

Summary of Zirconium Fire Investigations during Spent Fuel Pool Complete LOCAs

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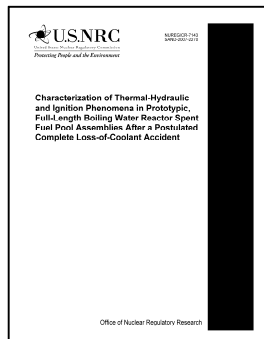
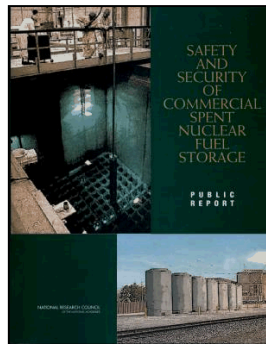
BWR Test Series
Funded by USNRC

PWR Test Series
Funded by USNRC and OECD



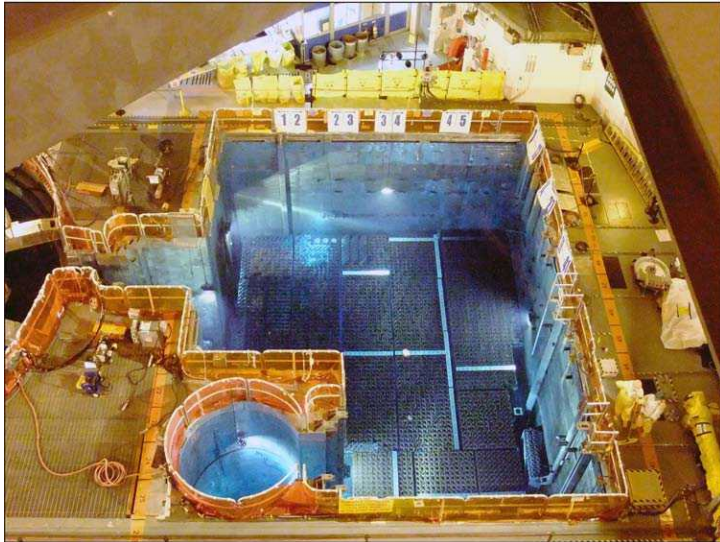
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Post 9/11 Environment

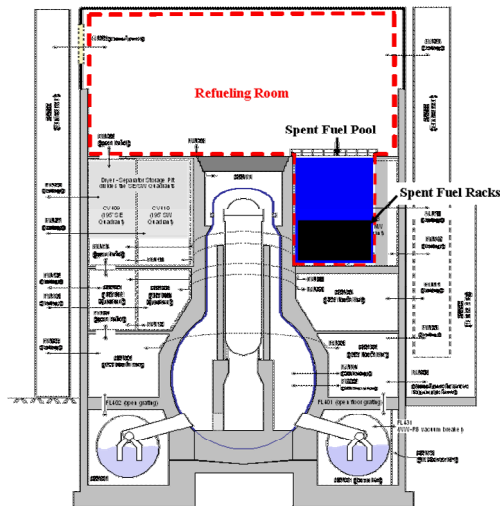


- 2003 – Article identifying potential vulnerabilities of current spent fuel storage
 - Highlighted possibility of zirconium cladding fires in modern, high-density spent fuel pools (SFPs)
 - Recommended transfer to dry storage within five years of discharge
- 2004 – National Research Council produced comprehensive report for Congress on safety and security of spent fuel
 - Found a propagating zirconium cladding fire possible for some partial and complete loss-of-coolant-accidents (LOCAs) in SFPs
 - Resulting in large quantities of radioactive materials to the environment
 - Recommended that USNRC investigate vulnerabilities and consequences of LOCAs in SFPs
- 2005 – USNRC commissioned complete LOCA testing program for boiling water reactor (BWR) fuel
 - Demonstrated zirconium fires in near-prototypic spent fuel
 - Showed potential for propagation between assemblies
- 2009 – USNRC and OECD commissioned complete LOCA testing for pressurized water reactor (PWR) fuel
 - Two full-scale ignition tests completed
 - Clad ballooning and nitrogen depletion observed

Overview

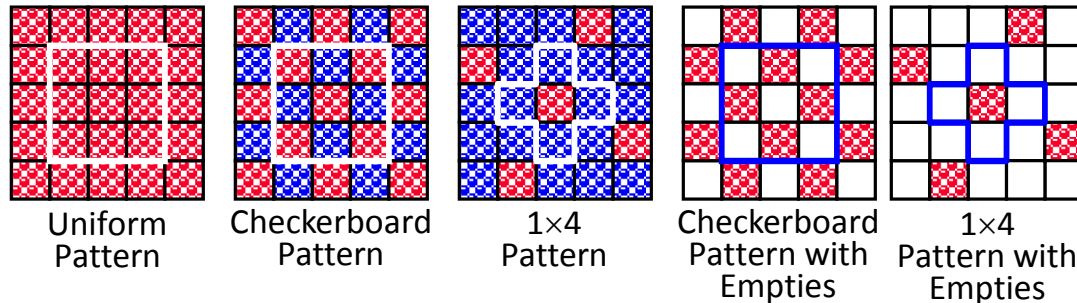





BWR Spent Fuel Pool



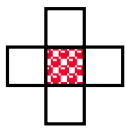

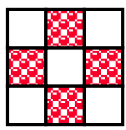
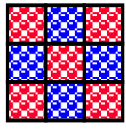
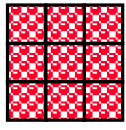
- Validate severe accident codes for whole pool LOCA analyses
- Phased experimental approach
 - Study physical phenomena separately
 - Provide input parameters to accident codes
 - Examine nature of Zircaloy fires in prototypic assemblies
 - Validate predictive capability
 - Develop mitigation strategies

Spent Fuel Pool Configurations



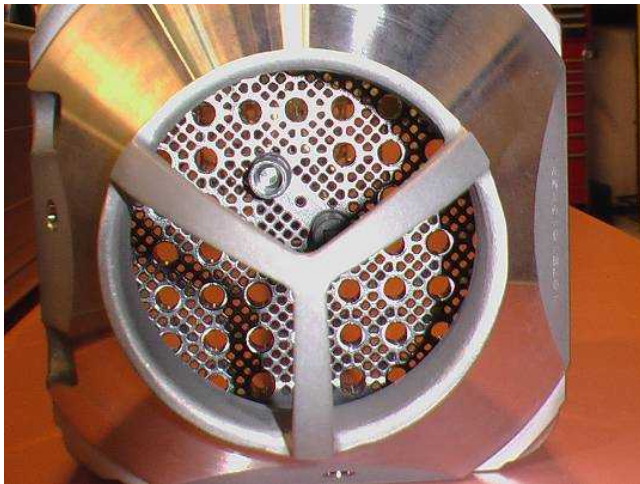
-  Recently discharged, high-power assembly
-  Low-powered assembly discharged many years earlier
-  Empty rack cell

- Low-density racking least vulnerable
- High-density racking with interspersed high and low powered assemblies is best practice for pools near capacity

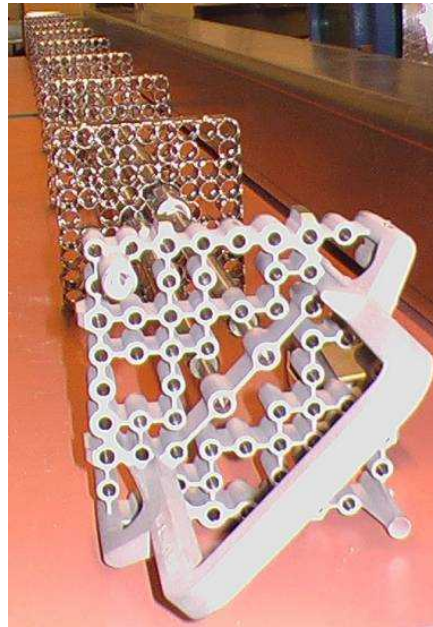
Configuration		Ranking
1x4 empties		Best
1x4		
Checkerboard with empties		Good
Checkerboard		Moderate
Uniform		Worst

BWR Hardware

- Prototypic GE 9x9 BWR Hardware
 - Full length, prototypic GE 9x9 BWR components
 - Electric heater rods with Zr cladding for ignition testing



Nose piece & debris catcher



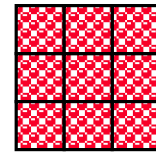
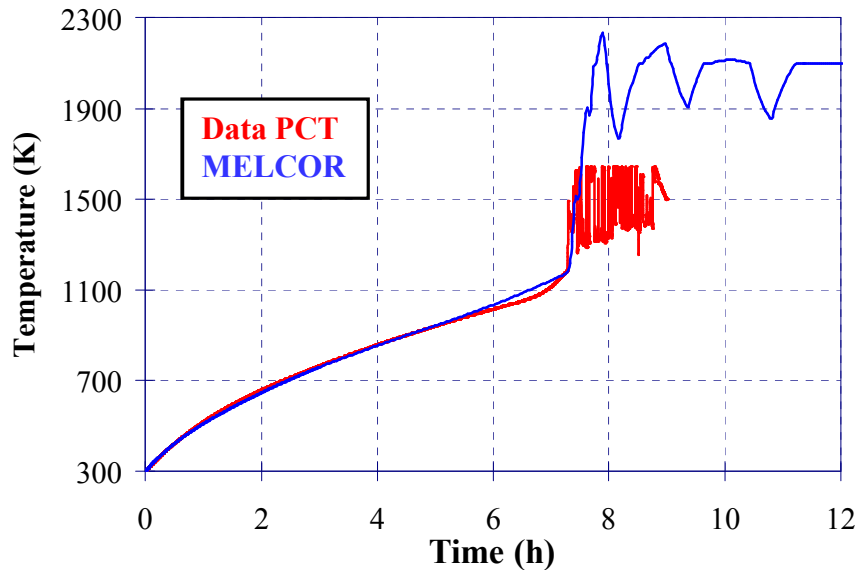
Upper tie plate



BWR channel, water tubes & spacers

Full Length Zr BWR

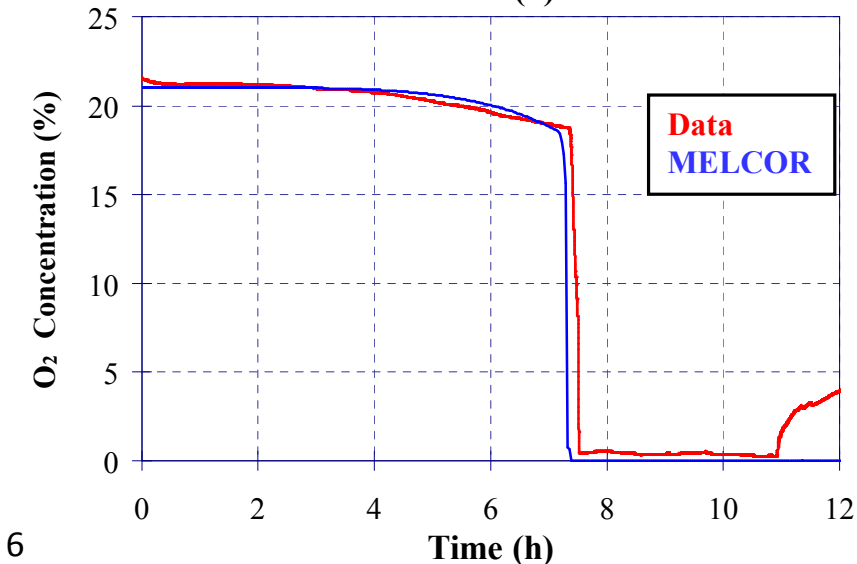
(Ignition Results)



Uniform
Loading



- Assembly power 5.0 kW
 - Situational equivalent of a cluster of 100 day-old assemblies
- MELCOR within 40 K
 - Ignition predicted to within 5 minutes
- Oxygen depletion accurately modeled
 - O₂ reaction kinetics adequately represented

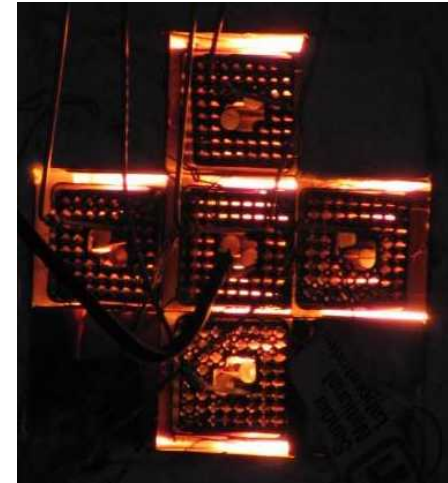
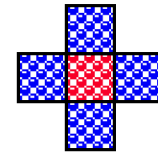
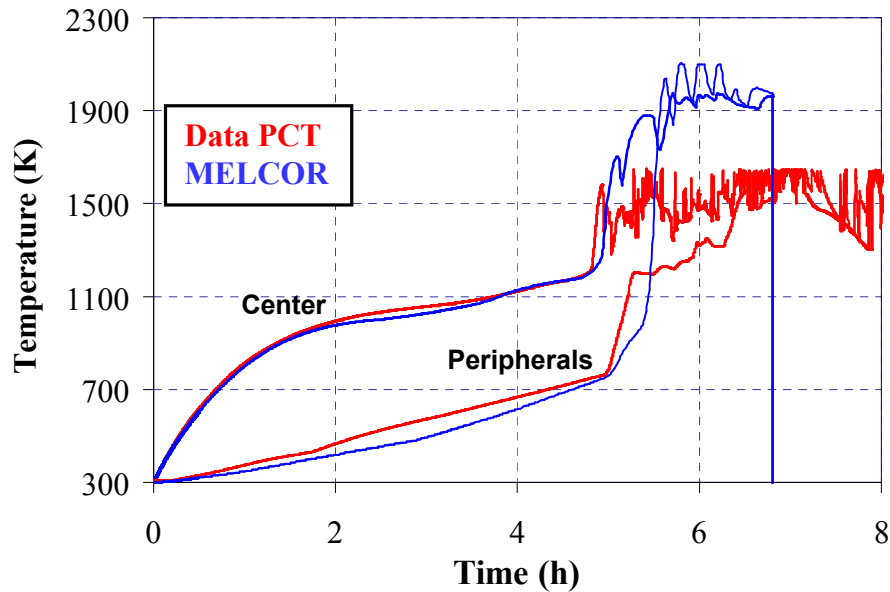


Full Length Zr BWR

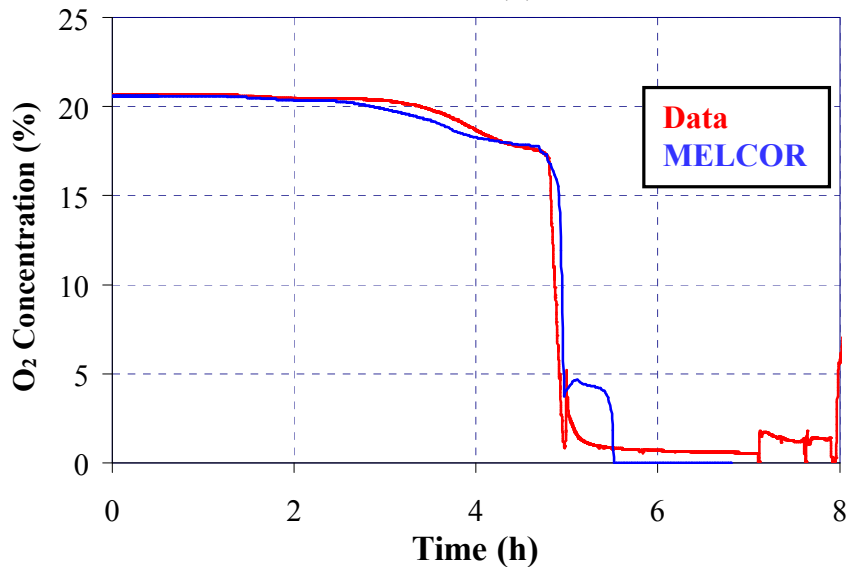
(Ignition Test)



Zircaloy BWR 1×4 Ignition



- “Hot” center assembly in 1×4 arrangement
 - Equivalent of 15 day-old fuel surrounded by background assemblies
 - Air flow rates and temperatures independently controlled
- MELCOR results within 40 K
 - Ignition modeled to within 10 minutes



BWR 1×4 Ignition

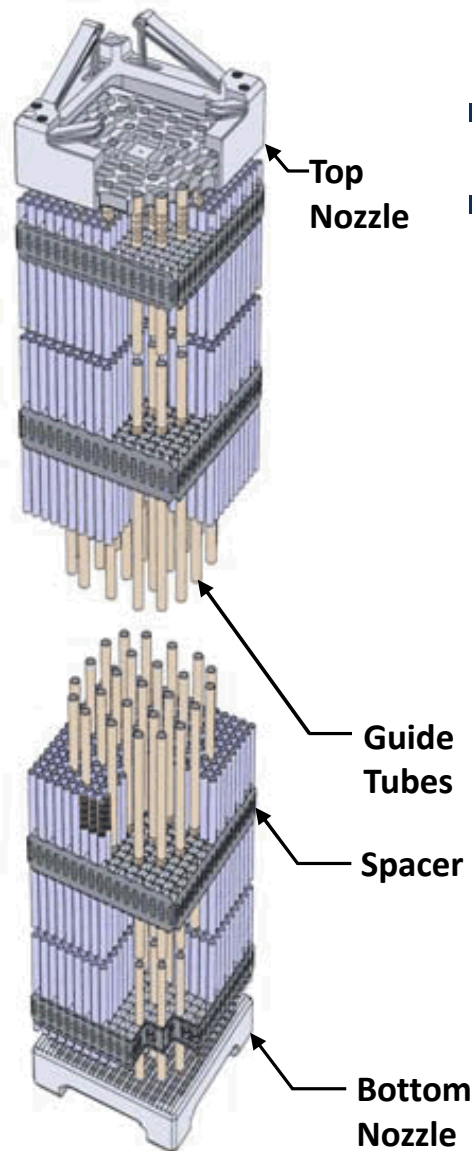
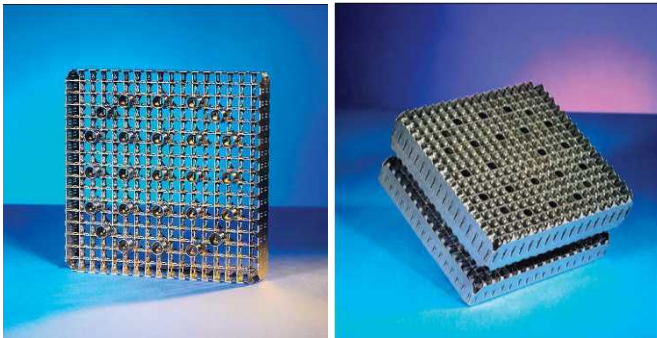
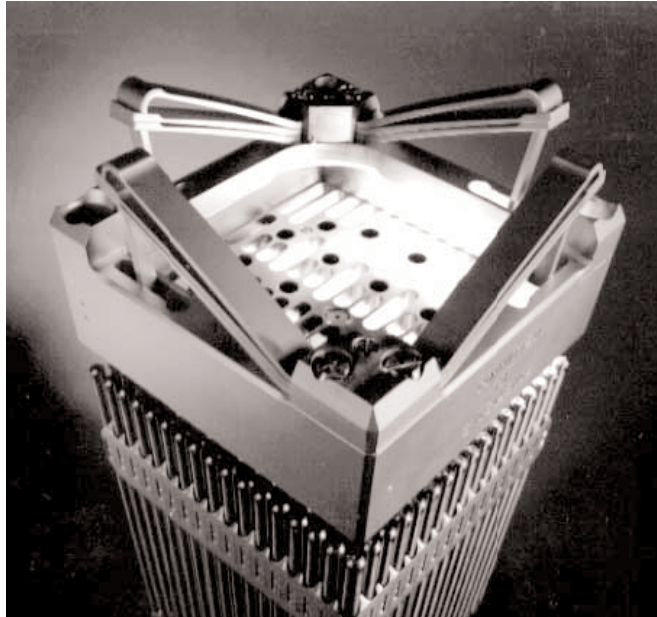
Before



After

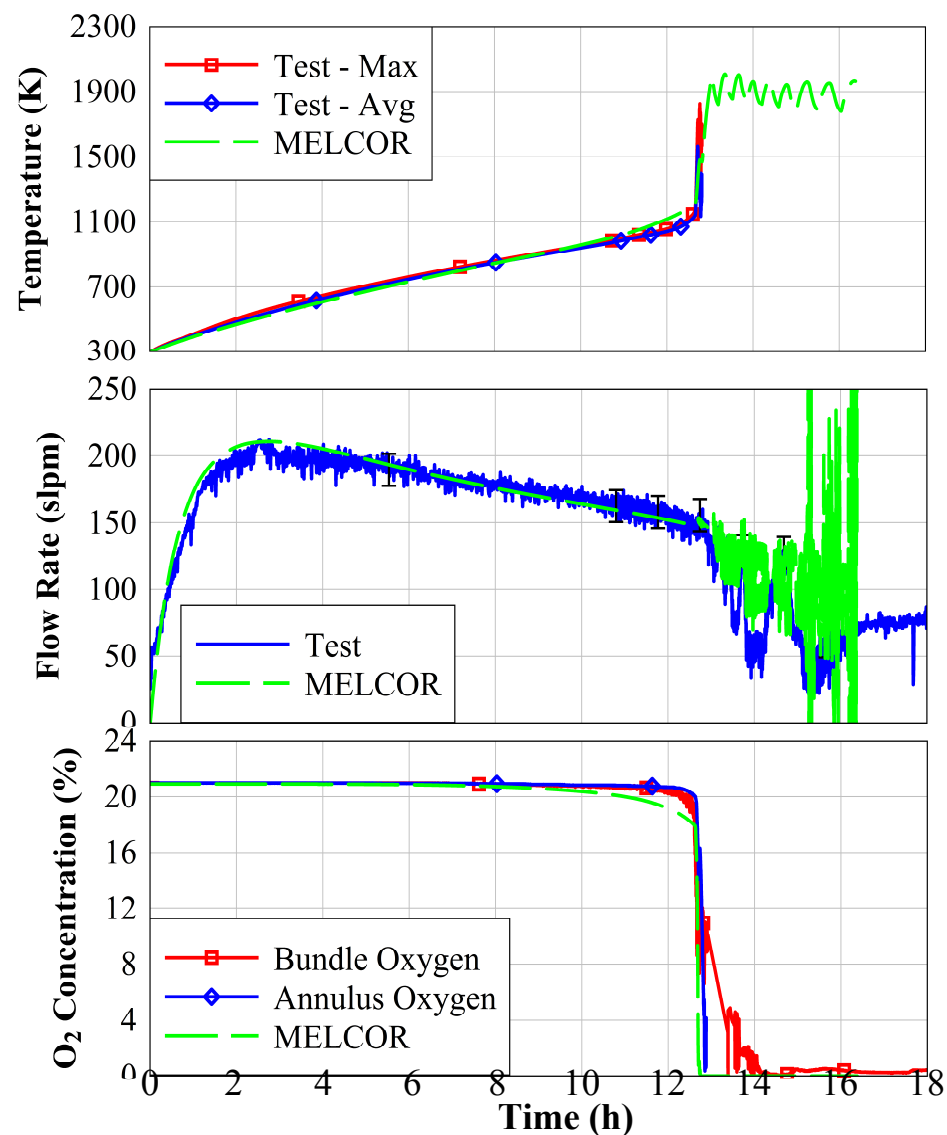


PWR Hardware



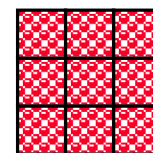
- Prototypic 17×17 PWR
- More form losses than BWR (7 spacers)
 - 8 grid spacers
 - 3 flow mixers
 - 1 debris catcher
 - 264 electric heater rods

PWR Phase 1 Ignition Test Results

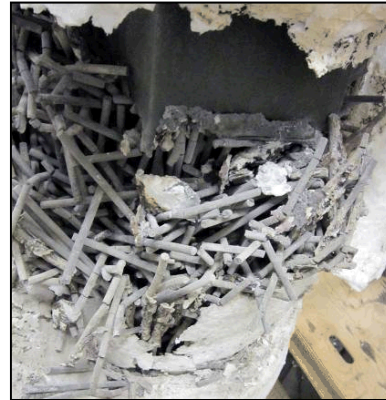


- Assembly power 5.0 kW
 - Situational equivalent of a cluster of 15 month-old assemblies (hot neighbor BC)
- Modeling predicts ignition within 10 minutes
- Thermocouples failed after ignition
 - Sharp transition to breakaway oxidation
 - Oxygen depletion at time of ignition
- Predicted flow rate within experimental uncertainty
- Interesting dynamics on burn-front movement
 - Usually downward to follow oxygen and fresh Zr

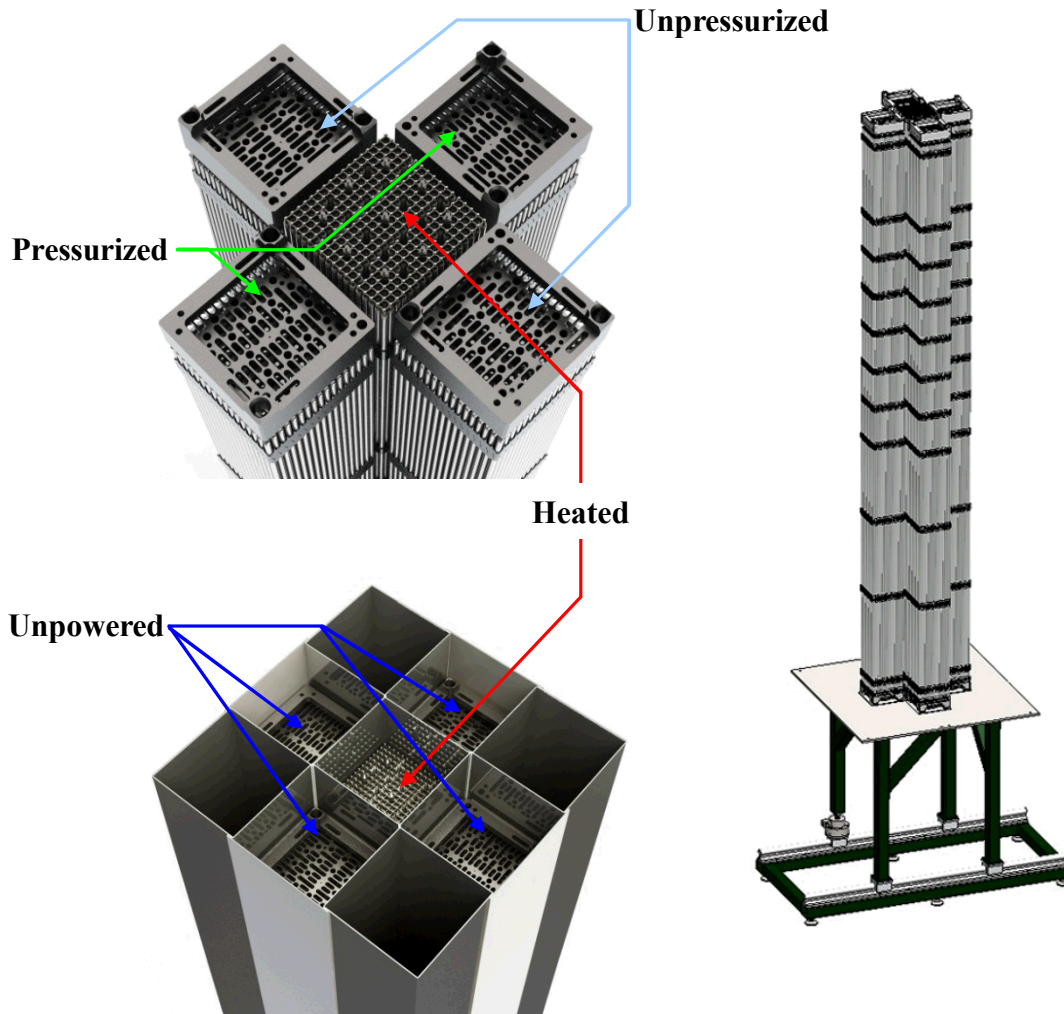
Phase 1 (Uniform Loading) =



PWR Phase 1 Ignition Test

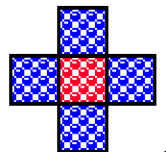


PWR Phase 2 Test Assembly



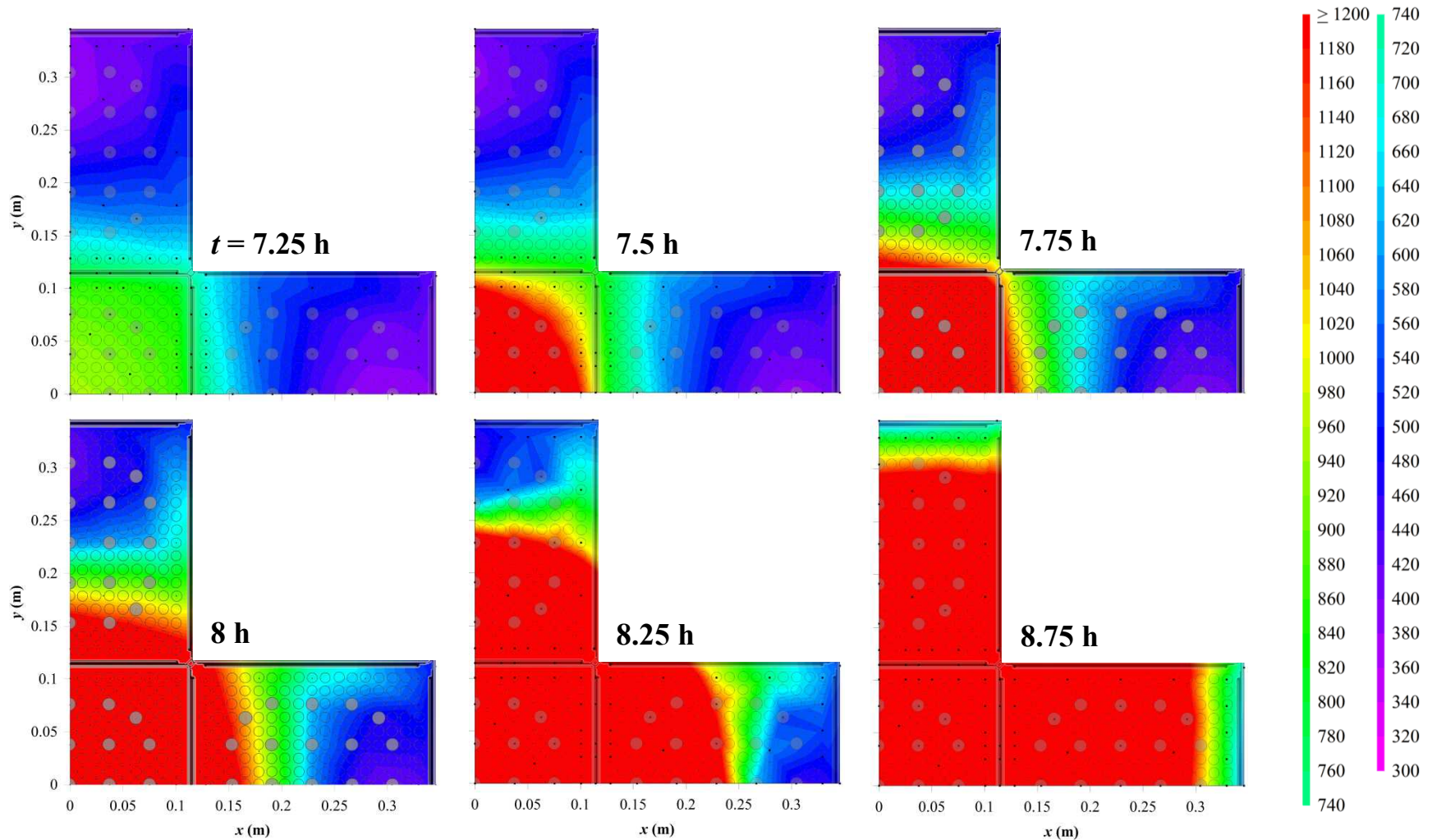
- “Cold Neighbor” Boundary
- Test Assembly
 - 5 full length assemblies in 1×4 arrangement
 - Center heated, peripheral unheated
 - Two peripheral assemblies with all pressurized rods
 - Single prototypic 3×3 pool rack
- Pre-ignition Tests
 - Measure response of different aged assemblies
- Ignition Test
 - Time to ignition for each assembly
 - Time to ballooning
 - Nitrogen reactions

Phase 2 (1×4 Loading) =

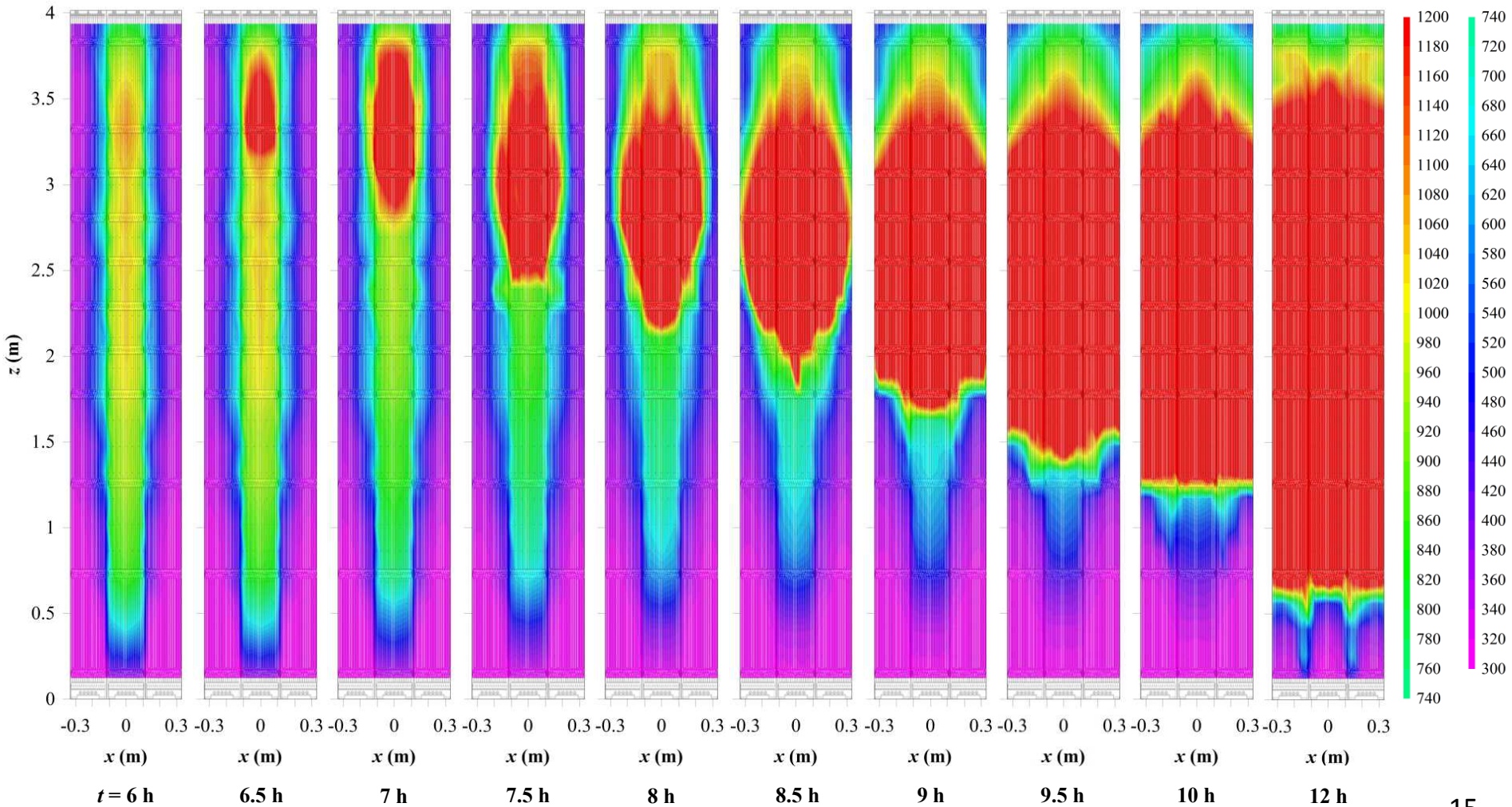


Transverse Propagation

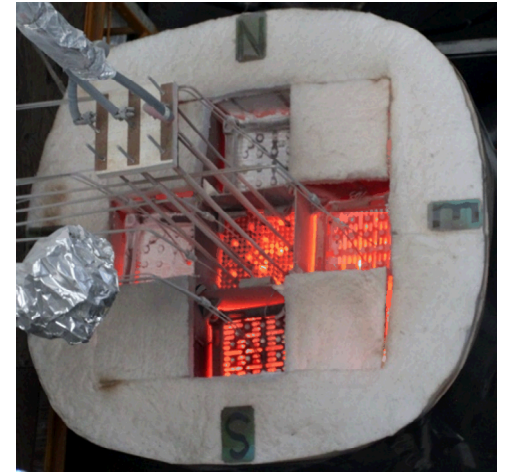
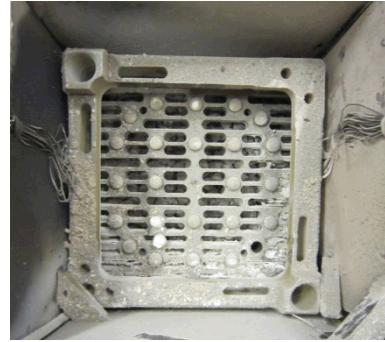
($z = 2.54$ m)



Midplane Propagation

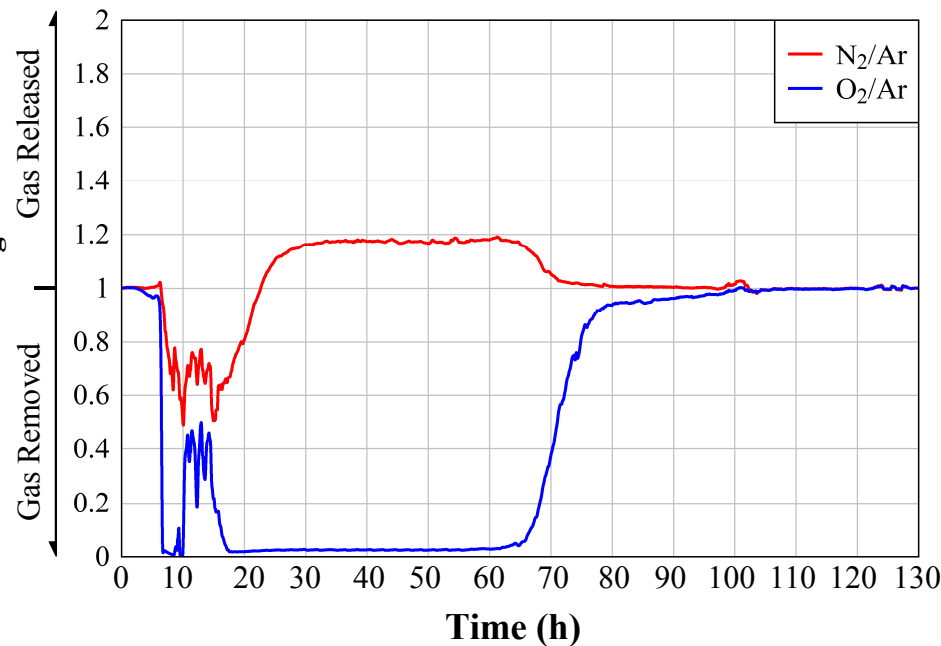


PWR Phase 2 Ignition Test

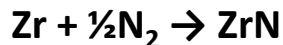
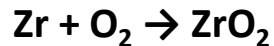


Implications of ZrN Formation

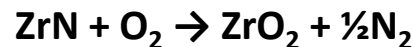
Exhaust Gas Analysis by Mass Spectrometry



Stage 1 Oxidation



Stage 2 Oxidation



- Substantial conversion to ZrN
 - After Stage 1 Oxidation
 - ~22% ZrO₂
 - ~78% ZrN
 - Doubles the energy release
- Nitrogen reactions significant
 - Greater propensity for burn propagation to adjacent assemblies
 - Higher temperatures
 - More energetic burn

Summary

- Sandia SFP complete LOCA ignition testing successfully completed
 - BWR Phase 1 (Uniform) – June 2006
 - BWR Phase 2 (1×4) – August 2006
 - PWR Phase 1 (Uniform) – March 2011
 - PWR Phase 2 (1×4) – June 2012
- Available NUREG/CRs
 - NUREG/CR-7143, “Characterization of Thermal-Hydraulic and Ignition Phenomena in Prototypic, Full-Length Boiling Water Reactor Spent Fuel Pool Assemblies After a Postulated Complete Loss-of-Coolant Accident”
 - NUREG/CR-7144, “Laminar Hydraulic Analysis of a Commercial Pressurized Water Reactor Fuel Assembly”
 - NUREG/CR-7215, “Spent Fuel Pool Project Phase 1: Pre-Ignition and Ignition Testing of a Single Commercial 17×17 Pressurized Water Reactor Spent Fuel Assembly under Complete Loss of Coolant Accident Conditions”
 - NUREG/CR-7216, “Spent Fuel Pool Project Phase II: Pre-Ignition and Ignition Testing of a 1×4 Commercial 17×17 Pressurized Water Reactor Spent Fuel Assemblies under Complete Loss of Coolant Accident Conditions”