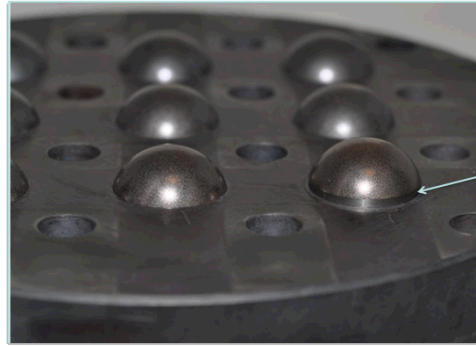


Advanced Percussive Drilling Technology for Geothermal Exploration and Development



Advanced Percussive Drilling Technology for Geothermal Exploration and Development

Giann Su, David Raymond, Somuri Prasad

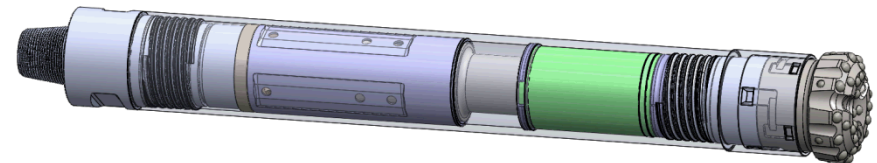
Sandia National Laboratories

Dale Wolfer

Atlas Copco Secoroc

Atlas Copco Partnership

- Headquartered in Stockholm, Sweden
- Industrial group with products and services for mining and construction
 - Compressed air and gas equipment
 - Industrial tools and assembly systems
 - Down the hole hammers suited for geothermal environments
- Production facilities in more than 20 countries
- \$~12 B revenue in 2016
- Prior SNL DARPA work showed promise for hammers in harsh environments
 - Efficient at drilling hard rock
 - Very durable
 - Low weight on bit and torque requirements
- Current work result of competitive bid process for DOE Funding Opportunity Announcement
 - Funded separately by DOE
 - Atlas Copco has cost share
- Established a broader CRADA including others at Sandia
- Synergy between other Sandia work and Atlas Copco needs

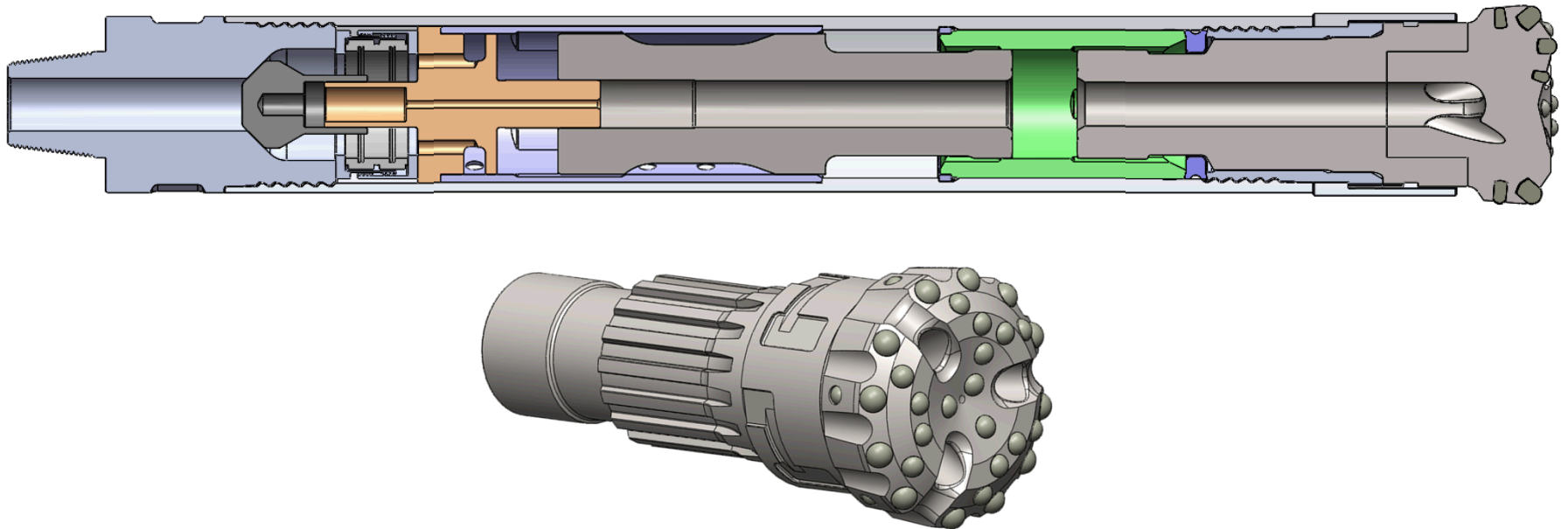


Project Objectives

- To construct the conceptual definition of a High Temperature (HT) pneumatic percussive hammer.
- Identification, testing, evaluation and qualification of constituent materials for this hammer.
- Perform computational modeling of the available power delivery of conceptual designs.
- Provide Proof-of-Concept (POC) validation via laboratory testing of representative design features.
- Implement prototype hardware development of a high temperature pneumatic percussive hammer.
- Conduct laboratory drilling tests to validate performance of prototype hardware at conventional temperatures.
- Perform laboratory drilling tests to validate performance in a high temperature test cell simulating a geothermal drilling environment.

Proof of Concept Hammer

- Valveless cycle
- No polymeric or elastomeric parts or seals
- No fluid lubrication
- Performance comparable to current commercial DTHH

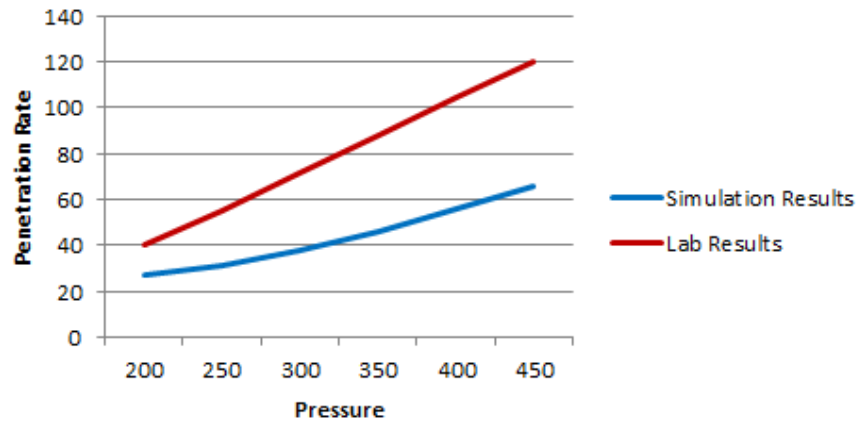


Scientific/Technical Approach

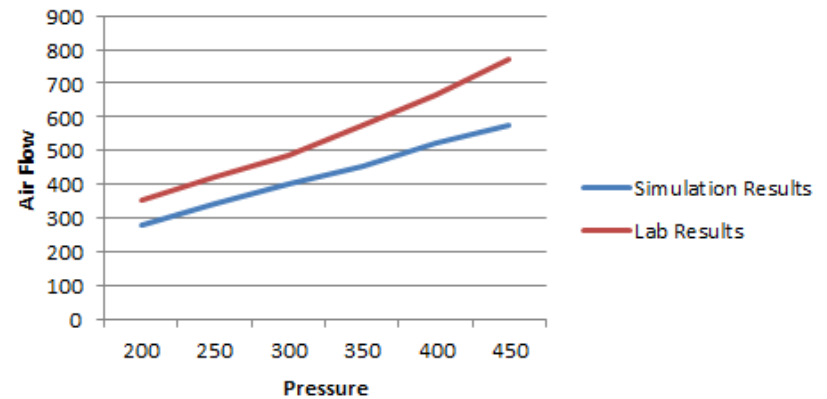
- Phase 1: Proof of Concept
 - Requirements definition for operating conditions
 - Thermodynamic cycle computational modeling of proposed DTH cycles
 - Finite Element Analysis (FEA) of structural components and systems
 - Systems solution and configuration definition
 - HT percussive hammer design, analysis and evaluation
 - Materials selection, qualification and testing along with review of technical literature for identification of potential materials and/or processes
 - Coupon level environmental coatings and bulk property testing
- Phase 2: Component and System Level Testing
 - Establish baseline prototype hammer performance at the Atlas Copco Roanoke test facility
 - Provide Proof-of-Concept (POC) validation via laboratory testing of representative design features.
 - Build full-scale prototype hammers based on design and material selection from Phase 1
 - Test and characterize prototype hammers under ambient conditions at the Atlas Copco Roanoke test facility
 - Design, build and test high-temperature test facility
 - Validate performance of prototype HT hammer at temperatures up to 572 F on the high-temperature facility

Simulation vs Prototype Results

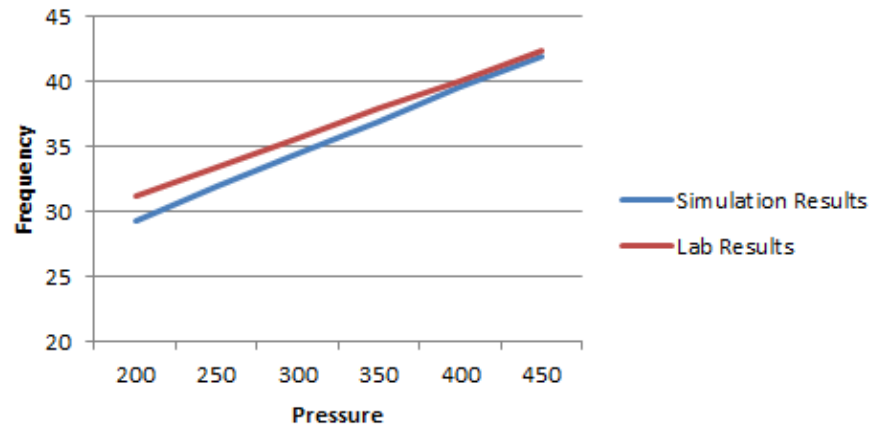
Penetration Rate (ROP)



Air Flow



Frequency

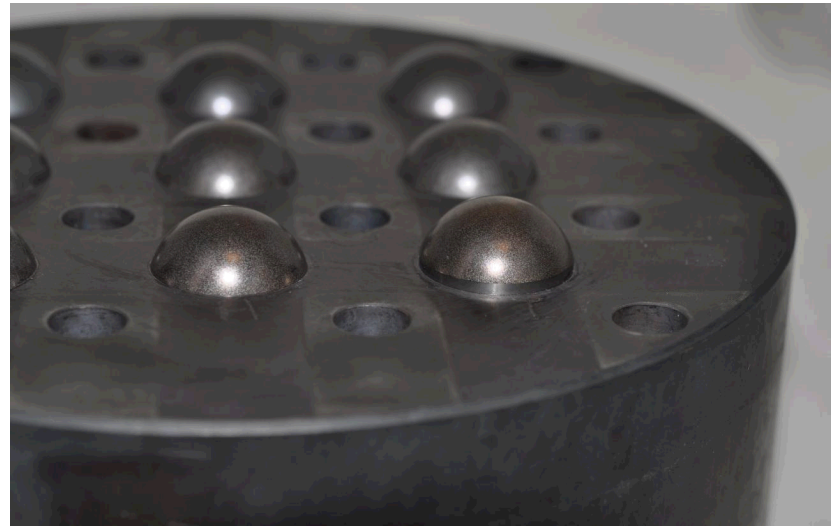


Internal Sealing

- Initial testing showed internal leakage between the Air Distributor and Cylinder dramatically limited hammer performance
- Low temperature testing using a conventional Buna –N o-ring showed that effective sealing would correct the problem
- Alternatives for High Temperature sealing
 - Interference fit
 - Permanent joining of Air Distributor and Cylinder
 - High temperature, graphite filled valve packing seal
 - High temperature elastomer
- Evaluated valve packing and Kalrez o-ring
 - Valve packing provided fair sealing performance, more development is necessary
 - Kalrez o-ring is a drop in replacement for standard elastomers and is fully capable of performing satisfactory in the target environment (Max. temperature rating 327 C)

Button Retention Testing

- Impact testing up to 12,000 g
- Varying interference fits to simulate button hole expansion due to temperature
- Two buttons with the least interference began shifting at 10,000 g
- All other buttons remained in place up to 12,000 g
- Conclusion: current interference fit is suitable to retain buttons in a bit, up to 600 F



Material Selection

- Focus on Casing, Air Distributor, Piston, Bearing
 - Conventional parts are tempered below the target geothermal operating temperature
 - Fatigue resistance is a key property
 - Corrosion resistance is important
- Selection Process
 - Literature search to determine properties of current materials and identify candidate materials with good physical properties at 300 C
 - Qualification testing of candidate material, including
 - Tensile strength
 - Charpy impact toughness
 - Fatigue
 - Abrasion resistance
 - Friction and wear characteristics
- Results
 - No candidate material showed better properties than the existing casing material. Surface hardening will be omitted from part specifications
 - A precipitation hardening stainless steel was selected for the piston
 - A hot working tool steel was selected for the Air Distributor and Bit Bearing

Lubricious and Wear Resistant Coatings

■ Thermal Spray Coatings

- Four (4) commercially available coatings tested
- Testing Conducted:
 - Hardness
 - Abrasive wear
 - Friction
 - Tensile adhesion of coating
 - Impact fatigue resistance

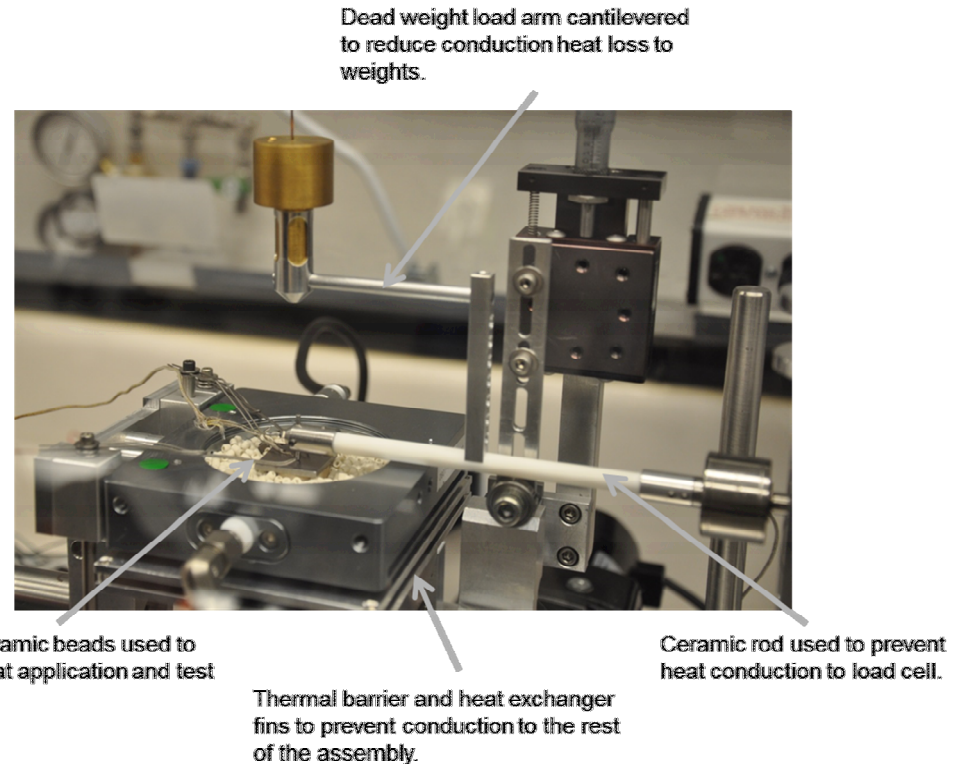
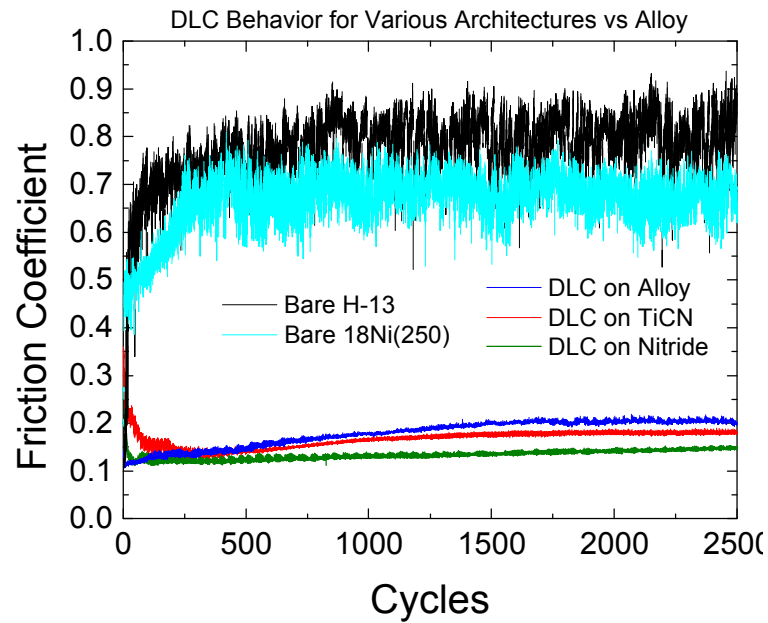


■ Vapor Deposition Coatings

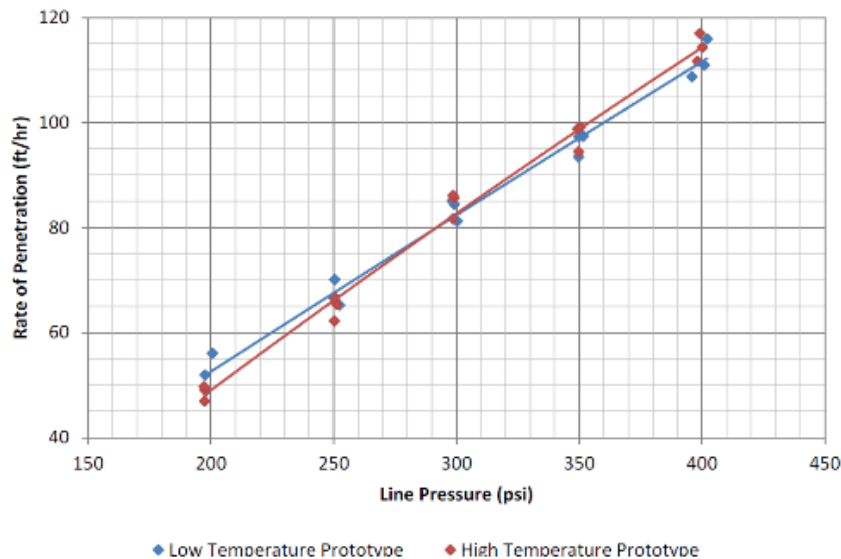
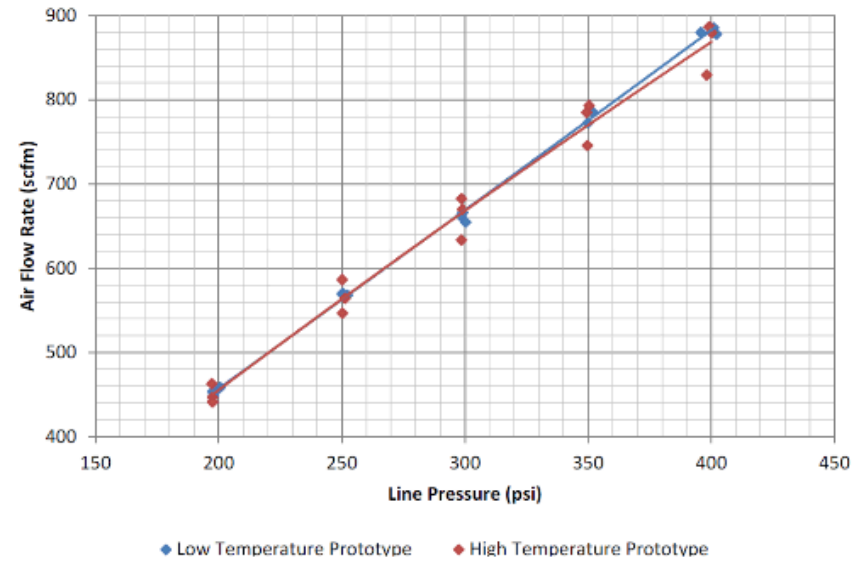
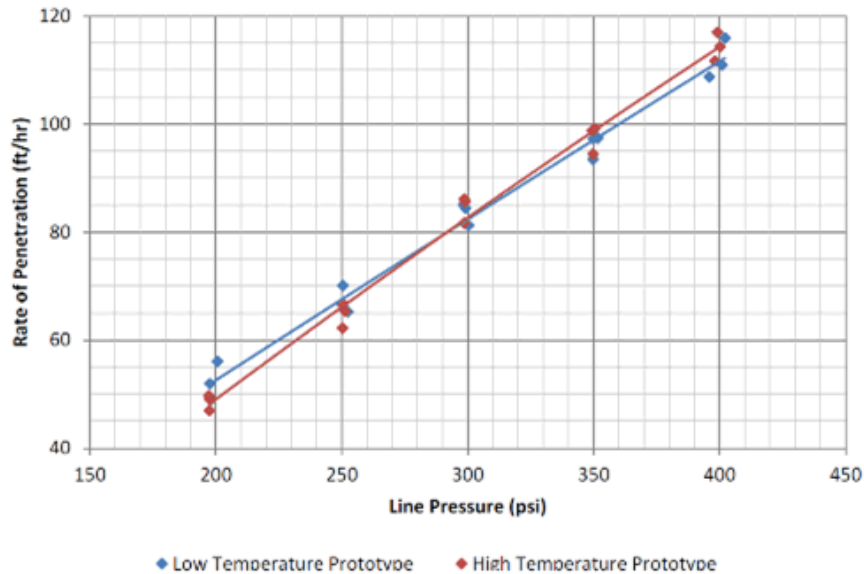
- Two (2) candidate coatings evaluated
 - Diamond-like carbon (DLC) with ceramic barrier level
 - DLC with multiple barrier layers (nanolaminate and ceramic barrier layer)
- Tested for friction and wear properties at 300 C
 - Multiple layer sample developed cracks and delaminated
 - DLC with single barrier layer showed good friction resistance and no delamination



Coatings Friction and Wear Testing



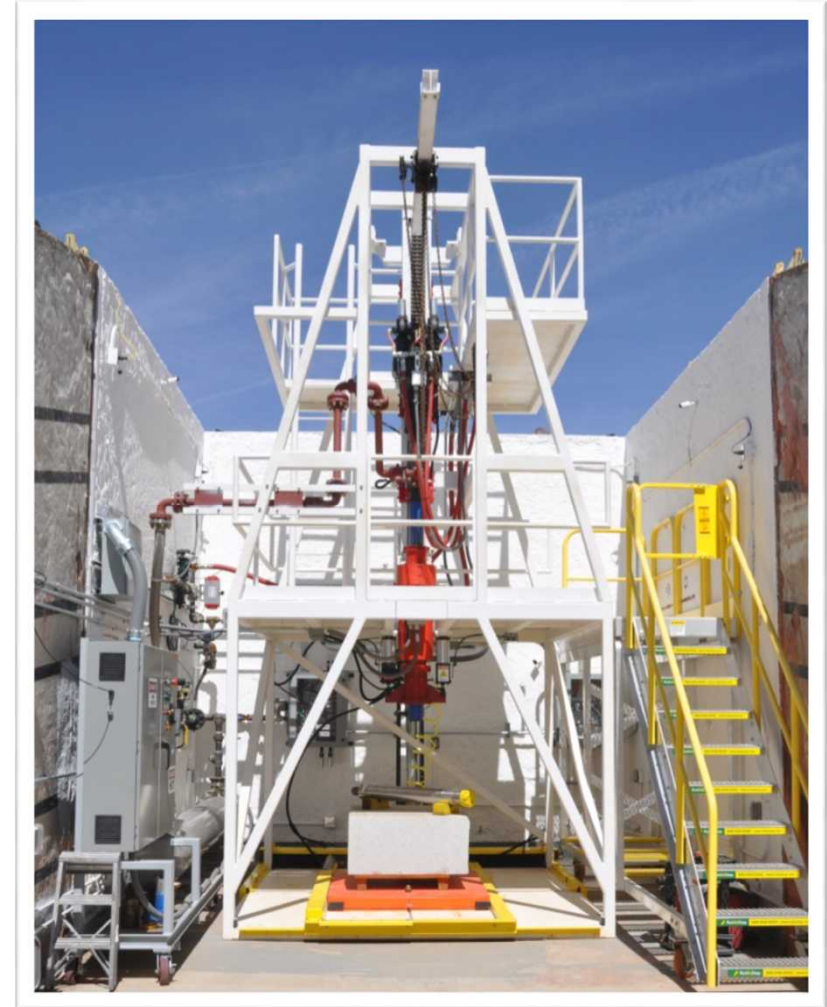
Baseline Results



Conducted at A-C test cell

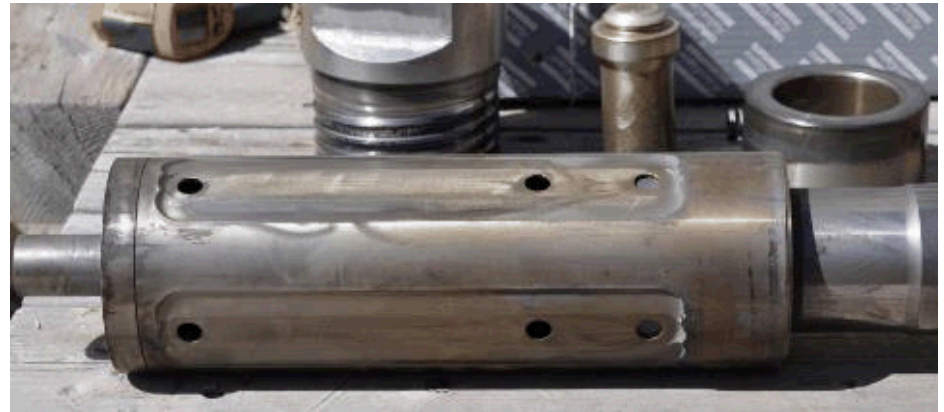
High Operating Temperature Facility Sandia National Laboratories

- Capacities
 - Weight on Bit (WOB) – to 6000 lbf
 - Rotation speed – up to 60 rpm
 - Rotation torque – up to 2500 ft -lbf
 - Hammer heater – up to 300 C (9kW heater)
 - Process gas heater – up to 300C (190 kW heater)
- Features
 - Remote operation
 - Automated drilling
 - Automated rock positioning
 - Closed-loop control of drilling parameters
 - Cuttings collection system with dust washdown
 - Two-stage air filtration



Preliminary HOT Facility Testing

- Validate DAQ
- Verify control system
- Shakedown system



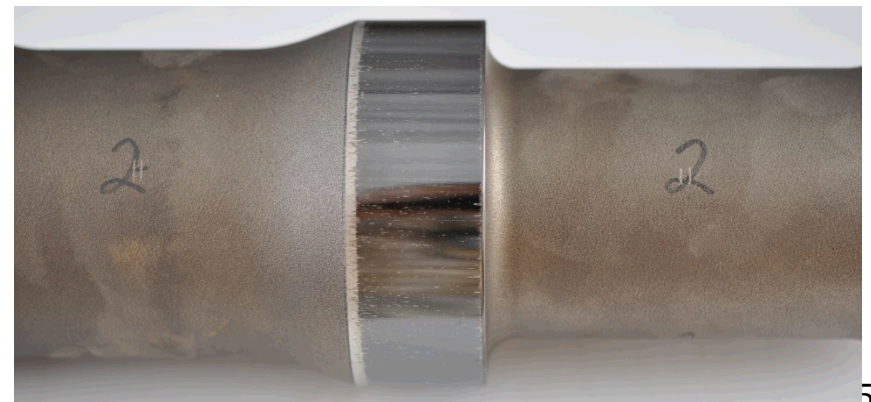
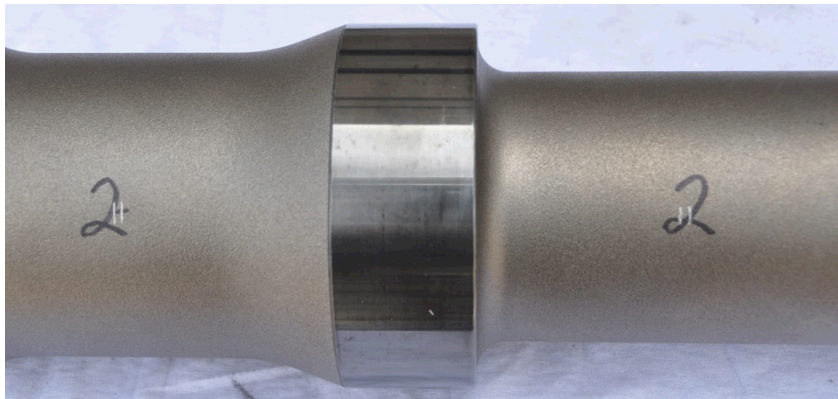
Residual assembly lube after heating to 400°F

Piston #1 (HT Material Candidate)

New

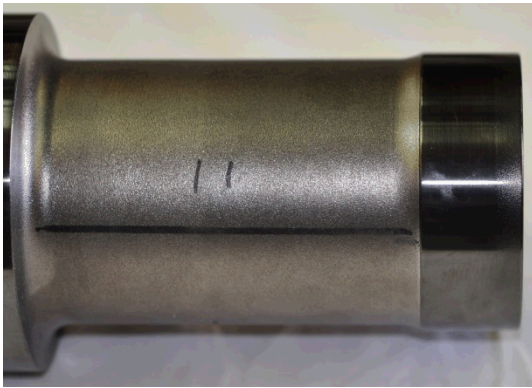


After ~39 ft

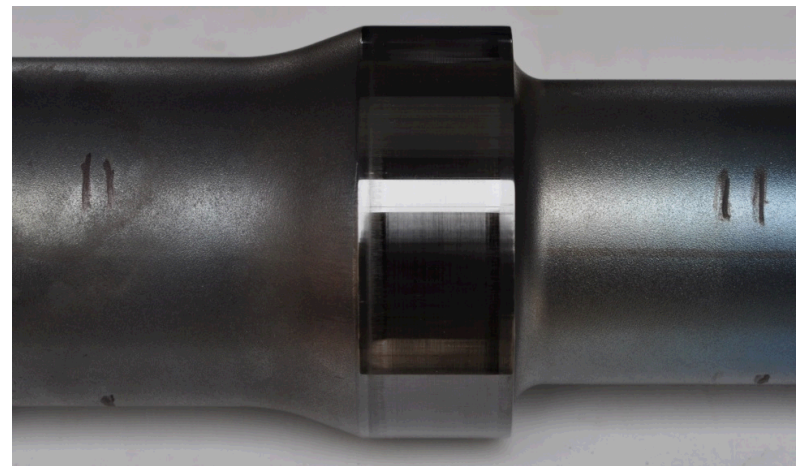
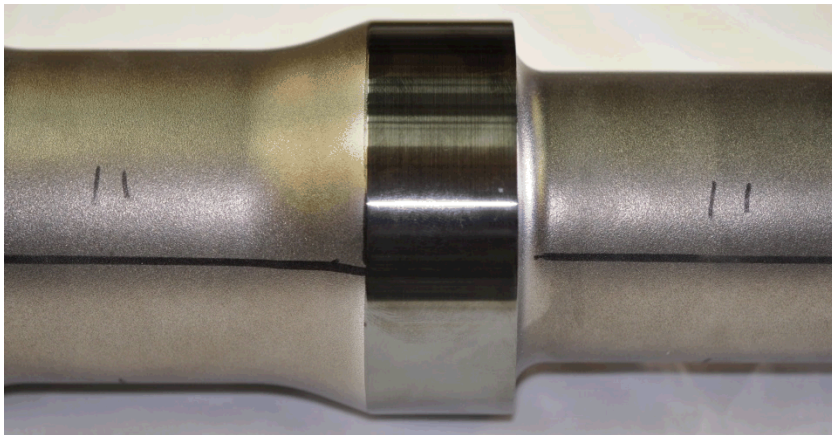
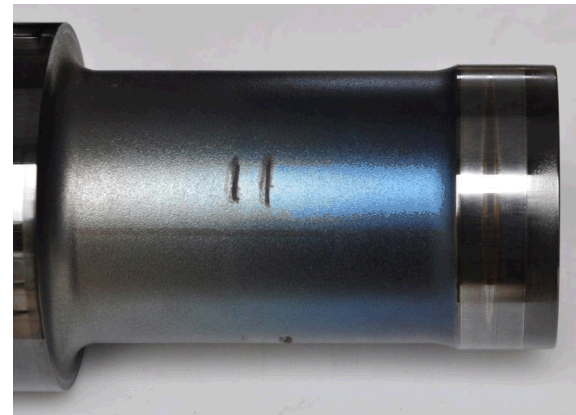


Piston #2 (Alternate Material)

New

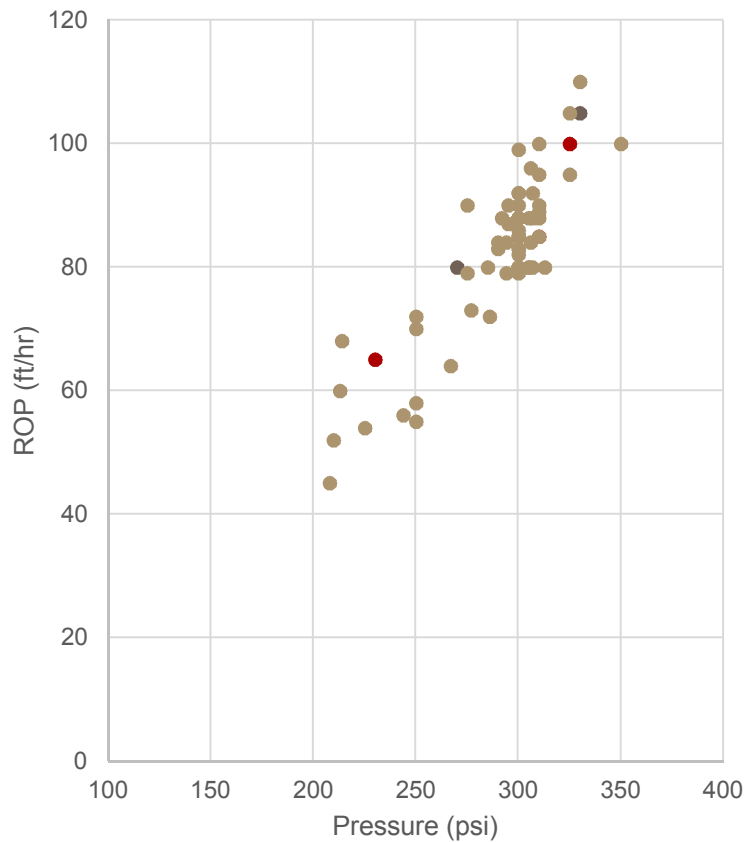


After ~200 ft

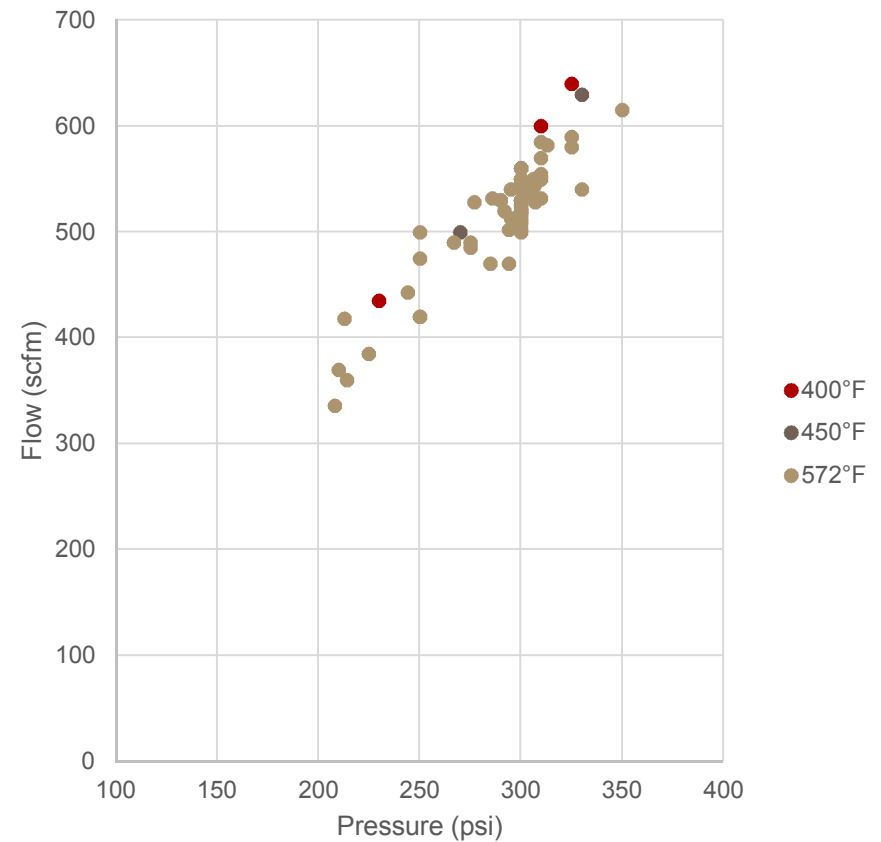


Overall HT Performance

ROP vs. Pressure



Flow vs. Pressure



Results

- Validated HOT Facility performance with Atlas-Copco Roanoke test facility
- Drilling performance evaluated at temperature (~ 300 C)
- Drilling performance in line with expectations
- Achieved target rate of 100 ft/hr at temperature
- Over 200 ft drilled at temperature in lab environment
- Gradual progression of wear on piston stem
- Seeking opportunities to conduct additional field testing

Acknowledgements

- Sandia National Labs
 - Doug Blankenship, Jeff Greving, Elton Wright, Dennis King, Anirban Mazumdar, Dennis King, Anirban Mazumdar, Steve Buerger, Rand Garfield, Lisa Deibler, and Carlos Medrano
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Questions?

