



Conceptual Design of a Low-Enriched Horizontal Split-Table Critical Assembly

Nuclear Criticality Safety Program Preliminary Horizontal Split-Table Experiment Design Meeting

Las Vegas, NV

July 31, 2014

**Gary A. Harms
Sandia National Laboratories**

SAND2014-XXXXP



Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.





What is Ahead

- **We were asked to provide a cost estimate for a large horizontal split-table critical assembly**
- **We initiated a conceptual design for such an assembly**
- **What follows is a description of the conceptual design**



Our charge

Explore the possibility of:

A large, 6' x 6' or greater, horizontal split table at SNL working under the current security cat environment.

**J. N. McKamy
July 12, 2012**



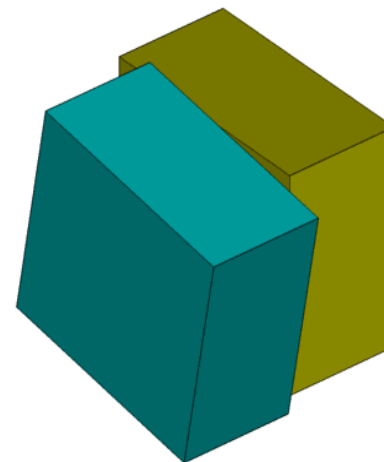
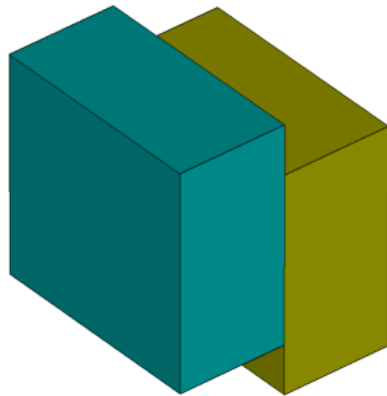
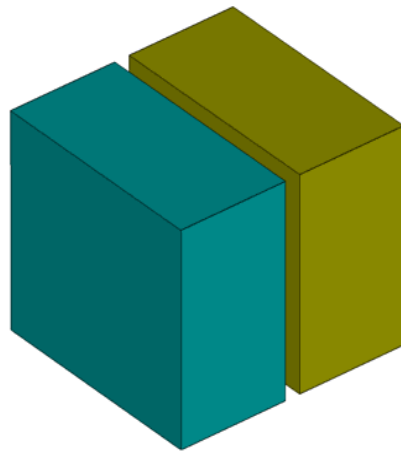
Low-Enriched General-Purpose Split-Table Critical Assembly – IER-226

- **C_{EdT} :**
 - Allison Miller (SNL)
 - Mike Dunn (ORNL)
 - Thomas Miller (ORNL)
 - Dave Heinrichs (LLNL)
 - Gary Harms (SNL)
- **CED-1 Conceptual Design is complete**
- **CED-2 Final Design has been initiated**
- **Note that this IER is for the design of the Critical Assembly, not for a specific experiment**



Split-Table Sensitivities

- **Possible Geometric Inaccuracies**





We Needed Some Notional Critical Experiments to Explore the Uncertainties

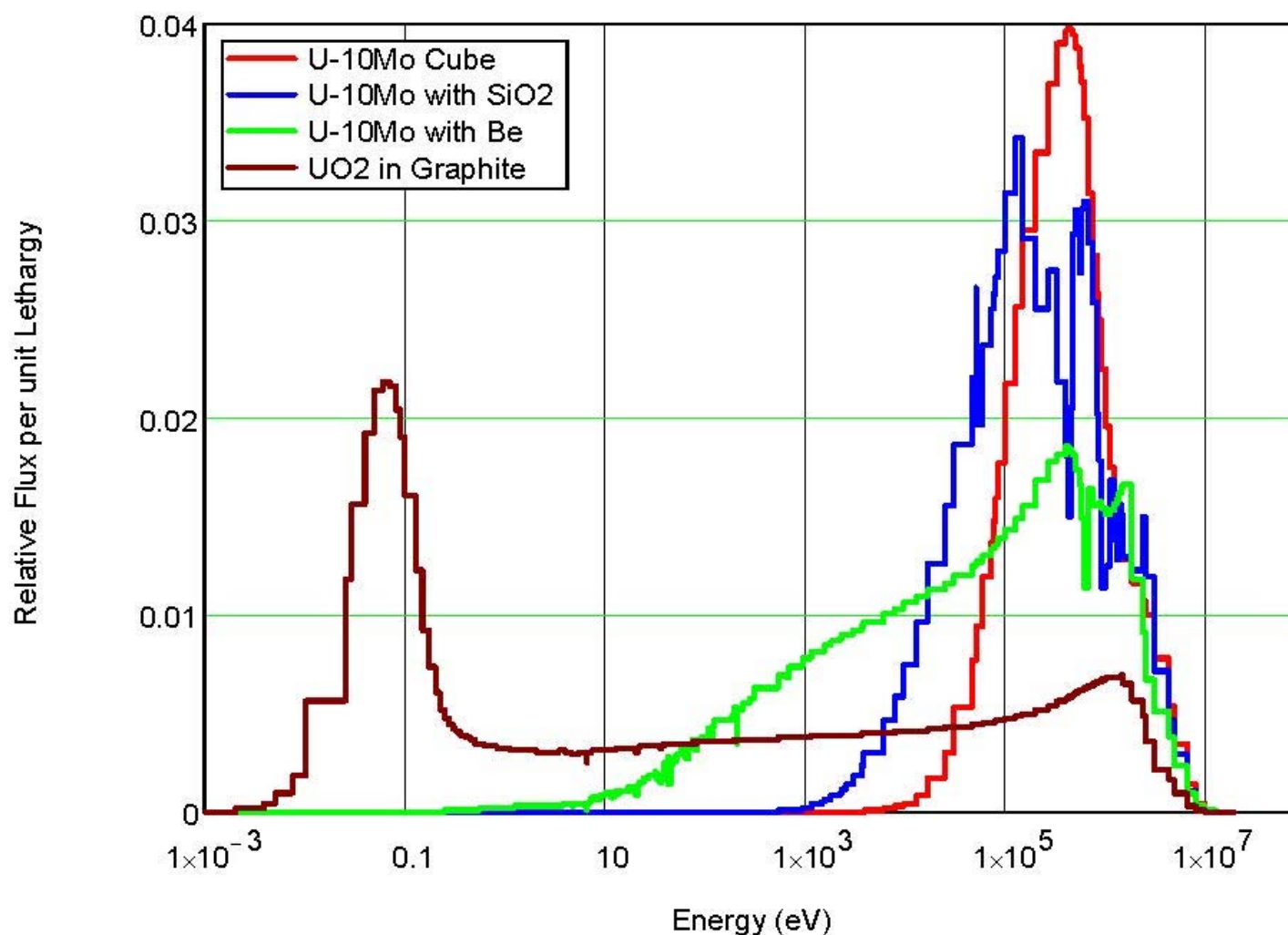
- **U-10Mo Cube**
- **U-10Mo with SiO₂**
- **U-10Mo with Beryllium**
- **UO₂ mixed with and reflected by graphite**

Table 2-2. Characteristics of Four Critical Assemblies Used in Study

	U-10Mo Cube	U-10Mo with SiO ₂	U-10Mo with Be	UO ₂ with Graphite
Fuel	U-10Mo	U-10Mo	U-10Mo	UO ₂
Fuel Intrinsic Density (g/cm³)	16.86	16.86	16.86	10.97
Diluent	None	SiO ₂	Beryllium Metal	Graphite
Diluent Intrinsic Density	-	2.648	1.848	1.70
Diluent Volume Fraction (%)^[1]	-	64	87	99.816
Void Fraction in the Core (%)	0	10	10	10
Fueled Volume Side Length (cm)	43.78	100	100	100
Fuel Mass (kg)	1,415	5,463	1,973	18.2
Reflector	None	None	None	Graphite
Reflector Thickness (cm)	-	-	-	50

1. Fraction of the non-void core volume that is occupied by the diluent.

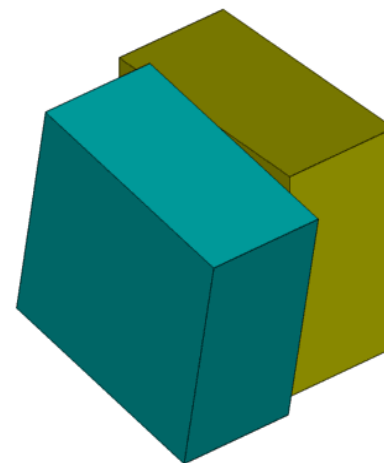
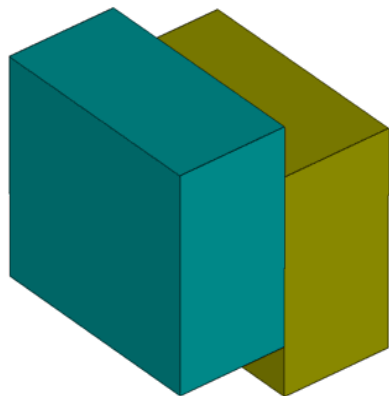
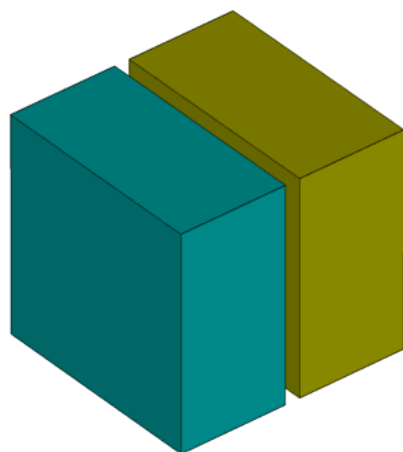
Neutron Spectra of the Four Notional Critical Assemblies



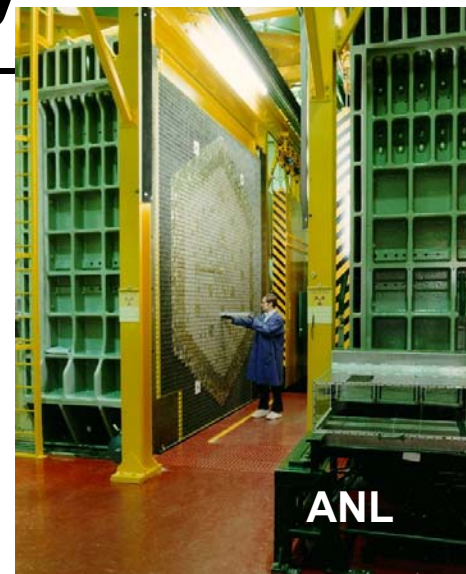
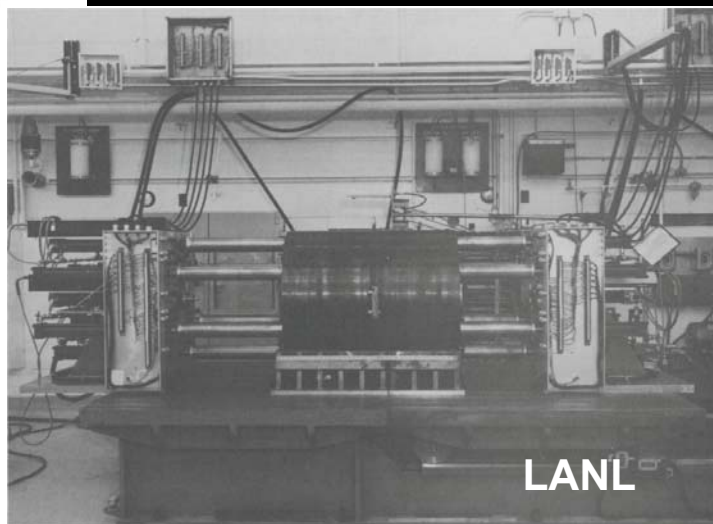


Split-Table Sensitivities

- **Possible Geometric Inaccuracies**



Split Table History



- We did a literature survey of past split tables in the US

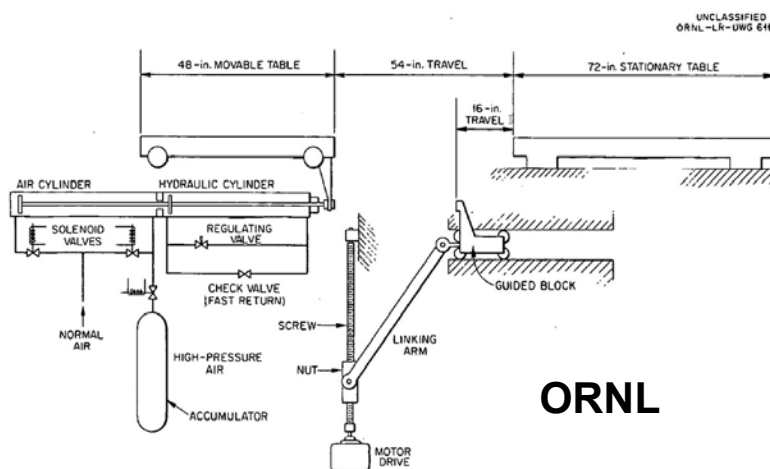
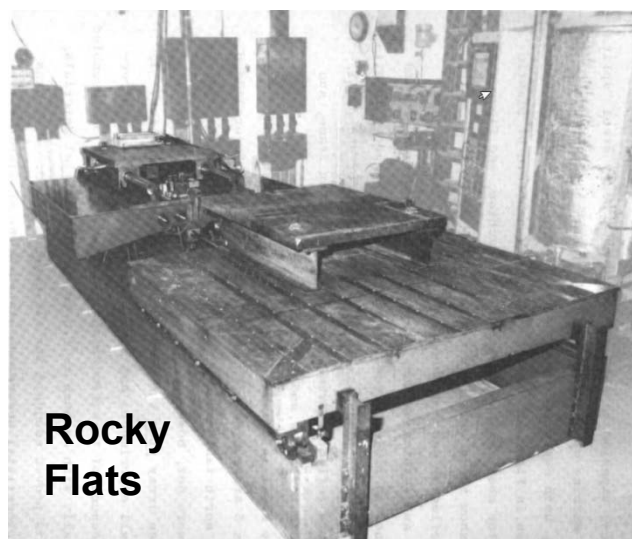


Fig. 3.6.3. Schematic of Drive Arrangement for Split-Table Machine.



Common Features

- **Two major core-supporting structures**
 - Horizontal motion
- **Very large in dimensions and mass**
- **A system for precise location of the two “halves”**
- **A fast-acting fail-safe safety system**
- **A control system for fine reactivity adjustment**
 - Design dependent on the experiment
- **A plant-protection system to back the operators up in unplanned events**



Design Options

- **All past systems we surveyed were constructed from purpose-built components**
- **OPTION 1 – do the same thing here**
 - All components designed and built from scratch
- **OPTION 2 – use commercial “off-the-shelf” (COTS) components where possible**
 - In particular, the movable table shares many characteristics with existing large boring/milling machines
 - Can one of these machines be the basis for the critical assembly?



Critical Assembly Design Goals

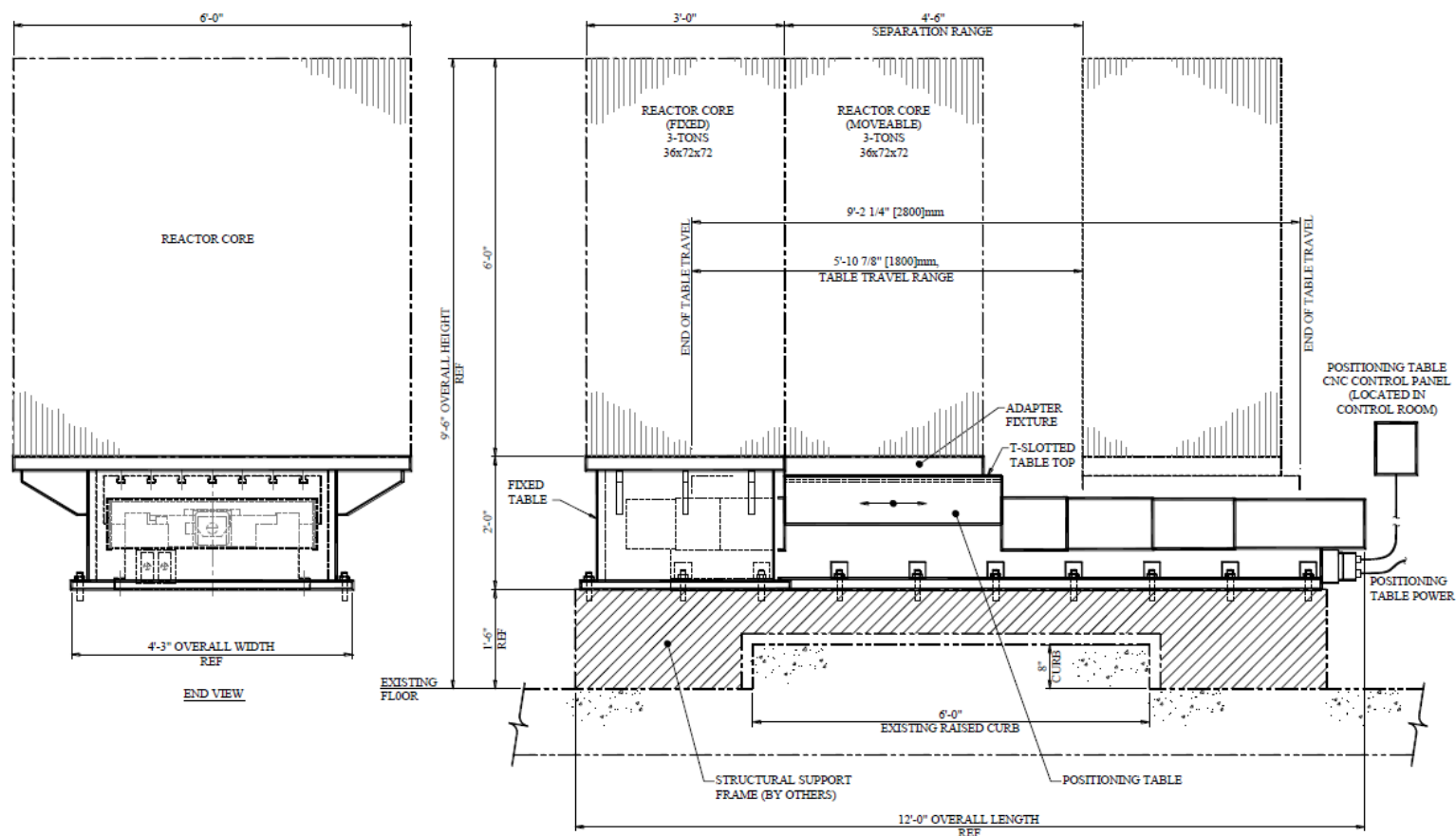
Experiment:

- 6 ft x 6 ft x 6 ft experiment
- 6,000 kg total, 3,000 kg on the movable platform
- Platform position(s) must be known to within approximately 0.0005-inch or better.
- Platforms are to be flat and parallel.
- Metal platform to be structurally sound to control and maintain relative position throughout all ranges of motion up to maximum payload.
- Fixed table and movable table must come together and touch.
- Fixed and movable tables must separate by at least 3 ft.
- Position reporting on three axes is preferred.

Control:

- Platform separates using a simple remote command/control approach.
- Provision for monitoring and reporting travel speed, direction, and position.
- Safety interlocks required to control unintended system response.
- Translation axis must move and be controlled, however, there is no speed requirement.
- The split-table control system and the reactor control system are separate.
- Capability to control the split-table locally as well as from a remote control room.

Option 2 Using a COTS Movable Table Appears to be the Most Cost-Effective Approach



The assembly would consist of a modified commercial boring/milling machine and a purpose-built fixed table



Critical Experiment Feasibility

- **Systems Using Fuel Currently Available at the SCX**
 - 7uPCX and BUCCX Fuel with Polyethylene
 - 7uPCX Fuel with Graphite Moderator
 - Harder Neutron Spectra with Existing Fuel (?)
 - Quantities and enrichment limit options for hard spectra
- **Systems with New Fuel**
 - Uranium Metal with 10 Weight Percent Molybdenum (U-10Mo)
 - Homogeneous Systems with U-10Mo Fuel
 - System with U-10Mo Plates Interleaved with Graphite



Shutdown Mechanisms

- **Experiment Dependent**
- **Separation of Two Halves**
 - Primary or Secondary Shutdown
 - SCRAM Initiated
- **Insertion of Absorber Rods**
 - Most Appropriate for Thermal Systems
- **Reflector Control**
 - Most Appropriate for Hard-Spectrum Experiments
- **In-Core Control Mechanisms**



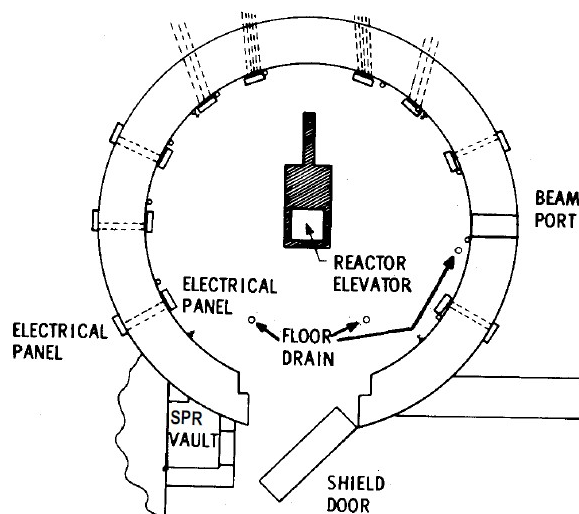
Critical Experiments at Sandia

- **The primary purpose of the reactor facilities at Sandia is to support our nuclear weapons mission**
- **The facilities and staff necessary to enable that work are exactly what are needed to support critical experiments.**
- **We are operating a water-moderated pin-fueled critical assembly**

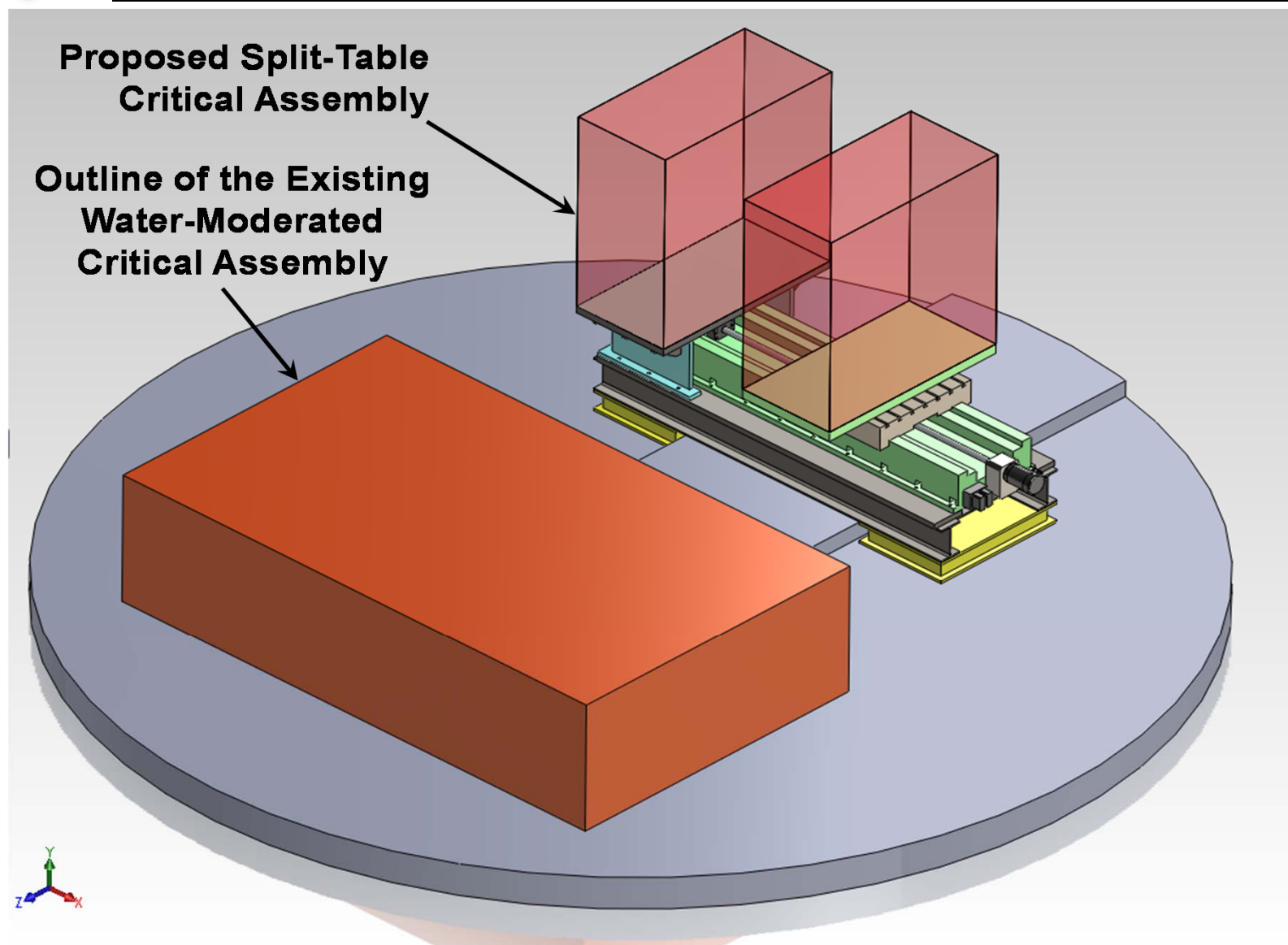
We operate our critical experiments in the Sandia Pulsed Reactor Facility



- The SPRF is an operating Nuclear Facility
- The SPRF has:
 - ✓ a professional operating staff and supporting infrastructure
 - ✓ an existing Authorization Basis (AB)
 - ✓ room in its schedule – the HEU SPR fuel has been removed
- We modify the AB as needed for the critical experiments
- The AB is current
- The reactor building is a 30-ft inside diameter concrete cylindrical shell capped by a hemispherical shell
- The dropped reactor room ceiling is 12 ft above the borated concrete floor
- The walls and ceiling are 4-in gypsum, 4-in borated gypsum from inside to outside



Possible Layout in the Reactor Room





Current Limitations on Our Water-Moderated Experiments

- **Design Features**

- All CA cores are designed so that criticality cannot be obtained without liquid moderator in the core tank.
- ASSEMBLY fuel type SHALL be UO₂.
- ASSEMBLY core UO₂ mass SHALL be no less than 50 kg.
- ASSEMBLY fuel enrichment (weight % ²³⁵U) SHALL be no more than 20%.

- **Specific Administrative Controls**

- The total amount of UO₂ ($\leq 20\%$ enrichment) associated with active critical experiments SHALL be no greater than 500 kg.
- The accumulated energy production for the ASSEMBLY SHALL be no more than 15 MJ over a ONE YEAR PERIOD.



The Current Limitations Will Need To Change

- **Design Features**

- ~~– All CA cores are designed so that criticality cannot be obtained without liquid moderator in the core tank.~~
- ~~– ASSEMBLY fuel type SHALL be UO₂.~~
- ~~– ASSEMBLY core UO₂ mass SHALL be no less than 50 kg.~~
- ~~– ASSEMBLY fuel enrichment (weight % ²³⁵U) SHALL be no more than 20%.~~

- **Specific Administrative Controls**

- ~~– The total amount of UO₂ ($\leq 20\%$ enrichment) associated with active critical experiments SHALL be no greater than 500 kg.~~
- ~~– The accumulated energy production for the ASSEMBLY SHALL be no more than 15 MJ over a ONE YEAR PERIOD.~~



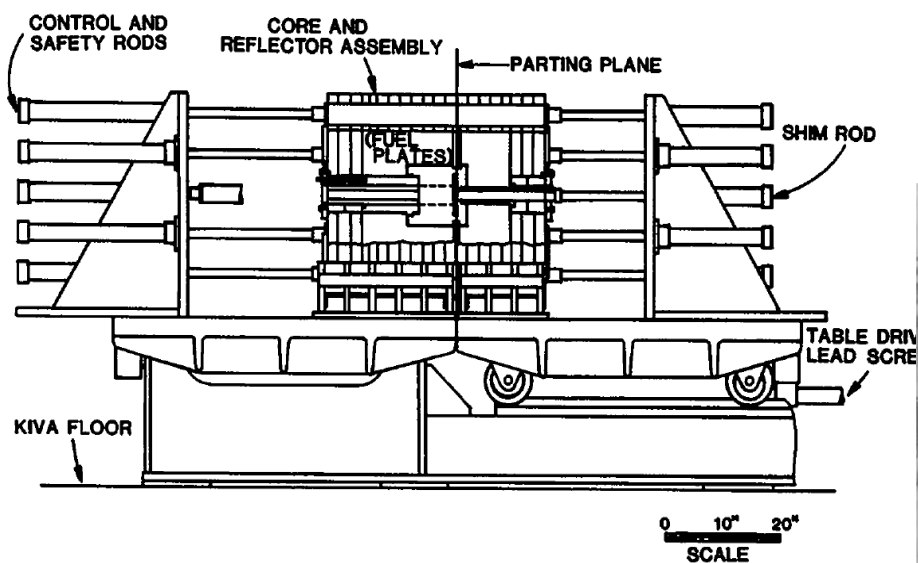
Concluding Remarks

- **We were asked to provide a cost estimate for a large horizontal split-table critical assembly**
- **We initiated a conceptual design for such an assembly**
- **We arrived at a design that was based on a commercially-available movable component with the remainder purpose-built components**
- **The conceptual design is for the Critical Assembly**
- **Experiment design to follow**

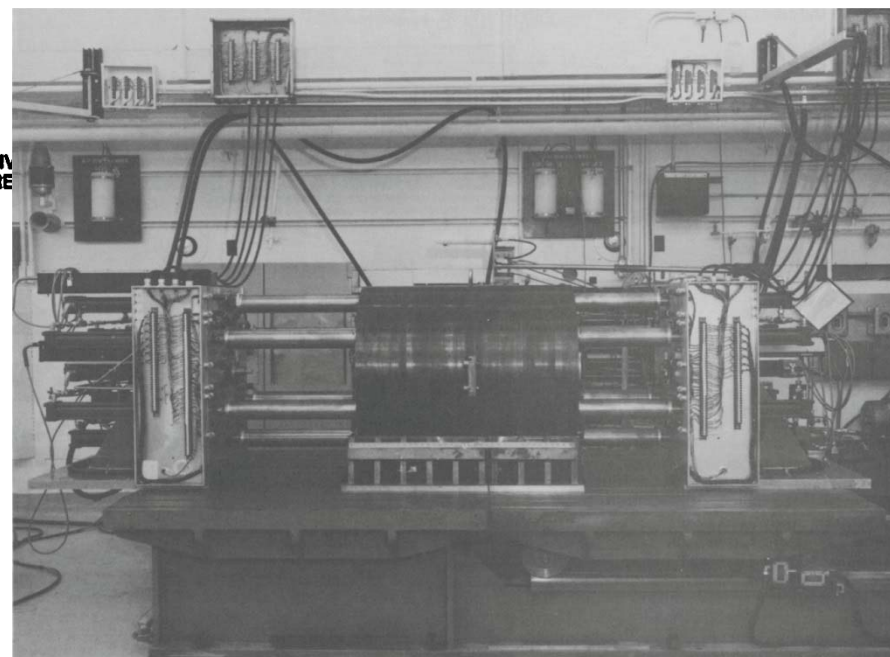
Critical Experiments at Sandia



Survey of Past Split-Table Machines



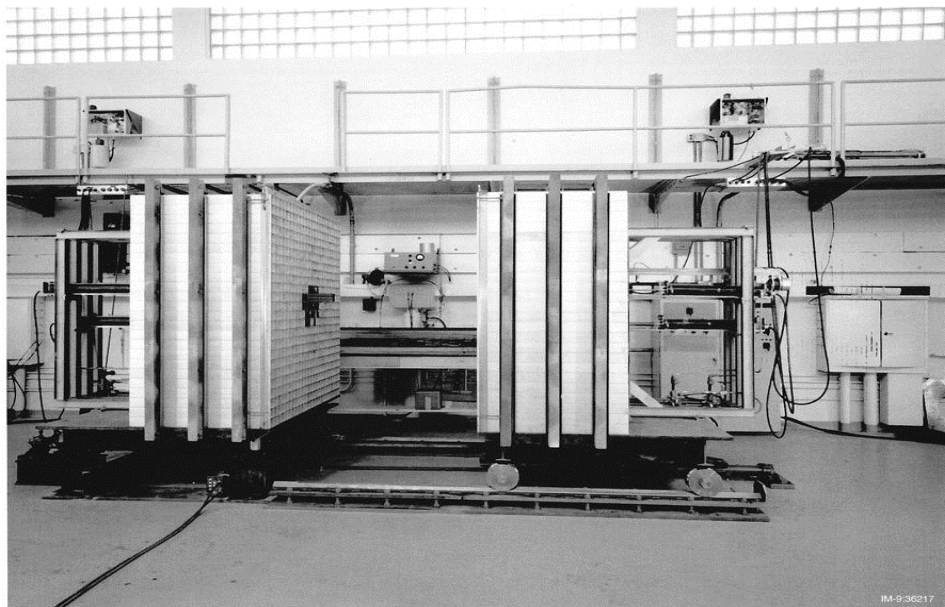
ional Laboratory



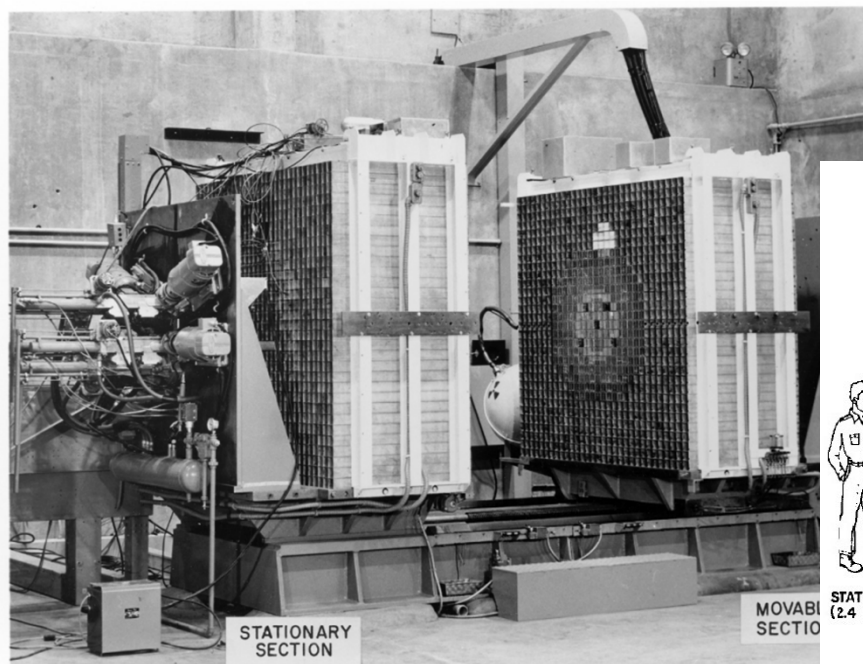


Survey of Past Split-Table Machines

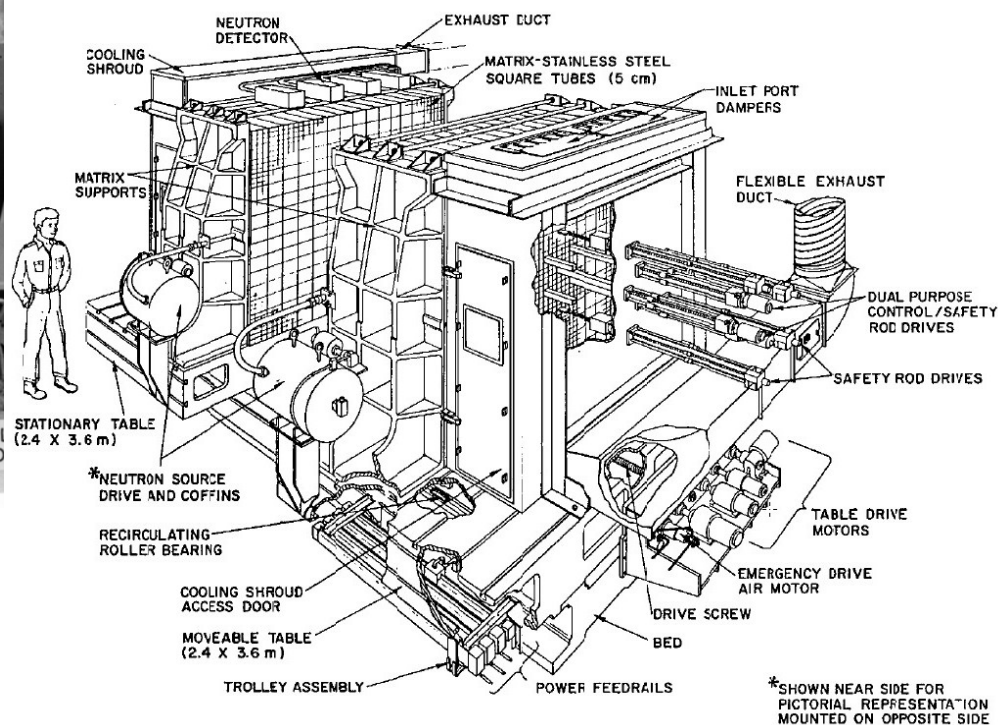
- **Honeycomb – Los Alamos National Laboratory**

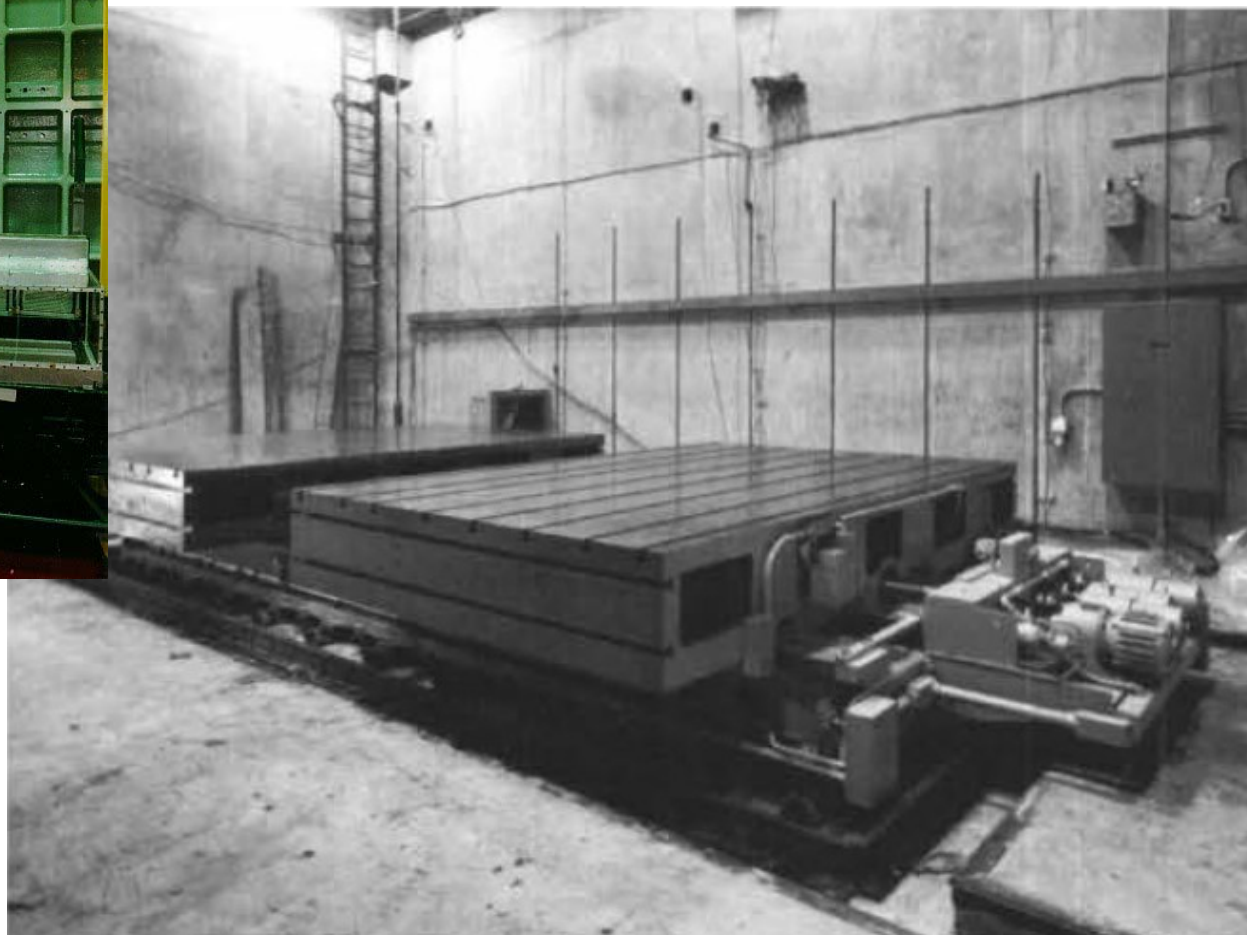


Survey of Past Split-Table Machines



National Laboratory





Survey of Past Split-Table Machines

• Horizontal Split Table Critical Assembly - Oak Ridge

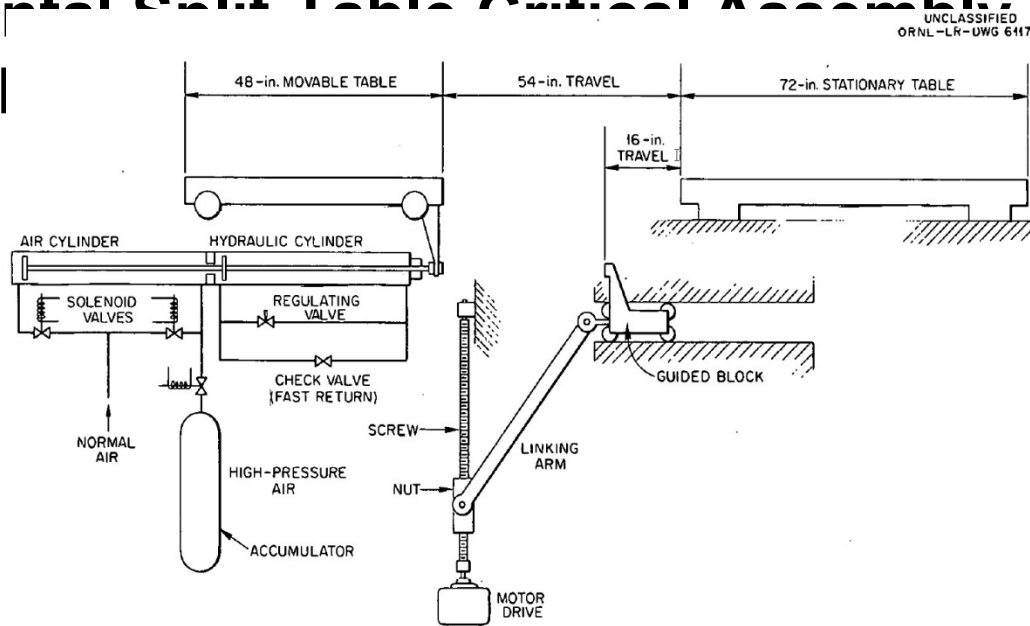
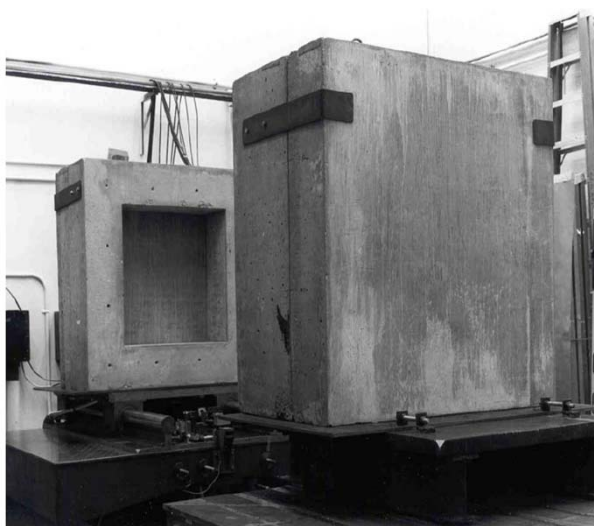
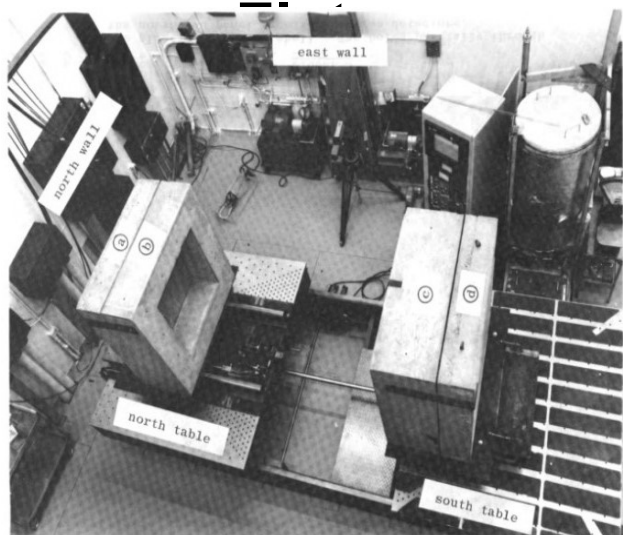


Fig. 3.6.3. Schematic of Drive Arrangement for Split-Table Machine.

Survey of Past Split-Table Machines

- Horizontal Split-Table Critical Assembly – Rocky





Neutron Spectra in the Notional Assemblies

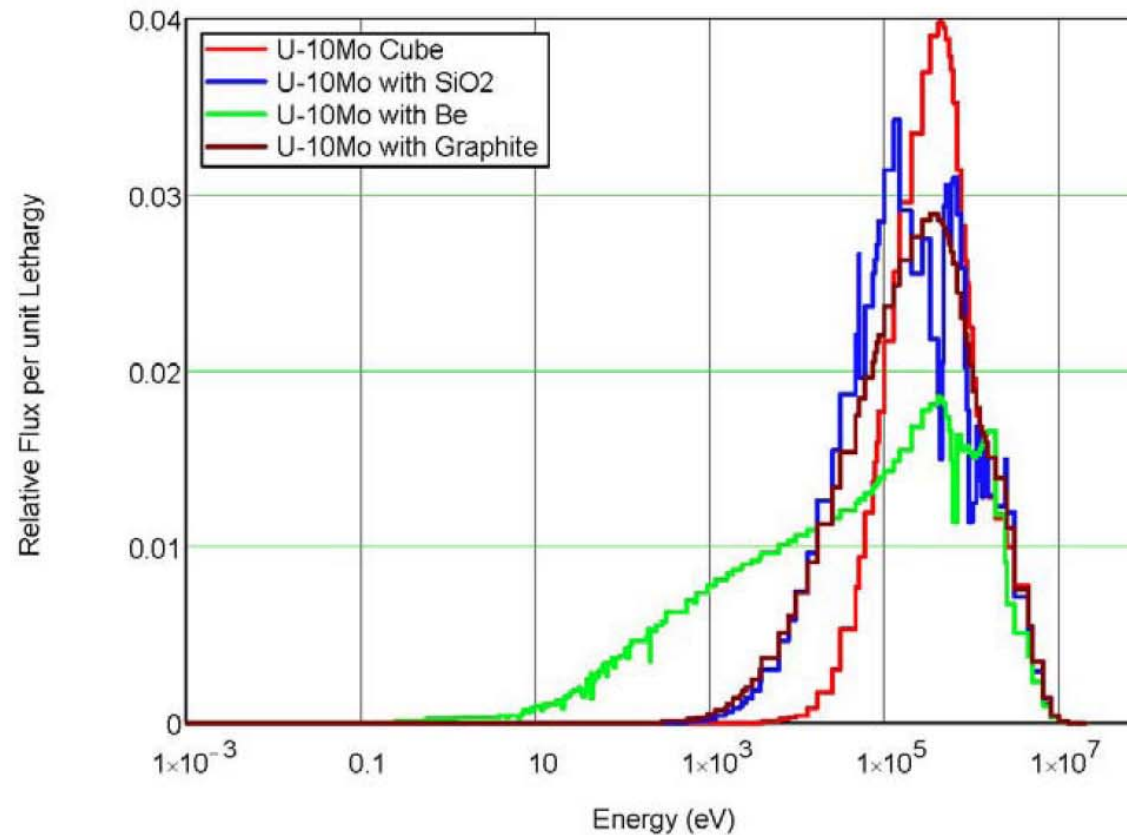


Figure 5-4 Comparison of Neutron Spectra in Four U-10Mo Fueled Systems



Assembly Design Requirements

Experiment:

- 6 ft x 6 ft experiment
- 6,000 kg
- Platform position(s) must be established, maintained, and controlled along a 3-axis reference datum to within approximately 0.0005-inch or better (intent to report in the 4th decimal).
- Platforms are to be flat and parallel (intent to establish these tolerances in the 4th decimal).
- Metal platform, structurally sound to control and maintain position relative to datum tolerances throughout all ranges of motion up to maximum payload.
- Fixed table and movable table must come together and touch.
- Position reporting in three (3) axis is preferred.

Control:

- Platform separates using a simple remote command/control approach with the capability to start, stop, and change direction at the desire of the operator.
- Provision for monitoring and reporting system response will be required for travel speed, direction, and position.
- Safety interlocks will be required to control unintended or inadvertent system response.
- Translation axis must move and be controlled, however, there is no rate of motion (movable table speed) requirements.
- No interface between the split-table control system and the reactor control system (i.e., any SCRAM feature would be performed by the reactor control system).
- Capability to control the split-table locally as well as from a remote control room shall be provided.