

# SPE Phase I Material Properties

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Scott Broome

Sandia National Laboratories

Aviva Sussman, Erika Swanson,  
Jennifer Wilson

Los Alamos National Laboratory

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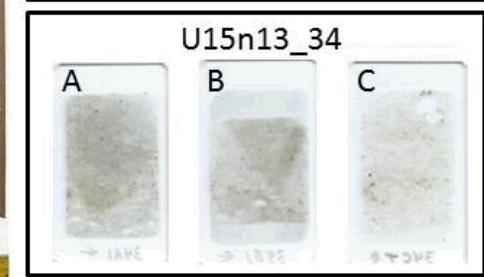
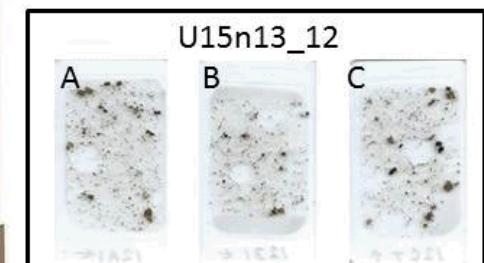
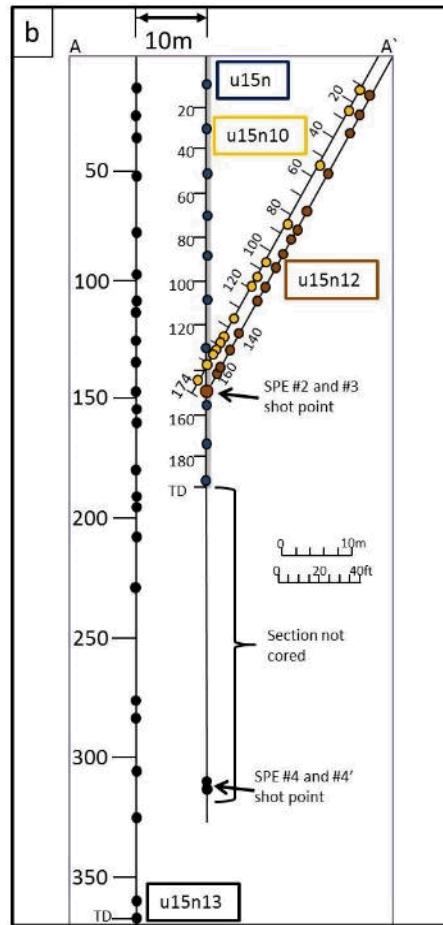
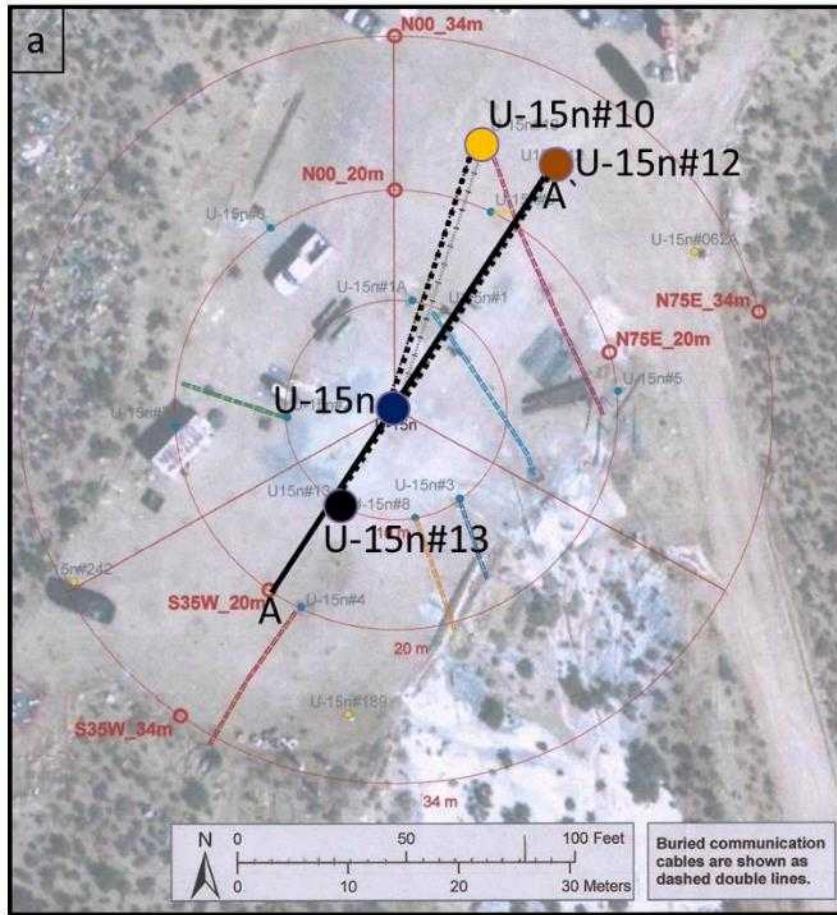
# Material and Fracture Property Analyses

## Linked multi-scale analyses on pre-SPE-1 and post SPE-2, 3 and 5 granite

- **Optical Microscopy**
  - defines extent of damage and controls on surface effects
  - provides damage history (tectonic vs explosion)
  - constrains anisotropy
- **Core-scale Material Property Testing**
  - Unconfined and Triaxial compression (Hydrocode model development)
  - Dynamic and Quasi-static Brazilian Disc Tension (Hydrocode model development)
  - Triaxial compression to investigate permeability and damage relationship
- **Core-scale Fracture Property Testing**
  - Direct Shear tests on natural fractures
  - Triaxial shear on natural fractures (incorporating pore pressure and confining pressure on natural fractures)
  - P&S velocity as a function of fracture aperture with water as coupling medium

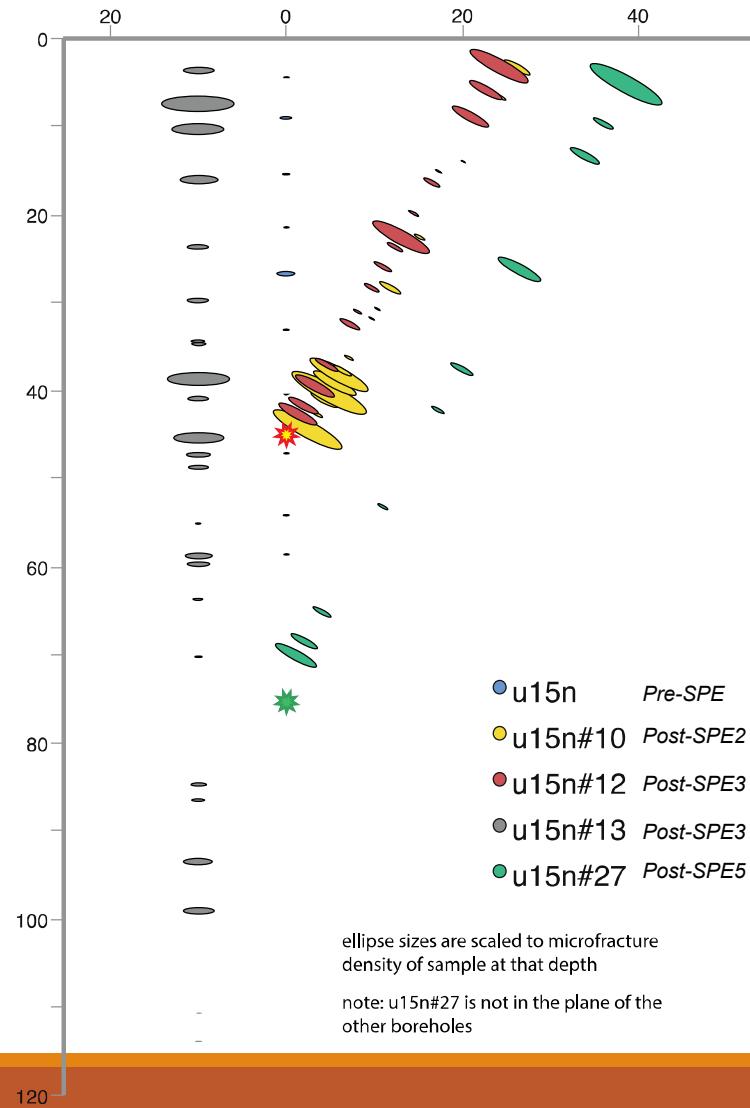
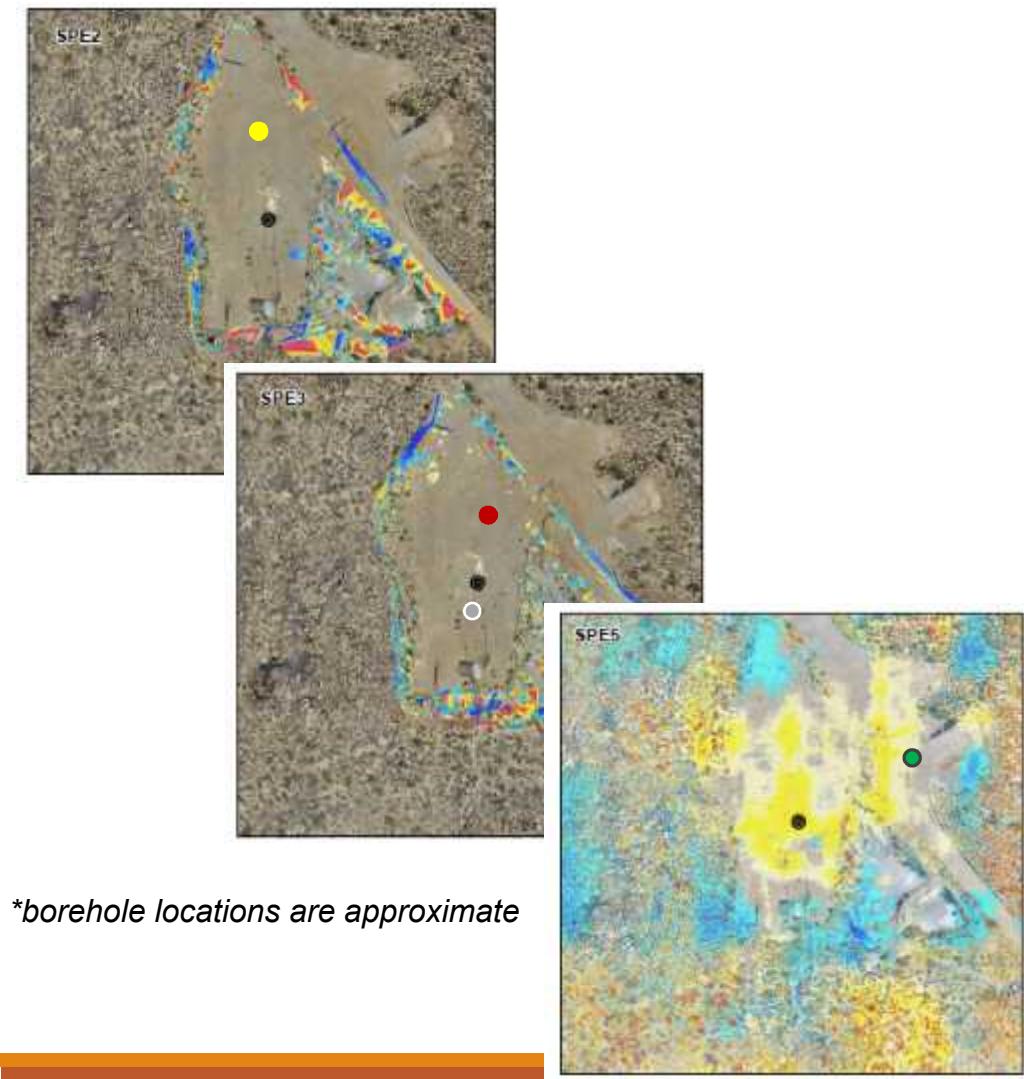
# Material and Fracture Property Analyses

## Linked multi-scale analyses on pre-SPE-1 and post SPE-2, 3 and 5



# Microscale Material and Fracture Property Analyses

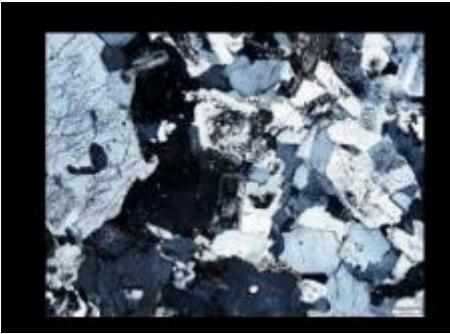
## Linked multi-scale analyses on pre-SPE-1 and post SPE-2, 3 and 5 granite demonstrate rock behavior that controls surface effects



# Microscale Material and Fracture Property Analyses

## Optical Microscopy: anisotropy and damage history

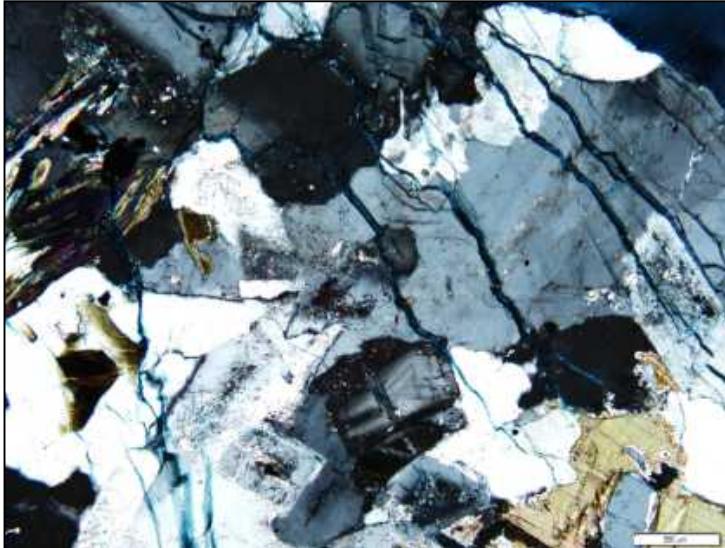
U15n13  
78ft depth  
Intact granite



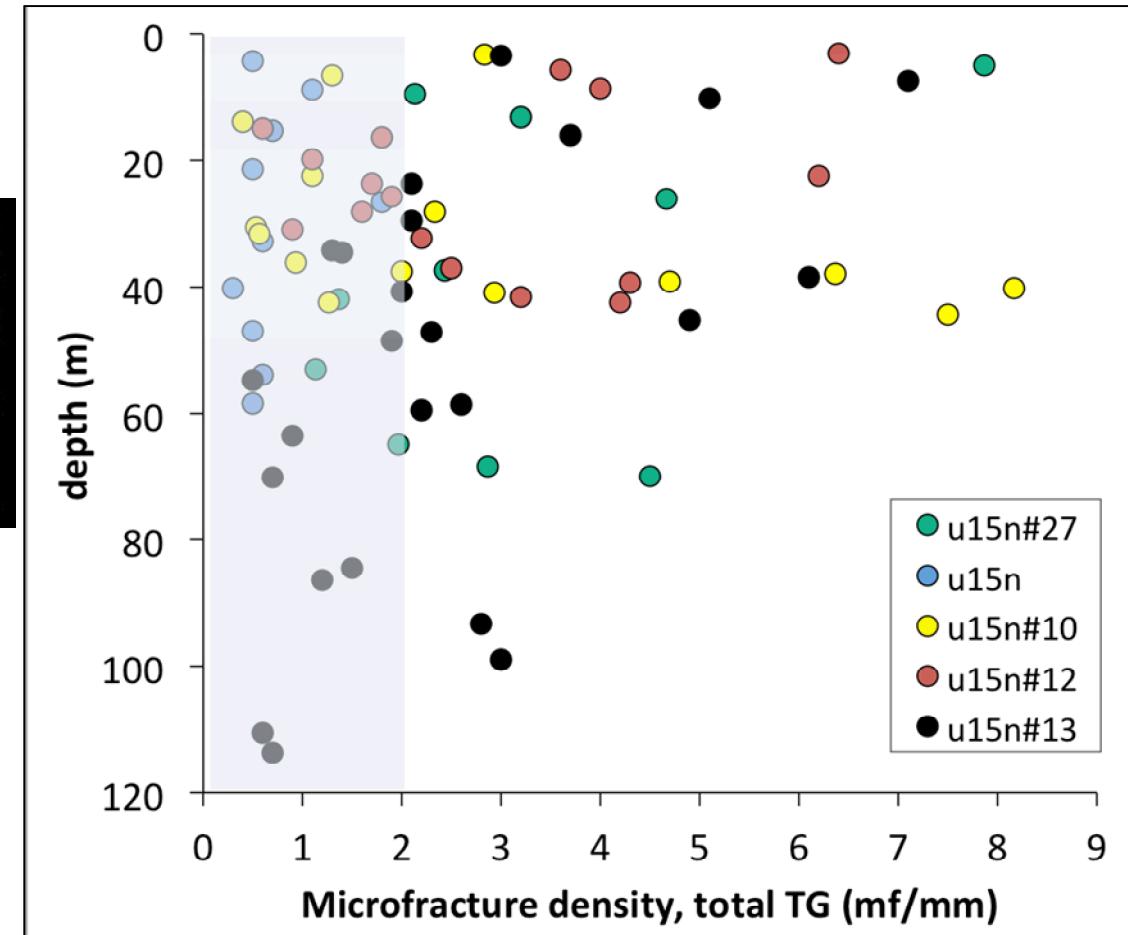
U15n13  
148ft depth  
Faulted granite



U15n13  
34 ft depth  
"Weathered" granite



Postshot

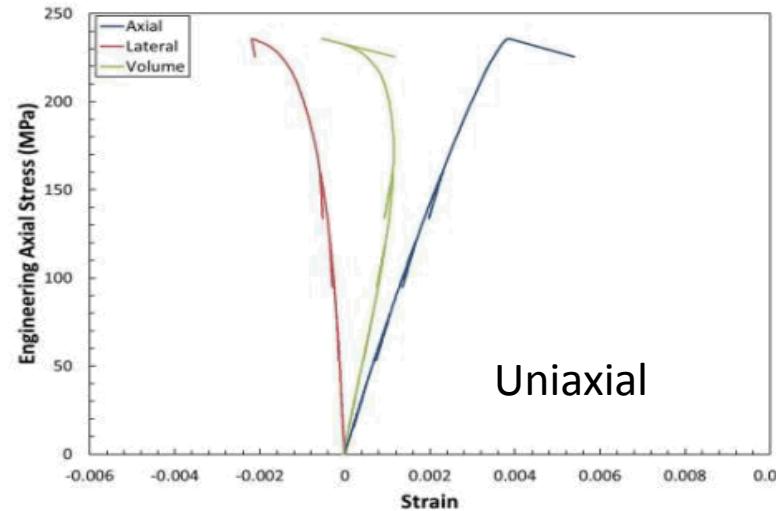


# Core Scale Material Property Analyses

## Uniaxial

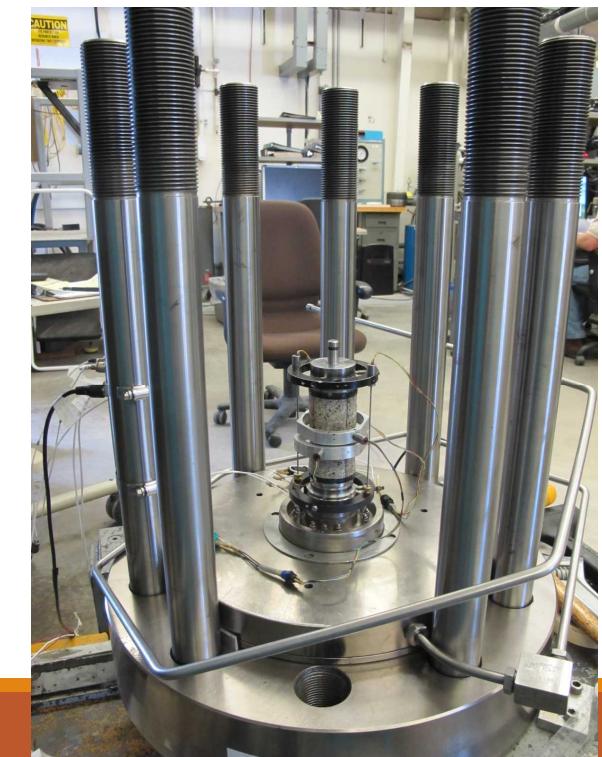
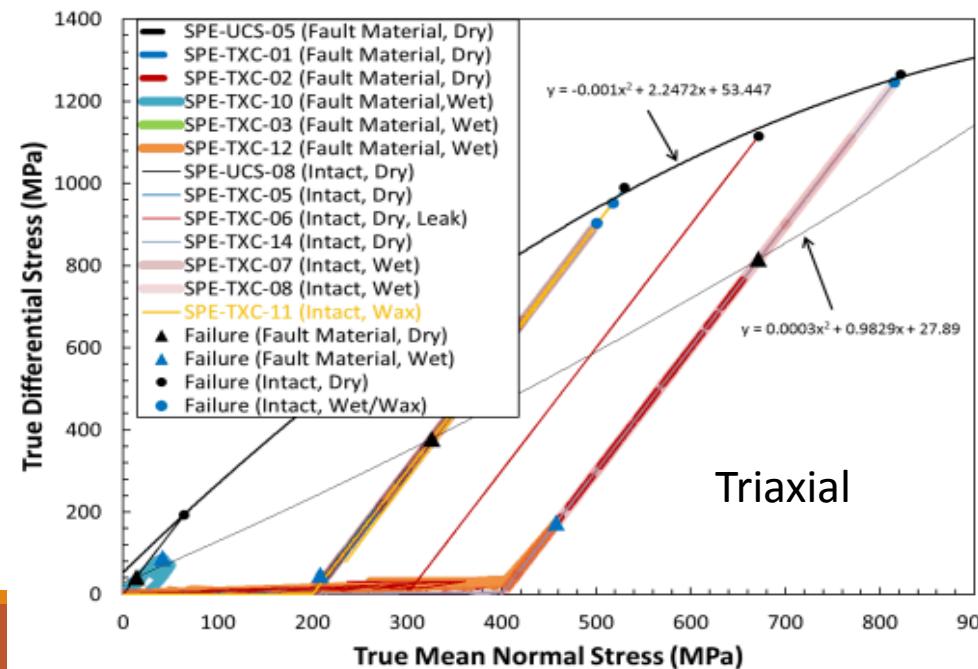
- Performed from source hole U-15n (pre SPE), U-15n#10 (post SPE2), U-15n#12 (post SPE3), U-15n#13 (post SPE3), and U-15n#27 (post SPE5)
- Used to compare to previous work on Climax Stock and understand rock strength variation between SPE events
- Hydrocode model development

## Uniaxial and Triaxial compression



## Triaxial

- Performed from source hole U-15n (pre SPE), U-15n#10 (post SPE2), and U-15n#27 (post SPE5)
- Used to establish failure envelope for intact and weathered (both wet and dry) materials
- Hydrocode model development



# Core Scale Material Property Analyses

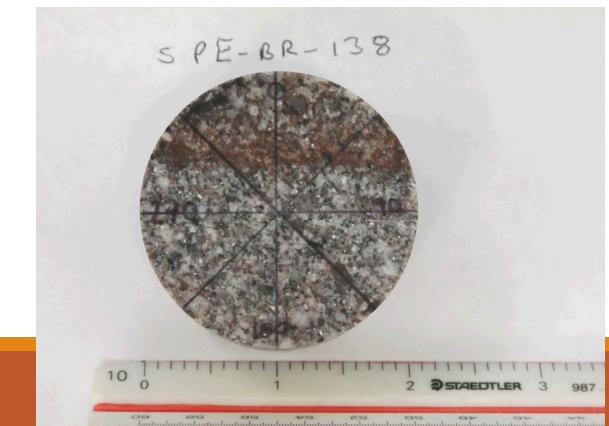
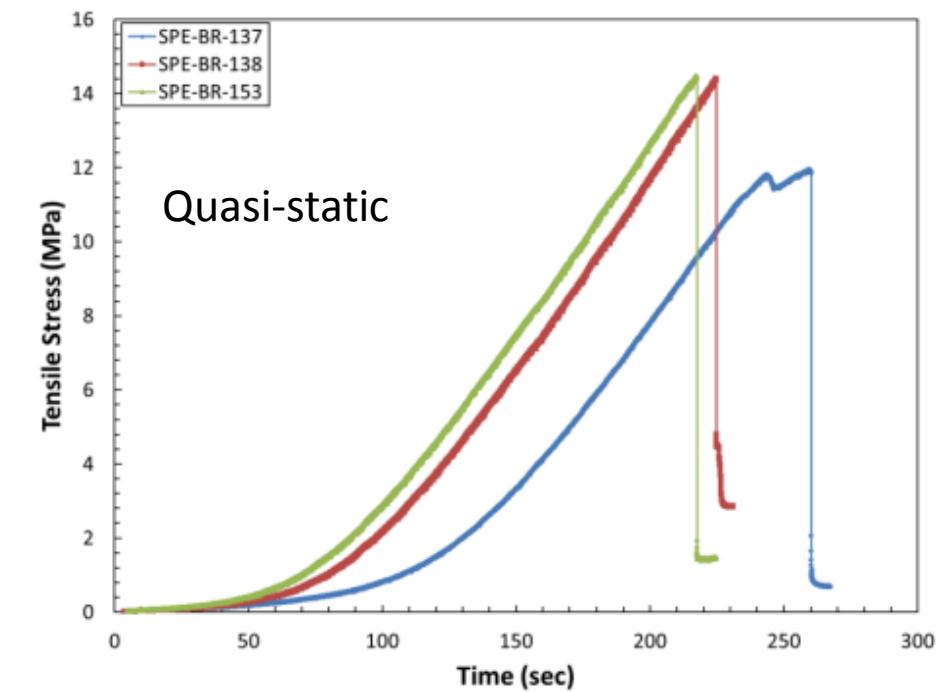
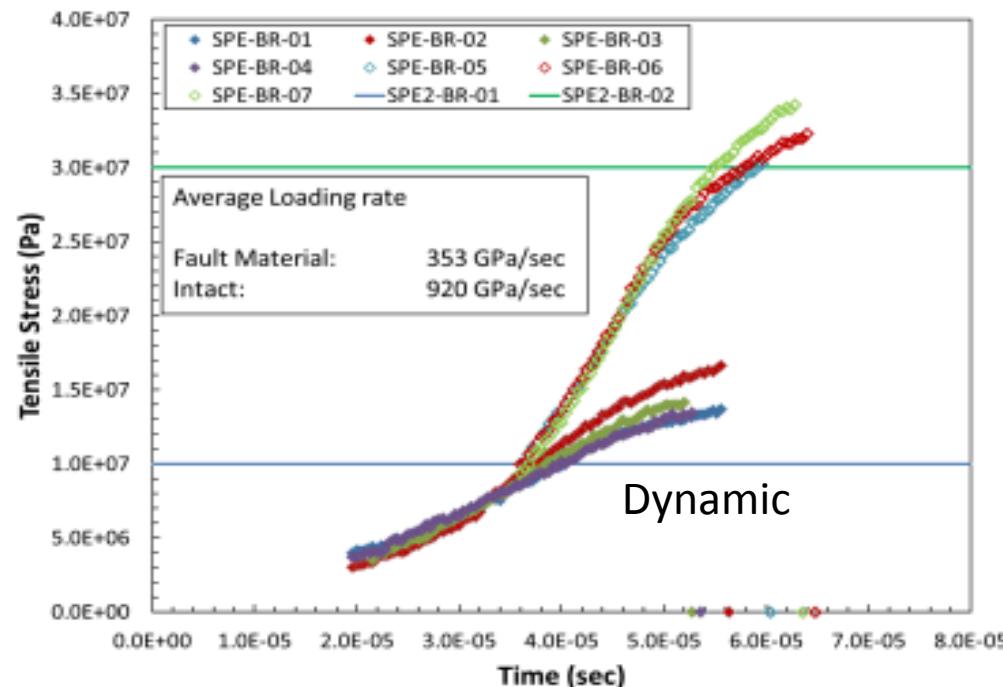
## Dynamic/Quasi-static Disc Tension

### Dynamic

- Performed from source hole U-15n (pre SPE) and U-15n#10 (post SPE2)
- Strain rate  $\sim 200/\text{second}$
- FDEM development

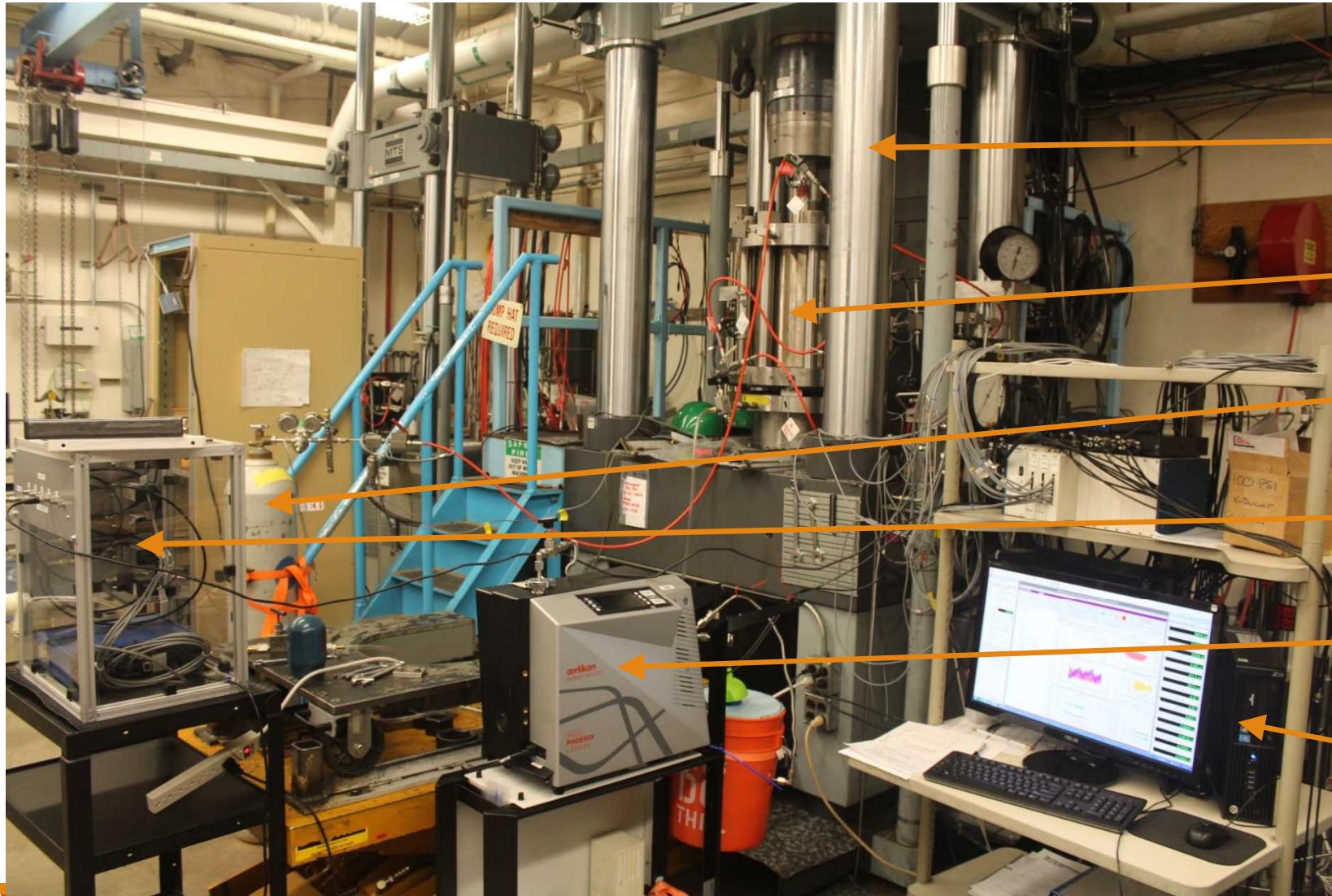
### Quasi-static

- Performed from source hole U-15n (pre SPE)
- Strain rate  $\sim 1\text{E-}4/\text{second}$
- FDEM development



# Core Scale Material Property Analyses

Triaxial compression to investigate permeability and damage relationship



Load frame

Pressure vessel

Upstream helium source

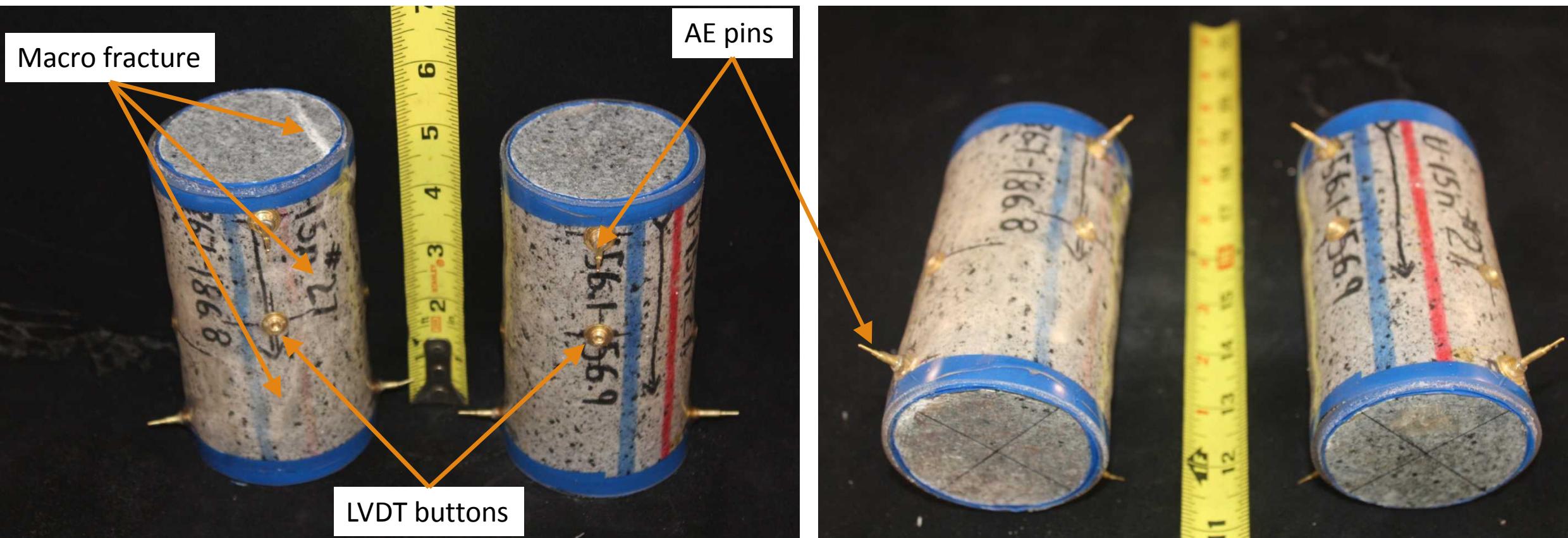
Flow bench

Helium leak detector

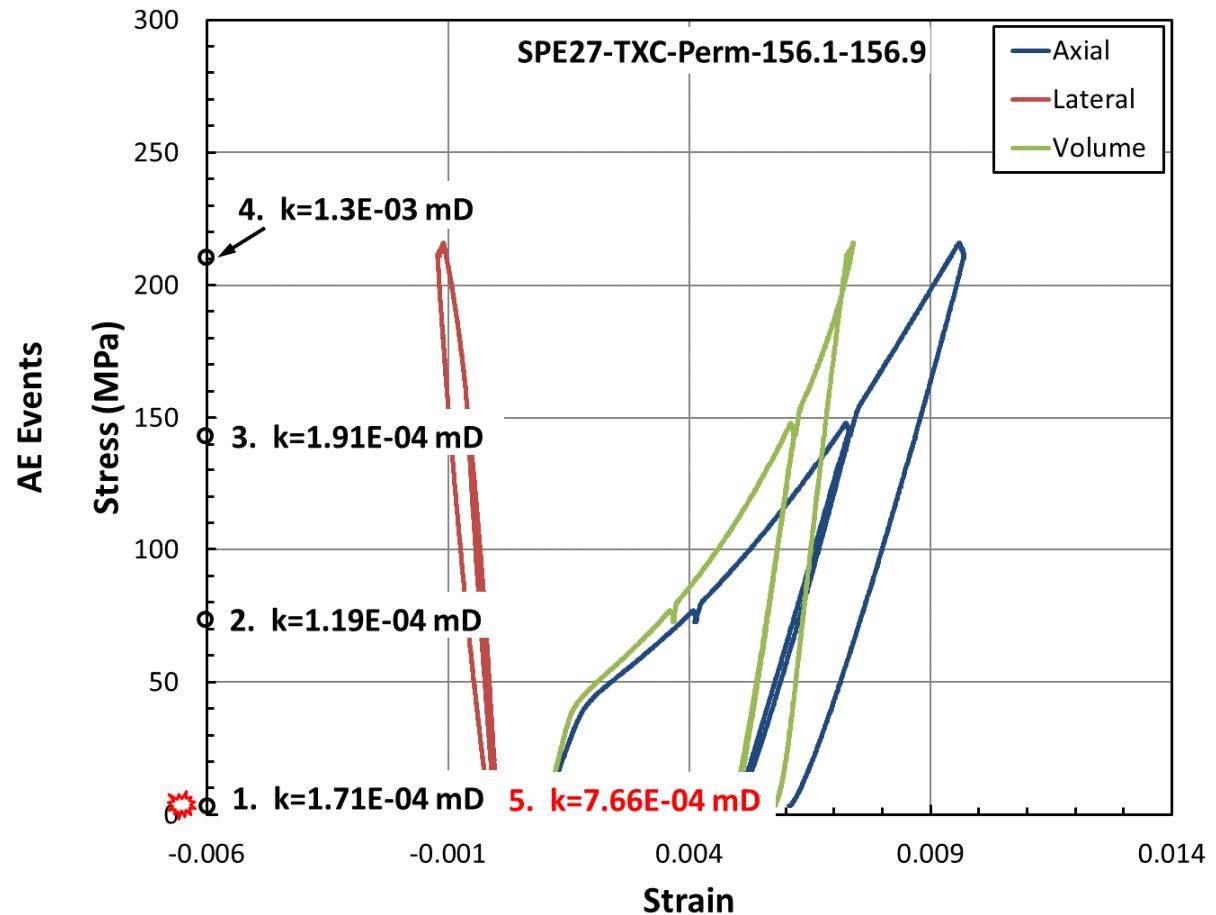
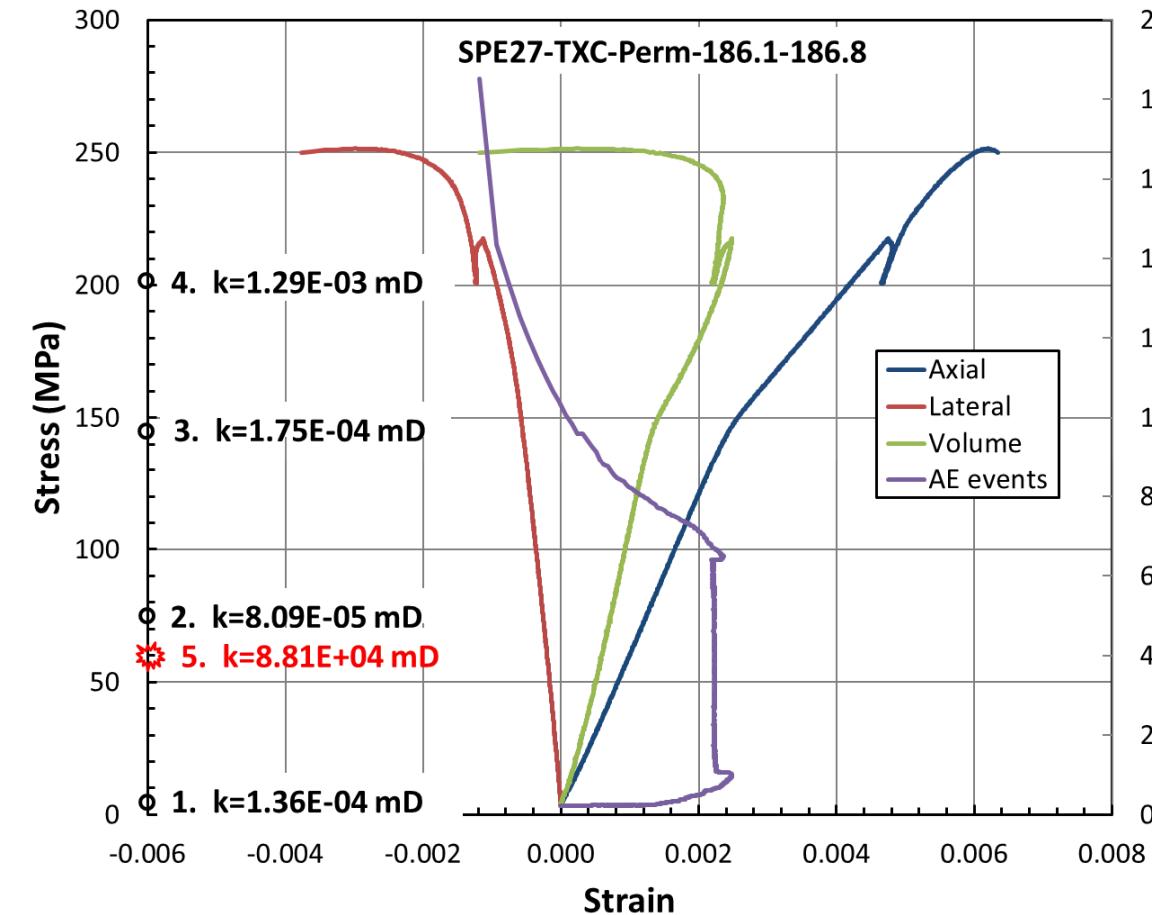
Data Acquisition System

# Core Scale Material Property Analyses

Triaxial compression to investigate permeability and damage relationship



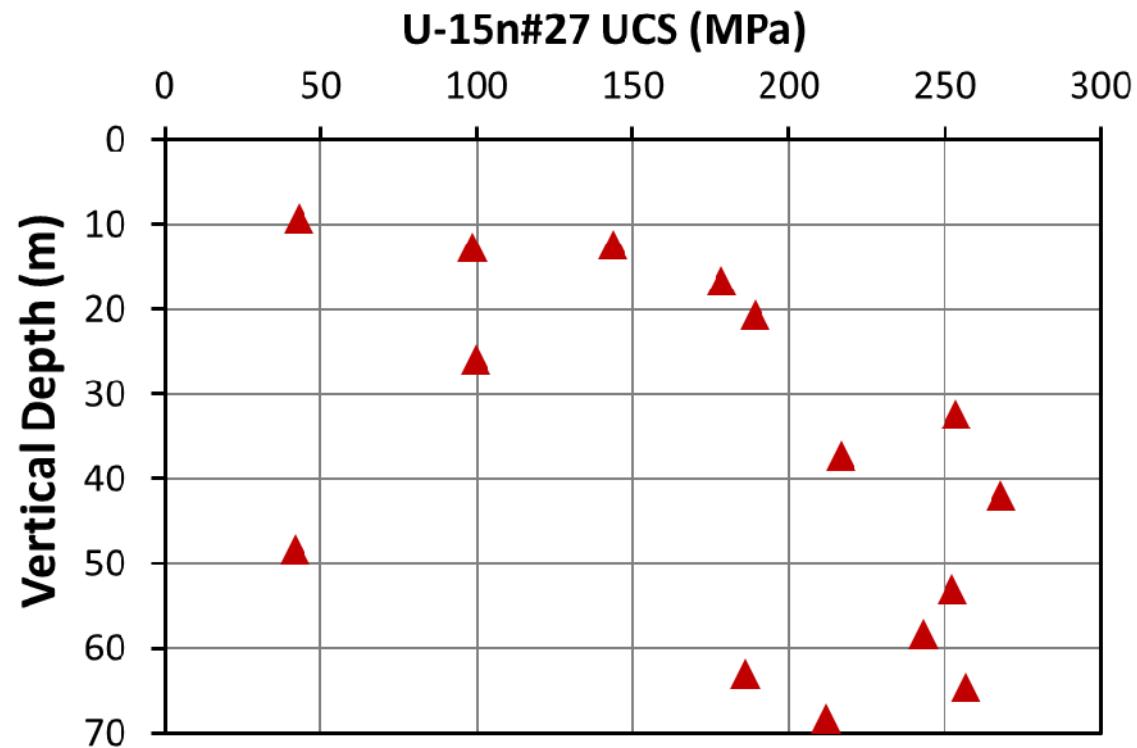
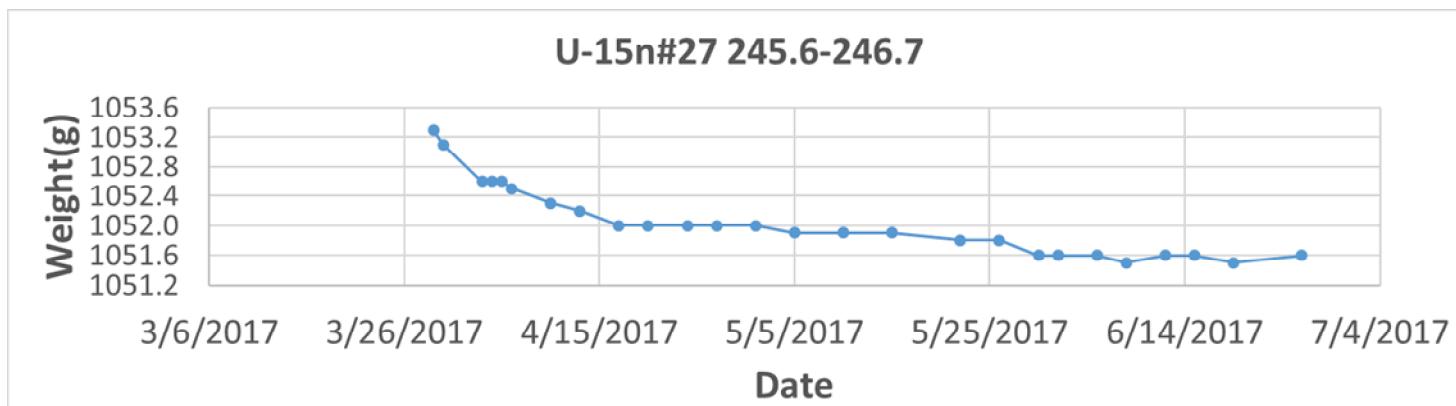
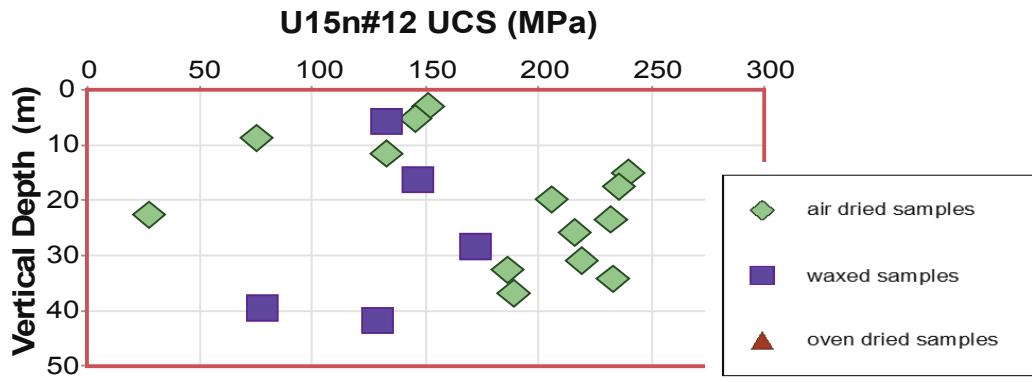
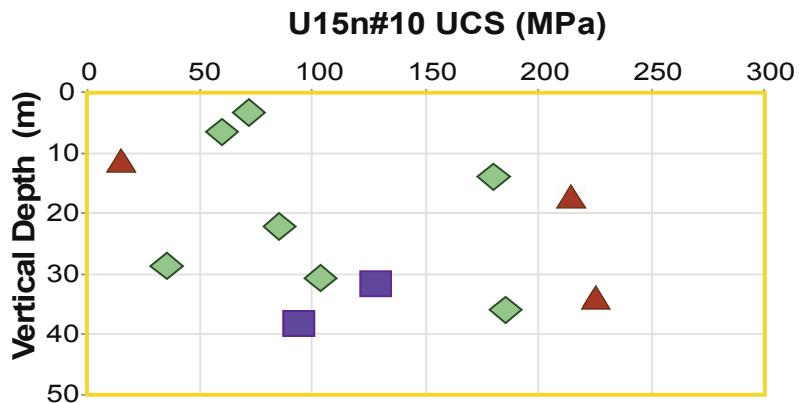
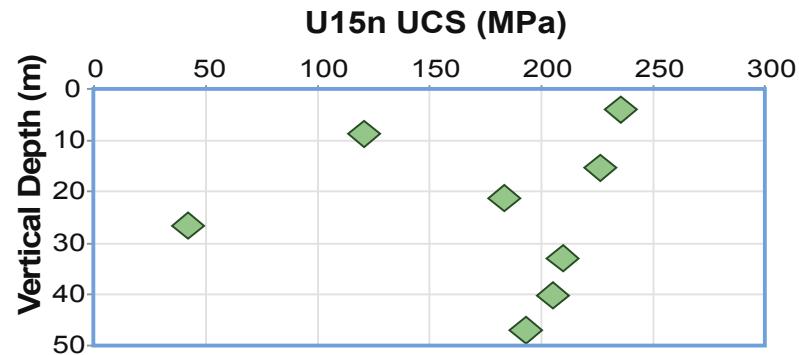
Samples each photo (Left) SPE27-TXC-Perm-186.1-186.8 and (Right) SPE27-TXC-Perm-156.1-156.9  
Buttons mount LVDT's to measure radial strain  
Pins record Acoustic Emissions



- Baseline permeability  $\sim 1E-04$  mD taken at 3.5 MPa hydrostatic pressure
- Permeability decreases at 75 MPa Axial Stress
- Permeability increases at 145 MPa (above hydrostatic baseline) and then again at 210 MPa Axial Stress (one order of magnitude above baseline)
- Sample SPE27-TXC-Perm-186.1-186.8 taken to failure. Post failure permeability is seven orders of magnitude above previous measured permeability
- Sample SPE27-TXC-Perm-156.1-156.9 unloaded after Axial Stress of 210 MPa. Hydrostatic permeability now half an order of magnitude greater than undamaged hydrostatic permeability

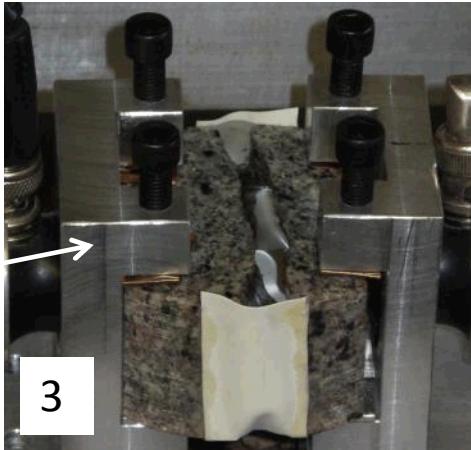
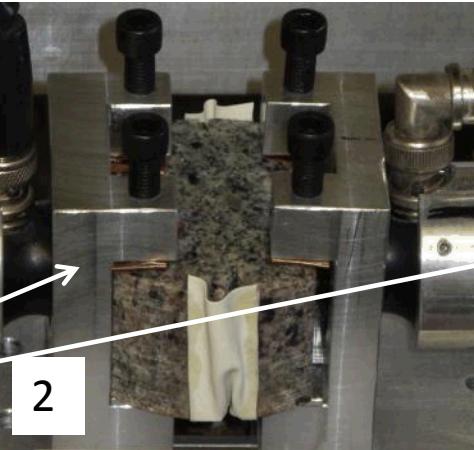
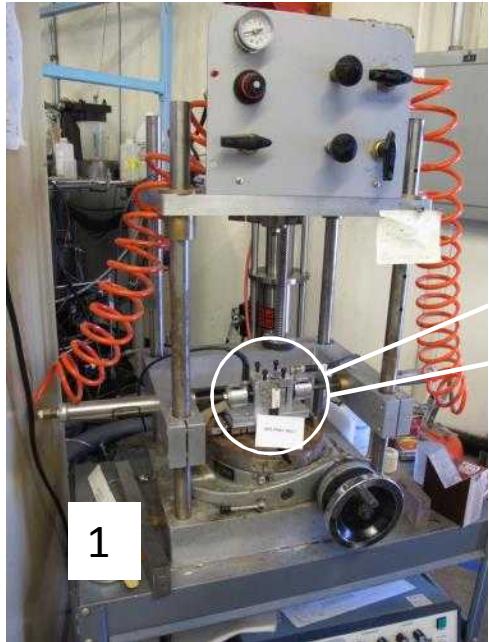
# Core Scale Material Property Analyses

Unconfined compressive strength varies with water content



# Core Scale Fracture Property Analyses

## P&S velocity as a function of fracture aperture with water as coupling medium

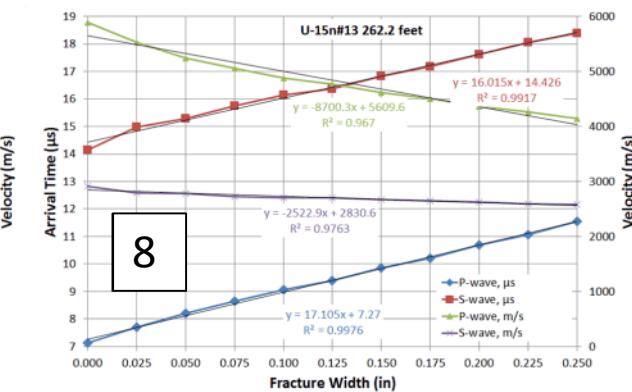
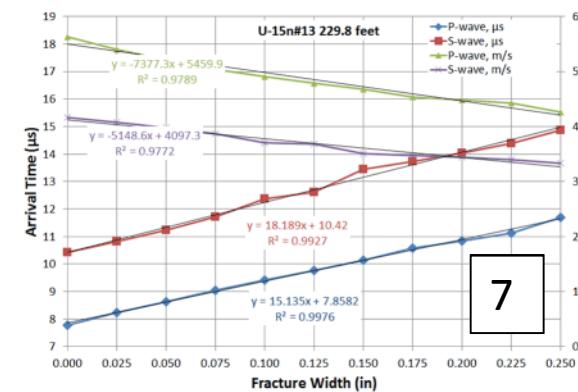
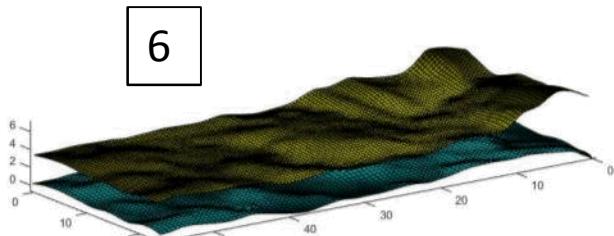


Water filled closed gap.

0.250" gap filled with water.

SPE-FRAC-262.2

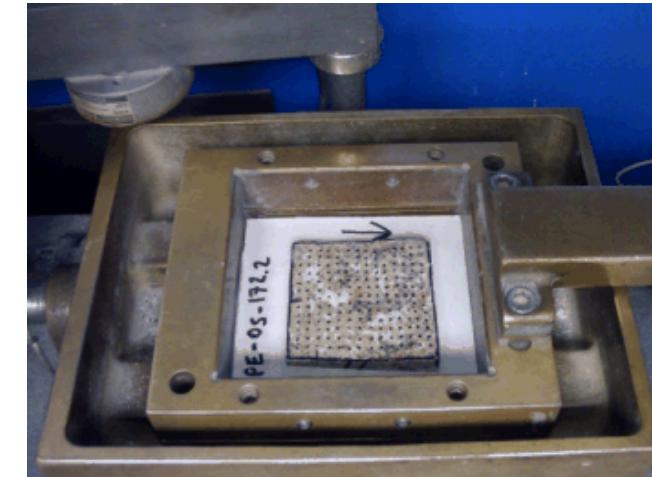
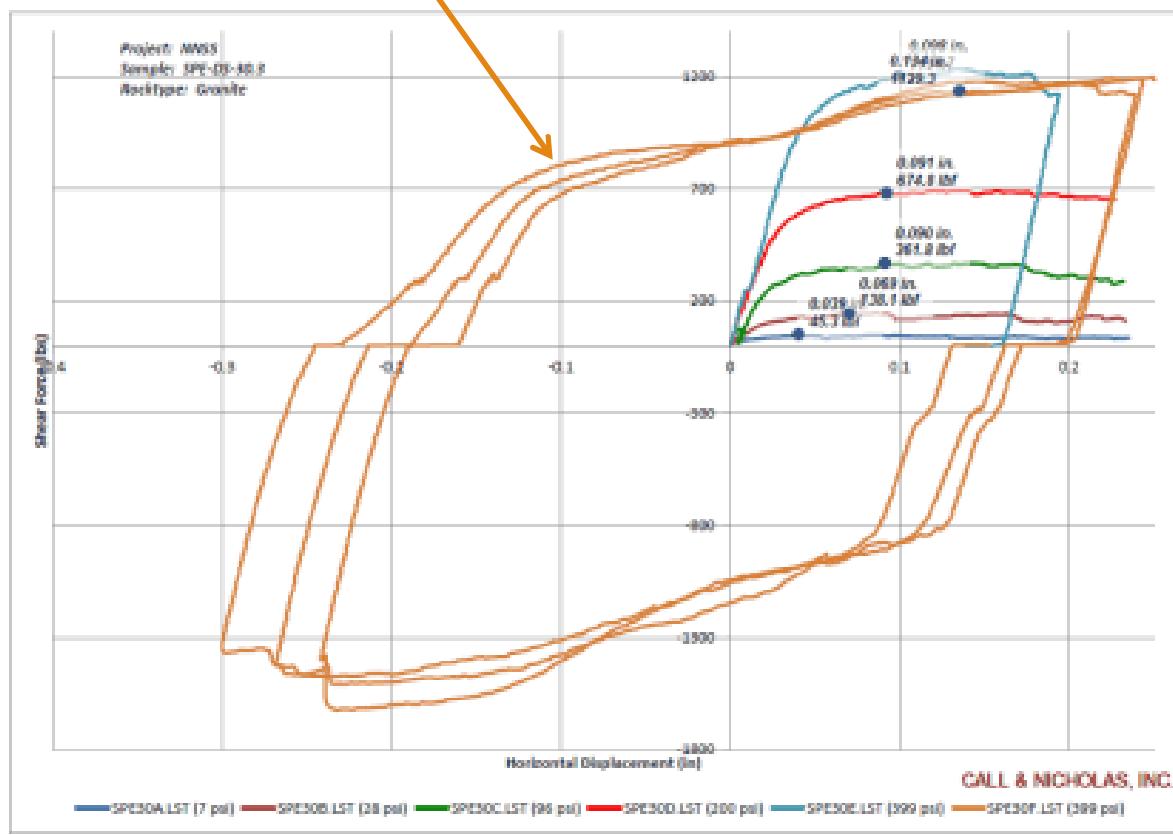
SPE-FRAC-262.2



# Core Scale Fracture Property Analyses

## Direct Shear on Natural Fractures

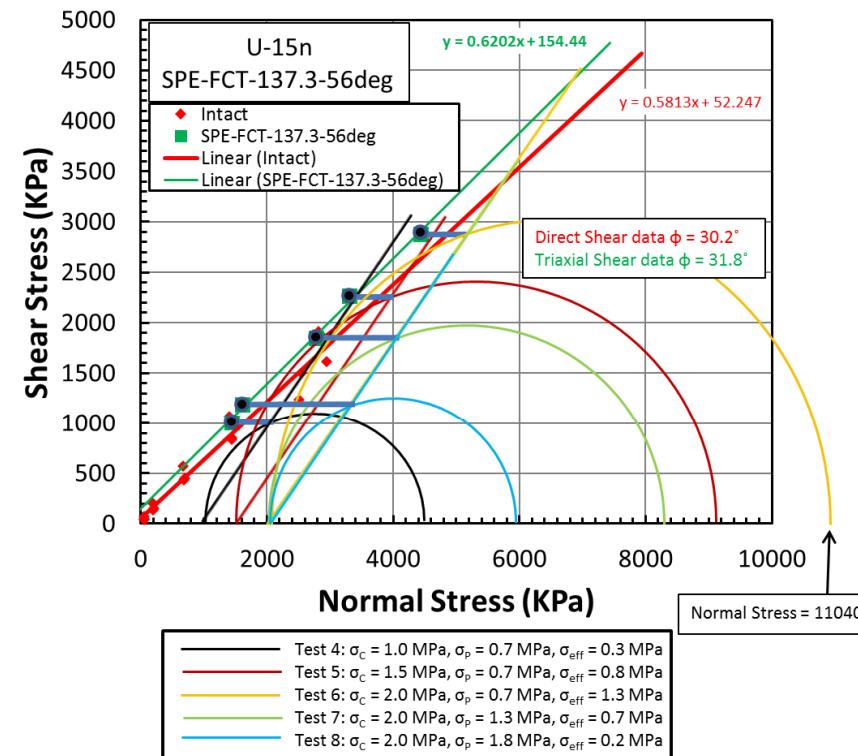
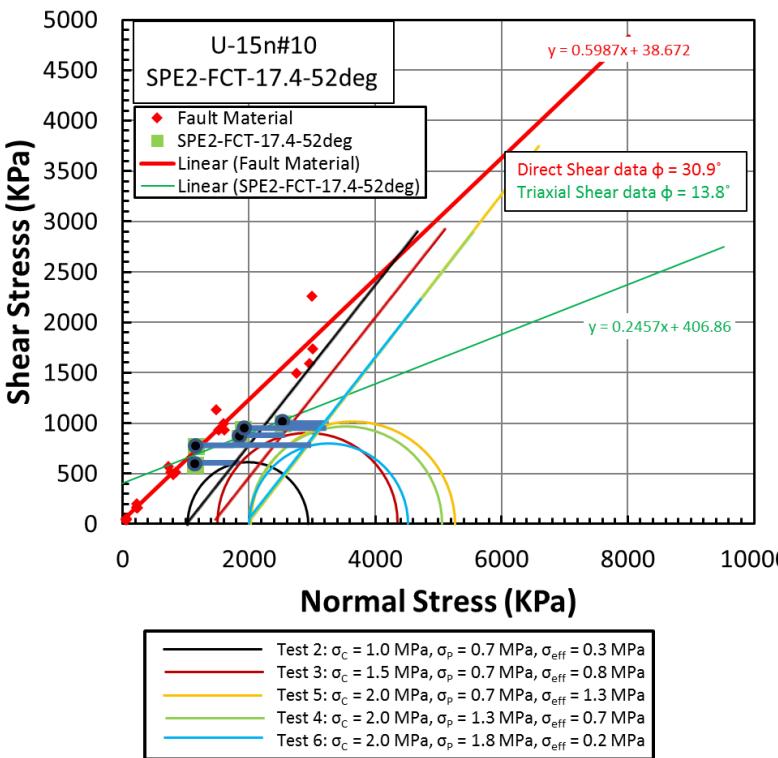
- Core from source hole U-15n (pre SPE) and U-15n#10 (post SPE2)
- Determine Friction angle and cohesion of natural fractures
- Dry and saturated testing conditions
- Repetitive shearing performed



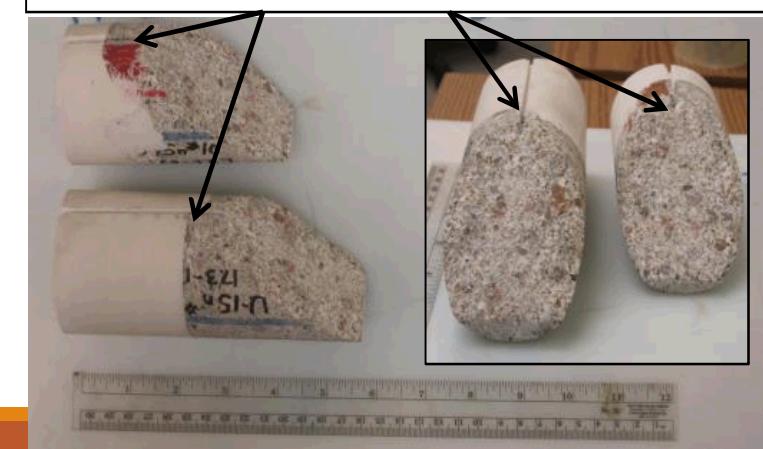
# Core Scale Fracture Property Analyses

## Triaxial Shear on Natural Fractures

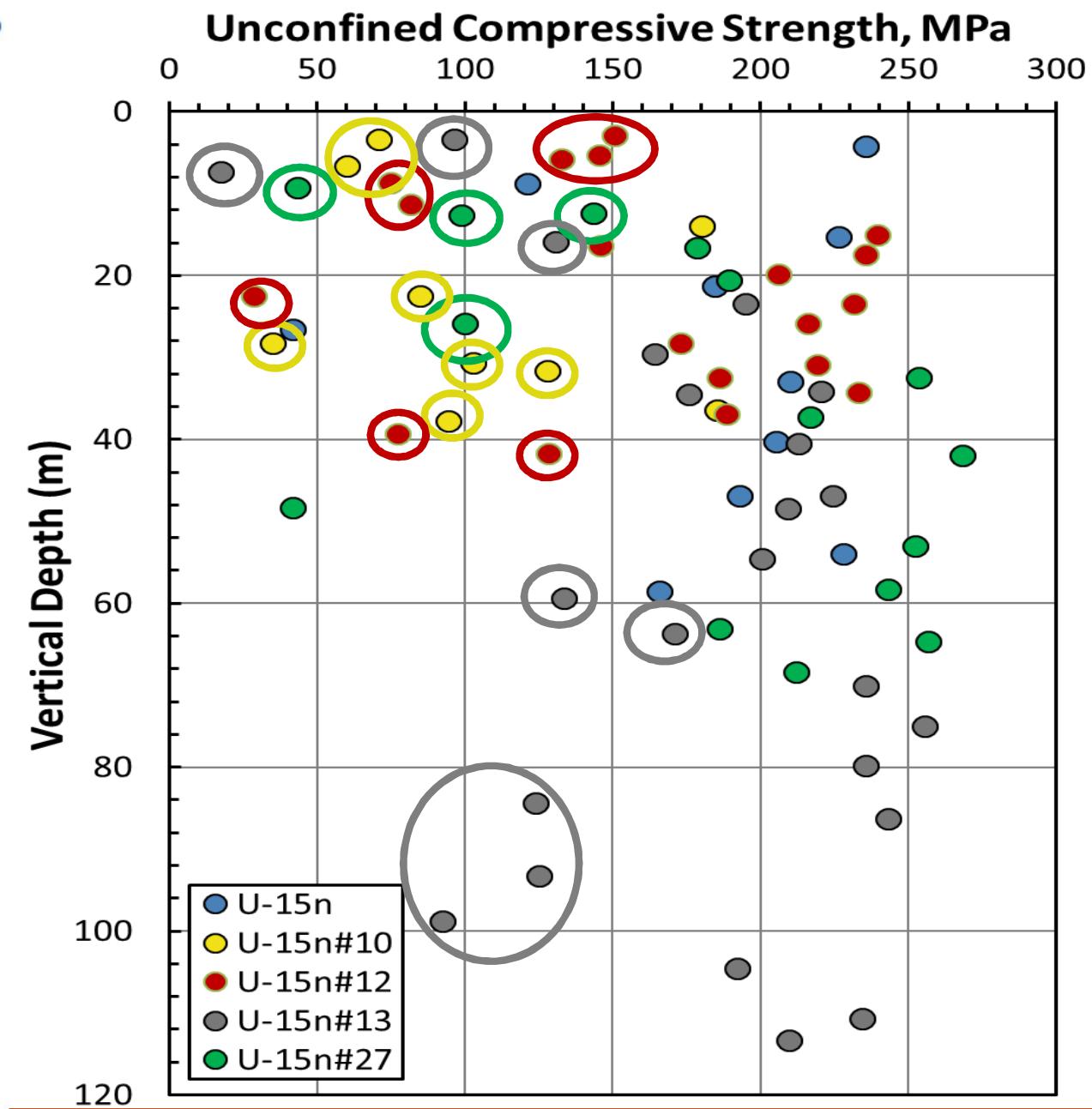
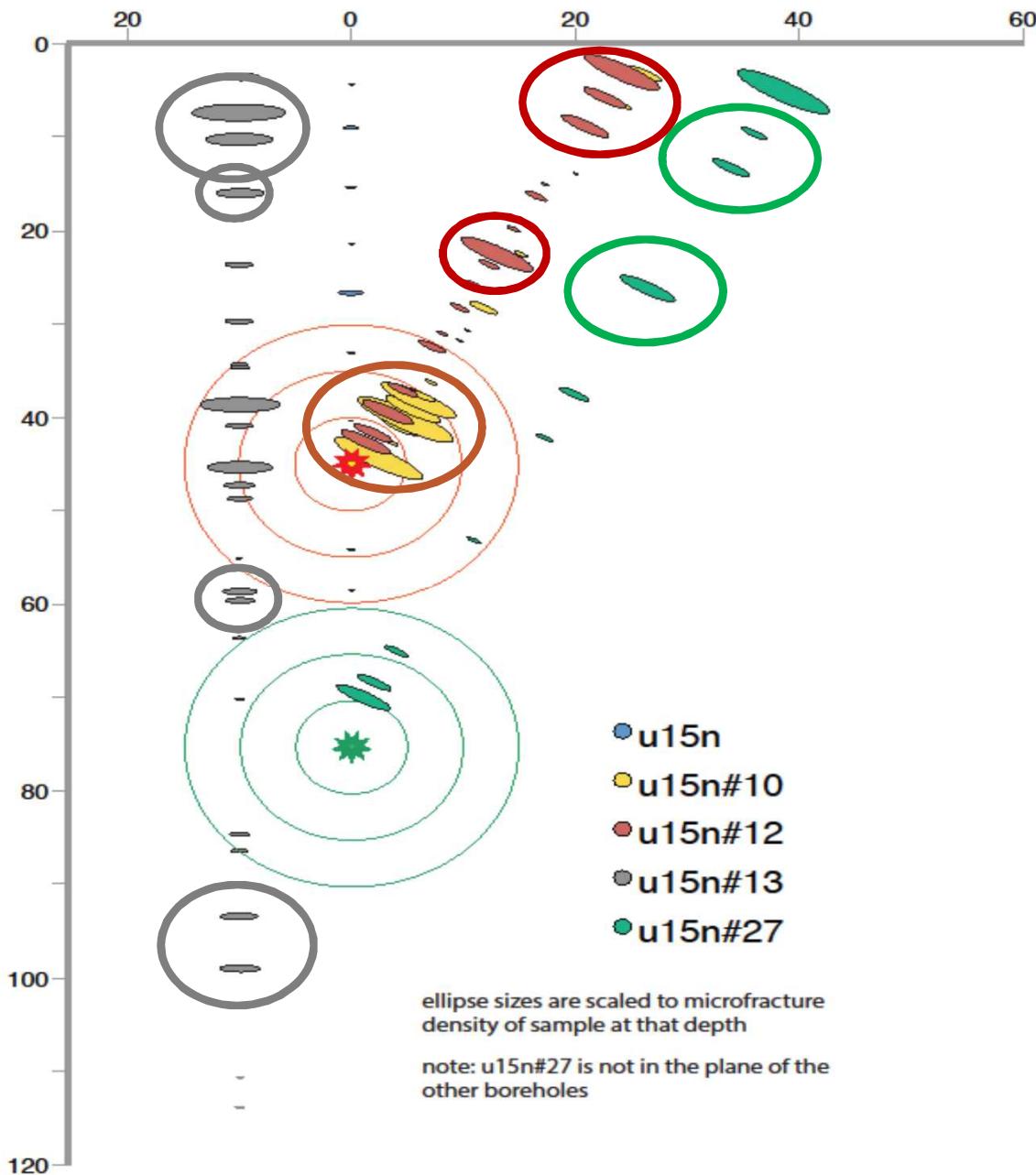
- Core from source hole U-15n (pre SPE) and U-15n#10 (post SPE2)
- Determine Friction angle and cohesion
- Incorporate fracture surface fluid pressure and confining pressure
- Characterization of wet weathered material possible



Grooves cut in rock to facilitate transmission of pore fluid to natural fracture surface.

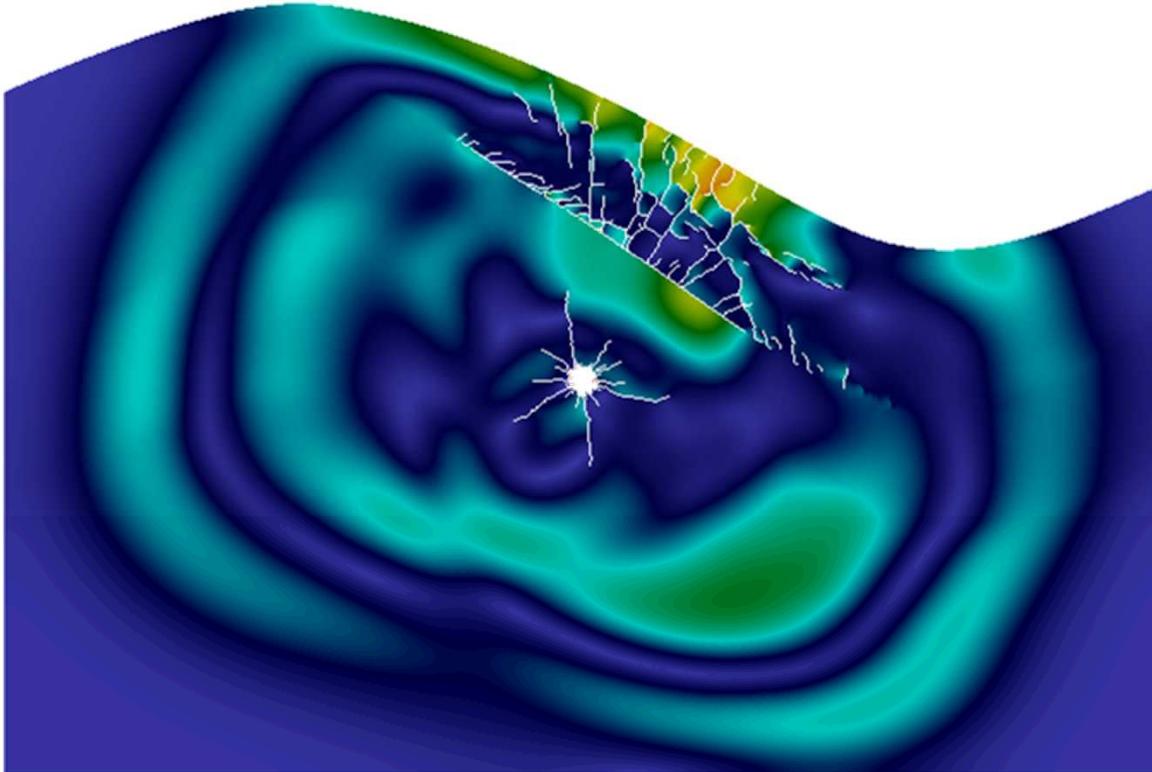


# Linking Micro to Core Scale Material Properties

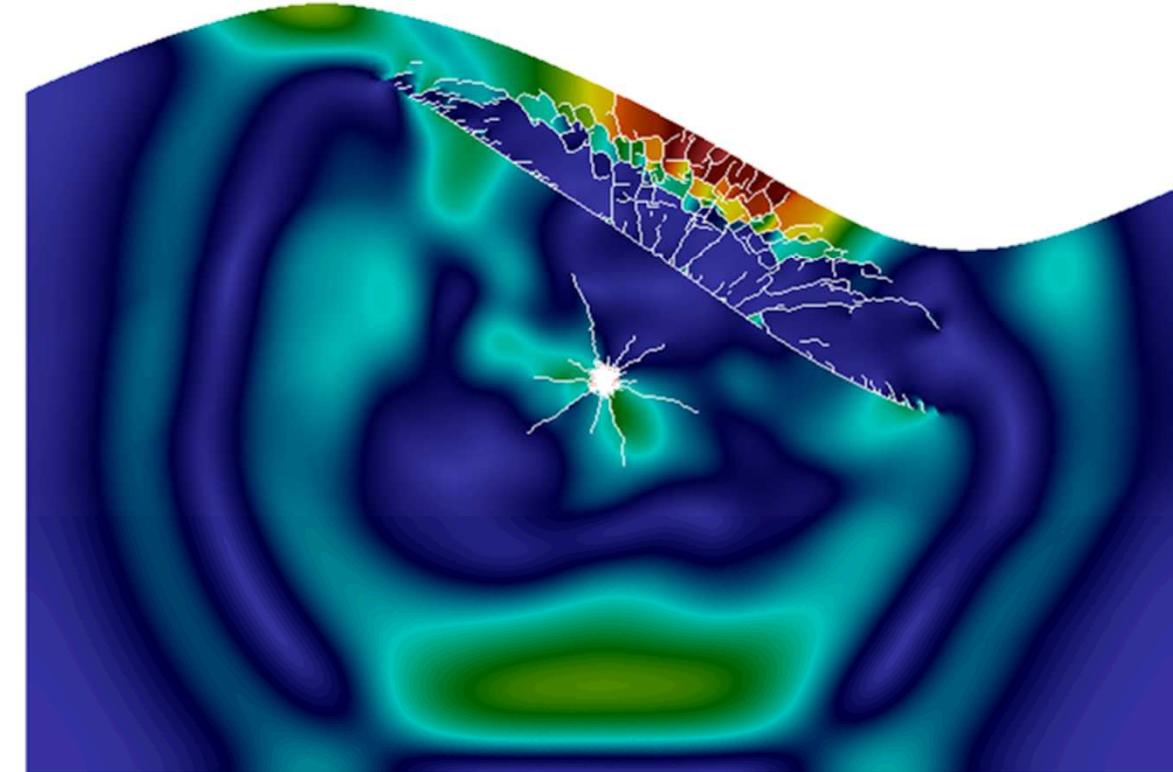


# Micro-scale Material and Fracture Property Analyses

Optical microscopy data incorporated into models

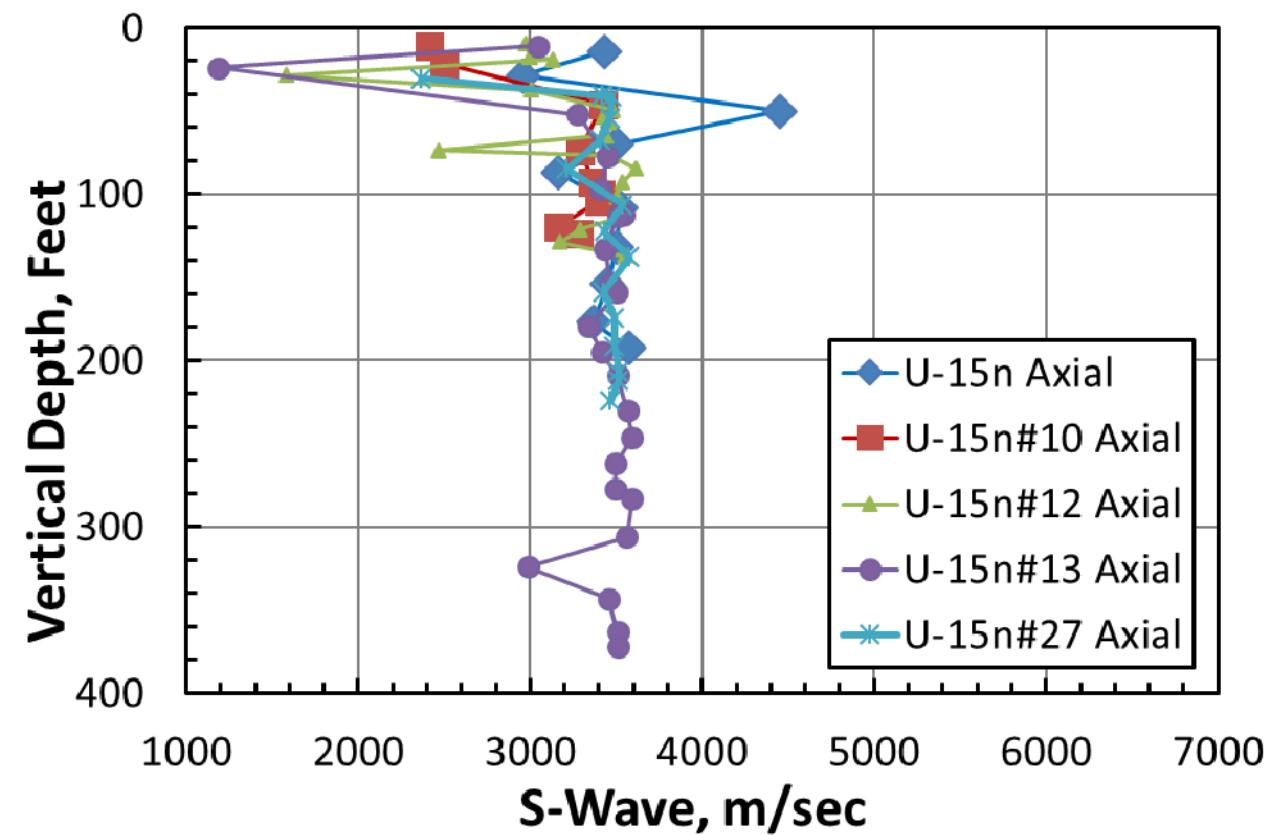
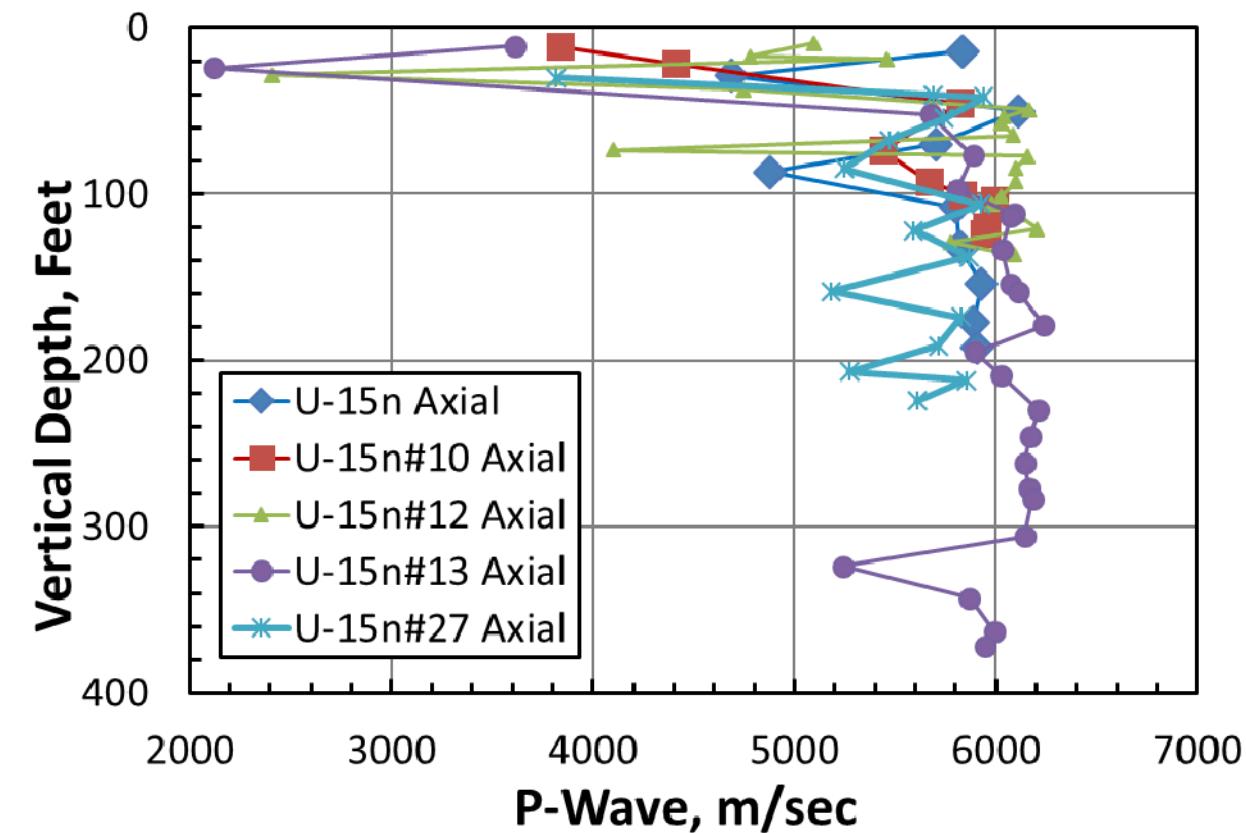


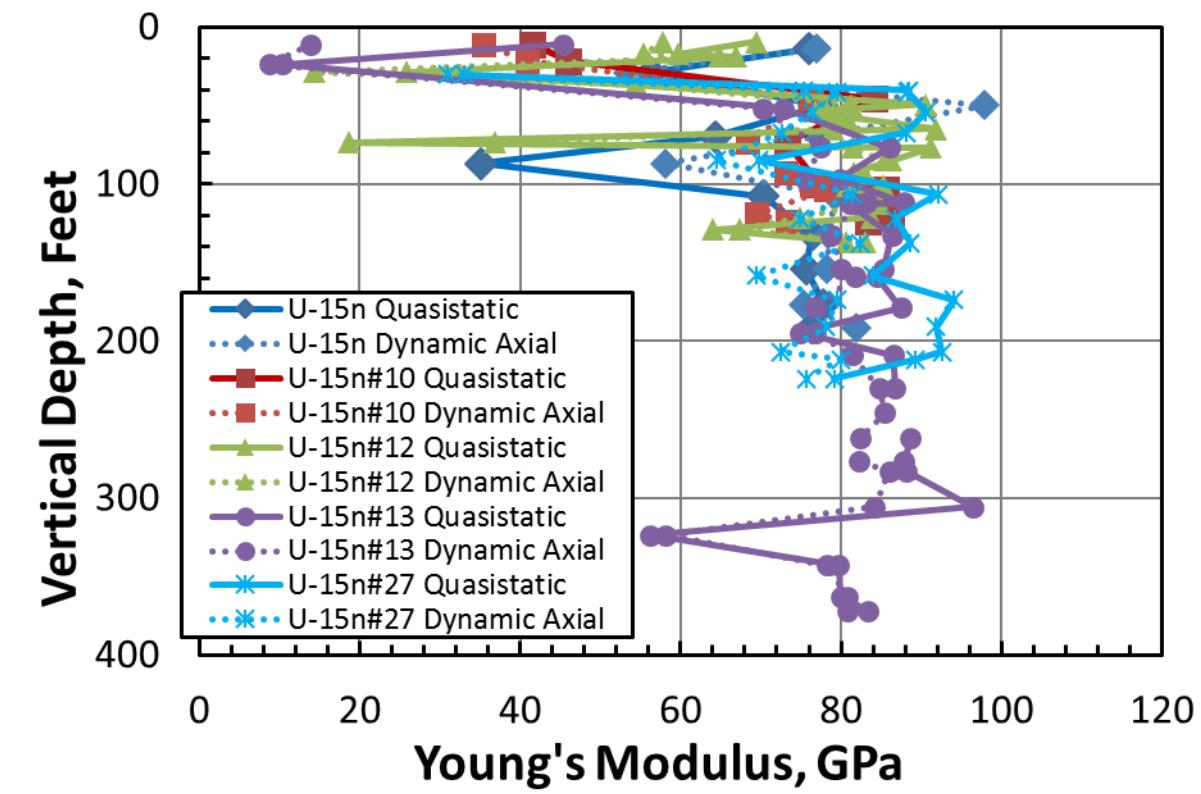
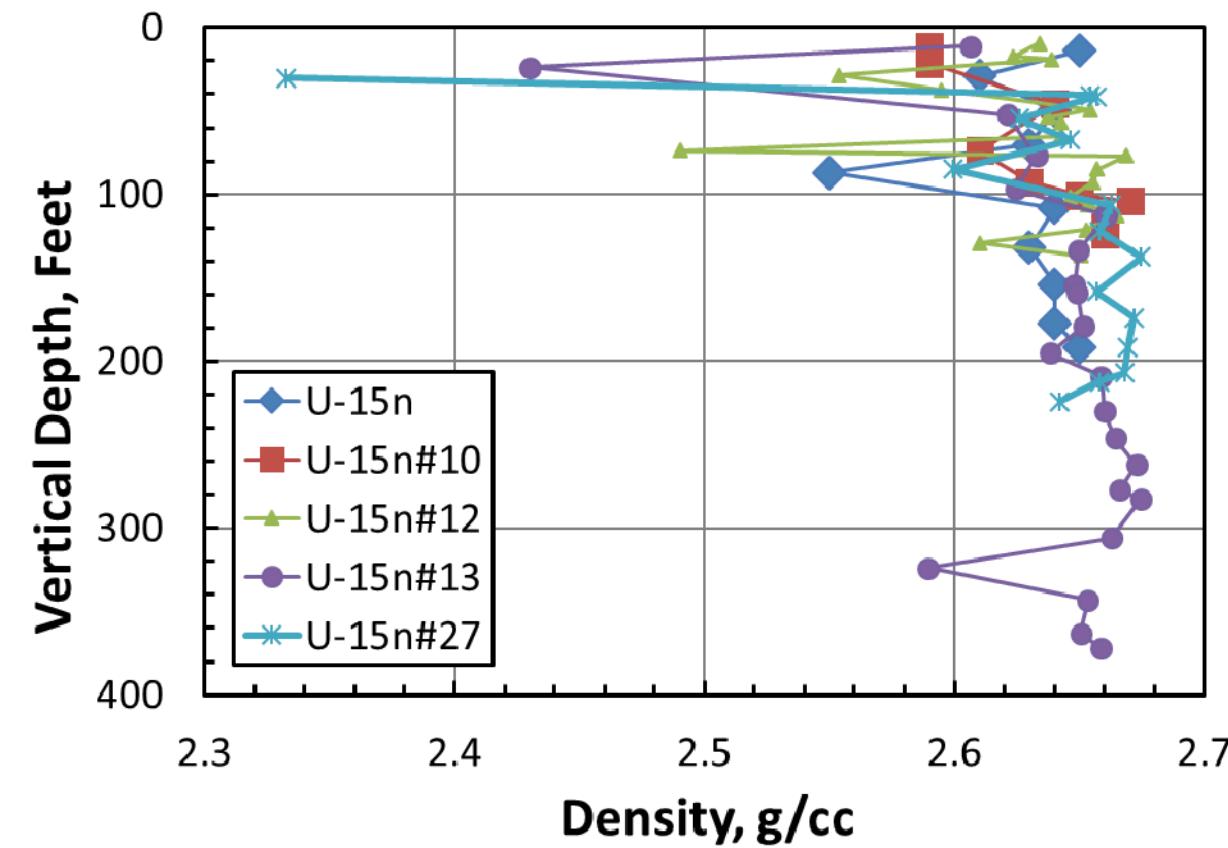
Anisotropic Medium

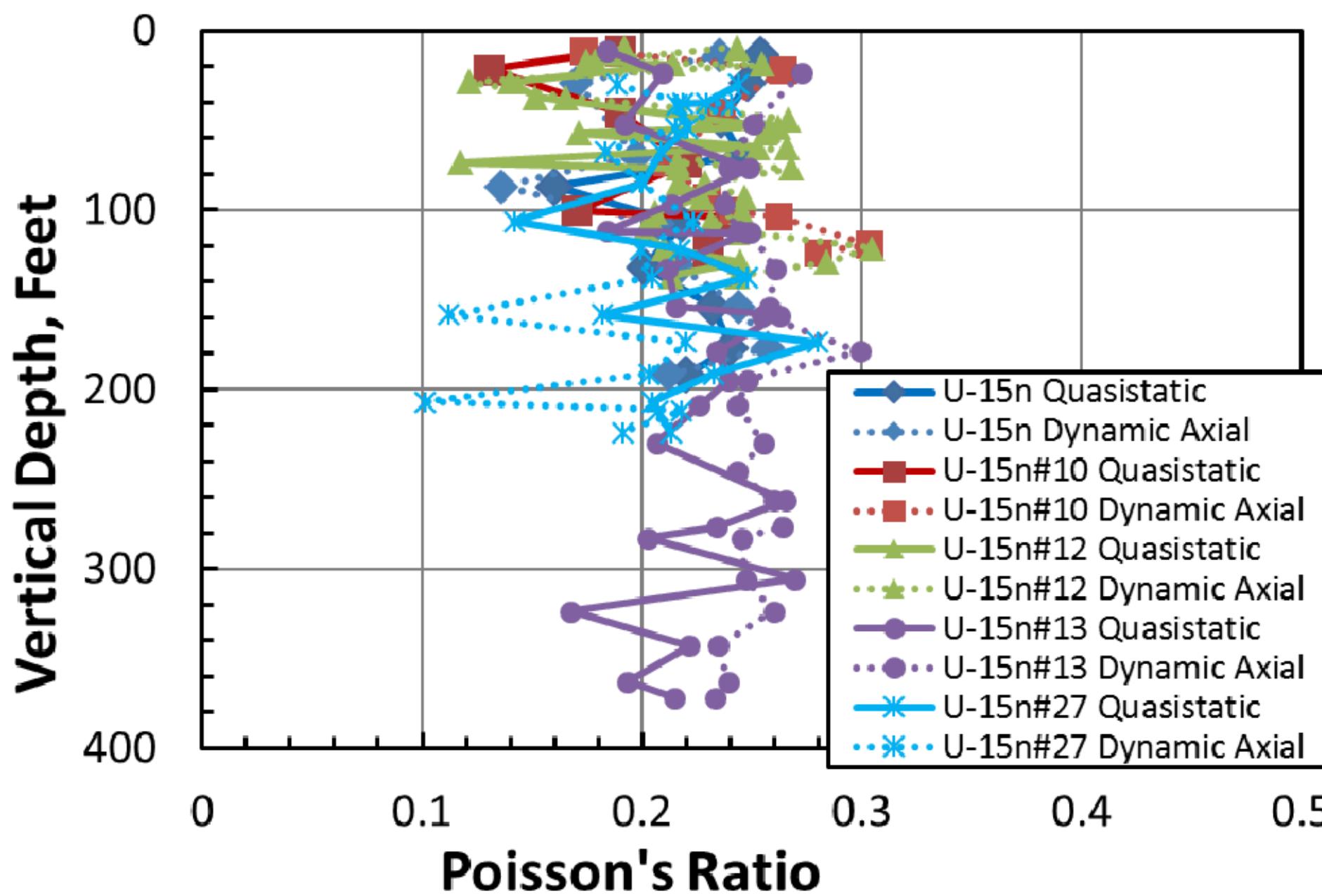


Isotropic Medium

# Backup slides







# Normalized SPE Phase 1 Material Properties

