

Novel Experimental Techniques to Investigate Wellbore Damage Mechanisms

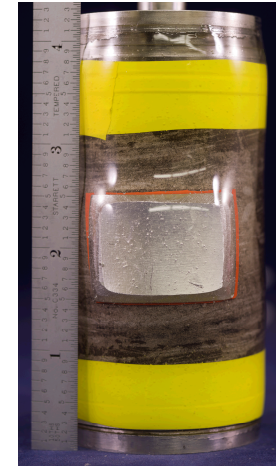
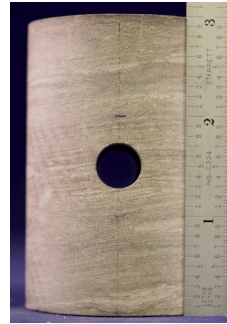
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In Situ Stress States

- In situ stress state vital for subsurface engineering projects, hazard predictions
- Few measurement techniques
 - Flatjacks, overcoring, anelastic strain recover, borehole methods
- Borehole methods
 - Integrate density logs for vertical stress
 - Leak off tests for minimum horizontal stress
 - Maximum horizontal stress must be calculated from borehole breakouts
- Borehole breakouts
 - Diametrically opposed shear/compressive/buckling fractures resulting from stress concentration at borehole
 - Measure width using imaging logs, calculate maximum horizontal stress assuming failure envelope, rock properties
- DOE Jason 2014 Report – errors in stress measurement can be as high as 30-40% in complicated terranes

Laboratory Wellbore Simulations

- True Triaxial Systems
 - Recreate in situ stress state
 - Expensive, niche equipment
- Hollow cylinders
 - Common equipment
 - No differential stress
- Sandia Wellbore Simulation (SWESI)
 - Utilizes standard equipment
 - Recreates in situ stress state
 - Kirsch's hole in a plate



SWESI Geometry

- 50 mm diameter sample, 75 mm long
 - 11.3 mm hole perpendicular to axis
- Borehole cover
 - Solid
 - Tapped for pore fluid
- Silicone rubber pad
- UV cure polyurethane

Mancos Shale

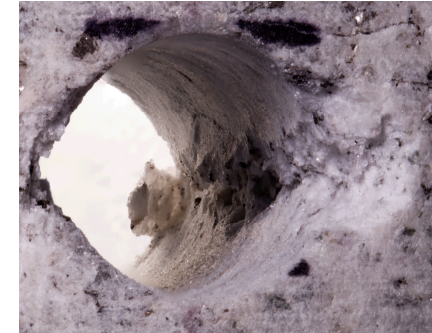
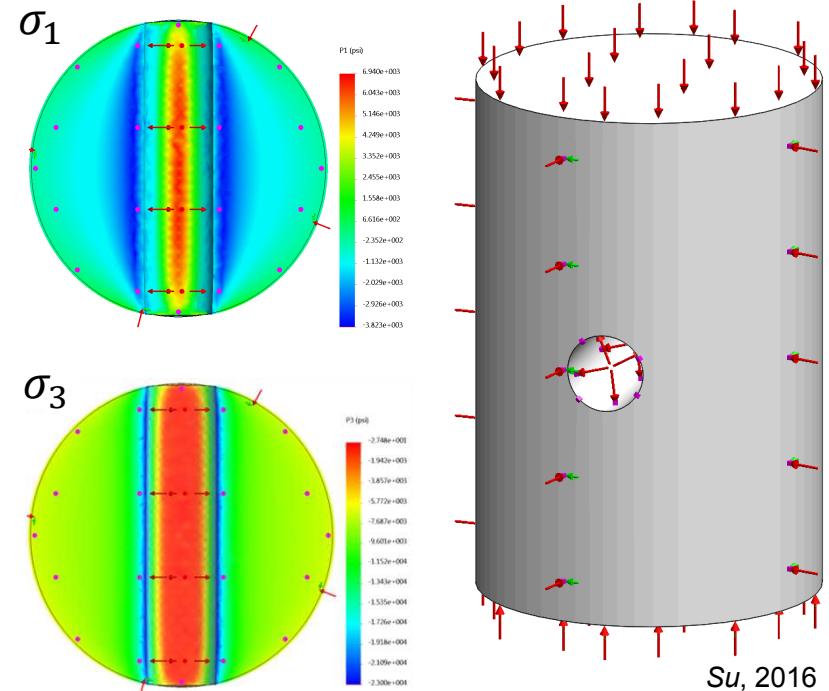
- Finely laminated Cretaceous mudrock
- Cores prepared 3 orientations
 - Parallel, perpendicular, 45 degrees
- 3 different confining pressures
 - 6.89, 13.79, and 20.68 MPa
- $1.6 \times 10^{-5} \text{ sec}^{-1}$ strain rate

Sierra White Granite

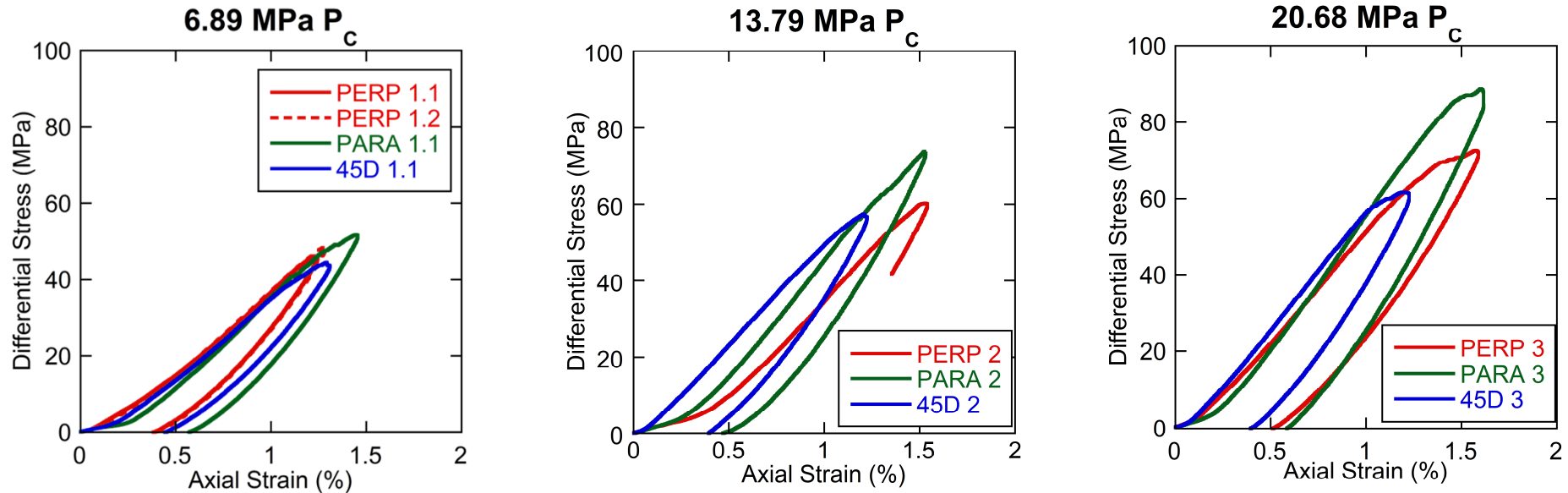
- Granodiorite, 1-3 mm grain size
- 3 different borehole chemistries
 - Dry, DI water, Na/Ca Bicarbonate (pH 9)
- 3 different effective confining pressures
 - 8.6, 17.2, and 34.4 MPa
- $3 \times 10^{-6} \text{ sec}^{-1}$ strain rate

SWESI Validation

- 3d Elastic modelling
 - Simulate 89 kN axial force, 6.89 MPa confining pressure
 - Stresses distributed evenly along wellbore
- Deformation results in breakouts
 - Shear fracture bounded breakout
 - Distributed evenly along wellbore



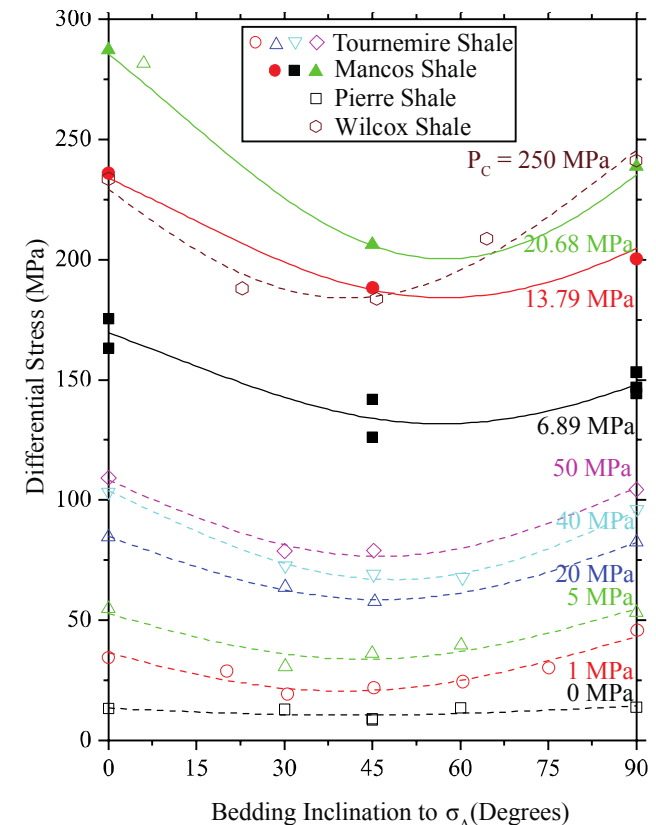
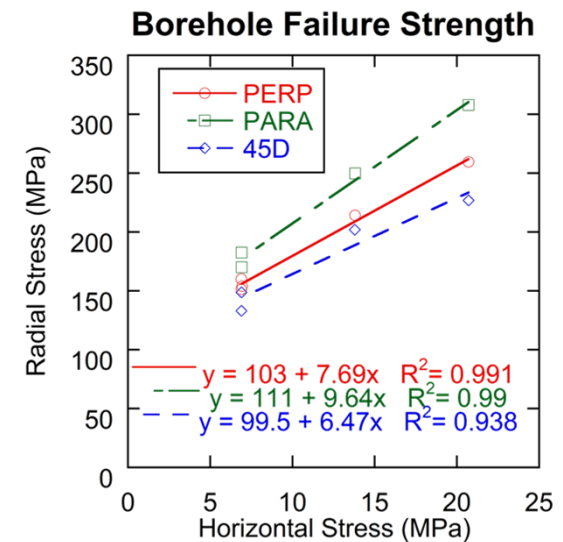
Bedding Effects on Borehole Breakout



- Bedding orientation affects failure strength
 - Parallel stronger than perpendicular, stronger than 45 degrees
- Failure strength increases with increasing confining pressure
- Bedding orientation affects sample stiffness
 - Parallel stronger than perpendicular, stronger than 45 degrees

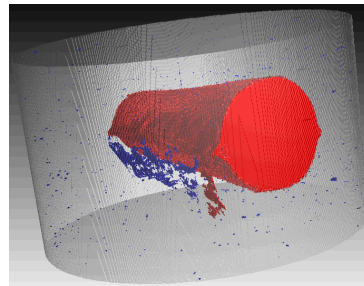
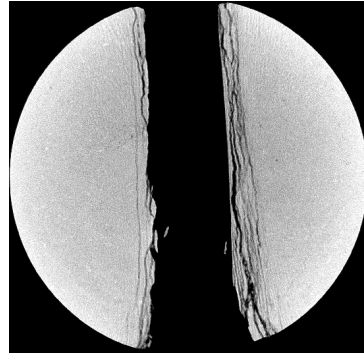
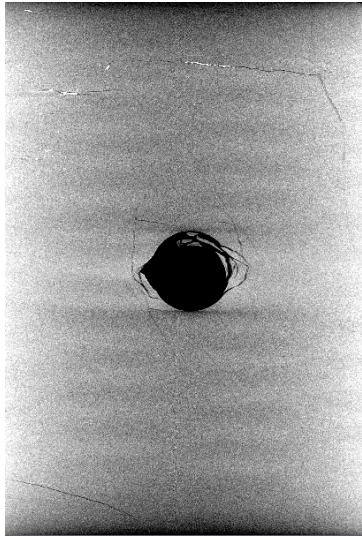
Bedding Effects on Failure Strength

- Borehole strength from Kirsch's solution
 - $\sigma_{Borehole} = 3 * \sigma_{Axial} - P_C$
- Borehole strength increases with increasing P_C
 - Parallel > Perpendicular > 45 Degrees
- Borehole strength fit with *Donath, 1972* failure envelope
 - $\sigma_D = A - B \cos 2(C - \theta)$
 - A, B, C constants
 - θ inclination of bedding to axial stress
- Borehole strength higher than failure strength
- Minimum angle higher for borehole
- Larger stress variation for P_C
 - Increases with increasing P_C

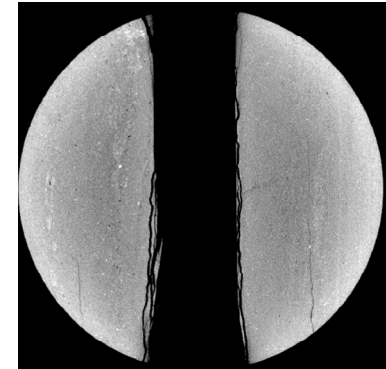
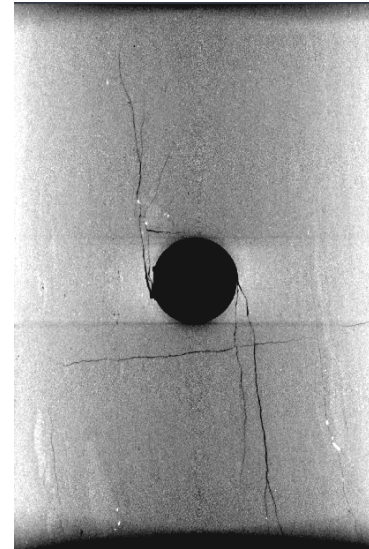


Breakout Geometry

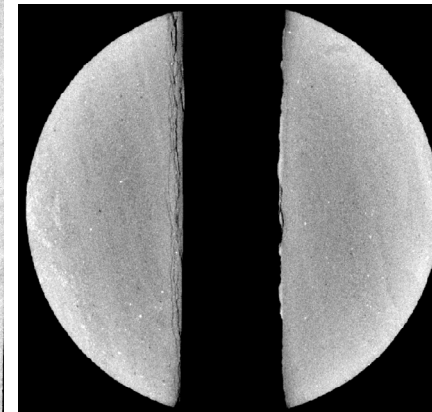
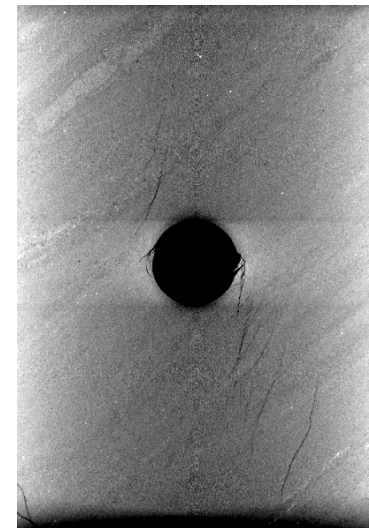
Perpendicular



Parallel

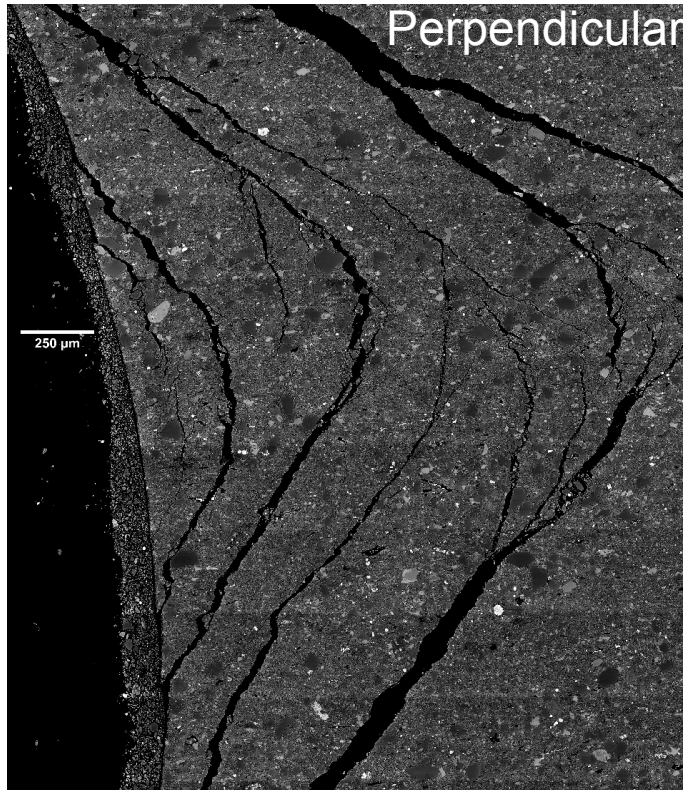


45 Degrees



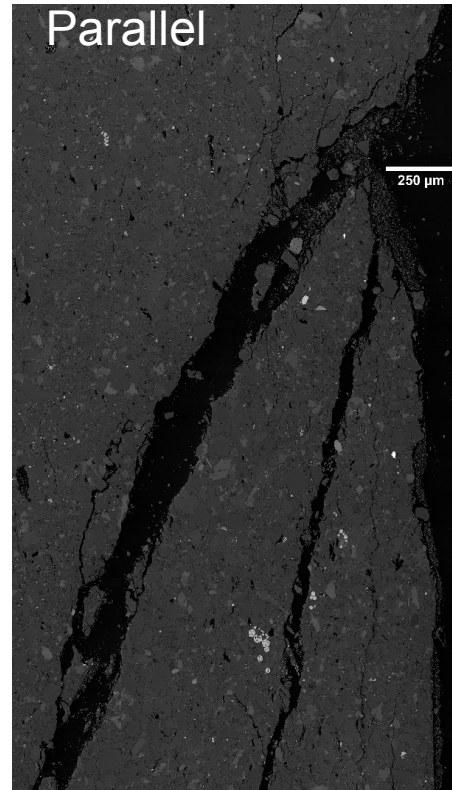
- Perpendicular - dog eared shape; breakouts grow larger
- Parallel - Vertical fractures; no breakout; forms at bottom
- 45 Degrees - Dog ear shape; En echelon fractures

Breakout Microstructures



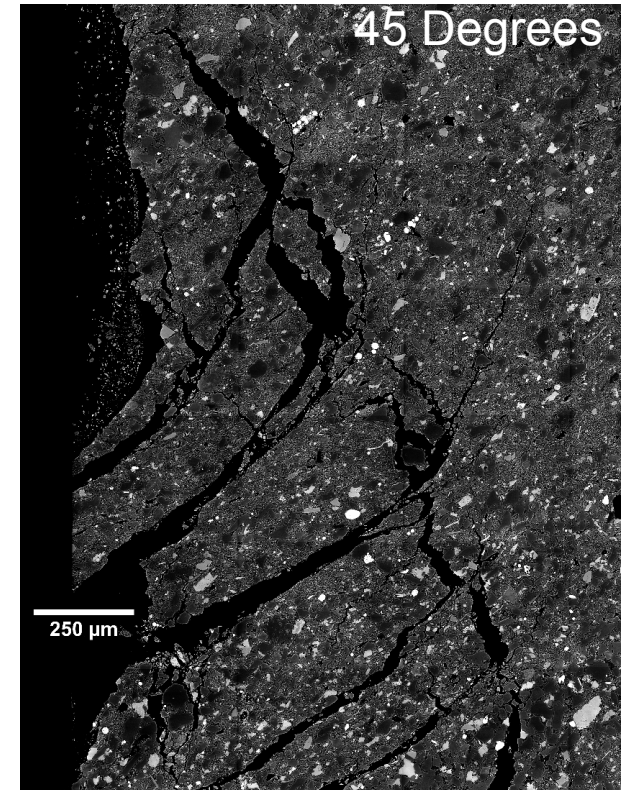
Perpendicular

- Rounded nose
- Branching, horsetail tips



Parallel

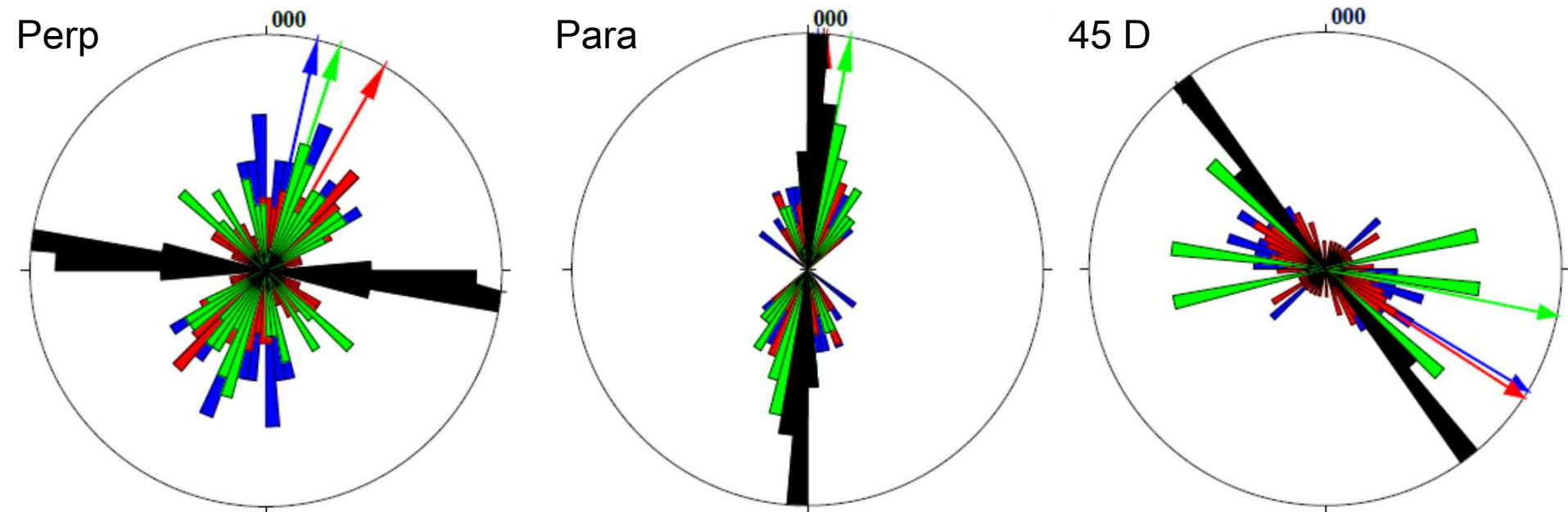
- Long vertical fractures
- Fractures don't intersect



45 Degrees

- En echelon progression
- Fracture along bedding

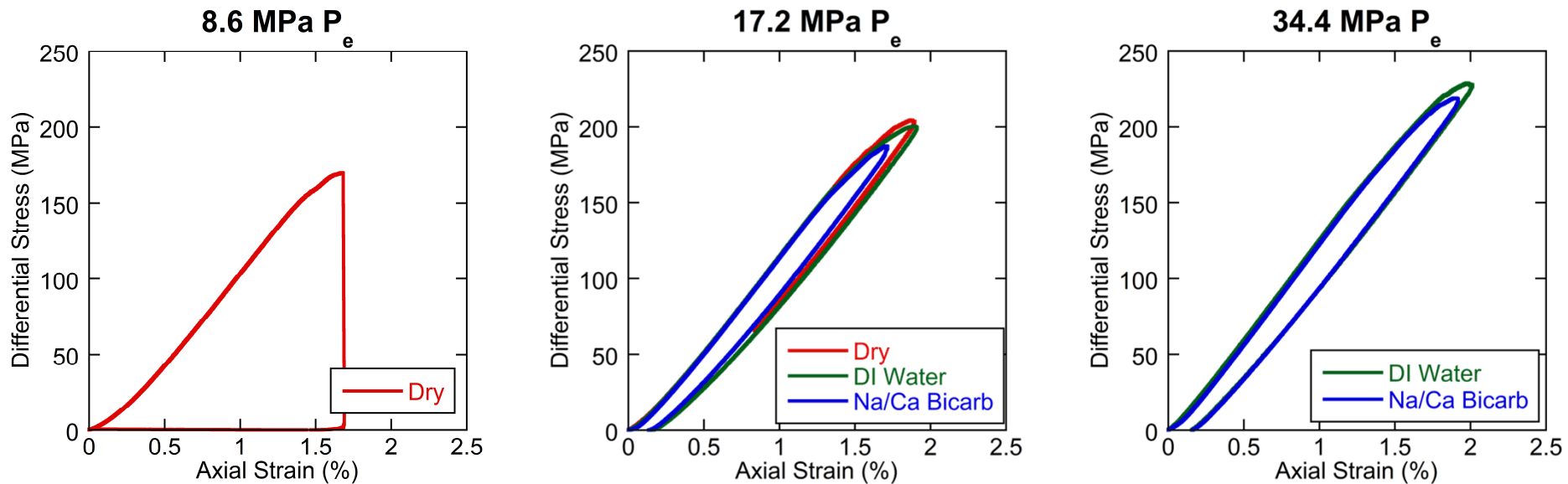
Bedding Effects on Fracture Orientation



Bedding
Light
Dark
Mixed

- Fracture measured from thin section using Image J
 - Layering based on grey value
- Perpendicular – Steeper dip in clastic layers than clay rich layers
- Parallel – Highest dips, follows bedding dip
- 45 Degrees – shallowest dips, subparallel to bedding

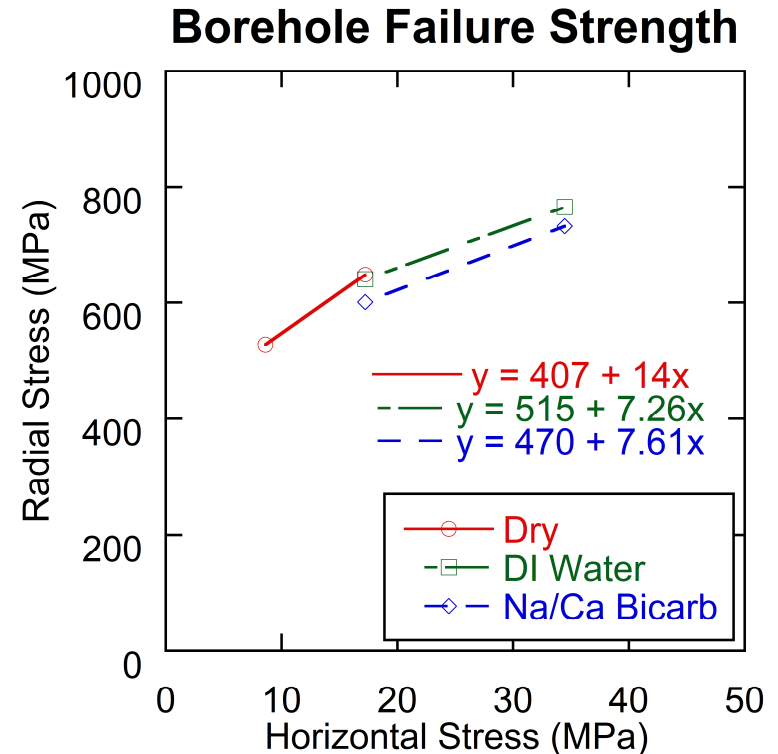
Fluid effects on Borehole Breakout



- Failure strength increases with increasing effective pressure
- Low P_e failure by through going fracture, little breakout
 - Higher pressure tests fail by slight stress drop
- Fluid alters failure strength
 - Na/Ca bicarbonate weaker
- Fluid does not affect stiffness

Fluid effects on Borehole Breakout

- Borehole strength from Kirsch's solution
 - $\sigma_{Borehole} = 3\sigma_{Axial} - P_C$
- Borehole strength increases with increasing P_C
 - Big increase from 8.6 MPa to 17.2 MPa P_C
- Parallel slopes for different fluids
 - Na/Ca bicarbonate shifted to lower strength
 - Room temperature
- Future work
 - Different fluids (acid, mineral oil)
 - Different load paths



Conclusion

- SWESI sample geometry capable of recreating borehole deformation mechanisms
 - Resulting failure consistent with borehole breakout geometries
- Flexibility of geometry and triaxial loading frames allow for wide range of testing conditions
 - Different bedding orientations, fluid chemistries, confining pressures, strain rates
- Bedding orientation has strong influence on borehole breakout
 - Clear variation in failure strength, breakout geometry, fracture orientation
- Fluid chemistry influence failure strength
 - No change for DI water, weakening for basic solutions