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Analysis of 100 SGIP Interconnection Studies

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Analysis of Utility SGIP Interconnection Studies

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Abstract

The purpose of the report is to describe the findings from the analysis of 100 Small Generation Interconnection Procedure (SGIP) studies and describe the methodology used to develop the database. The database was used to identify the most likely impacts and mitigation costs associated with PV system interconnections. A total of 100 SGIP reports performed by 3 utilities and one regional transmission operator (RTO) were analyzed. Each record within the database represents an itemized SGIP report and includes information about the generation facility, interconnection topology, electrical power system characteristics, identified adverse system impacts, mitigation options, and costs associated with interconnection the generation facility. The analysis identified several key findings:

- 44% of generation facilities that entered the SGIP study process had no adverse impact on the electrical power system.
- Interconnection topologies were strongly correlated to the presence/absence of adverse system impacts.
- Protection impacts were the most common adverse system impact.
- 50% of SGIP studies identified total connection costs of less than \$689,431.
- 50% of SGIP studies identified total connection costs per MW of less than \$133,833

ACKNOWLEDGMENTS

Data used for this analysis were obtained from a number of sources that deserve acknowledgment:

- **OATI webOasis** – the majority of SGIP reports were accessed through the OATI webOasis™ portal. The OATI webOasis™ website is used by many transmission providers to publicly publish the availability of open access electrical transmission services. As such, many transmission providers also include SGIP reports on the OATI webOasis™ site. OATI webOasis's main page can be found at: <http://www.oatioasis.com/>
- **PNM** – The entirety of PNM SGIP reports used in this report were accessed through PNM's OATI webOasis™ portal. PNM's SGIP reports can be found at: <http://www.oatioasis.com/pnm/index.html>
- **APS** – The entirety of APS's SGIP reports used in this report were accessed through APS's OATI webOasis™ portal. SGIP reports from APS can be found at: <http://www.oatioasis.com/azps/>
- **PacifiCorp** – The entirety of PacifiCorp SGIP reports used in this report were accessed through PacifiCorp's OATI webOasis™ portal. PacifiCorp SGIP reports can be found by navigating to its webOasis portal: <http://www.oasis.oati.com/ppw/>
- **PJM** – A regional transmission organization (RTO), PJM manages and coordinates the operation of all or part of the transmission system within 13 states. As such, SGIP studies performed within PJM's service area are found on PJM's "Generation Queues: Active" database. All SGIP reports used in this report from PJM were accessed through the database. The database can be found at: <http://www.pjm.com/planning/generation-interconnection/generation-queue-active.aspx>

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NOMENCLATURE

| | |
|-------|--|
| DOE | Department of Energy |
| EPS | Electrical Powers System |
| FERC | Federal Energy Regulatory Commission |
| GF | Generation Facility |
| IC | Interconnecting Customer |
| OATT | Open Access Transmission Tariff |
| OASIS | Open Access Same-Time Information System |
| PCC | Point of Common Coupling |
| RTO | Regional Transmission Operator |
| SGIP | Small Generator Interconnection Procedures |
| SNL | Sandia National Laboratories |
| SVC | Static VAR Compensator |

1. INTRODUCTION

Sandia National Laboratories (SNL) developed a database of Small Generator Interconnection Procedure (SGIP) studies to identify the most common impacts for PV system interconnections and the costs to mitigate adverse system impacts. The definition of an adverse system impact is a negative effect due to the interconnection of a generation facility (GF), which compromises the performance, reliability or safety of the existing electrical power system (EPS). The purpose of the report is to describe the findings from the analysis of 100 SGIP studies and describe the methodology used to develop the database of impacts.

Developed by FERC, the SGIP is a common standard interconnection procedure adopted by many states or used as a guide for developing their own interconnection rules for the distribution system. The SGIP outlines the process a utility and interconnecting customer (IC) performs before interconnecting a small GF to the EPS.

The SGIP applies to GFs of 20 MW or less. The SGIP consists of three evaluation procedures: (1) a 10 kW Inverter Process, (2) a Fast Track process (typically 2-5 MW or less) and (3) a study process¹. SNL was interested in analyzing reports associated with photovoltaic facilities that entered the study process under the SGIP. The goal of the SGIP study analysis was to:

- Classify the interconnection types and facility costs associated with photovoltaic generation interconnection requests.
- Analyze the types of adverse system impacts.
- Identify common mitigation options and analyze the costs associated with the adverse system impacts.

A total of 100 SGIP PV interconnection reports performed by 3 utilities and one regional transmission operator (RTO) were analyzed to determine the types of impacts and associated costs. All reports in the database were performed by electrical system providers (EPS) providers that had either adopted the SGIP completely or with some modifications. The reports used to populate the database were acquired through online queues of the aforementioned utilities and RTO. The online queues for the three utilities were found by navigating to their respective webpage on the OASIS website. OASIS is an internet based tool used to share information relating to electrical power transmission such as price and product availability.

The scope of this database and analysis is to evaluate costs associated with GFs that entered the SGIP study process, and therefore the report does not cover cost data or impacts associated with GFs that were fast tracked and did not enter the study process.

¹ Small Generator Interconnection Procedures(FERC SGIP),
<http://www.ferc.gov/industries/electric/indus-act/gi/small-gen.asp#skipnav>

1.1. SGIP Study Process

The SGIP outlines the formal process utilities and IC must follow when evaluating a request for parallel operation of a GF with the EPS. The request is initiated by an IC to assess the feasibility of interconnecting a new small GF to the EPS or expanding the capacity of an existing GF. In either case the SGIP applies to new facilities and facility expansions with generation outputs of 20 MW or less. When an interconnection request enters the study process, it will go through three levels of review with more stringent study requirements at each new level. Most small generation interconnection studies are evaluated based on the following process:

- **Feasibility Study (FeS)** – identifies any potential adverse system impact associated with interconnecting the GF and determines the feasibility of connecting at various interconnection points.
- **System Impact Study (SiS)** – identifies the electrical system impacts that would result if the proposed GF were interconnected without project modifications, specifically focusing on adverse system impact such as equipment thermal over load ratings, voltage violations, protection requirements and power quality.
- **Facility Study (FaS)** – provides a cost estimate for equipment and labor required to 1) complete the interconnection engineering and construction work and 2) equipment and labor required to mitigate any adverse system impacts identified in the SIS.

Upon the completion of each study a detailed report is prepared and transmitted to the IC. Along with outlining the results of the study the report also defines the utility's additional requirements, the interconnection topology and the interconnection facilities necessary to interconnect the GF to the EPS.

2. DATABASE OVERVIEW

This section provides a brief description of the database and describes the procedures used to standardize information derived from the various SGIP report formats. Each record within the database represents an itemized SGIP report and includes information about the GF, interconnecting EPS, identified adverse system impacts, mitigation options and cost associated with interconnecting the GF. The database is grouped into four categories – Facility & Feeder Information, Adverse System Impacts & Mitigation, Binned Costs and Itemized Interconnection Costs. A full description for each category is found in Appendix B.

The database is a compilation of information derived from multiple SGIP reports performed by three electrical utilities, PNM, Arizona Public Service (APS), PacifiCorp and one regional transmission operator (RTO), PJM. The database contains 100 records; each record within the database is a summary of an SGIP report performed by one of the previously identified data sources. A breakdown of SGIP reports found in the database by facility size and utility is shown in Figure 1. More than half (59%) of the SGIP reports in the database have generation capacities of 6 MW or less. Furthermore, 82% of the SGIP reports in the database have generation capacities of 10 MW or less.

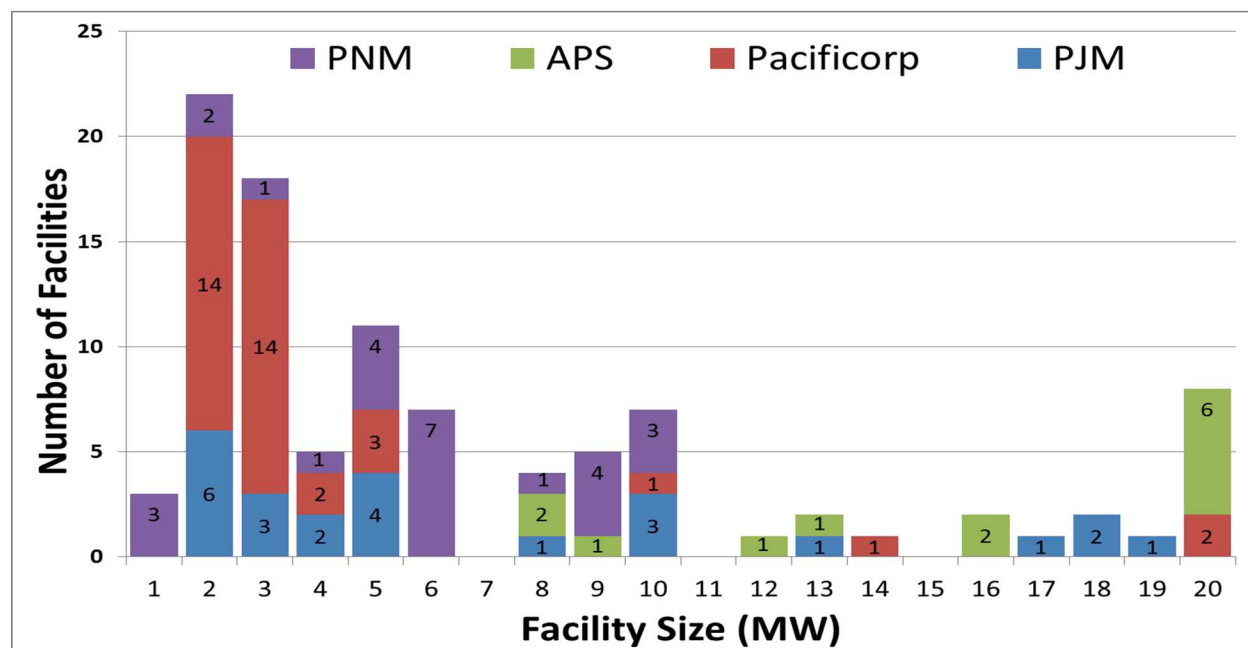


Figure 1. Number of SGIP Reports by Facility Size and EPS provider

SGIP reports found in the database were accessed through online data sources that are available to the public. Specifically, PNM², APS³ and PacifiCorp⁴ reports were accessed through their

² PNM queue, <http://www.oasis.oati.com/PNM/>

respective online queue databases, which are available through the web OASIS website. PJM⁵ reports were accessed through PJM's online queue database found on PJM's website.

Along with the most recent study performed, the queue would generally provide all prior study reports performed on the GF. For example, if a FaS was performed on a proposed GF, the queue would typically provide both the FaS and SiS reports. Also, in some cases, when mutually agreed upon the study process proceeded directly to the SiS without performing a FeS.

SGIP reports found in the database represent facilities at various stages in the study process. Typically each record within the database was developed by reviewing each SGIP report available in the queue. Costs used in the database were derived from the costs reported in the most recent SGIP report. Figure 2 shows the number and types of reports used to develop the cost for each studied GF in the database. In many cases the FeS and SiS were performed at the same time and a single hybrid FeS/SiS report was prepared and made available in the queue.

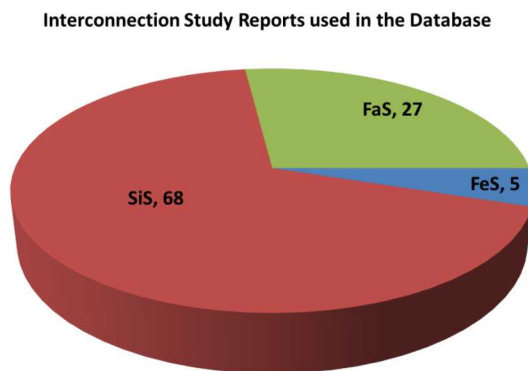


Figure 2. Type of SGIP Study Reports Used in Database.

The types of reports made available in the queues varied by utility. Reports made available through PNM's queue were predominantly only SiS reports. In many cases PacifiCorp and PJM queues provided all three reports with PJM providing FeS/SiS hybrid reports.

A details on of the database structure are described in Appendix B.

³ APS Queue, <http://www.oasis.oati.com/azps/index.html>

⁴ PacifiCorp Queue, <http://www.oasis.oati.com/ppw/index.html>

⁵ PJM Queue, <http://pjm.com/planning/generation-interconnection/generation-queue-active.aspx>

3. UTILITY OVERVIEW

This section provides a brief description of the utilities that provided the SGIP reports. Also, this section highlights trends identified in the SGIP reports for each utility.

3.1. PNM Resources

PNM Resources is an investor-owned energy holding company that operates within New Mexico. Servicing 498,700 electrical customers within New Mexico, PNM Resources is the state's largest electrical provider⁶. SGIP studies obtained from PNM were accessed through PNM's West Trans Oasis (oatioasis.com) webpage. The Database contains 26 SGIP studies from PNM, which are binned by MW size and shown in Figure 3. Facility sizes ranged from 1 MW to 10 MWs with the largest concentration falling within the 6 MW range. A total of 18 studies performed by PNM provided enough information to determine costs associated with interconnection and/or mitigation. Reports performed by PNM provided an abundance of information about the interconnecting EPS. Generally PNM provided substation and feeder load data and detailed distribution circuit figures.

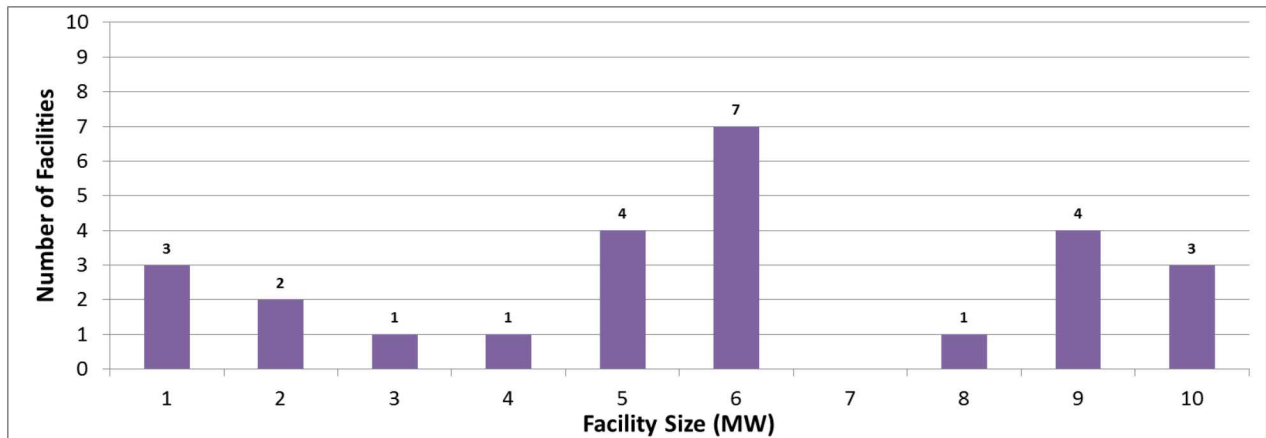


Figure 3. PNM SGIP Reports by Facility Size

This includes normal and emergency substation transformer ratings as well as load data for the interconnecting feeder and adjacent feeders.

All SGIP reports in the database from PNM identified that the GF would interconnect through an existing low voltage distribution circuit (see Interconnection Topology section). Furthermore, all SGIP reports identified interconnection voltages at the PCC of 12.47 kV. No advanced anti-islanding protection schemes other than the inverters build-in functions were required for PNM SGIP studies. PNM SGIP studies also consistently identified the need for IntelliRuptor switches at the ICs GF to facilitate protection requirements.

⁶ Source: <http://www.pnm.com/about/>

3.2. APS

A subsidiary of Pinnacle West Capital Corporation, APS serves over one million customers mainly in northern and central Arizona⁷. SGIP studies obtained from APS were accessed through APS's West Trans Oasis (oatioasis.com) webpage. The database contains 13 SGIP studies from APS, which are binned by MW size and shown in Figure 4. Studied facility sizes ranged from 8 MW to 20 MW with almost half falling within the 20 MW range. All of APS SGIP reports provided enough information to determine interconnection and mitigation costs if any.

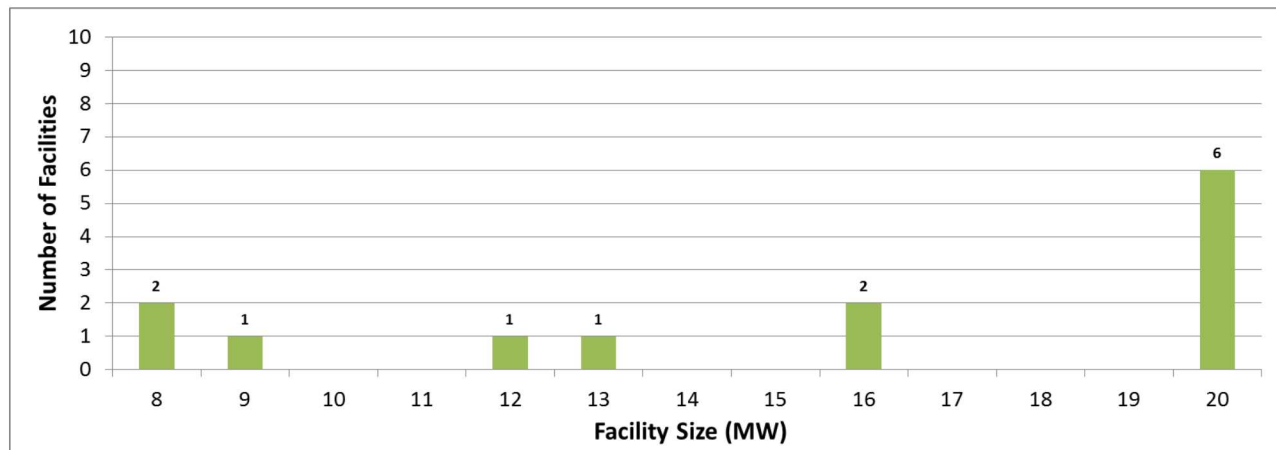


Figure 4. APS SGIP Reports by Facility Size

Reports performed by APS provided detailed information of the conductor requirements and components /modifications required at the interconnecting substation. More than half of APS's SGIP reports identified the need to construct new distribution circuits from the substation to the GF to facilitate the interconnection. The building of new distribution circuits limited the amount of existing equipment exposed to possible adverse system impacts by the GF. In fact, all adverse system impact identified in the SGIP studies occurred on equipment located at the interconnecting substation. Also, almost all SGIP reports identified advanced anti-islanding protection requirements which required equipment that facilitated transfer trip schemes.

In keeping with the definition of adverse system impacts, transfer trip requirements were not considered adverse system impacts, because the GFs interconnected through newly built distribution circuits not through existing circuits. The need to build new distribution circuits and anti-islanding protection requirements accounted for the high total interconnection cost associated with APS SGIP reports.

3.3. PacifiCorp

Through its three subsidiaries, Pacific Power, Rocky Mountain Power and PacifiCorp Energy, PacifiCorp serves approximately 1.8 million customers across six western states. PacifiCorp

⁷ Source: <http://www.aps.com/en/ourcompany/aboutus/companyprofile/Pages/home.aspx>

serves customers across 136,000 square miles in parts of California, Oregon, Washington, Idaho, Utah and Wyoming. PacifiCorp operates 75 generation units, 62,930 miles of distribution line and 16,200 miles of transmission line⁸. SGIP studies obtained from PacifiCorp were obtained through its West Trans Oasis (oatioasis.com) webpage. The Database contains 37 SGIP studies which are binned by MW size and shown in Figure 5. Generation Capacities ranged from 2 MW to 20 MW with the majority (89%) having capacities of 5 MW or less. All of PacifiCorps SGIP studies provided enough detail to identify costs associated with the interconnection of the GF.

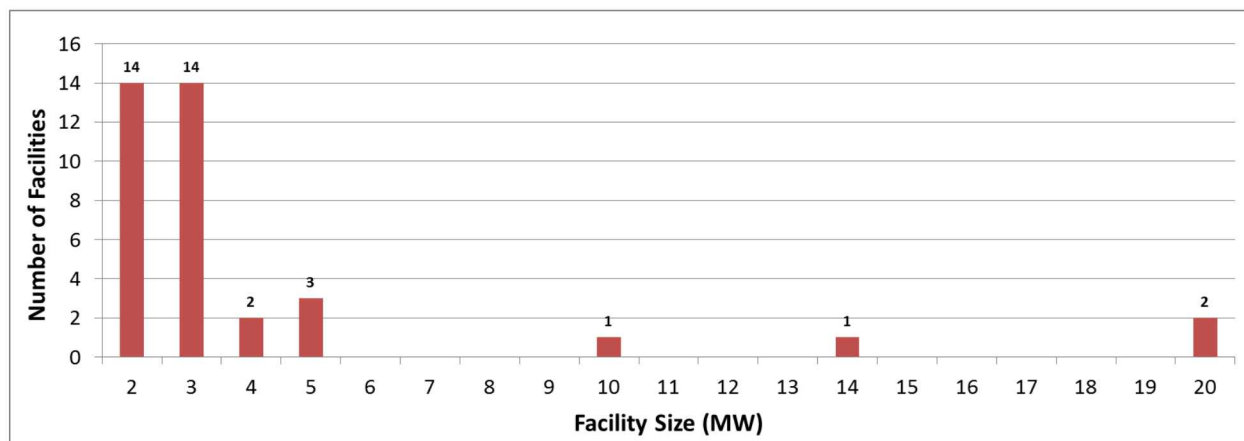


Figure 5. PacifiCorp SGIP Reports by Facility Size.

Reports performed by PacifiCorp provided detailed information in regard to justification of protection equipment required to mitigate adverse system impacts. The majority of GFs entering the study process identified that the GF would interconnect through an existing distribution circuit. PacifiCorps SGIP reports overwhelmingly identified protection impacts requiring advanced relay functions to mitigate anti-islanding concerns and protection schemes to ensure fault protection equipment did not reclose on energized line (see Deadline Checking).

Transfer trip and deadline checking requirements for GFs that interconnected through existing distribution circuits were considered adverse system impacts. This is due to the fact that the protection requirements were needed to protect existing EPS infrastructure. The need to implement anti-islanding and deadline checking protection schemes accounted for the high total interconnection cost associated with PacifiCorp SGIP reports.

3.4. PJM

PJM is a Regional Transmission Operator that coordinates the movement of wholesale electricity for all or parts of Delaware, Illinois, Indiana, Kentucky, Maryland, Michigan, New Jersey, North Carolina, Ohio, Pennsylvania, Tennessee, Virginia, West Virginia and the District of Columbia⁹. Within its territory PJM controls the operation of 183,604 MW of generation and 62,556 miles of

⁸ Source:

http://www.pacificorp.com/content/dam/pacificorp/doc/About_Us/Company_Overview/PC_FACTSHEET_2013_Fweb.pdf

⁹ Source: <http://www.pjm.com/about-pjm/who-we-are.aspx>

high-voltage transmission lines¹⁰. As part of its role as an RTO, PJM also oversees the planning and construction of requests for new generation facilities or increases in the capacity of existing generation facilities request within its territory. With the permission of FERC PJM currently processes interconnection requests according to its own developed interconnection procedures, which are largely based on the SGIP.

The database contains 24 SGIP studies performed jointly by PJM and 4 electrical utilities. The four utilities are: Jersey Central Power and Light (JCP&L), Atlantic City Electric (ACE), First Energy and Public Service Electric and Gas Company (PSE&G). Facility sizes ranged from 2 MW to 19 MW and are binned by MW size as shown in Figure 6. The SGIP studies found in this Database represent only a fraction of the currently 242 active interconnection requests within its queue. Currently the database contains SGIP studies performed from January 2008 to June 2013. A total of 15 studies performed by PJM provided enough information to determine cost associated with interconnection and mitigation.

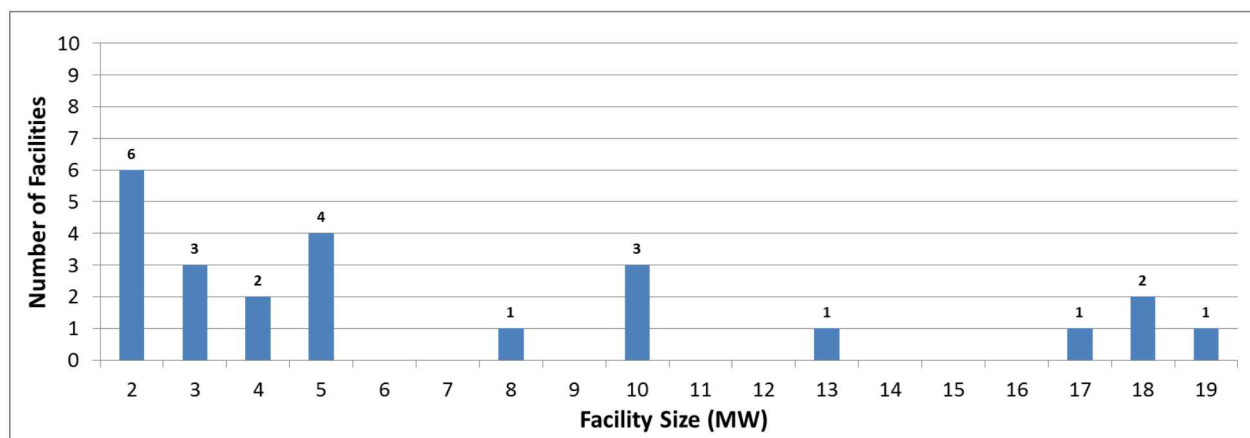


Figure 6. PJM SGIP Reports by Facility Size.

GFs interconnection within PJMs service territory identified the most diverse characteristics. Generation capacities were much more evenly spread from 2 MW to 19 MW and interconnected through a broader range of interconnection voltages (12.47kV, 13.8 kV, 23 kV, 26 kV, 34.5 kV and 46 kV). The three SGIP studies with the most expensive total connection cost came from PJM and the three studies required double feeder service to accommodate the generation capacity of the facility. PJM SGIP reports were the only reports that utilized double feeder service. Mixed FeS/SiS hybrid reports were exclusively found in PJMs queue. Generally, PJM provided FeS, SiS, FaS and Interconnection Service Agreements for all studied GF in the queue.

¹⁰ Source: <http://www.isorto.org/site/c.jhKQIZPBImE/b.8641105/k.BBB9/PJM.htm>

4. INTERCONNECTION TOPOLOGY

The interconnection topology describes the interconnection facilities required to accommodate the interconnection of the GF. The interconnection topologies identified in the SGIP reports were binned into 3 categories: tap existing low voltage distribution circuit, build new distribution circuit from substation, and tap existing high voltage distribution circuit. Each category gives a general indication of the components required to interconnect the GF to the existing EPS.

The decision to interconnect using a specific interconnection topology varied from utility to utility and reflects a combination of factors, such as the proposed location of the GF, distribution system capacity limits and type of interconnection request (new facility or expansion of existing interconnection). In some instances the SGIP reports indicated that the interconnection customer requested a specific interconnection topology, but in most cases it was assumed that the EPS provider determined the topology.

4.1. Tap Existing Low Voltage Distribution Circuit

Facilities were binned within this category if the SGIP report identified that the GFs proposed PCC was located on a distribution circuit that was currently serving customers. Nominal system voltage at the PCC ranged from 12.47 kV to 34.5 kV. Interconnection facilities required for this configuration generally included short spans of conductors with associated poles, metering and communication equipment. Also included in this category were studies that identified the interconnection customer was requesting the expansion of an existing GF. Figure 7 illustrates a GF interconnecting through an existing distribution circuit.

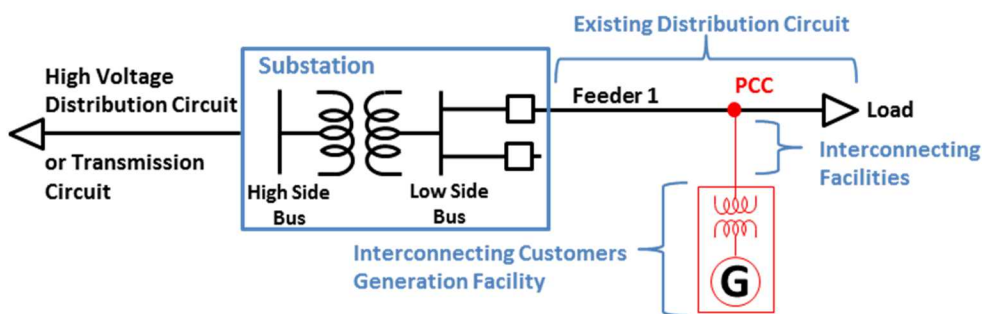


Figure 7. Tap Existing Low Voltage Distribution Circuit Topology

4.2. Build New Distribution Circuit from Substation

Facilities were binned within this category if the report identified the need to construct one or more distribution feeders from the Substation to the GF. This interconnection topology included two distinct interconnection topologies: single feeder service and double feeder service.

Interconnection facilities for single feeder service topology required new three-phase conductors from the substation to the GF. Generally this also included substation modifications such as bus modifications, new feeder position, feeder getaway, and relay equipment. Figure 8 illustrates the circuit topology for facilities requiring a new single feeder distribution circuit.

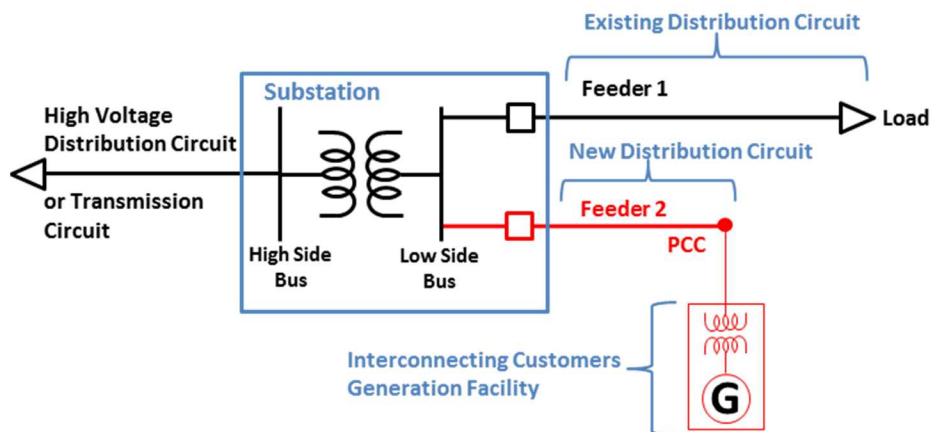


Figure 8. Single Feeder Service Topology

Facilities were binned within the double feeder service topology if the SGIP study identified the need to split the output of the GF between two new distribution feeders, one specifically constructed to service the proposed GF. Double feeder service topologies essentially required two PCCs for the interconnecting GF. Three SGIP studies in the database required double feeder service topologies to interconnect. In all three cases, double feeder service topologies were used to conform to distributive generation capacity limits, which impose a cap on the amount of generation that can be interconnected to distribution feeders and substation transformers.

Figure 9 illustrates a typical double feeder service interconnection for a proposed GF. Interconnection facilities requiring double feeder service included a new three-phase distribution circuit from a new substation transformer to the GF. This topology also typically required modifications to the interconnecting substation such as: a new substation transformer, feeder breaker, relays, and feeder getaway.

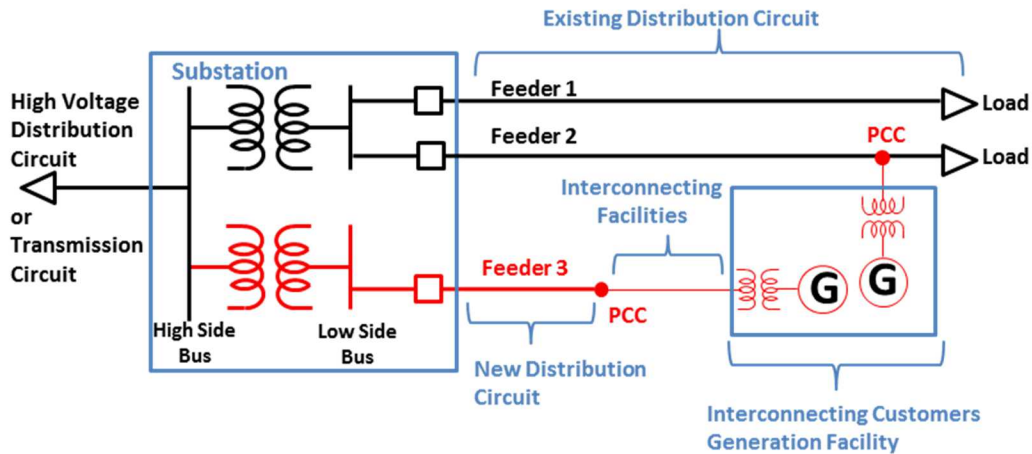


Figure 9. Double Feeder Service Topology

4.3. Tap Existing High Voltage Distribution Circuit

Facilities were binned within this category if the SGIP study identified that the PCC of the GF was located on distribution circuits interconnecting on the high side of the substation transformer. The nominal system voltage for the EPS at the PCC for these facilities was 69 kV or less. Figure 10 illustrates a typical circuit topology for facilities interconnecting through existing high voltage distribution circuits. Interconnection facilities for this configuration typically included conductor spans from the GF to the existing high voltage distribution circuit and metering and communication equipment.

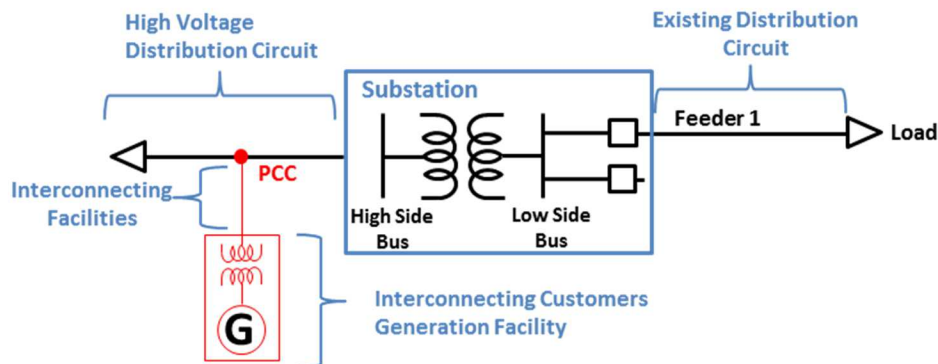


Figure 10. Tap Existing High Voltage Distribution Circuit Topology

5. IMPACT CLASSIFICATION & MITIGATION

This section defines the methodology used to classify impacts identified in the individual SGIP studies. The impacts identified in the SGIP reports fell into four main categories: Overvoltage, Voltage Deviation, Thermal Overload and Protection.

5.1. Overvoltage

Impacts were classified as overvoltage impacts if the SGIP report identified that the proposed GF caused a voltage violation above the voltage range set by the EPS provider. Although not specifically stated in all SGIP reports, it was assumed that overvoltage violations referred to voltage levels exceeding ANSI Range-A. Under normal conditions of Range-A, ANSI C84.1-2011¹¹ requires that service voltage remain within plus or minus 5% of nominal system voltage.

Mitigation for overvoltage impacts were binned into four categories: Inverter PF Correction, LTC Adjustments, Voltage Regulation Control Modifications and Voltage Regulation Equipment Modifications.

Inverter PF Correction

This mitigation category was used to identify SGIP reports that mitigated overvoltage impacts by requiring that inverters located at the GF operate at a power factor (PF) other than unity. SGIP reports identifying inverter PF correction indicate that inverters located at the GF would be either absorbing or injecting reactive power at the PCC to either mitigate voltage rise cause by the interconnection of the GF or address low voltage conditions on the feeder.

LTC Adjustments

This mitigation category was used to identify SGIP reports that mitigated overvoltage impacts by adjusting load tap changer (LTC) settings on the substation transformer.

Voltage Regulation Control Modifications

This mitigation category indicates that overvoltage impacts were mitigated by modifying the controls to existing voltage regulator equipment located on the EPS. In this context voltage regulator equipment would include voltage regulators, capacitor banks and static VAR compensators (SVC). An example of a mitigation that would be binned within the voltage regulator control modifications category would be an SGIP report that identified the need to change the control strategy of a capacitor bank from VAR controlled to voltage controlled.

Voltage Regulator Equipment Modifications

This mitigation category indicates that overvoltage impacts were mitigated by installing new voltage regulator equipment or modifying the location of existing voltage regulator equipment. In this context voltage regulator equipment would include Voltage regulators, Capacitor banks and SVC owned by the EPS provider.

¹¹ Reference: ANSI Standard C84.1-2011 Electrical System Equipment- Voltage Ratings (60Hz)

5.2. Voltage Deviation

Impacts were classified as voltage deviations if the SGIP report identified an excessive voltage difference at a specific point on the EPS between the GF operating at 100% of capacity (online) and the GF operating at 0% of capacity (offline). It's important to note that voltage deviation is not synonymous with voltage flicker. Voltage deviation is a sustained voltage drop or rise caused by the GF coming online or offline, while voltage flicker is a repetitive variation in voltage over a specific time interval. Generally, voltage deviations were identified at the substation low-side bus serving the GF. The mitigation for voltage deviation impacts are the same as those described for overvoltages.

5.3. Thermal Overload

Impacts were classified as thermal overloads when the SGIP report identified that the interconnection of the proposed GF caused a component on the EPS to reach or exceed an operational thermal limit as defined by the EPS operator. Upgrades to existing conductors from single-phase to three-phase to accommodate the interconnection of the GF were not considered thermal impacts. Also, fuse upgrades or fuse location modifications were not included as thermal impacts. This was due to the fact that most SGIP reports did not associate a cost to the fuse modification and when the report did identify costs they were relatively inexpensive.

5.4. Protection

Impacts were classified as protection impacts when the SGIP report identified that existing protection equipment needed modification or new protection equipment was required to accommodate the interconnection of the GF. This also included equipment modifications or new equipment required to perform advanced relay function such as deadline checking or transfer trip schemes. Protection impacts were binned into five classifications: recloser, directional relay, deadline checking, transfer trip, and high side fault protection. The five categories give a general indication of what type of impact was identified and how the impact was mitigated.

Recloser

Impacts were binned into this category if the SGIP report identified that the interconnection of the GF required modifications to the reclosers, the recloser location or the installation of new reclosers to handle increased fault current. Not included in this category are single phase reclosers that were replaced with three phase units in response to single phase lines being converted to three phase.

Directional Relay

Impacts were binned into this category if the SGIP report indicated that the interconnection of the GF required modifications or installation of new relays to protect the EPS from possible faults on the distribution circuit or faults at the substation. Examples include modifications to protect against substation bus faults or upgrades to directional relays to protect the transformer from reverse power flow.

Deadline Checking

Impacts were binned into this category if the SGIP report identified that the interconnection of the GF required a protection scheme to ensure fault protection equipment did not reclose onto an energized line. This was required to ensure that temporary faults on the distribution line have time to clear before protection equipment recloses onto the line. Equipment required for this type of protection scheme generally included new relays and current transformers as well as communication equipment.

Transfer Trip

Impacts were binned into this category if the SGIP report identified that protection of the EPS required a protection scheme to enable fast disconnection of multiple generators. This also includes protection schemes to trip remote relays on adjacent feeders. Typically this included new relays and voltage transformers as well as communication equipment.

High Side Fault protection

Impacts were classified as high side fault protection if the SGIP report identified that the interconnection of the GF required monitoring of faults on the high side of the substation transformer servicing the GF. This includes faults on conductors between substations and faults on the high-side bus of the service transformer. Equipment needed to implement this protection scheme included the installation of relays and equipment at the interconnecting substation and possibly remote substations.

6. GENERAL STATISTICS

This section highlights general statistics found in the dataset. As indicated in Figure 11, facility sizes found in the dataset ranged from 1 MW to 20 MW. Generally, facilities larger than 2 MW but less than 20 MW enter the study process by default. Facilities found in the dataset less than 2 MW entered the study process by failing one or more of the 10 Fast Track Screens. Specifically, the five Fast Track Screens relevant for facilities studied in the dataset are:

- The small generation facility's capacity must be less than 15% of the peak load on the circuit.
- The total small generation facility's contribution to fault current shall not exceed more than 10% of the distribution circuits' maximum fault current.
- The addition of the small generation facility must not cause distribution equipment to exceed 87.5% of short circuit interruption capability.
- The capacity of the small generation facility shall not exceed 10 MW if interconnecting to an area with known transient stability limitations
- No construction of facilities by the Transmission Provider on its own system shall be required to accommodate the small generation facility.

The number of SGIP studies in the database, binned by identified generation capacity is illustrated in Figure 11.

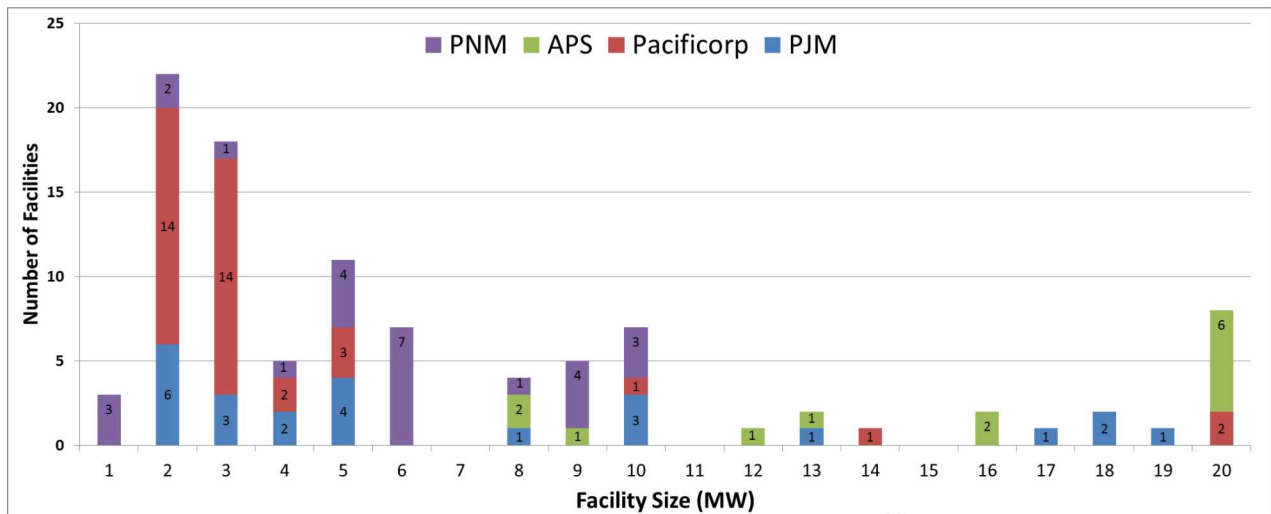


Figure 11. Facility Size Binned by MW¹²

Generation capacities identified in the SGIP reports were largely dependent on which utility data source the reports came from. The majority of SGIP reports that identified generation capacities in the 2 MW range (63%) were reports performed by PacifiCorp. All SGIP reports identifying

¹² The dataset depicted in Figure 11 represent SGIP reports binned by 1MW increments of generation capacity.

facilities in the 6 MW capacity range were performed by PNM, while the majority of reports identifying 20 MW generation capacity were performed by APS. The largest concentration of generation facilities was found in the 2 MW capacity range, with 25% of SGIP reports identifying generation capacities between 2 MW and less than 3 MW. More than half of the dataset, 66% of SGIP studies had generation capacities of less than 7 MW.

The number of SGIP reports binned by interconnection voltage is illustrated in Figure 12. The interconnection voltage was defined as the operational voltage of the electrical system at the PCC. The majority of facilities (70%) found in the dataset interconnect to the 12.47 kV level. All SGIP reports that identified interconnection voltages of 69 kV were also reports that identified 20 MW generation capacities. The remaining 20 MW facilities were split between the 12.47 kV and 34.5 kV interconnection voltages.

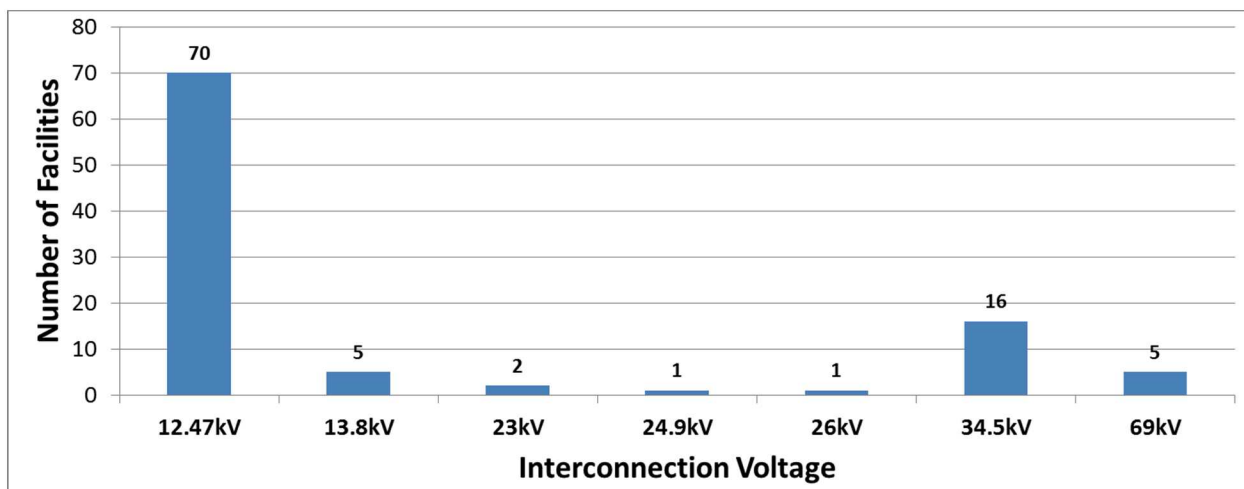


Figure 12. Facilities Binned by Interconnection Voltage

Of the 100 SGIP reports in the database, 99 provided enough information to identify the proposed interconnection topology of the generation facility. The exception was an SGIP report that did not specifically state in the body of text or in the accompanying circuit diagrams whether the GF would interconnect through existing infrastructure or would require new construction. As indicated in Figure 13, ~70% of the studies identified that the GF would interconnect through an existing low voltage distribution circuit.

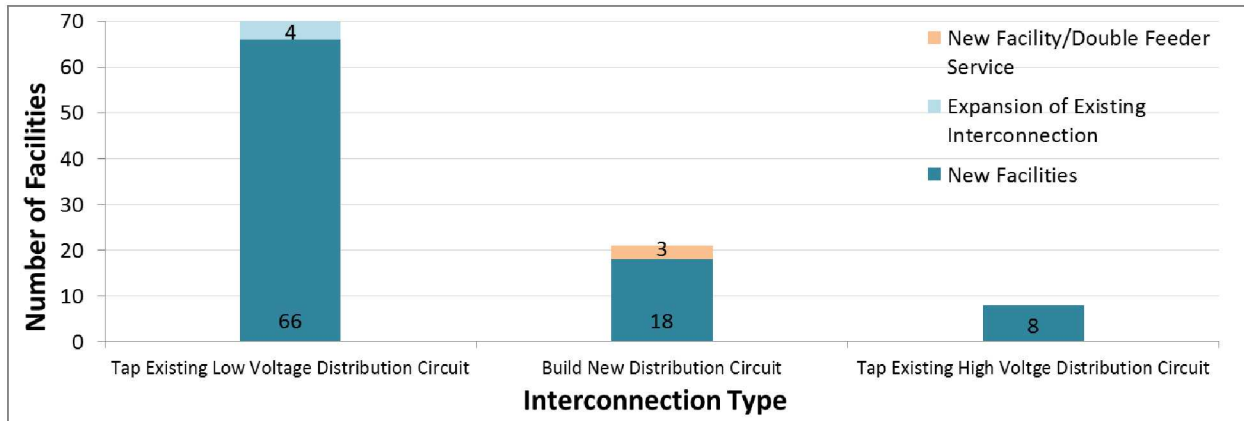


Figure 13. Proposed Interconnection Topology

A breakdown of interconnection topologies by generation capacity is shown in Figure 14 . Interconnection Topologies were largely dependent on the generation capacity of the GF. All SGIP reports that identified interconnecting through existing low voltage distribution circuits had generation capacities of 10 MW or less. Also, the majority of SGIP reports that identified interconnecting through existing high voltage distribution circuits had generation capacities of 20 MW.

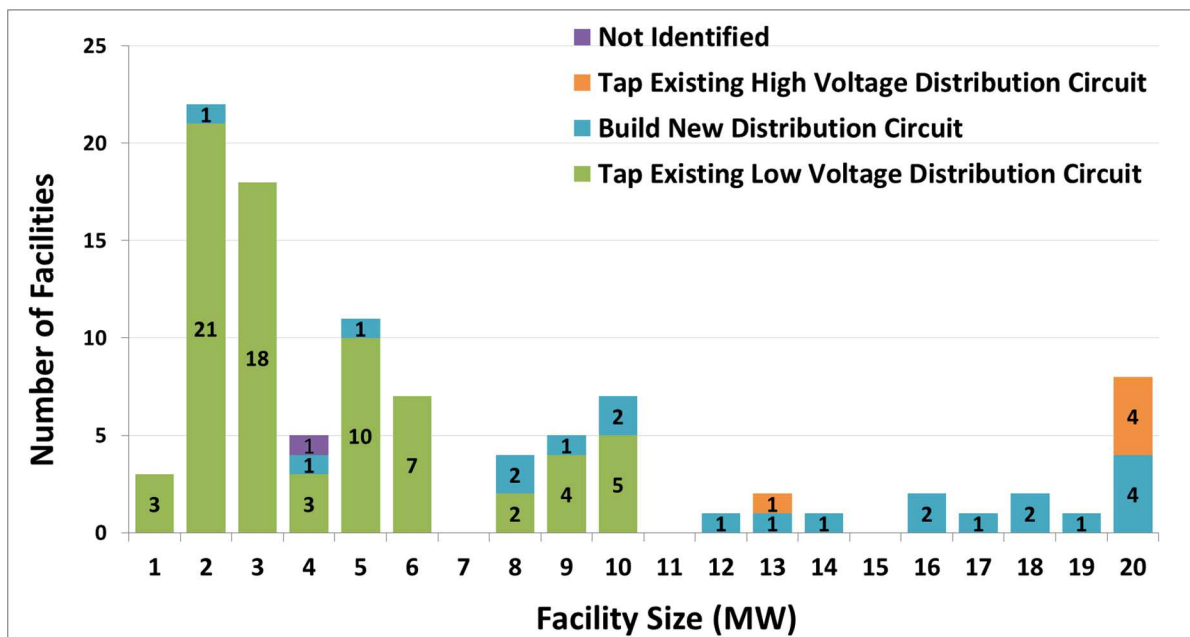


Figure 14. Interconnection Topologies by Facility Size

The interconnection topologies of the GF were strongly correlated to the presence/absence of adverse impacts. Generally, adverse system impacts are more probable if a GF was interconnecting through an existing distribution circuit.

Figure 15 highlights adverse system impact by two interconnection topologies: tap existing low voltage distribution circuit and tap existing high voltage distribution circuit. 68% of generation facilities that identified tapping an existing distribution circuits caused one or more adverse impacts on the EPS.

Adverse system impacts are less probable if the interconnection of the GF required the construction of a new distribution circuit from the substation. As indicated in Figure 16, three facilities (14% of SGIP reports) that identified interconnecting through new distribution circuits had an adverse effect on the existing EPS at equipment located at the substation. The advantage of building new distribution circuits is that the impacts are limited to the equipment located at the interconnecting substation.

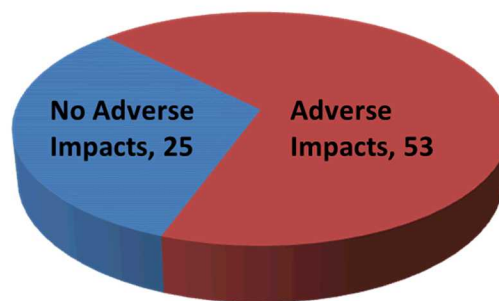


Figure 15. Tap Existing High and Low Distribution Circuits

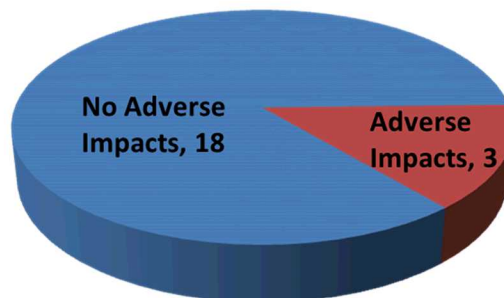


Figure 16. Build New Distribution Circuit¹³

¹³ One SGIP study is left out of the analysis for Figures 15 and 16. The report did not provide an interconnection topology but the report identified no adverse impact caused by the interconnection.

Taking the dataset as a whole regardless of interconnection topology, Figure 17 shows that 44% of SGIP studies identified no adverse system impact imposed on the EPS due to the interconnection of the GF. Facilities that required the construction of new distribution feeders and did not identify adverse system impact were binned in the no adverse impact group.

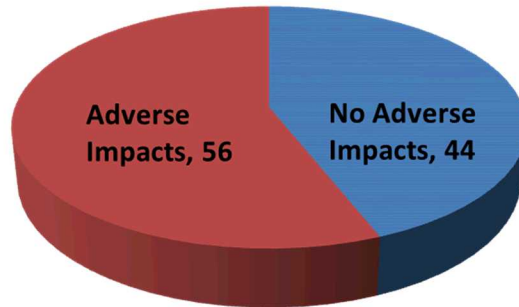


Figure 17. Identified Impacts for All SGIP Studies in Database

7. IDENTIFIED IMPACTS & MITIGATION

The database contains 56 SGIP reports that identified one or more adverse system impacts associated with the interconnection of the GF. Three main impacts identified in the SGIP reports were voltage impacts, thermal overload impacts and protection impacts. The dataset represented in this section is highlighted in Figure 18, where SGIP reports are binned by identified impacts. All thermal overloads occurred in conjunction with other impacts.

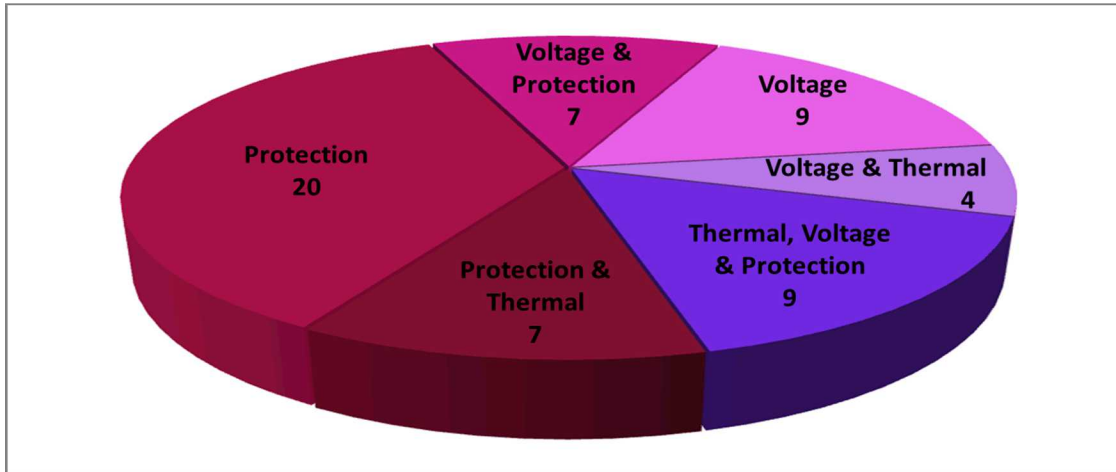


Figure 18. SGIP Reports Binned by Identified Impacts.

7.1. Voltage

This section highlights all SGIP studies that identified a voltage issue requiring mitigation. It is important to note that the facilities highlighted in this section may have had more than one adverse system impact. The subset highlighted in this section is illustrated in Figure 19, where voltage impacts are grouped into four groups, those with purely voltage impacts and those with voltage and one or more other impacts. The voltage impacts identified in the SGIP reports were classified into two categories: Overvoltage and Voltage Deviation. The breakdown between the two categories is illustrated in Figure 20. Overvoltage impacts represent the majority of identified voltage issues.

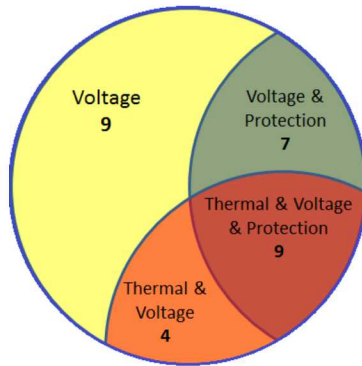


Figure 19. Impact Set¹⁴

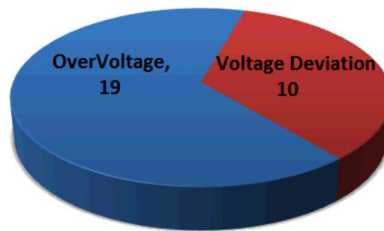


Figure 20. Impact Classification

19 SGIP studies identified overvoltage issues associated with the interconnection of the GF. Overtoltage impacts were mitigated by three methods: inverter PF correction only, voltage regulator equipment changes and Inverter PF correction and conductor upgrades

Table 1 lists the 9 SGIP reports out of 12 that utilized only inverter PF correction at the generation facilities to mitigate overvoltage impacts. Facility sizes ranged from 4 MW-10 MW with interconnection voltages ranging from 12.47 kV-13.8 kV. Utilizing the reactive power control capabilities of the PV inverters provided the added benefit of imposing no added cost to the utility company for mitigating overvoltage impacts.

¹⁴ Subset represents all 29 SGIP reports in dataset that identified a voltage impact.

Table 1: Overvoltage Mitigation Utilizing PF Correction Only

| Study ID | Size | Interconnection Voltage | PF Correction | Mitigation Cost |
|------------------------------------|------|-------------------------|-------------------------------------|-----------------|
| Lost Horizon 10MW | 10.0 | 12.47kV | Operate at 99% Lagging PF \$0.00 | \$0 |
| Project Hondale 9MW | 9.0 | 13.8kV | Operate at 95.5% Leading PF \$0 | \$0 |
| Project Los Chaves | 6.0 | 12.47kV | Operate at 96% Lagging PF \$0 | \$0 |
| Project Alamogordo Airport -Site 1 | 6.0 | 12.47kV | Operate at 99% Lagging PF \$0 | \$0 |
| Project Tularosa 9MN | 9.0 | 12.47kV | Operate at 98.5% Lagging PF \$0 | \$0 |
| Project GDP Tome 9 MW | 9.0 | 12.47kV | Operate at 98.5% Lagging PF \$0 | \$0 |
| Project Pajarito 5,000 KVA | 5.0 | 12.47kV | Operate at 97.5% Lagging PF \$0 | \$0 |
| Project Hondale | 6.0 | 13.8kV | Operate at 97% Lagging PF \$0 | \$0 |
| Project Tome 4MW | 4.0 | 12.47kV | Operate at PF other an unity \$0 | \$0 |

Table 2 lists the 7 SGIP studies that utilized voltage regulator equipment modifications and/or voltage regulator control modifications to mitigate overvoltage impacts. Three out of the seven also used inverter PF correction in the mitigation process. Costs associated with voltage regulator equipment modifications and voltage regulator control modifications ranged from \$3,500 to \$98,562. The lower end cost was associated with modifications to the controls of an existing capacitor bank. The higher end cost was associated with the installation of both a capacitor bank and voltage regulator.

Table 2: Overvoltage Mitigation Utilizing Voltage Regulation Equipment and PF Correction.

| Study ID | Size | PCC Distance | Vreg/Cap/SCV | PF Correction | LTC | Vreg/Cap/SCV | Mitigation Cost |
|------------------------------------|------|--------------|--|--------------------------------|-------------------------|--|-----------------|
| V2-035 | 2 | | • Upgrade Vreg \$89,562 | | | | \$98,562 |
| Q0454 | 3 | 47572 | • Install Line Regulator \$UNK | | | | \$UNK |
| Project Alamogordo Airport -Site 2 | 6.0 | 26,815 | • New 1200kVAR Cap Bank \$UNK | • Operate at 99% lag PF \$0 | | | \$UNK |
| Project Juwi 8MW | 8.0 | 27,562 | • Remove 1800kVar Cap Bank \$0 | • Operate at 98% Lag PF \$0 | | | \$0 |
| Project Tome 10,000KVA | 10.0 | 10,831 | | | | • Upgrade Cap Bank Controller \$3,500 | \$3,500 |
| Project Mesa Del Sol | 10.0 | 21,211 | • New Vreg • New Cap Bank \$50,081 | • Operate at 98% Lag PF \$0 | | | \$50,500 |
| Project Los Morros 9MN | 9.0 | 4,300 | | | • LTC Adjustment \$0 | | \$0 |

Table 3 lists the three overvoltage cases that were mitigated by upgrading conductors. In all three cases, the conductor upgrades were required primarily to mitigate thermal overload impacts that resulted from the interconnection of the GF. The cost associated with conductor upgrades range

from \$104,100 to \$383,700. Facility sizes ranged from 2.1 MW-3 MW and interconnection voltages were at the 12.47 kV class.

Table 3: Overvoltage Mitigation Utilizing Conductor Upgrades

| Study ID | Size | Conductor Upgrade | Vreg/Cap/SCV | Mitigation |
|----------|------|--|-------------------------|------------|
| Q0456 | 2.1 | • Line upgrade of 5808ft from #4ACSR to #4/OAAC \$111,300 | | \$111,300 |
| Q0459 | 3 | • Line upgrade of 5439ft from #6Cu to 4/OAAC \$104,100 | | \$104,100 |
| Q0457 | 2.1 | • Line upgrade of 12144ft from #6Cu to 4/OAAC • Line upgrade of 3696ft from #2ACSR to 4/OAAC \$383,700 | • Vreg Upgrade \$UNK | \$383,700 |

Total Overvoltage Mitigation Costs vs. Facility Size for 17 SGIP reports that identified the costs to mitigate overvoltage impacts is illustrated in Figure 21. Two of the reports had unknown costs. Data points identifying zero cost represent SGIP reports that identified mitigation through the use of inverter PF correction. Non-zero mitigation costs were associated with GFs in the lower and upper MW capacity range. Total overvoltage mitigation costs ranged from \$0 to \$383,700.

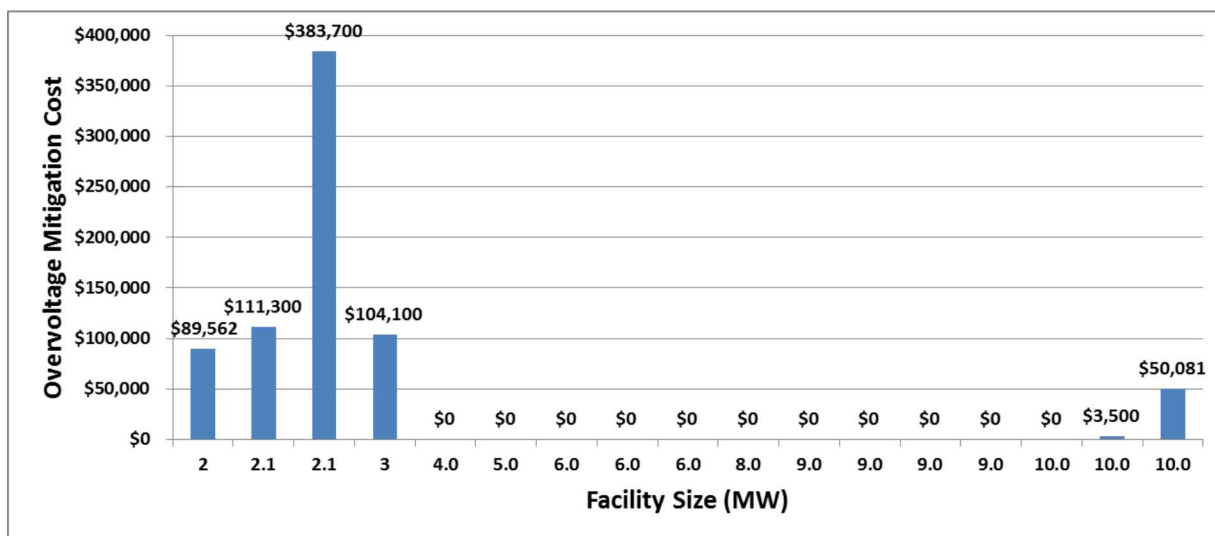


Figure 21. Total Overvoltage Mitigation Cost vs. Facility Size¹⁵

10 SGIP studies identified voltage deviation impact associated with the interconnection of the GF to the EPS. Table 4 identifies the mitigation costs associated with voltage deviation impacts.

¹⁵ Subset represents 17 SGIP reports that identified overvoltage impacts. Two SGIP reports are left out of this subset because the reports did not identify costs associated with mitigating the impact.

Voltage deviation impacts were identified for facilities ranging from 2 MW to 20 MW, with three facilities at 20 MW and the remaining at 5 MW or less. Due to unique mitigation techniques employed for these studies, voltage deviation impacts were some of the most expensive to mitigate. For example, one study identified the need for a 5MVAR Static VAR Compensator to mitigate voltage deviation impacts cause by the interconnection of the GF. Two other studies identified Voltage Deviations at substation busses which required the installation of voltage regulators on every feeder at the substation.

Table 4 Voltage Deviation Mitigation and Costs

| Study ID | Size | Interconnection Voltage | PCC Distance | Vreg/Cap Modifications | Line Upgrade | Mitigation Cost |
|----------|------|-------------------------|--------------|---|---|--------------------|
| U2-059 | 2 | 12.47kV | | <ul style="list-style-type: none"> Reprogram CapBank Upgrade (3) Vregs \$UNK | | \$UNK |
| Q0451 | 2.97 | 12.47kV | 31680 | <ul style="list-style-type: none"> Vreg location Modification \$In Line Upgrade | <ul style="list-style-type: none"> Line upgrade of 22176ft to 477 kcmil AAC \$1,411,200 | \$1,411,200 |
| Q0489 | 3 | 12.47kV | 36960 | | <ul style="list-style-type: none"> Line upgrade 2400ft of #2 ACSR to 477 AAC line upgrade 11000ft of 1/0 ACSR to 477 AAC \$434,800 | \$434,800 |
| Q0491 | 3 | 12.47kV | 27984 | <ul style="list-style-type: none"> Upgrade Vreg \$In Line Upgrade | <ul style="list-style-type: none"> Line upgrade 28433ft #4 ACSR to 795 AAC Line upgrade 1478ft 1/0 ACSR to 795 AAC \$1,703,900 | \$1,703,900 |
| Q0490 | 3 | 12.47kV | 30096 | <ul style="list-style-type: none"> Upgrade Vreg \$In Line Upgrade | <ul style="list-style-type: none"> Line upgrade 19008ft to 477 AAC Line upgrade 12144ft of #2 Al UG to 1000 AL UG \$2,415,100 | \$2,415,100 |
| Q0488 | 3 | 34.5kV | 82896 | <ul style="list-style-type: none"> Replace regulator control \$In Line Upgrade | <ul style="list-style-type: none"> Line Upgrade 64416ft of #6 Copper to 4/0 ACSR \$878,000 | \$878,000 |
| Q0422 | 5 | 12.47kV | | <ul style="list-style-type: none"> New 1200kVAR CapBank \$UNK | | \$UNK |
| Q166 | 20 | 12.47kV | | <ul style="list-style-type: none"> (6) New Vregs \$1,100,000 | | \$1,100,000 |
| Q190 | 20 | 12.47kV | | <ul style="list-style-type: none"> (4) New Vregs \$600,000 | | \$600,000 |
| Q122 | 20 | 69kV | | <ul style="list-style-type: none"> New 5MVAR SCV \$5,000,000 | | \$5,000,000 |

7.2. Thermal

This section highlights the 20 SGIP reports that identified thermal overloads requiring mitigation. The dataset represented in this section is highlighted in Figure 22 where thermal issues are grouped into three categories, those with purely thermal overloads and those with thermal overload and one or more other impacts. As indicated by Figure 22, all 20 SGIP reports identified that thermal overloads occurred in conjunction with one or more other impacts.

Three of the studies discussed in the overvoltage section with overvoltage impacts were mitigated when upgrades to conductors were performed. The conductor upgrades were required primarily to mitigate thermal overload impacts that resulted from the interconnection of the GF and secondarily to mitigate the overvoltage impacts. All three studies were facility sizes of 3 MW or less and the conductor upgrades were to 4/0AAC.

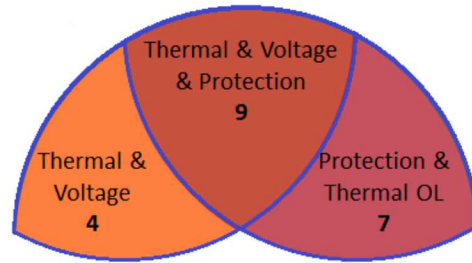


Figure 22. Thermal Overload Impact Set

A breakdown of specific overloaded components is depicted in Figure 23. As indicated in Figure 23 the vast majority of thermal overloads occurred on feeder conductor sections.

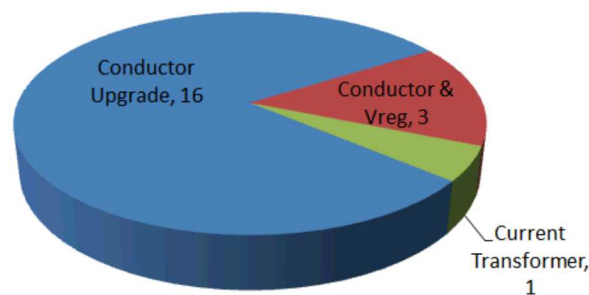


Figure 23. Facilities Adversely Impacted by Thermal Overloads

Table 5 identifies EPS characteristics and thermal overload mitigation costs. Lengths of conductors that experienced Thermal Overloads ranged from 450 ft. to 31,152 ft. with costs to upgrade ranging from \$19.16/ ft. to \$109/ft.

Thermal overloads were identified for facilities interconnecting to EPS at PCC locations ranging from 2,640 ft. to 47,572 ft. from the substation. Facility sizes in this dataset ranged from 2 MW to 10 MW with no obvious correlation between system size and thermal impacts.

Table 5: Thermal Mitigation Costs

| Study ID | Size | PCC Distance | Conductor Length | Conductor Cost/ft | Other Upgrades Component | Cost | Total Thermal Mitigation Cost |
|------------------------------------|------|--------------|--|-------------------|--------------------------|----------|-------------------------------|
| Q0392 | 2 | | 1,750 | \$98.86 | | | \$173,000 |
| Q0456 | 2.1 | | 5,808 | \$19.16 | | | \$111,300 |
| Q0457 | 2.1 | | 15,840 | \$24.22 | | | \$383,700 |
| Q0458 | 2.5 | | 1,200 | \$86.67 | | | \$104,000 |
| Q0463 | 2.97 | | 13,400 | \$65.96 | | | \$883,800 |
| Q0504 | 2.97 | 38,016 | 19,640 | \$47.56 | | | \$934,000 |
| Q0459 | 3 | | 5,439 | \$19.14 | | | \$104,100 |
| Q0471 | 3 | 22,176 | 18,480 | \$68.23 | | | \$1,260,800 |
| Q0454 | 3 | 47,572 | 21,648 | \$UNK | | | \$UNK |
| Q0422 | 5 | | 450 | \$UNK | | | \$UNK |
| Project Alamogordo Airport -Site 2 | 6.0 | 26,815 | 7,233 | \$UNK | | | \$UNK |
| Project Tularosa 9MN | 9.0 | 28,342 | 2,672 | \$67.80 | | | \$181,162 |
| Project GDP Tome 9 MW | 9.0 | 32,159 | 1,026 | \$22.59 | | | \$23,182 |
| Q0490 | 3 | 30,096 | 31,152 | \$UNK | Vreg Upgrade | \$UNK | \$2,415,100 |
| Q0491 | 3 | 27,984 | 29,911 | \$UNK | Vreg Upgrade | \$UNK | \$1,703,900 |
| Project Los Morros 9MN | 9.0 | 4,300 | | | CT Upgrade | \$20,000 | \$20,000 |
| Q0499 | 4.5 | 2,640 | 800 | \$UNK | Vreg Upgrade | \$UNK | \$191,600 |
| Project Mesa Del Sol | 10.0 | 21,211 | 1,875 | \$26.31 | | | \$49,328 |
| Q0376 | 10 | | 6,600 | 108.79 | | | \$718,000 |
| Lost Horizon 10MW | 10.0 | 15,954 | Facility will remain off line during contingency | | | | \$0 |

Table 6 identifies ampacity capacity ratings for conductors before and after they were upgraded. No general trend was identified for conductors that needed to be upgraded.

One SGIP study identified that the interconnection of the GF caused thermal overloads on conductors when the feeder was in contingency configuration. To mitigate the thermal violation the SGIP study identified that the GF would curtail 100% of its output when the feeder was in contingency operation. The study was notable in that it was the only one that identified 100% curtailment of GF output to mitigate a system impact. It was likely that this solution was a cost effective solution for both the utility and the GF owner since contingencies are relatively rare events.

Table 6: Ampacity Upgrades

| Study ID | Size | PCC Distance | Conductor | |
|------------------------------------|--------|-----------------|------------|------------|
| | | | From | TO |
| Q0392 | 2 | | 180 | 510 |
| Q0456 | 2.1 | 13,200 | 140 | 299 |
| Q0457 | 2.1 | 25,872 | 120 180 | 299 299 |
| Q0458 | 2.5 | | 180 | 299 |
| Q0463 | 2.97 | | 180 230 | 510 510 |
| Q0504 | 2.97 | 38,016 | 120 | 510 510 |
| Q0459 | 3 | 16,579 | 120 | 299 |
| Q0471 | 3 | 22,176 | 230 | 510 |
| Q0454 | 3 | 47,572 | 230 | 510 |
| Q0490 | 3 3 | 30,096 | 300 135 | 670 550 |
| Q0491 | 3 3 | 27,984 | 140 230 | 720 720 |
| Q0499 | 4.5 | 2,640 | 170 | 299 |
| Q0422 | 5 | 11,088 | 230 | 299 |
| Project Alamogordo Airport -Site 2 | 6 | 26,815 | 230 | 440 |
| Project Tularosa 9MN | 9 | 28,342 | 340 | 440 |
| Project GDP Tome 9 MW | 9 | 32,159 | 180 | 440 |
| Project Mesa Del Sol | 10 | 21,211 | 180 | 440 |
| Q0376 | 10 | | 490 | 720 |

7.3. Protection

This section highlights the 43 SGIP studies that identified a protection issue requiring mitigation. The dataset represented in this section is highlighted in Figure 24 where protection issues are grouped into four categories, those with purely protection issues and those with protection issues and one or more other impacts. Interconnection voltages for studies identifying protection issues ranged from 12.47 kV to 46 kV, with 32 studies identified 12.47 kV, 1 identifying 13.8 kV, 9 identifying 34.5 kV and 1 identifying 46 kV as the interconnection voltage. Facilities sizes in the dataset ranged from 2 MW to 20 MW, with 41 reports identifying facility sizes less than 10 MW.

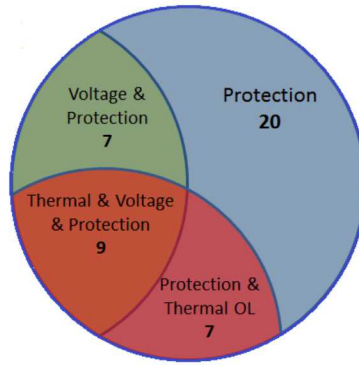


Figure 24. Protection Impact Set

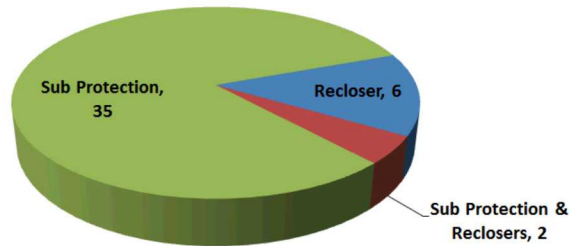


Figure 25. Protection Impact Mitigation

For the purposes of this analysis protection mitigation was binned into two categories: recloser and substation modification. The breakdown between the two categories is shown in Figure 25. The substation protection category includes impacts requiring deadline checking, transfer trip directional relays and high side fault protection. The majority of the reports that identified protection impacts required substation modifications to interconnect the GF.

Table 7 highlights a subset of the substation protection category, those that only required relay modifications to mitigate protection impacts. Generally the relay modifications were required to protect the EPS from possible faults on the substation bus or faults in the substation transformer. Facility sizes for the 5 SGIP studies ranged from 2 MW-13 MW with mitigations costs ranging from \$2,000 to \$505,200.

Table 7: Substation Fault Protection- Relay Modifications Only

| Study ID | Size | Interconnection Voltage | PCC Distance | Protection Requirments | Protection Mitigation Cost |
|------------------------------------|------|-------------------------|--------------|------------------------|----------------------------|
| Project Bonanza | 2.0 | 12.47kV | 8,409 | Relay Adjustment | \$UNK |
| Project Alamogordo Airport -Site 1 | 6.0 | 12.47kV | 27,525 | Relay Adjustment | \$5,000 |
| Project Las Vegas | 6.0 | 12.47kV | 10,900 | Relay adjustment | \$0 |
| Project Hondale 9MW | 9.0 | 13.8kV | 16,737 | Directional Relay | \$2,000 |
| V4-077 | 13 | 46kV | 2640 | Relay Upgrades | \$505,200 |

Table 8 summarizes the remainder of substation protection impacts, those that required relay modification in conjunction with advanced protection schemes. Thirty studies identified the need for advanced relay functionality to mitigate protection impacts. Facilities sizes ranged from 2 MW to 20 MW with a majority (28 reports) identifying facilities 5 MW or less. SGIP reports that identified the need for advanced relay functions exhibited large variations between mitigation costs, which ranged from \$74,600 to \$1,300,000. The variation was attributed to the fact that implementing advanced relay functionality did not conform to a standard procedure. Some implementations only required communication lines from the substation to the GF while others required major construction modifications at the substation to install the required equipment. Modifications ranged from substation bus expansion to full substation expansions.

Table 8: Substation Fault Protection- Relay Modifications & Advanced Protection Schemes

| Study ID | Size | Interconnection Voltage | PCC Distance | Directional Relay | Deadline Checking | Transfer Trip | High Side Faults | Recloser | Protection Mitigation Cost |
|----------|------|-------------------------|--------------|-------------------|-------------------|---------------|------------------|----------|----------------------------|
| Q0463 | 2.97 | 12.47kV | | Directional Relay | Deadline Checking | Transfer Trip | | Recloser | \$667,900 |
| Q0493 | 3 | 12.47kV | 9950 | | Deadline Checking | Transfer Trip | | Recloser | \$257,400 |
| Q0499 | 4.5 | 12.47kV | 2640 | | Deadline Checking | Transfer Trip | High Side Faults | | \$632,200 |
| Q0376 | 10 | 12.47kV | | | Deadline Checking | Transfer Trip | High Side Faults | | \$1,177,200 |
| Q0310 | 20 | 34.5kV | | | | | High Side Faults | | \$1,300,000 |
| Q0456 | 2.1 | 12.47kV | | Directional Relay | Deadline Checking | Transfer Trip | | | \$618,900 |
| Q0457 | 2.1 | 12.47kV | | Directional Relay | Deadline Checking | Transfer Trip | | | \$1,048,700 |
| Q0385 | 2.75 | 12.47kV | | Directional Relay | Deadline Checking | Transfer Trip | | | \$435,000 |
| Q0451 | 2.97 | 12.47kV | 31680 | Directional Relay | Deadline Checking | Transfer Trip | | | \$642,900 |
| Q0459 | 3 | 12.47kV | | Directional Relay | Deadline Checking | Transfer Trip | | | \$961,500 |
| Q0471 | 3 | 34.5kV | 22176 | Directional Relay | | Transfer Trip | | | \$112,100 |
| Q0454 | 3 | 34.5kV | 47572 | Directional Relay | Deadline Checking | Transfer Trip | | | \$223,800 |
| Q0392 | 2 | 12.47kV | | Directional Relay | | Transfer Trip | | | \$264,000 |
| Q0249 | 2.3 | 12.47kV | | Directional Relay | Deadline Checking | | | | \$74,600 |
| Q0458 | 2.5 | 12.47kV | | | Deadline Checking | Transfer Trip | | | \$117,600 |
| Q0492 | 3 | 12.47kV | 5280 | | Deadline Checking | Transfer Trip | | | \$211,300 |
| Q0475 | 3 | 12.47kV | 11088 | | Deadline Checking | Transfer Trip | | | \$300,000 |
| Q0489 | 3 | 12.47kV | 36960 | | Deadline Checking | Transfer Trip | | | \$380,100 |
| Q0491 | 3 | 12.47kV | 27984 | | Deadline Checking | Transfer Trip | | | \$472,200 |
| Q0490 | 3 | 12.47kV | 30096 | | Deadline Checking | Transfer Trip | | | \$404,900 |
| Q0464 | 3 | 34.5kV | 47572 | | Deadline Checking | Transfer Trip | | | \$NONE |
| Q0488 | 3 | 34.5kV | 82896 | | Deadline Checking | Transfer Trip | | | \$518,000 |
| Q0422 | 5 | 12.47kV | | | Deadline Checking | Transfer Trip | | | \$241,600 |
| Q0495 | 4.8 | 12.47kV | 5193 | | Deadline Checking | | | | \$116,200 |
| Q0389 | 2 | 12.47kV | | | Deadline Checking | | | | \$511,000 |
| V4-075 | 2 | 12.47kV | | | | Transfer Trip | | | \$130,000 |
| Q0502 | 2.97 | 12.47kV | 7920 | | | Transfer Trip | | | \$274,400 |
| Q0504 | 2.97 | 12.47 | 38016 | | | Transfer Trip | | | \$122,500 |
| Q0455 | 3 | 34.5kV | 47572 | | | Transfer Trip | | | \$NONE |
| Q0473 | 3 | 34.5kV | 28512 | | | Transfer Trip | | | \$NONE |
| Q0472 | 3 | 34.5kV | 14256 | | | Transfer Trip | | | \$NONE |
| V4-068 | 5 | 34.5kV | 23,760 | | | Transfer Trip | | | \$UNK |

SGIP reports that identified the need to monitor high side faults represent the most expensive mitigation costs for facilities requiring advanced relay functionality. This was attributed to the fact that monitoring high side faults required the installation of equipment on high side conductors servicing substation and at remote substations. Table 9 summarizes key characteristics identified in the SGIP studies for facilities using reclosers to mitigate protection impacts. Two SGIP studies identified the need to install more than one recloser to mitigate the identified protection impacts. As indicated in Table 9, facilities sizes ranged from 2 MW to 9 MW. Mitigation cost utilizing reclosers ranged from \$45,000 to \$178,900.

Table 9: Protection- Recloser Modifications

| Study ID | Size | Interconnection Voltage | PCC Distance | # Units | Protection Mitigation Cost |
|-----------------------------|------|----------------------------|-----------------|---------|-------------------------------|
| V2-035 | 2 | 12.47kV | | 1 | \$67,850 |
| U2-059 | 2 | 12.47kV | | 1 | \$UNK |
| Q0211 | 2.75 | 12.47kV | | 2 | \$178,900 |
| Project Los Morros 6,000 KW | 6.0 | 12.47kV | 4,155 | 2 | \$90,000 |
| Project Los Morros 9MN | 9.0 | 12.47kV | 4,300 | 1 | \$45,000 |
| Project Tularosa 9MN | 9.0 | 12.47kV | 28,342 | 1 | \$45,000 |

8. COST ANALYSIS

The analysis highlighted in this section is for the 90 SGIP reports which provided enough information to identify costs associated with the interconnection of the GF. This section provides a general cost overview of the 90 SGIP studies along with an analysis of costs by interconnection topology.

Total connection cost was defined as the aggregate of mitigation and interconnection facilities costs to safely and reliably interconnect the GF. Total connection cost vs. facility size is illustrated in Figure 26 for the 63 studies that identified total connection costs. Each data point is color coded to identify the interconnection topology. Figure 26 shows total connection costs ranging from \$22,000 to \$11,516,445 with 50% of SGIP studies having a total connection cost of less than \$689,431.

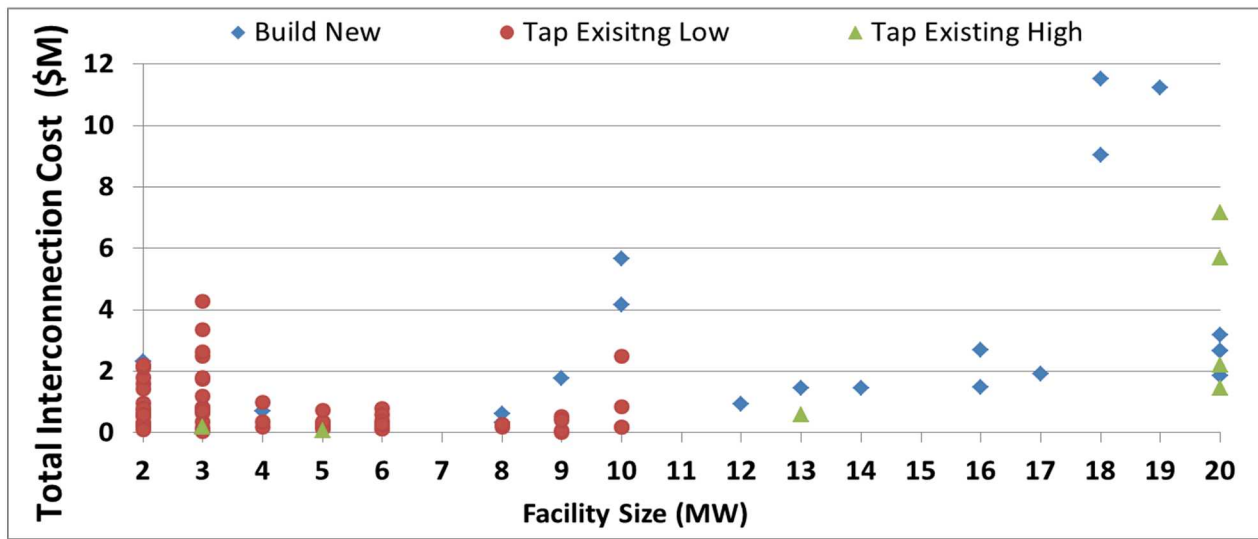


Figure 26 Total Connection Costs vs. Facility Size¹⁶

The three most expensive facilities depicted in Figure 26 represent facilities that identified the need to split the generation between two substation transformers. Furthermore all three required the installation of a new transformer at the substation as well as the construction of new distribution circuits from the substation to the GF. All three SGIP studies came from PJM and were identified as V4-023, V4-024 and V2-046 with interconnection cost of \$11.5 million, 9 million and 11.2 million respectively.

Total connection cost vs. interconnection voltage for the 63 SGIP reports is shown in Figure 27. The three most expensive GF identified in the dataset are found in the 12.47 kV class, and

¹⁶ Subset represents 63 SGIP reports that identified total connection costs.

represent the three facilities identified previously. The two least expensive facilities with total connection cost of \$22,000 and \$29,150 are found at 13.8 kV and 34.5 kV respectively.

Generation facilities interconnecting through 12.47 kV circuits had the largest total connection cost variation. Total connection costs for generation facilities interconnecting through 12.47 kV circuits vary from \$65,000 to \$11,451,445. The smallest total connection cost variation occurs when interconnection through 13.8 kV circuits. Total connection costs for generation facilities interconnecting through 13.8 kV circuits vary from \$22,000 to \$321,000.

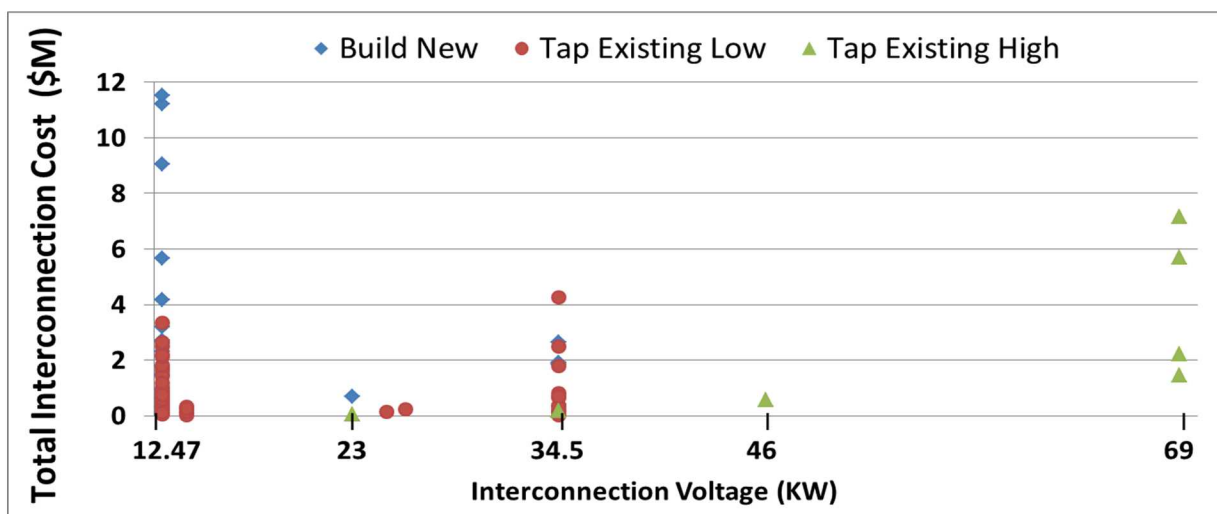


Figure 27 Total Connection Cost vs. Interconnection Voltage¹⁷

Total connection costs vs. facility size for SGIP reports that identified adverse system impacts is depicted in Figure 28. The subset illustrated in Figure 28 represents 53 SGIP reports. Total connection cost for studies that identified adverse impacts ranged from \$22,000 to \$7,165,454. 50% of SGIP studies identifying adverse system impacts had a total connection cost of less than \$700,000.

¹⁷ Subset represents 63 SGIP reports that identified total connection costs.

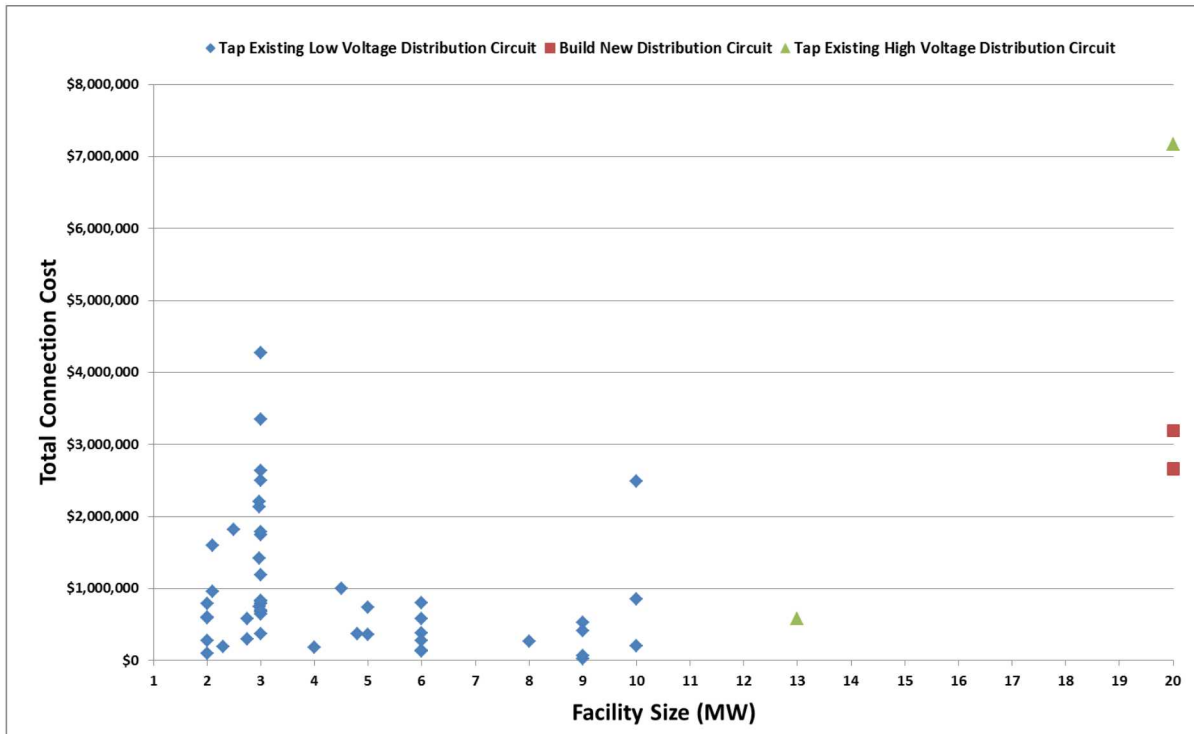


Figure 28. Facilities with Adverse System Impacts¹⁸

The variability in costs shown in Figure 28 reflects many factors such as facility size, mitigation requirements and interconnection configuration. The following sections address costs in relation to the various interconnection topologies.

8.1. Tap Existing Distribution Circuit

This section addresses costs associated with generation facilities identified as interconnecting through an existing distribution circuits. The 62 SGIP reports shown in Figure 29 have total connection cost varying between \$22,000 and \$4,273,200. All SGIP studies which identified the GF interconnecting through an existing distribution circuit are facilities of 10 MW or less. 50% of facilities interconnecting through existing distribution circuits had a total connection cost of less than \$519,600 and 80% had a total connection cost less than \$1,000,000.

¹⁸ Subset represents 53 SGIP reports that identified adverse system impacts and total costs to mitigate.

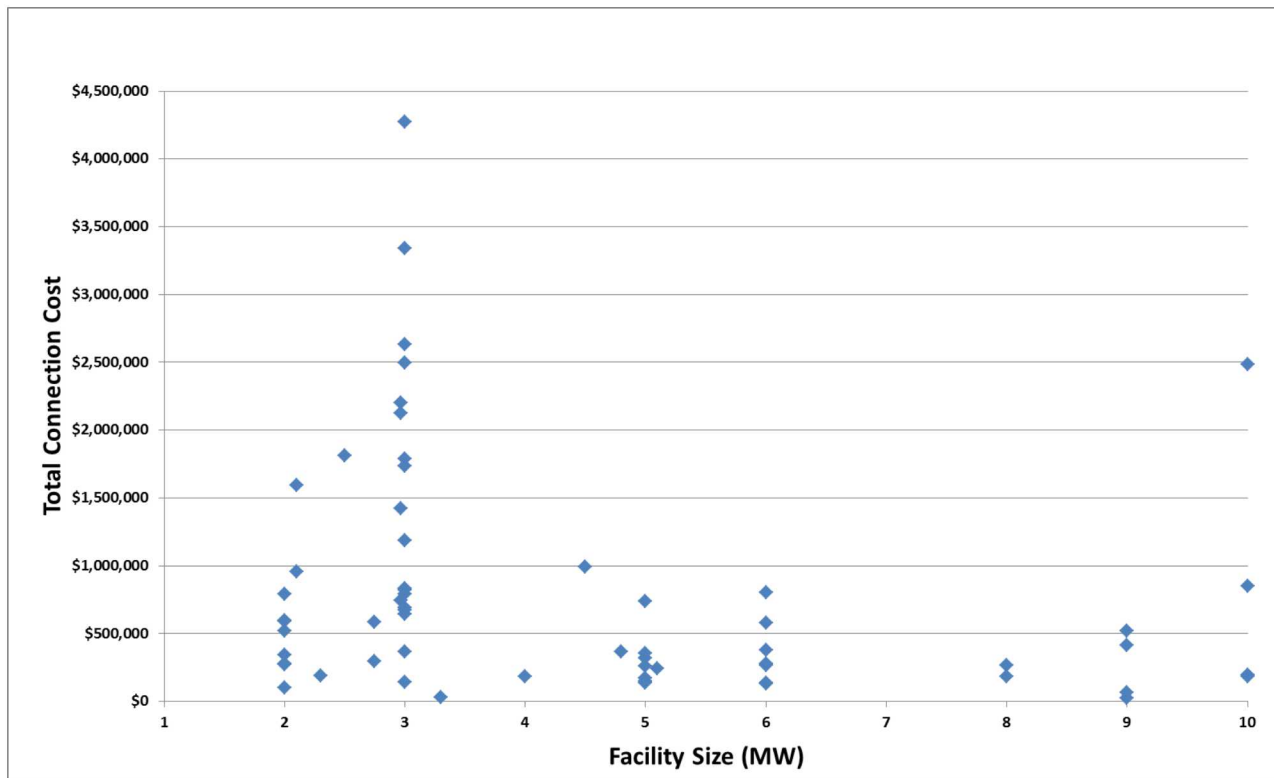


Figure 29: Total Connection Cost vs. Facility Size for GF Interconnecting Through Existing Distribution Circuit¹⁹

The price per MW for facilities interconnecting through existing distribution circuits is illustrated in Figure 30. The total connection cost per MW ranged from \$2,444 per MW to \$1,424,400 per MW. The largest price variation occurs for 3 MW facilities which ranged from \$8,833 to \$1,424,400. 50% of facilities had a total cost per MW of less than \$133,833.

¹⁹ Subset represents 62 SGIP reports that identified interconnecting through existing distribution circuits. This includes both tap existing low voltage distribution circuits and tap existing high voltage distribution circuit topologies.

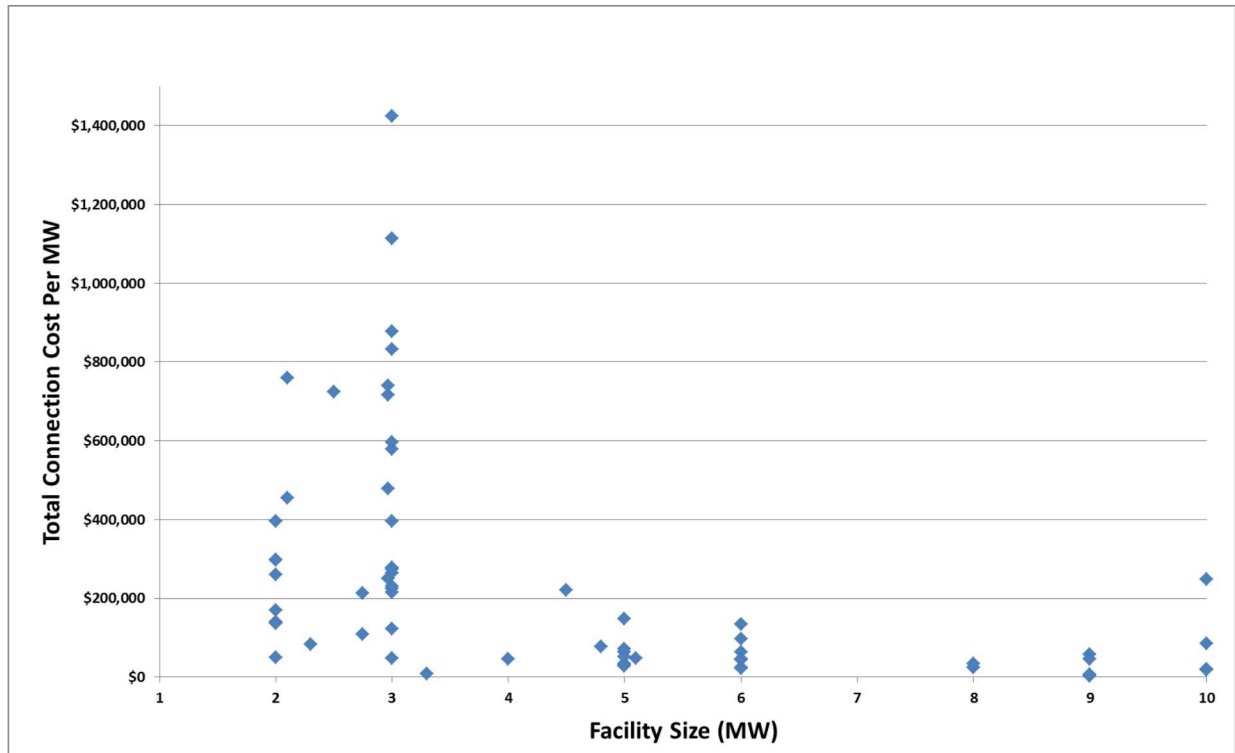


Figure 30. Price per MW vs. Facility Size for GF Interconnecting Through Existing Distribution Circuit²⁰

A subset of the data discussed above, facilities identified as not having an adverse system impact is depicted in Figure 31. The dataset contains 14 facilities with total connection cost per MW varying between \$8,833 and \$259,800. 80% of facilities identified in Figure 31 had total connection cost per MW of less than \$64,200.

²⁰ Subset represents 62 SGIP reports that identified interconnecting through existing distribution circuits. This includes both tap existing low voltage distribution circuits and tap existing high voltage distribution circuit topologies.

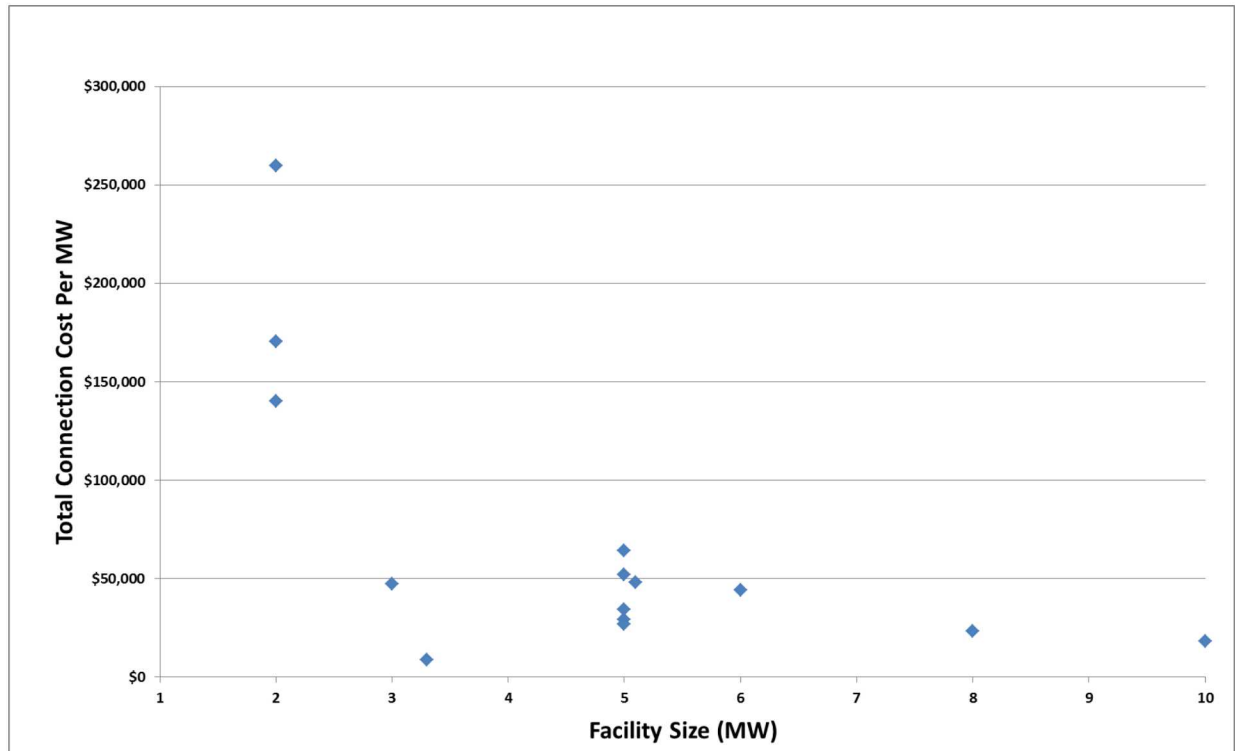


Figure 31. Total Connection Cost per MW vs. Facility Size for GF Interconnecting through Existing Distribution Circuit that had No Adverse Impacts²¹

8.2. Build New Distribution Circuit from Substation

This section addresses total connection costs for SGIP studies that identified the GF would require the construction of a new distribution circuit from the substation to the GF. The dataset illustrated in Figure 32 includes both facilities with and without adverse system impacts and contains a total of 19 SGIP studies. Total connection cost for the studies illustrated in Figure 32 ranged from \$325,000 to \$11,516,445. The three most expensive facilities identified represent facilities that required double feeder service. All three facilities were interconnecting to 12.47 kV systems and ranged from 18 MW to 19.9 MW in size. 50% of facilities had a total connection cost of less than \$2 million.

²¹ Subset represents 14 SGIP reports that did not identify adverse impacts and were interconnecting through existing distribution circuits. This includes both tap existing low voltage distribution circuits and tap existing high voltage distribution circuit topologies.

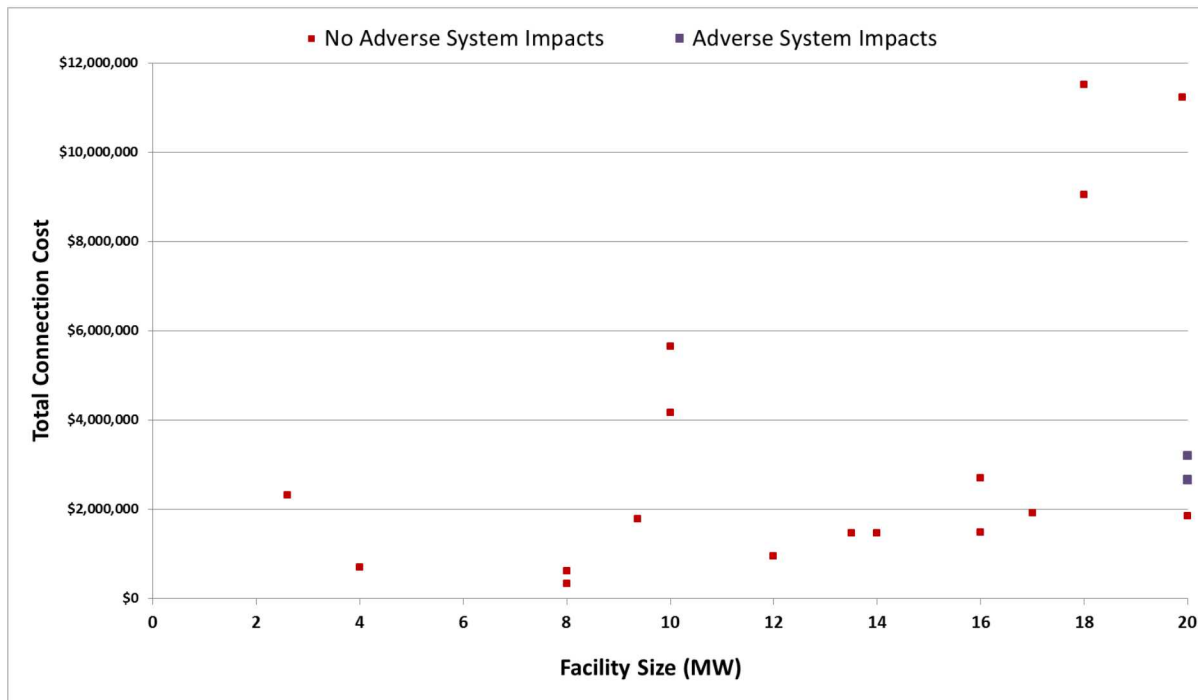


Figure 32. Build New Distribution Circuit: Total Connection Cost vs Facility Size

Generally, building new distribution circuits limited the amount of distribution equipment exposed to possible adverse impacts. But impacts were still identified at the substation for facilities of sufficient generation capacity. Three SGIP studies identified adverse system impacts associated with the GF interconnecting through a new distribution circuit and each study was for a 20 MW system. Two of the impacts were identified as voltage deviation issues caused by the output capacity of the GFs. The two voltage deviation issues occurred at the substation bus and required the installation of voltage regulators on all feeders of the bus. The final study of the three required line pilot relaying to protect remote substations from exposure cause by substation contingency operations. The SGIP report identified the need to install a 138 kV breaker, VT's and CT's at a remote substation as well as installing VT's at the substation servicing the GF.

8.3. Interconnection and Mitigation Cost Ratio

Mitigation for overvoltage impacts were accomplished through the use of inverter PF correction, LTC adjustments, voltage regulation control modifications, and voltage regulation equipment modifications. 15 of the 19 reports identifying overvoltage impacts provided mitigation costs. 9 reports required only PF correction at the inverters to mitigate the identified overvoltage impacts. The remainder of the reports required a combination of inverter PF correction and other mitigation strategies. Figure 33 shows the proportion of overvoltage mitigation costs with respect to total interconnection costs.

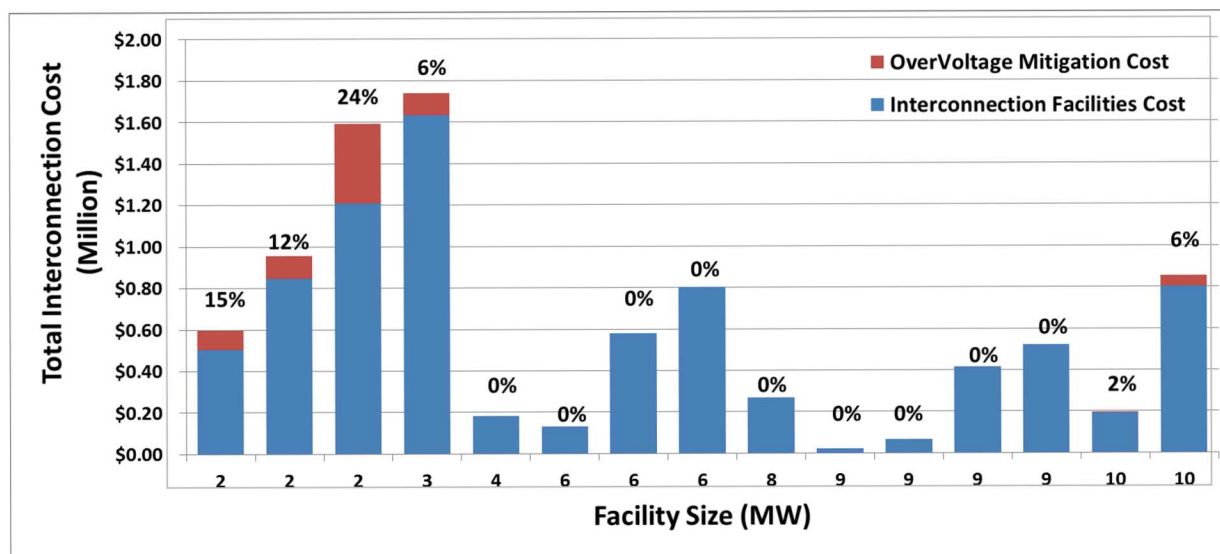


Figure 33 Overvoltage Mitigation Costs

Facilities in Figure 33 with zero mitigation cost represent the SGIP reports that mitigated overvoltage impacts with inverter PF correction, roughly half. Utilizing the GF's inverters to regulate reactive power eliminated the need for the utility to mitigate overvoltage impacts. Mitigation costs for overvoltage impacts ranged from 0% to 24% of the total interconnection cost, as shown in Fig. 33. Actual costs for overvoltage mitigation ranged from \$0 to \$383,700.

10 SGIP reports identified a voltage deviation impact. Voltage deviations were defined as a voltage change greater than 3% between the base case and the PV case at any point on the feeder. Figure 34 shows the proportion of mitigation cost to total interconnection costs for 8 of the SGIP reports that identified costs for mitigating voltage deviation impacts. Mitigating voltage deviations required a combination of mitigation strategies including: installing new voltage regulator equipment, modifications to voltage regulator equipment locations, and conductor upgrades.

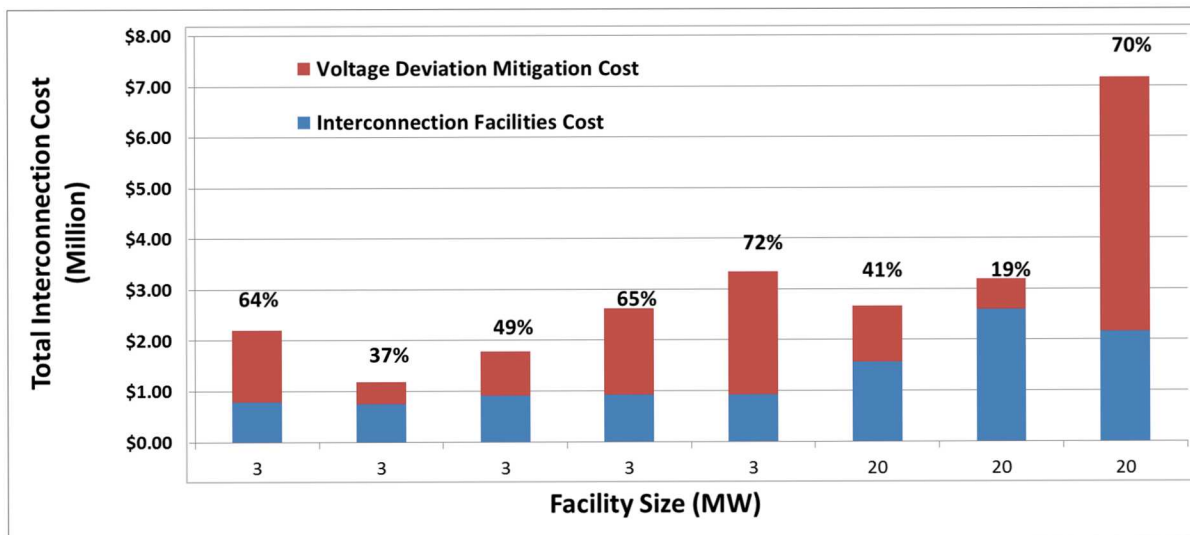


Figure 34. Voltage Deviation Mitigation Costs

Due to unique mitigation techniques, voltage deviation impacts were identified as being some of the most expensive to mitigate. One study identified the need for a 5 MVAR Static VAR compensator. Two other studies identified voltage deviations at the substation bus requiring the installation of voltage regulators on all substation feeders. Mitigation costs for voltage deviation impacts ranged from 19% to 72% of the total interconnection cost, as shown in Figure 34. Actual cost for voltage deviations ranged from \$434,800 to 5,000,000.

20 SGIP reports identified thermal overloads requiring mitigation. 17 SGIP reports provided mitigations costs for thermal impacts. The proportion of mitigation to total connection costs for reports that identified mitigation costs are illustrated in Figure 35.

The majority of thermal impacts occurred on feeder conductor sections. 4 SGIP reports required both upgrades to conductor sections and upgrades to voltage regulator equipment to mitigate thermal impact violations. Mitigation costs for thermal impacts ranged from 6% to 72% of the total interconnection cost. Actual costs for thermal mitigation ranged from \$20,000 to \$2,415,100.

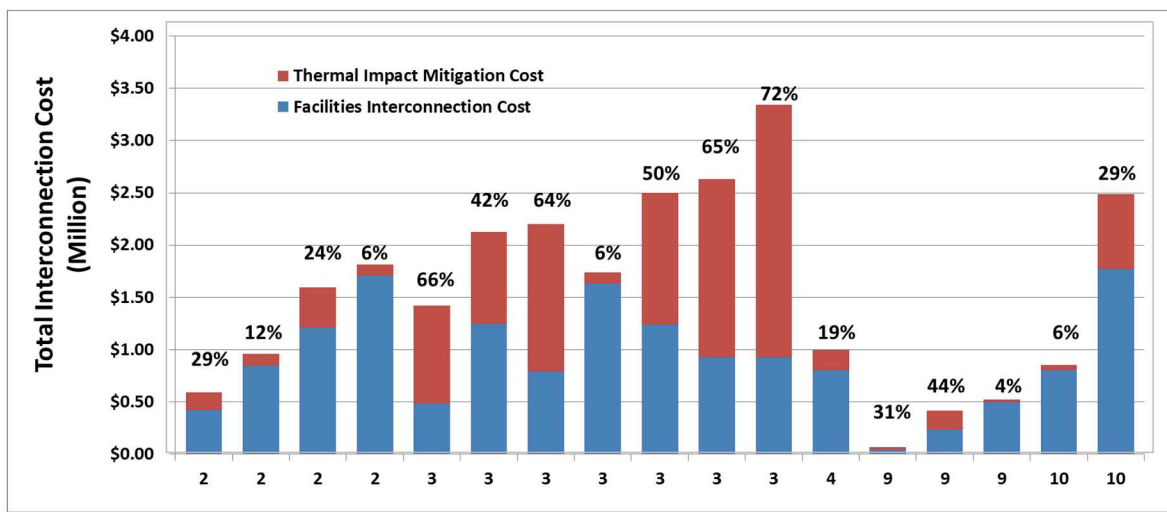


Figure 35. Thermal Mitigation Costs

43 SGIP reports identified protection issues requiring mitigation. Mitigation for protection impacts were binned into two categories substation relay modifications and distribution protection modifications.

Substation relay modifications included adjusting existing relay settings, implementing advanced relay functions such as deadline checking and transfer trip protection and installing protective relaying on the high side bus to protect against faults on the high side of the distribution substation. Distribution protection modifications included modifications to existing reclosers, or the installation of new reclosers on the existing distribution circuit.

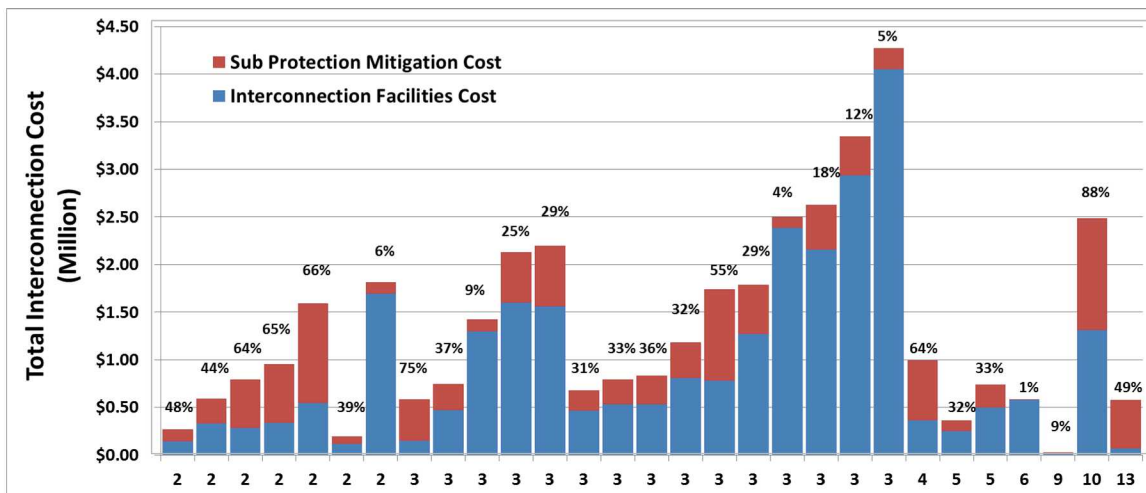


Figure 36. Protection Mitigation Costs for Substation Relay Modifications

Figure 36 highlights mitigation costs for SGIP reports that mitigated protection impacts through the use of substation relay modifications. Mitigations Costs ranged from \$2,000 to \$1.3 million and had mitigation cost ratios of 1% to 88% of the total interconnection cost. The large mitigation cost variation was attributed to the fact that implementing advanced relay functionality did not conform to a standard procedure. Some implementations only required communication lines from the substation to the GF while others required major construction modifications at the substation to install the required equipment.

Figure 37 highlights mitigation costs for 7 SGIP reports that mitigated protection impacts through the use of distribution protection modifications. Two SGIP reports identified the need to install more than one recloser to mitigate the identified protection impacts. Mitigations costs ranged from \$45,000 to 178,900.

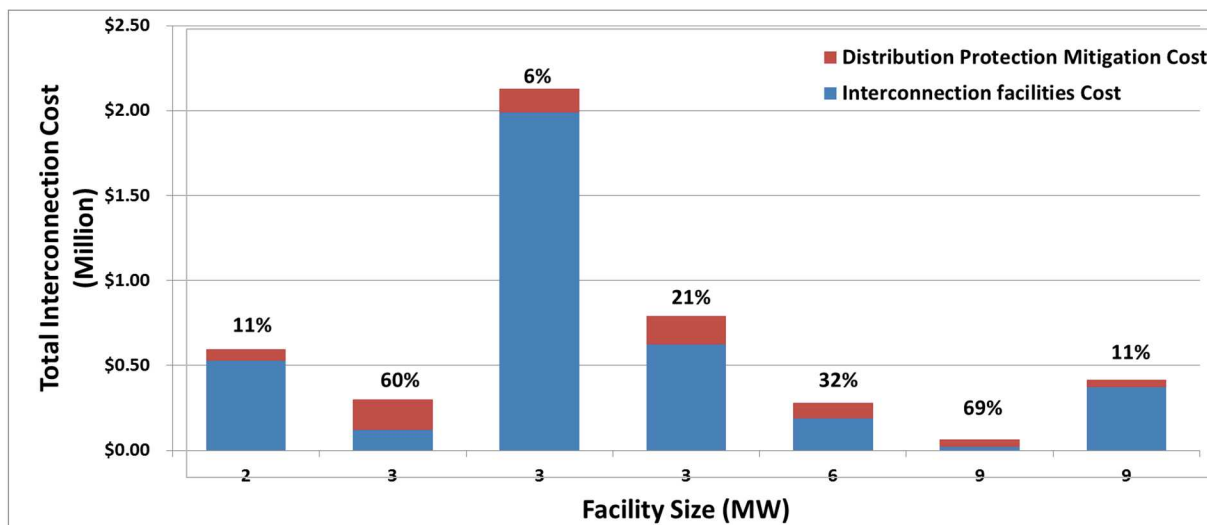


Figure 37 Protection Mitigation Costs for Distribution Protection Modifications

9. CONCLUSIONS

SNL analyzed a total of 100 SGIP interconnection reports performed by three utilities and one regional transmission operator (RTO). The analysis identified three interconnection topologies used to interconnect GF to the local EPS. It was observed that the interconnection topologies were strongly correlated to the presence/absence of adverse impacts. Generally, adverse system impacts were more probable if the GF interconnected through an existing distribution circuit. Adverse system impacts were found in 68% of GFs interconnecting through existing distribution circuits. Adverse system impacts were less probable if the GF required the construction of a new distribution circuit. Adverse system impacts were found in only 1% of GF interconnecting through newly constructed distribution circuits. Building new distribution circuits to interconnect GFs essentially limits the amount of existing equipment outside of the substation exposed to possible adverse system impacts.

Overvoltage impacts were overall the easiest and least expensive to mitigate, with almost half requiring no added cost. Mitigation costs for overvoltage impacts ranged from 0% to 24% of total interconnection costs. Voltage deviation impact mitigations were much more difficult and costly. Mitigation costs for voltage deviation ranged from 19% to 70% of total interconnection costs. Thermal overload impacts were also expensive to mitigate. Mitigation costs for thermal impacts ranged from 4% to 72% of total interconnection costs.

Protection impacts were the most likely adverse system impact identified. The majority of protection impacts were associated with transfer trip requirements to protect against GF islanding. Mitigation cost for protection impacts associated with advanced relay functions ranged from \$74,600 to \$1,300,000. Mitigation costs for protection ranged from 9% to 69% of total interconnection costs. The wide cost variation for advanced relay protection schemes was correlated to the variation in equipment needed to implement the advanced functionality from study to study.

50% of SGIP studies identified total connection costs of less than \$689,431 and 50% of SGIP studies identified total connection costs per MW of less than \$133,833.

As this report showed with a sample set of 100 cases, 44% of the requests that went into the study process identified no negative impacts. SNL is conducting research to identify more efficient screening methods to avoid this high rate of false positives requiring time consuming studies to be performed that identify no adverse impacts.

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APPENDIX A: OVERVIEW OF INTERCONNECTION TERMS

The basic one line diagram of a typical Small Generator Interconnection is shown in Figure 38. The figure gives a general overview of the interconnection circuit and identifies sub circuit locations referred to in this report.

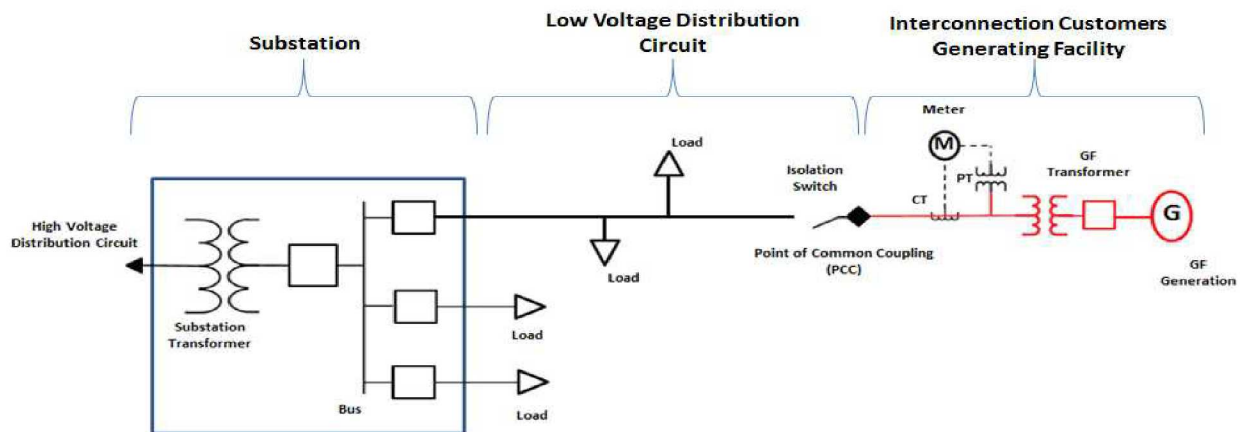


Figure 38 Overview of Interconnection to EPS

Generating Facility (GF)

The GF refers to the interconnection customer's electrical generator (PV), inverters, protective equipment and all equipment owned, maintained and operated by the IC. Generally, this would include all equipment on the customer side of the point of common coupling.

Low Voltage Distribution Circuit

Low voltage distribution circuit refers to the electrical provider's facilities and equipment used to transmit electricity from the substation to customer usage points. This would include utility owned facilities such as: conductors, transformers, protection equipment and power factor correction equipment. Nominal system voltages for facilities in this category ranged from 12.47 kV to 34.5 kV. This term was used to generally refer to three phase feeders and associated laterals between the customer and substation.

Point of Common Coupling (PCC)

The PCC refers to the point where the GF is electrically and physically connected to the local EPS. Generally, this point is demarcated by a meter and/or a disconnect switch owned and operated by the local utility. This term is also synonymous with the term Point of Interconnection.

Substation

Substations generally have switching, protection and control equipment, and transformers that transform voltage from high voltage transmission lines to low voltage distribution lines.

High Voltage Distribution Circuit

This refers to the electrical providers facilities interconnecting through the high side bus of the substation. For the purposes of this report this term was used to reference conductors operating at 69 kV.

APPENDIX B: DATABASE STRUCTURE AND FIELD NAMES

Database Structure

The database consists of four worksheets; each of which is populated with SGIP reports from one of the previously identified EPS providers. Records are tabulated horizontally with each record representing an itemized SGIP report. Switching between the different utility tables is accomplished by selecting the desired utility worksheet tab at the bottom of the table. Within each worksheet are four major field categories: Facility & Feeder Information, Adverse System Impacts & Mitigation, Binned Costs, and Itemized Interconnection Costs. Within each field category are subfields which correspond to information relating to its parent field category. Field categories occupy row 2 and Subfields occupy row 3 of each worksheet.

| Field Categories | Subfield Name | Study ID | Date | DG type | Facility Size | Units | Type of Inverter | Interconnection voltage level | Distance of PCC from Substation (feet) | Feeder name | Substation | Interconnection Type |
|------------------|---------------|---|--------|---------|---------------|-------|------------------|-------------------------------|--|---------------|--------------------|---|
| | | Project Reeves 3,000 KW | Sep-10 | PV | 3.0 | MW | SMA SC 500CP | 12.47kV | 3,775 | Reeves 11 | Reeves | Tap Existing Low Voltage Distribution Circuit |
| | | Project Los Morros 6,000 KW | Oct-10 | PV | 6.0 | MVA | SMA SC 500CP | 12.47kV | 4,155 | Los Morros 21 | Los Morros Unit II | Tap Existing Low Voltage Distribution Circuit |
| | | Project Alamogordo Airport-Site | Mar-11 | PV | 6.0 | MVA | SMA 500HE | 12.47kV | 27,525 | Feeder 12-83 | Alamogordo South | Tap Existing Low Voltage Distribution Circuit |
| | | Project Alamogordo Airport-Site | Mar-13 | PV | 6.0 | MW | SMA 500HE | 12.47kV | 26,815 | Feeder 12-83 | Alamogordo South | Tap Existing Low Voltage Distribution Circuit |

Utility Tab

Figure 39. Worksheet Field Category Identification.

Facility & Feeder Information

The Facilities & Feeder Information field category and its corresponding subfields are shown in Figure 39. The Facilities & Feeder Information field contains 11 subfields, which occupy columns A through K of the worksheet. Information about the GF and the interconnecting EPS are found within the Facilities & Feeder Information fields. This includes facility size, interconnection voltage, point of common coupling (PCC) location, interconnecting substation and interconnection topology.

The Interconnection Topology section provides a full description of the types of interconnection topologies found in the studies. Fields left blank within this category indicated that the SGIP report did not provide that specific information. Under column A of the Facilities & Feeder Information category is the Study ID subfield which identifies the specific study with a hyperlink to the SGIP report. A more detailed description of the specific subfields within the Facilities & Feeder Information field is found in Appendix B.

Adverse System Impacts & Mitigation

The Adverse System Impact & Mitigation field and its corresponding subfields are shown in Figure 40. The Adverse System Impact & Mitigation field contains 10 subfields, which occupy columns L through U of the Excel file. Information about the identified impacts, mitigation and mitigation costs are found within the Adverse Impact & Mitigation Field. The Impacts Identified subfield (Column L) list all adverse system impact identified in the SGIP report. There are six impact classifications: Voltage Deviation, Thermal Overload (Thermal OL), Overvoltage, Contingency, Distribution Fault protection and Substation Protection. A full discussion of each impact classification is found within the Impact Classification Section.

Each impact classification has its own impact mitigation subfield (columns N through U). If an impact is listed in the Impact Identified subfield, its corresponding mitigation and mitigation cost can be found under the specific impact mitigation subfield. If multiple mitigations were required then each new mitigation was separated by a new line and began with a bullet symbol.

For example the SGIP report Highlighted in Figure 40 indicated that an overvoltage and thermal overload were identified (column L). A conductor upgrade was required to mitigate the thermal overload and the estimated cost to perform the mitigation was \$49,328 (column P). The overvoltage impact required the removal of a voltage regulator, the installation of a new capacitor bank and power factor correction at the GFs inverter (column R). The total cost for overvoltage mitigation was estimated at \$50,081.

| | L | M | N | O | P | Q | R | S | T | U |
|----|---|---|------------------------|--------------------------|--|----------------------|---|--------------------|--------------------------------------|-------------------------------|
| 1 | | | | | | | | | | |
| 2 | Adverse System Impact & Mitigation | | | | | | | | | |
| 3 | Impacts Identified? | Flow of electricity from distribution system through Sub transformer | Voltage flicker | Voltage Deviation | Thermal OL | Under Voltage | Over Voltage | Contingency | Distribution Fault Protection | Sub-Station Protection |
| 38 | Over Voltage Thermal OL | At min and maximum load conditions No mitigation | | | • Line upgrade of 1,875ft from 2ACSR to 397AAC | | • Operate at 98% Lagging PF • Vreg Removal/ New Cap Bank | | | |
| 39 | | | | | \$49,328 | | \$50,081 | | | |

Figure 40. Adverse System Impact & Mitigation Identification.

Three Binned Cost Categories

The following section describes costs identified in the SGIP reports, binned into three categories; Interconnection Facilities cost, Mitigation Cost, and Total Connection Cost.

Interconnection Facilities Costs – Costs for facilities necessary to interconnect the GF to the EPS. This very broad cost category included any cost incurred to physically and electrically interconnect the GF to the EPS. Costs associated with mitigating identified impacts were not included in this cost category.

Mitigation Costs – Costs associated with mitigating any adverse system impacts identified in the SGIP reports. Fields left blank in this cost category indicate that no adverse impacts were identified in the SGIP study. Fields listed with zero cost indicate that adverse impacts were found, but no mitigation cost was incurred. Generally, fields with zero mitigation costs represent

SGIP reports that mitigated the impact through the use of advanced inverter functions. Fields with the symbol \$UNK indicate that adverse impacts were identified in the SGIP report, but no clear cost was associated with that specific mitigation.

Total Connection Cost - Cost incurred to interconnect the GF to the EPS. Total Connection Costs represent the aggregate cost of both Mitigation Cost and Interconnection Facilities Costs. Fields with the symbol \$UNK indicate that Total Connection Costs were not defined in the SGIP report.

| | V | W | X | Y | Z | AA | AB | AC | AD | AE | AF | AG |
|----|-----------------------|-----------------------------------|-----------------------------------|---------------------------------------|-------------------------------------|----------------------|----------------|------------|----------|-----------------|----|----|
| 1 | Binned Costs | | | Itemized Interconnection Costs | | | | | | | | |
| 2 | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | |
| 4 | Total Connection Cost | Direct Connection Facilities Cost | | PNM disconnect point | Interconnection | PNM Metering | Communication | | | | | |
| 5 | \$141,900 | \$141,900 | | \$52,800 | \$40,700 | \$19,400 | \$29,000 | | | | | |
| 6 | Total Connection Cost | Mitigation Cost | Direct Connection Facilities Cost | PNM disconnect point (Interruption) | Interconnection (Line Construction) | PNM Primary Metering | Communication | Protection | | | | |
| 7 | \$278,800 | \$90,000 | \$188,800 | \$51,000 | \$68,300 | \$24,500 | \$45,000 | \$90,000 | | | | |
| 8 | Total Connection Cost | Mitigation Cost | Direct Connection Facilities Cost | PNM disconnect point | Interconnection (Line Construction) | PNM Primary Metering | Communications | Protection | Recloser | Line Upgrade | | |
| 9 | \$581,219 | \$5,000 | \$576,219 | \$52,800 | \$176,000 | \$19,400 | \$45,000 | \$5,000 | \$31,300 | \$251,719 | | |
| 10 | Total Connection Cost | Mitigation Cost | Direct Connection Facilities Cost | PNM disconnect Point | Interconnection (Line Construction) | PNM Primary Metering | Communication | | | System Upgrades | | |
| 11 | \$381,502 | \$215,509 | \$165,993 | \$41,853 | \$14,534 | \$64,606 | \$45,000 | | | \$215,509 | | |

Figure 41. Binned Costs and Itemized Interconnection Costs Fields.

Itemized Interconnection Costs

The Itemized Interconnection Cost field contains 14 subfields which occupy columns Y through AI of the worksheet. This section lists itemize costs as identified in the SGIP report. Itemized costs found in this section were derived from the most recent SGIP report performed on the GF. Figure 41 shows an example of the costs section in the database.

Database Field Names

Facility & Feeder Information (Columns A- K)

Study ID (Column A)

This field contains the project name or queued identification number for the SGIP report. In either case the information found in this field can be used to identify the specific study with the utilities online queue, Further more each study ID name is hyperlinked to its corresponding SGIP report

Date (Column B)

This field contains the date (in month/day/year format) that the SGIP report was submitted to the interconnecting customer.

Facility Size (Column D)

This field contains the aggregate nameplate generation capacity of the proposed generation facility under study.

Inverter Model (Column F)

This field contains the make and model of the proposed inverters at the generation facility. Not all studies provided this information in the SGIP report; any blank spaces in this field indicate that inverter information was not provided in the report.

Interconnection Voltage Level (Column G)

This field identifies the nominal operational voltage of the EPS at the proposed PCC. Interconnection voltages found in the database ranged from 12 kV to 69 kV.

PCC Distance from Substation (Column H)

This field identifies the distance (in feet) from the substation to the PCC. Information found in this field indicates that the SGIP report clearly identified a PCC distance from the substation.

Feeder Name (Column I)

This field contains the name of the feeder at which the PCC is located. Blank cells indicate that the feeder name was not identified in the report. Generally, blank cells correspond to interconnections that required the construction of new distribution feeders.

Substation (Column J)

This field identifies the name of the substation at which the PCC is located. Blank cells indicate that the substation was not identified in the report.

Interconnection Type (Column K)

This field identifies the interconnection topology for the proposed generation facility. The four interconnection topologies found in this field are: Tap Existing Low Voltage Distribution Circuit, Build New Distribution Circuit from Substation, Double Feeder Service and Tap Existing High Voltage Distribution Circuit. A full description of each interconnection topology

is found in section 3 of this report. Blank cells in this field indicate that the interconnection topology was not identified in the SGIP report.

Adverse System Impact & Mitigation (Columns L-U)

Impacts Identified (Column L)

This field list all adverse impacts associated with the interconnection of the generation facility. If multiple impacts were identified each new impact begins on a new line within the cell. The list of impact classifications found in this field include: **ContingencyOV**, **ContingencyP**, **ContingencyTOL**, **No Adverse Impact**, **Overvoltage**, **Protection**, **Thermal OL**, and **Voltage Deviation**. If an impact is listed in the Impact Identified subfield its corresponding mitigation and mitigation cost are found under the specific impact category subfield (columns N-U).

If adverse impacts were identified while the EPS was in contingency configuration the Impact Identification subfield contains one or more of the following impact classifications: **ContingencyOV**, **ContingencyP**, **ContingencyTOL**. The classifications represent overvoltage, protection and thermal operational limit impacts respectively. Mitigation for all three contingency classifications is found under the contingency impact category subfield (column S).

The impact classification **No Adverse Impact** indicates that the report did not identify adverse system impacts associated with the interconnection of the generation facility.

Flow of Electricity from Distribution System Through Substation Transformer. (Column M)

This field indicates if the SGIP report identified that the interconnection of the generation facility contributed to possible reverse power flow through the substation transformer. This field gives a brief description of the condition in which reverse power flow is possible. Blank fields indicate the reverse power flow was not identified in the SGIP report.

Voltage Deviation (Column O)

If voltage deviation impacts were identified in the GSIP report the corresponding mitigation and mitigation cost can be found under this subfield. If the impact required more than one mitigation each new mitigation is separated with a new line and begin with a bullet symbol.

The aggregate cost associated with mitigation can be found at the bottom of the subfield (in red). If the symbol **\$UNK** is found at the bottom of the subfield, this indicates that a mitigation cost was not identified in the SGIP report. In some reports mitigation cost for voltage deviation impacts were binned with mitigation costs for other impacts. I that case, a reference to where the binned cost can be found in the **Itemized Interconnection** field can be found at the bottom of the subfield.

For example the image highlighted below indicates that the SGIP report identified a thermal OL and overvoltage impact. The report provided a binned cost for both mitigations which can be found under the **System Upgrades** subfield in the **Itemized Interconnection Costs** field.

| Impacts Identified? | Flow of electricity from distribution system through Sub transformer | Voltage flicker | Voltage Deviation | Thermal OL | Under Voltage | Over Voltage |
|----------------------------|--|-----------------|-------------------|---|---------------|--|
| Thermal OL Over Voltage | At min load conditions No mitigation | | | • Line Upgrade of 7233ft from 110ACSR with 337AAC \$In System Upgrades | | • Operate at 99% lag PF • Install 1200kVAR temp controlled Cap Bank \$In System Upgrades |

Thermal OL (Column P)

If a thermal overload impact was identified in the SGIP report the corresponding mitigation and mitigation cost can be found under this subfield. If multiple mitigations were identified for the impact each new impact is separated with a new line and began with a bullet symbol. Refer to the **Voltage Deviation** subfield section for SGIP reports that did not identify mitigation costs or for reports that binned multiple mitigation cost.

Overvoltage (Column R)

If an overvoltage impact was identified in the SGIP report the corresponding mitigation and mitigation cost can be found under this subfield. If the impact required more than one mitigation, each new mitigation is separated with a new line and begins with a bullet symbol. Refer to the **Voltage Deviation** subfield section for SGIP reports that did not identify mitigation costs or for reports that binned multiple mitigation cost.

Contingency (Column S)

If an adverse system impact occurred while the EPS was in contingency operation the impact classification, mitigation and mitigation cost can be found in this subfield. Each new impact classification begins with a bullet symbol and a description of the mitigation we precede just below it. The aggregate cost associated with mitigation can be found at the bottom of the subfield (in red). If the symbol **\$UNK** is found at the bottom of the subfield, this indicates that a mitigation cost was not identified in the SGIP report. Impacts occurring while in contingency are identified in the Impacts Identified subfield with one of the following classifications: **ContingencyOV**, **ContingencyP**, **ContingencyTOL**.

Distribution Fault Protection (Column T)

If the SGIP report identified protection impacts and mitigation for the impact was accomplished through the use of reclosers on the distribution circuit a description of the mitigation and mitigation cost can be found in this subfield. If more than one recloser modification was required the number of reclosers was bound by brackets in the mitigation description. The aggregate cost associated with mitigation can be found at the bottom of the subfield (in red).

Substation Protection (Column U)

If the SGIP report identified protection impacts and mitigation for the impact was accomplished through the use of equipment modifications at the substation a description of the mitigation and mitigation cost can be found in this subfield. Example of equipment include: new relays, relay modifications or advanced relay functions.

Binned Costs (Columns V-X)

Total Connection Costs (Column V)

The total cost associated with interconnection the generation facility to the EPS is found within this subfield. The cost reflected in this subfield is the aggregate cost of quantities found in the **Mitigation Cost** and **Interconnection Facilities Cost** subfields. If the SGIP report did not identify cost associated with the interconnection of the generation facility, the symbol **\$UNK** was placed in this subfield.

Mitigation Cost (Column W)

The total cost associated with mitigating all adverse system impacts is found within this subfield. If the SGIP report did not provide costs for mitigating the adverse impact , the symbol **\$UNK** was placed in this subfield.

Interconnection Facilities Costs (Column X)

This is a very broad cost category and would include any cost incurred to physically and electrically interconnect the GF to the EPS.

Itemized Interconnection Costs (Columns Y-AL)

The Itemized Interconnection Costs field list cost as identified in the SGIP report.

APPENDIX C: DEFINITIONS

Adverse System Impacts – A negative effect, due to the interconnection of the generating facility, which compromises the performance, reliability or safety of the existing Electrical Power System (EPS).

Contingency –An event (planned or unplanned) that creates an outage of an electrical power system component such as a transmission or distribution line, generator, transformer or conductor.

Deadline Checking –A protection scheme that blocks the automatic reclosing of protection equipment (relays, reclosers) until the lines are de-energized. This scheme ensures that faults have adequate time to clear and protection against damaging equipment.

Electric Power System (EPS) – The connected system or power apparatus used to deliver electric power from the source to the utilization device.

EPS Provider – Refers to the governing entity that performed or commission the SGIP report. This is a general term and is used to reference one or all of the data sources (APS, PNM, PacifiCorp, PJM) used to compile the database

Generating Facility (GF) - All equipment owned, maintained and operated by the Interconnection Customer including electrical generators, inverters, protective equipment, etc.

High Voltage Distribution Circuit – refers to the infrastructure interconnecting to the high side bus of the distribution substation. Nominal system voltages in this category were at the 69 kV and below. This circuit class defines a specific interconnection topology.

Interconnection Customer (IC) – An entity interconnected or proposing to interconnect its Generating Facility for parallel operation with the local EPS.

Interconnection Facilities Cost – are the facilities necessary to make a direct electrical connection from the GF to the EPS. This does not include equipment required to mitigate adverse system impacts.

Interconnection Voltage – The nominal system voltage of the EPS at which the PCC is located. Interconnection voltages identified in this reports range from 12.47 kV to 69 kV.

Low Voltage Distribution Circuit – refers to the infrastructure interconnecting the customer to the substation low side bus. Typically nominal system voltages range from 12.47 kV to 34.5 kV. Generally distribution circuits are typically owned and maintained by the local utility. Distribution Circuit equipment typically includes: feeder breakers, conductors, poles, switches, transformers, voltage regulators, capacitors and protection equipment.

Mitigation – Identifies costs associated with mitigating the adverse system impacts resulting from interconnecting the GF.

Point of Common Coupling (PCC) - The point where the Generating Facility is electrically connected to the EPS. The point of Common Coupling is synonymous with the Point of interconnection.

Total Connection Cost per MW – Represents the Total Connection Cost per nameplate capacity (MW) of the GF.

Transfer trip – An anti-islanding protection scheme used to ensure that the GF is isolated from the EPS in case of feeder is shutdown.

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