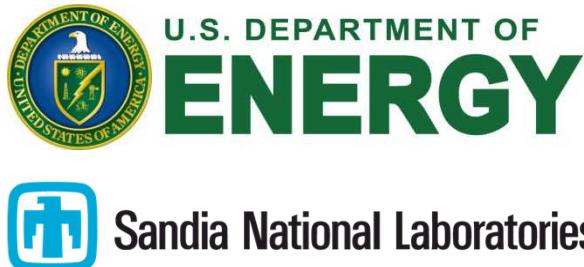


Effect of Fracture Toughness Testing Geometry on Opening Style: Implications for Subsurface Crack Propagation

Alex Rinehart

E&ES (NMT) and Geomechanics (SNL)

E&ES Seminar
New Mexico Tech
28 August 2014



Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.

Acknowledgements

Co-authors

Thomas Dewers and Joseph Bishop

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Advisor

Glenn Spinelli

This material is based upon work supported as part of the Center for Frontiers of Subsurface Energy Security, an Energy Frontier Research Center funded by the U.S. Department of Energy, Office of Science, Office of Basic Energy Sciences under Award Number DE-SC0001114. Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.

To Begin....

**Mechanical strength of Lower Tuscaloosa
Injection Horizon at CO₂ injection
reservoir conditions.**

**Effect of fracture toughness testing
geometry on opening style.**

**Automatic overlapping phase arrival
picker: Picking P&S waves from acoustic
emissions.**

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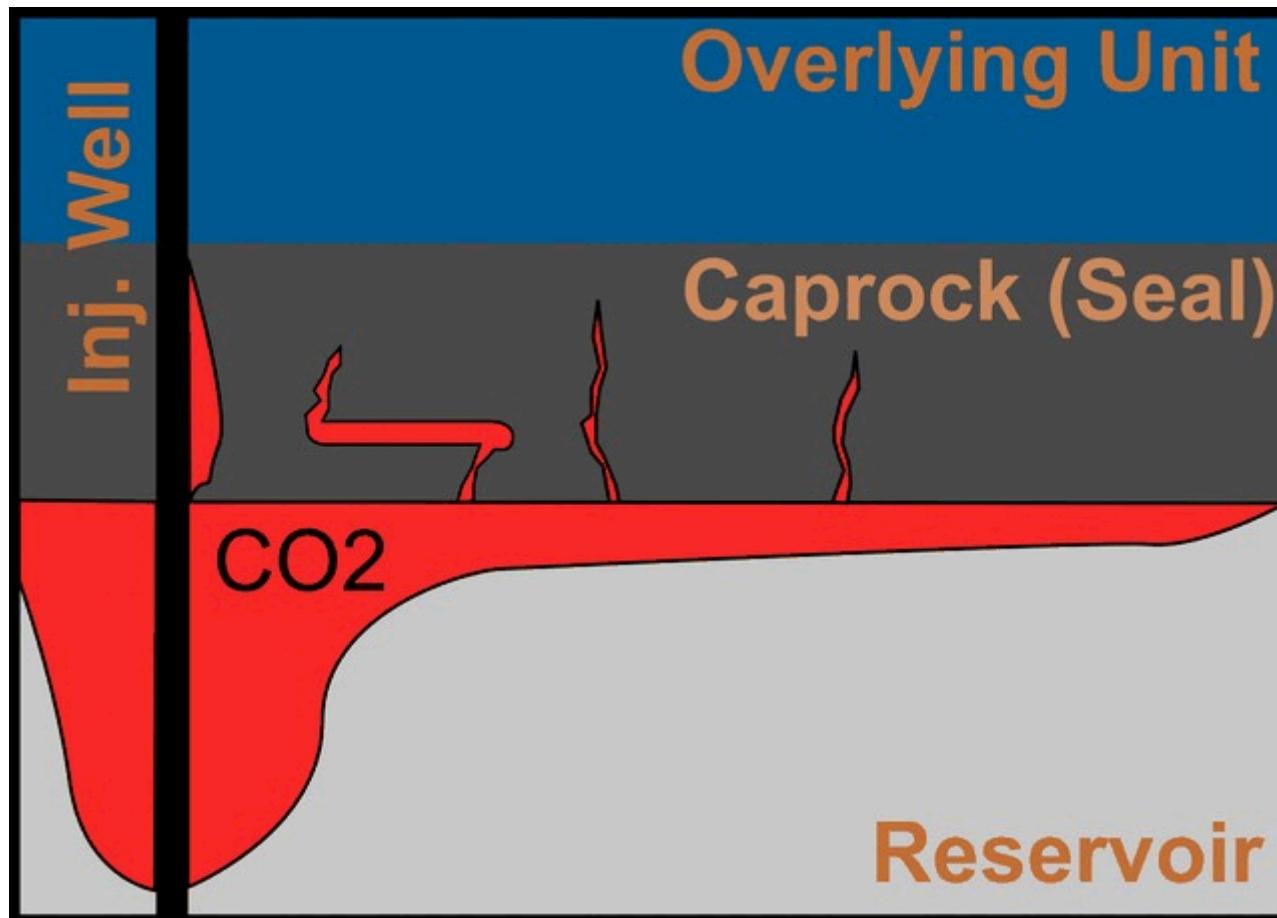
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Why Care About Fractures?

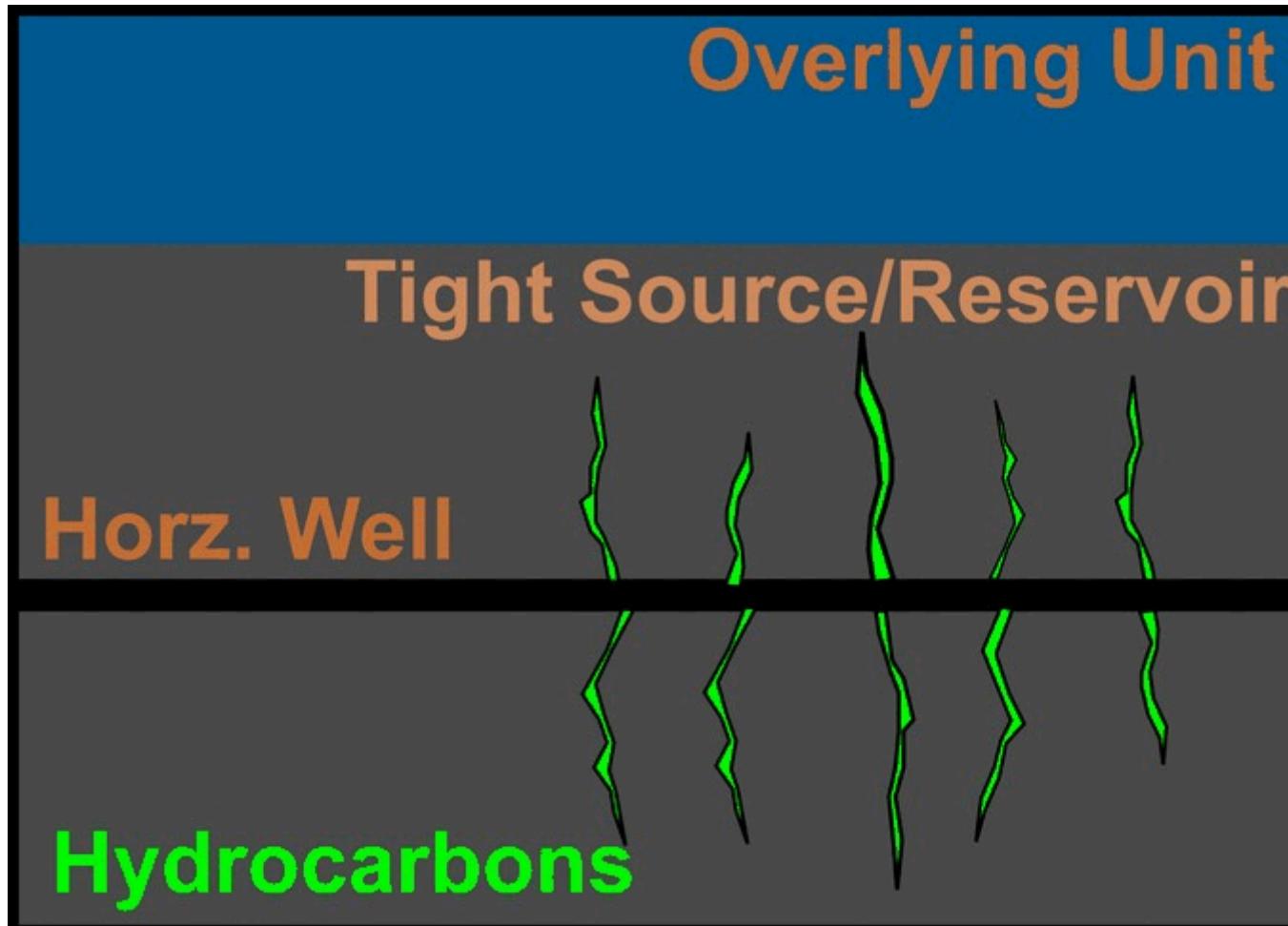
Fractures are a fast flow path in tight rocks.



Subsurface CO2 storage leakage pathway.

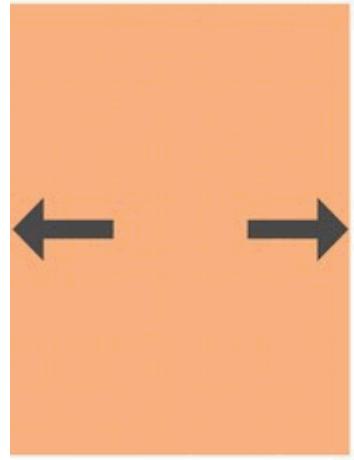
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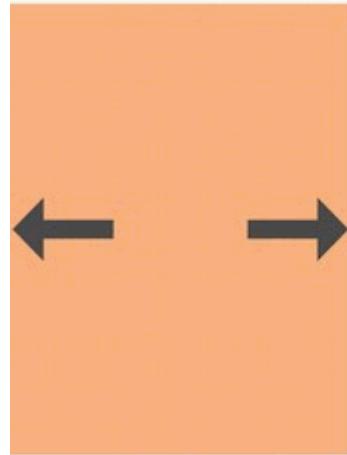
Natural Gas Release in Shales

Fractures Defined

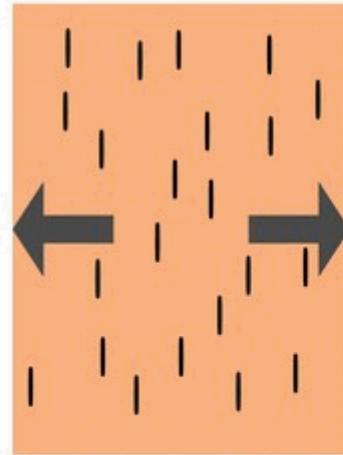


Elastic

Fractures Defined

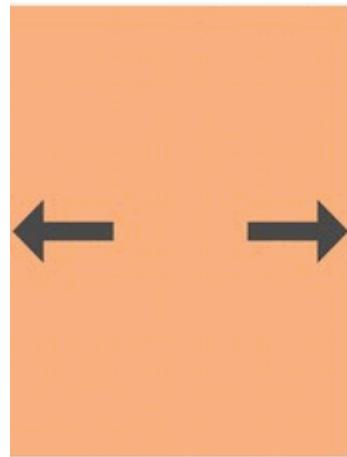


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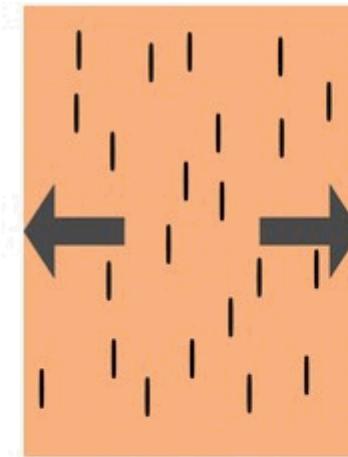


**Distributed
Damage
(Yield)**

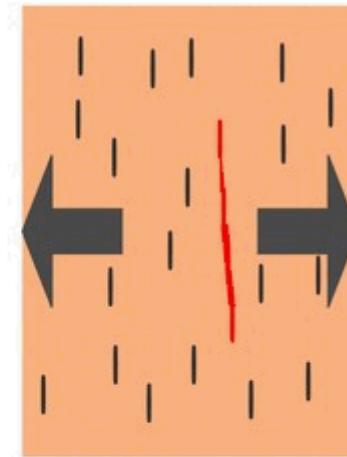
Fractures Defined



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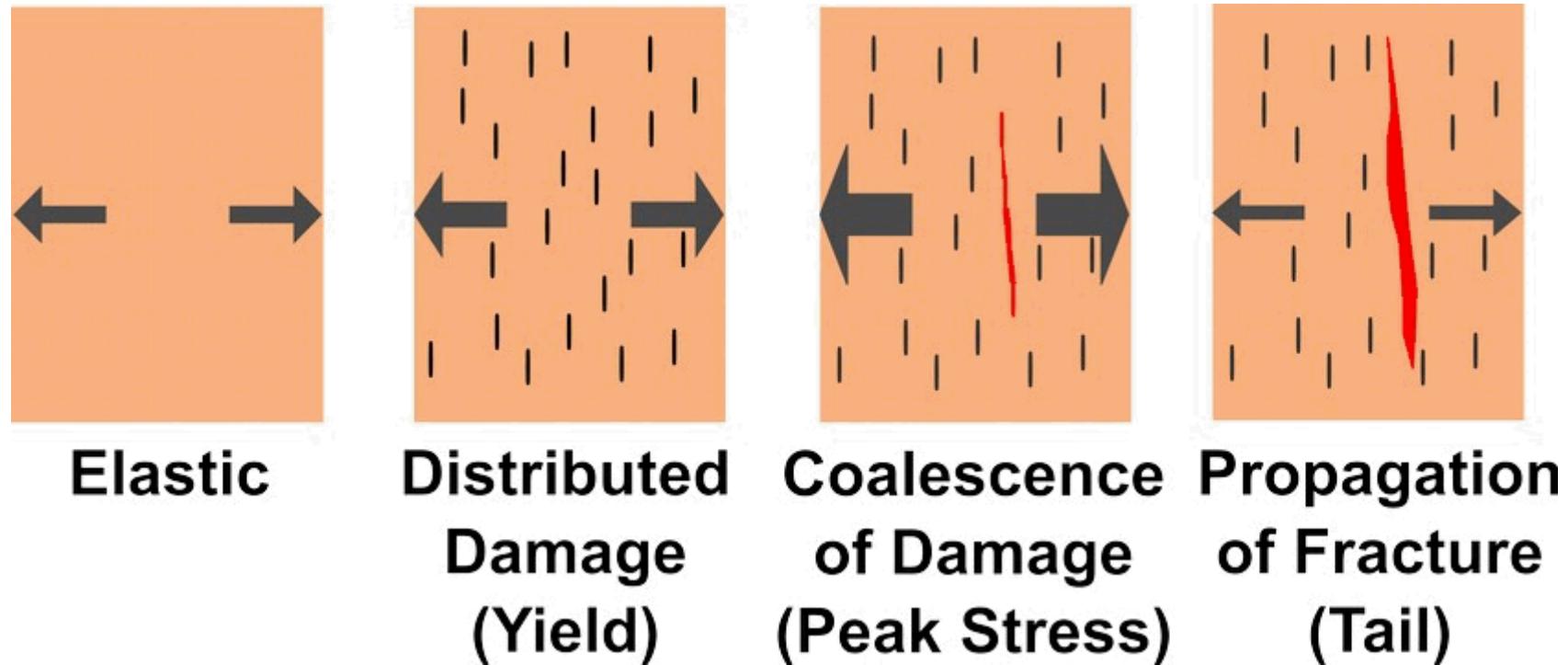


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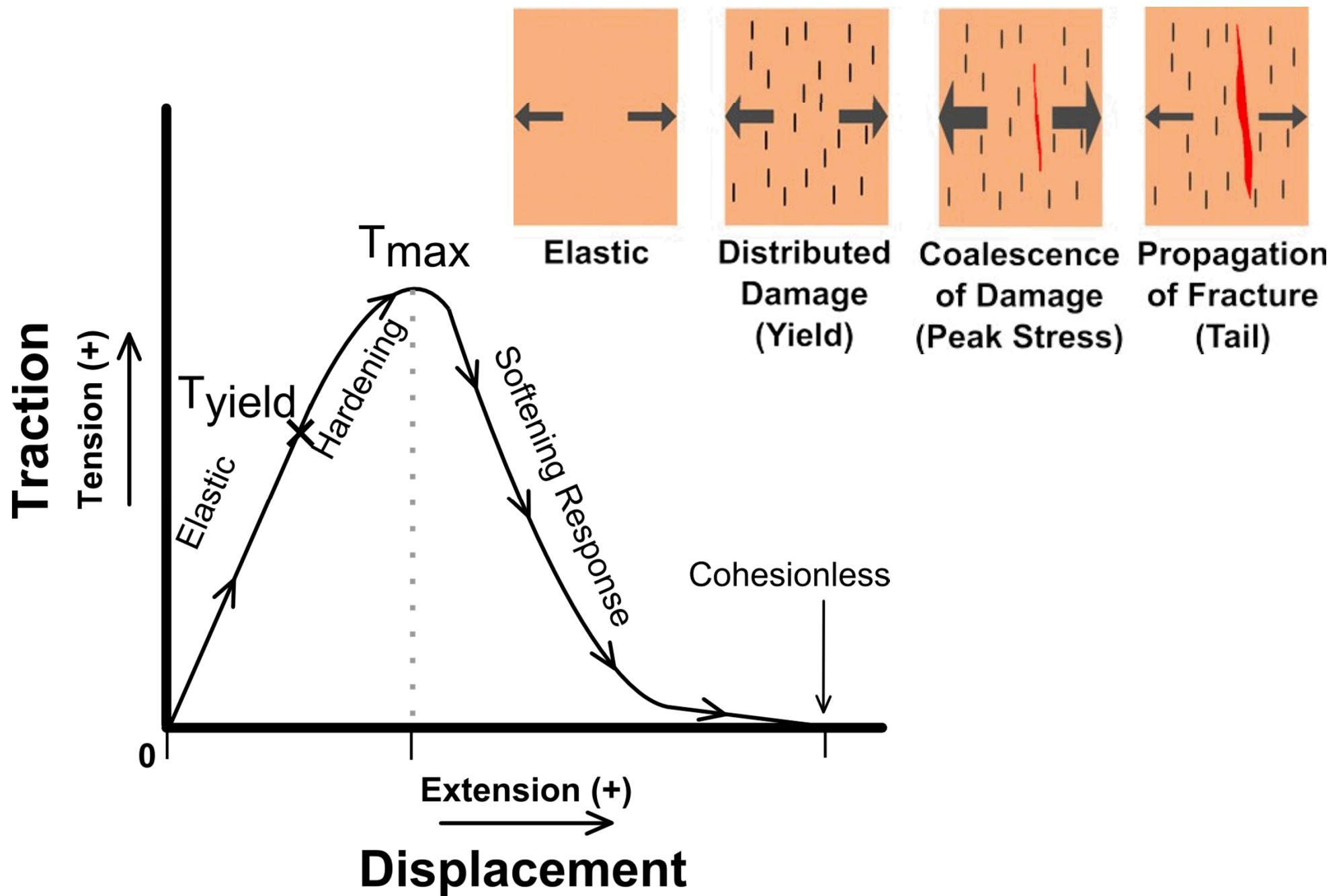
**Coalescence
of Damage
(Peak Stress)**

Fractures Defined

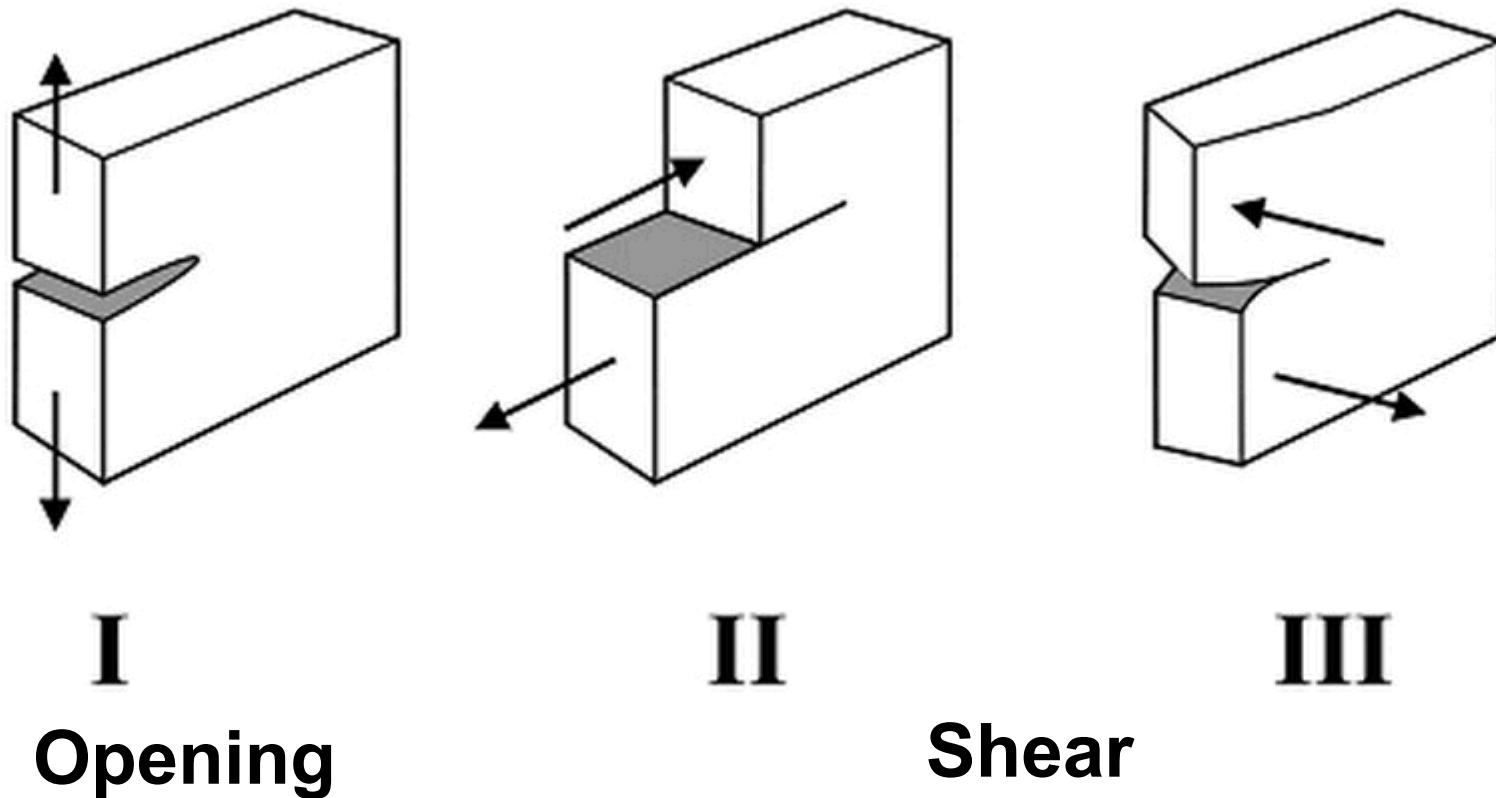


The coalescence of damage into a single roughly planar opening with limited surrounding damage.

Fractures Defined



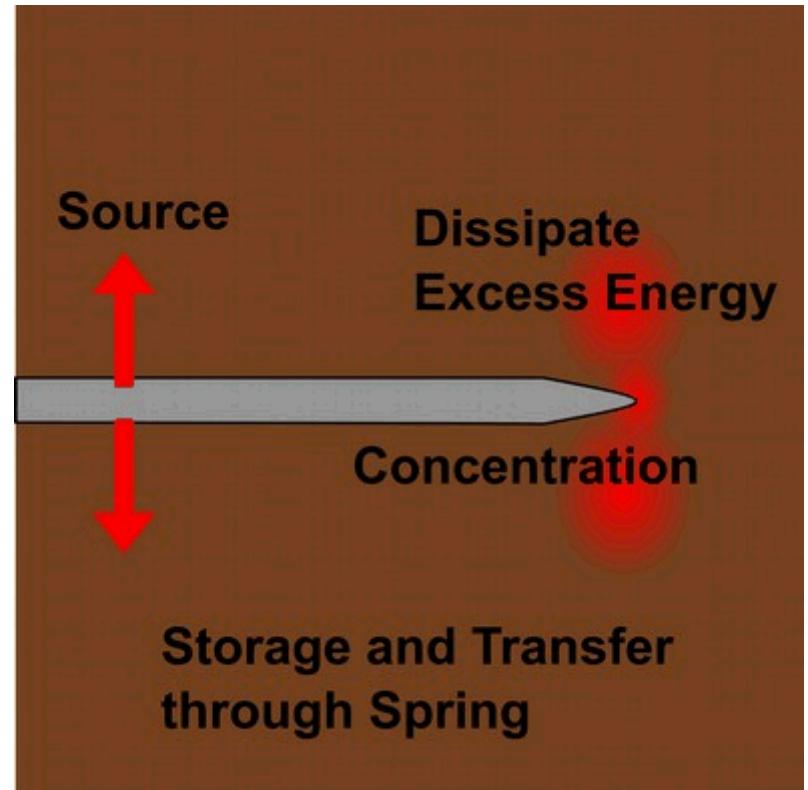
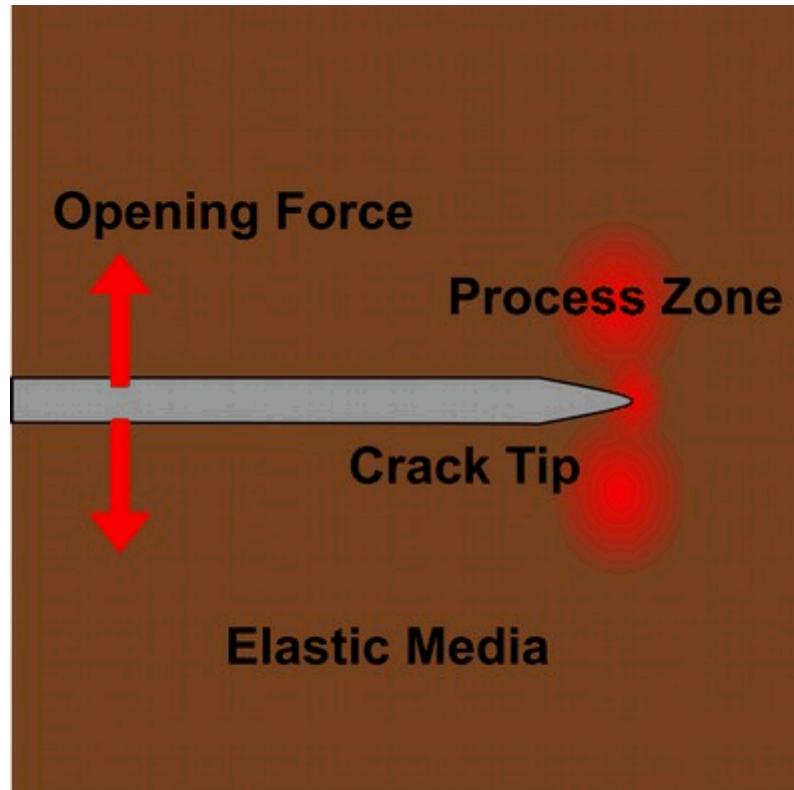
Modes: Opening vs. Shear



For rocks, shear mode is often to 5x stronger than opening mode

http://www.doitpoms.ac.uk/tplib/brittle_fracture/same.php

The Parts of a Fracture



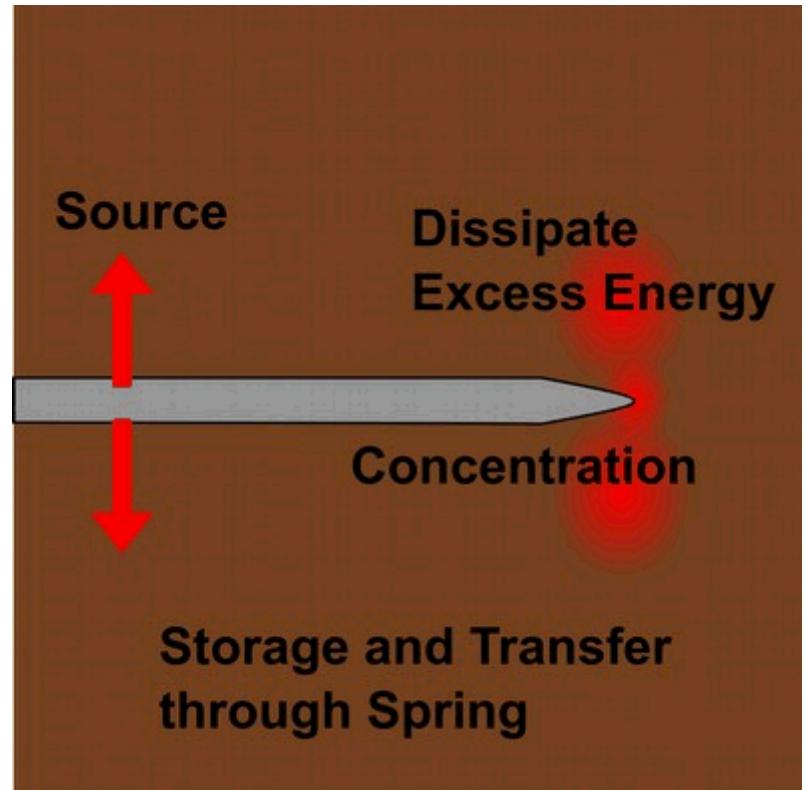
The Energy Balance

Softer the spring, the more displacement needed to get enough force (energy) to propagate fracture.

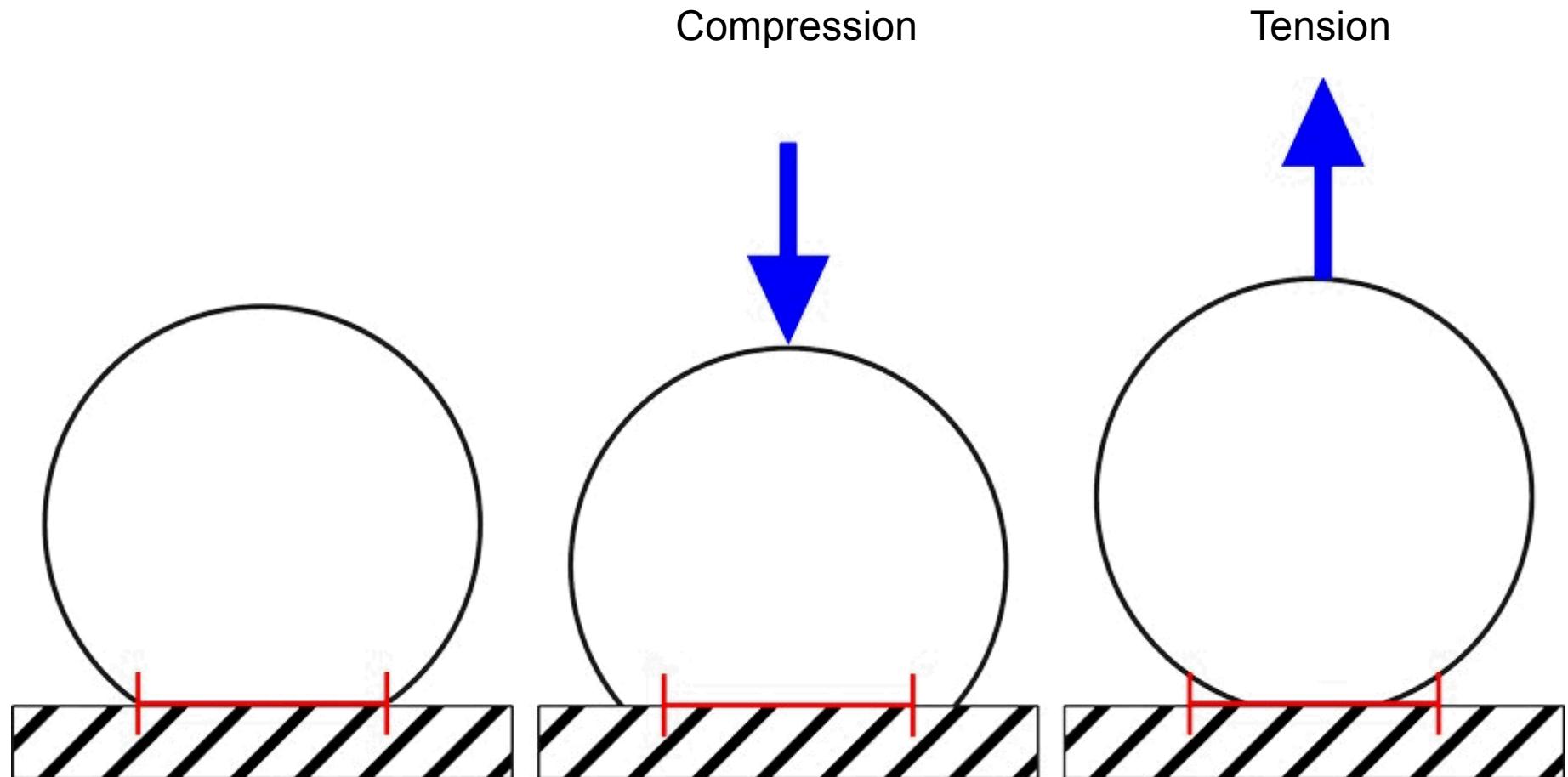
'Spring compliance' controlled by inherent material properties and tension/compression stress state.

Magnitude of excess energy controlled by fracture mode:

Shear Strength > Opening Strength

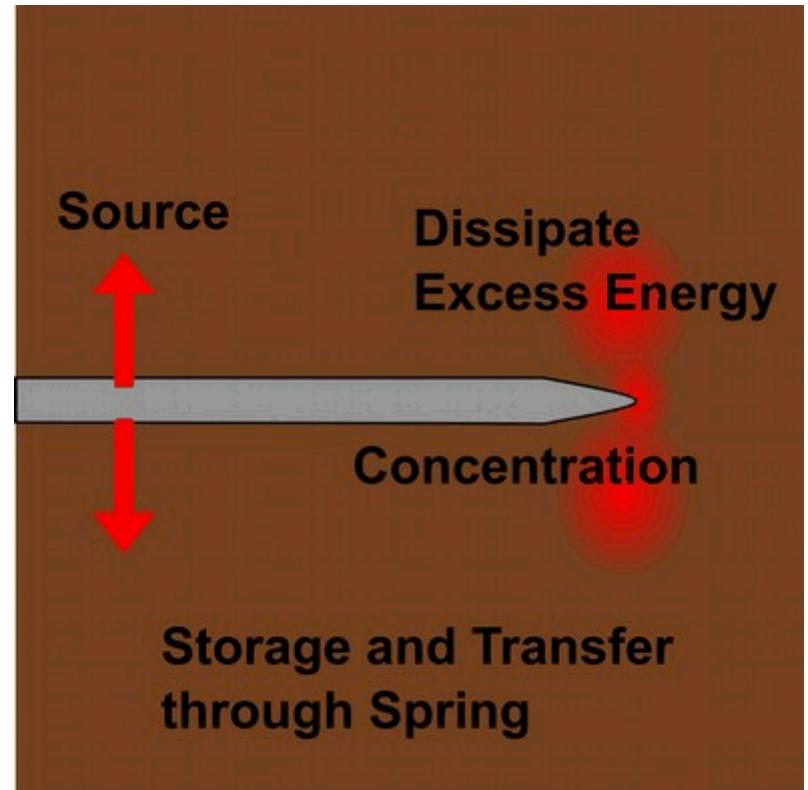
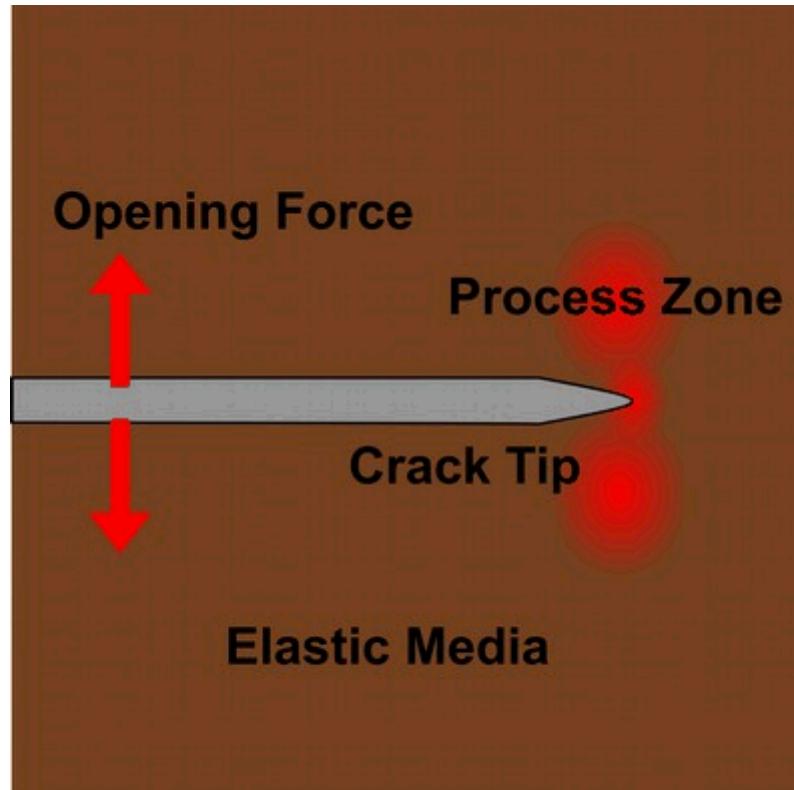


Tension vs. Compression

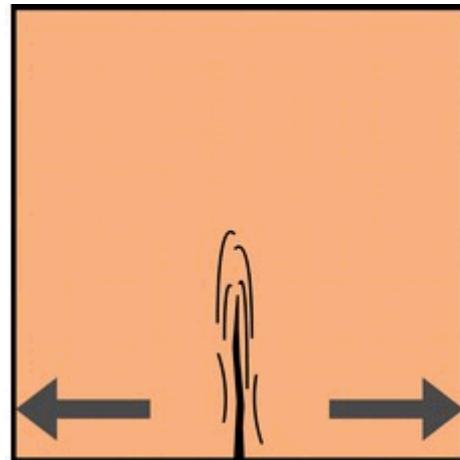


Both b/c of pores closing and grain contacts, elastic modulii are less stiff in tension than in compression.

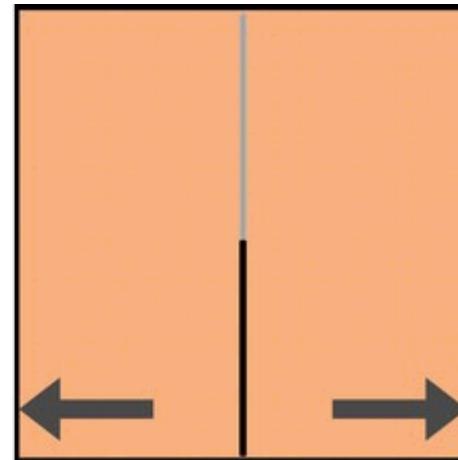
The Parts of a Fracture



Cohesive Fracture Approach



**'Real' Fracture
w/ Distributed
Damage and
Complex
Geometry**

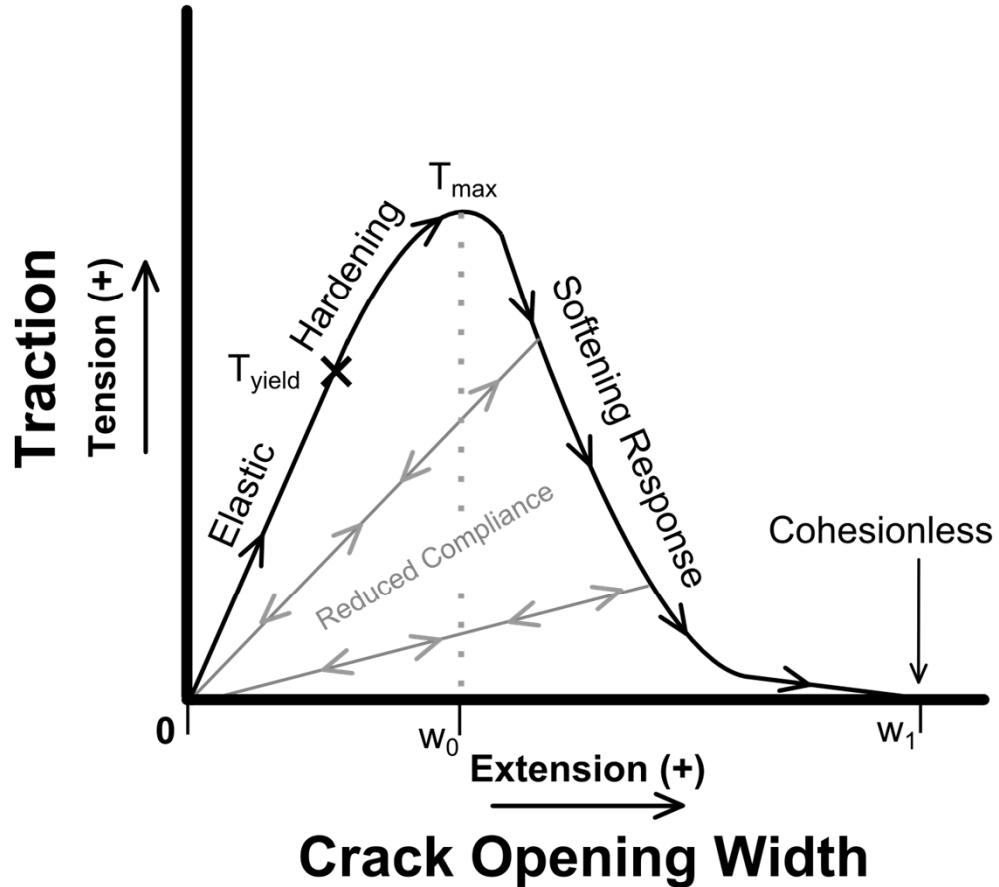


**Cohesive
Fracture w/
Finite Defined
Zone of
Damage**

Cohesive fracture lumps all inelastic deformation into thin finite zone.

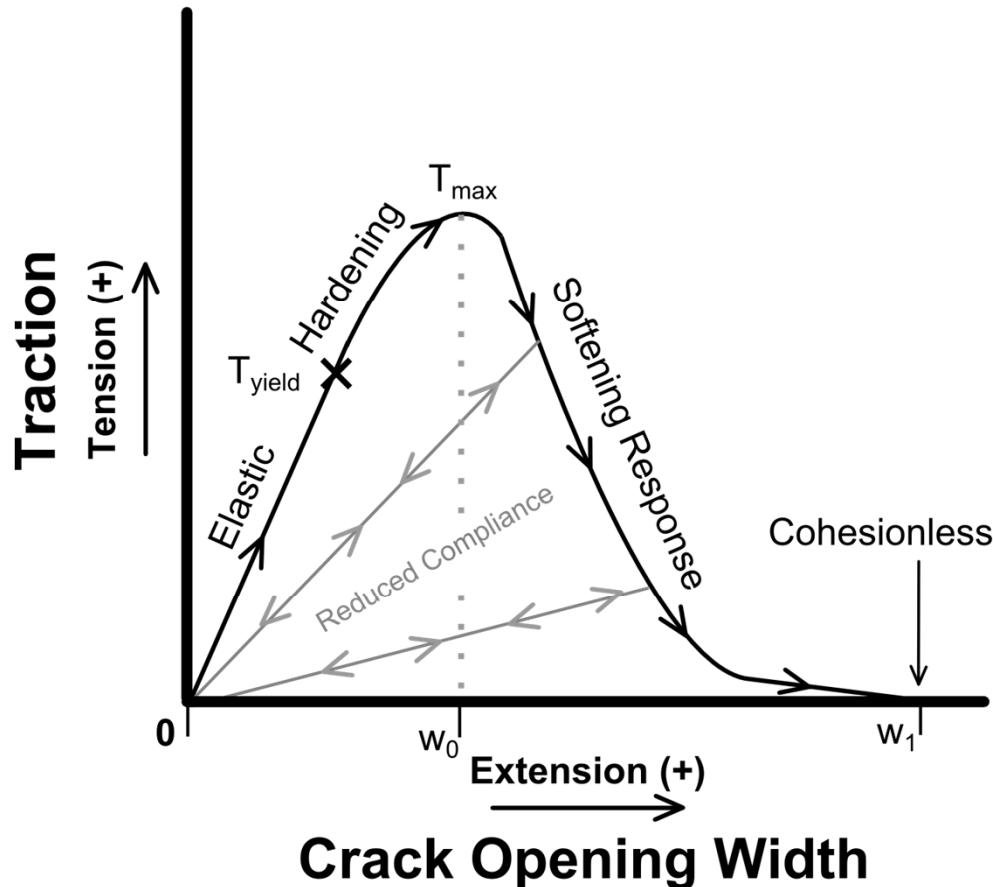
Cohesive Fracture Approach

General

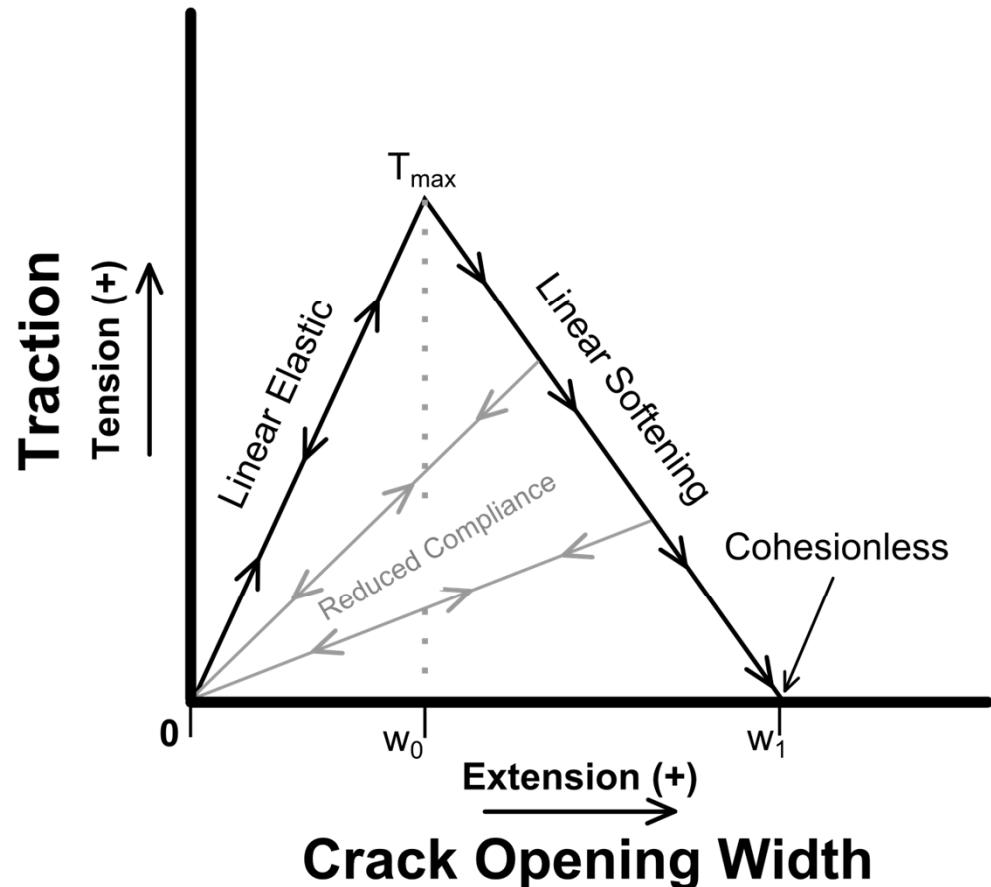


Cohesive Fracture Approach

General

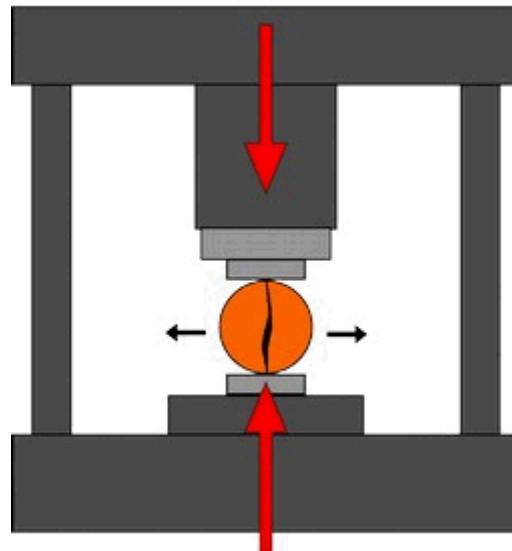
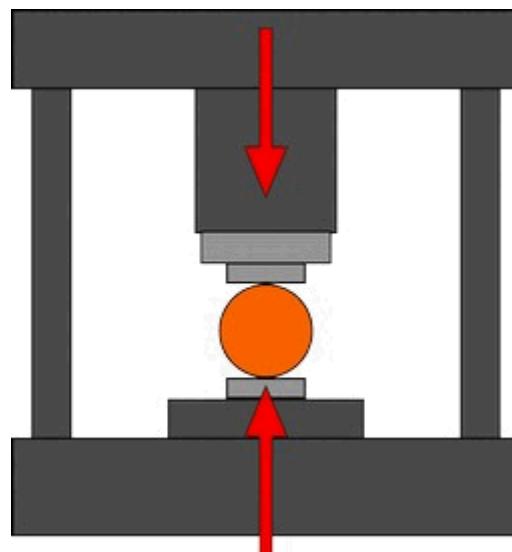


Linear Softening



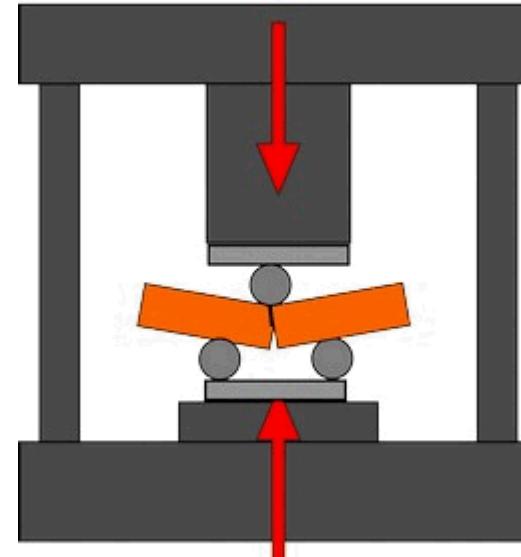
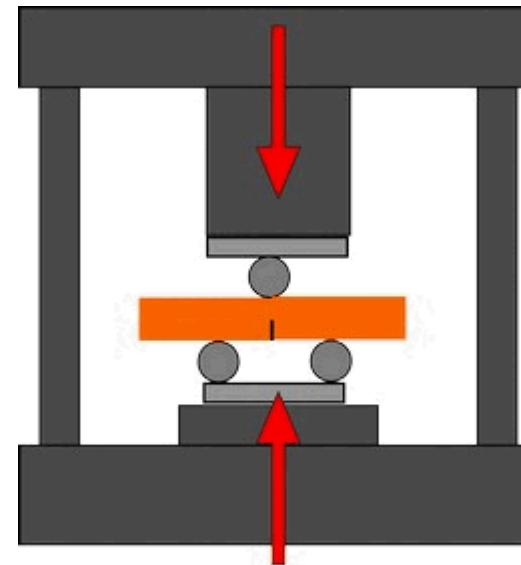
Posited in geomaterials, but little work systematically confirming approach.

Approaches to Fractures (Testing)



Brazil Test

Tensile Splitting Stress



Notched 3-Point-Bend
Fracture Toughness

Approaches to Fractures (Testing)

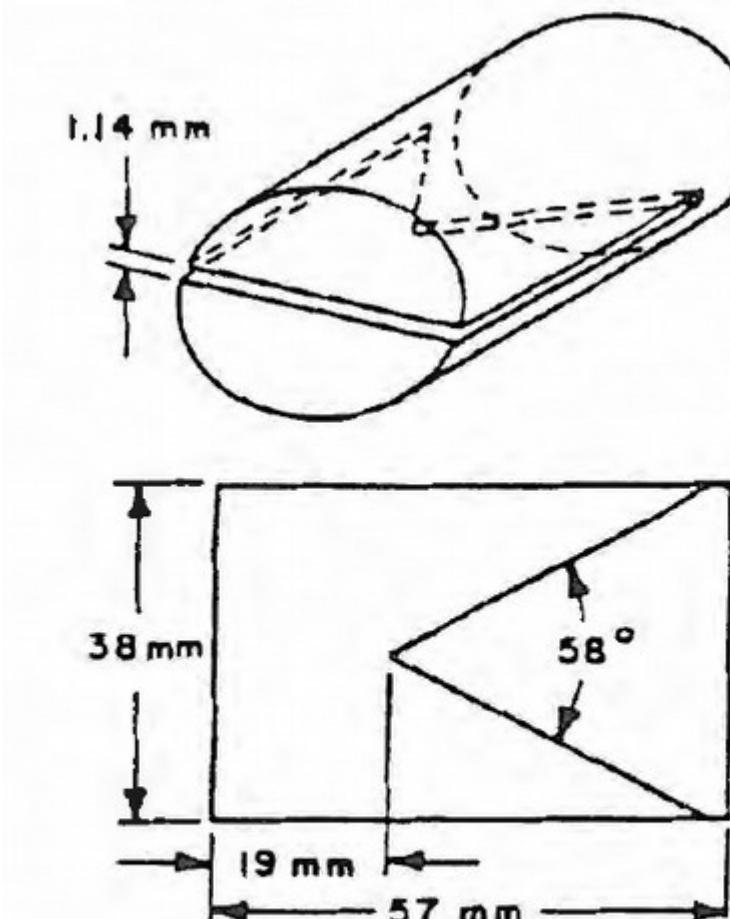
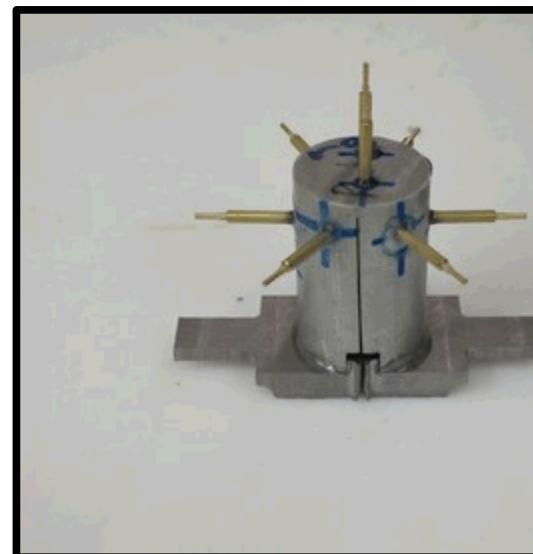


Fig. 1 Specimen Geometry.

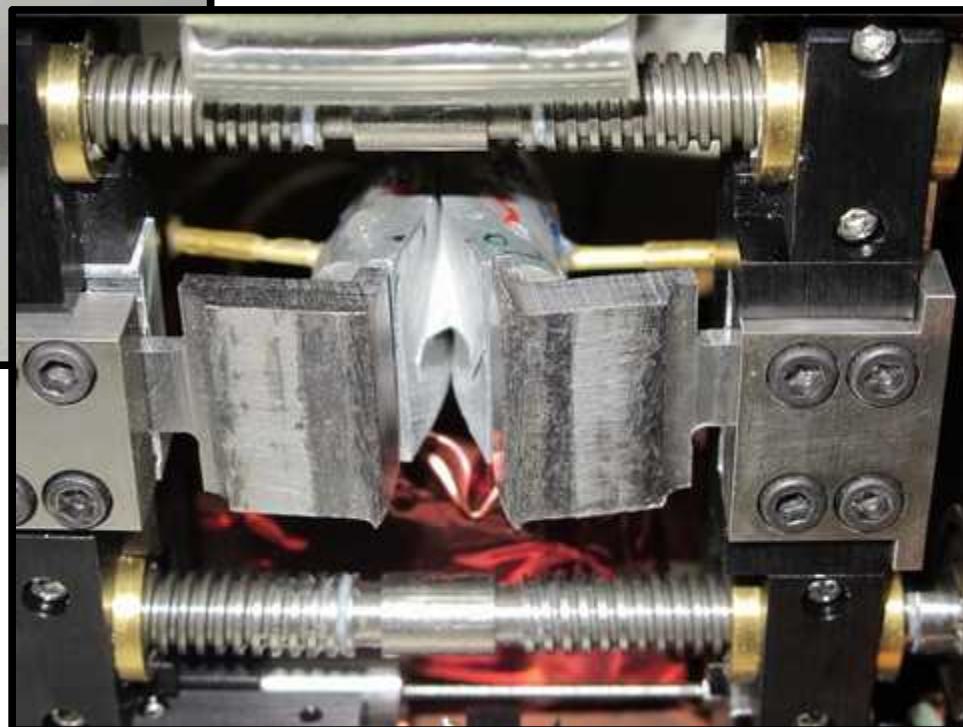
**Short-Rod
Fracture Toughness**

Senseny and Pfeifle (1987)

Approaches to Fractures (Testing)



Pre-Test



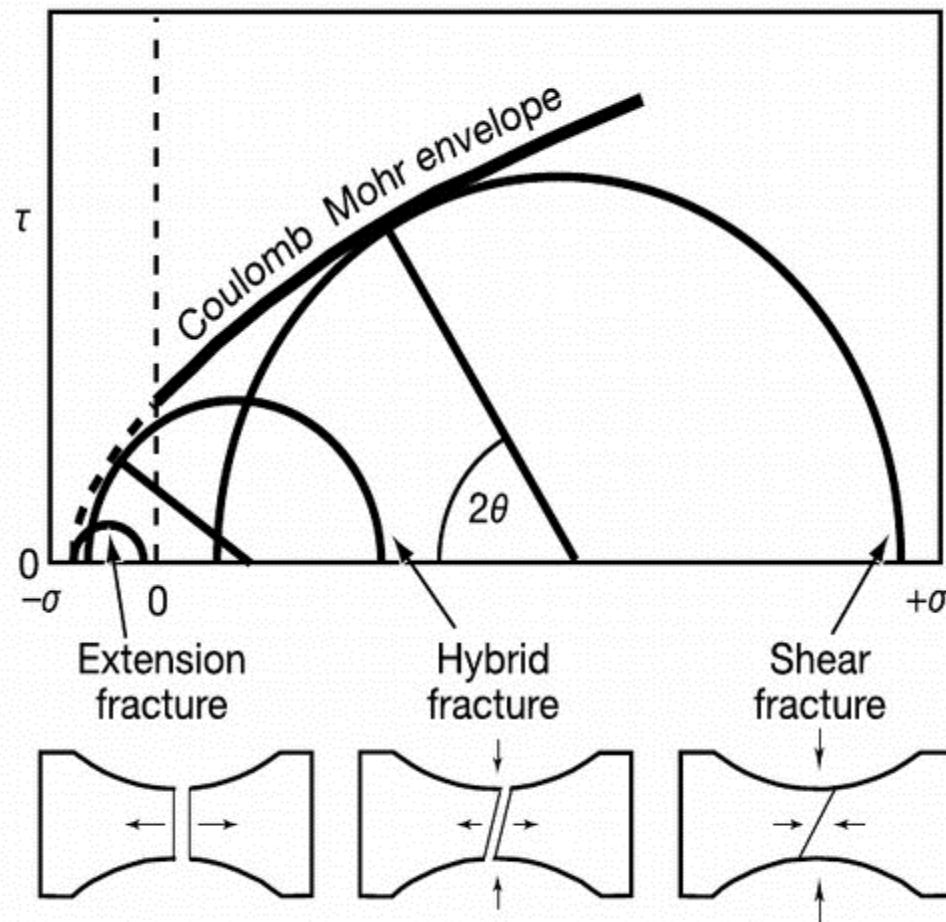
During Test



Post-Test

**Short-Rod
Fracture Toughness**

Subsurface Fractures in the Field



Mixed-mode fractures predominate fracture propagation deep (3,000 m depth).

Extension (Mode I) fractures dominate at shallow depths (<1,000 m depth).

The Big Question....

How sensitive are cohesive fracture model parameters to changes in geometry?

Do changing processes or simply changing stresses cause geometry dependence?

Which testing geometry is appropriate for parameterizing models for subsurface applications?

Calibration and Confirmation Outline

Notched 3-point bend (N3PB) geometry, mesh and experiments.

Short-rod geometry, mesh and experiments.

Short-rod cohesive fracture modeling and calibration.
Qualitative observations of deformation.

N3PB confirmation of cohesive fracture model.
Qualitative observations of deformation.

Summary of pros and cons of cohesive fracture modeling for parameterizing fracture propagation.

Calibration and Confirmation Outline

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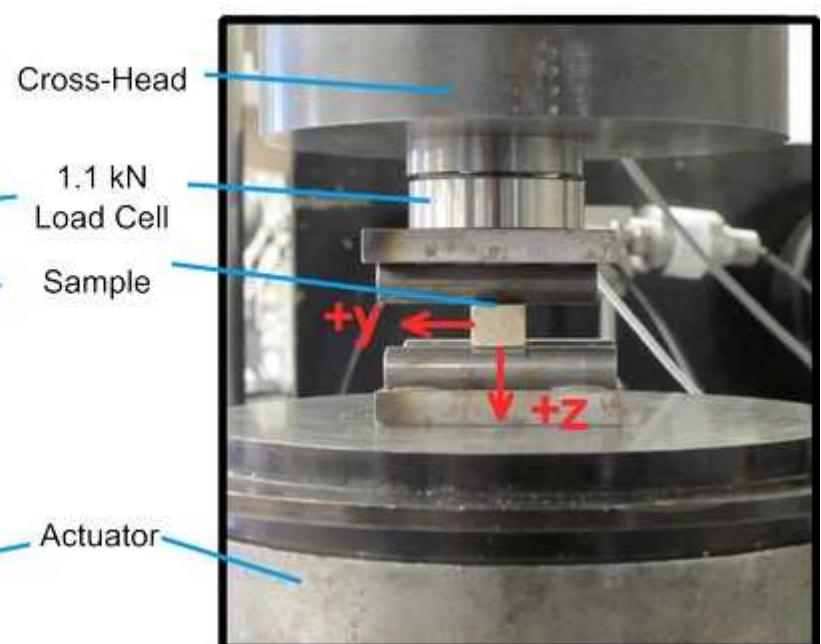
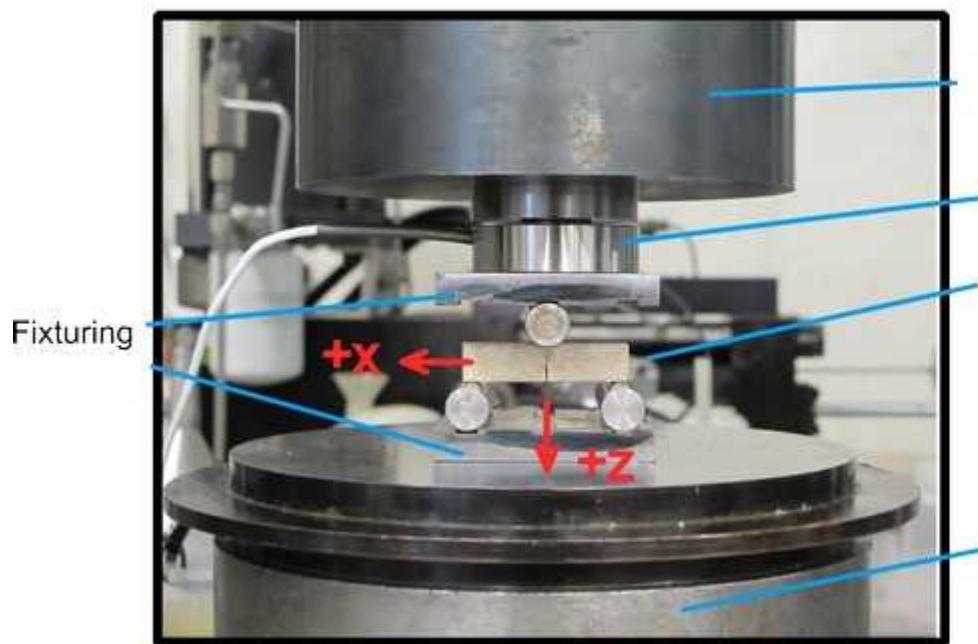
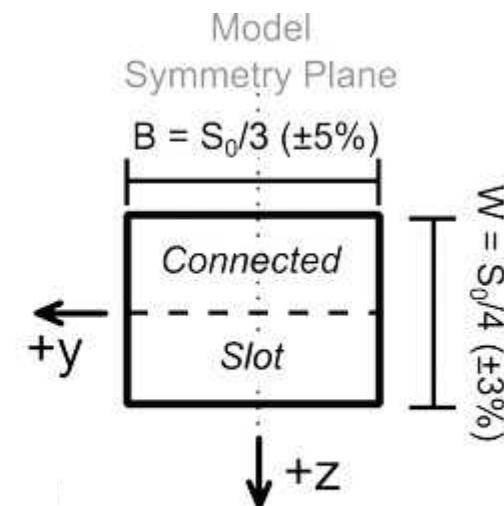
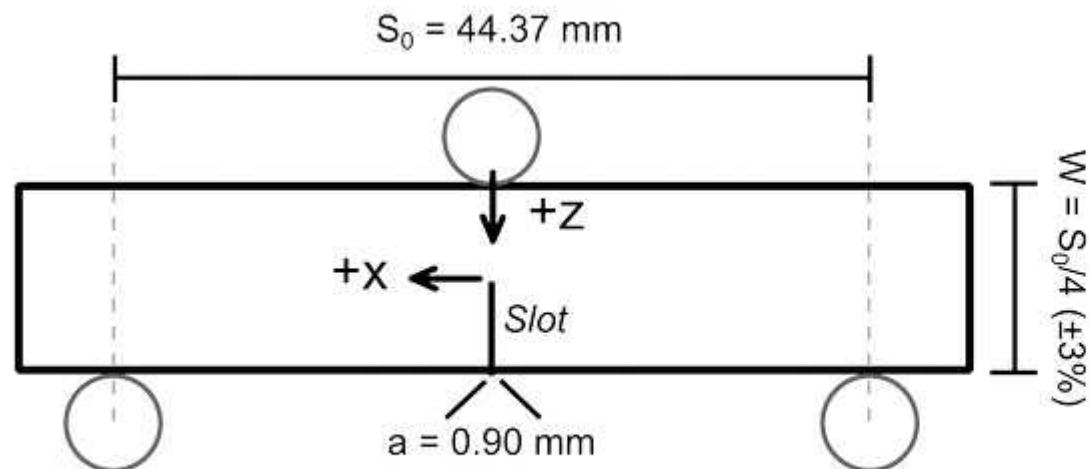
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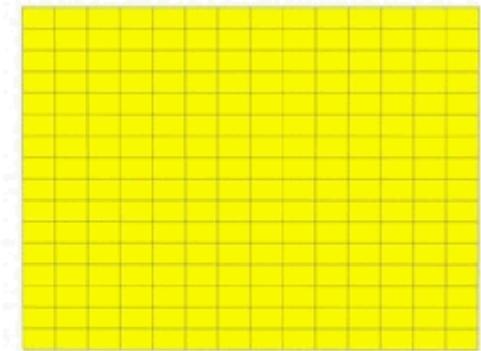
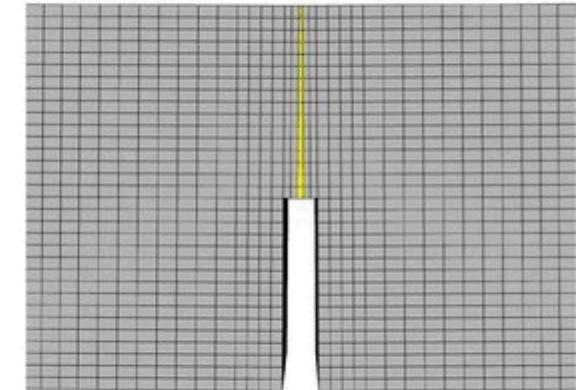
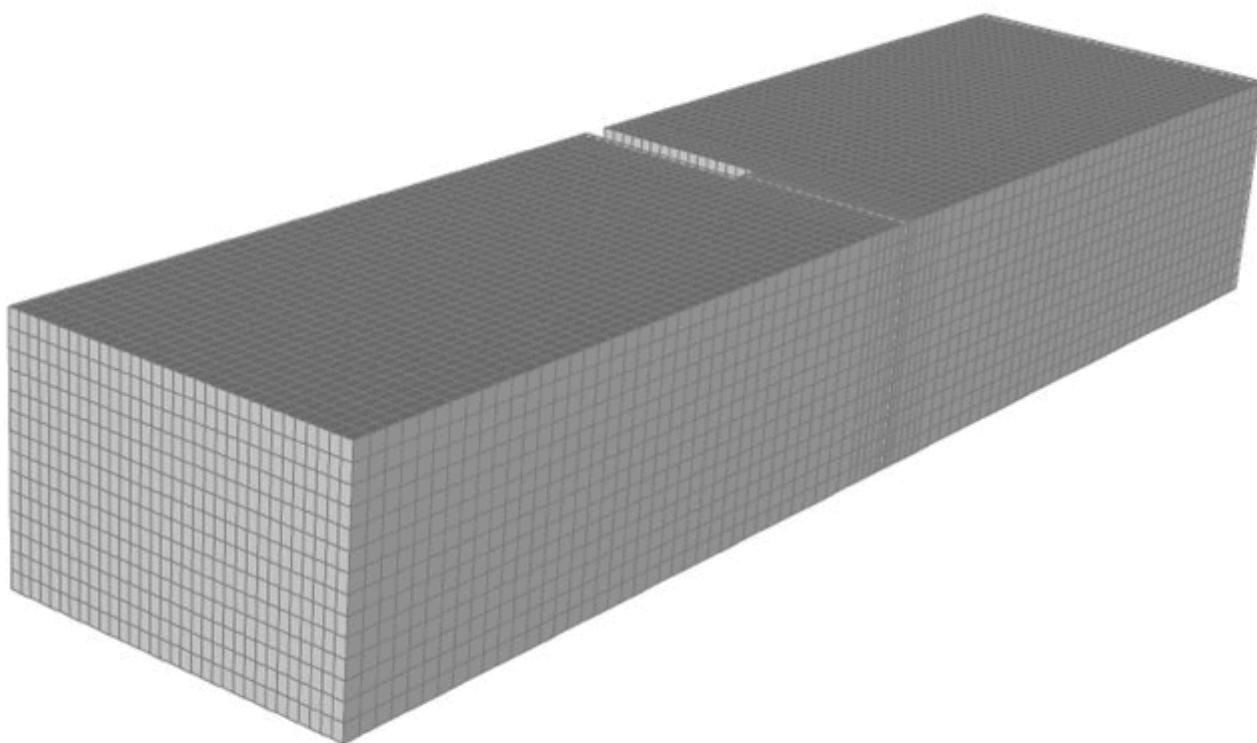
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3PB Tests and Geometry



N3PB Mesh



Calibration and Confirmation Outline

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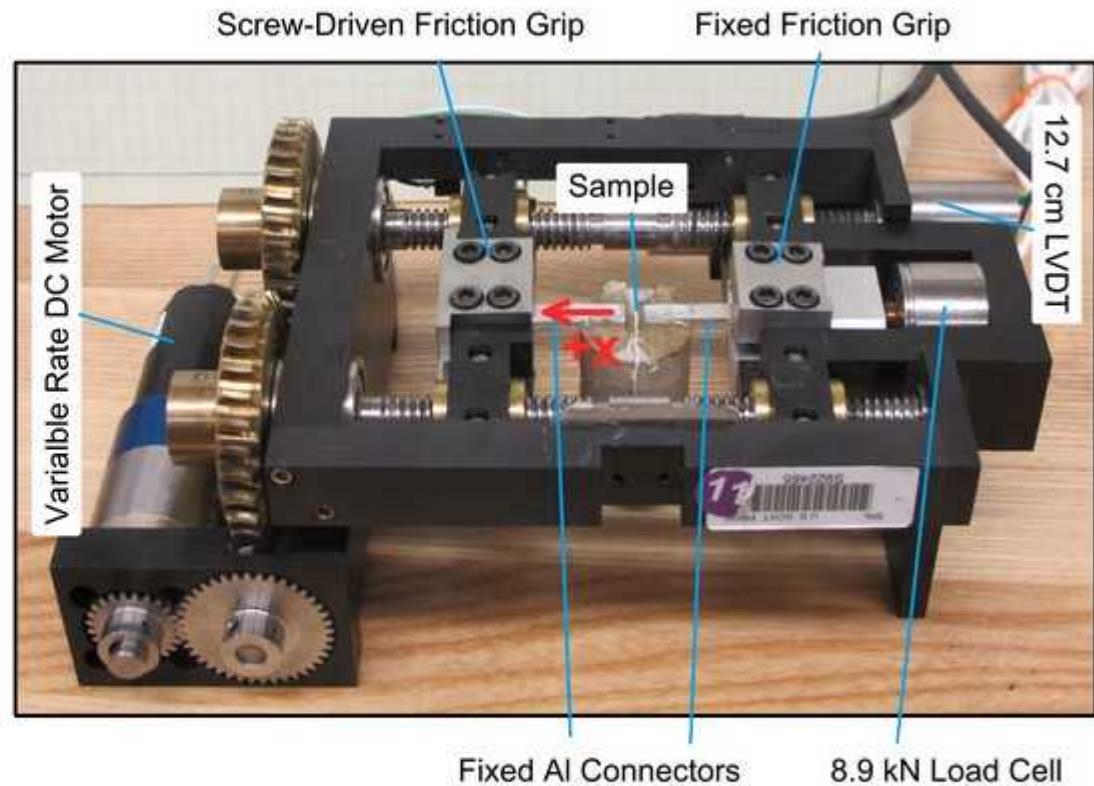
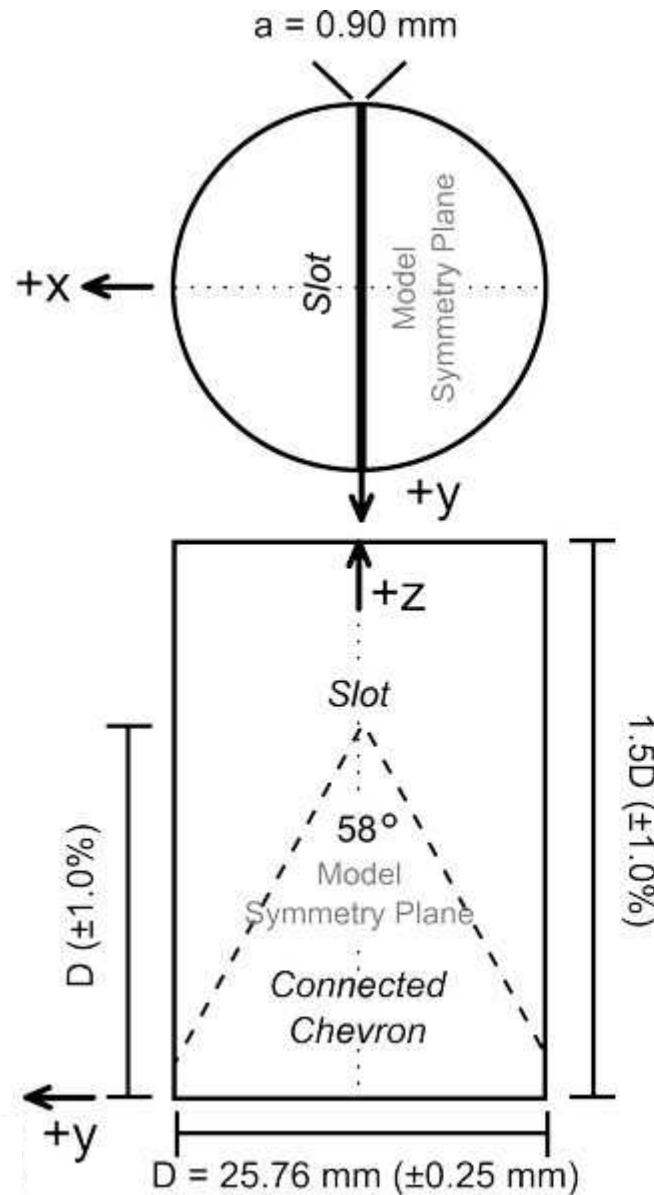
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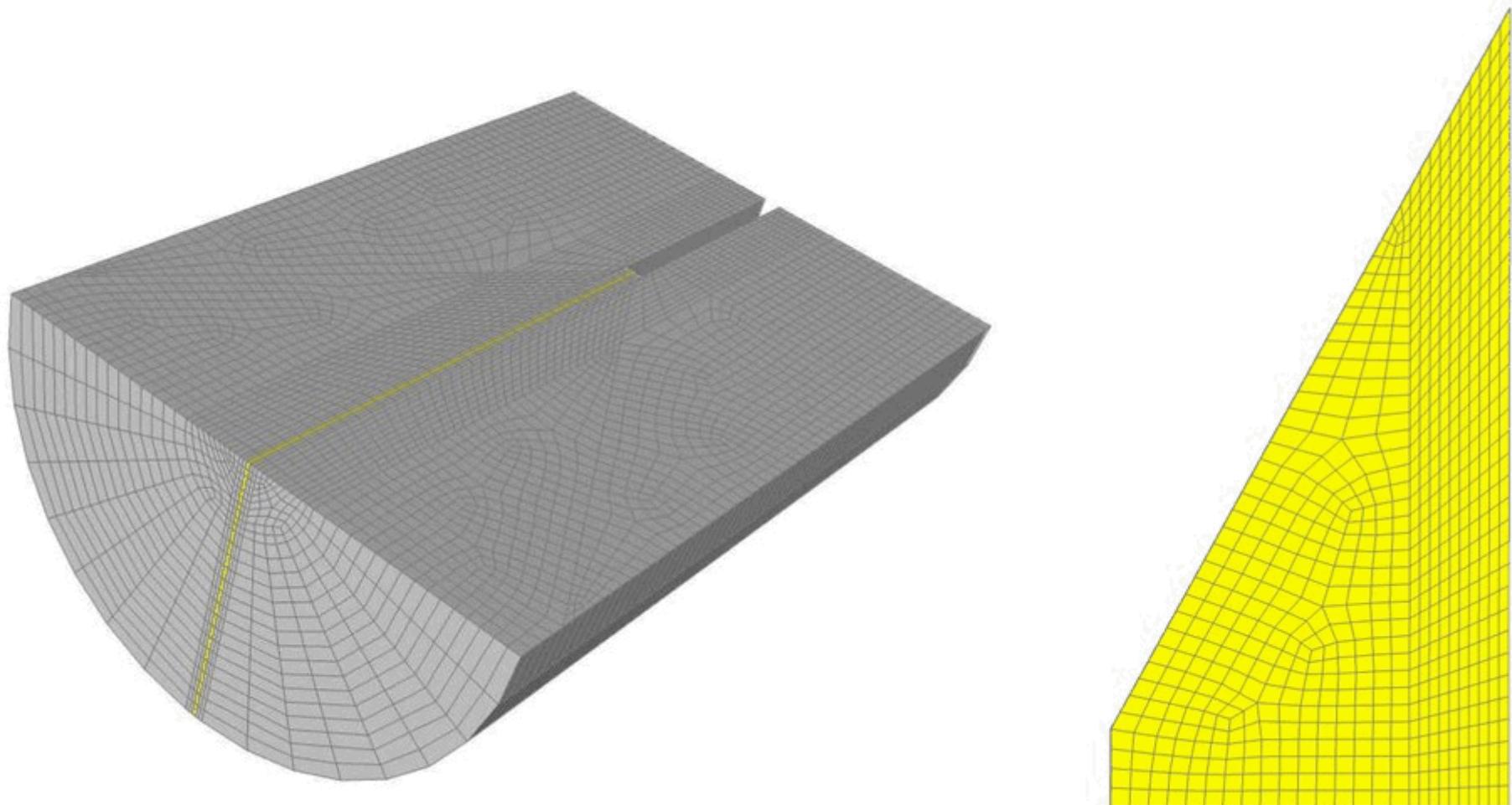
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Short-Rod Tests and Geometry



Short-Rod Mesh



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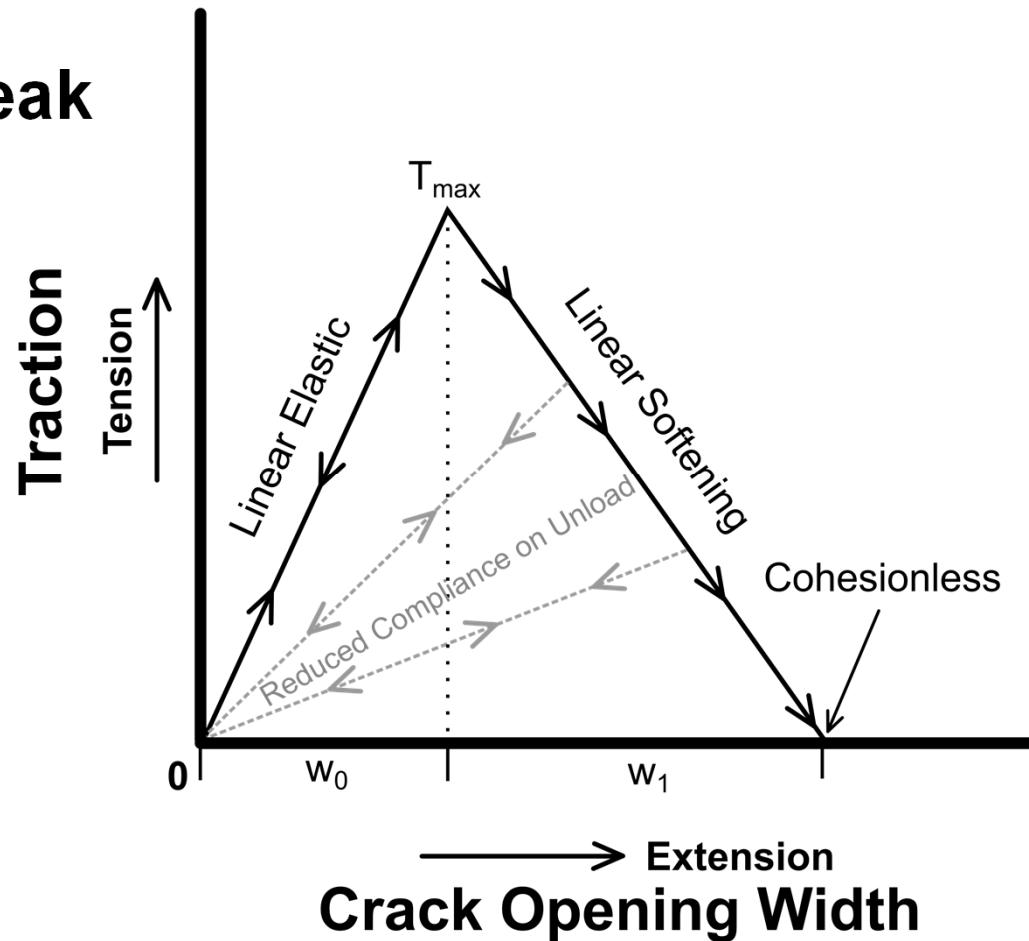
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Calibration Strategy

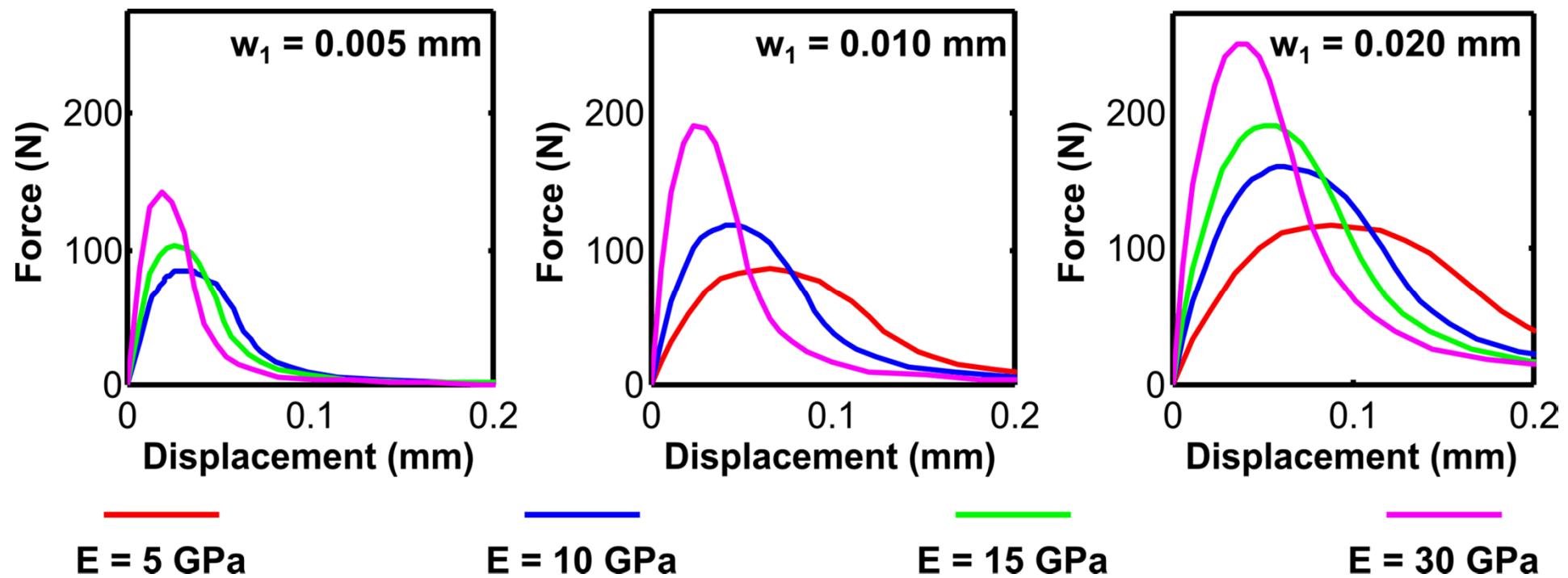
Fix $\sigma_t = 5.9$ MPa from Brazil tests.

Begin with $E=39$ GPa from UCS tests, vary to calibrate elastic response.

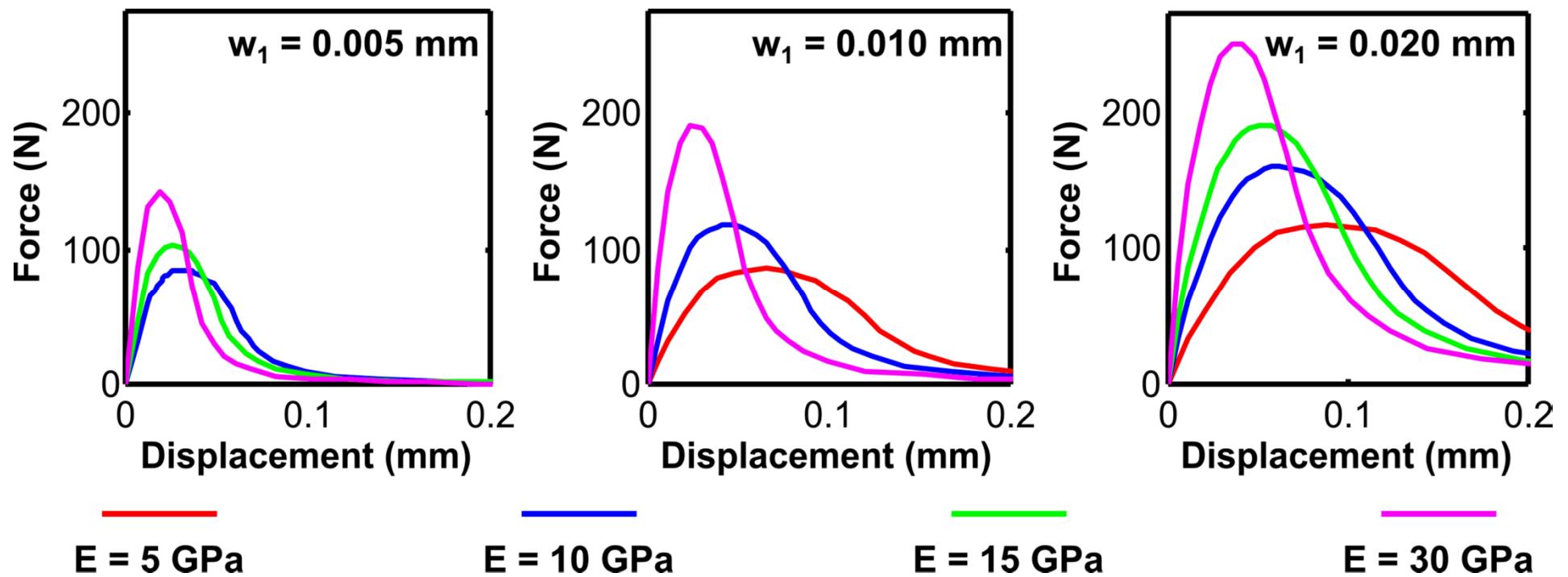
Vary w_1 to match peak and softening.



Parameters and Sensitivity



Parameters and Sensitivity

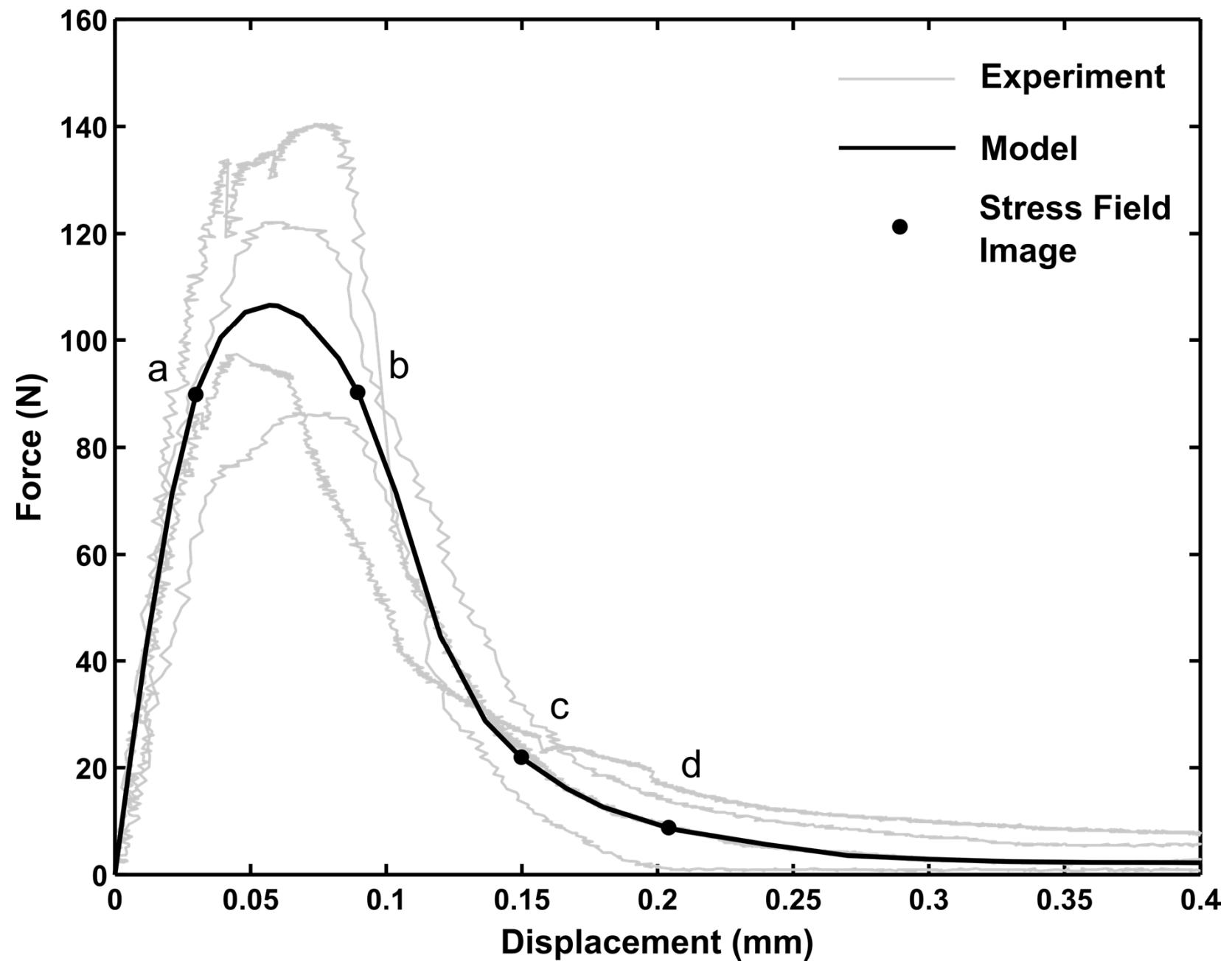


$\sigma_t = 5.9 \text{ MPa}$ fixed.

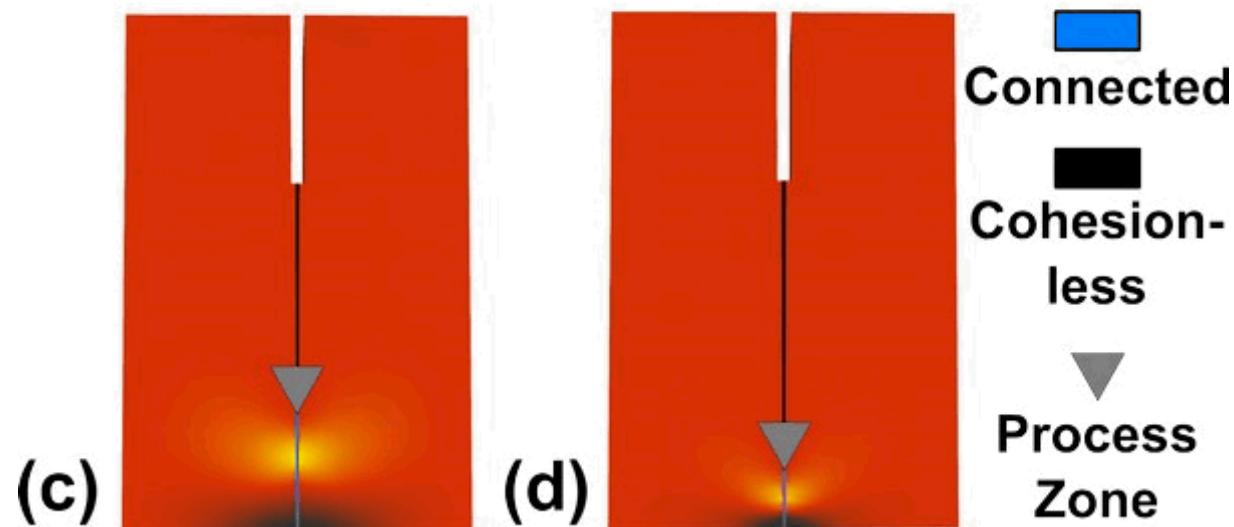
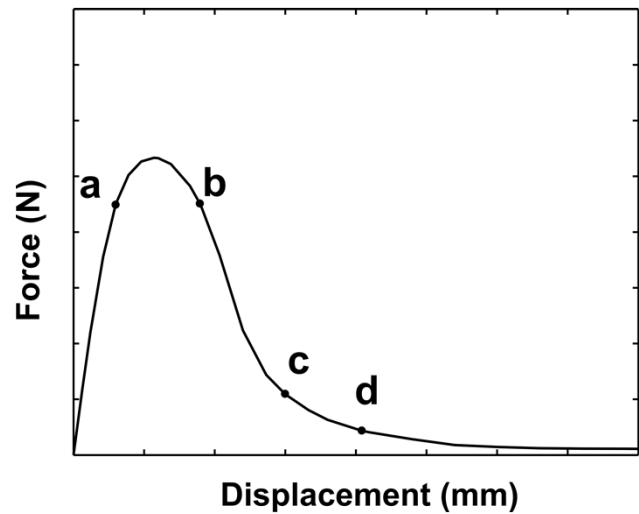
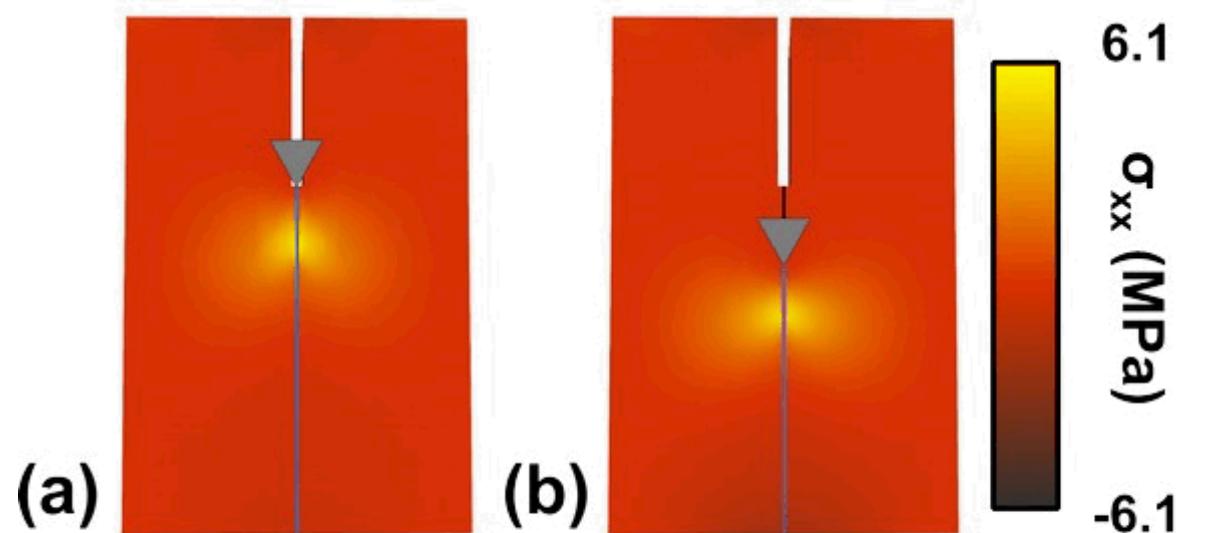
$E = 7.0 \text{ GPa}$

$w_1 = 0.0115 \text{ mm}$

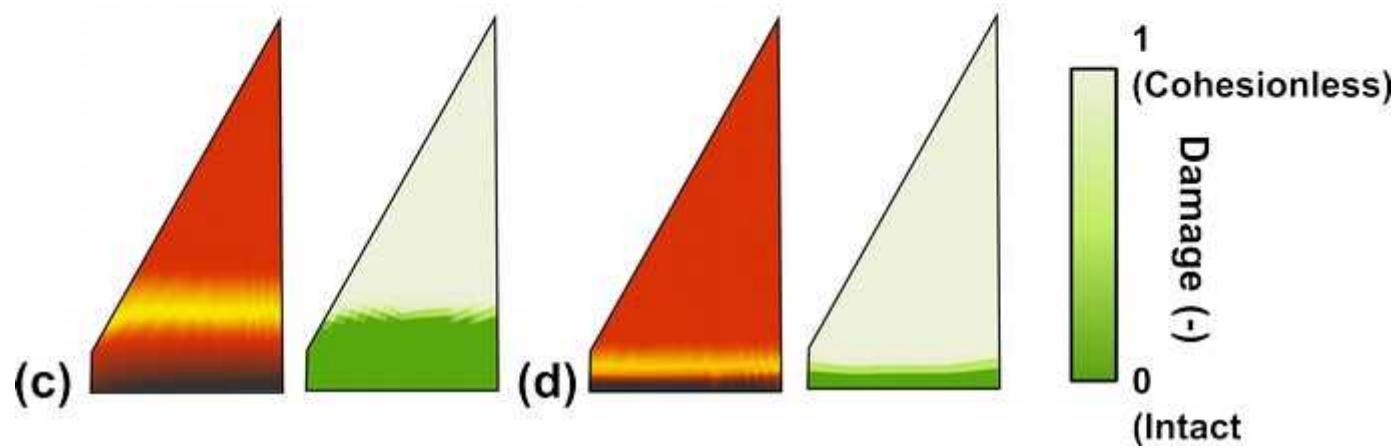
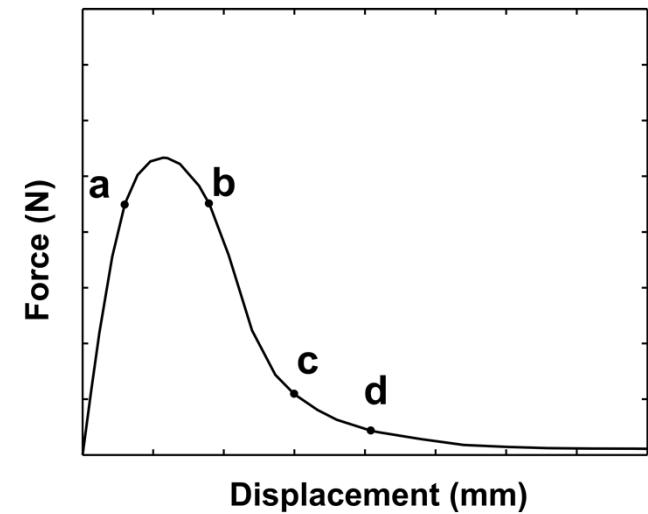
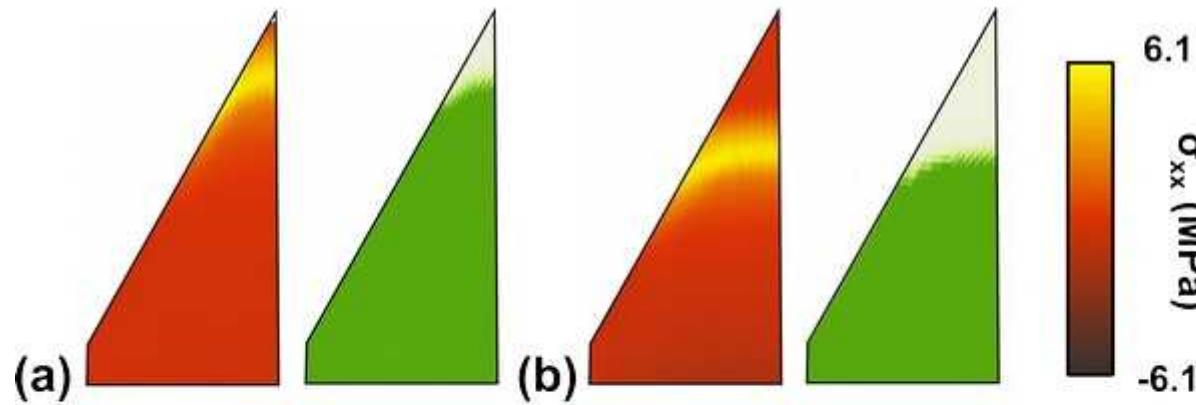
Calibration Results



Calibration Results

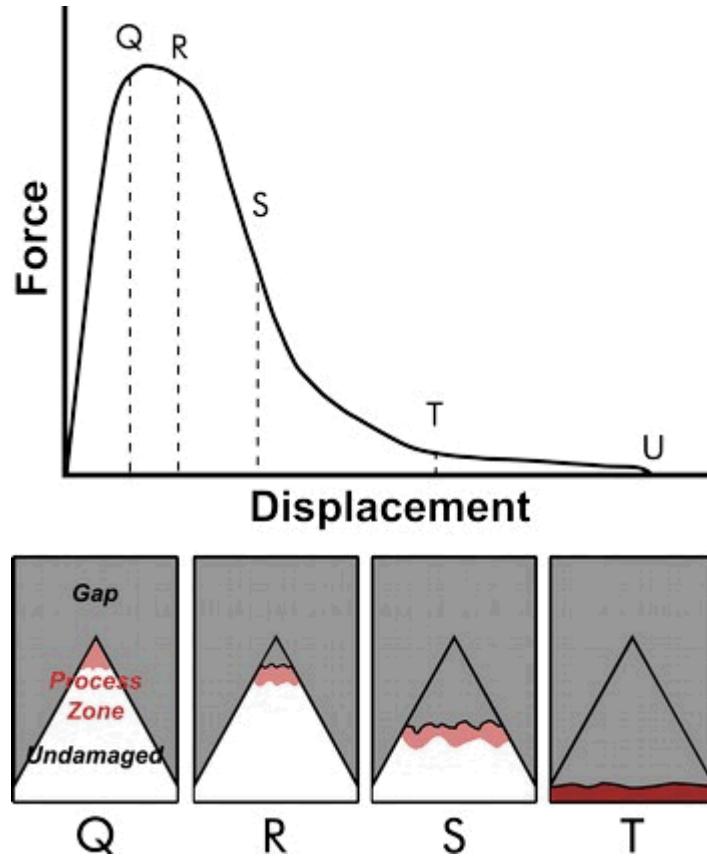


Calibration Results



Process Cartoon

Short-Rod



Calibration Summary

Cohesive fracture model can be calibrated to match elastic loading, yield, peak and **softening behavior** by

Fixing maximum tensile stress with Brazil tests.
Varying E and w_1 in order to calibrate.

Qualitative model fracture propagation similar to observed fracture propagation.

Matching softening behavior uncommon in other test geometries. May imply test geometry 'best at' separating Mode 1 behavior.

Large difference in elastic properties ($E = 7$ GPa in tension vs. $E = 39$ GPa in compression).

Calibration and Confirmation Outline

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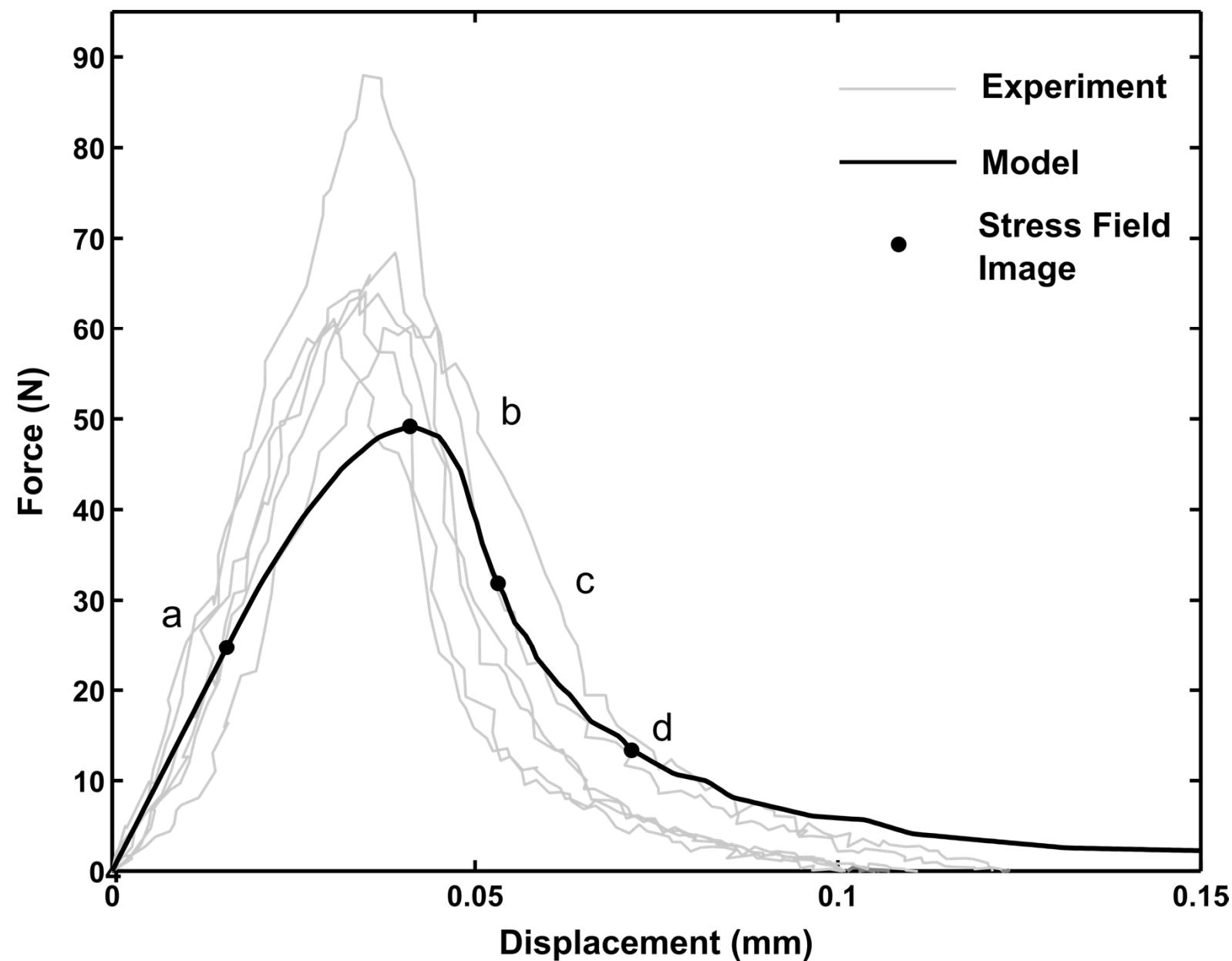
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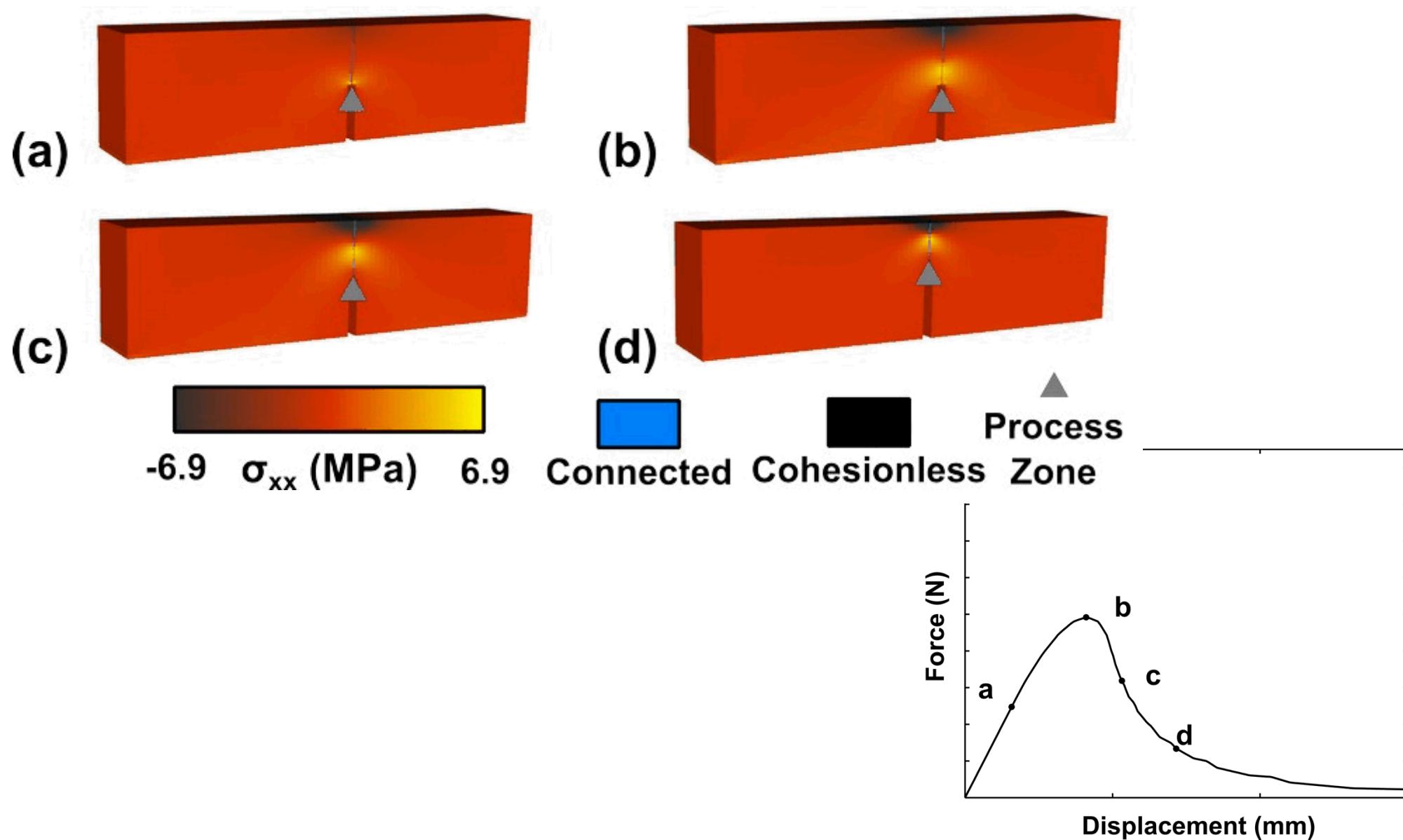
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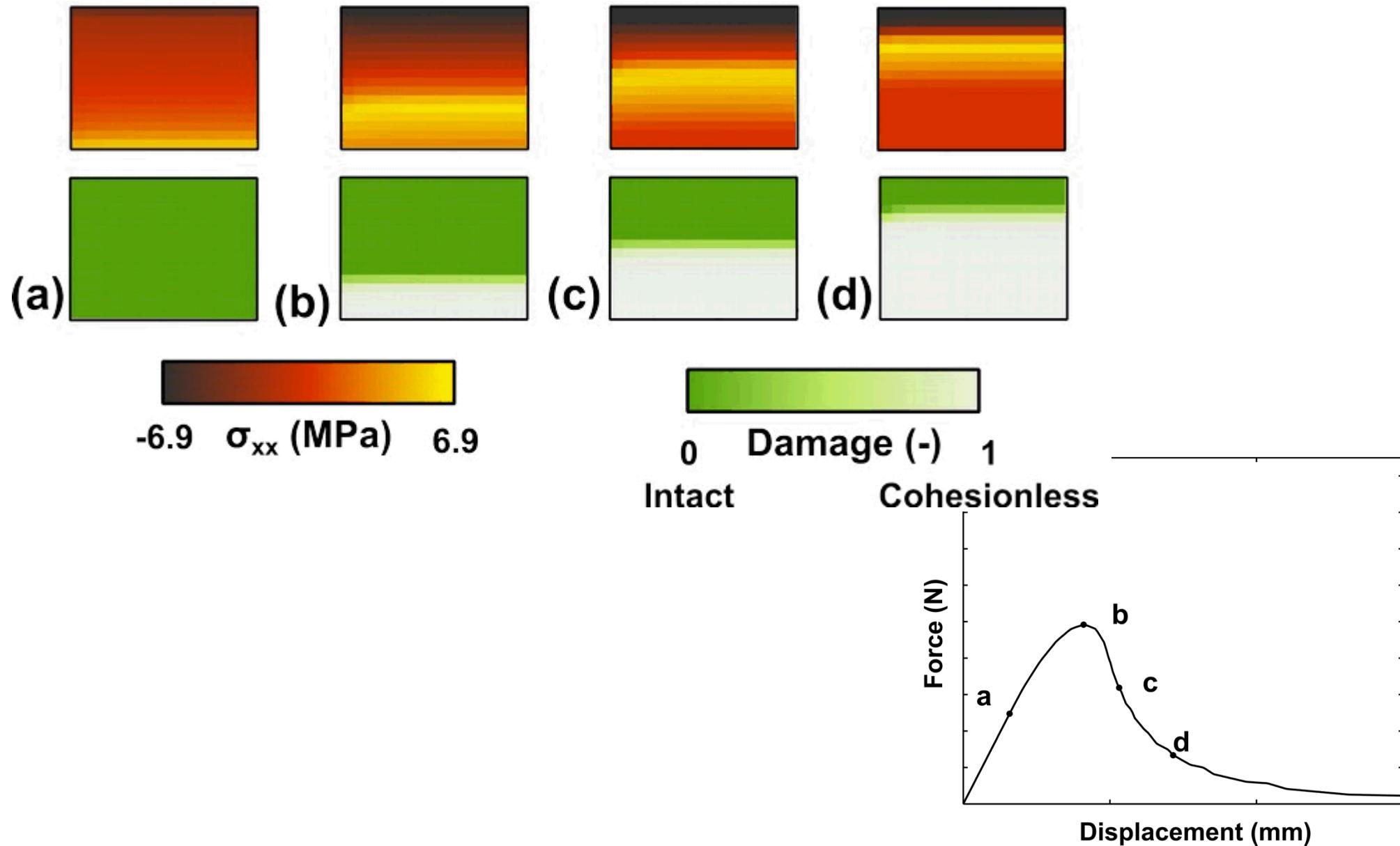
Confirmation Results



Confirmation Results

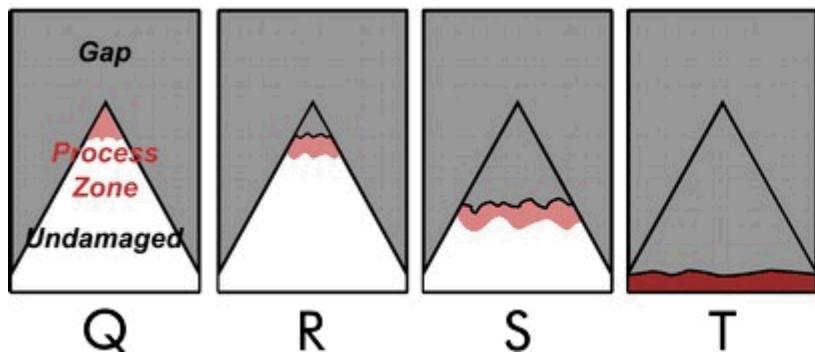
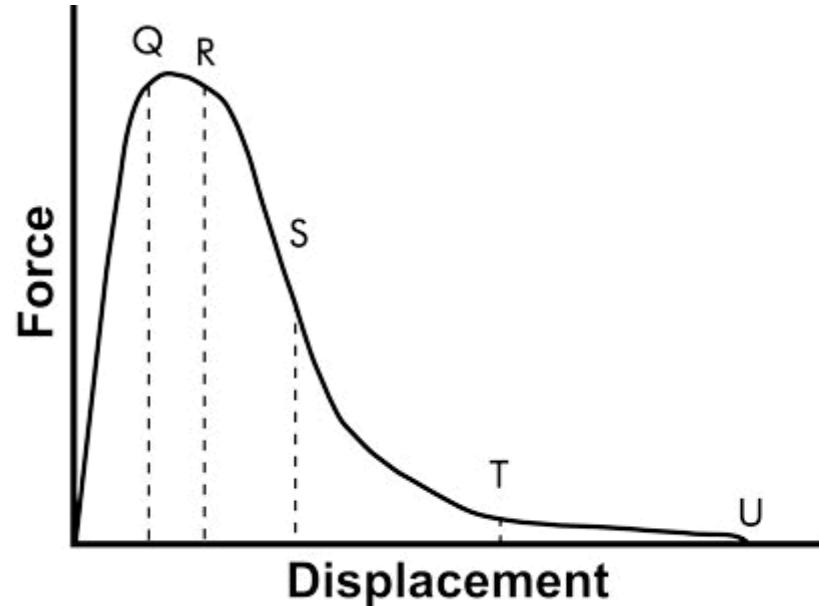


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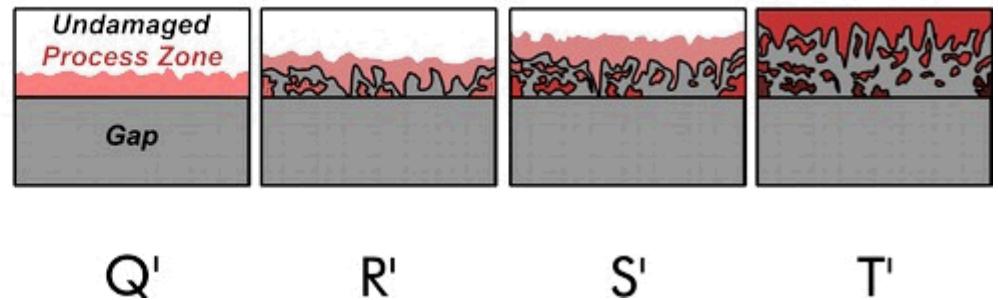
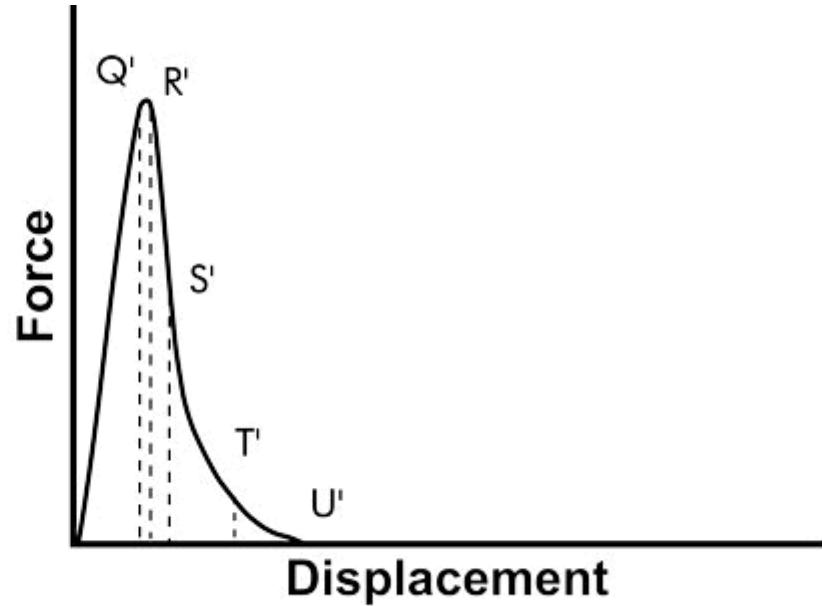


Process Cartoon

Short-Rod



N3PB



Confirmation Summary

Calibrated cohesive fracture model fell within uncertainty for peak stress and initial softening.

N3PB model initial elastic response 'softer' than measured.

N3PB response showed yielding pre-peak not observed.

N3PB model does not accurately depict large-displacement behavior.

Qualitative diffuse fracture pattern does not match modeled fracture propagation pattern.

More volume immediately in compression and likely predominant shear failures in fracture both control change in response with geometry.

Conclusions

Cohesive elements can, within $O(1)$, be used to predict crack propagation in different geometries.

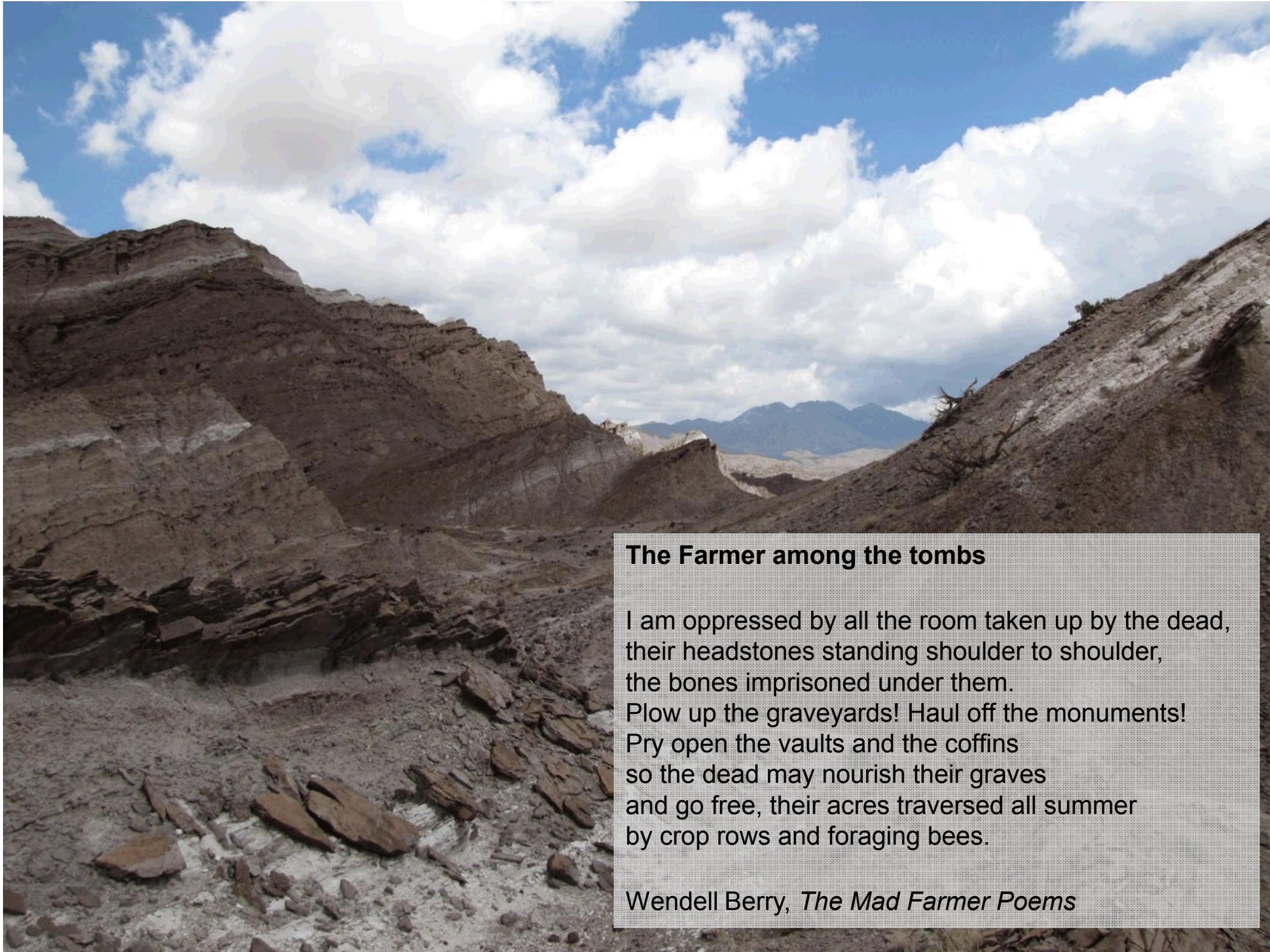
Varying stress state in Indiana limestone significantly affects effective elastic properties between short-rod and 3pb simulations.

Short-rod provides a more accurate Mode 1 fracture geometry than N3PB.

Bulk plasticity or microcracking along edge of fracture needed to portray propagation.

Cohesive crack mimics tail in short-rod, not N3PB.

'Cold-runs' of 3pb fall within uncertainty, but display yielding before any of experiments.



The Farmer among the tombs

I am oppressed by all the room taken up by the dead,
their headstones standing shoulder to shoulder,
the bones imprisoned under them.
Ply up the graveyards! Haul off the monuments!
Pry open the vaults and the coffins
so the dead may nourish their graves
and go free, their acres traversed all summer
by crop rows and foraging bees.

Wendell Berry, *The Mad Farmer Poems*