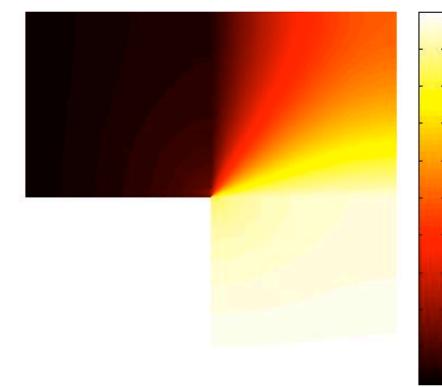
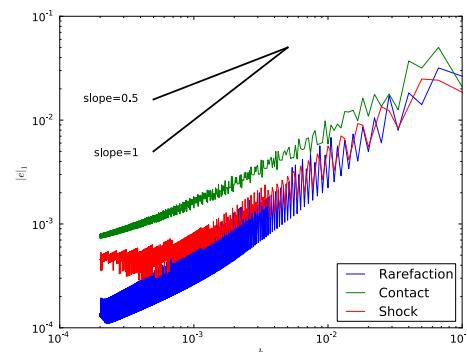
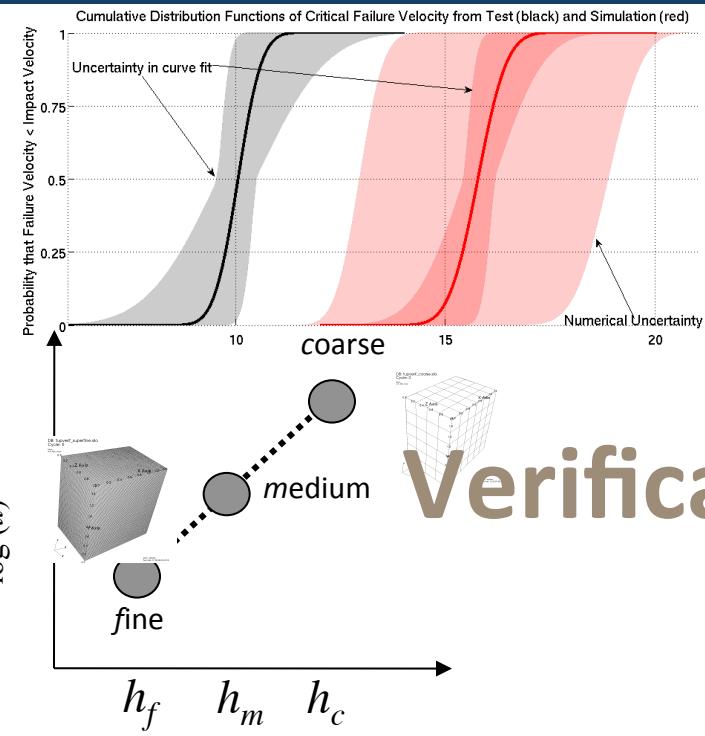


*Exceptional service in the national interest*

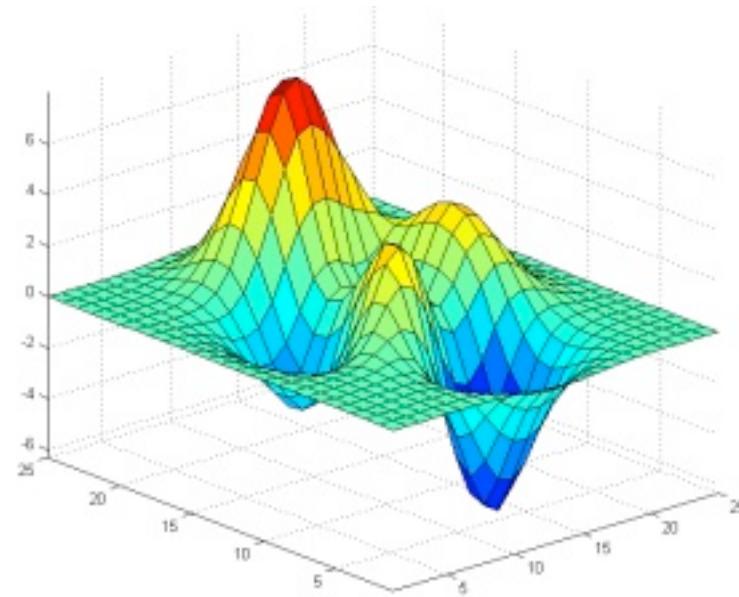


# Verification and Model Selection

Bill Rider, WCCM, Barcelona July 21, 2014

# What verification means in numerical analysis!

“For the numerical analyst there are two kinds of truth; the truth you can prove *and the truth you see when you compute.*” – Ami Harten



# *Code* Verification vs. *Solution* Verification

## **Code** Verification:

- You have an **exact solution**, so you compute **exact errors**
- You are testing your **code** (implementation, algorithm)
- **Hard** estimates of convergence properties
- **Metrics** are defined by numerical analysis

## **Solution** Verification:

- You don't have an exact solution, you **estimate numerical errors**
- You test your **solution(s)**
- **Soft** estimates of numerical error
- **Metrics are defined by the analyst** – integrated quantities, point values, functionals of the solution

# The Standard Setting For Calculation Verification: Richardson extrapolation for error estimation

- We begin with the standard error form,

$$\tilde{u} = u_h + A h^p$$

Diagram illustrating the standard error form:

- Prefactor** (blue box): Mesh converged solution, i.e.,  $h \rightarrow 0$
- Convergence rate** (green box): Characteristic length scale of mesh cell, “ $\Delta x$ ”
- Computed solution on mesh of char’c size  $h$**  (orange box):  $u_h$
- Characteristic length scale of mesh cell, “ $\Delta x$ ”** (red box):  $A h^p$

- The standard safety factor gives an uncertainty estimate (the *GCI*\*):

$$\delta = \tilde{u} - u_f \quad U_{num} = F_s |\delta|; F_s = 1.25$$

- This safety factor gives an ostensible 95% confidence interval,
  - ~2 std. dev. from CFD “experience” and computational experiments.
- Other forms will provide different estimates of  $F_s$ .
- **For two grids**, no estimate for  $\delta$  is possible, and the uncertainty is intentionally “generous”:  $U_{num} = F_s |u_f - u_c|; F_s = 3$

\* GCI: Grid Convergence Index, i.e., Roache’s approach

# Error bars are subject to interpretation

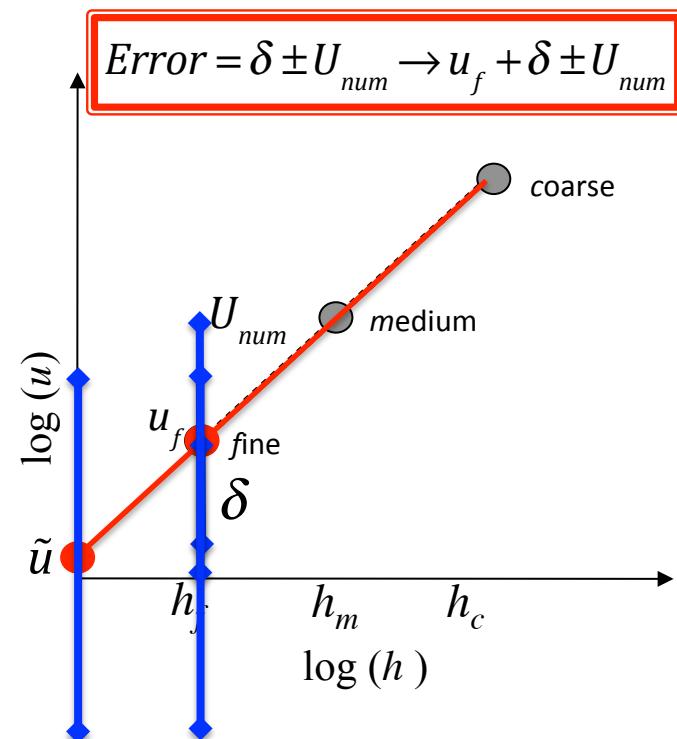
$$\delta = \tilde{u} - u_f$$

$$U_{num} = F_s |\delta|; F_s = 1.25$$

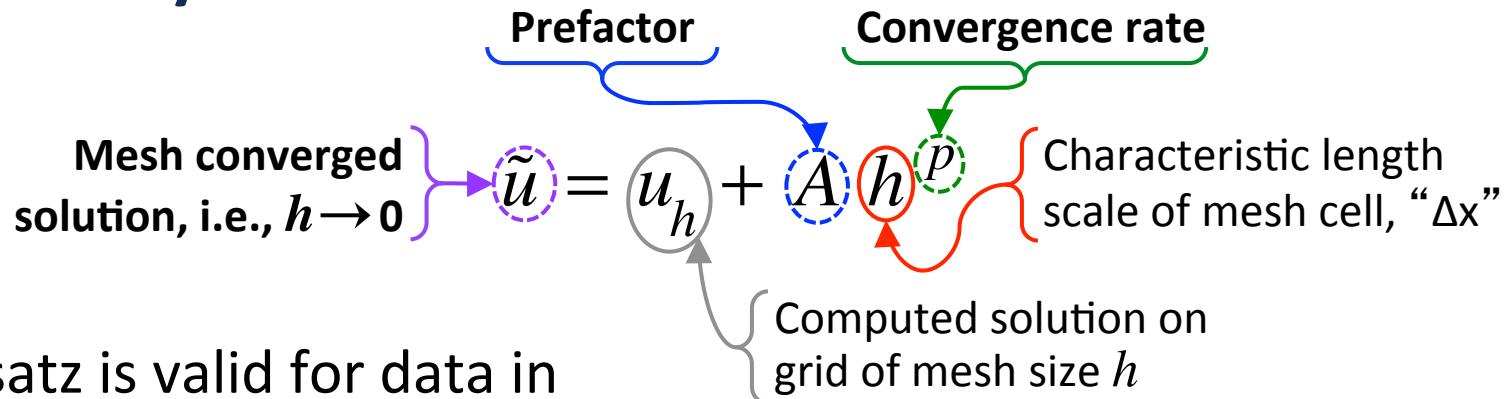
$$u_{best} = \tilde{u} \pm U_{num}$$

Where should the error bar be placed (i.e., centered)?

- We have choices (two examined here):
  - Around the finest grid solution
  - Around the mesh converged solution
  - **The mesh converged solution is a best estimate and should define error.**
  - Error on the fine grid “should” be asymmetric.
  - The difference is significant



# There are some potential dangers to conscientiously avoid.



- This ansatz is valid for data in the asymptotic range of convergence.
  - Usually, we assume that the calculations are in the asymptotic range of convergence.
  - With two calculations, we have an **under-determined** fit through the results ( ).
  - With many calculations, the error ansatz is **fully determined** or over-determined; one can perform a **regression** fit.



# An example of how verification can go “off the rails”

Preliminary Verification Results for CFD\* for a CASL challenge problem

(GTRF) with Fuego and Drekar ( $\Delta p$ ), just spatial resolution

# ele.	Mesh	Fuego	Drekar
664K	Coarse	31.8 kPa	26.7 kPa
1224K	Medium	24.6 kPa	23.8 kPa
1934K	Fine	24.4 kPa	22.0 kPa

**Fuego**

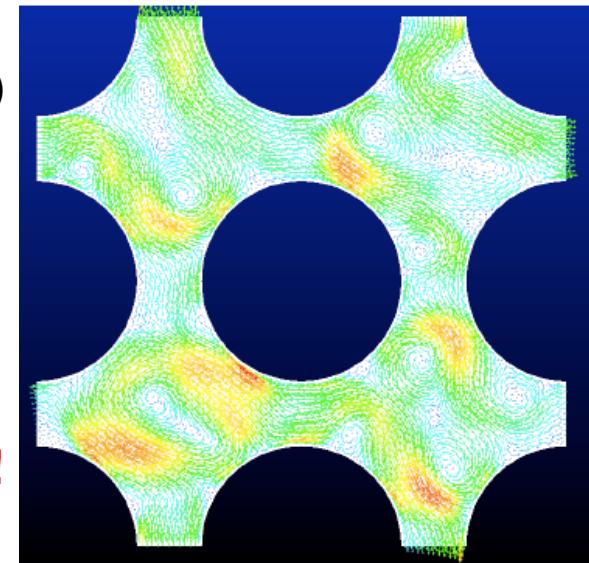
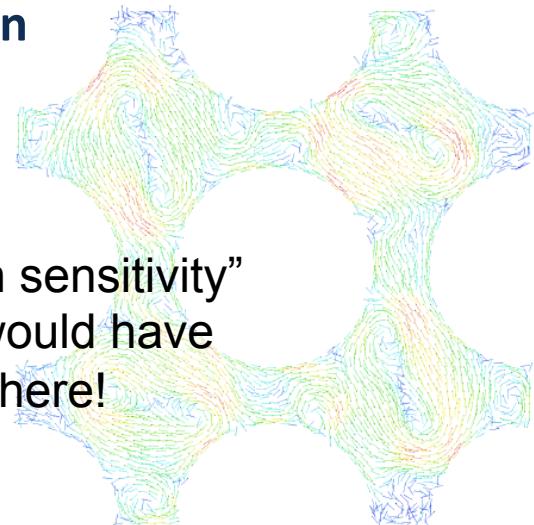
$$\Delta p(h) = 24340 + 26.6h^{1.85!!}$$

95 % Error Bound 80Pa (Roache, GCI) to 18.6kPa (Stern)

**Drekar**

$$\Delta p(h) = 17420 + 16370h^{1.234}$$

A “mesh sensitivity”  
study would have  
us stop here!

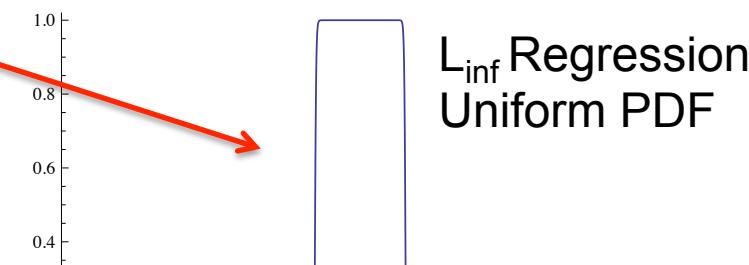
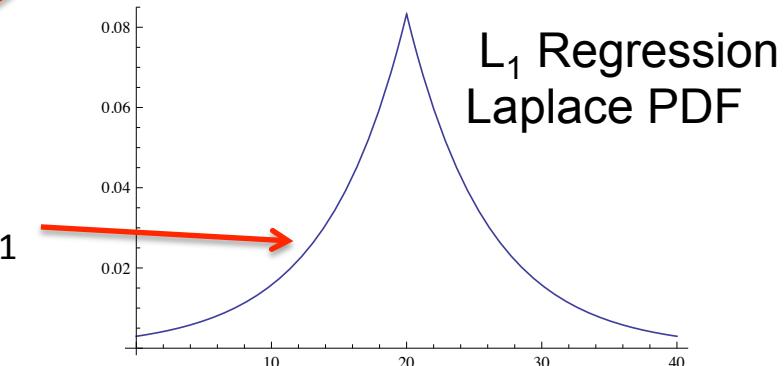
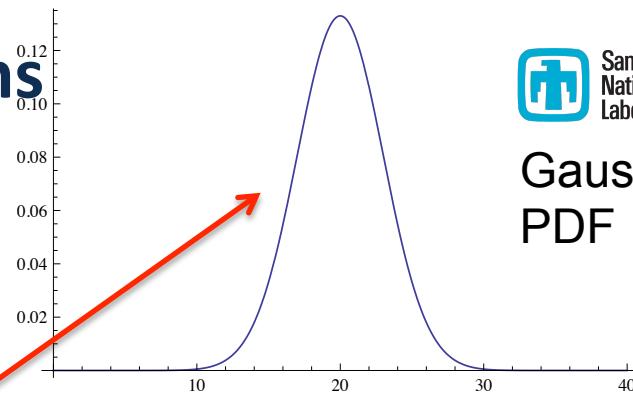


**The Fuego result exemplifies one of the problems with the standard setting, 16<sup>th</sup> order convergence is absurd!**

**Preview: Our procedure gives a  $\Delta p = 16.1 \text{ kPa} \pm 13.5 \text{ kPa}$ .**

# Brief Digression: Regression, norms and probability distributions

- Minimization of the residual for regression carries implications about optimality. The fit is optimal if the errors are distributed:
  - Gaussian implies  $L_2$ , *the standard approach* (unweighted)
  - Laplace (double exponential) implies  $L_1$  (absolute value)
  - Uniform implies  $L_{\infty}$  (maximum)
- Regression can be done in any norm if the data is either under- or over-determined and can include constraints as well.*



Use robust statistics not standard statistics

# We define a robust multi-regression (RMR) method to encode expert information, with robust statistics.

- The standard method is fragile and includes implicit assumptions regarding statistics, error and convergence, which are not included in the analysis.
- We apply the following algorithm to the data (2 or more grids):
  1. A structured principled way to introduce specific expert knowledge. Bounds on extrapolated solution could be entered too (such as positivity).
  2. Produce a set of estimates with defined explicit assumptions regarding statistics of the error, and free of the fragility of a single estimate.
  3. Apply robust statistical techniques to produce results with confidence. Run over subsets of data (jack-knife).
  4. Produce a bounding estimate using the same approach. Useful when the data is non-monotonic.

# We can demonstrate our method by solving a linear ODE.

- The equation is trivially solvable. We use a forward Euler method here.

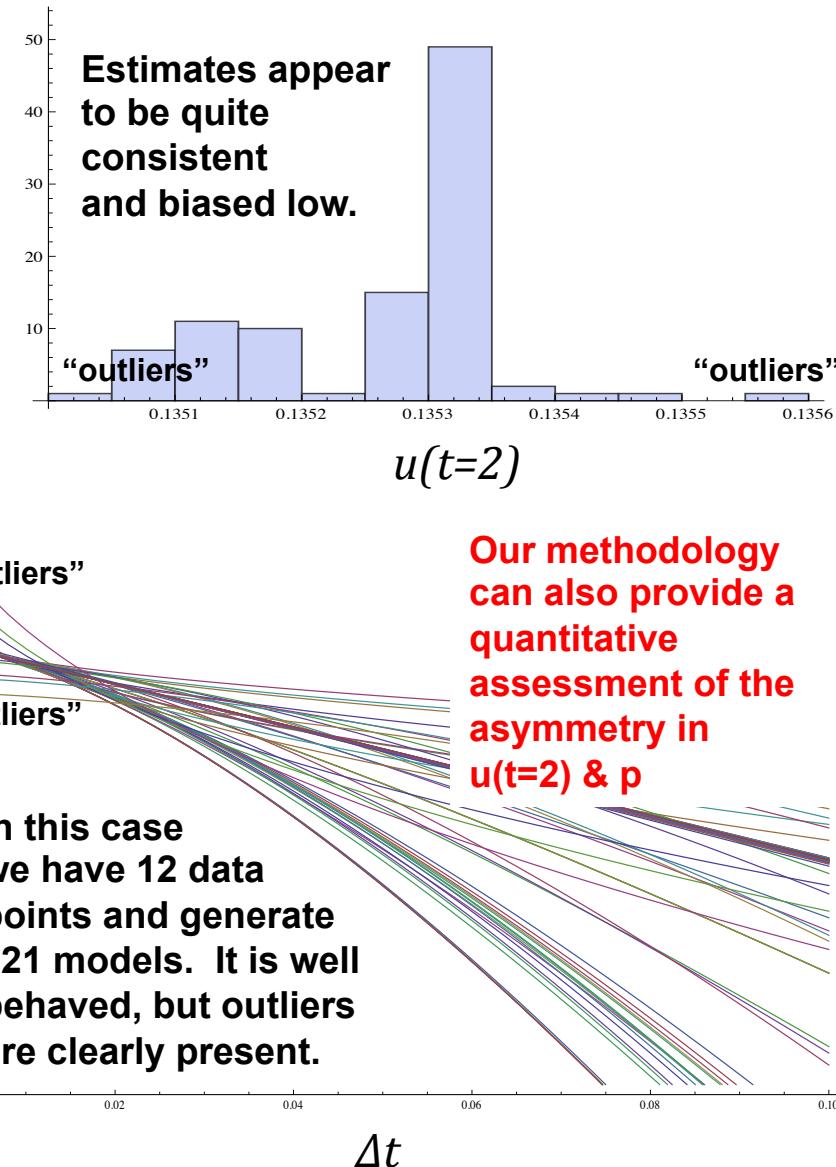
$$\dot{u} = -u \rightarrow u^{n+1} = u^n - \Delta t u^n$$

- The estimate and uncertainty strongly coincide with the analytical result.

$$u(t=2) = 0.135316 \pm 0.000138247, p = 1.0219 \pm 0.0154$$

- The uncertainty “fans out” for  $\Delta t$  smaller than the finest time step used for computed results.
- Roache’s GCI approach does not capture the analytical solution!

$$u(t=2) = 0.134794 \pm 0.000517851, p = 1.03878$$



# Solution Verification for Drekar gives estimates are very close to the three grid estimates given earlier!

Mesh	$\Delta p$ (pa)
671K	23400
1049K	26781
2664K	23804
5832K	22040
12522K	20745

RMR (all)

$$\Delta p = 16500 \pm 5435 + Ah^{0.53 \pm 0.09} Pa$$

RMR (drop coarse grid)

$$\Delta p = 16280 \pm 7060 + Ah^{1.08 \pm 0.27} Pa$$

GCI (all)

$$\Delta p = 23250 \pm 1635 + Ah^{0.5} Pa$$

GCI (drop coarse grid)

$$\Delta p = 16450 \pm 6960 + Ah^{1.05} Pa$$

- The results are convergent, but at a rate comparable with expectations for “rough” flows like turbulence, that is 1<sup>st</sup> order accurate.
- Uncertainties are large.
- RMR gives reliable results with or without dropping the non-convergent data point (671K)
- The CGI is extremely unreliable without screening the data.

**The estimated solution is frighteningly close to the estimates from the earlier Fuego calculations!**

# Next: Investigate Model Selection Procedures

- Verification is usually done with an assumed error ansatz
  - Almost always a power law form
- It would be beneficial to assume less, and define a better error model more supported by the data.
- Statistical estimation procedures exist for examining the form of the model that best fits the data
- Examples: AIC, BIC, **LASSO**
- Note, that these methods are well-defined for linear models, and verification has been shown to generally require nonlinear models

# We decided to explore the LASSO Method in this context

- LASSO has already been applied to verification as one of the fits used in the robust verification work
- In its linear form it is a simple regularized least squares method

$$\min \|Ax - b\|_2 + \lambda \|x\|_1$$

- As the Lagrange multiplier is increased in size the solution becomes increasingly “sparse”.
- Closely related to  $\min \|x\|_1$  constrained by  $Ax = b$
- **Our greatest leap is applying it to the nonlinear model selection**

$$\min \|f(x) - b\|_2 + \lambda \|x\|_1$$

# Variants of LASSO that may be better

- One does not have to do a regularized least squares.
- The L1 norm might be useful

$$\min \left\| f(\mathbf{x}) - \mathbf{b} \right\|_1 + \lambda \left\| \mathbf{x} \right\|_1$$

- ...or the Danzig estimator using the infinity norm.

$$\min \left\| f(\mathbf{x}) - \mathbf{b} \right\|_\infty + \lambda \left\| \mathbf{x} \right\|_1$$

- All work the same way, as the Lagrange multiplier becomes large most of the coefficients go to zero.

# The L1 Norm has some remarkable properties useful for model selection

- *Some have said that L1 is “magic”*
- Specifically, the L1 norm promotes sparsity under the minimization framework
- This is used in compressed sensing (and basis pursuit)

$$\min \|\mathbf{x}\|_1 \text{ constrained by } A\mathbf{x} = \mathbf{b}$$

$$\min \|\mathbf{x}\|_1 \text{ constrained by } \|A\mathbf{x} - \mathbf{b}\|_2 < \varepsilon$$

- The approach allows us to rank the portions of the model from piece-by-piece by examining the terms that remain nonzero for a changing Lagrange multiplier.

**“Any sufficiently  
advanced technology is  
indistinguishable from magic.”**

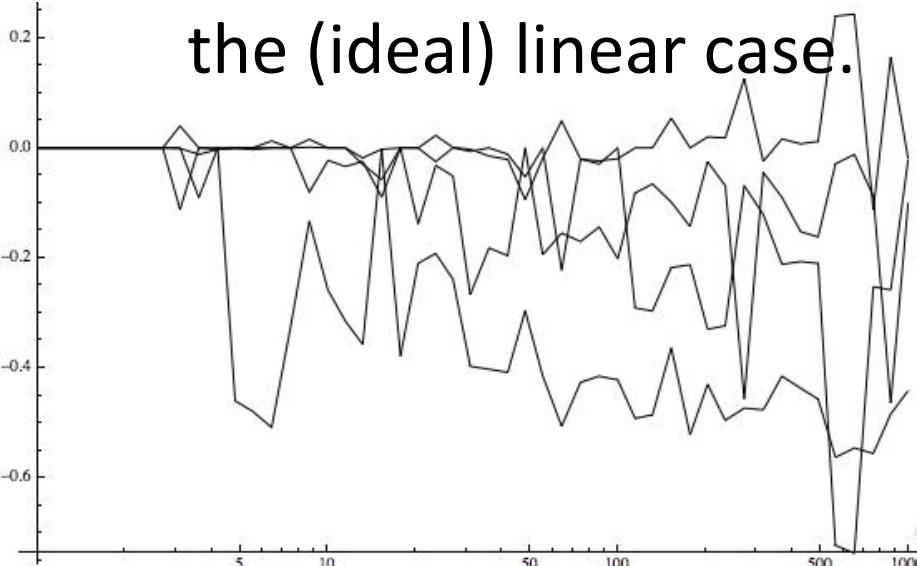
– Arthur C. Clarke

# Simple example with model selection

- I will use the simple ODE problem as the first test.
- Broaden the potential terms in the model to include other possible terms:  $\tilde{u} = u_h + A h^p$

$$\tilde{u} = u_h + A_p h^p + A_1 h + A_2 h^2 + A_e [1 - \exp(b_e h)] + A_L \log(1 + b_L h)$$

- The results are unexpected. The trends are clear, but the plots of the coefficients are not nearly as clean as the (ideal) linear case.



$$\min \left\| \tilde{u}(\mathbf{A}) - u_h \right\|_\infty + \lambda \left\| \mathbf{A} \right\|_1$$

$$\tilde{u} = u_h + A_1 h + A_2 h^2$$

# Let's look at the performance as error estimators term-by-term

- We use a L1 estimator for each (if you do one fit, I'd recommend L1 instead of L2!)

$$u_{\text{true}} = \exp(-2) = 0.135335$$

- The linear plus quadratic was chosen (polynomial)

$$u_{1,2} = 0.135337 - 0.135337h - 0.0211486h^2; r = 0.0000609$$

- Exponential

$$u_{\text{exp}} = 0.135337 - 0.454392 \left[ 1 - \exp(0.298264h) \right]; r = 0.000146$$

- Logarithmic

$$u_{\text{log}} = 0.135470 - 2.130270 \log(1 + 0.298264h); r = 0.002867$$

- Power Law  $u_{\text{power}} = 0.135235 - 0.148584h^{1.03656}; r = 0.000640$

# Example with picking out cross terms

- We are testing a model with two-dimensional transient heat conduction and chemistry for solute deposition in nuclear reactor cores. The code is poorly documented and it is not clear how coupled it actually is.
- We are going to use the LASSO to investigate what the error model should look like

$$\tilde{u} = u_h + A_x \Delta x^{p_x} + A_y \Delta y^{p_y} + A_t \Delta t^{p_t} + A_{xy} (\Delta x \Delta y)^{p_{xy}} + A_{xt} (\Delta x \Delta t)^{p_{xt}} + A_{yt} (\Delta y \Delta t)^{p_{yt}} + A_{xyt} (\Delta x \Delta y \Delta t)^{p_{xyt}}$$

- If we just use every term over-fitting is a distinct possibility
- We find that the model that stands out is rather different than we would have chosen a priori. This model does well,

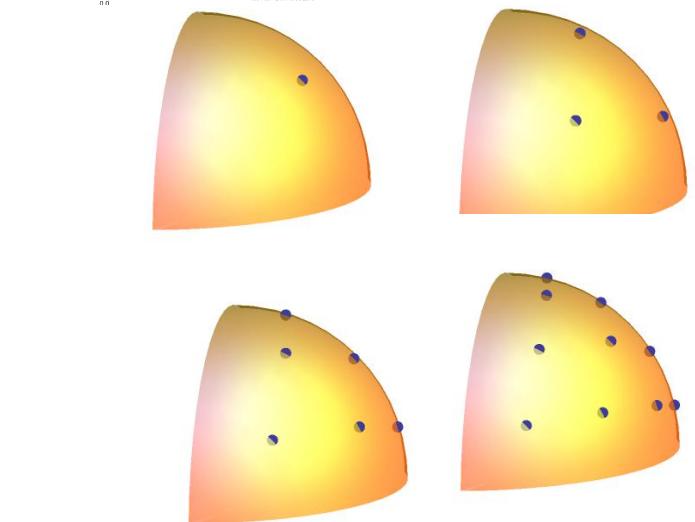
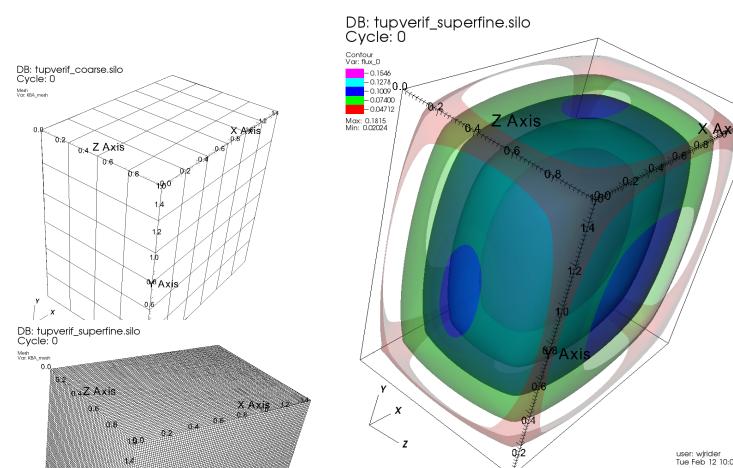
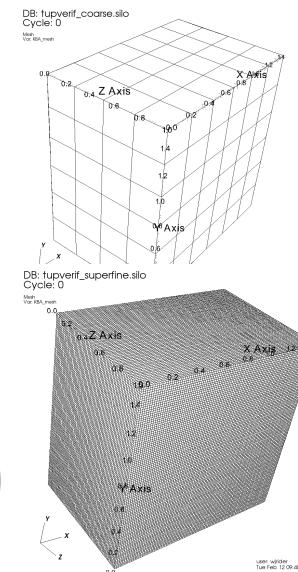
$$\tilde{u} = u_h + A_x \Delta x^{p_x} + A_y \Delta y^{p_y} + A_t \Delta t^{p_t} + A_{xy} (\Delta x \Delta y)^{p_{xy}} + A_{xyt} (\Delta x \Delta y \Delta t)^{p_{xyt}}$$

# Applying this to Sn Neutronics

- We apply the verification techniques to the ORNL neutronics code Denovo, which solves the transport equation using discrete ordinates.

$$\Omega \cdot \nabla \psi(x, \Omega, E) + \sigma(x, E) \psi(x, \Omega, E) = \int dE' \int_{4\pi} d\Omega' \sigma_s(x, \Omega' \cdot \Omega, E' \rightarrow E) \psi(x, \Omega', E')$$

- The solution depends on six “coordinates” three space, two angular, and energy.
- We reduce this to space and angle while examining their distinct discretization.
- At this point only very simple problems have been examined.



# We need to modify the standard verification setting to accommodate the discrete ordinates method

- The basic approach remains, but we have two variables that convergence critically depends upon,

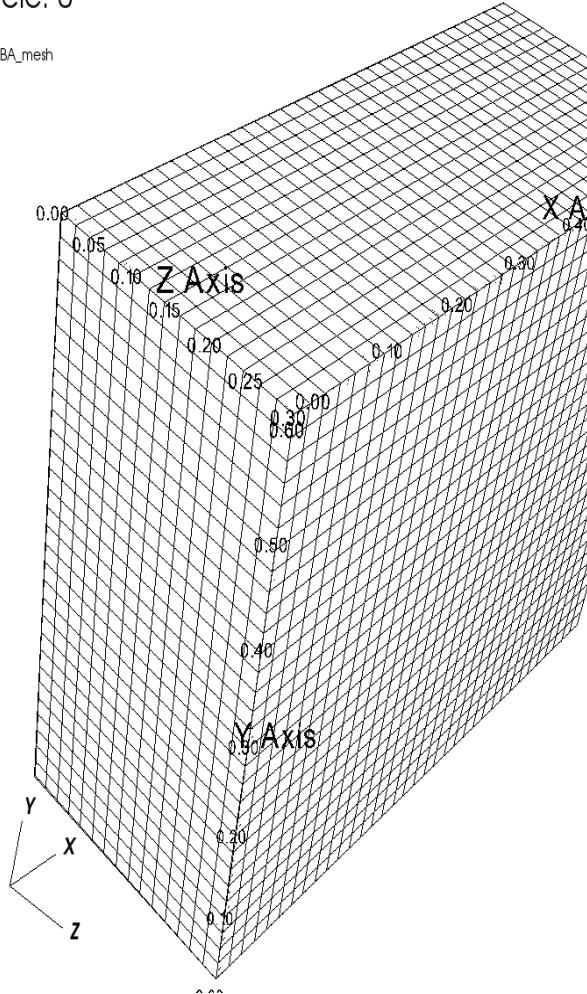
$$\tilde{u} = u_h + A h^p + B / n^q + C (h/n)^r$$

- A secondary issue is the theoretical expectations for the convergence with respect to the number of quadrature points where we have chosen a form like Jarrell (2010),
- We have examined four different spatial discretizations of the streaming term: Step characteristic, linear discontinuous, trilinear discontinuous, and diamond differencing with negative flux fix-up
- We have examined four different quadratures: level symmetric, Gauss-Legendre, Quadruple Range, and LDFE.

# The integrated scalar flux for the downscatter problem.

DB: twd\_coarse.silo  
Cycle: 0

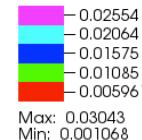
Mesh  
Var: KBA\_mesh



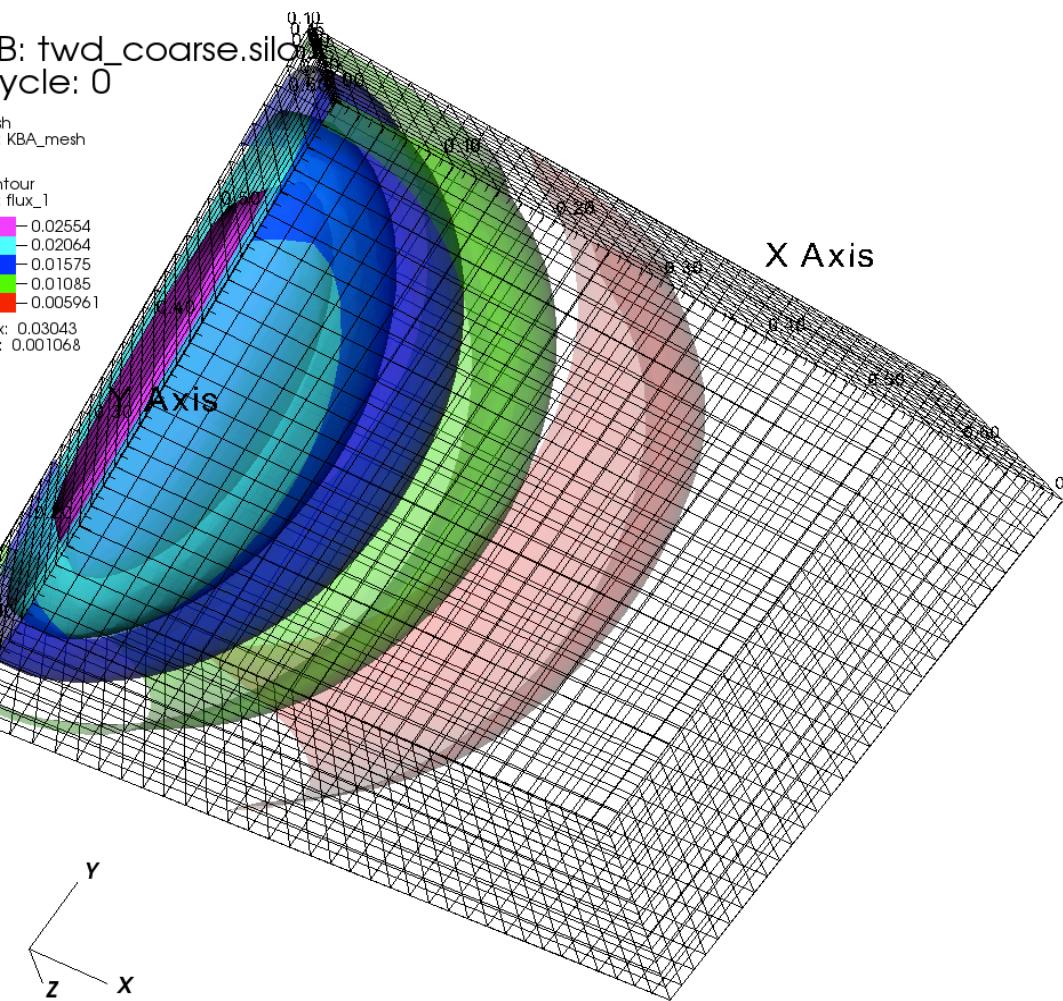
DB: twd\_coarse.silo  
Cycle: 0

Mesh  
Var: KBA\_mesh

Contour  
Var: flux\_1

  
0.02554  
0.02064  
0.01575  
0.01085  
0.005961  
Max: 0.03043  
Min: 0.001068

Max: 0.03043  
Min: 0.001068



user: wjrider  
Wed Feb 13 12:33:10 2013

# Neutronics Results

- We find little support for the h-p version of the error model
  - The third term in the error model drops out immediately as the size of the Lagrange multiplier is increased.
- We also examine the nature of the error model itself as before

$$\tilde{u} = u_h + Ah^p + \alpha[1 - \exp(\kappa h)] + B/n^q + \beta[1 - \exp(n/n)] + C(h/n)^r + \gamma[1 - \exp(\xi h/n)]$$

- We find the power law in space and the coupled space-angle power term dominate.

# Summary and Future Work

- The basic idea appears to work well.
  - We have concerns about applying this to nonlinear models where theory is weaker.
- We can use it to determine the dominant terms in a proposed error model
- The exponential terms are repeatedly chosen by the procedure, this needs further examination
  - The exponential terms are a better basic error model
  - The LASSO procedure is somehow biased toward them
- We will continue the exploration.

# Who Am I ?

- I'm a staff member at Sandia, and I've been there SNL for 7 1/2 years. Prior to that I was at LANL for 18 years. I've worked in computational physics since 1992.
- In addition, I have expertise in hydrodynamics (incompressible to shock), numerical analysis, interface tracking, turbulence modeling, nonlinear coupled physics modeling, nuclear engineering...
- I've written two books and lots of papers on these, and other topics.

