + f$$

Energy:

$$\rho C_p \frac{\partial T}{\partial t} + \rho C_p v \cdot \nabla T = \nabla \cdot (\kappa \nabla T) +$$

H_v

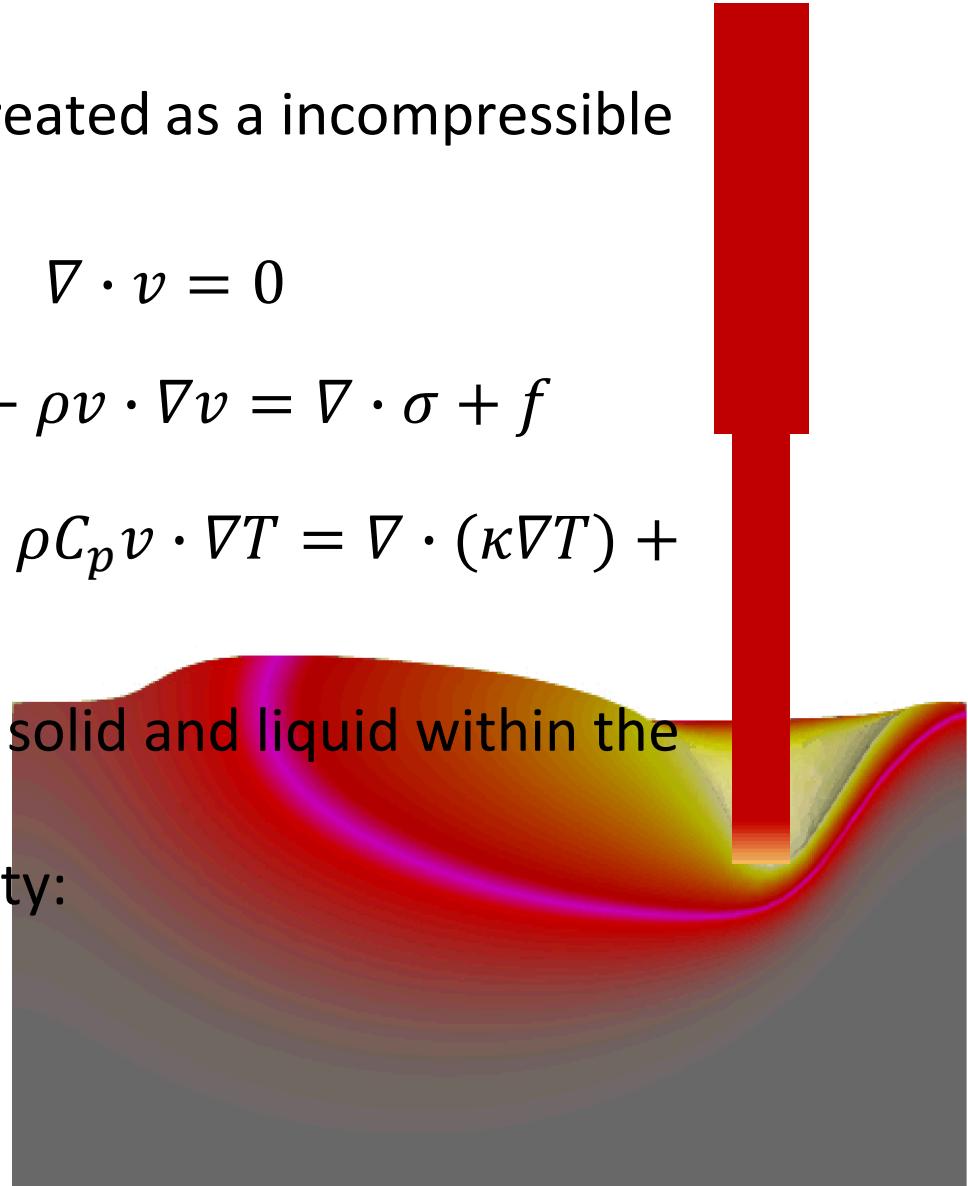
- Phase transition between the solid and liquid within the metal

is handled through the viscosity:

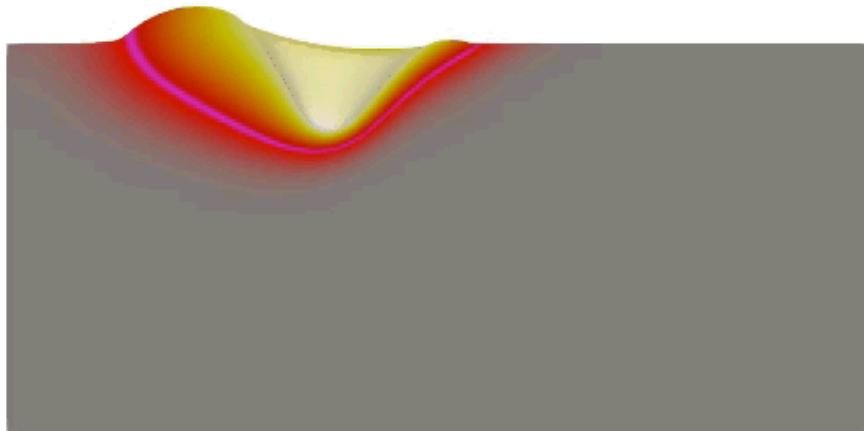
Solid Liquid phase transition

created Sudden Increase in

Viscosity at Melt Temperature

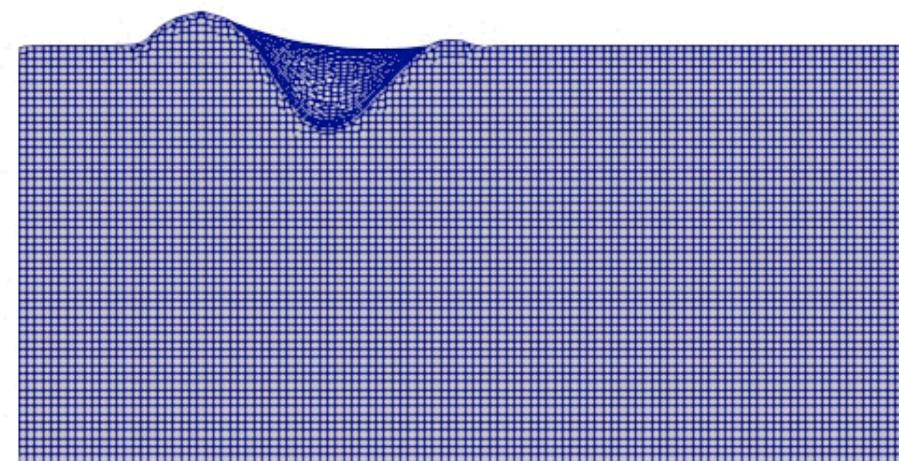
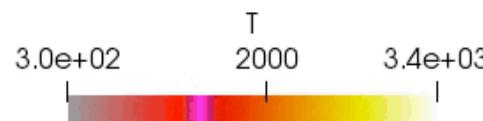


Solid mechanics Couple

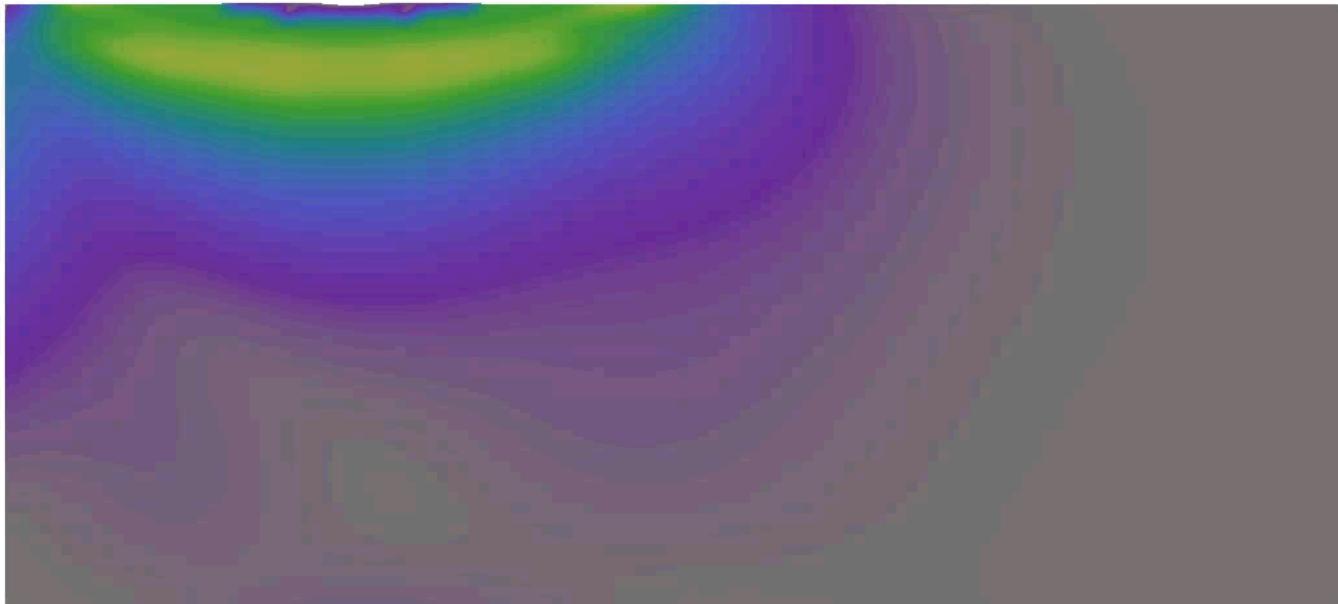


Map Temperature History to conformal mesh of CDFEM geometry

Drastically reduce stiffness of “melted Elements

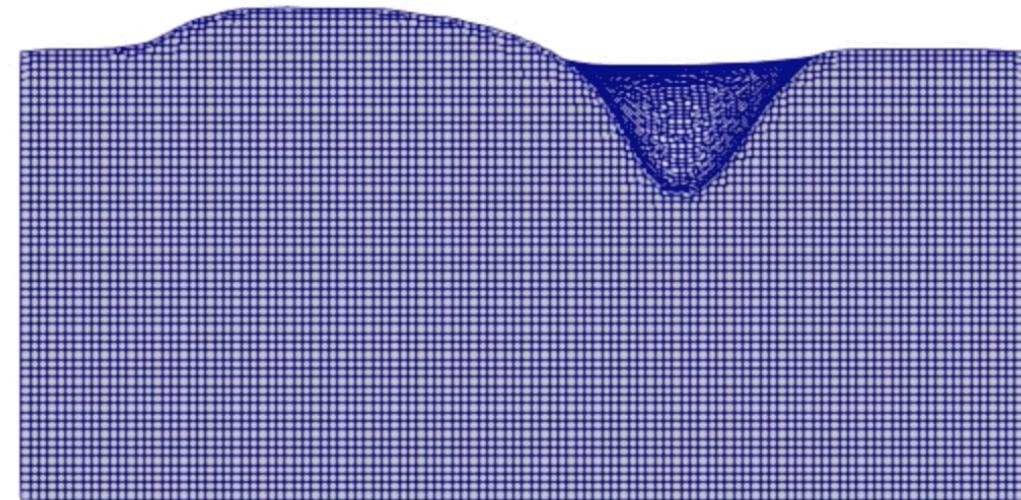
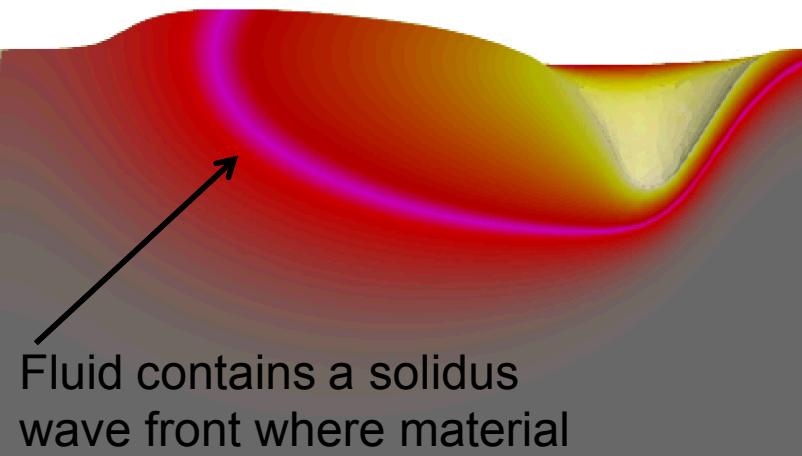
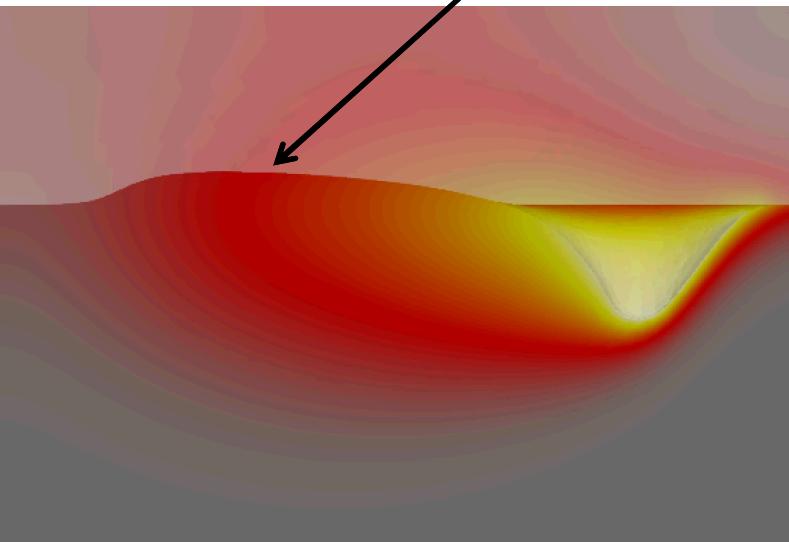


Residual Stress Predicted By Fluid Model



Residual Stress from Fluid Model

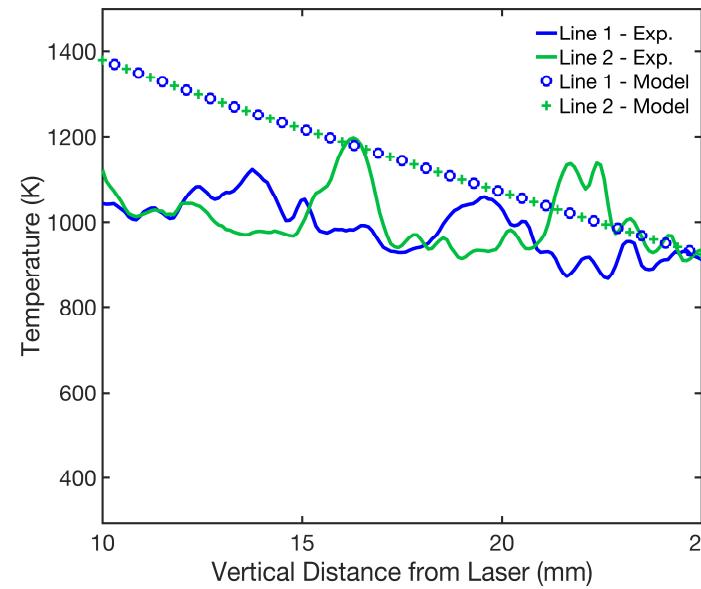
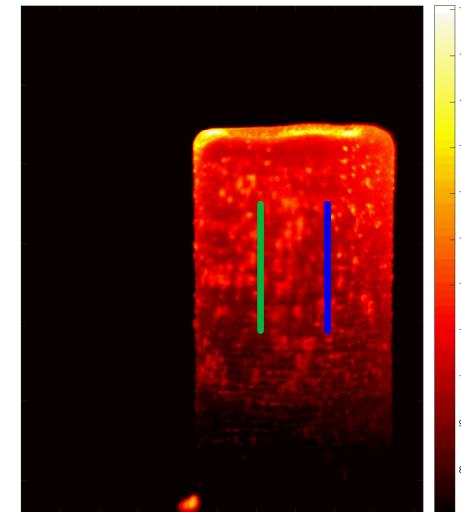
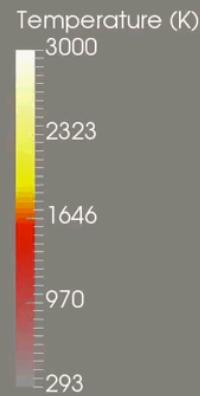
Fluid model predicts an evolving gas boundary



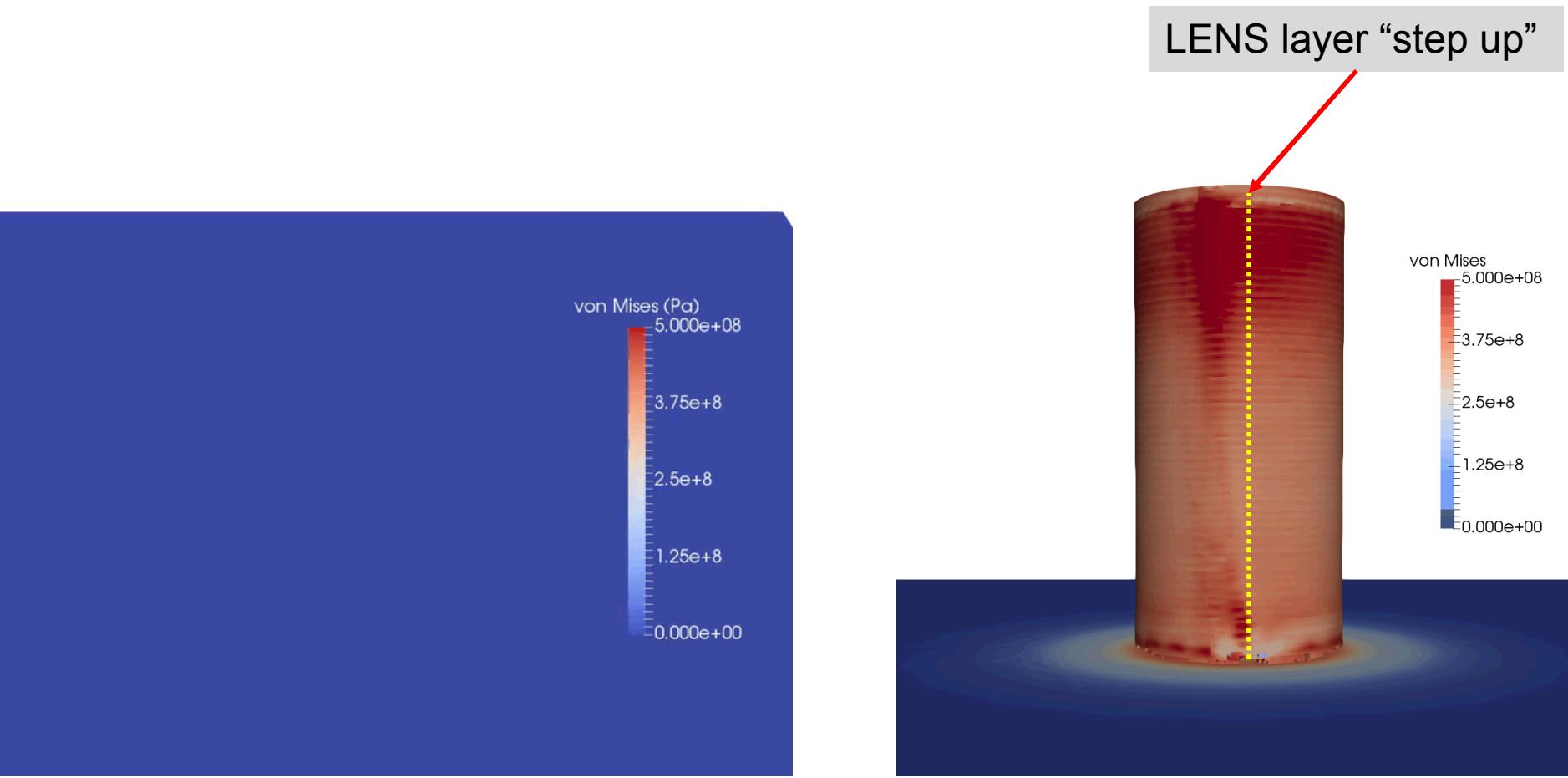
Generate a Lagrangian mesh from fluid model results to use for Solid mechanics calculation. Element stiffness transitions from soft to stiff based on the solidous wave front.

Experimental Comparison - Thermal

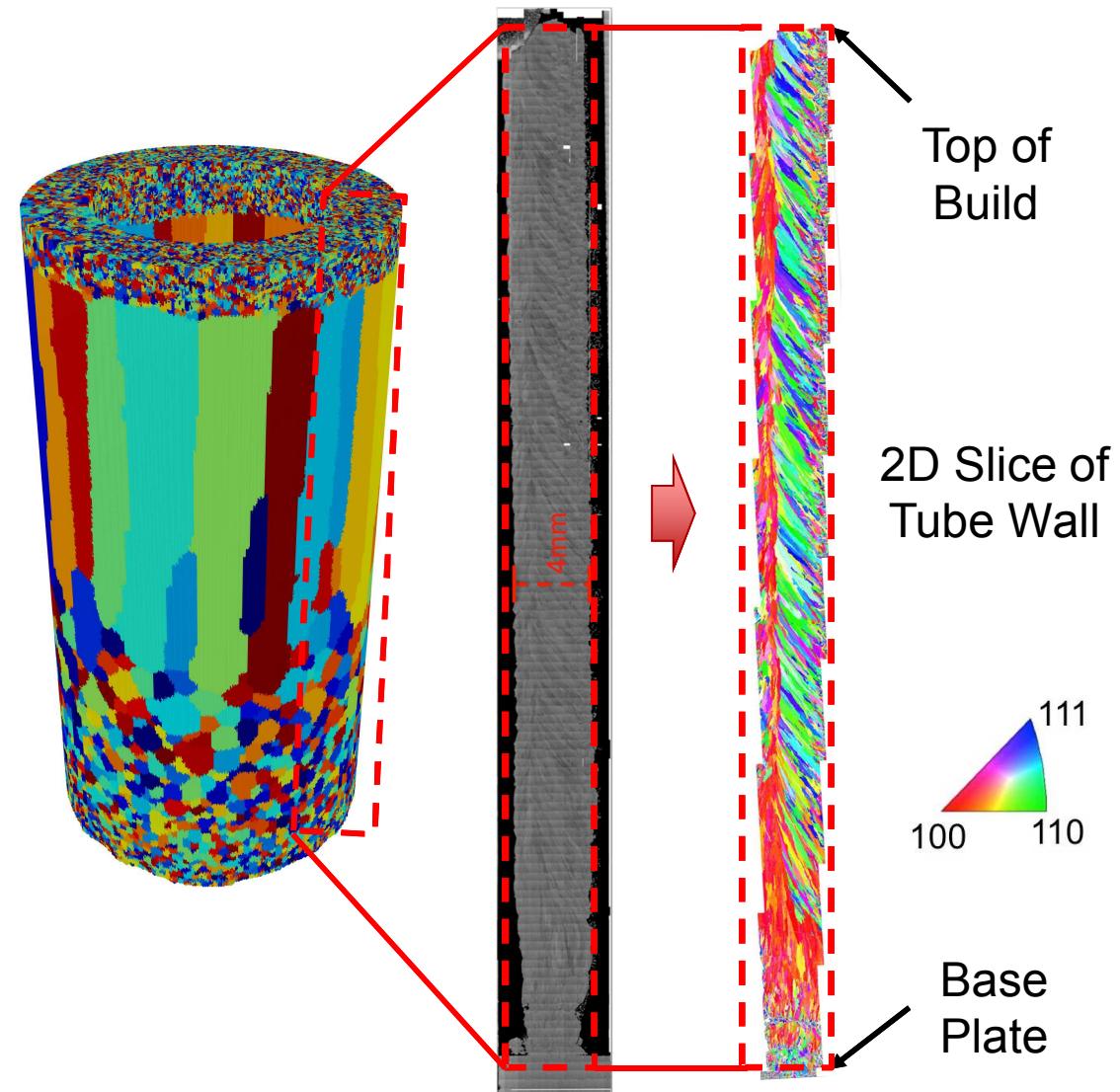
Time: 0.00 s



Experimental Comparison - Residual Stress



Experimental Comparison - Microstructure

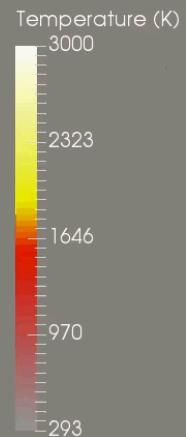
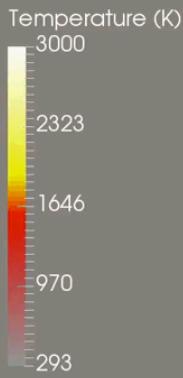


Thermal Comparison

Single Build

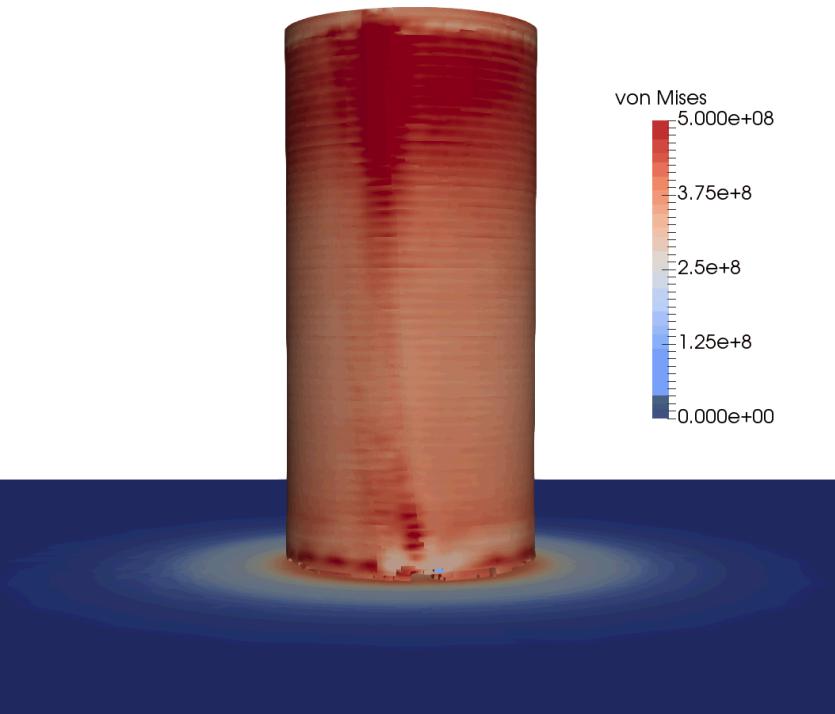
Double Build – 8 Second
Inter-layer Delay

Time: 0.00 s

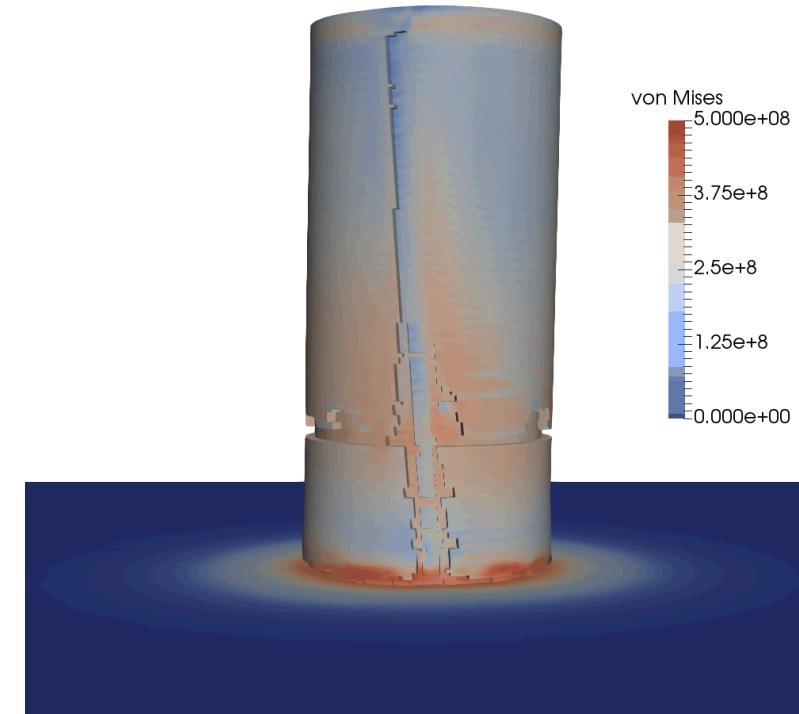


Delay time causes lower overall von Mises stress

Single Build

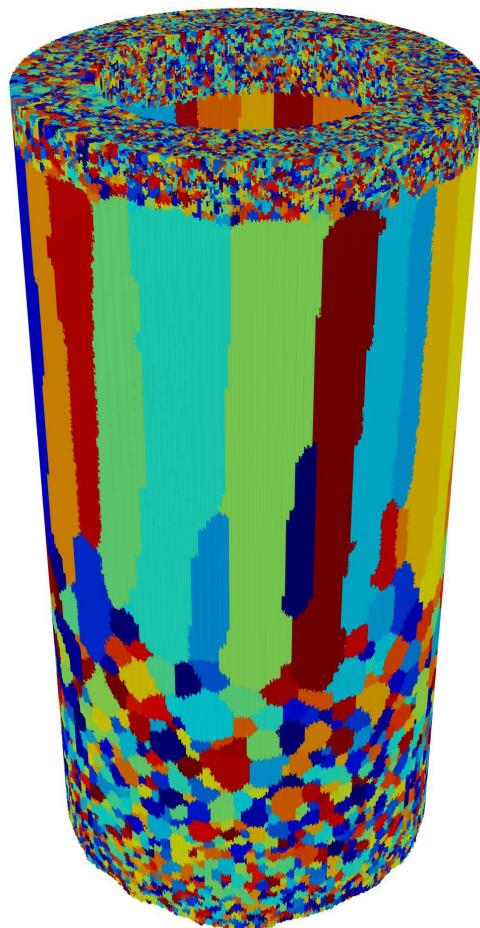


Double Build – 8 Second
Inter-layer Delay

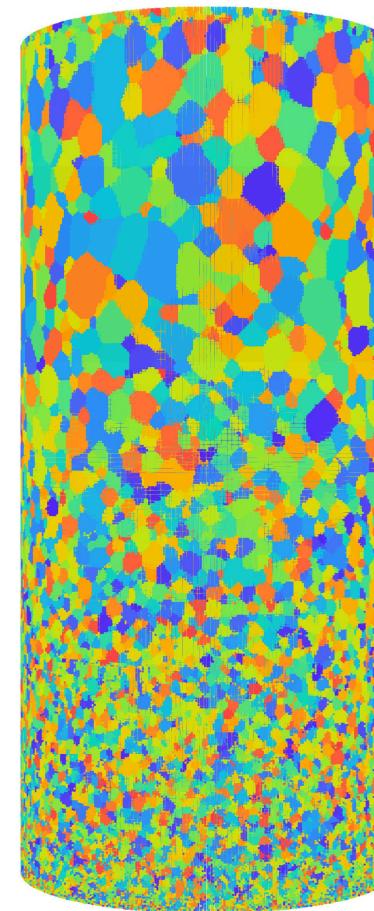


Delay time inhibits equiaxed to columnar transition

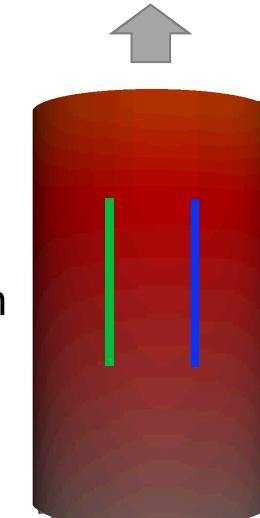
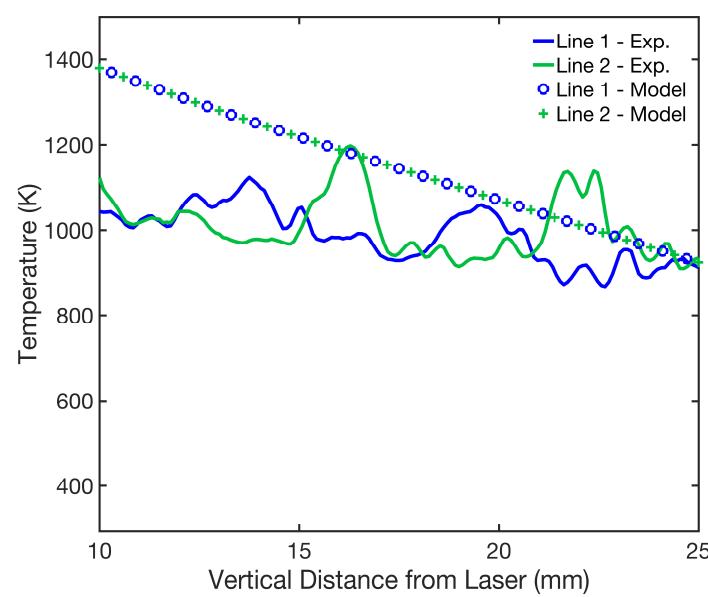
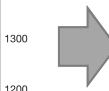
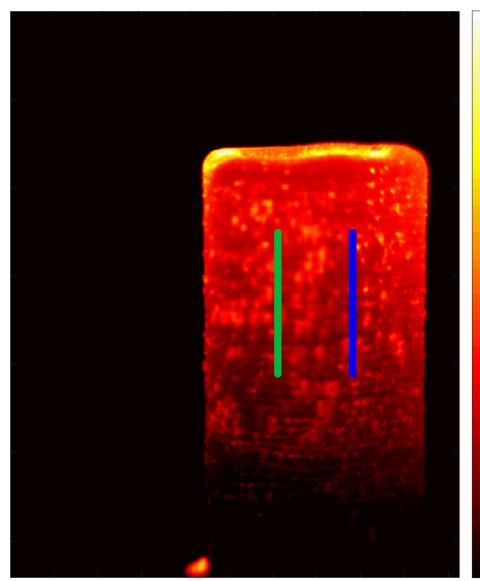
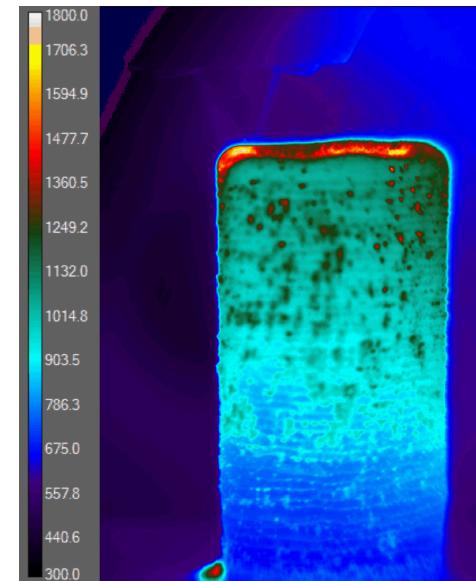
Single Build



Double Build – 8 Second
Inter-layer Delay



Comparison to IR Imaging



Simulation
Results

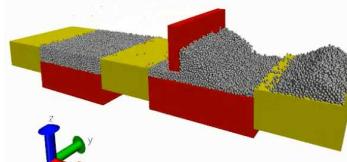
- IR camera mounted on LENS machine
- Assumes constant emissivity
- Compared to simulation

SNL Modeling Work

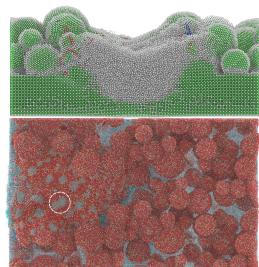
Codes

LAMMPS, SPPARKS,
Sierra/Aria,
Sierra/Adagio

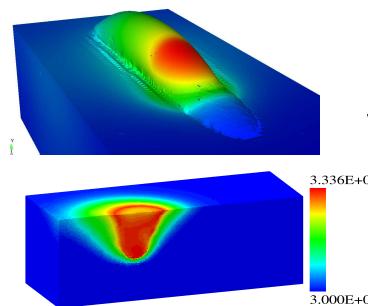
Powder Spreading
Dan Bolintineanu



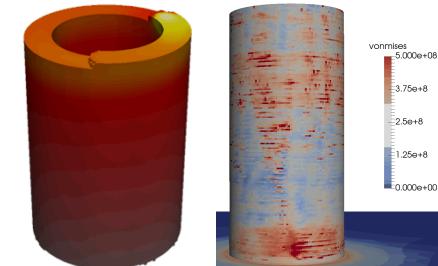
Powder Behavior
Mark Wilson



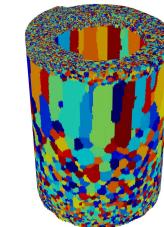
Mesoscale Thermal Behavior
Mario Martinez & Brad Trembacki



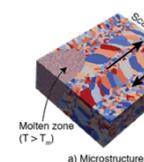
Part Scale Thermal & Solid Mechanics
Kyle Johnson, Kurtis Ford & Joe Bishop



Part Scale Microstructure
Theron Rodgers



Mesoscale Texture/Solid Mechanics/CX
Judy Brown, Theron Rodgers and Kurtis Ford



10^{-6}

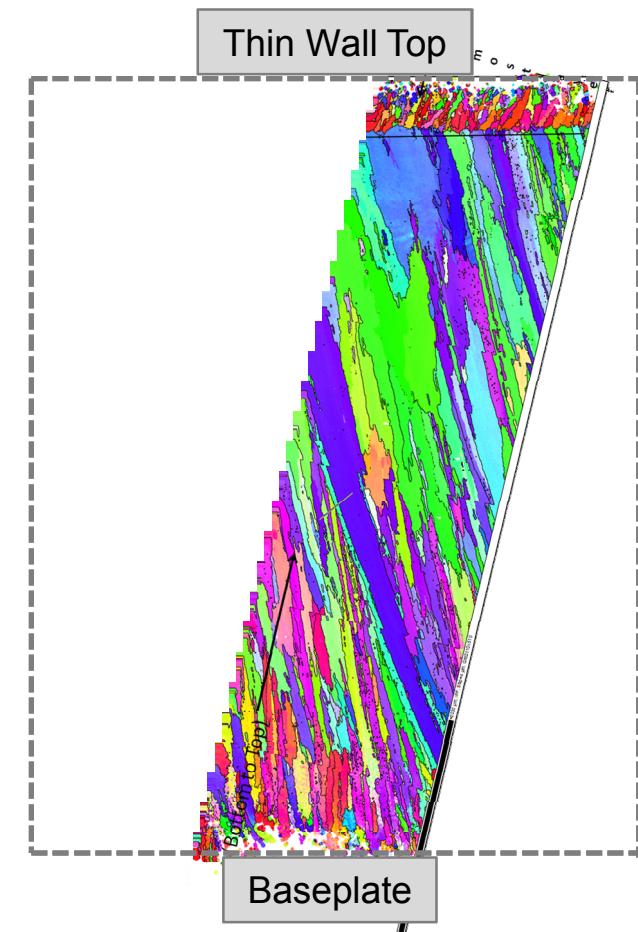
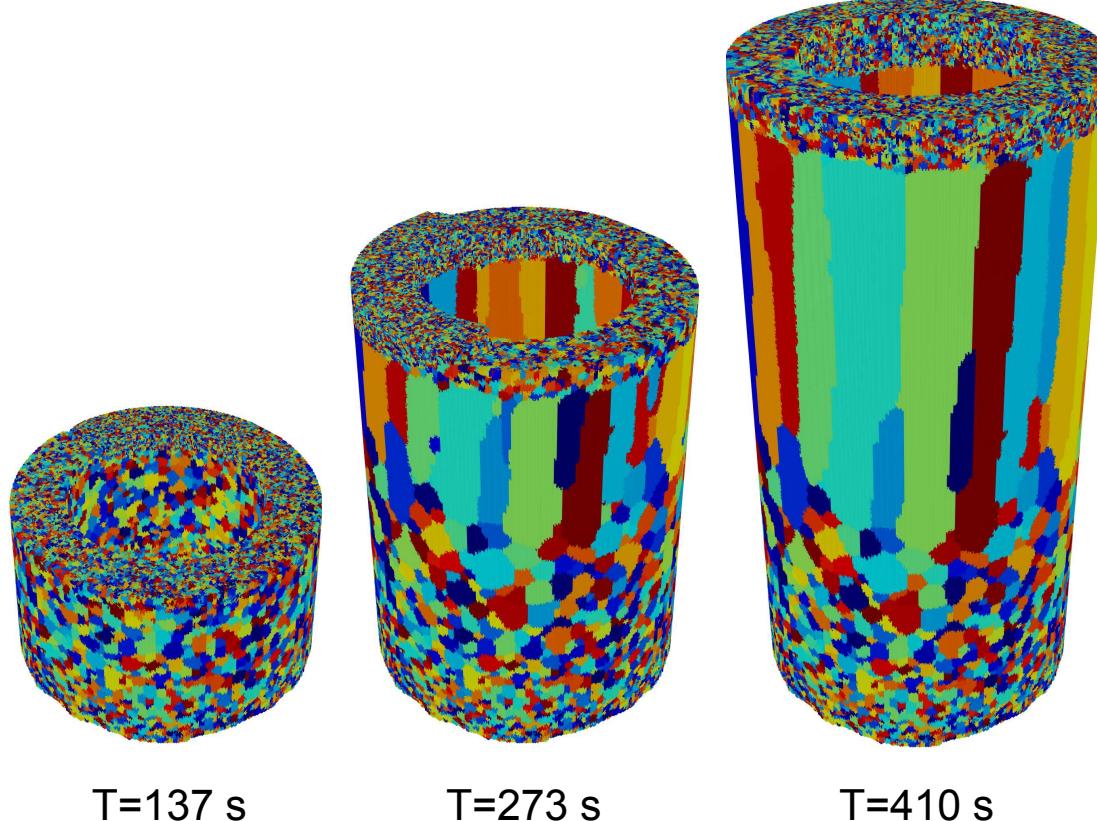
10^{-3}

Length Scale (m)

1

47

Equiaxed to Columnar Transition Observed in Literature



Thin wall IN718 LENS build at 900 W
Parimi *et al.* 2013

- **Multi Scale Solid Mechanics Models of Additive Manufacturing**
- **Kurtis R. Ford, Bradley Trembacki, Kyle Johnson, David Noble, Mario Martinez, Joe Bishop**
Sandia National Laboratories, Albuquerque, NM
-
- TMS 2018 Target Symposium: *Additive Manufacturing of Metals: Establishing Location-Specific Processing-Microstructure-Property Relationships*
- In this work a continuum-scale thermal/fluid model is coupled to a history-dependent elasto-viscoplastic internal state variable model of 304L stainless steel to predict the residual stress in an additively manufactured part. The thermal/fluid model tracks an evolving metal-gas interface with a conformal decomposition finite element method (CDFEM). The resulting bead shape and thermal history inform the elastic-viscoplastic constitutive model and a residual stress is calculated. These results are compared to a second more scalable model that does not represent the fluid mechanics of the melt pool explicitly. Instead, an idealized heat generation source is used with element activation to simulate element solidification on a larger scale. The two models are compared and contrasted with experimental data.
- Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525. Unclassified Unlimited Release: SAND####