

# Modified 3D-helix-like instability structure for imploding Z-pinch liners that are premagnetized with a uniform axial field

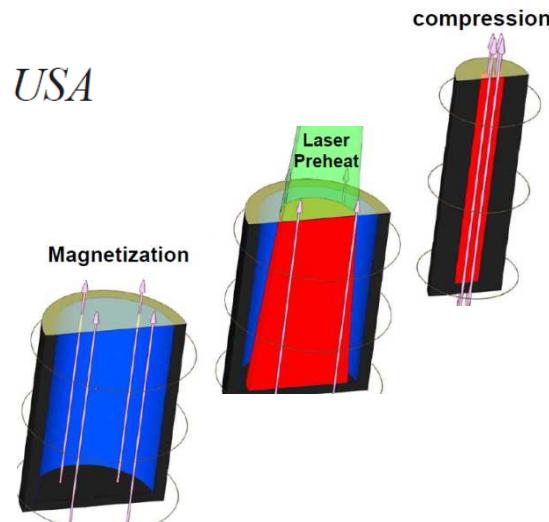
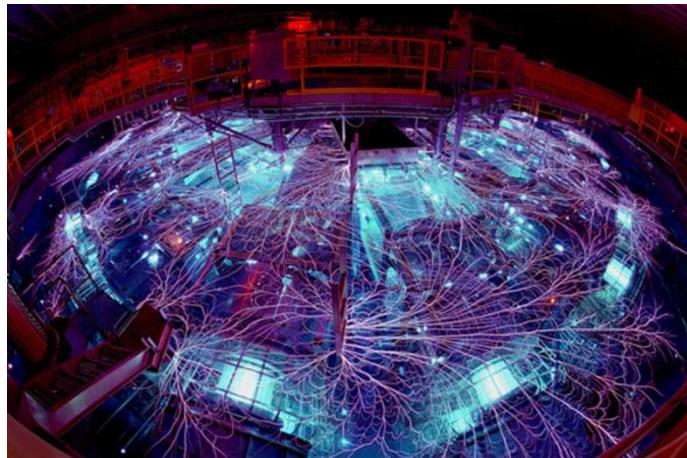
SAND2014-16754PE

T.J. Awe, C.A. Jennings, R.D. McBride, M.E. Cuneo, D.C. Lamppa, M.R. Martin, D.C. Rovang,  
D.B. Sinars, S.A. Slutz, A.C. Owen, M.R. Gomez, S.B. Hansen, E.C. Harding, M.C. Herrmann, M.C.  
Jones, P.F. Knapp, J.L. McKenney, K.J. Peterson, G.K. Robertson, G.A. Rochau, M.E. Savage, P.F.  
Schmit, A.B. Sefkow, W.A. Stygar, R.A. Vesey, E.P. Yu

*Sandia National Laboratories, Albuquerque, New Mexico 87185 USA*

K. Tomlinson, D.G. Schroen

*General Atomics, San Diego, California 92121 USA*



**SAND Number:XX-XX**



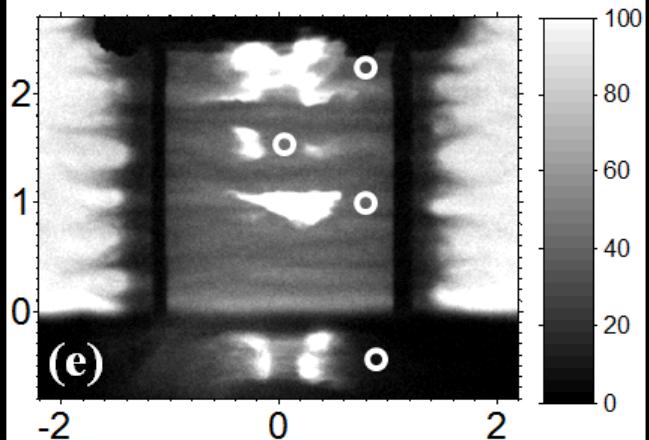
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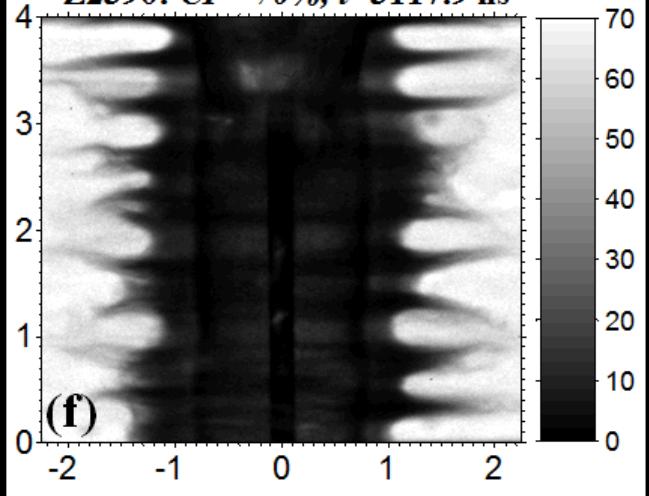
# —Presentation Topic—

$B_{z,0} = 0 \text{ T}$

Z2465:  $CP = 50\%$ ,  $t = 3093.2 \text{ ns}$



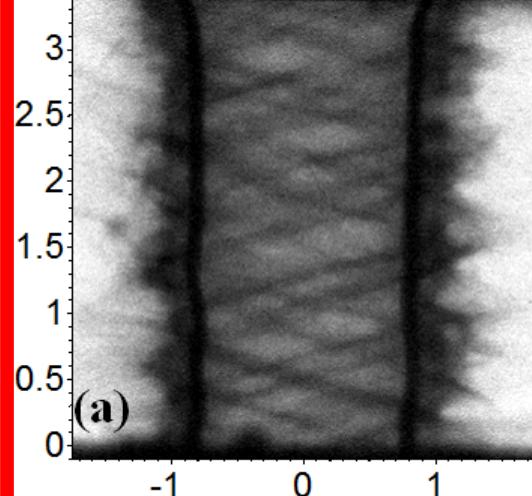
Z2390:  $CP = 70\%$ ,  $t = 3117.9 \text{ ns}$



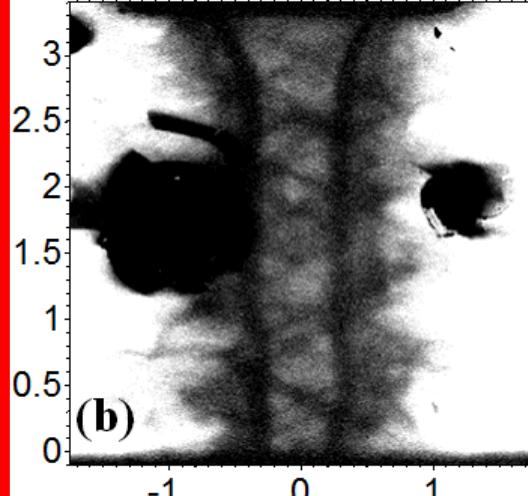
Azimuthally correlated MRT

$B_{z,0} = 7 \text{ T}$

Z2480-t1:  $CP = 63\%$ ,  $t = 3094.3 \text{ ns}$



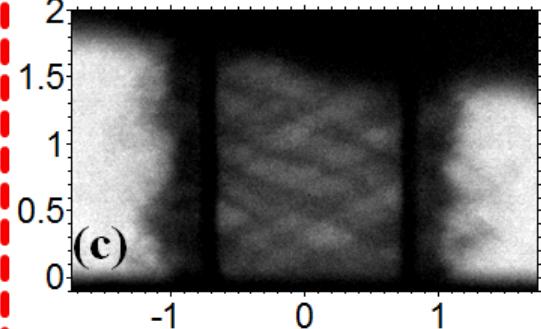
Z2480-t2:  $CP = 84\%$ ,  $t = 3100.3 \text{ ns}$



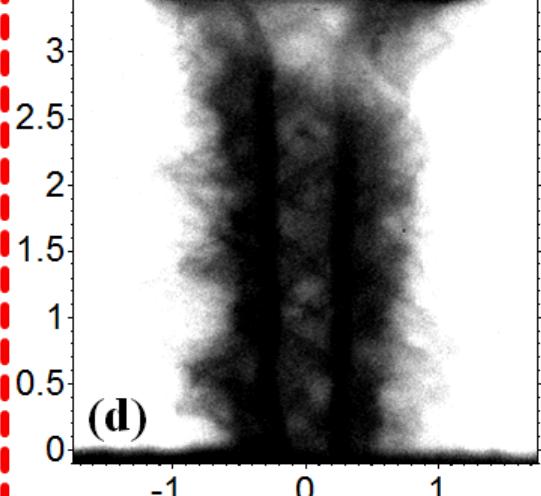
Helix-like instability structure

$B_{z,0} = 10 \text{ T}$

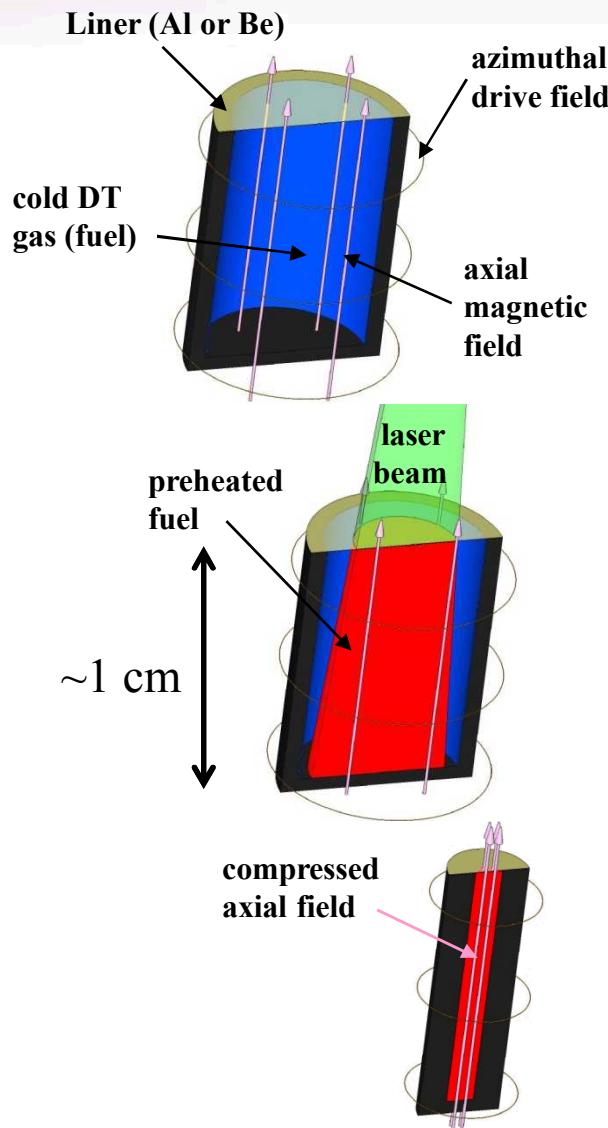
Z2481-t1:  $CP = 65\%$ ,  $t = 3094.8 \text{ ns}$



Z2481-t2:  $CP = 86\%$ ,  $t = 3100.8 \text{ ns}$

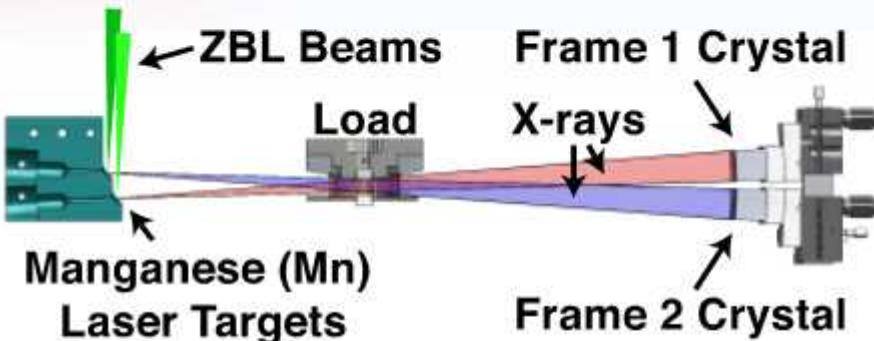


# MagLIF: Fuel pre-heat & magnetization allow relatively slow implosions to achieve significant fusion yield

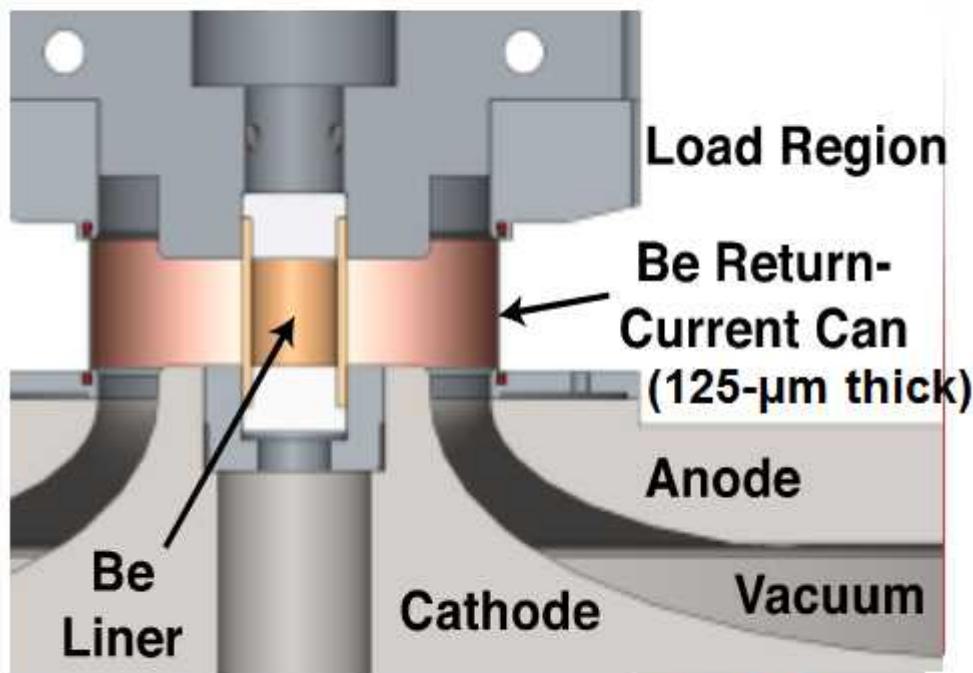
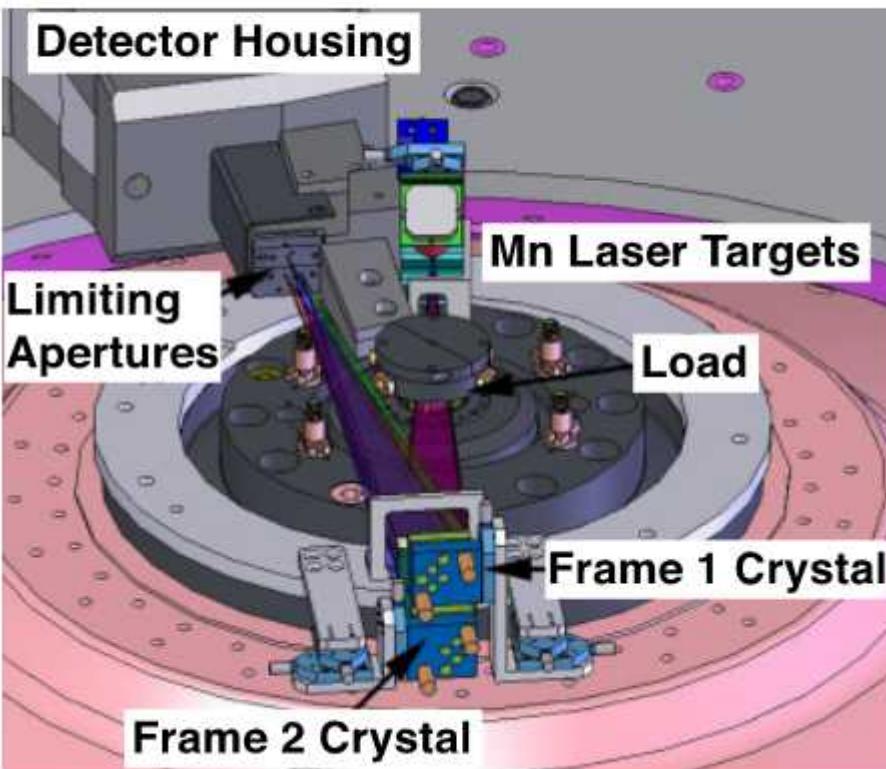


- An initial 30 T axial magnetic field is applied
  - Compressed field inhibits thermal conduction losses
  - May help stabilize implosion at late times
- During the ~100 ns implosion, the fuel is heated using the Z-Beamlet laser (about 6 kJ in designs)
  - Preheating to ~300 eV reduces the compression needed to obtain fusion temperatures to 23 on Z
  - Preheating reduces the implosion velocity needed to ~100 km/s, allowing us to use thick liners that are more robust against instabilities
- ~50-250 kJ energy in fuel; 0.2-1.4% of capacitor bank
- Stagnation pressure required is ~5 Gbar
- Gain = 1 may be possible on Z using DT (fusion yield = energy into fusion fuel, also called “scientific breakeven”)  
Early experiments would use DD fuel

Presentation focuses on liner dynamics; primary diagnostic is two-frame monochromatic ( $6151 \pm 0.5$  eV) radiography\*



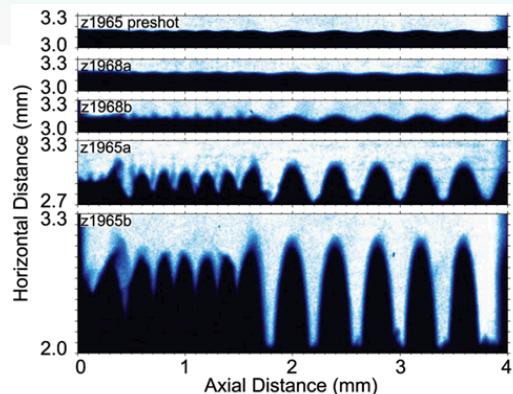
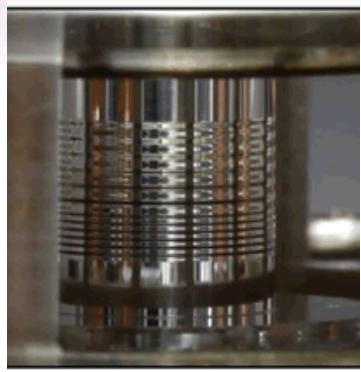
- Spherically-bent quartz crystals (2243)
- 15 micron resolution (edge-spread)
- We can see through imploding beryllium (not so for aluminum and other higher-opacity materials).



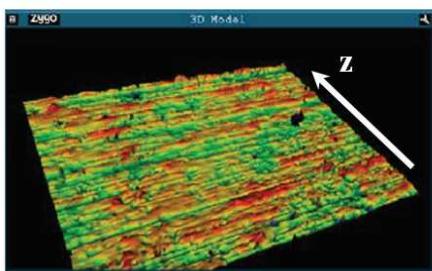
\* G. R. Bennett *et al.*, RSI (2008).



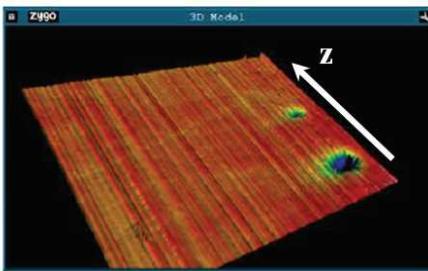
# Experiments have focused on developing predictive capability of instability growth of imploding liners



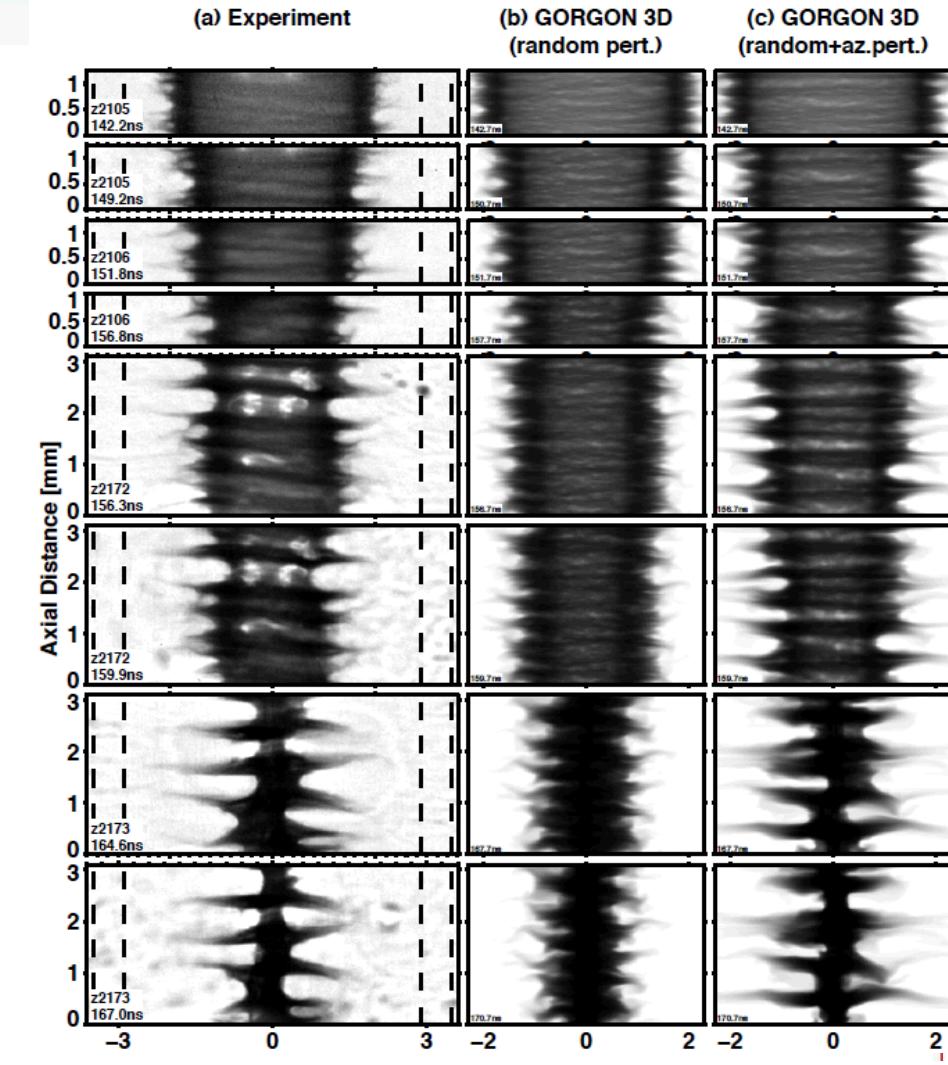
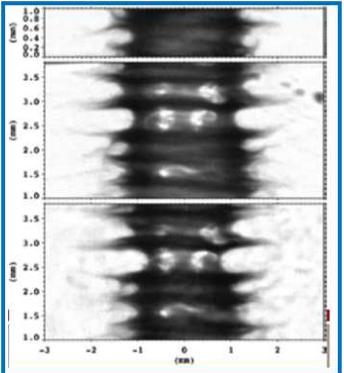
D.B. Sinars *et al.*, Phys. Rev. Lett. 105, 185001 (2010)  
D.B. Sinars, Invited Presentation, 2010 APS-DPP



Standard process  $\rightarrow$  50 nm RMS



Axially polished  $\rightarrow$  50 nm RMS



R.D. McBride *et al.*, PRL 109, 135004 (2012)  
R.D. McBride, Invited Presentation, 2012 APS-DPP

# MagLIF Helmholtz-like coil pair first fielded on Z imploding-liner experiments in February of 2013

## Field strength requirements:

- 10 T seed field with full diagnostic access
- 30 T coils will have limited diagnostic access

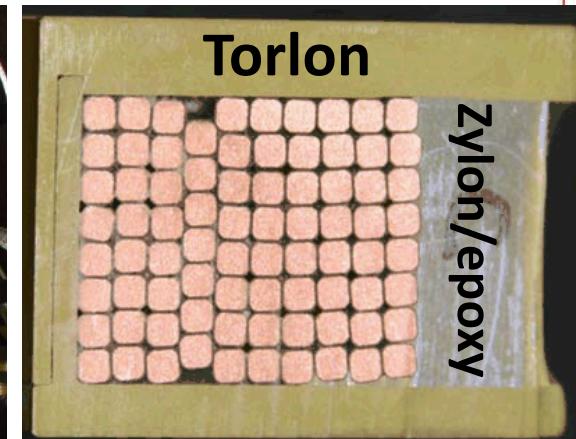
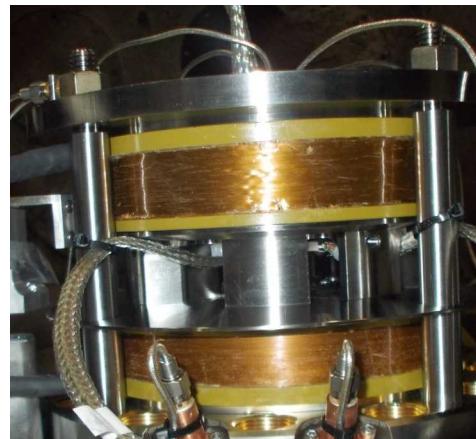
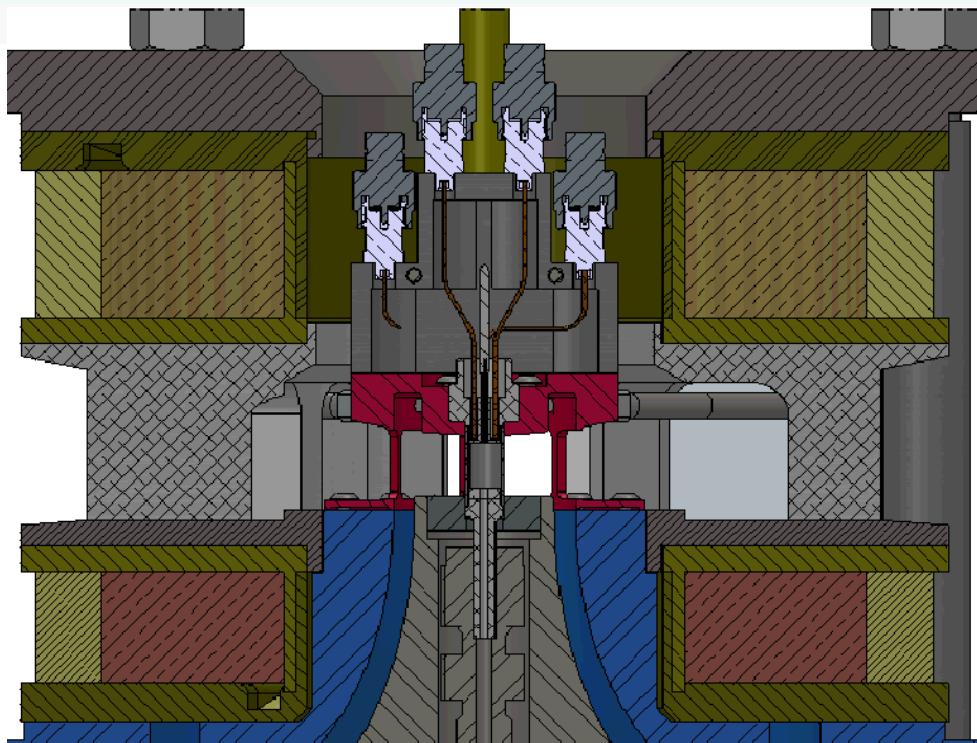
## Capacitor bank

2x4 mF,  $V_{max} = 15$  kV

Use: 4 mF, 7 kV, 8.6 kA, 10 T

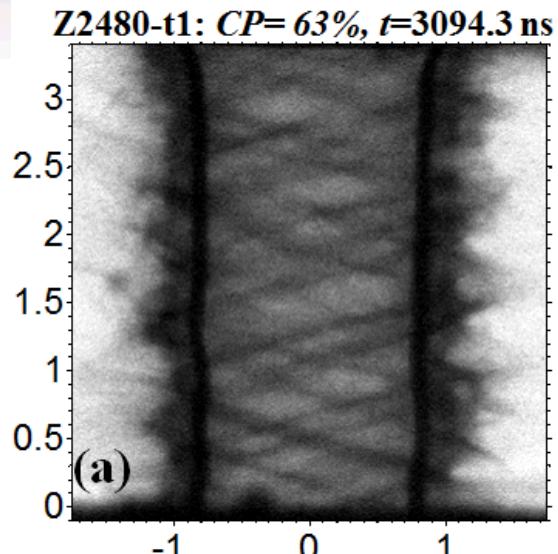
## Pulse length requirement:

- Coil:  $\sim 1$  mH
- Must not crush or buckle target or hardware
- Fully magnetize liner/fuel with uniform field
- 3.5 ms risetime used

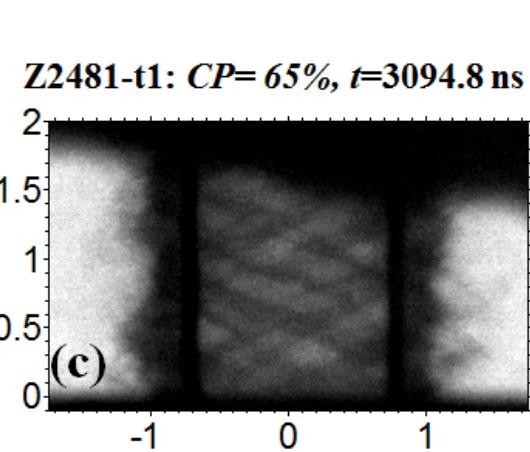


# Helix-like instabilities develop on premagnetized liners

$B_{z,0} = 7 \text{ T}$

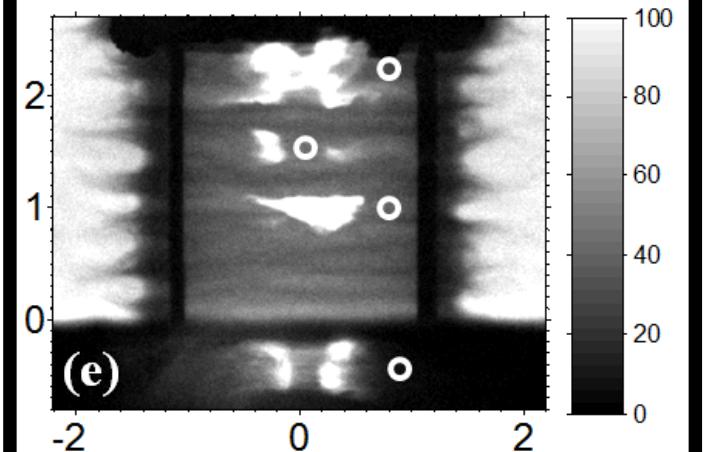


$B_{z,0} = 10 \text{ T}$

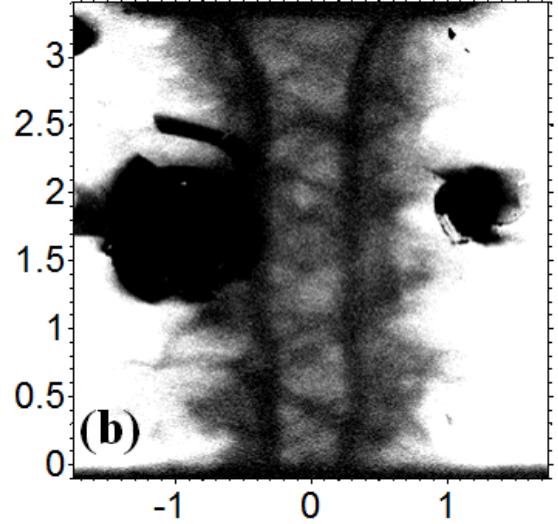


$B_{z,0} = 0 \text{ T}$

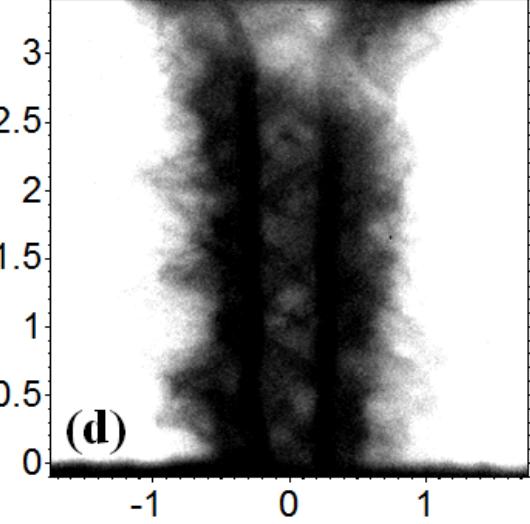
Z2465:  $CP = 50\%$ ,  $t = 3093.2 \text{ ns}$



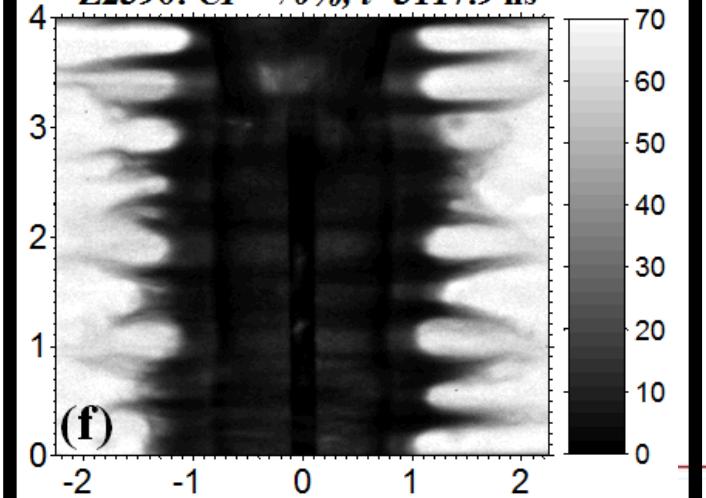
Z2480-t2:  $CP = 84\%$ ,  $t = 3100.3 \text{ ns}$



Z2481-t2:  $CP = 86\%$ ,  $t = 3100.8 \text{ ns}$



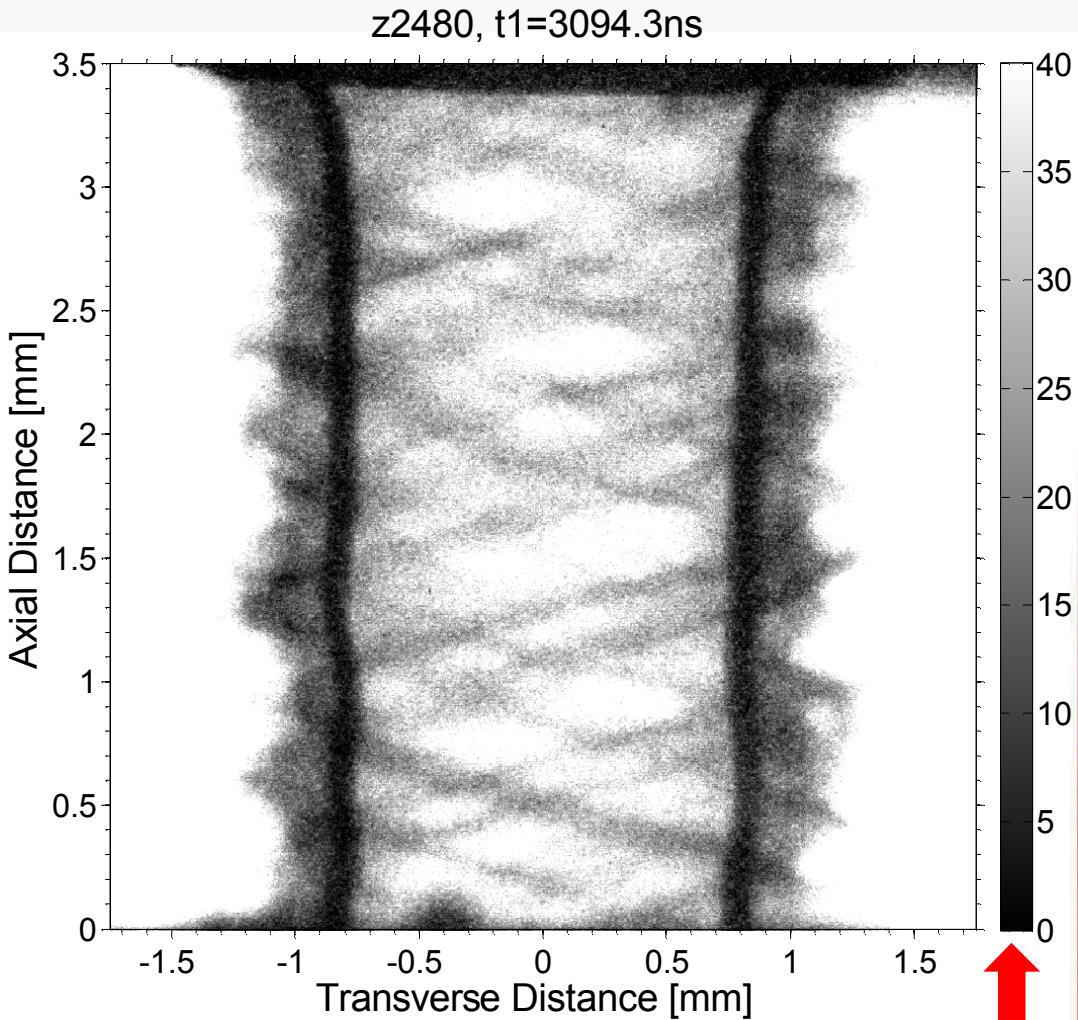
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# Well-connected helical structures are easily traced through multiple cycles

High-density structures are at large angle to the z axis

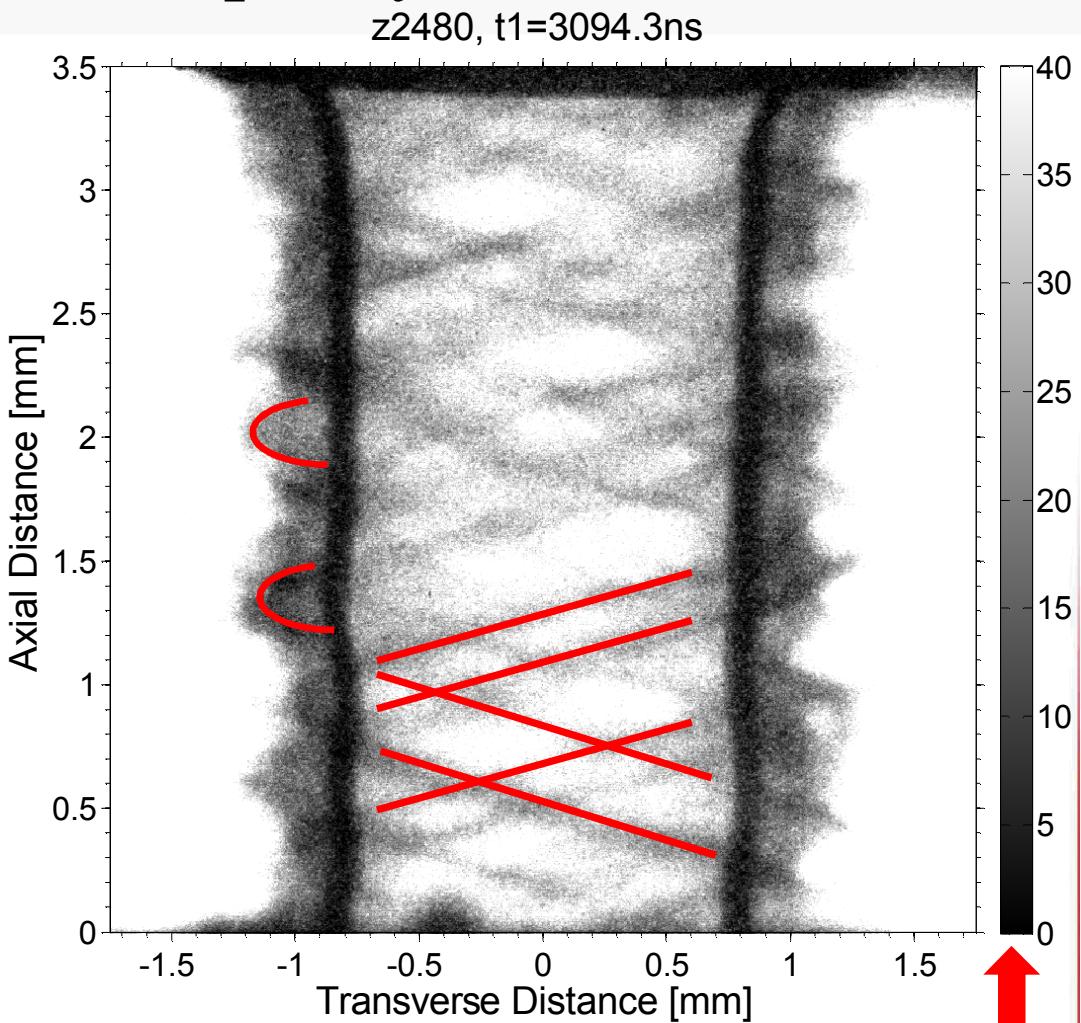
Penetrating radiography “sees” structures at “front” and “back” of liner, so structures with positive and negative slope are observe. This results in the observed cross-hatched pattern



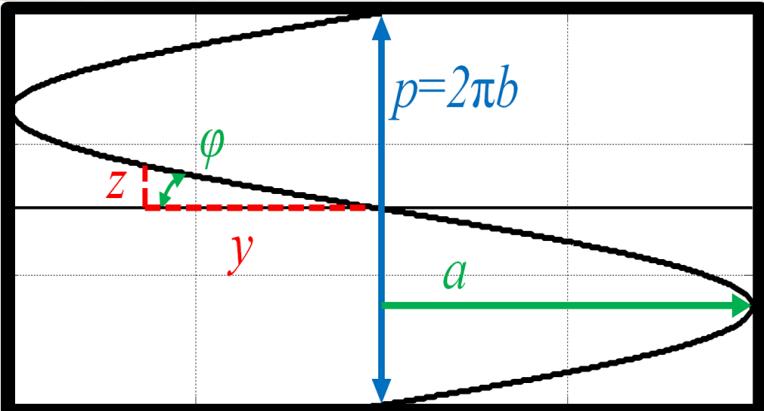
# Well-connected helical structures are easily traced through multiple cycles

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# A simple cylindrical helix model fits the data well



## *Cylindrical helix model*

$$y(\theta) = a \cdot \sin(\theta)$$

$$z(\theta) = p \cdot \theta / 2\pi$$

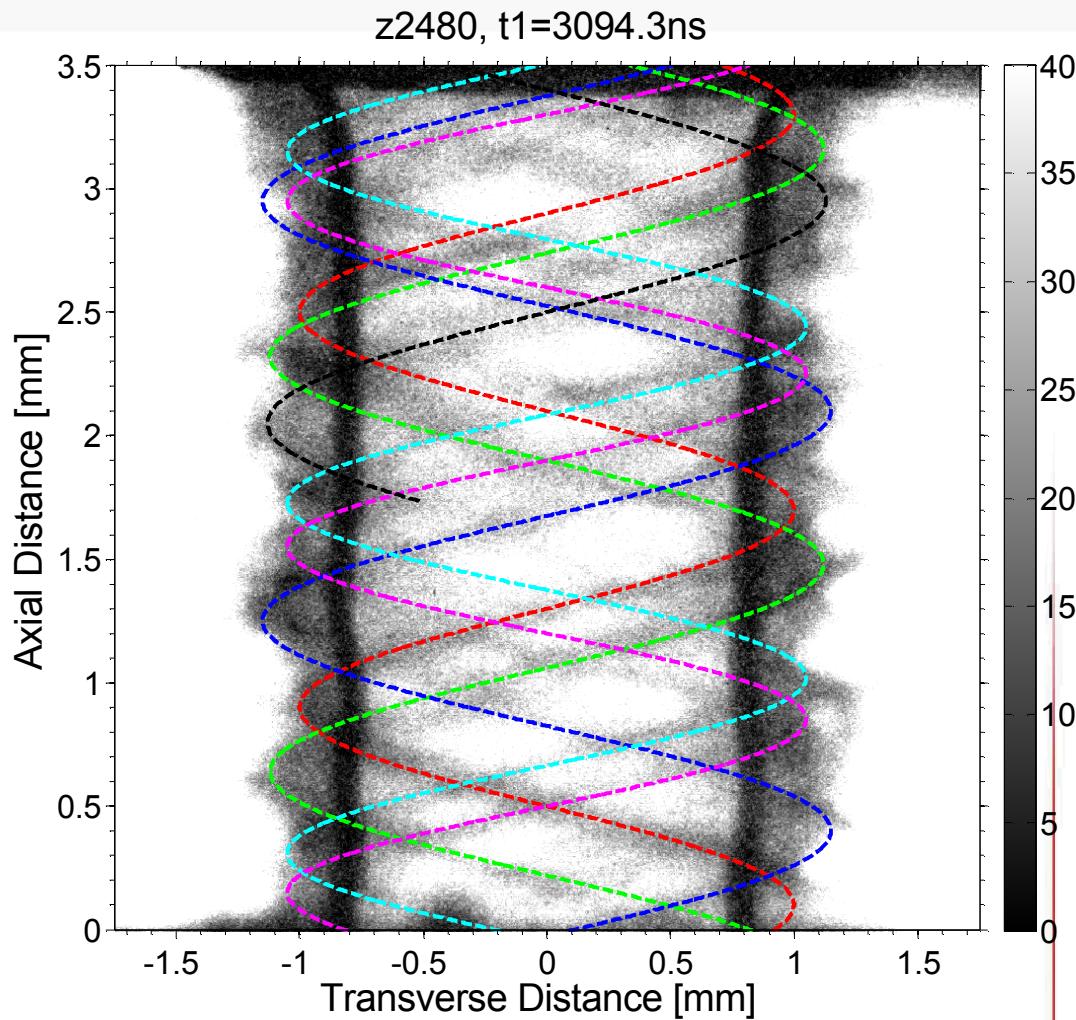
$a$  = radius

$p$  = pitch

## “pitch angle”

$$\varphi = \tan^{-1}(z/y)$$

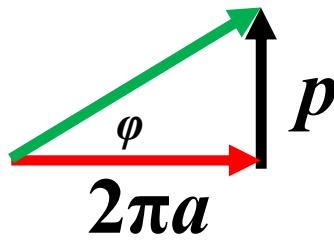
$$\varphi \approx \tan^{-1}(p/2\pi a)$$



$$a_{\text{avg}} = 1.07 \text{ mm}$$

$$p_{\text{avg}} = 1.56 \text{ mm}$$

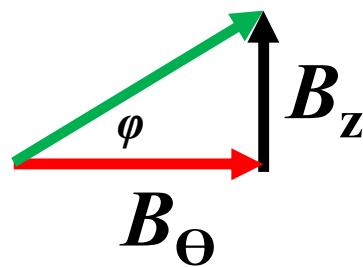
$B_z + B_\Theta$  magnetic field streamlines follow a helical path along a cylindrical surface



$$p = 2\pi a \tan(\phi)$$

-or-

$$\phi = \tan^{-1}(p/2\pi a)$$



$$B_z/B_\Theta = \tan(\phi_B)$$

-or-

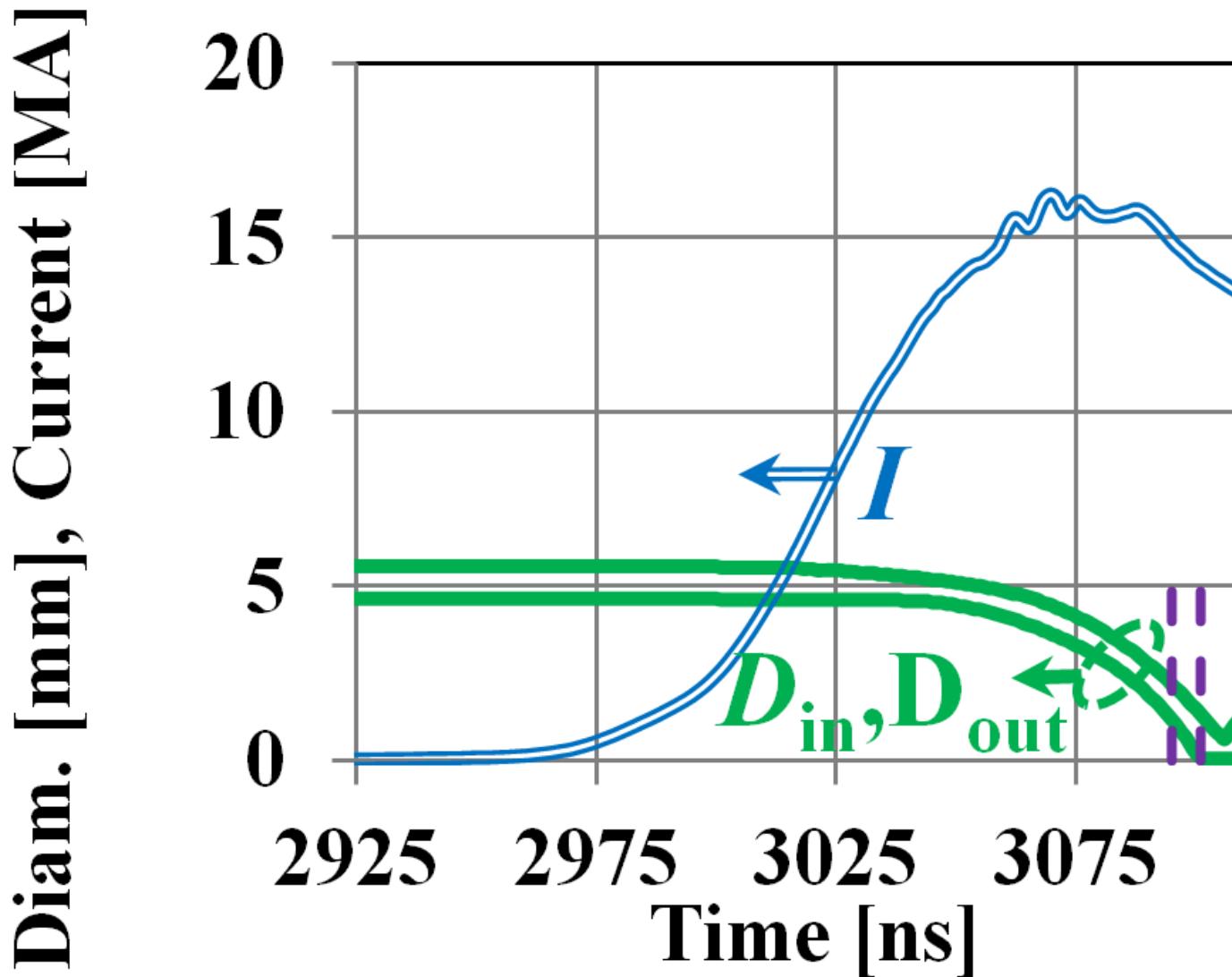
$$\phi_B = \tan^{-1}(B_z/B_\Theta)$$

$$p_B = 2\pi a (B_z/B_\Theta)$$

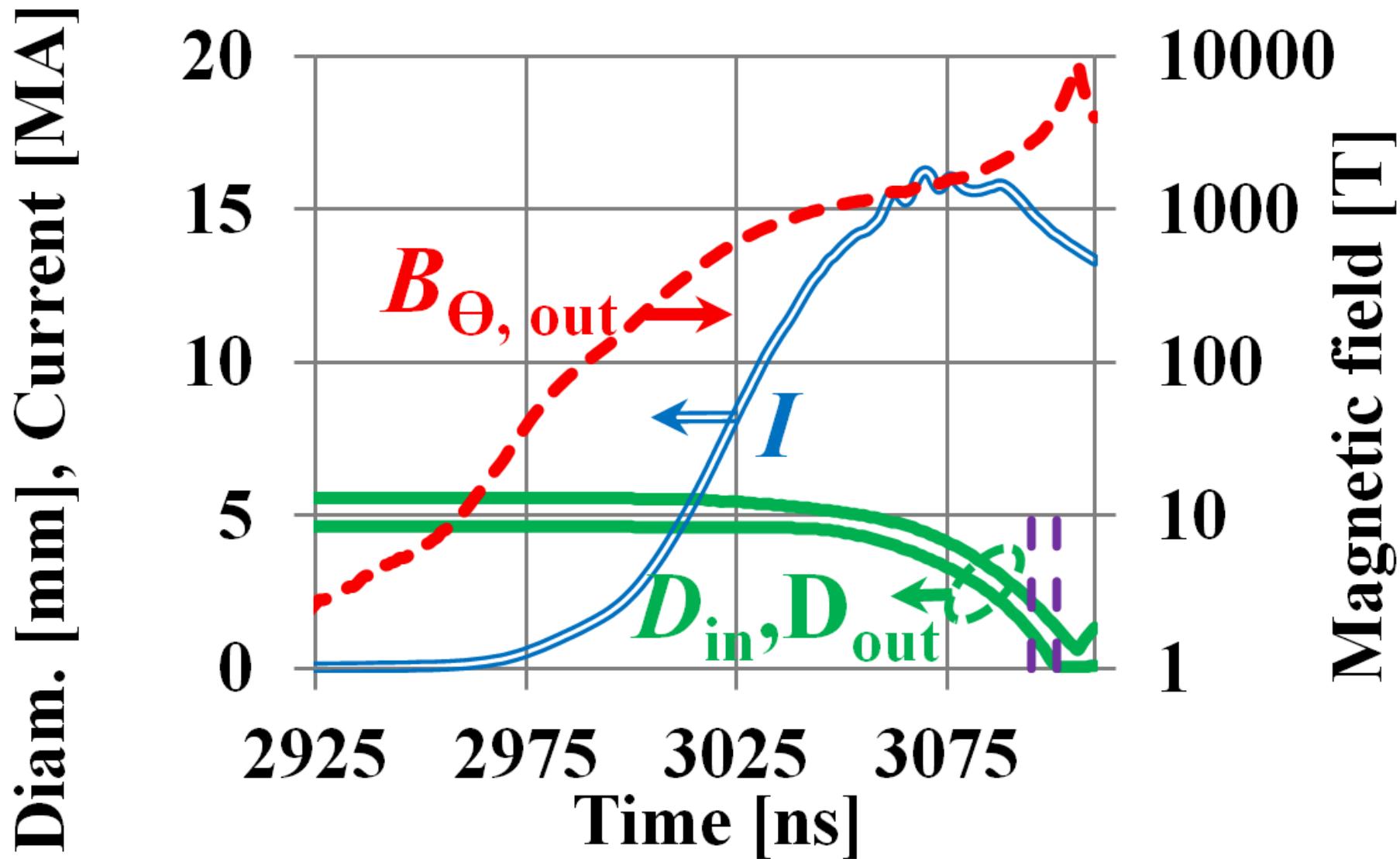
- MRT theory shows that instabilities will have the highest growth rate for  $\mathbf{k} \cdot \mathbf{B} = 0$
- If a helical magnetic field topology can be maintained, helical instability structure is to be expected



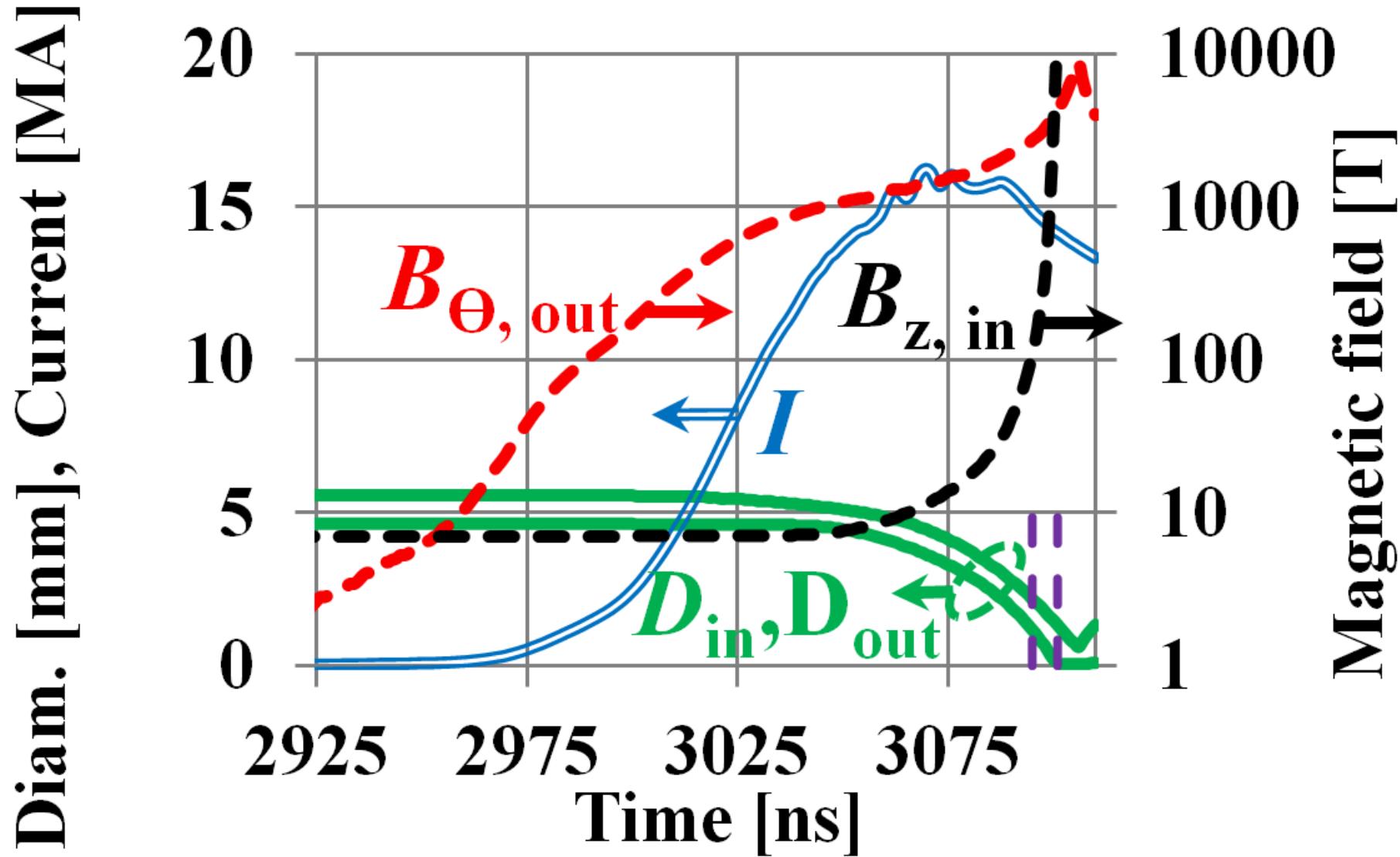
The time-dependent pitch angle of the magnetic field streamline on the liner surface can be estimated



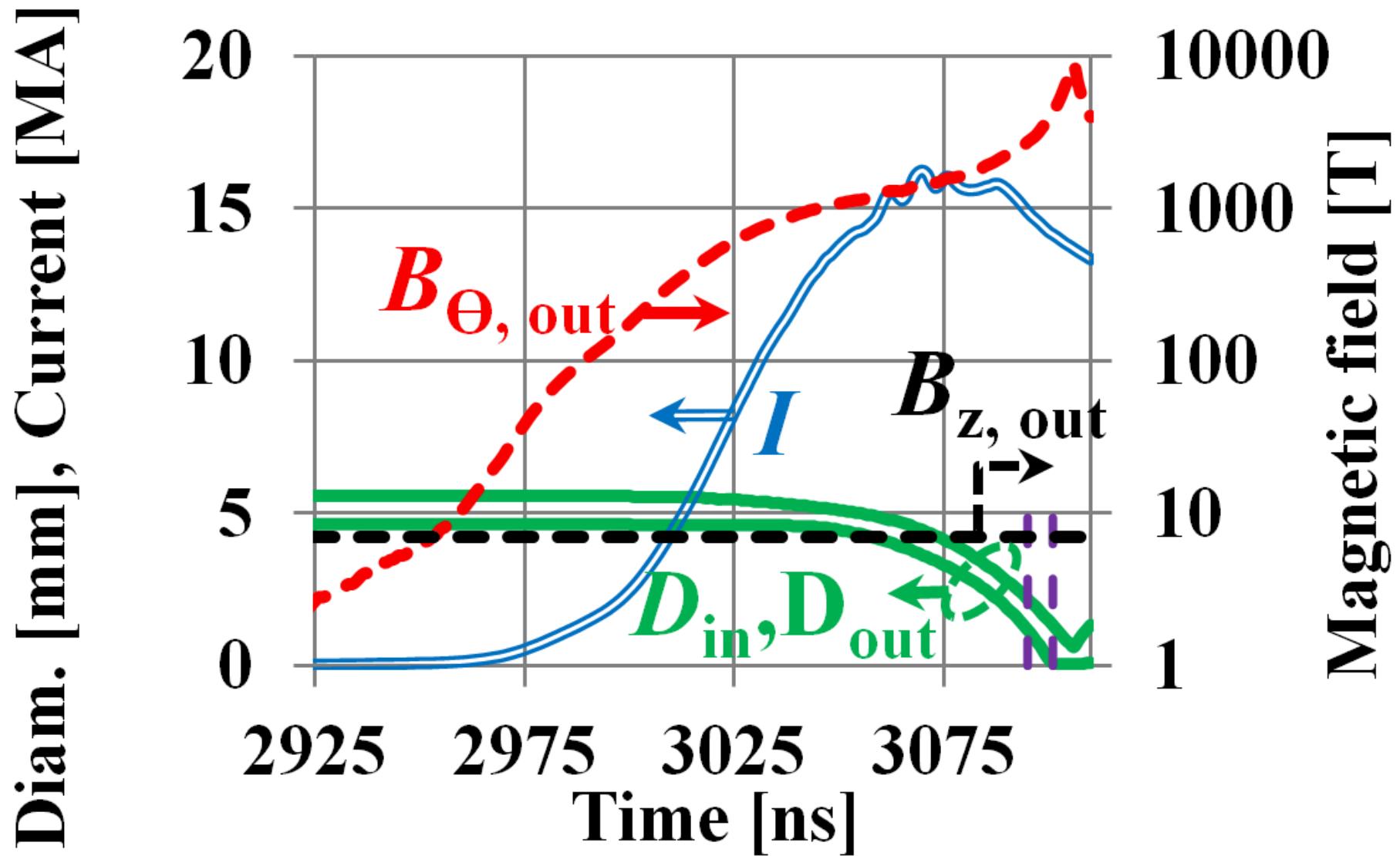
$B_\Theta$  is calculated using the experiment current and GORGON liner trajectory



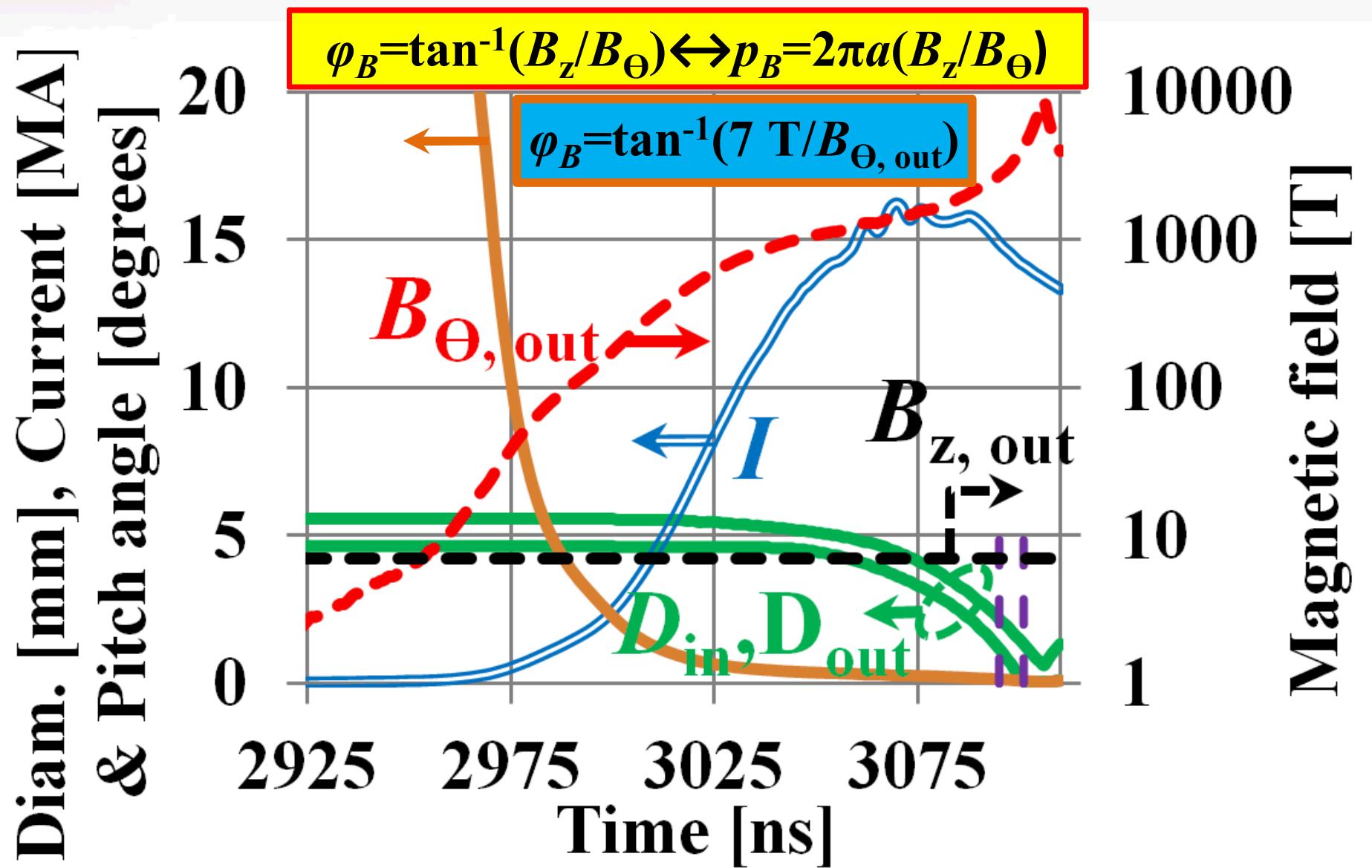
$B_{z, \text{in}}$  is calculated using  $B_{z,0}=7$  T, GORGON liner trajectory, and by assuming perfect flux conservation



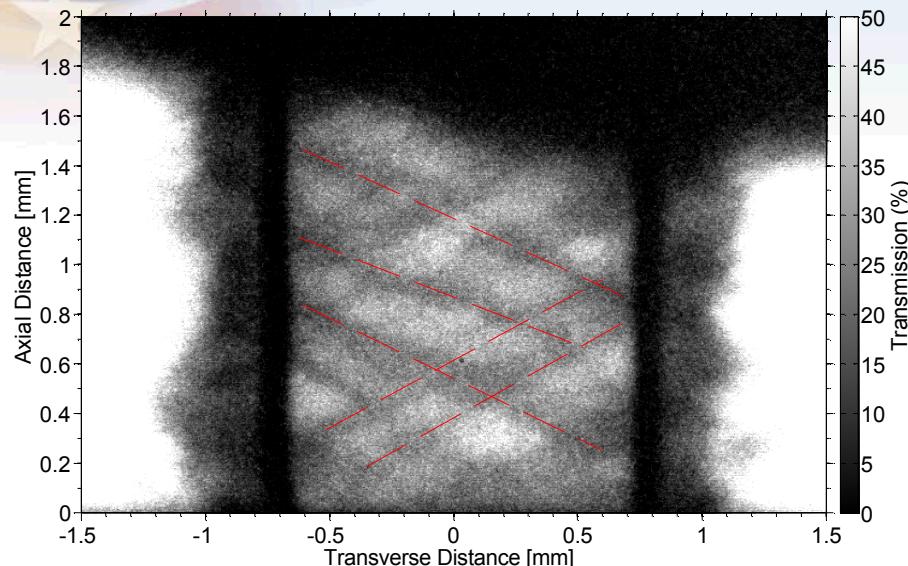
Helical perturbations presumably grow from the liner's surface, so the nearly constant  $B_{z,\text{out}}$  is most pertinent



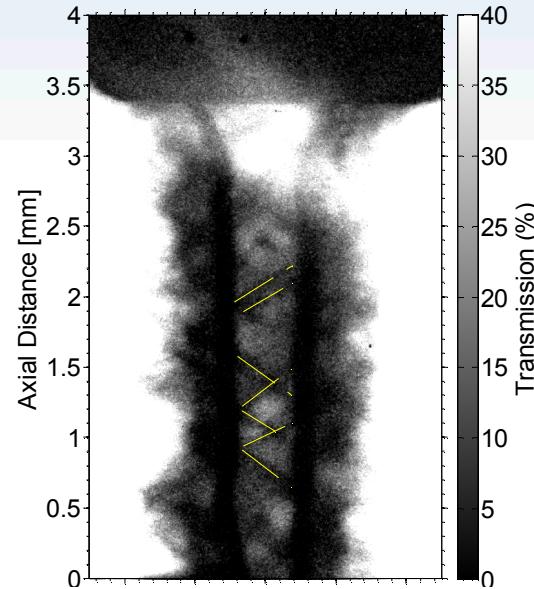
Briefly,  $B_\Theta \approx B_z$  early in the experiment, but presumably  $B_\Theta \gg B_z$  throughout the entire implosion



# The pitch angle, $\varphi$ , can be obtained for all radiographs



$$\varphi_{\text{avg}} = 26^\circ$$



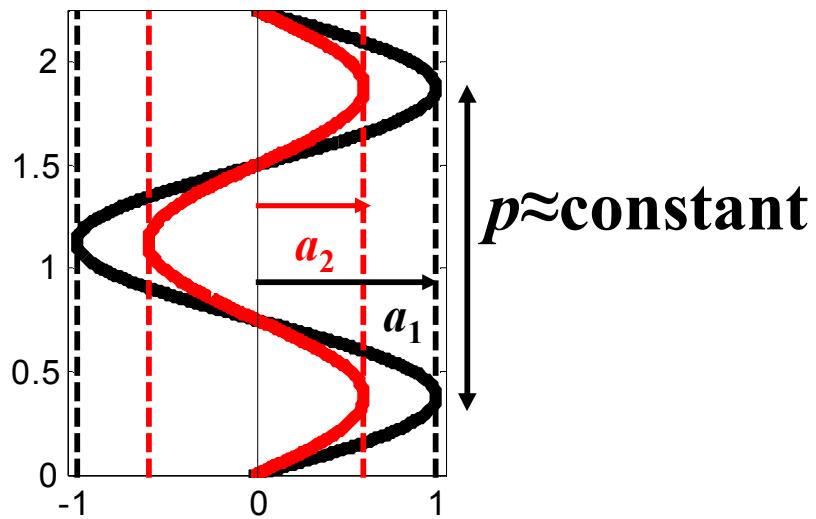
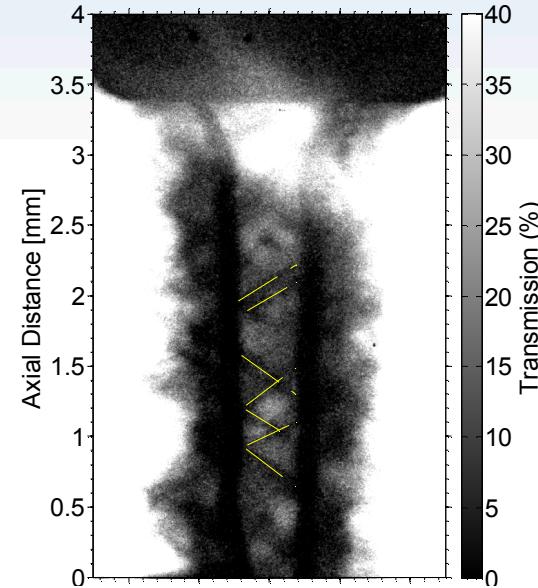
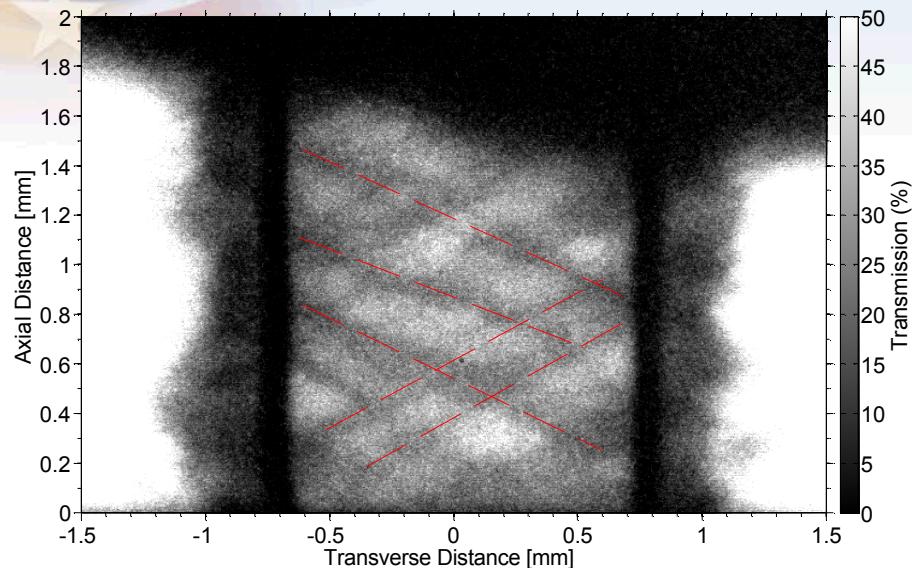
$$\varphi_{\text{avg}} = 33^\circ$$

Radiograph	2480-t1	2480-t2	2481-t1	2481-t2
$B_{z,0}$ [T]	7		10	
Radiograph time [ns]	3094.3	3100.3	3094.8	3100.8
$R_{\text{in,avg.}}(t)$ [ $\mu\text{m}$ ]	$870 \pm 25$	$365 \pm 30$	$810 \pm 30$	$335 \pm 30$
$CR = R_{\text{in,0}} / R_{\text{in}}(t)$	$2.7 \pm 0.1$	$6.4 \pm 0.5$	$2.9 \pm 0.1$	$6.9 \pm 0.6$
# of lines fit	8	8	5	7
$\varphi_{\text{Avg}}$ [deg]	16.4	25.6	25.9	32.9
Std. Dev. [deg]	1.6	1.2	2.9	4.2

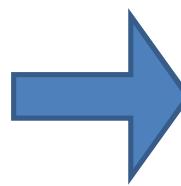
$\varphi_{\text{avg}}$  increases with both  $B_{z,0}$  and liner convergence

Increasing  $\varphi_{\text{avg}} \approx \tan^{-1}(p/2\pi a) \rightarrow$  pitch changes slowly relative to implosion; helices are entrained in liner wall

For constant pitch, the pitch angle will grow large



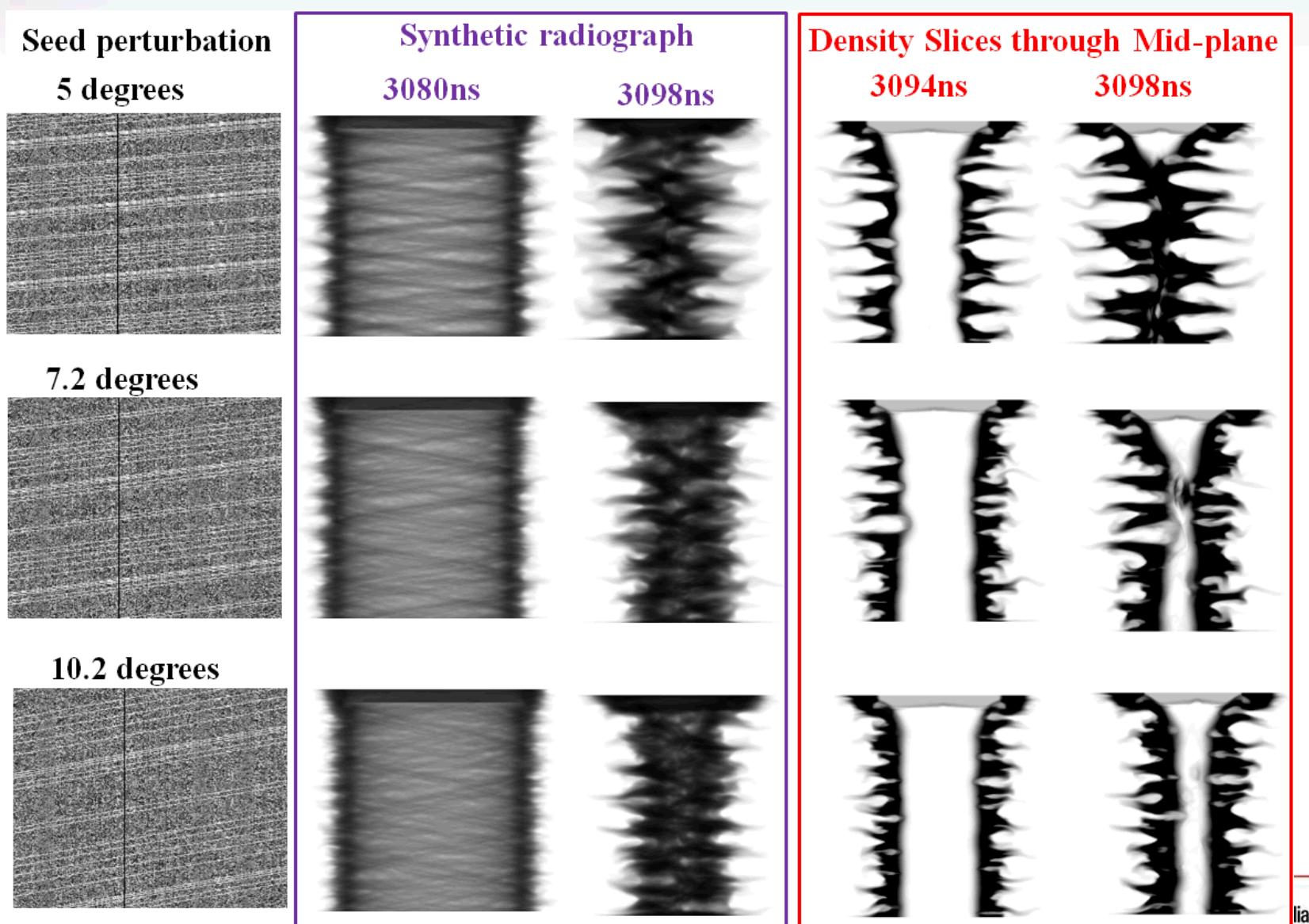
$$C \equiv a_1/a_2$$



$$\varphi_{t2} = \tan^{-1}(C \cdot \tan(\varphi_{t1}))$$

Increasing  $\varphi_{\text{avg}} \approx \tan^{-1}(p/2\pi a) \rightarrow$  pitch changes slowly relative to implosion; helices are entrained in liner wall

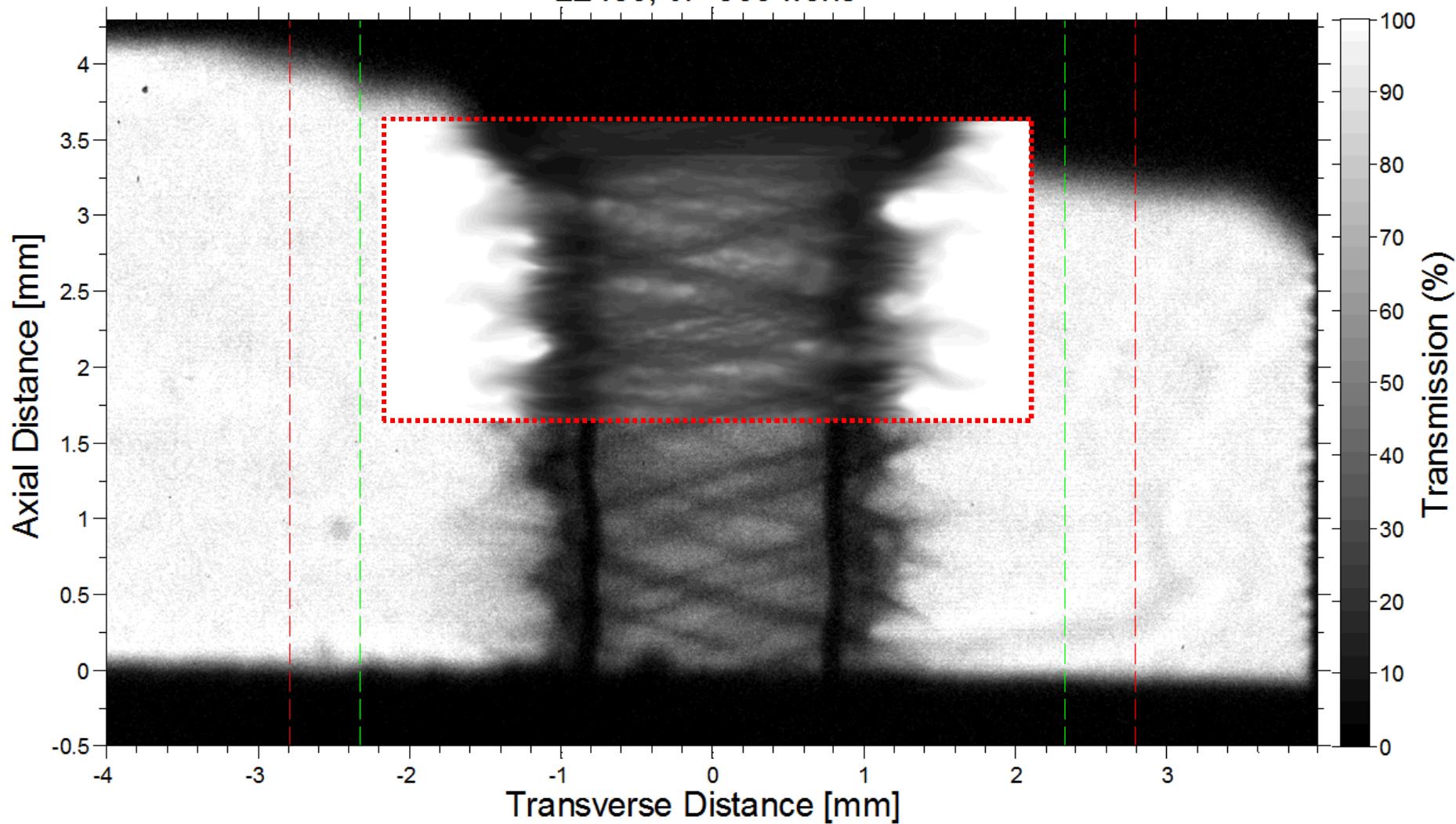
3D MHD simulations show that an initial helical perturbation will grow in amplitude and pitch angle as the liner converges



\*\*\*GORGON simulations by Chris Jennings\*\*\*

GORGON simulations initialized with a 7.2° perturbation match the late-time instability structure of the  $B_{z,0}=7$  T experiment

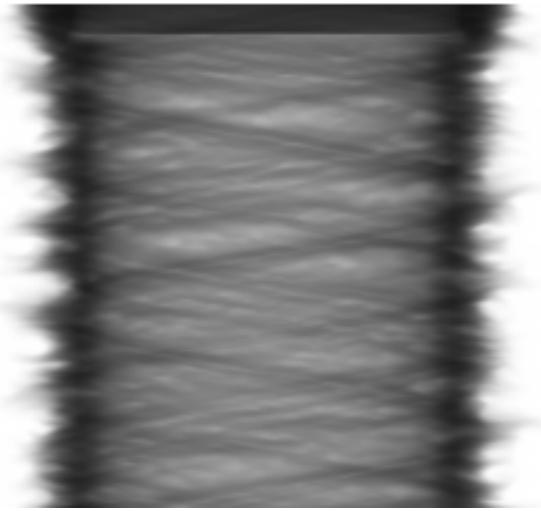
$z2480, t1=3094.3\text{ns}$



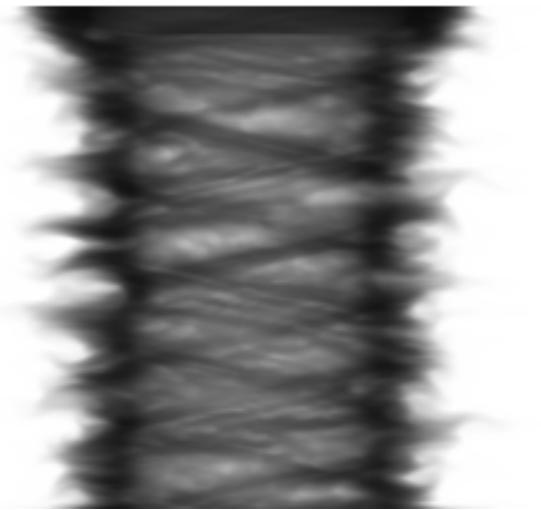
Once set by initial conditions the perturbation does not require further action of the applied  $B_z$  to persist

**No  $B_z$  field**

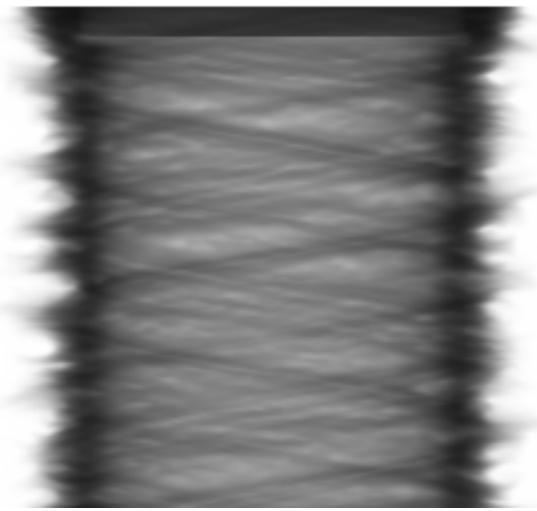
3082 ns



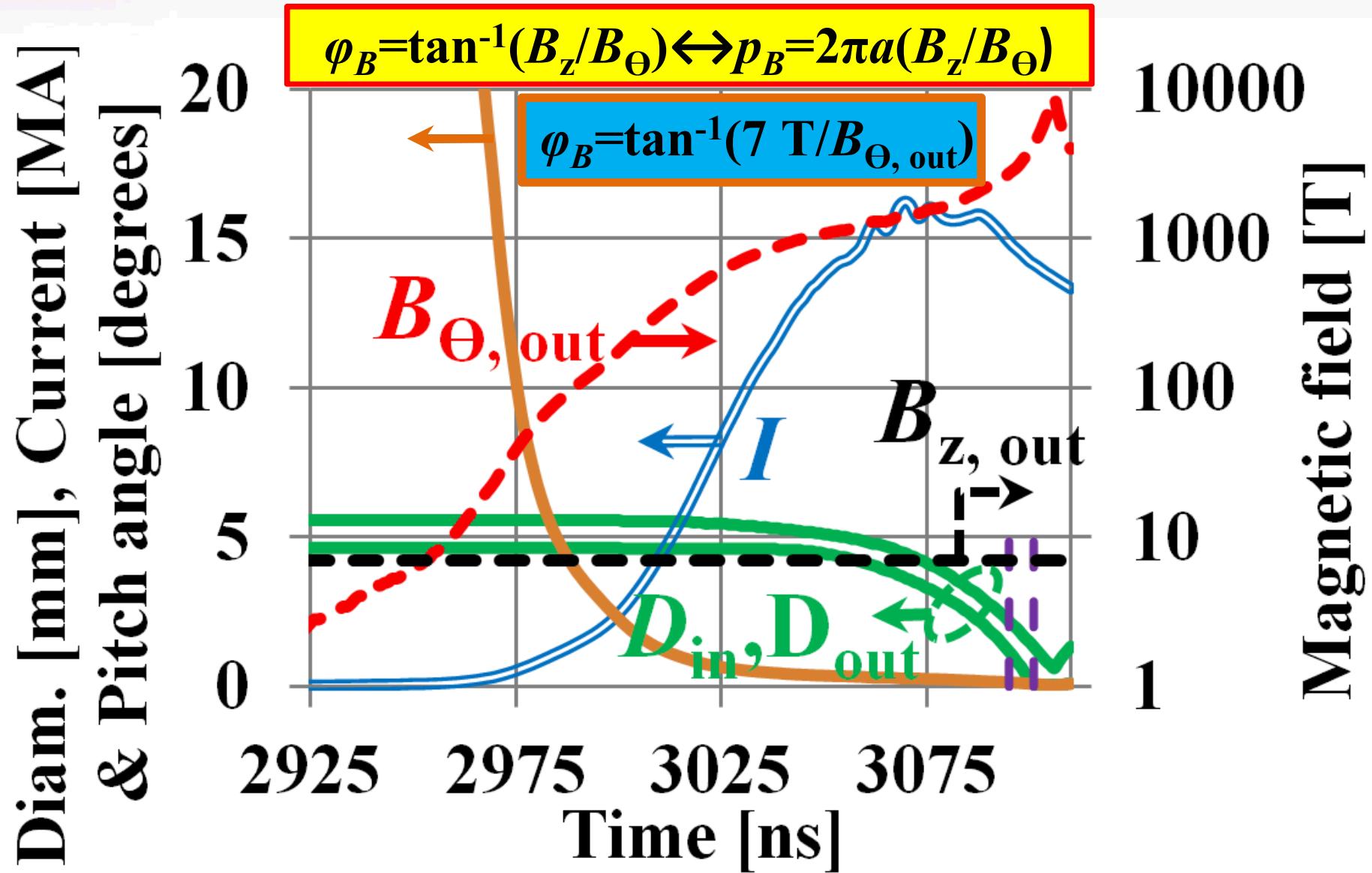
3090 ns



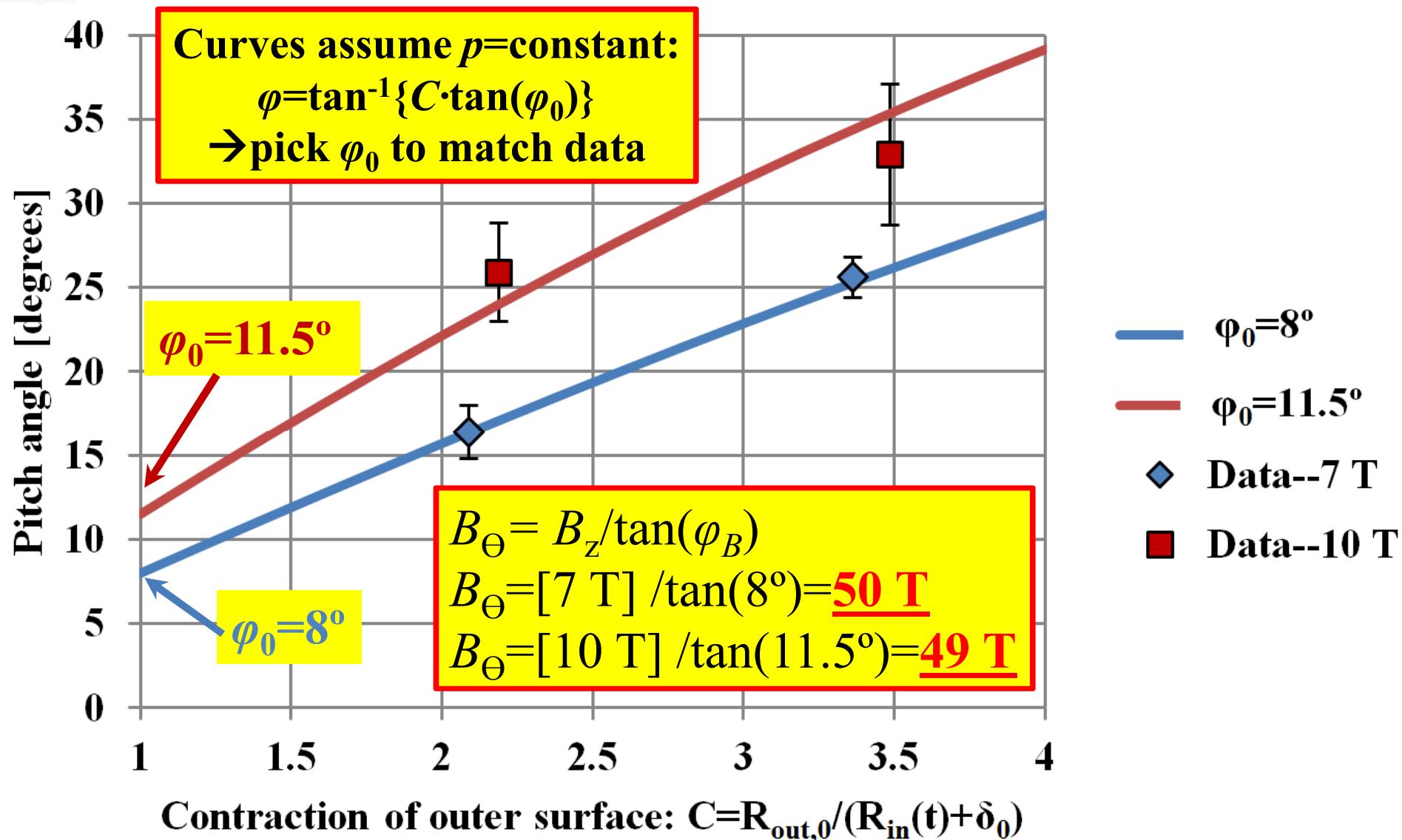
**$B_{z,0} = 10$  T**



GORGON: If the perturbation is set when  $B_\Theta \approx B_z$ , it will persist and grow, even for  $B_\Theta \gg B_z$  throughout the implosion



Data supports constant pitch ( $p$ ) assumption: Relatively small initial pitch angle ( $\varphi$ ) increases as the liner implodes



Several physical processes occur at  $B_\Theta \sim 50$  T which could allow a seed to be imprinted in the liner surface

- For  $B \geq 23$  T, the magnetic pressure  $P_B = B_\Theta^2/2\mu_0$  exceeds the 207 MPa yield strength of the S-65 structural grade  
Be used to fabricate the liners
- Be melts at  $\sim 1550$  K
  - Temperature scaling with magnetic field for a thick conductor is given by  $T \sim B^2/2c_v\mu_0$
  - Using  $c_v = 3.55 \times 10^6$  J/K·m<sup>3</sup>, we find  $B_{\text{melt}} = 118$  T
- Electrothermal instabilities (ETI) can be seeded at temperatures well below melt when non-uniform joule heating leads to density perturbations



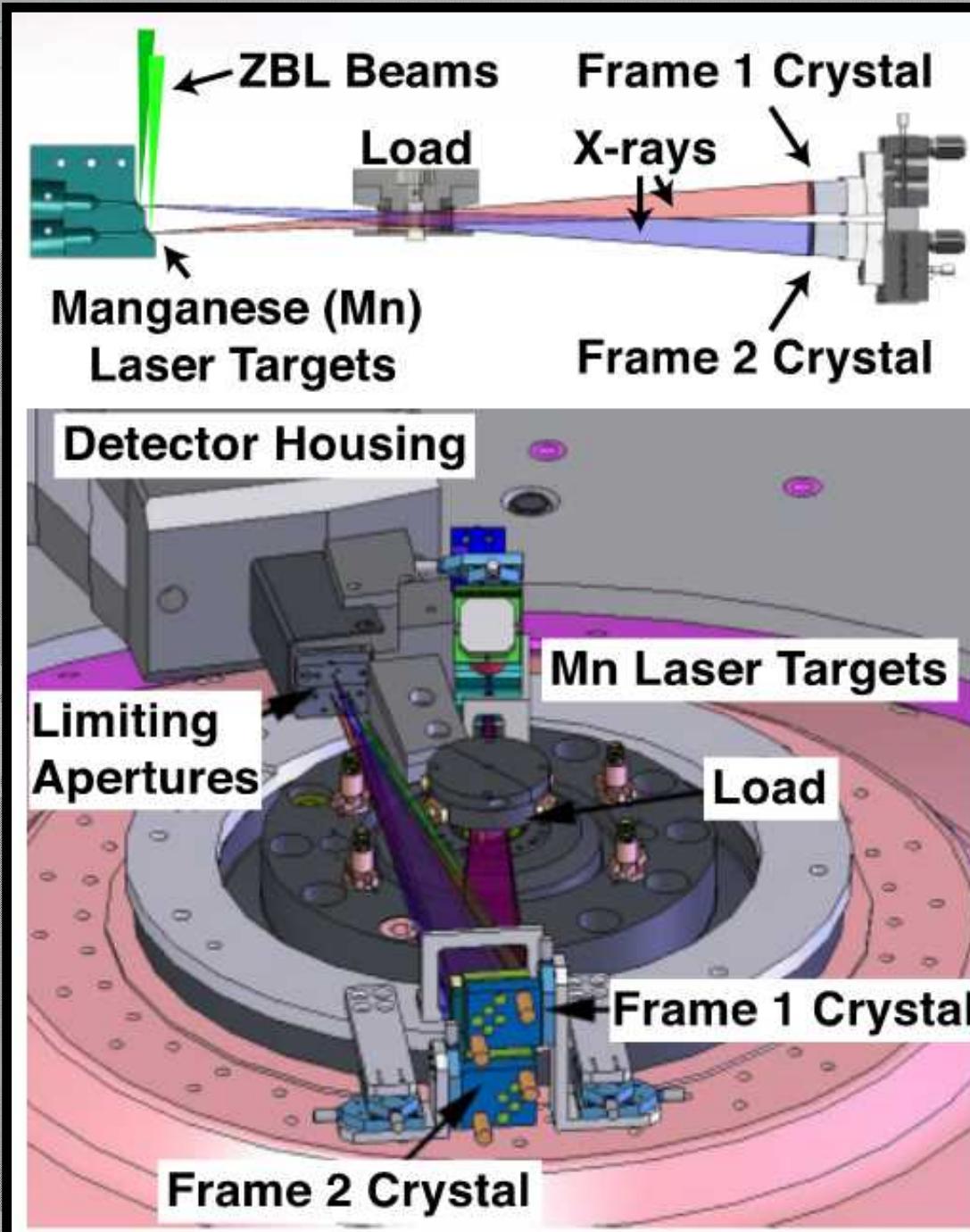
# Hypothesis: Premagnetization provides higher fuel uniformity at stagnation

- (1) Feedthrough rate is slower for helical instabilities (vs. “standard” azimuthally correlated instabilities)
- (2) Compressed axial field stabilizes  $m=0$  instabilities near stagnation

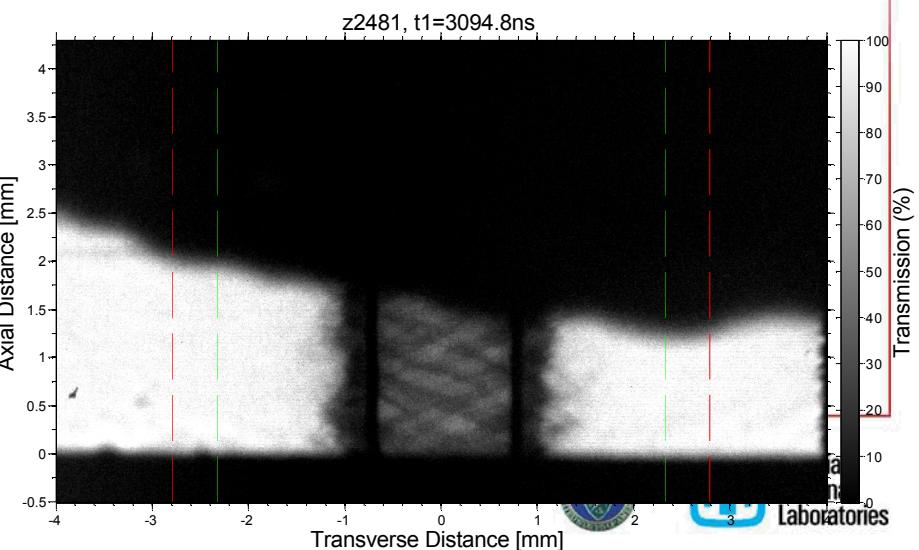
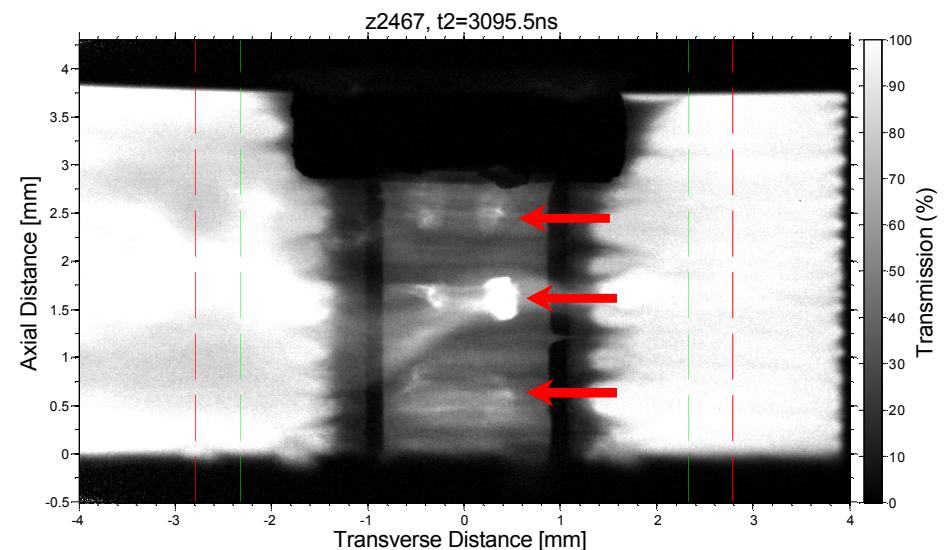
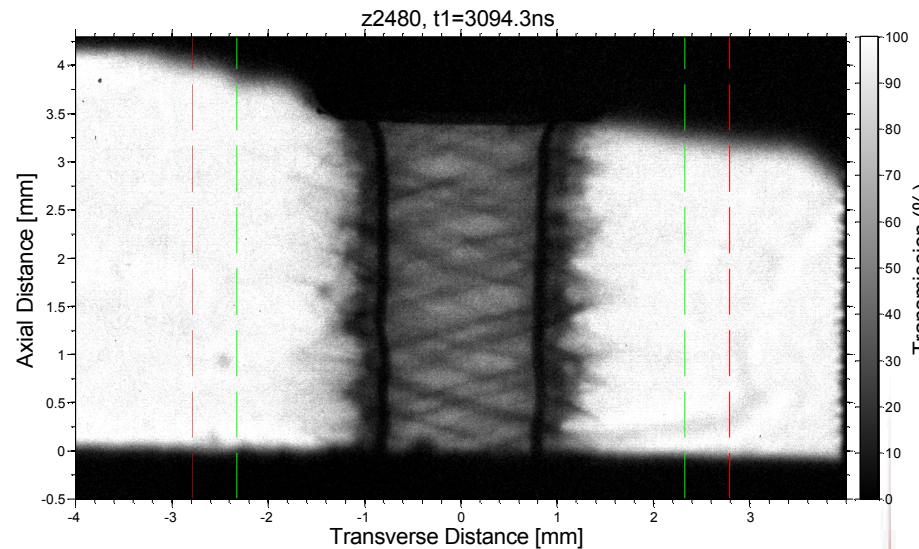
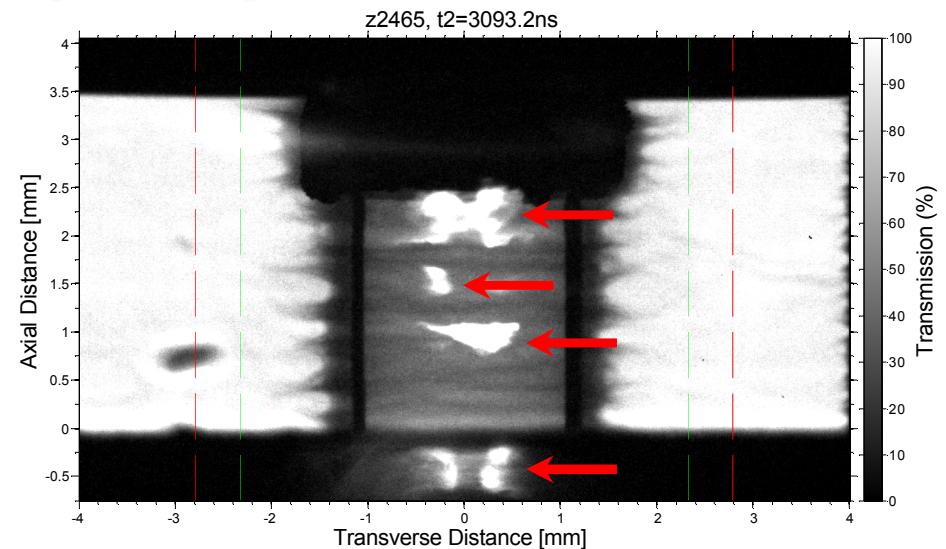


Reduced  
that the

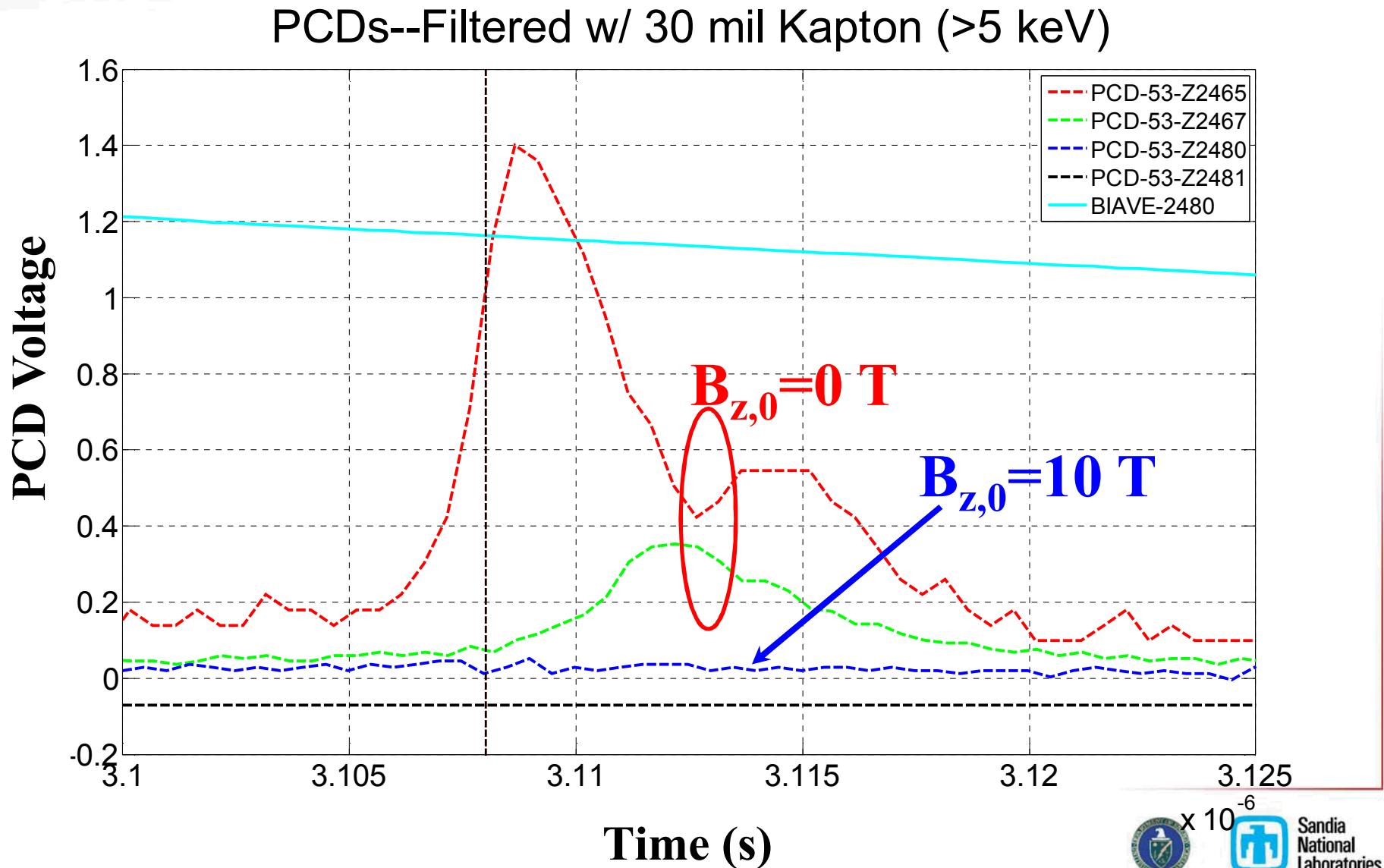
pports  
ability



# Reduced *time integrated* self emission (TISE) supports that the axial magnetic field enhances stability



Harder X-ray emissions are reduced when the liner/fuel are pre-magnetized with an axial field

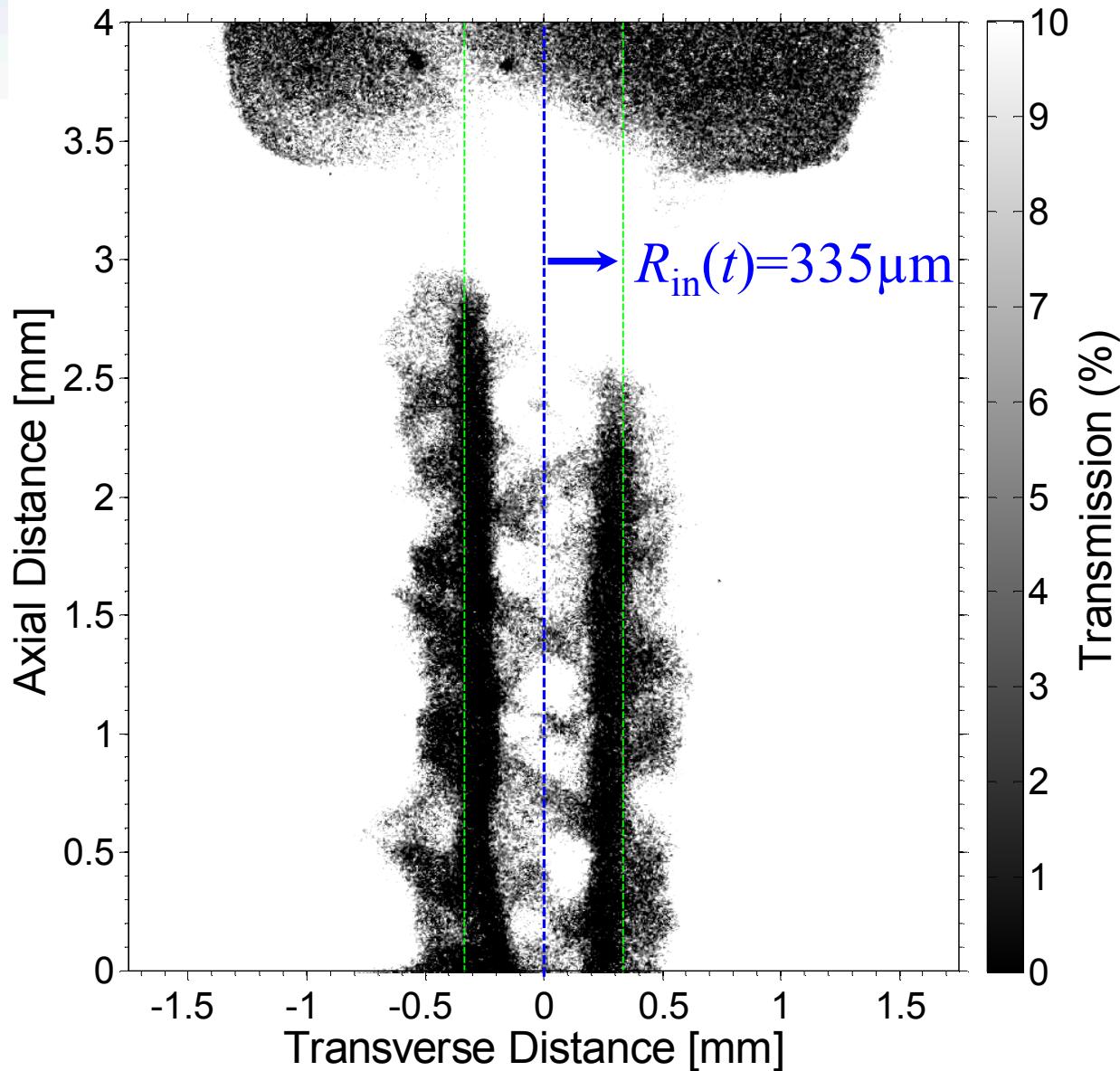


# Implosion remains highly uniform at CR=7

$$\text{CR} \equiv R_{\text{in},0}/R_{\text{in}}(t)$$

**Highest CR  
radiograph in the  
MagLIF program  
to date**

**CR~10 is  
maximum  
possible for Be  
opacity (areal  
density increases  
with CR)**



# Summary & Conclusions

- Liner implosion & MRT studies using penetrating radiography provide valuable data for benchmarking codes & characterizing a MagLIF-relevant liner implosion through to stagnation
- In stark contrast to liners with no seed  $B_z$  field, pre-magnetized liners develop 3D helix-like surface instabilities
- If a small helical perturbation can be set when  $B_\Theta \approx B_z$ , simulations show it will persist and grow, even when  $B_\Theta \gg B_z$  during the entire implosion
- A radiograph of a liner at a convergence ratio of 7 shows that the liner's inner wall remains highly uniform
- Evidence suggests that liner/fuel axial premagnetization may have a stabilizing effect
  - Reduced feedthrough rate of helical perturbation
  - Compressed axial field stabilizes  $m=0$  instabilities at stagnation