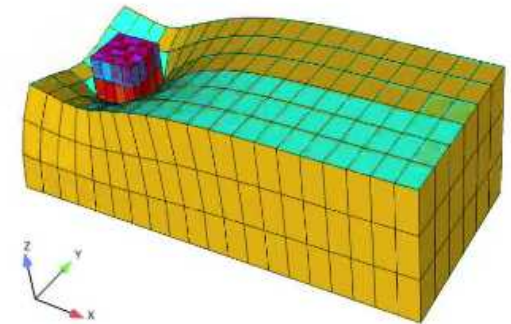
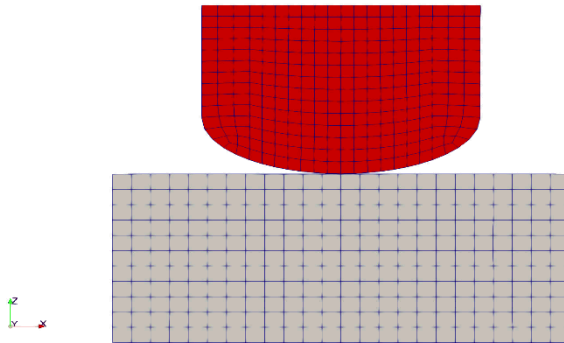


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-----  
-----



# SIERRA/SM Implicit Contact: Troubleshooting

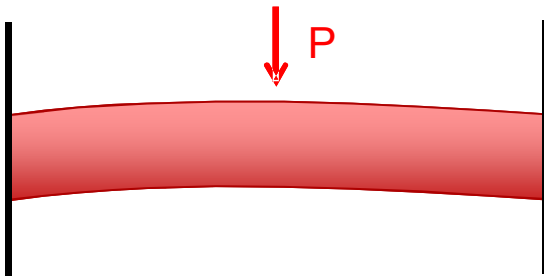
November 2017

SIERRA/SolidMechanics Team

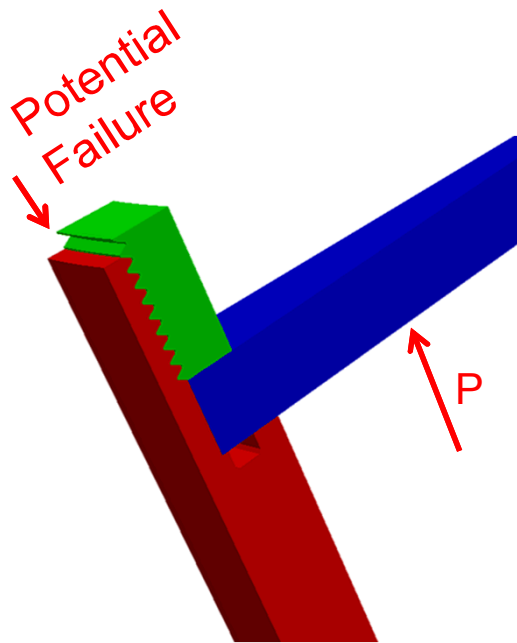
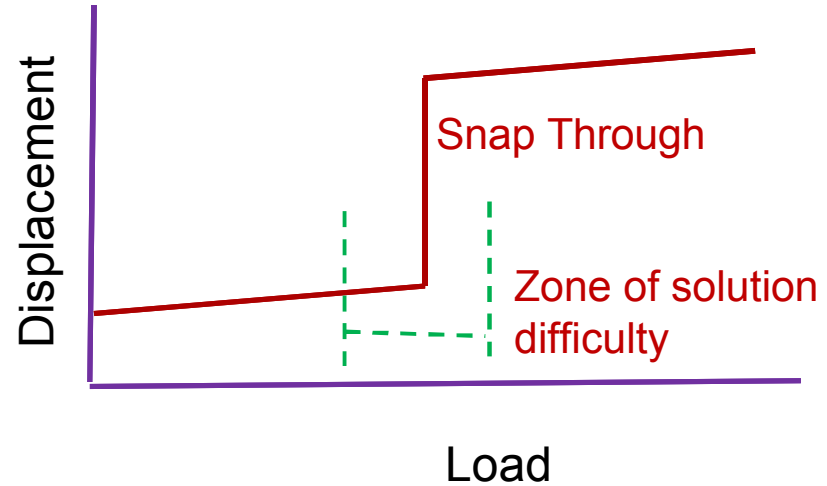
# Outline

- Revisit common pitfalls for implicit quasi-statics
- Revisit recommended solver settings for contact problems
- Revisit logfile and expand upon logfile-based debugging
  - Linear Solver
  - Control Contact
- Other debugging tools
  - Visualization
  - Iteration plotting
  - Problem simplification/isolation
  - *Etc.*
- Debugging example problems
  - Resistance forge weld
  - Pressurized can with threaded lid
  - Stiff square indenting into soft material
- Summary

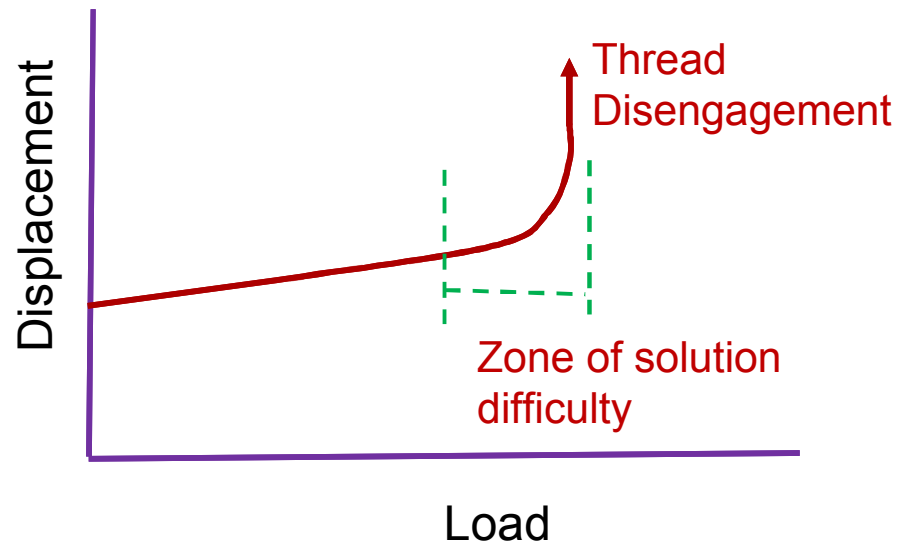
# Common Pitfalls for Implicit Quasi-statics



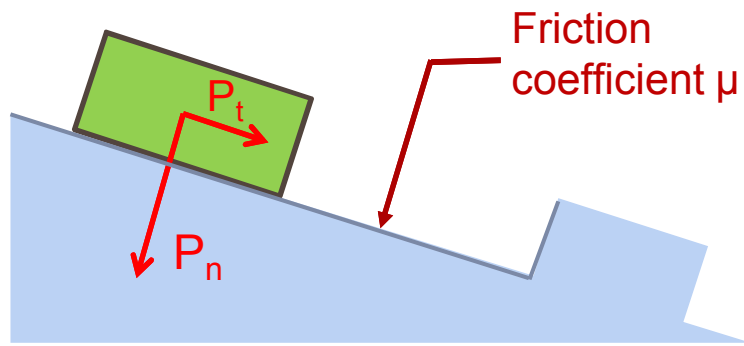
Buckling



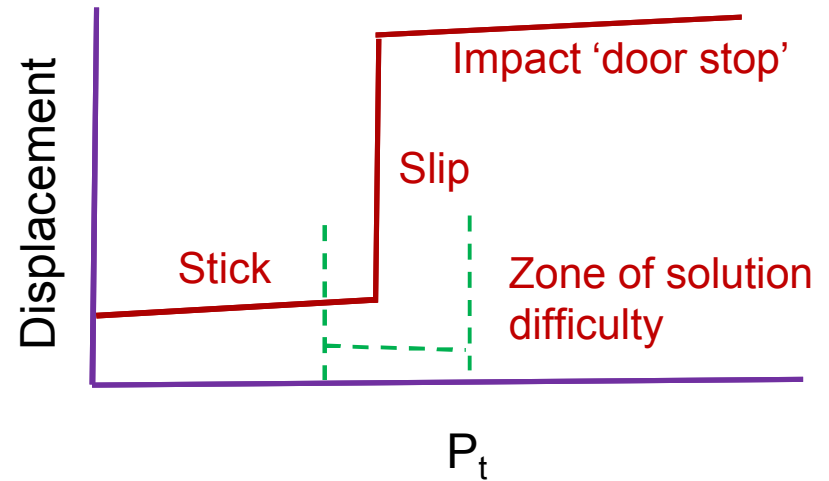
Nearby Failure Conditions



# Common Pitfalls for Implicit Quasi-statics



Stick/Slip



- Rate-dependent material models
- Multiple constraints on nodes (e.g. where contact intersects kinematic BC's)
- Sharp material non-linearity and/or incompressible materials
- P-delta effects
- Poorly-shaped elements in input mesh
- Initial overlap in input mesh (use "Overlap Removal"; inspect mesh after)
- Thermal-Mechanical coupling

# Recommended Robust Contact Solver Settings

```
begin solver
  begin loadstep predictor
    scale factor = 0.0 0.0
  end
end
```

Turns off loadstep  
predictor (can cause  
more harm than good)

```
begin control contact
  target relative residual = 1.0e-4
end
```

Usable range: 1.0e-2 to 1.0e-8

↑  
~10X spread recommended

```
begin cg
  target relative residual = 1.0e-5
  acceptable relative residual = 1.0
  maximum iterations = 100
  begin full tangent preconditioner
    tangent diagonal scale = 1.0e-6
  end
end
end
```

Allows constraints  
to change between  
captured and  
released

Provides limited resilience  
to rigid body modes

# Log File Debugging

## The log file should be a primary source for debugging

- Look for all error and/or warning messages
- If using adaptive time stepping, look for cutbacks
  - This is often where the trouble started: inverted or poorly-shaped elements, contact lost, loss of static equilibrium, *etc.*
- Look for acceptable tolerances (“<A”) achieved instead of target tolerances (“<T”)
  - Why?
  - Can it be avoided?

# Log File Debugging: Linear Solve

```
=====
Begin load step =      0 Solution period Apst_Procedure_p1 is      0.0% complete
      Old Time      Time Step      New Time      Stop Time      CPU Time(s)      Wall Time(s)
      0.0000e+00      1.0000e+00      1.0000e+00      1.0000e+00      8.1388e-01      2.0306e-02
=====
```

LINEAR		MP	RESIDUAL	RELATIVE RESIDUAL	EXTERNAL REFERENCE	ENERGY DISPLACEMENT	
RBM	ITER	ITER					
-	-	0	1.534e+11	9.714e-01	1.579e+11	-	-
0	U	1	5.045e+10	6.957e-01	7.252e+10	5.301e+08	7.486e+00
0	1	2	2.802e+10	4.079e-01	6.870e+10	1.865e+08	5.993e-01
0	1	3	8.507e+09	1.272e-01	6.690e+10	1.025e+06	1.696e-01
0	1	4	1.399e+09	2.112e-02	6.621e+10	3.374e+03	1.777e-03
0	1	5	6.609e+08	9.969e-03	6.630e+10	6.803e+03	1.677e-04
0	1	6	2.010e+08	3.031e-03	6.632e+10	8.050e+01	4.362e-05
0	1	7	7.116e+07	1.073e-03	6.631e+10	4.210e-01	9.116e-06
0	1	8	3.546e+07	5.348e-04	6.630e+10	4.855e-02	1.109e-06
0	1	9	1.414e+07	2.133e-04	6.631e+10	1.567e-02	2.213e-07
0	1	10	4.935e+06	7.443e-05<T	6.631e+10	1.533e-03	2.833e-08

Rigid body  
modes

Tangent re-  
calculation  
("U"pdate)

2-norm of  
nodal force  
imbalance

Residual normalized  
by reference quantity

convergence  
status

Reference  
quantity (external  
force, energy, etc.)

Alternative  
Convergence  
Criteria

# Log File Debugging: Linear Solve

=====								
Begin load step =	0		Solution period		Apst_Procedure_p1 is		0.0% complete	
Old Time	Time Step		New Time		Stop Time		CPU Time(s)	
0.0000e+00	1.0000e+00		1.0000e+00		1.0000e+00		8.1388e-01	
							Wall Time(s)	
							2.0306e-02	
-----								
	LINEAR		MP		RELATIVE	EXTERNAL		
	RBM	ITER	ITER	RESIDUAL	RESIDUAL	REFERENCE	ENERGY	DISPLACEMENT
-----								
		-	0	1.534e+11	9.714e-01	1.579e+11	-	-
0	U	1	1	5.045e+10	6.957e-01	7.252e+10	5.301e+08	7.486e+00
0		1	2	2.802e+10	4.079e-01	6.870e+10	1.865e+08	5.993e-01
0		1	3	8.507e+09	1.272e-01	6.690e+10	1.025e+06	1.696e-01
0		1	4	1.399e+09	2.112e-02	6.621e+10	3.374e+03	1.777e-03
0		1	5	6.609e+08	9.969e-03	6.630e+10	6.803e+03	1.677e-04
0		1	6	2.010e+08	3.031e-03	6.632e+10	8.050e+01	4.362e-05
0		1	7	7.116e+07	1.073e-03	6.631e+10	4.210e-01	9.116e-06
0		1	8	3.546e+07	5.348e-04	6.630e+10	4.855e-02	1.109e-06
0		1	9	1.414e+07	2.133e-04	6.631e+10	1.567e-02	2.213e-07
0		1	10	4.935e+06	7.443e-05<T	6.631e+10	1.533e-03	2.833e-08

## Rigid Body Modes (RBM's):

- If =0: no rigid body modes detected by solver
- If >0:
  - Add BC's to constrain free DOF's in one or more element blocks
  - Use ITERATION PLOT to find any missed RBM's
  - If loss of contact, element death, *etc.* cause static problem to become dynamic: try using explicit dynamics, implicit dynamics, or control damped solve



# Log File Debugging: Linear Solve

```
=====
Begin load step =      0 Solution period Apst_Procedure_p1 is      0.0% complete
      Old Time      Time Step      New Time      Stop Time      CPU Time(s)      Wall Time(s)
      0.0000e+00      1.0000e+00      1.0000e+00      1.0000e+00      8.1388e-01      2.0306e-02
=====
```

	LINEAR		MP		RELATIVE	EXTERNAL		
	RBM	ITER	ITER	RESIDUAL	RESIDUAL	REFERENCE	ENERGY	DISPLACEMENT
-	-	0	1.534e+11	9.714e-01	1.579e+11	-	-	
0	U	1	5.045e+10	6.957e-01	7.252e+10	5.301e+08	7.486e+00	
0	1	2	2.802e+10	4.079e-01	6.870e+10	1.865e+08	5.993e-01	
0	1	3	8.507e+09	1.272e-01	6.690e+10	1.025e+06	1.696e-01	
0	1	4	1.399e+09	2.112e-02	6.621e+10	3.374e+03	1.777e-03	
0	1	5	6.609e+08	9.969e-03	6.630e+10	6.803e+03	1.677e-04	
0	1	6	2.010e+08	3.031e-03	6.632e+10	8.050e+01	4.362e-05	
0	1	7	7.116e+07	1.073e-03	6.631e+10	4.210e-01	9.116e-06	
0	1	8	3.546e+07	5.348e-04	6.630e+10	4.855e-02	1.109e-06	
0	1	9	1.414e+07	2.133e-04	6.631e+10	1.567e-02	2.213e-07	
0	1	10	4.935e+06	7.443e-05<T	6.631e+10	1.533e-03	2.833e-08	

## Tangent Update:

- Benefits: much better convergence rate when problem is non-linear
- Drawbacks: computationally expensive
- When to try more frequent updates: no RBM's but residual is stagnating
- Indicator that it is beneficial: residual drops significantly at each update
- Tips:
  - Try changing ITERATION UPDATE: controls tangent update frequency
  - Try changing SMALL NUMBER OF ITERATIONS: avoids updates at start of load step when previous load step converged quickly

# Log File Debugging: Linear Solve

=====									
Begin load step =	0		Solution period		Apst_Procedure_p1 is		0.0% complete		
Old Time	Time Step		New Time		Stop Time		CPU Time(s)		Wall Time(s)
0.0000e+00	1.0000e+00		1.0000e+00		1.0000e+00		8.1388e-01		2.0306e-02
-----									
	LINEAR		MP			RELATIVE	EXTERNAL		
	RBM	ITER	ITER		RESIDUAL	RESIDUAL	REFERENCE	ENERGY	DISPLACEMENT
-----									
	-	-	0		1.534e+11	9.714e-01	1.579e+11	-	-
	0	U 1	1		5.045e+10	6.957e-01	7.252e+10	5.301e+08	7.486e+00
	0	1	2		2.802e+10	4.079e-01	6.870e+10	1.865e+08	5.993e-01
	0	1	3		8.507e+09	1.272e-01	6.690e+10	1.025e+06	1.696e-01
	0	1	4		1.399e+09	2.112e-02	6.621e+10	3.374e+03	1.777e-03
	0	1	5		6.609e+08	9.969e-03	6.630e+10	6.803e+03	1.677e-04
	0	1	6		2.010e+08	3.031e-03	6.632e+10	8.050e+01	4.362e-05
	0	1	7		7.116e+07	1.073e-03	6.631e+10	4.210e-01	9.116e-06
	0	1	8		3.546e+07	5.348e-04	6.630e+10	4.855e-02	1.109e-06
	0	1	9		1.414e+07	2.133e-04	6.631e+10	1.567e-02	2.213e-07
	0	1	10		4.935e+06	7.443e-05<T	6.631e+10	1.533e-03	2.833e-08

## Solution Iterations:

- When to increase max iterations: residual still dropping at max
- When to decrease max iterations: residual bottoming out before max
- When to use min iterations >0: residual <T but still substantially decreasing  
(in this case, increasing min iterations can improve convergence of subsequent steps)

# Log File Debugging: Linear Solve

```
=====
Begin load step =      0 Solution period Apst_Procedure_p1 is      0.0% complete
      Old Time      Time Step      New Time      Stop Time      CPU Time(s)      Wall Time(s)
      0.0000e+00      1.0000e+00      1.0000e+00      1.0000e+00      8.1388e-01      2.0306e-02
=====
```

LINEAR		MP		RELATIVE	EXTERNAL		
RBM	ITER	ITER	RESIDUAL	RESIDUAL	REFERENCE	ENERGY	DISPLACEMENT
-	-	0	1.534e+11	9.714e-01	1.579e+11	-	-
0	U 1	1	5.045e+10	6.957e-01	7.252e+10	5.301e+08	7.486e+00
0	1	2	2.802e+10	4.079e-01	6.870e+10	1.865e+08	5.993e-01
0	1	3	8.507e+09	1.272e-01	6.690e+10	1.025e+06	1.696e-01
0	1	4	1.399e+09	2.112e-02	6.621e+10	3.374e+03	1.777e-03
0	1	5	6.609e+08	9.969e-03	6.630e+10	6.803e+03	1.677e-04
0	1	6	2.010e+08	3.031e-03	6.632e+10	8.050e+01	4.362e-05
0	1	7	7.116e+07	1.073e-03	6.631e+10	4.210e-01	9.116e-06
0	1	8	3.546e+07	5.348e-04	6.630e+10	4.855e-02	1.109e-06
0	1	9	1.414e+07	2.133e-04	6.631e+10	1.567e-02	2.213e-07
0	1	10	4.935e+06	7.443e-05	6.631e+10	1.533e-03	2.833e-08

## Convergence Status:

- When to tighten target: residual still dropping; or, later step fails to converge
- When to loosen target: current target is small and never achieved
- When to tighten acceptable: CG is outer loop of single-/multi-level solve and observably bad solution(s) accepted; later step fails
- When to loosen acceptable: CG is inner loop of multi-level solve (e.g. to avoid erroring-out when control contact has a bad model problem)

# Log File Debugging: Linear Solve

RBM	LINEAR ITER	MP ITER	RESIDUAL	RELATIVE RESIDUAL	EXTERNAL REFERENCE	ENERGY	DISPLACEMENT
0	1	1	2.616e-06	2.677e-02	9.772e-05	4.940e-24	7.156e-34
0	1	2	2.616e-06	2.677e-02	9.772e-05	4.940e-24	7.156e-34
0	1	3	2.616e-06	2.677e-02	9.772e-05	4.940e-24	7.156e-34
0	1	4	2.616e-06	2.677e-02	9.772e-05	4.940e-24	7.156e-34
0	1	5	2.616e-06	2.677e-02	9.772e-05	4.940e-24	7.156e-34

## Residual / Relative Residual:

- If stagnating at a large value:
  - Another indicator of potential RBM's
  - Add BC's to constrain free DOF's in one or more element blocks
  - Use ITERATION PLOT to find any missed RBM's
  - If loss of contact, element death, *etc.* cause static problem to become dynamic: try using explicit dynamics, implicit dynamics, or control damped solve

# Log File Debugging: Control Contact

Max gap/overlap in any captured interaction

Max gap/overlap compared to face size

Number of evaluated interactions (constant over load step)

Released = open no stiffness  
Captured = closed, have stiffness  
Dubious = changing states

Indicates change in dubious / captured / released interactions

Max change in constraint force among all active interactions

2-norm of linear solve residual + contact gap residual (gap times stiffness)

```

-----
MAX GAP = 8.096e-01 PREVIOUS = 0.000e+00
MAX RELATIVE GAP = 1.457e+00 PREVIOUS = 0.000e+00
NUM INTERACTIONS = 82
RELEASED INTERACTIONS = 52
CAPTURED INTERACTIONS = 30
DUBIOUS INTERACTIONS = 0
RELATIVE LMULT CHANGE = 1.000e+00
ACTIVE SET CHANGE
-----
CONTACT ITERATION = 0, STEP 0
ABSOLUTE RESIDUAL = 6.587e+10
RELATIVE RESIDUAL = 5.414e-01
  
```

# Log File Debugging: Control Contact

```
-----  
MAX GAP = 8.096e-01 PREVIOUS = 0.000e+00  
MAX RELATIVE GAP = 1.457e+00 PREVIOUS = 0.000e+00  
NUM INTERACTIONS = 92  
RELEASED INTERACTIONS = 52  
CAPTURED INTERACTIONS = 30  
DUBIOUS INTERACTIONS = 0  
RELATIVE LMULT CHANGE = 1.000e+00  
ACTIVE SET CHANGE  
-----  
CONTACT ITERATION = 0, STEP 0  
ABSOLUTE RESIDUAL = 6.587e+10  
RELATIVE RESIDUAL = 5.414e-01
```

## Max Gap / Max Relative Gap; Lagrange Multiplier Change:

- If oscillating or stagnating at a large value:
  - Use smaller load step
  - Eliminate discontinuous or large changes in BC's
  - Evaluate log file and visualize previous load steps to see if the cause is a previously poor contact solution
  - Try solver settings that help avoid inherently discontinuous behavior of contact: e.g. Lagrange multiplier settings in control contact, AL penalty factor in contact interactions

# Log File Debugging: Control Contact

```
-----  
MAX GAP = 8.096e-01 PREVIOUS = 0.000e+00  
MAX RELATIVE GAP = 1.457e+00 PREVIOUS = 0.000e+00  
NUM INTERACTIONS = 82  
RELEASED INTERACTIONS = 52  
CAPTURED INTERACTIONS = 30  
DUBIOUS INTERACTIONS = 0  
RELATIVE IMULT CHANGE = 1.000e+00  
ACTIVE SET CHANGE  
-----  
CONTACT ITERATION = 0, STEP 0  
ABSOLUTE RESIDUAL = 6.587e+10  
RELATIVE RESIDUAL = 5.414e-01
```

## Interactions:

- If # dubious interactions never converges to zero and/or, # released/captured interactions continuously change over many contact iterations:
  - Use smaller load step, smoother BC's, different AL settings
  - Evaluate log file and visualize previous load steps to see if the cause is a previously poor contact solution
  - Previously static contact solution could be going dynamic: try explicit dynamics, implicit dynamics, more BC's to maintain static equilibrium, and/or control damped solve

# Log File Debugging: Control Contact

```
-----  
MAX GAP              = 8.096e-01 PREVIOUS = 0.000e+00  
MAX RELATIVE GAP     = 1.457e+00 PREVIOUS = 0.000e+00  
NUM INTERACTIONS     = 82  
RELEASED INTERACTIONS = 52  
CAPTURED INTERACTIONS = 30  
DUBIOUS INTERACTIONS = 0  
RELATIVE LMULT CHANGE = 1.000e+00  
ACTIVE SET CHANGE  
-----  
CONTACT ITERATION = 0, STEP 0  
ABSOLUTE RESIDUAL = 6.587e+10  
RELATIVE RESIDUAL = 5.414e-01
```

## Contact Iterations:

- Reasonable # of iterations: ~5 to ~50
- When to increase max. iterations:
  - Residual still steadily decreasing at max. iterations
  - Contacts are unstable or frequently changing over time
  - Other aspects of problem are temporally non-linear: boundary conditions, thermal conditions, plasticity, failure, ...
- How to decrease iterations necessary for convergence:
  - Smaller load step size
  - Come into current load step with a good initial state (evaluate solutions from previous load steps)



# Log File Debugging: Control Contact

```
-----  
MAX GAP              = 8.096e-01 PREVIOUS = 0.000e+00  
MAX RELATIVE GAP     = 1.457e+00 PREVIOUS = 0.000e+00  
NUM INTERACTIONS     = 82  
RELEASED INTERACTIONS = 52  
CAPTURED INTERACTIONS = 30  
DUBIOUS INTERACTIONS = 0  
RELATIVE LMULT CHANGE = 1.000e+00  
ACTIVE SET CHANGE  
-----  
CONTACT ITERATION = 0, STEP 0  
ABSOLUTE RESIDUAL = 6.587e+10  
RELATIVE RESIDUAL = 5.414e-01
```

## Absolute / Relative Residual:

- Recommendation is to place Control Contact at the outer-most loop (highest level) of the multi-level solve
- Therefore, these residuals represent the quality of the solution of each load step
  - This impacts: solution state and contact interactions used for subsequent load steps, amount of gap/overlap, *etc.*

# Other Debugging Tools

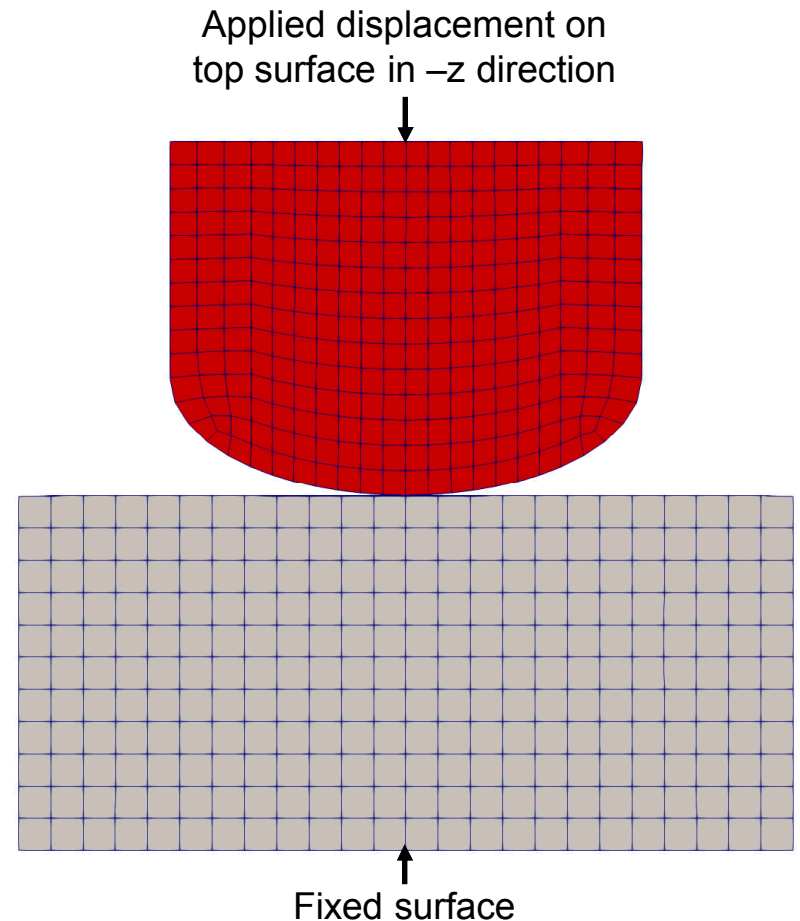
**Every problem is different but almost all require one or more of the following in addition to log file parsing:**

- Visualization. What to look for:
  - Unintended gaps and overlaps
  - Objects passing through each other where contact is expected
  - Non-smooth contact\_status and/or contact\_force fields
- Use `ITERATION PLOT` in solver command blocks
  - This outputs fields for each solution iteration
  - Look for when & where the problem is first going awry
- Try explicit dynamics to separate implicit solver issues from other issues: contact, BC's, mesh, *etc.*
- Output mesh after INITIAL OVERLAP REMOVAL to detect possible poorly-shaped or inverted elements from the removal process
- Problem simplification/isolation: coarsen mesh, remove blocks, use elastic materials, create restart checkpoints, *etc.*

# Debugging Example: Resistance Forge Weld

## Modeled Physics & Numerics

- Elastoviscoplastic material model
- Electrical-thermal-mechanical coupling
- Curved contact interface
- Multiple constraints (some nodes in symmetry plane also in contact)
- Material softening due to heating
- Contact interactions transitioning from frictional to glued



# Debugging Example: Resistance Forge Weld

## Issue: run crashes

### 1. Explore the log file:

- Error caught in material model
- Multiple time step cutback attempts due to inverted elements before crash
- No issue with electrical-thermal

```
Transfer Aria To Adagio, time 0.038, time step 0.001
Advance Adagio_Mechanical, time 0.038, time step 0.001
=====
Begin load step = 46 Solution period time weld is 0.0% complete
Old Time      Time Step      New Time      Stop Time      CPU Time(s)      Wall Time(s)
3.7000e-02    1.0000e-03    3.8000e-02    1.0000e+03    6.9063e+03    1.5030e+09
SIERRA execution failed during execute with the following exception:
Solve loadstep routine encountered a fatal error
Element ComputeInternalForce routine encountered a fatal error
Error: invalid strain rate (NaN). Consider reducing time increment.
error thrown from lame/include/models/Material.h:752
=====
Transfer Aria To Adagio, time 0.037, time step 7.629e-09
Advance Adagio_Mechanical, time 0.037, time step 7.629e-09
=====
Begin load step = 45 Solution period time weld is 0.0% complete
Old Time      Time Step      New Time      Stop Time      CPU Time(s)      Wall Time(s)
3.7000e-02    7.6294e-09    3.7000e-02    1.0000e+03    6.6741e+03    1.5030e+09
=====
              LINEAR      MP      RESIDUAL      RELATIVE      BELYTSCH      ENERGY DISPLACEMENT
              RBM      ITER      ITER
-----
              -      -      0      1.484e+04      3.426e-01      4.330e+04      -
              -      -      -      -      -      -      -
              -      -      -      -      -      -      -
=====
```

Possibly triggered by a bad solution on the previous step or sudden increase in time step? Code fails to recover from error and run crashes

### 2. Visualize results

- Last converged solution looks wrong
- Finding first occurrence of time step cutbacks can point you to the first accepted bad result

```
Caught an Error:
Element ComputeInternalForce routine encountered a fatal error
In method:::: SelectiveDeviatoricElement::ComputeInternalForce ::::
The element on processor 1 with id 5483 has invalid Determinant(J): -2.84632e-09
Attached nodes: 1107 1108 1767 1766 1162 1175 1731 1730
In method:::: SelectiveDeviatoricElement::ComputeInternalForce ::::
The element on processor 1 with id 5483 has invalid Determinant(J): -9.85255e-10
Attached nodes: 1107 1108 1767 1766 1162 1175 1731 1730
In method:::: SelectiveDeviatoricElement::ComputeInternalForce ::::
The element on processor 1 with id 5484 has invalid Determinant(J): -4.54856e-09
Attached nodes: 1107 1109 1768 1767 1175 1108 1732 1731
In method:::: SelectiveDeviatoricElement::ComputeInternalForce ::::
The element on processor 1 with id 5484 has invalid Determinant(J): -1.50281e-09
Attached nodes: 1108 1109 1768 1767 1175 1188 1732 1731
In method:::: SelectiveDeviatoricElement::ComputeInternalForce ::::
The element on processor 1 with id 5488 has invalid Determinant(J): -2.13962e-10
Attached nodes: 1766 1767 1772 1771 1730 1731 1736 1735
In method:::: SelectiveDeviatoricElement::ComputeInternalForce ::::
The element on processor 1 with id 5489 has invalid Determinant(J): -7.22179e-10
Attached nodes: 1767 1768 1773 1772 1731 1732 1737 1736
Attempting to recover by cutting back time step
resetMaterialFailureMarks, Setting 0elements back to alive
Region adagio_mechanical will cut back time step
Transient Time Weld failed, step 38, time 3.70000000e-02, time step 7.6294e-09
```

Time step cutbacks seen also early on in the simulation but code recovered. Time step too big?

### 3. Attempted fixes:

- Increase max iterations of model problem (no noticeable improvement).
- Tighten contact solver tolerance(no noticeable improvement).
- Ungroup interactions (big improvement)

```
Performing contact search
Equation System aria_thermo_elec->main:
* Step : Transient, Strategy: NEWTON, Time: 3.80e-02, Step: 1.00e-03
* Matrix: Solver: "aztec_solver", Unknowns: 13430, Nonzeros: unknown
* Mesh : Processor 0 of 4: 1707 of 5496 elems, 2315 of 6715 nodes
=====
NONLINEAR      LINEAR
Step  Resid  Delta  Itns Status  Resid  Asm/Slv Time
-----
1  1.87e+08  3.29e+12  500  ok  1.12e+14  5.8e-02/4.5e-01
2  2.27e+17  5.67e+20  500  ok  3.44e+18  5.3e-02/4.6e-01
3  3.09e+21  2.49e+24  31  ok  2.80e+15  5.1e-02/5.6e-02
4  2.55e+21  2.49e+24  11  ok  1.41e+14  5.1e-02/4.0e-02
5  1.09e+10  3.67e+13  31  ok  4.39e+03  5.2e-02/5.6e-02
6  3.18e+07  3.26e+10  22  ok  1.11e+01  5.1e-02/4.9e-02
7  2.84e+02  2.93e+05  30  ok  2.38e-04  5.0e-02/5.8e-02
8  1.15e-01  3.24e+02  37  ok  4.91e-08  5.4e-02/6.6e-02
9  6.33e-04  5.15e+00  38  ok  4.07e-10  5.5e-02/6.5e-02
10 7.96e-08  4.09e-04  33  ok  8.03e-15  5.4e-02/6.2e-02
11 6.87e-14      NoOp      5.3e-02
Termination reason: 6.86502e-14 < nonlinear_residual_tolerance(1e-08),
and 0 < nonlinear_correction_tolerance(1e-06)
```

# Debugging Example: Resistance Forge Weld

## Issue: run crashes

### 1. Explore the log file:

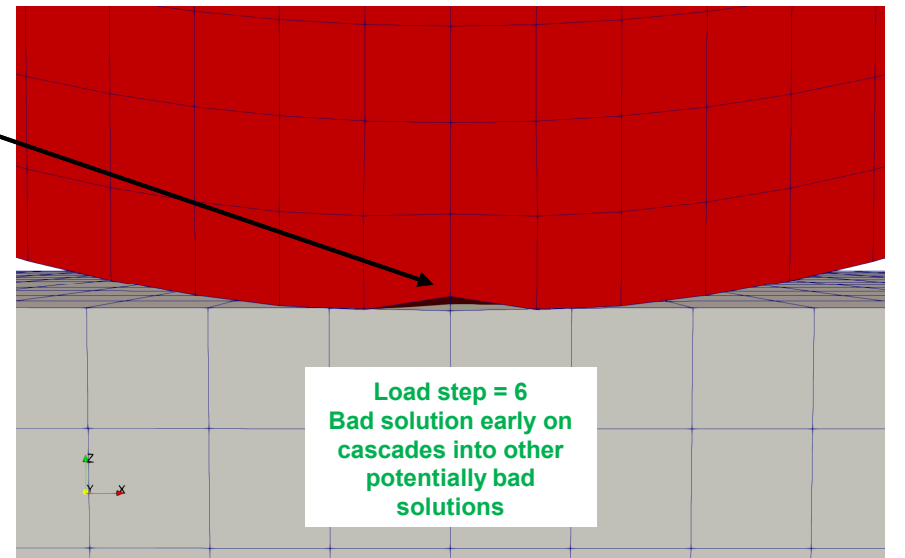
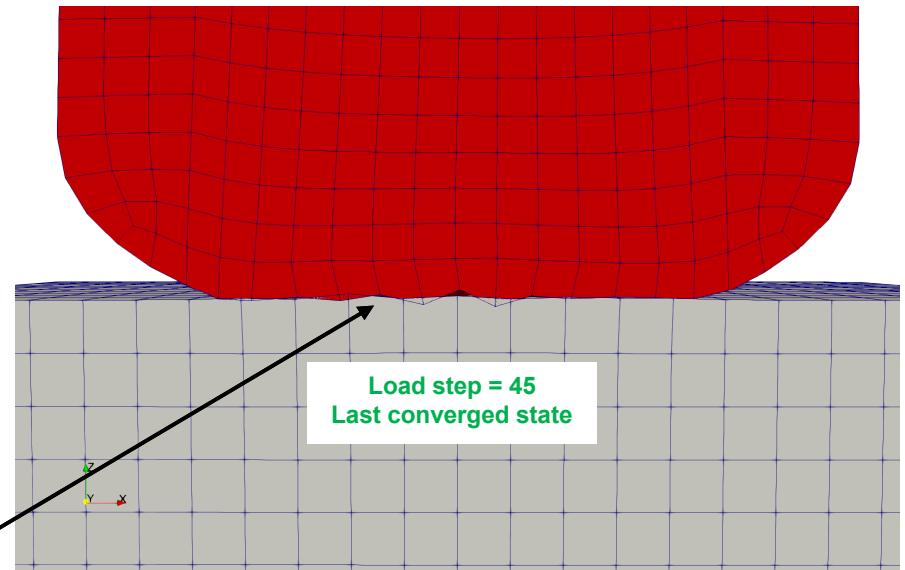
- Error caught in material model
- Multiple time step cutback attempts due to inverted elements before crash
- No issue with electrical-thermal

### 2. Visualize results

- Last converged solution looks wrong
- Finding first occurrence of time step cutbacks can point you to the first accepted bad result

### 3. Attempted fixes:

- Increase max iterations of model problem (no noticeable improvement).
- Tighten contact solver tolerance(no noticeable improvement).
- Ungroup interactions (big improvement)



# Debugging Example: Resistance Forge Weld

## Issue: run crashes

### 1. Explore the log file:

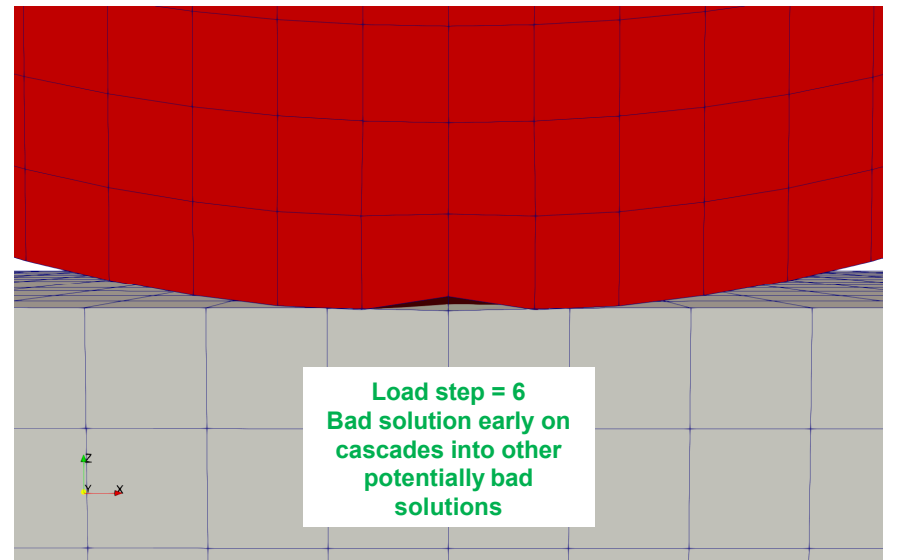
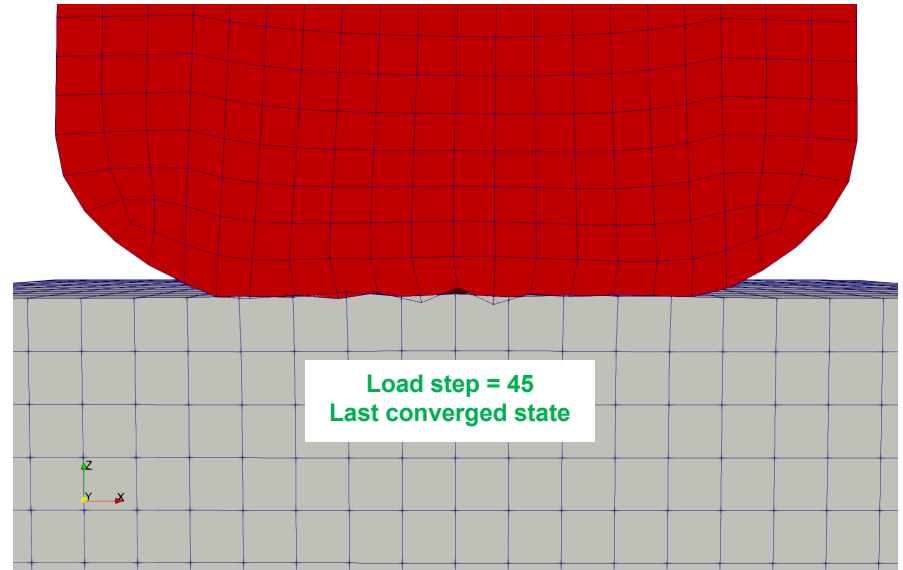
- Error caught in material model
- Multiple time step cutback attempts due to inverted elements before crash
- No issue with electrical-thermal

### 2. Visualize results

- Last converged solution looks wrong
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# Debugging Example: Resistance Forge Weld

## Issue: run crashes

### 1. Explore the log file:

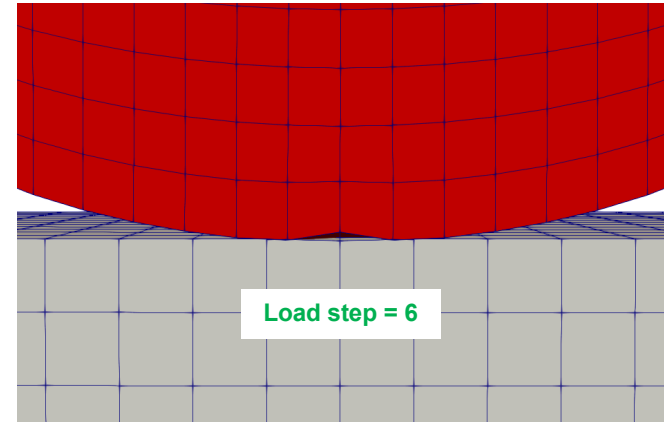
- Error caught in material model
- Multiple time step cutback attempts due to inverted elements before crash
- No issue with electrical-thermal

### 2. Visualize results

- Last converged solution looks wrong
- Finding first occurrence of time step cutbacks can point you to the first accepted bad result

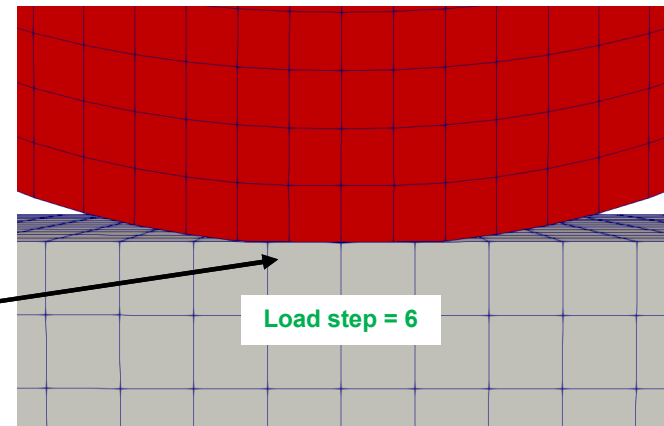
### 3. Attempted fixes:

- Increase max iterations of model problem (no noticeable improvement).
- Tighten contact solver tolerance (no noticeable improvement).
- Ungroup interactions (big improvement)



```
Begin Interaction mech_int1
  surfaces = block_1, block_2
  friction Model = nfd
  developer command: group interactions = false
End

begin nodal field dependent friction model nfd
  contact transition reduction method = min
  initial contact transition value = 0.1 # not bonded
End
```



# Debugging Example: Resistance Forge Weld

## Issue: run crashes

### 1. Explore the log file:

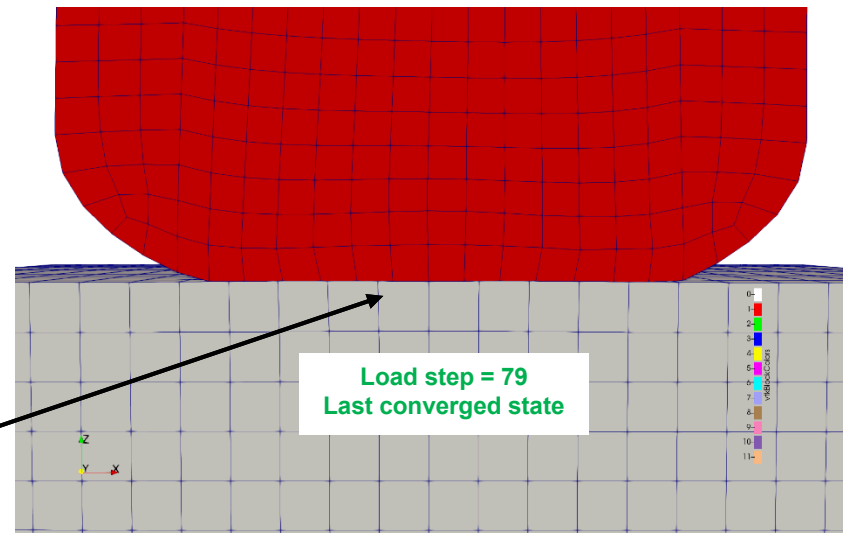
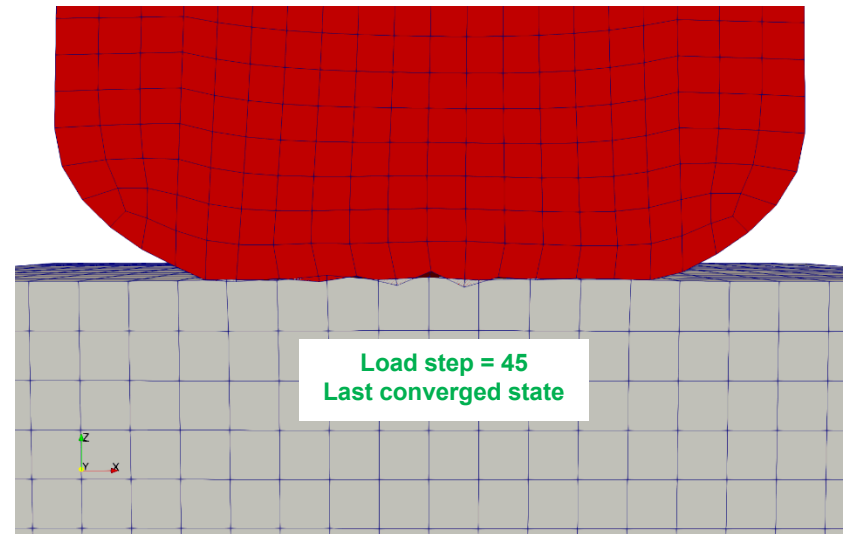
- Error caught in material model
- Multiple time step cutback attempts due to inverted elements before crash
- No issue with electrical-thermal

### 2. Visualize results

- Last converged solution looks wrong
- Finding first occurrence of time step cutbacks can point you to the first accepted bad result

### 3. Attempted fixes:

- Increase max iterations of model problem (no noticeable improvement).
- Tighten contact solver tolerance (no noticeable improvement).
- Ungroup interactions (big improvement)





# Debugging Example: Resistance Forge Weld

## Issue: run crashes

### 1. Explore the log file:

- Error caught in material model
- Multiple time step cutback attempts due to inverted elements before crash
- No issue with electrical-thermal

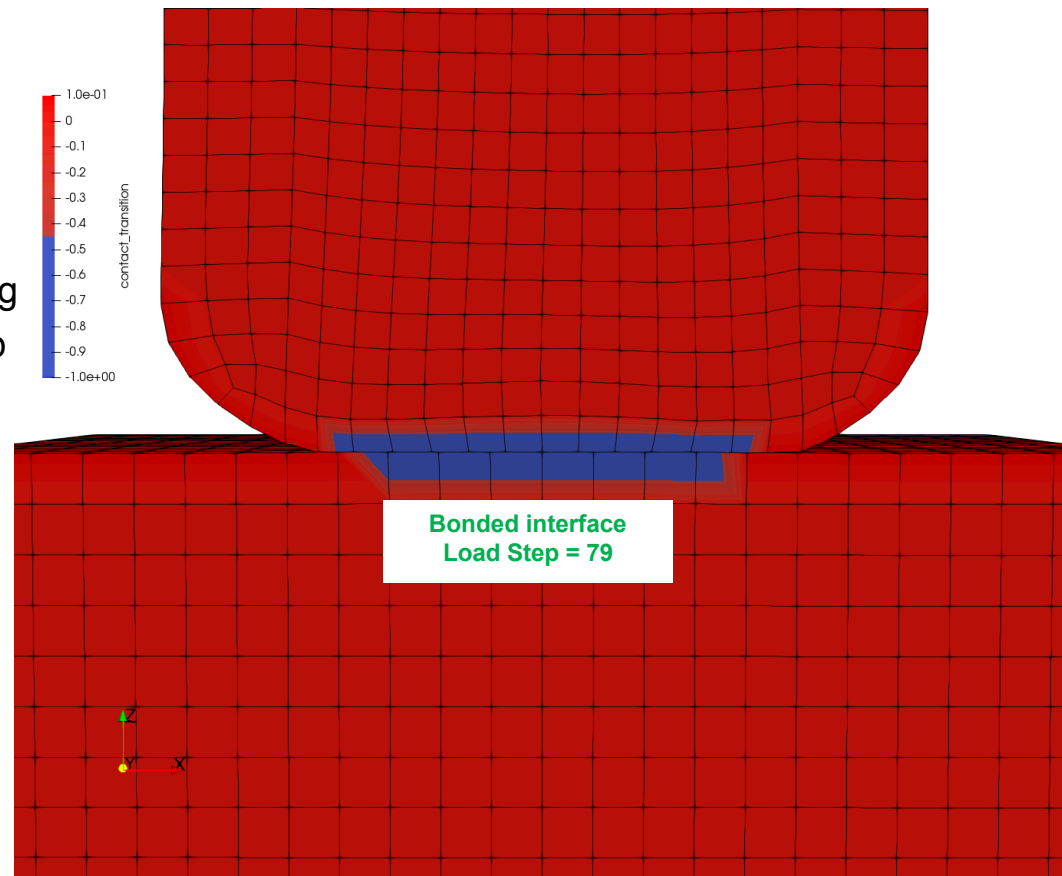
### 2. Visualize results

- Last converged solution looks wrong
- Finding first occurrence of time step cutbacks can point you to the first accepted bad result

### 3. Attempted fixes:

- Increase max iterations of model problem (no noticeable improvement).
- Tighten contact solver tolerance(no noticeable improvement).
- Ungroup interactions (big improvement)

- The option to ungroup interactions is still in development
- Our tests have not justified making it the default
- It improves the contact solution for some problems, such as this one with non-planar faces in contact.

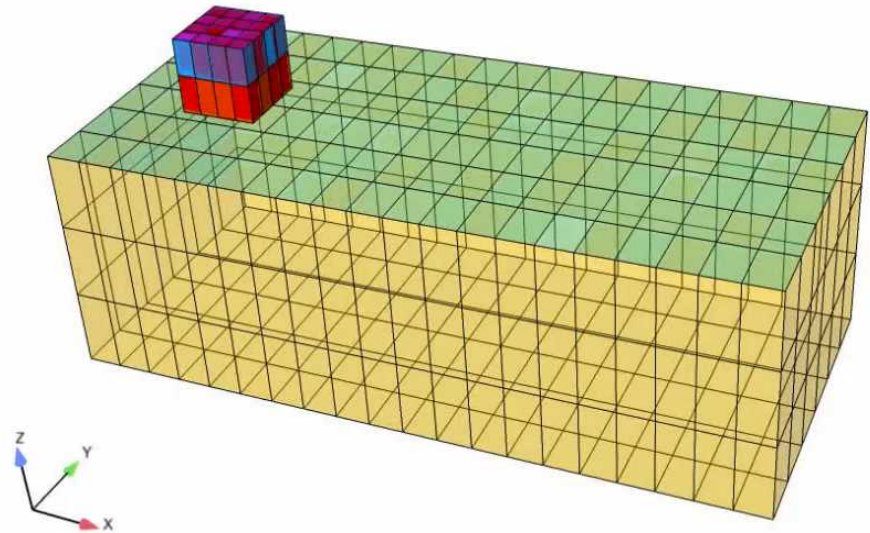


# Debugging Example: Stiff Block on Soft Block

## Modeled Physics & Numerics

- Implicit quasi-statics
- Large difference in stiffness between contacting blocks
- Different mesh sizes between contacting blocks
- Large deformation contact
- Corner contact
- Stick-slip transition
- Mean-quadrature hex8
- Hyperelastic hourglass control

**Initial setup:  
contact lost & solver  
fails at 33% of simulation**



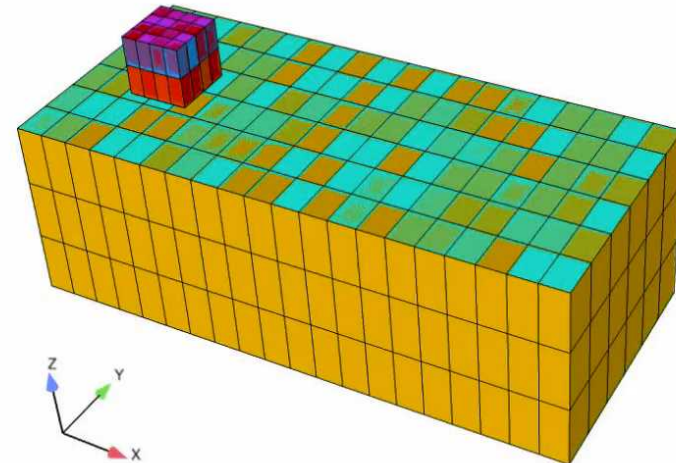
# Debugging Example: Stiff Block on Soft Block

## Debugging Process

- Observed that corners of cube were penetrating the most
  - Changed from `face_face` to `node_face` for better corner contact
- Aided contact by manually defining most robust master/slave surfaces:
  - Coarse mesh  $\rightarrow$  master
  - Fine mesh  $\rightarrow$  slave
- Observed intermittent loss of `contact_force` of some nodes
  - Manually increased search tolerance

## Final setup:

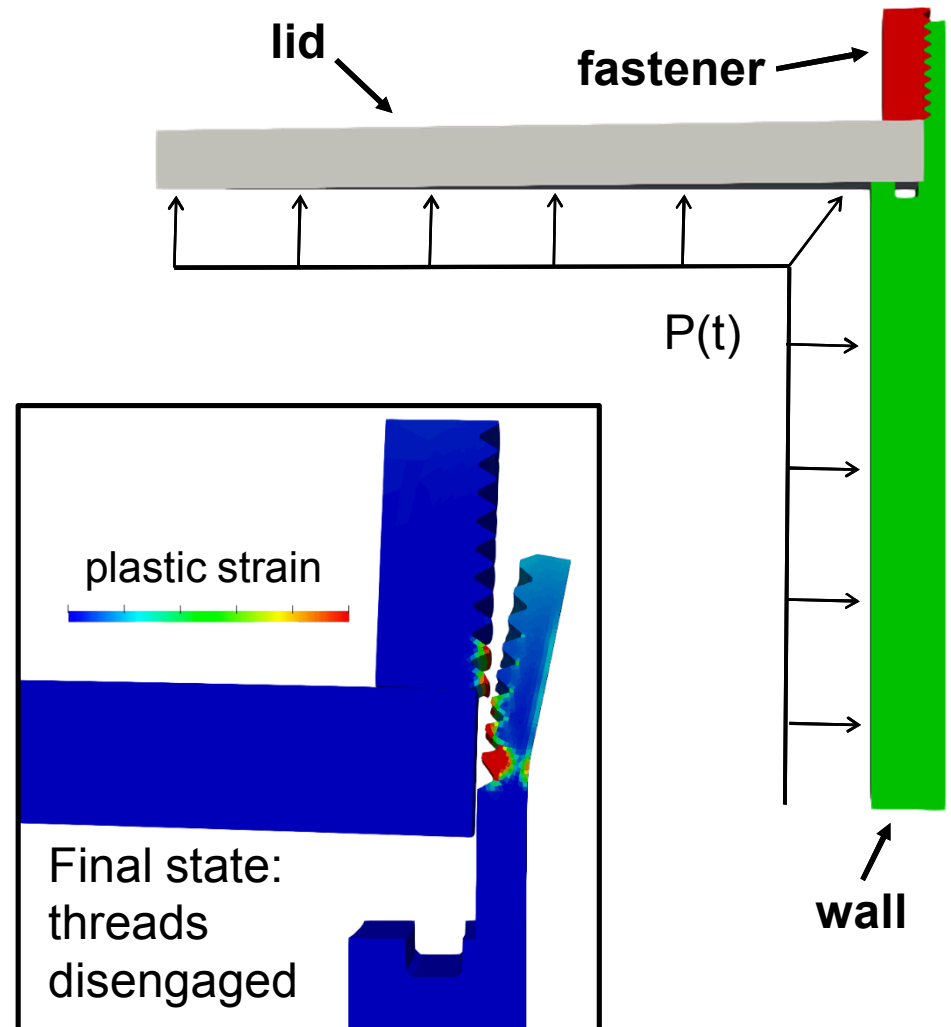
**better contact enforcement &  
simulation runs to completion**



# Debugging Example: Pressurized Can

## Modeled Physics & Numerics

- Mean-quadrature hex8
- Elasto-visco-plastic
- Thermal-mechanical
  - Temperature dependent material parameters
  - No thermal strain
- External heating above lid
- Ramped internal pressure
- Frictional contact
  - Between lid and wall of can
  - Along threaded fastener
- Contact seating
- Transition from static to dynamic
  - Lid/threads disengaging due to pressure and thermal softening
- Multiple stick-slip transitions



# Debugging Example: Pressurized Can

## Input Deck Settings of a Successful & Efficient Analysis

```
begin implicit dynamics
  # switch from statics to dynamics
  # before lid starts disengaging
  active periods = p2
end

begin adaptive time stepping
  cutback factor = 0.5
  maximum failure cutbacks = 4
end adaptive time stepping

begin contact definition sliding
  skin all blocks = on
  begin friction model const_friction
    friction coefficient = 0.3
  end friction model const_friction
  begin interaction defaults
    general contact = on
    self contact = off
    friction model = const_friction
    al penalty = 0.005
  end interaction defaults
end contact definition sliding
```

```
begin solver
  begin loadstep predictor
    type = scale_factor
    scale factor = 0.0
  end loadstep predictor

  begin control contact
    target relative residual = 1.0e-4
    acceptable relative residual = 1.0e-3
    maximum iterations = 50
  end control contact

  begin cg
    target relative residual = 5.0e-5
    acceptable relative residual = 1.0e3
    maximum iterations = 30
    reference = belytschko
    begin full tangent preconditioner
      nodal preconditioner = probe
      minimum smoothing iterations = 5
      small number of iterations = 20
    end full tangent preconditioner
  end cg
end solver
```

# Debugging Example: Pressurized Can

## Input Deck Settings of a Successful & Efficient Analysis

```
begin implicit dynamics
  # switch from statics to dynamics
  # before lid starts disengaging
  active periods = p2
end

begin adaptive time stepping
  cutback factor = 1.0e-4
  maximum failure = 1.0e-3
end adaptive time stepping

begin contact definition sliding
  skin all blocks
  begin friction model const_friction
    friction coefficient = 0.3
  end friction model const_friction
  begin interaction defaults
    general contact = on
    self contact = off
    friction model = const_friction
    al penalty = 0.005
  end interaction defaults
end contact definition sliding

begin solver
  begin loadstep predictor
    type = scale_factor
    scale factor = 0.0
  end loadstep predictor

  begin control contact
    target relative residual = 5.0e-5
    acceptable relative residual = 1.0e3
    maximum iterations = 30
    reference = belytschko
    begin full tangent preconditioner
      nodal preconditioner = probe
      minimum smoothing iterations = 5
      small number of iterations = 20
    end full tangent preconditioner
  end cg
end solver
```

**In the following slides we explore what happens if these settings are used but with one command modified.**

# Debugging Example: Pressurized Can

## Implicit Dynamics vs. Quasi-statics When Threads Disengage

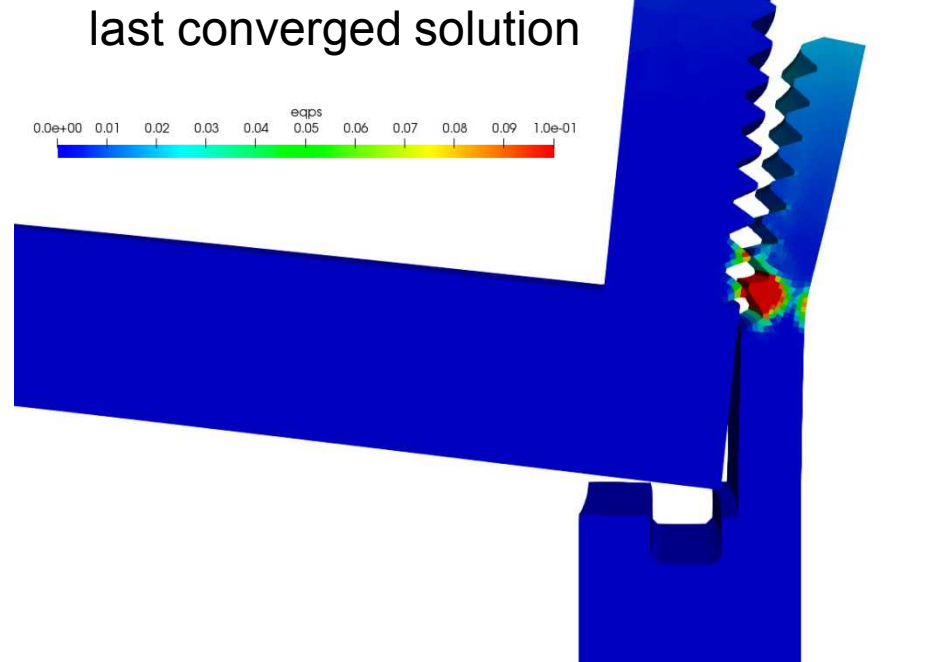
```
begin implicit dynamics
  active periods = p2
end
```



```
# begin implicit dynamics
#   active periods = p2
# end
```

runs to completion

fails: immediately before threads disengaging



# Debugging Example: Pressurized Can

## Non-default AL Penalty vs. Default

```
begin interaction defaults
```

```
...
```

```
  al penalty = 0.005
```

```
end interaction defaults
```



```
begin interaction defaults
```

```
...
```

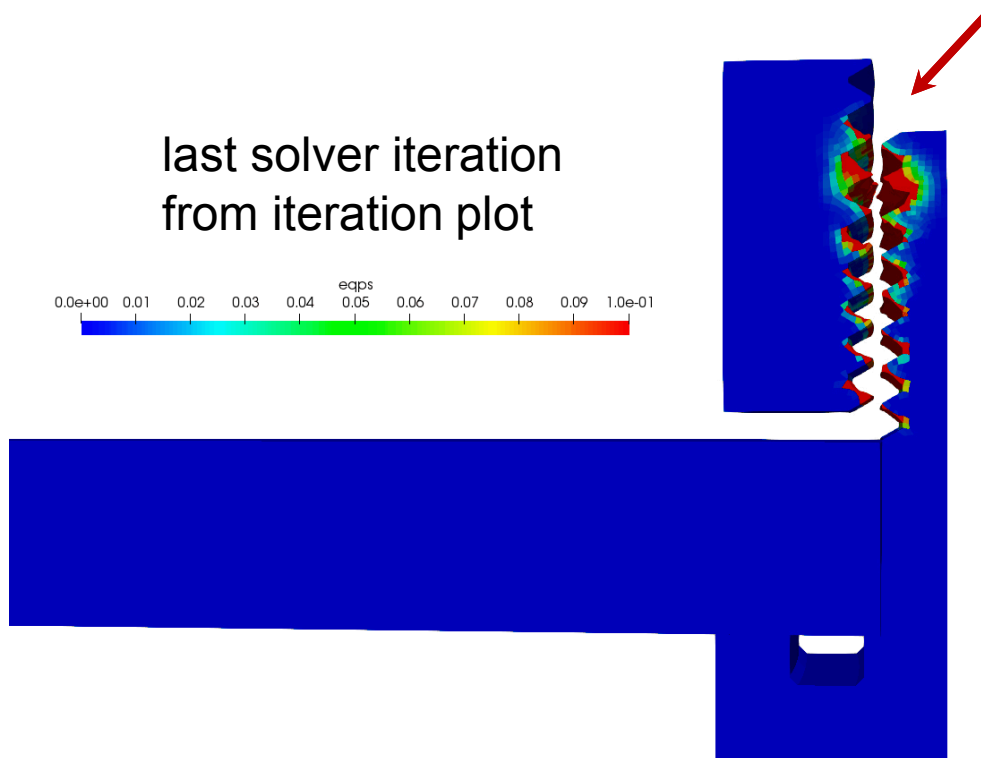
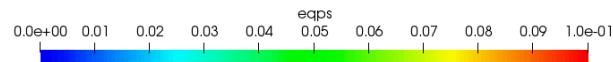
```
  # default [al penalty = 1.0]
```

```
end interaction defaults
```

runs to completion

fails: contact seating unsuccessful in first step

last solver iteration  
from iteration plot





# Debugging Example: Pressurized Can

## Skin All Blocks w/ General Contact vs. Specifying Surface-Surface Interactions

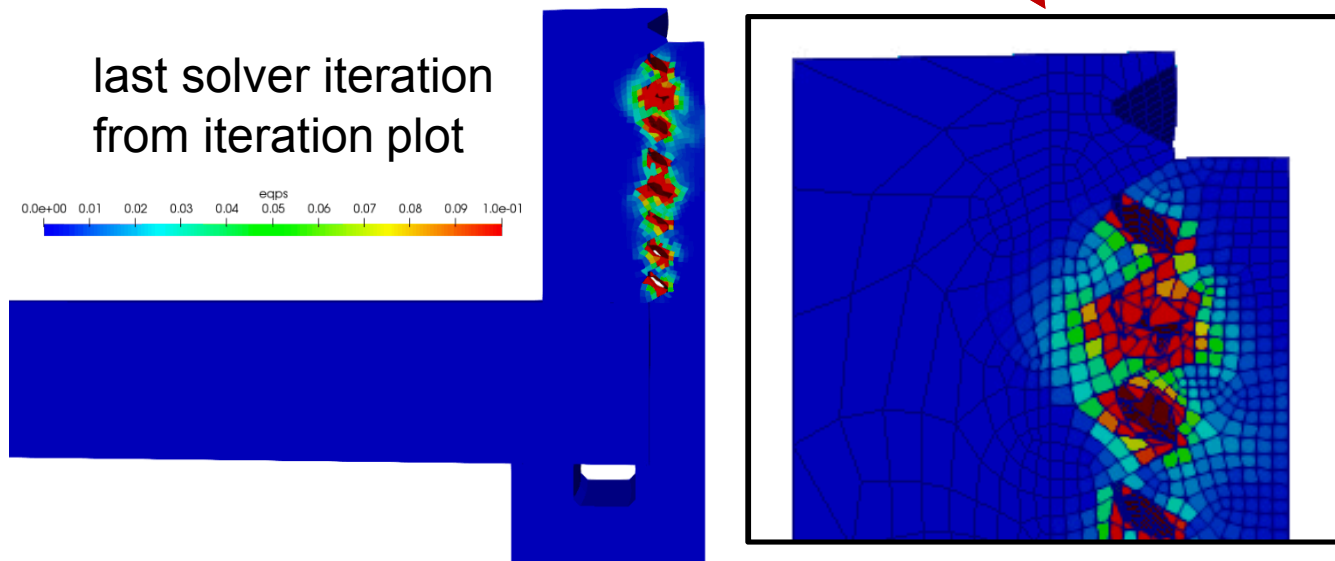
```
begin contact definition sliding
  skin all blocks = on
  begin interaction defaults
    general contact = on
    ...
```



```
contact surface cs5 contains surface_5
contact surface cs6 contains surface_6
begin interaction threads
  master = surf_5
  slave = surf_6
  friction model = const_friction
end interaction threads
... [ring-lid and lid-wall interactions]
```

runs to completion

fails: inverted elements in first step



# Debugging Example: Pressurized Can

## Not Using Predictor vs. Using Predictor

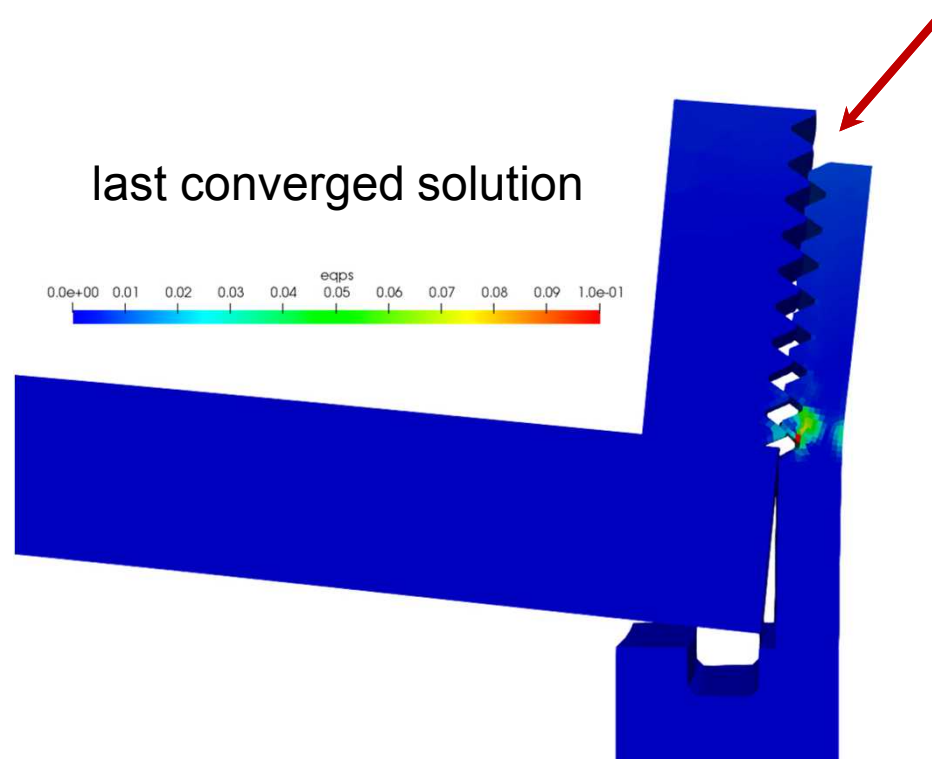
```
begin loadstep predictor
  type = scale_factor
  scale factor = 0.0
end loadstep predictor
```

runs to completion



```
begin loadstep predictor
  type = scale_factor
  scale factor = 1.0
end loadstep predictor
```

fails: 2 steps before threads disengage



# Debugging Example: Pressurized Can

## Using Smoothing Iterations vs. Not Using Smoothing Iterations

```
begin cg
...
begin full tangent preconditioner
...
  minimum smoothing iterations = 5
end full tangent preconditioner
end cg
```

**runs to completion**

**run time = 1300 sec.**

```
begin cg
...
begin full tangent preconditioner
...
  # default [minimum smoothing iterations = 0]
end full tangent preconditioner
end cg
```

**runs to completion**

**run time = 5000 sec.**

**~4X slowdown**

# Debugging Example: Pressurized Can

## Using Small Number of Iterations vs. Not Using Small Number of Iterations

```
begin cg
...
begin full tangent preconditioner
...
  small number of iterations = 20
end full tangent preconditioner
end cg
```

runs to completion

run time = 1300 sec.

```
begin cg
...
begin full tangent preconditioner
...
  # default [update tangent every step]
end full tangent preconditioner
end cg
```

runs to completion

run time = 2700 sec.

**~2X slowdown**

# Summary

- One set of contact solver settings will not be robust for all problems.
- Use the recommended settings to start and be careful when moving parameters from one analysis to the next.
- Identify potential pitfalls in your model.
- The log file is your first line of defense.
- Refer to the “Implicit Solver” and “Contact” sections in the Sierra/SM User’s Guide for further guidance, as well as the “Troubleshooting Guide for Implicit Convergence” appendix.
- Reach out to sierra-help, other analysts or a developer near you.
- Analyst input is of paramount importance to improve default solver settings and log file readability.